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Forsmark site investigation

Single-hole injection tests in borehole KFM09A

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March 2006

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Abstract

Borehole KFM09A is a deep core-drilled borehole within the site investigations in the Forsmark area. The borehole is inclined, c 60 degrees from the horizontal plane, about 800 m long and grouted to a depth of about 108 m. The borehole diameter is 77.3 mm.

This report presents injection tests performed using the pipe string system PSS3 in borehole KFM09A and the test results.

The main aim of the injection tests in KFM09A was to characterize the hydraulic conditions of the rock adjacent to the borehole on different measurement scales (100 m, 20 m and 5 m). Hydraulic parameters such as transmissivity and hydraulic conductivity were determined using analysis methods for stationary as well as transient conditions together with the dominating flow regime and possible outer hydraulic boundaries.

The injection tests gave consistent results on the different measurement scales regarding transmissivity. During most of the tests, some period with pseudo-radial flow could be identified from the injection period, making a relatively straight-forward transient evaluation possible. However, the recovery periods in KFM09A were often strongly affected by wellbore storage, making a transient evaluation of this period more difficult.

The total transmissivity in KFM09A is dominated by the sections 166.0–171.0 m and 431.0–436.0 m. Together these two sections contribute to about half the transmissivity of the entire borehole.

The injection tests provide a database for statistical analysis of the hydraulic conductivity distribution along the borehole on the different measurement scales. Basic statistical parameters are presented in this report.

Sammanfattning

Borrhål KFM09A är ett djupt kärnborrhål inom platsundersökningarna i Forsmarksområdet. Borrhålet är ca 800 m långt, lutar ca 60 grader från horisontalplanet och har injekterats till ca 108 m längd. Borrhålsdiametern är 77,3 mm.

Denna rapport beskriver genomförda injektionstester med rörgångssystemet PSS3 i borrhål KFM09A samt resultaten från desamma.

Huvudsyftet med injektionstesterna var att karaktärisera de hydrauliska förhållandena av berget i anslutning till borrhålet i olika mätskalor (100 m, 20 m och 5 m). Hydrauliska parametrar såsom transmissivitet och hydraulisk konduktivitet bestämdes med hjälp av analysmetoder för såväl stationära som transienta förhållanden tillsammans med dominerande flödesregim och eventuella yttre hydrauliska randvillkor.

Injektionstesterna gav samstämmiga resultat för de olika mätskalorna beträffande transmissivitet. Under de flesta tester kunde en viss period med pseudoradiellt flöde identifieras från flödesperioden, vilket möjliggjorde en standardmässig transient utvärdering. Återhämtningsperioden i KFM09A var däremot ofta starkt påverkad av brunnsmagasinseffekter, vilket gjorde en unik transient utvärdering av denna period svårare. Den totala transmissiviteten i KFM09A domineras av sektionerna 166,0–171,0 m och 431,0–436,0 m. Tillsamans utgör de nästan hälften av den totala transmissiviteten i hela borrhålet.

Resultaten från injektionstesterna utgör en databas för statistisk analys av den hydrauliska konduktivitetens fördelning längs borrhålet i de olika mätskalorna. Viss statistisk analys har utförts inom ramen för denna aktivitet och grundläggande statistiska parametrar presenteras i rapporten.

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1 Introduction

The injection tests in borehole KFM09A at Forsmark, Sweden, were carried out during November and December of 2005 by Geosigma AB. The borehole KFM09A is a deep cored borehole within the on-going site investigation in the Forsmark area. The borehole is about 800 m long and cased from the top down to about 8 m borehole length a stainless steelpipe with an inner diameter of 78 mm. From 8 m down to the bottom the diameter is 77.3 mm and from 8 m to about 108 m the hole is grouted. The borehole is inclined, c 60 degrees from the horizontal plane, and the location of the borehole is shown in Figure 1-1.

This document reports the results obtained from the injection tests in borehole KFM09A. The activity is performed within the Forsmark site investigation. The work was carried out in compliance with the SKB internal controlling documents presented in Table 1-1. Data and results were delivered to the SKB site characterization database.

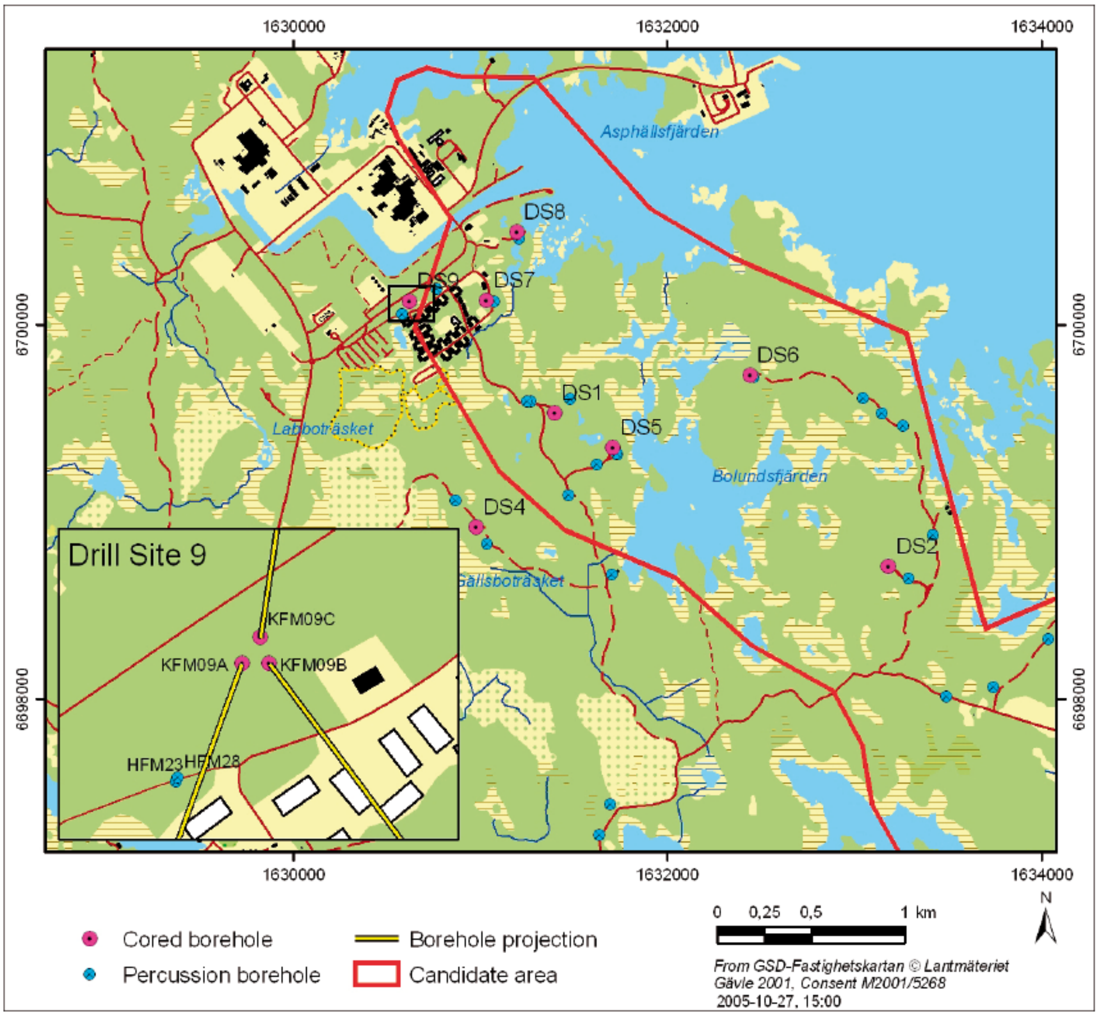

Figure 1-1. *The investigation area at Forsmark including the candidate area selected for more detailed investigations. Borehole KFM09A is situated at drill site DS9.*

Table 1-1. SKB internal controlling documents for performance of the activity.

Activity Plans	Number	Version
Hydraulic injection tests in borehole KFM09A with PSS3	AP PF 400-05-104	1.0
Method descriptions	**Number**	**Version**
Mätsystembeskrivning (MSB) – Allmän del. Pipe String System (PSS3)	SKB MD 345.100	1.0
Mätsystembeskrivning för: Kalibrering, PSS3	SKB MD 345.122	1.0
Mätsystembeskrivning för: Skötsel, service, serviceprotokoll, PSS3	SKB MD 345.124	1.0
Metodbeskrivning för hydrauliska injektionstester	SKB MD 323.001	1.0
Instruktion för analys av injektions- och enhålspumptester	SKB MD 320.004	1.0
Instruktion för rengöring av borrhålsutrustning och viss markbaserad utrustning	SKB MD 600.004	1.0

2 Objectives

The main aim of the injection tests in borehole KFM09A was to characterize the hydraulic properties of the rock adjacent to the borehole on different measurement scales (100 m, 20 m and 5 m). The primary parameter to be determined was hydraulic transmissivity from which hydraulic conductivity can be derived. The results of the injection tests provide a database which can be used for statistical analyses of the hydraulic conductivity distribution along the borehole on different measurement scales. Basic statistical analyses are presented in this report.

Other hydraulic parameters of interest were flow regimes and outer hydraulic boundaries. These parameters were analysed using transient evaluation on the test responses during the flow- and recovery periods.

3 Scope

3.1 Borehole data

Technical data of the tested borehole are shown in Table 3-1 and in Appendix 4. The reference point of the boreholes is defined as the centre of top of casing (ToC), given as "Elevation" in the table below. The Swedish National coordinate system (RT90) is used for the horizontal coordinates together with RHB70 for the elevation. "Northing" and "Easting" refer to the top of the boreholes.

Table 3-1. Technical data of borehole KFM09A (printout from SKB database, SICADA).

Borehole length (m):	799.67				
Drilling Period(s):	**From Date**	**To Date**	**Secup(m)**	**Seclow(m)**	**Drilling Type**
	2005-09-05	2005-10-27	0.000	799.67	Core drilling
Starting point coordinate:	**Length(m)**	**Northing(m)**	**Easting(m)**	**Elevation**	**Coord System**
	0.000	6700115.04	1630647.50	4.29	RT90-RHB70
Angles:	**Length(m)**	**Bearing**	**Inclination (– = down)**		
	0.000	200.08	–59.46		
Borehole diameter:	**Secup(m)**	**Seclow(m)**	**Hole Diam(m)**		
	0.000	799.67	0.0773		

3.2 Tests performed

The injection tests in borehole KFM09A, performed according to Activity Plan AP PF 400-05-104 (see Table 1-1), are listed in Table 3-2. The injection tests were carried out with the Pipe String System (PSS3). The test procedure and the equipment is described in the measurement system description for PSS (SKB MD 345.100) and in the corresponding method descriptions for hydraulic injection tests (SKB MD 323.001, Table 1-1).

Some of the tests were not performed as intended because the time required for achieving a constant head in the test section was judged to be too long or, in other cases, equipment malfunctions caused pressure and/or flow rate disturbances. Whenever such disturbances were expected to affect data evaluation, the test was repeated. Test number (Test no in Table 3-2) refers to the number of tests performed in the actual section. For evaluation, only data from the last test in each section were used.

Table 3-2. Single-hole injection tests performed in borehole KFM09A.

Borehole Bh ID	Test section secup	seclow	Section length	Test type[1)] (1–6)	Test no.	Test start date, time YYYYMMDD hh:mm	Test stop date, time YYYYMMDD hh:mm
KFM09A	106	206	100	3	1	20051117 16:09	20051117 17:59
KFM09A	206	306	100	3	1	20051117 19:03	20051117 20:53
KFM09A	306	406	100	3	1	20051117 21:47	20051117 23:36
KFM09A	406	506	100	3	1	20051118 09:59	20051118 11:49
KFM09A	506	606	100	3	2	20051121 12:52	20051121 15:13
KFM09A	606	706	100	3	1	20051121 06:14	20051121 08:03
KFM09A	691	791	100	3	1	20051121 08:51	20051121 10:40
KFM09A	106	126	20	3	1	20051128 16:44	20051128 18:19
KFM09A	126	146	20	3	1	20051129 06:29	20051129 07:43
KFM09A	146	166	20	3	1	20051129 08:20	20051129 09:35
KFM09A	166	186	20	3	1	20051129 10:00	20051129 11:15
KFM09A	186	206	20	3	1	20051129 12:14	20051129 13:31
KFM09A	206	226	20	3	1	20051129 14:01	20051129 14:47
KFM09A	226	246	20	3	1	20051129 15:38	20051129 16:56
KFM09A	238	258	20	3	1	20051129 17:18	20051129 18:37
KFM09A	258	278	20	3	1	20051129 18:58	20051129 20:17
KFM09A	278	298	20	3	1	20051129 21:03	20051129 22:25
KFM09A	286	306	20	3	1	20051129 22:41	20051129 23:57
KFM09A	306	326	20	3	1	20051130 06:29	20051130 07:48
KFM09A	326	346	20	3	1	20051130 08:16	20051130 09:35
KFM09A	346	366	20	3	1	20051130 10:06	20051130 11:22
KFM09A	366	386	20	3	1	20051130 12:06	20051130 13:23
KFM09A	386	406	20	3	1	20051130 13:50	20051130 15:08
KFM09A	406	426	20	3	1	20051130 15:30	20051130 16:47
KFM09A	426	446	20	3	2	20051130 18:18	20051130 19:38
KFM09A	446	466	20	3	1	20051130 20:03	20051130 21:45
KFM09A	466	486	20	3	1	20051130 22:03	20051130 23:20
KFM09A	486	506	20	3	1	20051201 08:06	20051201 09:34
KFM09A	506	526	20	3	1	20051201 10:01	20051201 11:22
KFM09A	526	546	20	3	1	20051201 11:41	20051201 13:46
KFM09A	545	565	20	3	1	20051201 14:21	20051201 15:09
KFM09A	566	586	20	3	1	20051201 15:34	20051201 16:17
KFM09A	586	606	20	3	1	20051202 07:55	20051202 08:37
KFM09A	606	626	20	3	1	20051202 08:58	20051202 10:22
KFM09A	626	646	20	3	1	20051202 10:43	20051202 12:05
KFM09A	646	666	20	3	1	20051202 13:12	20051202 14:35
KFM09A	666	686	20	3	1	20051202 14:57	20051202 16:13
KFM09A	686	706	20	3	1	20051205 08:22	20051205 09:53
KFM09A	691	711	20	3	1	20051205 10:10	20051205 11:12
KFM09A	711	731	20	3	1	20051205 12:46	20051205 13:30
KFM09A	731	751	20	3	1	20051205 13:49	20051205 15:12
KFM09A	751	771	20	3	1	20051205 15:30	20051205 16:54
KFM09A	771	791	20	3	1	20051205 18:09	20051205 19:26
KFM09A	106	111	5	3	1	20051207 07:32	20051207 08:52
KFM09A	111	116	5	3	1	20051207 09:08	20051207 10:24
KFM09A	116	121	5	3	2	20051221 15:48	20051208 17:51
KFM09A	121	126	5	3	1	20051207 12:52	20051207 14:09
KFM09A	126	131	5	3	1	20051207 14:26	20051207 16:04
KFM09A	128	133	5	3	1	20051207 16:21	20051207 17:40
KFM09A	133	138	5	3	1	20051207 17:58	20051207 19:16
KFM09A	138	143	5	3	1	20051207 19:42	20051207 21:13

Borehole Bh ID	Test section secup	seclow	Section length	Test type[1)] (1–6)	Test no.	Test start date, time YYYYMMDD hh:mm	Test stop date, time YYYYMMDD hh:mm
KFM09A	141	146	5	3	1	20051207 21:27	20051207 22:45
KFM09A	146	151	5	3	1	20051207 23:02	20051208 00:17
KFM09A	151	156	5	3	1	20051208 06:16	20051208 06:59
KFM09A	156	161	5	3	1	20051208 07:10	20051208 08:26
KFM09A	161	166	5	3	1	20051208 08:36	20051208 09:52
KFM09A	166	171	5	3	1	20051208 10:03	20051208 11:19
KFM09A	171	176	5	3	1	20051208 12:12	20051208 13:29
KFM09A	176	181	5	3	1	20051208 13:43	20051208 14:57
KFM09A	181	186	5	3	1	20051208 15:13	20051208 16:28
KFM09A	186	191	5	3	1	20051208 16:36	20051208 17:51
KFM09A	191	196	5	3	1	20051208 18:03	20051208 18:50
KFM09A	196	201	5	3	1	20051208 19:02	20051208 19:47
KFM09A	201	206	5	3	1	20051208 19:57	20051208 20:39
KFM09A	226	231	5	3	1	20051208 20:58	20051208 21:40
KFM09A	232	237	5	3	1	20051208 21:54	20051208 23:08
KFM09A	237	242	5	3	1	20051208 23:21	20051209 00:35
KFM09A	240.8	245.8	5	3	1	20051209 08:08	20051209 09:24
KFM09A	246.8	251.8	5	3	1	20051221 13:55	20051221 14:35
KFM09A	251.5	256.5	5	3	1	20051209 09:40	20051209 10:22
KFM09A	256.5	261.5	5	3	1	20051209 10:34	20051209 11:18
KFM09A	273	278	5	3	1	20051209 11:30	20051209 13:22
KFM09A	278	283	5	3	1	20051209 13:34	20051209 14:48
KFM09A	283	288	5	3	1	20051209 15:04	20051209 15:51
KFM09A	288	293	5	3	1	20051209 16:00	20051209 17:15
KFM09A	293	298	5	3	1	20051212 08:21	20051212 09:42
KFM09A	296	301	5	3	1	20051221 12:39	20051221 13:28
KFM09A	301	306	5	3	1	20051221 11:45	20051221 12:29
KFM09A	306	311	5	3	1	20051212 09:58	20051212 10:39
KFM09A	311	316	5	3	1	20051212 10:49	20051212 12:33
KFM09A	316	321	5	3	1	20051212 12:43	20051212 13:31
KFM09A	321	326	5	3	1	20051212 13:44	20051212 15:02
KFM09A	346	351	5	3	1	20051212 15:31	20051212 16:14
KFM09A	351	356	5	3	1	20051221 10:04	20051221 11:19
KFM09A	356	361	5	3	1	20051221 08:54	20051221 09:50
KFM09A	361	366	5	3	1	20051221 07:28	20051221 08:43
KFM09A	363	368	5	3	1	20051212 16:39	20051212 17:54
KFM09A	368	373	5	3	1	20051213 06:27	20051213 07:24
KFM09A	371	376	5	3	1	20051213 07:35	20051213 08:48
KFM09A	376	381	5	3	1	20051213 09:02	20051213 09:58
KFM09A	381	386	5	3	1	20051213 10:10	20051213 11:25
KFM09A	386	391	5	3	1	20051213 11:57	20051213 13:16
KFM09A	391	396	5	3	1	20051213 13:28	20051213 14:48
KFM09A	396	401	5	3	1	20051213 15:06	20051213 15:49
KFM09A	401	406	5	3	1	20051213 16:00	20051213 17:15
KFM09A	406	411	5	3	1	20051213 17:25	20051213 18:18
KFM09A	411	416	5	3	1	20051213 18:36	20051213 19:50
KFM09A	414	419	5	3	1	20051213 20:06	20051213 21:22
KFM09A	419	424	5	3	1	20051213 21:32	20051213 22:46
KFM09A	421	426	5	3	1	20051213 22:55	20051214 00:09
KFM09A	426	431	5	3	1	20051214 06:51	20051214 07:59
KFM09A	431	436	5	3	1	20051214 08:11	20051214 09:31
KFM09A	436	441	5	3	1	20051214 09:47	20051214 10:29
KFM09A	441	446	5	3	1	20051214 10:44	20051214 12:00

Borehole Bh ID	Test section secup	 seclow	Section length	Test type[1)] (1–6)	Test no.	Test start date, time YYYYMMDD hh:mm	Test stop date, time YYYYMMDD hh:mm
KFM09A	446	451	5	3	1	20051214 12:13	20051214 14:04
KFM09A	451	456	5	3	1	20051214 14:22	20051214 15:38
KFM09A	456	461	5	3	1	20051214 15:55	20051214 17:12
KFM09A	461	466	5	3	1	20051214 17:32	20051214 18:15
KFM09A	471	476	5	3	1	20051214 18:35	20051214 19:50
KFM09A	476	481	5	3	1	20051214 20:01	20051214 21:23
KFM09A	486	491	5	3	1	20051214 21:40	20051214 22:31
KFM09A	491	496	5	3	1	20051214 22:58	20051215 00:12
KFM09A	496	501	5	3	1	20051215 06:33	20051215 07:57
KFM09A	501	506	5	3	1	20051215 08:14	20051215 09:00
KFM09A	506	511	5	3	1	20051220 19:00	20051220 20:23
KFM09A	511	516	5	3	1	20051220 20:50	20051220 22:05
KFM09A	516	521	5	3	1	20051220 22:14	20051220 23:28
KFM09A	521	526	5	3	1	20051215 09:25	20051215 10:11
KFM09A	526	531	5	3	1	20051215 10:26	20051215 11:07
KFM09A	531	536	5	3	1	20051215 11:23	20051215 12:44
KFM09A	536	541	5	3	1	20051215 13:19	20051215 14:03
KFM09A	541	546	5	3	1	20051215 14:14	20051215 15:28
KFM09A	561	566	5	3	1	20051220 17:14	20051220 17:58
KFM09A	606	611	5	3	1	20051215 16:19	20051215 17:00
KFM09A	611	616	5	3	1	20051215 17:19	20051215 18:35
KFM09A	616	621	5	3	1	20051215 18:50	20051215 19:31
KFM09A	621	626	5	3	1	20051215 19:44	20051215 21:03
KFM09A	626	631	5	3	1	20051215 21:14	20051215 22:01
KFM09A	631	636	5	3	1	20051215 22:08	20051215 23:33
KFM09A	636	641	5	3	1	20051215 23:43	20051216 00:58
KFM09A	641	646	5	3	1	20051216 08:21	20051216 09:36
KFM09A	646	651	5	3	1	20051216 09:55	20051216 10:38
KFM09A	651	656	5	3	1	20051216 10:53	20051216 12:10
KFM09A	656	661	5	3	1	20051216 12:21	20051216 13:20
KFM09A	661	666	5	4	1	20051216 13:31	20051216 14:14
KFM09A	731	736	5	3	1	20051219 08:19	20051219 09:01
KFM09A	736	741	5	3	1	20051219 09:15	20051219 09:56
KFM09A	741	746	5	3	1	20051219 10:11	20051219 11:30
KFM09A	746	751	5	3	1	20051219 11:44	20051219 12:36
KFM09A	751	756	5	3	1	20051219 12:50	20051219 14:05
KFM09A	756	761	5	3	1	20051219 14:20	20051219 15:42
KFM09A	761	766	5	3	1	20051219 15:56	20051219 17:16
KFM09A	766	771	5	3	1	20051220 06:55	20051220 08:10
KFM09A	771	776	5	3	1	20051220 08:29	20051220 09:46
KFM09A	776	781	5	3	1	20051220 10:06	20051220 11:24
KFM09A	781	786	5	3	1	20051220 11:35	20051220 12:58
KFM09A	786	791	5	3	1	20051220 13:11	20051220 14:28

[1)] 3: Injection test.

3.3 Equipment checks

The PSS3 equipment was fully serviced, according to SKB internal controlling documents (SKB MD 345.124, service, and SKB MD 345.122, calibration), in May 2005.

Functioning checks of the equipment were performed during the installation of the PSS equipment at the test site. In order to check the function of the pressure sensors, the air pressure was recorded and found to be as expected. While lowering, the sensors showed good agreement with the total head of water ($p/\rho g$). The temperature sensor displayed expected values in the water.

Simple functioning checks of down-hole sensors were done at every change of test section interval. Checks were also made continuously while lowering the pipe string along the borehole.

4 Description of equipment

4.1 Overview

4.1.1 Measurement container

All of the equipment needed to perform the injection tests is located in a steel container (Figure 4-1). The container is divided into two compartments; a data-room and a workshop. The container is placed on pallets in order to obtain a suitable working level in relation to the borehole casing.

The hoisting rig is of a hydraulic chain-feed type. The jaws, holding the pipe string, are opened hydraulically and closed mechanically by springs. The rig is equipped with a load transmitter and the load limit may be adjusted. The maximum load is 22 kN.

The packers and the test valve are operated hydraulically by water filled pressure vessels. Expansion and release of packers, as well as opening and closing of the test valve, is done using magnetic valves controlled by the software in the data acquisition system.

The injection system consists of a tank, a pump and a flow m The injection flow rate may be manually or automatically controlled. At small flow rates, a water filled pressure vessel connected to a nitrogen gas regulator is used instead of the pump.

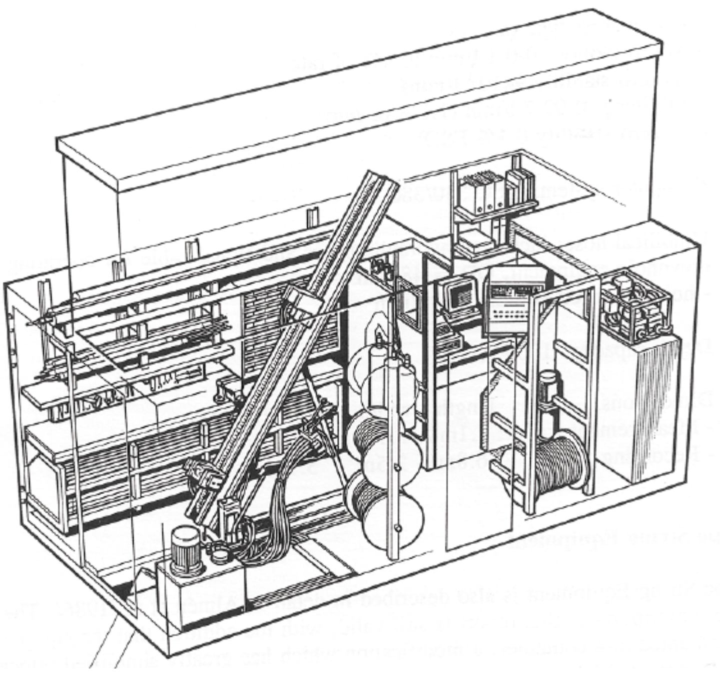

Figure 4-1. *Outline of the PSS3 container with equipment.*

4.1.2 Down-hole equipment

A schematic drawing of the down-hole equipment is shown in Figure 4-2. The pipe string consists of aluminium pipes of 3 m length, connected by stainless steel taps sealed with double o-rings. Pressure is measured above (P_a), within (P) and below (P_b) the test section, which is isolated by two packers. The groundwater temperature in the test section is also measured. The hydraulic connection between the pipe string and the test section can be closed or opened by a test valve operated by the measurement system.

At the lower end of the borehole equipment, a level indicator (calliper type) gives a signal as the reference depth marks along the borehole are passed.

The length of the test section may be varied (5, 20 or 100 m).

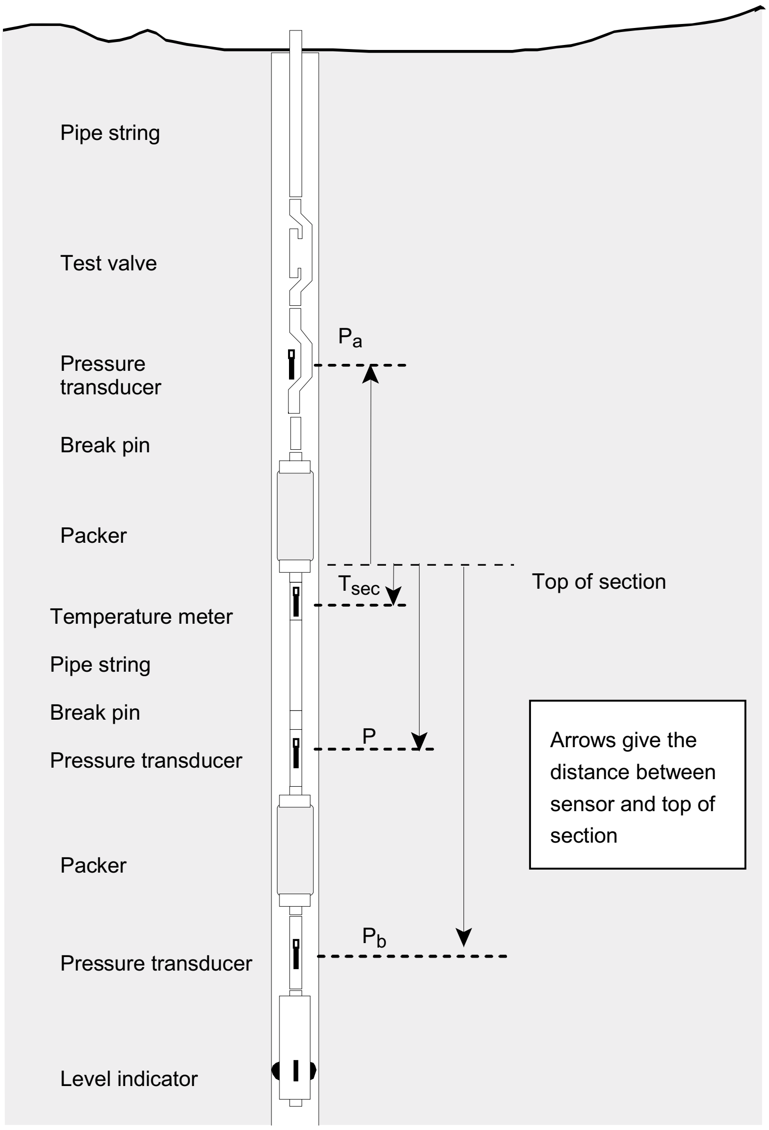

Figure 4-2. *Schematic drawing of the down-hole equipment in the PSS3 system.*

4.2 Measurement sensors

Technical data for the measurement sensors in the PSS system together with corresponding data of the system are shown in Table 4-1. The sensors are components of the PSS system. The accuracy of the PSS system may also be affected by the I/O-unit, cf Figure 4-3, and the calibration of the system.

The sensor positions are fixed relative to the top of the test section. In Table 4-2, the position of the sensors is given with top of test section as reference (Figure 4-2).

Table 4-1. Technical data for sensors together with estimated data for the PSS system (based on current experience).

Technical specification Parameter		Unit	Sensor	PSS	Comments
Absolute pressure	Output signal	mA	4–20		
	Meas. range	MPa	0–13.5		
	Resolution	kPa	< 1.0		
	Accuracy[1)]	% F.S	0.1		
Differential pressure, 200 kPa	Accuracy	kPa		< ±5	Estimated value
Temperature	Output signal	mA	4–20		
	Meas. range	°C	0–32		
	Resolution	°C	< 0.01		
	Accuracy	°C	±0.1		
Flow Qbig	Output signal	mA	4–20		
	Meas. range	m^3/s	$1.67\cdot10^{-5}$–$1.67\cdot10^{-3}$		The specific accuracy is depending on actual flow
	Resolution	m^3/s	$6.7\cdot10^{-8}$		
	Accuracy[2)]	% O.R	0.15–0.3	< 1	
Flow Qsmall	Output signal	mA	4–20		
	Meas. range	m^3/s	$1.67\cdot10^{-8}$–$1.67\cdot10^{-5}$		The specific accuracy is depending on actual flow
	Resolution	m^3/s	$6.7\cdot10^{-10}$		
	Accuracy[3)]	% O.R	0.1–0.4	0.5–20	

1) 0.1% of Full Scale. Includes hysteresis, linearity and repeatability.

2) Maximum error in % of actual reading (% o.r.).

3) Maximum error in % of actual reading (% o.r.). The higher numbers correspond to the lower flow.

Table 4-2. Position of sensors in the borehole and displacement volume of equipment in the test section.

Parameter	Length of test section (m) KFM09A 5	 20	 100
Equipment displacement volume in test section [1)]	3.6	13	61
Total volume of test section [2)]	23.5	93.9	469.3
Position for sensor Pa, pressure above test section, (m above secup) [3)]	1.87	1.88	1.88
Position for sensor P, pressure in test section, (m above secup) [3)]	–4.11	–19.11	–99.12
Position for sensor Tsec, temperature in test section, (m above secup) [3)]	–0.99	–0.99	–0.98
Position for sensor Pb, pressure below test section, (m above secup) [3)]	–6.98	–21.98	–101.99

1) Displacement volume in test section due to pipe string, signal cable, sensors and packer ends (in litre).

2) Total volume of test section (V= section length*π*d^2/4).

3) Position of sensor relative top of test section. A negative value indicates a position below top of test section, (secup).

4.3 Data acquisition system

The data acquisition system in the PSS equipment contains a standard office PC connected to an I/O-unit (Datascan 7320). Using the Orchestrator software, pumping and injection tests are monitored and borehole sensor data are collected. In addition to the borehole parameters, packer and atmospheric pressure, container air temperature and water temperature are logged. Test evaluation may be performed on-site after a conducted test. An external display enables monitoring of test parameters.

The data acquisition system may be used to start and stop the automatic control system (computer and servo motors). These are connected as shown in Figure 4-3. The control system monitors the flow regulator and uses differential pressure across the regulating valve together with pressure in test section as input signals.

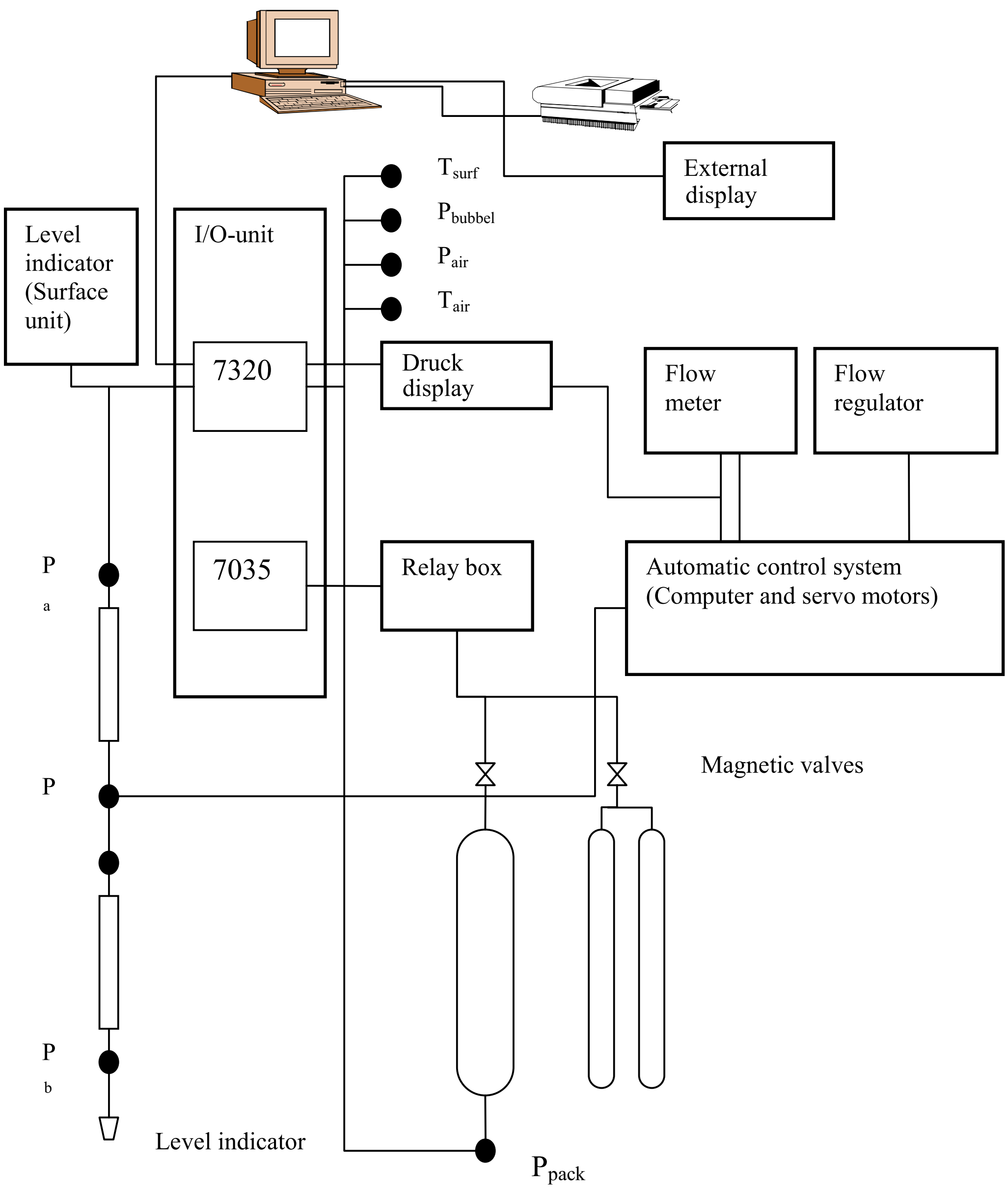

Figure 4-3. Schematic drawing of the data acquisition system and the automatic control system in PSS.

5 Execution

5.1 Preparation

5.1.1 Calibration

All sensors included in PSS are calibrated at the Geosigma engineering service station in Uppsala. Calibration is generally performed at least every year. Results from calibration, e.g. calibration constants, of sensors are kept in a document folder in PSS. If a sensor is replaced at the test site, calibration constants are altered as well. If a new, un-calibrated, sensor is to be used, calibration may be performed afterwards and data re-calculated.

5.1.2 Functioning checks

Equipment functioning checks were performed during the establishment of PSS at the test site. Simple function checks of down-hole sensors were done at every change of test section length, as well as while lowering the pipe string along the borehole.

5.1.3 Cleaning of equipment

Cleaning of the borehole equipment was performed according to the cleaning instruction (SKB MD 600.004, see Table 1-1), level 1.

5.2 Test performance

5.2.1 Test principle

The injection tests in KFM09A were carried out while maintaining a constant head of generally 200 kPa (20 m) in the test section. Before start of the injection period, approximately steady-state pressure conditions prevailed in the test section. After the injection period, the pressure recovery was measured.

For injection tests with 20 m and 5 m section length, the injection phase was interrupted if the injection flow was clearly below the measurement limit. Thereafter, the recovery was measured for at least 5 minutes to verify the low conductivity of the section.

5.2.2 Test procedure

Generally, the tests were performed according to the Activity Plan AP PF 400-05-104. Exceptions to this are presented in Section 5.5.

A test cycle includes the following phases: 1) Transfer of down-hole equipment to the next section, 2) Packer inflation, 3) Pressure stabilisation, 4) Injection, 5) Pressure recovery and 6) Packer deflation.

The estimated times for the various phases are presented in Table 5-1. Regarding the packer inflation times and actual injection and recovery times, slightly different procedures were used for the tests in 100 m sections compared to the tests in 20 m and 5 m sections in accordance with AP PF 400-05-104. Furthermore, slightly longer test times were used for the tests in 100 m sections, cf Table 5-1.

Table 5-1. Packer inflation times, pressure stabilisation times and test times used for the injection tests in KFM09A.

Test section length (m)	Packer inflation time (min)	Time for pressure stabilisation (min)	Injection period (min)	Recovery period (min)	Total time/test (min)[1)]
100	30	15	30	30	105
20	25	5	20	20	70
5	25	5	20	20	70

[1)] Exclusive of trip times in the borehole.

5.2.3 Test strategy

Firstly, injection tests in 100 m sections were performed in KFM09A in the interval 106. 0–791.0 m.

Secondly, injection tests in 20 m sections were carried out in the same interval, 106.0–791.0 m, since a detectable flow was found in every 100 m section. The 100 m sections were measured in five successive injection tests using a 20 m section length. Due to large fractures or cavities in the borehole, the positions of the packers had to be shifted in the section 206.0–306.0. This section was therefore measured with six injection tests with 20 m section length instead of five. As a result some of these 20 m sections are partly overlapping.

Finally, injection tests with 5 m section length were conducted in the 20 m sections who had a definable flow rate. These sections were 106–206 m, 226–326 m, 346–545 m, 606–666 m and 731–791 m. Four tests using a 5 m section length were performed within 20 m intervals with a few exceptions due to major fractures making it impossible to place the packers at the proper positions. Hence, some of the 5 m sections are partly overlapping.

In order to save time some other 20 m-sections with low but detectable flow were picked out. In these 20 m intervals, the 5 m sections assumed to contain the dominating flows (i.e. fractures) were chosen to be tested on the way down in the hole. The selection of these 5 m was based on visual inspection of BIPS images. If the flow measured in the 20- and 100 m sections didn't appear in the chosen 5 m sections, the other 5 m tests were conducted on the way up in the hole.

Since the results of the tests in 100 m sections would have a strong effect on the continued test program (i.e. whether a 100 m section would be measured with shorter sections as well), it was particularly important to ensure reliable results of these tests regarding sections close to the lower measurement limit.

The total number of injection tests was, as explained by the test strategy, dependent on the results of the previous tests.

5.3 Data handling

With the PSS system, primary data are handled using the Orchestrator software (Version 2.3.8). During a test, data are continuously logged in *.odl-files. After the test is finished, a report file (*.ht2) with space separated data is generated. The *.ht2-file (mio-format) contains logged parameters as well as test-specific information, such as calibration constants and background data. The parameters are presented as percentage of sensor measurement range and not in engineering units. The report file in ASCII-format is the raw data file delivered to the data base SICADA.

The *.ht2-files are automatically named with borehole id, top of test section and date and time of test start (as for example __KFM09A_0106.00_200511171609.ht2). The name differs slightly from the convention stated in Instruction for analysis of injection and single-hole pumping tests, SKB MD 320.004.

Using the IPPLOT software (Version 3.0), the *.ht2-files are converted to parameter files suitable for plotting using the code SKB-plot and analysis with the AQTESOLV software.

A backup of data files was created on a regular basis by CD-storage and by sending the files to the Geosigma office in Uppsala by a file transfer protocol. A file description table is presented in Appendix 1.

5.4 Analysis and interpretation

5.4.1 General

As described in Section 5.2.1, the injection tests in KFM09A were performed as transient constant head tests followed by a pressure recovery period. From the injection period, the (reciprocal) flow rate versus time was plotted in log-log and lin-log diagrams together with the corresponding derivative. From the recovery period, the pressure was plotted versus Agarwal equivalent time in lin-log and log-log diagrams, respectively, together with the corresponding derivative. The routine data processing of the measured data was done according to the Instruction for analysis of injection and single-hole pumping tests (SKB MD 320.004, see Table 1-1).

For evaluation of the test data, no corrections of the measured flow rate and absolute pressure data (e.g. due to barometric pressure variations or tidal fluctuations) have been made. For short-time single-hole tests, such corrections are generally not needed, unless very small pressure changes are applied. No subtraction of the barometric pressure from the measured absolute pressure has been made, since the length of the test periods are short relative to the time scale for barometric pressure changes. In addition, pressure differences rather than the pressure magnitudes are used by the evaluation.

5.4.2 Measurement limit for flow rate and specific flow rate

The estimated standard lower measurement limit for flow rate for injection tests with PSS is c 1 mL/min ($1.7 \cdot 10^{-8}$ m^3/s). However, if the flow rate for a test was close to, or below, the standard lower measurement limit, a test-specific estimate of the lower measurement limit of flow rate was made. The test-specific lower limit was based on the measurement noise level of the flow rate before and after the injection period. The decisive factor for the varying lower measurement limit is not identified, but it might be of both technical and hydraulic character. For approximately 40 per cent of the injection tests in KFM09A, the actual lower measurement limit of the flow rate was estimated ranging from $2.8 \cdot 10^{-9}$ m^3/s to $6.5 \cdot 10^{-9}$ m^3/s.

The lower measurement limit for transmissivity is defined in terms of the specific flow rate (Q/s). The minimum specific flow rate corresponds to the estimated lower measurement limit of the flow rate together with the actual injection pressure during the test, see Table 5-2. The intention during this test campaign was to use a standard injection pressure of 200 kPa (20 m water column). However, for some test sections in KFM09A, the actual injection pressure was considerably different. The highest injection pressure during the tests in KFM09A was 300 kPa and for eight of the tests the injection pressure was below 100 kPa. A low injection pressure is often the result of a test section of low conductivity due to a pressure increase, caused by packer expansion, before the injection start. A highly conductive section may also result in a low injection pressure due to limited flow capacity of PSS. The estimated test specific lower measurement limit for the specific flow rate in KFM09A ranged from $1.4 \cdot 10^{-10}$ m^2/s to $4.9 \cdot 10^{-10}$ m^2/s.

Table 5-2. Estimated lower measurement limit for specific flow rate and steady-state transmissivity for different injection pressures, measurement scales and estimated lower measurement limits for flow rate for the injection tests in borehole KFM09A.

r_w (m)	L_w (m)	Q-measl–L (m^3/s)	Injection pressure (kPa)	Q/s-measl–L (m^2/s)	Factor C_M in Moye's formula	TM-measl–L (m^2/s)
0.0385	100	1.7E–08	100	1.6E–09	1.30	2.1E–09
0.0385	100	1.7E–08	200	8.2E–10	1.30	1.1E–09
0.0385	100	1.7E–08	300	5.5E–10	1.30	7.1E–10
0.0385	100	1.2E–08	100	1.1E–09	1.30	1.5E–09
0.0385	100	1.2E–08	200	5.7E–10	1.30	7.4E–10
0.0385	100	1.2E–08	300	3.8E–10	1.30	5.0E–10
0.0385	100	5.0E–09	100	4.9E–10	1.30	6.4E–10
0.0385	100	5.0E–09	200	2.5E–10	1.30	3.2E–10
0.0385	100	5.0E–09	300	1.6E–10	1.30	2.1E–10
0.0385	20	1.7E–08	100	1.6E–09	1.04	1.7E–09
0.0385	20	1.7E–08	200	8.2E–10	1.04	8.5E–10
0.0385	20	1.7E–08	300	5.5E–10	1.04	5.7E–10
0.0385	20	1.2E–08	100	1.1E–09	1.04	1.2E–09
0.0385	20	1.2E–08	200	5.7E–10	1.04	6.0E–10
0.0385	20	1.2E–08	300	3.8E–10	1.04	4.0E–10
0.0385	20	5.0E–09	100	4.9E–10	1.04	5.1E–10
0.0385	20	5.0E–09	200	2.5E–10	1.04	2.6E–10
0.0385	20	5.0E–09	300	1.6E–10	1.04	1.7E–10
0.0385	5	1.7E–08	100	1.6E–09	0.82	1.3E–09
0.0385	5	1.7E–08	200	8.2E–10	0.82	6.7E–10
0.0385	5	1.7E–08	300	5.5E–10	0.82	4.5E–10
0.0385	5	1.2E–08	100	1.1E–09	0.82	9.4E–10
0.0385	5	1.2E–08	200	5.7E–10	0.82	4.7E–10
0.0385	5	1.2E–08	300	3.8E–10	0.82	3.1E–10
0.0385	5	5.0E–09	100	4.9E–10	0.82	4.0E–10
0.0385	5	5.0E–09	200	2.5E–10	0.82	2.0E–10
0.0385	5	5.0E–09	300	1.6E–10	0.82	1.3E–10

Whenever the final flow rate (Q_p) was not defined (i.e. not clearly above the measurement noise before and after the injection period), the estimated lower measurement limit for specific flow rate was based on the estimated lower measurement limit for flow rate for the specific test and a standard injection pressure of 200 kPa. This is done in order to avoid excessively high, apparent estimates of the specific flow rate for these low conductivity sections, which would have resulted if the actual pressure difference at start of injection had been used as injection pressure (since the actual pressure difference often was significantly less than 200 kPa, see above).

The lower measurement limits for the flow rate correspond to different values of steady-state transmissivity, T_M, depending on the section lengths used in the factor C_M in Moye's formula, as described in the Instruction for analysis of injection and single-hole pumping tests (SKB MD 320.004), see Table 5-2.

The practical upper measurement limit of hydraulic transmissivity for the PSS system is estimated at a flow rate of c 30 L/min ($5 \cdot 10^{-4}$ m^3/s) and an injection pressure of c 1 m. Thus, the upper measurement limit for the specific flow rate is $5 \cdot 10^{-4}$ m^2/s. However, the practical upper measurement limit may vary, depending on e.g. depth of the test section (friction losses in the pipe string).

5.4.3 Qualitative analysis

Initially, a qualitative evaluation of actual flow regimes, e.g. wellbore storage (WBS), pseudo-radial flow regime (PRF), pseudo-spherical flow regime (PSF) and pseudo-stationary flow regime (PSS), respectively, was performed. In addition, indications of outer boundary conditions during the tests were identified. The qualitative evaluation was mainly interpreted from the log-log plots of flow rate and pressure together with the corresponding derivatives.

In particular, time intervals with pseudo-radial flow, reflected by a constant (horizontal) derivative in the test diagrams, were identified. Pseudo-linear flow may, at the beginning of the test, be reflected by a straight line of slope 0.5 or less in log-log diagrams, both for the measured variable (flow rate or pressure) and the derivative. A true spherical flow regime is reflected by a straight line with a slope of –0.5 for the derivative. However, other slopes may indicate transitions to pseudo-spherical (leaky) or pseudo-stationary flow. The latter flow regime corresponds to almost stationary conditions with a derivative approaching zero.

The interpreted flow regimes can also be described in terms of the distance from the borehole:

- **Inner zone:** Representing very early responses that may represent the fracture properties close to the borehole which may possibly be affected by turbulent head losses. These properties are generally reflected by the skin factor.
- **Middle zone:** Representing the first response from which it is considered possible to evaluate the hydraulic properties of the formation close to the borehole.
- **Outer zone:** Representing the response at late times of hydraulic structure(s) connected to the hydraulic feature for the middle zone. Sometimes it is possible to deduce the character of the actual feature or boundary and evaluate the hydraulic properties.

Due to the limited resolution of the flow m and pressure sensor, the derivative may some times indicate a false horizontal line by the end of periods with pseudo-stationary flow. Apparent no-flow (NFB) and constant head boundaries (CHB), or equivalent boundary conditions of fractures, are reflected by an increase/decrease of the derivative, respectively.

5.4.4 Quantitative analysis

A preliminary steady-state analysis of transmissivity according to Moye's formula (denoted T_M) was made for the injection period for all tests in conjunction with the qualitative analysis according to the following equation:

$$T_M = \frac{Q_p \cdot \rho_w \cdot g}{dp_p} \cdot C_M \qquad (5\text{-}1)$$

$$C_M = \frac{1 + \ln\left(\frac{L_w}{2r_w}\right)}{2\pi} \qquad (5\text{-}2)$$

Q_p = flow rate by the end of the flow period (m^3/s)
ρ_w = density of water (kg/m^3)
g = acceleration of gravity (m/s^2)
C_M = geometrical shape factor (–)
dp_p = $p_p - p_i$ (Pa)
r_w = borehole radius (m)
L_w = section length (m)

From the results of the qualitative evaluation, appropriate interpretation models for the quantitative evaluation of the tests were selected. When possible, transient analysis was made on both the injection and recovery periods of the tests.

The transient analysis was performed using a special version of the test analysis software AQTESOLV, which enables both visual and automatic type curve matching. The quantitative transient evaluation is generally carried out as an iterative process of manual type curve matching and automatic matching. For the injection period, a model based on the Jacob and Lohman (1952) solution /1/ was applied for estimating the transmissivity and skin factor for an assumed value on the storativity when a certain period with pseudo-radial flow could be identified. The model is based on the effective wellbore radius concept to account for non-zero (negative) skin factors according to Hurst, Clark and Brauer (1969) /2/.

In borehole KFM09A, the storativity was calculated using an empirical regression relationship between storativity and transmissivity, see Equation 5-3 (Rhén et al. (1997) /3/. Firstly, the transmissivity and skin factor were obtained by type curve matching on the data curve using a fixed storativity value of 10^{-6}, according to the instruction SKB MD 320.004. From the transmissivity value obtained, the storativity was then calculated according to Equation 5-3 and the type curve matching was repeated. In most cases the change of storativity did not significantly alter the calculated transmissivity by the new type curve matching. Instead, the estimated skin factor, which is strongly correlated to the storativity using the effective borehole radius concept, was altered correspondingly.

$$S=0.0007 \cdot T^{0.5} \qquad (5\text{-}3)$$

S = storativity (–)
T = transmissivity (m^2/s)

For transient analysis of the recovery period, a model presented by Dougherty-Babu (1984) /4/ was used when a certain period with pseudo-radial flow could be identified. In this model, a variety of transient solutions for flow in fractured porous media is available, accounting for e.g. wellbore storage and skin effects, double porosity etc The solution for wellbore storage and skin effects is analogous to the corresponding solution presented in Earlougher (1977) /5/ based on the effective wellbore radius concept to account for non-zero (negative) skin factors. However, for tests in isolated test sections, wellbore storage is represented by a radius of a fictive standpipe (denoted fictive casing radius, r(c)) connected to the test section, cf Equation 5-6. This concept is equivalent to calculating the wellbore storage coefficient C from the compressibility in an isolated test section according to Equation 5-5.

The model by Dougherty-Babu (1984) was used to estimate the transmissivity and skin factor from the recovery period. The storativity was calculated using Equation 5-3 in the same way as described above for the transient analysis of the injection period. In addition, the wellbore storage coefficient was estimated, both from the simulated value on the fictive casing radius r(c) and from the slope of 1:1 in the log-log recovery plots.

For tests characterized by pseudo-spherical (leaky) flow or pseudo-stationary flow during the injection period, a model by Hantush (1959) /6/ for constant head tests was adopted for the evaluation. In this model, the skin factor is not separated but can be calculated from the simulated effective borehole radius according to Equation 5-4. This model also allows calculation of the wellbore storage coefficient according to Equation 5-6. In addition, the leakage coefficient K'/b' can be calculated from the simulated leakage factor r/B. The corresponding model for constant flow rate tests, Hantush (1955) /7/, was applied for evaluation of the recovery period for tests showing pseudo-spherical- or pseudo-stationary flow during this period.

$$\zeta = ln(r_w/r_{wf}) \qquad (5\text{-}4)$$

ζ = skin factor
r_w = borehole radius (m)
r_{wf} = effective borehole radius

Some tests showed fracture responses (a slope of 0.5 or less in a log-log plot). A model for single fractures was then used for the transient analysis as a complement to the standard models. The model by Ozkan-Raghavan (1991a) /8/ and (1991b) /9/ for a vertical fracture was employed. In this case, the test section length was used to convert K and S_s to T and S, respectively, after analysis by fracture models. The quotient K_x/K_y of the hydraulic conductivity in the x and the y-direction, respectively, was assumed to be 1.0 (one). Type curve matching provided values of K_x and L_f, where L_f is the theoretical fracture length.

The different transient estimates of transmissivity from the injection and recovery period, respectively, were then compared and examined. One of these was chosen as the best representative value of the transient transmissivity of the formation adjacent to the test section. This value is denoted T_T. In cases with more than one pseudo-radial flow regime during the injection or recovery period, the first one is assumed as the most representative for the hydraulic conditions in the rock close to the tested section. In most cases, the transient estimates of transmissivity from the injection period were considered more representative than those from the recovery period. The recovery responses were often strongly affected by wellbore storage and, frequently, no pseudo-radial flow regime was reached. In addition, pseudo-stationary flow sometimes occurred during the recovery period.

Finally, a representative value of transmissivity of the test section, T_R, was chosen from T_T and T_M. In general, the transmissivity from the transient evaluation, T_T, was considered as the best estimate. In 16 out of 102 tests with a definable final flow rate in KFM09A the steady-state transmissivity, T_M, was chosen as the most representative value of transmissivity of the test section. The latter transmissivity was chosen whenever a transient evaluation of the test data was not possible. Whenever the flow rate by the end of the injection period

(Q_p) was too low to be defined, and thus neither T_T nor T_M could be estimated, the representative transmissivity for the test section was considered to be less than T_M based on the estimated lower measurement limit for Q/s (i.e. $T_R<T_M$=Q/s-measl-L·C_M).

Estimated values of the borehole storage coefficient, C, based on actual borehole geometrical data and assumed fluid properties are shown in Table 5-3. The net water volume in the test section, V_w, has in Table 5-3 been calculated by subtracting the volume of equipment in the test section (pipes and thin hoses) from the total volume of the test section. For an isolated test section, the wellbore storage coefficient, C, may be calculated as by Almén et al, (1986) /10/:

$$C = V_w \cdot c_w = L_w \cdot \pi \cdot r_w^2 \cdot c_w \tag{5-5}$$

V_w = water volume in test section (m^3)
r_w = nominal borehole radius (m)
L_w = section length (m)
c_w = compressibility of water (Pa^{-1})

When appropriate, estimation of the actual borehole storage coefficient C in the test sections was made from the recovery period, based on the early borehole response with 1:1 slope in the log-log diagrams. The coefficient C was calculated only for tests with a well-defined line of slope 1:1 in the beginning of the recovery period. In the most conductive sections, this period occurred during very short periods at early test times. The latter values may be compared with the net values of C based on geometry and the value of C_{eff} based on laboratory experiments /11/, (Table 5-3).

Furthermore, when using the model by Dougherty-Babu (1984) /4/, a fictive casing radius, r(c), is obtained from the parameter estimation of the recovery period. This value can then be used for calculating C as by Almén et al, (1986) /10/:

$$C = \frac{\pi \cdot r(c)^2}{\rho \cdot g} \tag{5-6}$$

Although this calculation was not done regularly and the results are not presented in this report, the calculations corresponded in most cases well to the value of C obtained from the line of slope 1:1 in the beginning of the recovery period.

The estimated values of C from the tests may differ from the net values in Table 5-3 based on geometry. For example, the effective compressibility for an isolated test section may sometimes be higher than the water compressibility due to e.g. packer compliance, resulting in increased C-values.

Table 5-3. Calculated net values of C, based on the actual geometrical properties of the borehole and equipment configuration in the test section (C_{net}) together with the effective wellbore storage coefficient (C_{eff}) for injection tests from laboratory experiments /11/.

r_w (m)	L_w (m)	Volume of test section (m^3)	Volume of equipment in section (m^3)	V_w (m^3)	C_{net} (m^3/Pa)	C_{eff} (m3/Pa)
0.03865	100	0.469	0.061	0.408	$1.9 \cdot 10^{-10}$	$1.9 \cdot 10^{-10}$
0.03865	20	0.094	0.013	0.081	$3.7 \cdot 10^{-11}$	$4.3 \cdot 10^{-11}$
0.03865	5	0.023	0.04	0.020	$9.2 \cdot 10^{-12}$	$1.6 \cdot 10^{-11}$

The radius of influence at a certain time may be estimated from Jacob's approximation of the Theis' well function, Cooper and Jacob (1946) /12/:

$$r_i = \sqrt{\frac{2.25Tt}{S}} \tag{5-7}$$

T = representative transmissivity from the test (m^2/s)
S = storativity estimated from Equation 5-3
r_i = radius of influence (m)
t = time after start of injection (s)

If a certain time interval of pseudo-radial flow (PRF) from t_1 to t_2 can be identified during the test, the radius of influence is estimated using time t_2 in Equation 5-7. If no interval of PRF can be identified, the actual total flow time t_p is used. The radius of influence can be used to deduce the length of the hydraulic feature(s) tested.

Furthermore, an r_i-index (–1, 0 or 1) is defined to characterize the hydraulic conditions by the end of the test. The r_i-index is defined as shown below. It is assumed that a certain time interval of PRF can be identified between t_1 and t_2 during the test.

- r_i-index = 0: The transient response indicates that the size of the hydraulic feature tested is greater than the radius of influence based on the actual test time (t_2=t_p), i.e. the PRF is continuing at stop of the test. This fact is reflected by a flat derivative at this time.
- r_i-index = 1: The transient response indicates that the hydraulic feature tested is connected to a hydraulic feature with lower transmissivity or an apparent barrier boundary (NFB). This fact is reflected by an increase of the derivative. The size of the hydraulic feature tested is estimated as the radius of influence based on t_2.
- r_i-index = –1: The transient response indicates that the hydraulic feature tested is connected to a hydraulic feature with higher transmissivity or an apparent constant head boundary (CHB). This fact is reflected by a decrease of the derivative. The size of the hydraulic feature tested is estimated as the radius of influence based on t_2.

If a certain time interval of PRF cannot be identified during the test, the r_i-indices –1 and 1 are defined as above. In such cases the radius of influence is estimated using the flow time t_p in Equation 5-7.

5.5 Nonconformities

The test program in KFM09A was carried out according to the Activity Plan AP PF 400-05-104 with the following exceptions:

- The temperature sensors in the injection water at the ground surface, T_{surf}, and in the logging cabin, T_{air}, were out of order during the injection tests.
- The Tecalan hose connected to P_{bubbel}, the transducer measuring the ground water level, could not be put into position in the borehole before testing. This was due to the small diameter of the borehole which made it impossible to get it down to the ground water surface.
- Due to major fractures in the borehole, six tests with section length 20 m were performed instead of five tests in one of the 100 m sections (206.0–306.0 m). This leads to partly overlapping sections within this borehole interval.

- Due to major fractures in the borehole, some of the positions of the 5 m tests were shifted. This result in some partly overlapping sections, and that some of the intervals measured with different section lengths are not identical. Also two small intervals (231.0–232.0 m and 245.5–246.8 m) within the 20 m intervals were not covered by the 5 m tests.
- Drilling was conducted in an adjacent borehole KFM09B (from c 70–616 m) situated about 10 m from KFM09A at the same time as many of the tests were performed. The pressure in the section above was clearly affected by this activity for many of the tests. It is very likely that the conductive fractures in the upper part of the two boreholes are connected. The drilling affects the part of the borehole above the drilling position. Possible interference between the measured section and the section above (seen as a pressure increase) is therefore difficult to notice, since it is hard to know whether the increase is caused by drilling or by a hydraulic connection between the sections. The drilling is not thought to have affected the test results, other than maybe in one test section, i.e. 126.0–146.0 m. For some tests possible drilling effects are also noticed in the section below the test section.

6 Results

6.1 Nomenclature and symbols

The nomenclature and symbols used for the results of the injection tests in KFM09A are in accordance with the Instruction for analysis of injection and single-hole pumping tests (SKB MD 320.004). Additional symbols are explained in the text and in Appendix 5. Symbols used by the AQTESOLV software are explained in Appendix 3.

6.2 Routine evaluation of the single-hole injection tests

6.2.1 General test data

General test data and selected pressure and flow data from all tests are listed in Appendix 2.1 and 2.2, respectively.

During the injection tests in KFM09A, drilling was on-going in the upper part of KFM09B, which is located close to KFM09A. However, no injection tests were performed in the upper part of borehole KFM09A while drilling was performed in KFM09B. The pressure and flow rate in the tests in KFM09A were therefore assumed to be unaffected by these activities. However, for many tests the pressure above the test section was clearly affected, making the interpretation of possible interference with the section above the test section difficult.

6.2.2 Length corrections

The down-hole equipment is supplied with a level indicator located c 3 m below the lower packer in the test section, see Figure 4-2. The level indicator transmits a signal each time a reference mark in the borehole is passed. In KFM09A, reference marks were milled into the borehole wall at every 50 m (with a few exceptions).

During the injection tests in KFM09A with the PSS, length reference marks were detected as presented in Table 6-1. As seen from Table 6-1, all of the length marks of the borehole were detected. At each mark, the length scale for the injection tests was adjusted according to the reported length to the reference mark.

The largest difference between the reported and measured lengths at the reference marks during the injection tests was 0.16 m, at the 650 m reference mark. The difference between two consecutive measurements over a 100 m borehole interval was 0.11 m or less in all cases. A comparison of the measurements performed with different section lengths results in a maximum difference of 0.02 m.

Earlier experiences from field measurements with PSS show that the necessary length corrections usually increase versus borehole length. This was however not the case in borehole KFM09A where the correction sometimes increased and sometimes decreased between consecutive reference marks.

Since the length scale was adjusted in the field every time a reference mark was passed, and because the difference between consecutive marks was small, it was not found worthwhile to make any further adjustments after the measurements, e.g. by linear interpolation between reference marks.

Table 6-1. Detected reference marks during the injection tests in KFM09A.

Borehole length (m)	Detected during the injection tests in 100 m sections	Detected during the injection tests in 20 m sections	Detected during the injection tests in 5 m sections
50.0	Yes	Yes	Yes
99.0	Yes	Yes	Yes
150.0	Yes	Yes	Yes
200.0	Yes	Yes	Yes
250.0	Yes	Yes	Yes
300.0	Yes	Yes	Yes
350.0	Yes	Yes	Yes
400.0	Yes	Yes	Yes
450.0	Yes	Yes	Yes
500.0	Yes	Yes	Yes
550.0	Yes	Yes	Yes
600.0	Yes	Yes	Yes
650.0	Yes	Yes	Yes
725.0	Yes	Yes	Yes

6.2.3 General results

For the injection tests, transient evaluation was conducted, whenever possible, both on the injection and recovery periods (T_f and T_s, respectively) according to the methods described in Section 5.4.4. The steady-state transmissivity (T_M) was calculated by Moye's formula according to Equation 5-1. Transient evaluation was performed for all tests for which a significant flow rate, Q_p, could be identified, see Section 5.4.2. The quantitative analysis was conducted using the AQTESOLV software.

A summary of the results of the routine evaluation of the injection tests is presented, test by test, in Table 6-2 for KFM09A. Selected test diagrams are presented in Appendix 3. In general, one linear diagram showing the entire test sequence together with lin-log and log-log diagrams from the injection and recovery periods, respectively, are presented. The quantitative analysis was performed from such diagrams using the AQTESOLV software. From tests with a flow rate below the estimated lower measurement limit for the specific test, only the linear diagram is presented. The results of the routine evaluation of the tests in borehole KFM09A are also compiled in appropriate tables in Appendix 5 to be stored in the SICADA database.

The dominating transient flow regimes during the injection and recovery periods, as interpreted from the qualitative test evaluation, are listed in Table 6-2 and are further commented on in Section 6.2.4. Several of the responses during the recovery period were strongly influenced by wellbore storage effects. Thus, for many tests, pseudo-radial flow was not reached during this period. On the other hand, during the injection period, a certain time interval with pseudo-radial flow could, in most tests, be identified. Consequently, standard methods for single-hole tests with wellbore storage and skin effects were generally used for the routine evaluation of the tests. The approximate start and stop times of the pseudo-radial flow regime used for the transient evaluation are also listed in Table 6-2.

Some of the tests in KFM09C showed unusual responses, both during the injection- and recovery period, possibly representing flow in conductive fractures of limited extension. During the injection period the flow rate decreased rapidly indicating a closed no-flow boundary in these tests, but the final flow rate was still rather high. No transient evaluation of the injection period was possible for these tests. After stop of the injection the pressure recovered very slowly and only to a limited extent during the recovery period. Examples of such sections are 426.0–446.0 m and 146.0–151.0 m. One possible explanation to these responses is flow in a high-conductive fracture of limited extension, i.e. decreasing fracture aperture away from the borehole, or other geometrical restrictions of the fracture. Some other tests show initial pseudo-radial flow transitioning to flow in an apparent no-flow boundary, followed by slow and limited pressure recovery after the stop of the injection. An example is section 606.0–626.0 m.

For a few tests a type curve fit is yet displayed in the diagrams in Appendix 3, despite the estimated parameters from the fit are judged as non- representative and are thus not included in the result tables in SICADA. For these tests, the type curve fit is presented, for example, to illustrate that an assumption of pseudo-radial flow regime is not justified for the test. Instead, some other flow regime is likely to dominate. For example, for test responses showing only wellbore storage and tests approaching a pseudo-stationary flow, no unique transient evaluation is possible.

The transmissivity judged as the most reliable from the transient evaluation of the flow- and recovery periods of the tests was selected as T_T. The associated value of the skin factor is listed in Table 6-2. Since a fairly well-defined time interval with pseudo-radial flow in most cases could be identified from the injection period, the transmissivity calculated from this period is generally considered as the most reliable transmissivity, T_T, from the transient analysis of the injection tests in KFM09A. Furthermore, the transient evaluation of transmissivity from the injection period was for most of the tests also judged as the most representative estimate of transmissivity, T_R.

For those tests where transient evaluation was not possible or not considered representative, T_M was chosen as the representative transmissivity value, T_R. If Q_p was below the actual test-specific measurement limit, the representative transmissivity value was assumed to be less than the estimated T_M, based on Q/s-measl-L, see Section 5.4.2 and 5.4.4.

The results of the routine evaluation of the injection tests in borehole KFM09A are also compiled in appropriate tables in Appendix 5 to be stored in the SICADA database.

In Figure 6-1, a comparison of calculated transmissivities in 5 m sections from steady-state evaluation (T_M) and transmissivity values from the transient evaluation (T_T) is shown. The agreement between the two populations is in general considered as good. Steady-state analysis of transmissivity according to Moye's formula (denoted T_M) slightly overestimates the transmissivity if steady-state conditions do not prevail in the borehole. This is the explanation to the predominance of points below the 1:1 curve, especially for low values of transmissivity, since stady-state conditions is normally not attained during the injection period. In cases were an apparent no-flow boundary appears at the end of the injection period and transient evaluation is performed on the early part of the datacurve, the opposite can be true (i.e. TM is low in comparison with the transient estimate of transmissivity). In this case two different zones of the bedrock is obviously measured during the early and the late parts of the injection respectively, but when looking at the values only, the effect seen is that T_M is underestimated. The lower standard measurement limit of transmissivity in 5 m sections based on a flow rate of 1 mL/min and an injection pressure of 200 kPa is indicated in the figure.

The wellbore storage coefficient, C, was calculated from the straight line with a unit slope in the log-log diagrams from the recovery period in KFM09A, see Table 6-2. The coefficient C was only calculated for tests with a well-defined line of unit slope in the beginning of the recovery period. In the most conductive sections, this period occurred during very

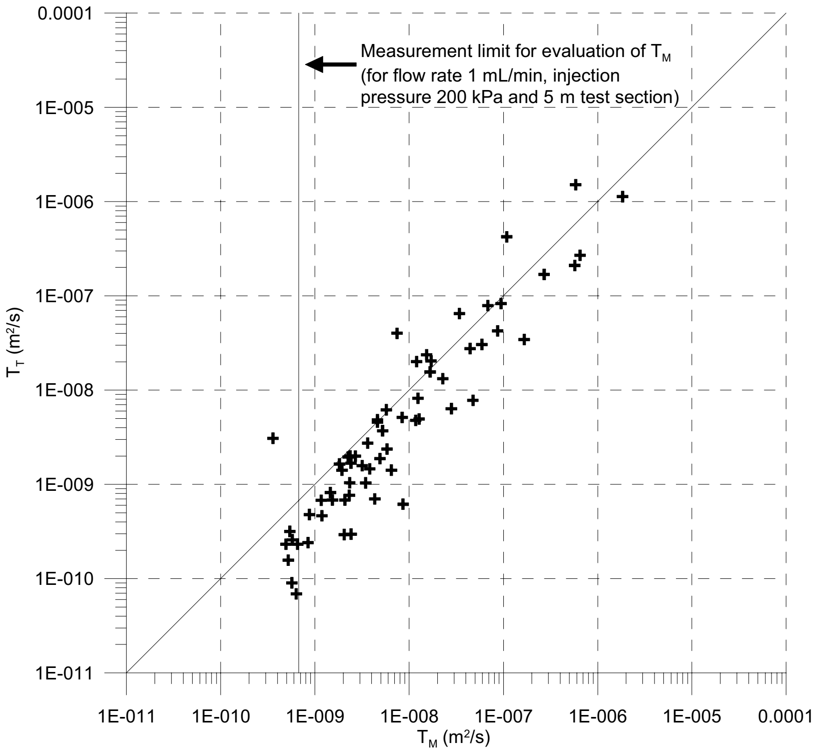

Figure 6-1. *Estimated transmissivities in 5 m sections from steady-state (T_M) and transient (T_T) evaluation in KFM09A.*

short intervals at very early times and is not visible in the diagrams. In sections with a very low transmissivity, the estimates of C may be uncertain due to difficulties in defining an accurate time for the start of the recovery period. Furthermore, the resolution of the pressure sensors causes the recovery to be quite scattered in sections of low transmissivity. The values of C presented in Table 6-2 may be compared with the net values of C_{net} (based on geometry) and the value of C obtained from laboratory experiments, C_{eff} /11/, both found in Table 5-3.

The number of tests with a well-defined line of unit slope for which it was possible to calculate C was as follows: 1 of 7 with the 100 m test section resulted in a well-defined 1:1 straight line. The corresponding figures for the 20 m tests were 7 out of 30, and for the 5 m tests 18 out of 64. Table 6-2 shows that there is, in general, a good agreement between the calculated C-values from the tests and those listed in Table 5-3, although the calculated values from the tests tend to be slightly higher. The higher C-values observed in the tests can be explained by the compressibility contribution of the rock formation and water in good hydraulic connection (i.e. open fractures) with the section.

The test in section 771.0–791.0 m resulted in a significantly higher estimate of C than tests in the other 20 m intervals. The estimation of C in the dominating 5 m test in the interval 771.0–791.0 m was also higher than in the other 5 m sections. No reasonable explanation has been found for the significantly higher wellbore storage coefficient estimated from the test in the interval of 786.0–791.0 m. Only one of the 100 m tests provided an estimate of C, the value in Table 5-3 was lower than this value. When constructing 95% confidence intervals (using a t-distribution) from calculated values of C from the tests, the values of C_{net} and C_{eff} listed in Table 5-3 are within these confidence intervals for the 5 m and 20 m sections. When constructing the same confidence intervals but excluding the tests with higher C-values the C_{net} still falls within the confidence interval for both 20 and 5 m. However C_{eff} falls below the confidence intervals.

Table 6-2. Summary of the routine evaluation of the single-hole injection tests in borehole KFM09A.

Secup (m)	Seclow (m)	Test start YYYYMMDD hh:mm	b (m)	Flow regime [1)] injection	recovery	T_M (m²/s)	T_f (m²/s)	T_s (m²/s)	T_T m²/s)	T_R [2)] (m²/s)	ξ (–)	t_1 (s)	t_2 (s)	dte_1 (s)	dte_2 (s)	C (m³/Pa)	r_i (m)	r_i-index (–)
106.0	206.0	20051117 16:09	100	PSF	WBS->PSF	4.89E–06	4.56E–07	4.68E–07	4.56E–07	4.56E–07	–6.79						62.84	–1
206.0	306.0	20051117 19:03	100	PRF	WBS->(PRF)	7.69E–08	4.19E–08	1.05E–07	4.19E–08	4.19E–08	–2.54	150	1800	700	1100		34.41	0
306.0	406.0	20051117 21:47	100	(PLF)->NFB	(PLF)->NFB	2.46E–07	1.62E–08	1.29E–07	1.29E–07	1.29E–07	–5.13						45.55	1
406.0	506.0	20051118 09:59	100	NFB	PLF->NFB	6.74E–07		1.14E–06	1.14E–06	6.74E–07	–5.76						69.31	1
506.0	606.0	20051121 12:52	100	NFB	(PRF)->NFB	1.13E–07		3.17E–07	3.17E–07	1.13E–07	–5.12						44.31	1
606.0	706.0	20051121 06:14	100	PRF->NFB	WBS->(PRF)->NFB	3.56E–08	1.64E–08	2.19E–08	1.64E–08	1.64E–08	–3.54	20	400			3.24E–10	12.82	1
691.0	791.0	20051121 08:51	100	PSF	WBS->PSF?	6.09E–08	6.92E–09	5.89E–09	6.92E–09	6.92E–09	–5.60						22.07	–1
106.0	126.0	20051128 16:44	20	PRF	WBS->PRF	4.06E–07	2.51E–07	4.99E–07	2.51E–07	2.51E–07	–3.14	100	1200	200	700		43.97	0
126.0	146.0	20051129 06:29	20	PRF	PLF/NFB?	1.28E–06	5.35E–07		5.35E–07	5.35E–07	–4.71	550	1200				53.12	0
146.0	166.0	20051129 08:20	20	PLF->(PRF?)	PLF/NFB?	2.52E–07	4.22E–08		4.22E–08	4.22E–08							28.35	0
166.0	186.0	20051129 10:00	20	PSF	PLF/WBS->PRF?	2.29E–06	6.19E–07	2.32E–06	6.19E–07	6.19E–07	–5.02						55.49	–1
186.0	206.0	20051129 12:14	20	PSF	WBS->	4.82E–09	3.28E–09		3.28E–09	3.28E–09	–1.13					5.75E–11	14.99	–1
206.0	226.0	20051129 14:01	20	–	–	<2.66E–10				<2.66E–10							–	–
226.0	246.0	20051129 15:38	20	PRF	WBS->	4.83E–08	4.65E–08		4.65E–08	4.65E–08	–0.24	300	1200				28.85	0
238.0	258.0	20051129 17:18	20	PRF	WBS->	1.20E–08	4.90E–09	4.33E–09	4.90E–09	4.90E–09	–3.44	200	1200			5.01E–10	16.43	0
258.0	278.0	20051129 18:58	20	(PRF)->NFB	WBS->(PRF)	2.61E–09	7.27E–10	1.46E–09	1.46E–09	1.46E–09	–3.09	100	600			7.53E–11	12.12	0
278.0	298.0	20051129 21:03	20	PRF1->PRF2	WBS->PRF	5.37E–09	2.59E–09	2.92E–09	2.59E–09	2.59E–09	–3.42	10	300	600	900		7.01	0
286.0	306.0	20051129 22:41	20	PLF/PRF	WBS->	2.95E–09	5.70E–10	1.39E–09	1.39E–09	1.39E–09	–3.56						11.95	–1
306.0	326.0	20051130 06:29	20	PRF->NFB	PRF->NFB	1.43E–08	3.12E–08	9.22E–08	3.12E–08	3.12E–08	–2.23	20	100	10	100		7.53	1
326.0	346.0	20051130 08:16	20	PRF	WBS->(PRF)	1.06E–09	4.17E–10	2.94E–10	4.17E–10	4.17E–10	–3.21	30	1200	1000	2000		8.87	0
346.0	366.0	20051130 10:06	20	PLF->(PRF)	WBS->PRF	2.18E–09	7.25E–10	7.56E–10	7.25E–10	7.25E–10	–3.71	300	1200	300	900	5.57E–11	10.19	0
366.0	386.0	20051130 12:06	20	PRF	PRF	6.50E–08	2.44E–08	3.94E–08	2.44E–08	2.44E–08	–4.23	200	1200	30	800		24.54	0
386.0	406.0	20051130 13:50	20	PLF/NFB	PLF/NFB?	1.38E–07		4.53E–08	4.53E–08	1.38E–07	–6.01						38.40	1
406.0	426.0	20051130 15:30	20	PRF->PSF	WBS->NFB	2.04E–08	4.69E–09	2.31E–08	2.31E–08	2.04E–08	–1.36	100	1000				23.85	1
426.0	446.0	20051130 18:18	20	NFB->	PLF/NFB	8.60E–07		1.26E–06	1.26E–06	8.60E–07	–5.73						60.65	1
446.0	466.0	20051130 20:03	20	PRF	WBS->	3.16E–09	1.97E–09	3.06E–09	1.97E–09	1.97E–09	–1.90	200	1200				13.08	0

Secup (m)	Seclow (m)	Test start YYYYMMDD hh:mm	b (m)	Flow regime [1] injection	recovery	T_M (m^2/s)	T_f (m^2/s)	T_s (m^2/s)	T_T m^2/s)	T_R [2] (m^2/s)	ξ (–)	t_1 (s)	t_2 (s)	dte_1 (s)	dte_2 (s)	C (m^3/Pa)	r_i (m)	r_i-index (–)
466.0	486.0	20051130 22:03	20	PLF->	WBS->(PRF)->NFB	2.37E–09	2.00E–10	1.86E–09	1.86E–09	1.86E–09	–2.90			100	500		8.32	1
486.0	506.0	20051201 08:06	20	PLF	WBS->	5.86E–09	1.00E–09		1.00E–09	1.00E–09							11.14	1
506.0	526.0	20051201 10:01	20	PRF->PSF	WBS->	2.33E–09		2.06E–10	2.06E–10	2.06E–10	–5.47						7.44	0
526.0	546.0	20051201 11:41	20	NFB	PRF	1.45E–07		4.12E–07	4.12E–07	1.45E–07	–4.72			100	1400		38.65	0
545.0	565.0	20051201 14:21	20	–	–	<2.66E–10				<2.66E–10							–	–
566.0	586.0	20051201 15:34	20	–	–	<2.66E–10				<2.66E–10							–	–
586.0	606.0	20051202 07:55	20	–	–	<2.66E–10				<2.66E–10							–	–
606.0	626.0	20051202 08:58	20	PRF->NFB	PRF->NFB	2.43E–08	1.28E–08	2.92E–08	1.28E–08	1.28E–08	–3.99	50	300	10	300		10.44	1
626.0	646.0	20051202 10:43	20	PRF	WBS->	4.21E–09	1.62E–09	2.70E–09	2.70E–09	2.70E–09	–1.83	200	1200			7.25E–11	14.16	–1
646.0	666.0	20051202 13:12	20	PRF	WBS->	5.22E–09	4.21E–09	1.53E–08	4.21E–09	4.21E–09	–0.94	50	1200				15.82	0
666.0	686.0	20051202 14:57	20	PLF	WBS->	6.82E–10	2.40E–11	6.30E–11	2.40E–11	6.82E–10	–6.35						10.05	1
686.0	706.0	20051205 08:22	20	PLF	WBS->	5.10E–10	9.24E–11	3.28E–10	9.24E–11	9.24E–11							6.10	1
691.0	711.0	20051205 10:10	20	–	–	<2.02E–10				<2.02E–10							–	–
711.0	731.0	20051205 12:46	20	–	–	<2.02E–10				<2.02E–10							–	–
731.0	751.0	20051205 13:49	20	PRF	WBS->	3.01E–09	1.62E–09	3.41E–09	3.41E–09	3.41E–09	0.71	120	1200			6.28E–11	15.03	–1
751.0	771.0	20051205 15:30	20	PLF->(PRF)	WBS->	1.82E–08	3.50E–09	4.72E–09	3.50E–09	3.50E–09	–5.20						15.22	1
771.0	791.0	20051205 18:09	20	PRF->PSF	WBS->	4.23E–08	6.54E–09	3.20E–09	6.54E–09	6.54E–09	–5.10					1.41E–09	17.81	–1
106.0	111.0	20051207 07:32	5	PSF	WBS->PSF->NFB	2.27E–08	1.32E–08	1.05E–08	1.32E–08	1.32E–08	–2.89						21.26	–1
111.0	116.0	20051207 09:08	5	PSF	WBS->PRF	2.33E–09	1.04E–09	1.00E–09	1.04E–09	1.04E–09	–3.22			500	800		11.26	–1
116.0	121.0	20051221 15:48	5	PRF1->PRF2	PRF->NFB	8.68E–08	4.25E–08	6.01E–08	4.25E–08	4.25E–08	–4.44	50	400	30	400		16.28	0
121.0	126.0	20051207 12:52	5	PRF1->PRF2	PRF1->PRF2	2.71E–07	1.69E–07	4.19E–07	1.69E–07	1.69E–07	–3.66	80	350	50	250		21.51	0
126.0	131.0	20051207 14:26	5	NFB	PLF	1.54E–09		6.83E–10	6.83E–10	6.83E–10							10.02	1
128.0	133.0	20051207 16:21	5	PLF?->PSF	PLF->PRF?	6.50E–07	2.69E–07	1.73E–07	2.69E–07	2.69E–07	–4.87			500	900		45.08	–1
133.0	138.0	20051207 17:58	5	PSF	WBS->NFB?->	5.71E–07	1.60E–07	2.10E–07	2.10E–07	2.10E–07	–4.48						41.99	0
138.0	143.0	20051207 19:42	5	PRF	PRF?	1.24E–08	8.19E–09	6.41E–09	8.19E–09	8.19E–09	–2.86	100	1200	300	500		18.68	0
141.0	146.0	20051207 21:27	5	PRF	PLF->NFB->	4.43E–08	2.77E–08	1.91E–08	2.77E–08	2.77E–08	–3.50						25.58	0
146.0	151.0	20051207 23:02	5	NFB->	PLF	4.75E–08		7.80E–09	7.80E–09	7.80E–09							18.36	1

Secup (m)	Seclow (m)	Test start YYYYMMDD hh:mm	b (m)	Flow regime [1)] injection	recovery	T_M (m^2/s)	T_f (m^2/s)	T_s (m^2/s)	T_T m^2/s)	T_R [2)] (m^2/s)	ξ (–)	t_1 (s)	t_2 (s)	dte_1 (s)	dte_2 (s)	C (m^3/Pa)	r_i (m)	r_i-index (–)
151.0	156.0	20051208 06:16	5	–	–	<2.10E–10				<2.10E–10							–	–
156.0	161.0	20051208 07:10	5	PLF->(PRF?)	PLF	1.66E–07	3.44E–08		3.44E–08	3.44E–08							26.90	0
161.0	166.0	20051208 08:36	5	PSS	WBS->PSS	4.60E–09	4.85E–09		4.85E–09	4.60E–09	0.00						16.31	–1
166.0	171.0	20051208 10:03	5	PSF	PLF->PRF?	1.84E–06	1.13E–06	2.11E–06	1.13E–06	1.13E–06	–3.98			400	700		64.48	–1
171.0	176.0	20051208 12:12	5	NFB	WBS	2.15E–09				2.15E–09							13.46	–
176.0	181.0	20051208 13:43	5	PRF	WBS->NFB	1.17E–08	4.78E–09		4.78E–09	4.78E–09	–3.96	50	1200			7.41E–11	16.33	0
181.0	186.0	20051208 15:13	5	NFB?	WBS	8.83E–09				8.83E–09							19.20	–
186.0	191.0	20051208 16:36	5	PRF	WBS->	4.60E–09	4.58E–09		4.58E–09	4.58E–09	–0.92	40	1200			2.51E–11	16.16	0
191.0	196.0	20051208 18:03	5	–	–	<2.17E–10				<2.17E–10							–	–
196.0	201.0	20051208 19:02	5	–	–	<1.68E–10				<1.68E–10							–	–
201.0	206.0	20051208 19:57	5	–	–	<2.17E–10				<2.17E–10							–	–
226.0	231.0	20051208 20:58	5	–	–	<2.17E–10				<2.17E–10							–	–
232.0	237.0	20051208 21:54	5	PSF	PSF	3.41E–08	6.48E–08	2.59E–08	6.48E–08	6.48E–08	3.62						31.56	–1
237.0	242.0	20051208 23:21	5	PRF	PSF->NFB	6.84E–08	7.88E–08	3.44E–08	7.88E–08	7.88E–08	–0.90	50	1200				32.90	0
240.8	245.8	20051209 08:08	5	PSF	WBS->	1.27E–08	4.95E–09	1.36E–08	4.95E–09	4.95E–09	–3.88						16.60	–1
246.8	251.8	20051221 13:55	5	–	–	<1.68E–10				<1.68E–10							–	–
251.5	256.5	20051209 09:40	5	–	–	<2.17E–10				<2.17E–10							–	–
256.5	261.5	20051209 10:34	5	–	–	<2.69E–10				<2.69E–10							–	–
273.0	278.0	20051209 11:30	5	PRF1->PRF2	WBS->PRF->	2.37E–09	2.00E–09	1.91E–09	2.00E–09	2.00E–09	–2.81	30	200	200	600	3.85E–11	5.36	0
278.0	283.0	20051209 13:34	5	PLF->PRF->NFB	PLF->PRF	3.81E–09	1.47E–09	2.13E–09	1.47E–09	1.47E–09	–4.20	60	500	200	1000		7.84	1
283.0	288.0	20051209 15:04	5	–	–	<2.17E–10				<2.17E–10							–	–
288.0	293.0	20051209 16:00	5	PLF?	WBS (NFB?)	6.35E–10	6.90E–11		6.90E–11	6.35E–10	–5.42					1.73E–11	9.95	0
293.0	298.0	20051212 08:21	5	PRF	WBS->PSF->	1.16E–09	6.79E–10	7.54E–10	6.79E–10	6.79E–10	–2.68	10	1200			1.72E–11	10.02	0
296.0	301.0	20051221 12:39	5	–	–	<1.68E–10				<1.68E–10							–	–
301.0	306.0	20051221 11:45	5	–	–	<1.68E–10				<1.68E–10							–	–
306.0	311.0	20051212 09:58	5	–	–	<2.67E–10				<2.67E–10							–	–
311.0	316.0	20051212 10:49	5	–	–	<1.16E–10				<1.16E–10							–	–

Secup (m)	Seclow (m)	Test start YYYYMMDD hh:mm	b (m)	Flow regime [1)] injection	recovery	T_M (m^2/s)	T_f (m^2/s)	T_s (m^2/s)	T_T m^2/s)	T_R [2)] (m^2/s)	ξ (–)	t_1 (s)	t_2 (s)	dte_1 (s)	dte_2 (s)	C (m^3/Pa)	r_i (m)	r_i-index (–)
316.0	321.0	20051212 12:43	5	–	–	<1.67E–10				<1.67E–10							–	–
321.0	326.0	20051212 13:44	5	PRF->NFB	PLF/NFB	1.20E–08	2.01E–08		2.01E–08	2.01E–08	–3.28	30	200				9.54	1
346.0	351.0	20051212 15:31	5	–	–	<2.69E–10				<2.69E–10							–	–
351.0	356.0	20051221 10:04	5	PRF	WBS->PRF?	1.94E–09	1.42E–09	2.03E–09	1.42E–09	1.42E–09	–1.68	30	1200			1.74E–11	12.05	0
356.0	361.0	20051221 08:54	5	–	–	<1.67E–10				<1.67E–10							–	–
361.0	366.0	20051221 07:28	5	PRF	WBS->	6.56E–10	2.32E–10		2.32E–10	2.32E–10	–2.96	20	1200				7.67	0
363.0	368.0	20051212 16:39	5	PRF	WBS->	4.93E–10	2.32E–10	5.68E–10	2.32E–10	2.32E–10	–2.93	30	1200			1.84E–11	7.66	0
368.0	373.0	20051213 06:27	5	–	–	<2.17E–10				<2.17E–10							–	–
371.0	376.0	20051213 07:35	5	PRF	PRF	5.89E–08	3.05E–08	3.88E–08	3.05E–08	3.05E–08	–5.05	100	600	20	700		18.36	0
376.0	381.0	20051213 09:02	5	–	–	<2.06E–10				<2.06E–10							–	–
381.0	386.0	20051213 10:10	5	–	–	<2.17E–10				<2.17E–10							–	–
386.0	391.0	20051213 11:57	5	NFB	PLF/NFB	9.43E–08		8.27E–08	8.27E–08	9.43E–08							34.73	1
391.0	396.0	20051213 13:28	5	PRF->PSF	WBS->	6.48E–09	1.42E–09	2.00E–09	1.42E–09	1.42E–09	–4.46	20	300				6.03	–1
396.0	401.0	20051213 15:06	5	–	–	<2.69E–10				<2.69E–10							–	–
401.0	406.0	20051213 16:00	5	PRF->NFB	WBS->NFB	1.70E–08	2.04E–08	2.06E–08	2.04E–08	2.04E–08	–0.66	100	250			1.30E–10	10.71	1
406.0	411.0	20051213 17:25	5	–	–	<2.18E–10				<2.18E–10							–	–
411.0	416.0	20051213 18:36	5	PRF1->PRF2	PRF->NFB	1.53E–08	2.37E–08	4.52E–08	2.37E–08	2.37E–08	–1.98	20	100	20	100		7.03	0
414.0	419.0	20051213 20:06	5	PRF	WBS->	5.42E–10	3.17E–10	1.19E–10	3.17E–10	3.17E–10	–1.85	30	1200				8.29	0
419.0	424.0	20051213 21:32	5	PRF1->PRF2	WBS->PRF	2.25E–09	1.95E–09	3.05E–09	1.95E–09	1.95E–09	–1.79	30	600	400	800	1.61E–11	9.23	0
421.0	426.0	20051213 22:55	5	PRF	WBS->PRF	2.41E–09	1.68E–09	1.62E–09	1.68E–09	1.68E–09	–2.50	20	1200	30	1100	1.90E–11	12.57	0
426.0	431.0	20051214 06:51	5	–	–	<3.19E–10				<3.19E–10							–	–
431.0	436.0	20051214 08:11	5	NFB	PLF->NFB	5.83E–07		1.51E–06	1.51E–06	5.83E–07	–5.47						54.77	1
436.0	441.0	20051214 09:47	5	–	–	<2.47E–10				<2.47E–10							–	–
441.0	446.0	20051214 10:44	5	NFB	PLF->NFB	7.44E–09		4.01E–08	4.01E–08	7.44E–09	–6.42						18.44	1
446.0	451.0	20051214 12:13	5	NFB	PLF->NFB	1.46E–09		8.19E–10	8.19E–10	8.19E–10	–6.02						10.51	1
451.0	456.0	20051214 14:22	5	PRF/PSF	WBS->	5.22E–10	1.57E–10	2.11E–10	1.57E–10	5.22E–10	–3.30						9.49	0
456.0	461.0	20051214 15:55	5	PRF->NFB	WBS->NFB	2.69E–09	2.00E–09	4.19E–09	2.00E–09	2.00E–09	–1.04	20	600				9.29	1
461.0	466.0	20051214 17:32	5	–	–	<1.16E–10				<1.16E–10							–	–

Secup (m)	Seclow (m)	Test start YYYYMMDD hh:mm	b (m)	Flow regime [1)] injection	recovery	T_M (m^2/s)	T_f (m^2/s)	T_s (m^2/s)	T_T m^2/s)	T_R [2)] (m^2/s)	ξ (–)	t_1 (s)	t_2 (s)	dte_1 (s)	dte_2 (s)	C (m^3/Pa)	r_i (m)	r_i-index (–)
471.0	476.0	20051214 18:35	5	PLF->PSF	PLF	2.04E–09	2.93E–10	7.33E–10	2.93E–10	2.93E–10	–5.33						8.22	–1
476.0	481.0	20051214 20:01	5	PRF->NFB	WBS->NFB	1.82E–09	1.65E–09	2.53E–09	1.65E–09	1.65E–09	–1.97	20	100				3.61	1
486.0	491.0	20051214 21:40	5	–	–	<2.17E–10				<2.17E–10							–	–
491.0	496.0	20051214 22:58	5	PRF	WBS->	3.18E–09	1.58E–09	1.65E–09	1.58E–09	1.58E–09	–3.36	60	1200			7.15E–11	12.38	0
496.0	501.0	20051215 06:33	5	NFB	PLF->NFB	2.43E–09		2.97E–10	2.97E–10	2.97E–10							8.15	1
501.0	506.0	20051215 08:14	5	–	–	<2.06E–10				<2.06E–10							–	–
506.0	511.0	20051220 19:00	5	NFB->PSF	WBS	8.76E–10	4.79E–10		4.79E–10	4.79E–10	0.00						9.28	–1
511.0	516.0	20051220 20:50	5	PSF->	WBS->	1.19E–09	4.65E–10	2.07E–10	4.65E–10	4.65E–10	–1.98						9.19	–1
516.0	521.0	20051220 22:14	5	(PRF)	WBS->	8.43E–10	2.41E–10	1.06E–09	2.41E–10	2.41E–10	–3.69					1.56E–11	7.81	0
521.0	526.0	20051215 09:25	5	–	–	<2.17E–10				<2.17E–10							–	–
526.0	531.0	20051215 10:26	5	–	–	<2.17E–10				<2.17E–10							–	–
531.0	536.0	20051215 11:23	5	NFB	PRF->NFB	1.09E–07		4.23E–07	4.23E–07	1.09E–07	–4.75			100	5000		35.98	1
536.0	541.0	20051215 13:19	5	–	–	<2.18E–10				<2.18E–10							–	–
541.0	546.0	20051215 14:14	5	(PRF)->NFB	PLF->PRF?	3.59E–10	3.09E–09	2.46E–09	3.09E–09	3.09E–09	–3.26	10	50	200	1500		2.99	1
561.0	566.0	20051220 17:14	5	–	–	<2.18E–10				<2.18E–10							–	–
606.0	611.0	20051215 16:19	5	–	–	<1.68E–10				<1.68E–10							–	–
611.0	616.0	20051215 17:19	5	PRF->NFB	PRF->NFB	1.67E–08	1.56E–08	3.44E–08	1.56E–08	1.56E–08	–3.50	30	200	10	100		8.96	1
616.0	621.0	20051215 18:50	5	–	–	<2.18E–10				<2.18E–10							–	–
621.0	626.0	20051215 19:44	5	PLF->(PRF)->NFB	PLF->PRF->NFB	5.82E–09	2.38E–09	5.56E–09	2.38E–09	2.38E–09	–4.28	40	400	60	300		7.92	1
626.0	631.0	20051215 21:14	5	–	–	<1.67E–10				<1.67E–10							–	–
631.0	636.0	20051215 22:08	5	(PRF)->NFB	WBS->PRF	5.76E–10	2.58E–10	1.00E–09	2.58E–10	2.58E–10	–3.98	30	100	50	500	1.71E–11	2.27	1
636.0	641.0	20051215 23:43	5	PRF	WBS->PRF	5.72E–09	6.19E–09	1.65E–08	6.19E–09	6.19E–09	0.08	20	1200	150	600	2.64E–11	17.42	0
641.0	646.0	20051216 08:21	5	PLF/PRF	WBS->	5.70E–10	1.59E–10	9.03E–11	9.03E–11	9.03E–11	–4.31						6.11	0
646.0	651.0	20051216 09:55	5	–	–	<1.16E–10				<1.16E–10							–	–
651.0	656.0	20051216 10:53	5	PRF	WBS->PRF->	5.23E–09	3.71E–09	1.32E–08	3.71E–09	3.71E–09	–2.52	40	1200				15.33	0
656.0	661.0	20051216 12:21	5	–	–	<2.69E–10				<2.69E–10							–	–
661.0	666.0	20051216 13:31	5	–	–	<1.68E–10				<1.68E–10							–	–

Secup (m)	Seclow (m)	Test start YYYYMMDD hh:mm	b (m)	Flow regime [1)] injection	recovery	T_M (m^2/s)	T_f (m^2/s)	T_s (m^2/s)	T_T m^2/s)	T_R [2)] (m^2/s)	ξ (–)	t_1 (s)	t_2 (s)	dte_1 (s)	dte_2 (s)	C (m^3/Pa)	r_i (m)	r_i-index (–)
731.0	736.0	20051219 08:19	5	–	–	<2.18E–10				<2.18E–10							–	–
736.0	741.0	20051219 09:15	5	–	–	<2.18E–10				<2.18E–10							–	–
741.0	746.0	20051219 10:11	5	PRF1->PRF2	WBS->NFB	3.63E–09	2.75E–09	1.02E–08	2.75E–09	2.75E–09	–0.91	40	300			1.92E–11	7.11	0
746.0	751.0	20051219 11:44	5	–	–	<2.18E–10				<2.18E–10							–	–
751.0	756.0	20051219 12:50	5	PLF->(PRF)->PSF	PLF	3.45E–09	1.04E–09	9.84E–10	1.04E–09	1.04E–09		200	700				8.51	–1
756.0	761.0	20051219 14:20	5	PRF	WBS->(PRF)	8.44E–09	5.14E–09	4.90E–09	5.14E–09	5.14E–09	–3.58	70	1200				16.63	0
761.0	766.0	20051219 15:56	5	(PRF)->PSF	PLF->	4.32E–09	7.00E–10	1.11E–09	7.00E–10	7.00E–10	–5.02						10.23	–1
766.0	771.0	20051220 06:55	5	PSF	WBS->	2.32E–09	7.66E–10	5.38E–10	7.66E–10	7.66E–10	–3.86					7.66E–11	10.43	–1
771.0	776.0	20051220 08:29	5	PSF	WBS->(PRF)	2.08E–09	6.84E–10	1.93E–09	6.84E–10	6.84E–10	–3.54						10.15	–1
776.0	781.0	20051220 10:06	5	PRF	WBS->(PRF)	4.90E–09	1.88E–09	1.75E–09	1.88E–09	1.88E–09	–3.69	100	1200			7.00E–11	12.93	0
781.0	786.0	20051220 11:35	5	PRF->PSF	WBS->	8.62E–09	6.16E–10	1.39E–09	6.16E–10	6.16E–10	–5.89						9.89	–1
786.0	791.0	20051220 13:11	5	PSF	WBS->	2.81E–08	6.36E–09	7.45E–08	6.36E–09	6.36E–09	–4.52					6.30E–10	17.71	0

[1)] The acronyms in the column "Flow regime" are as follow: wellbore storage (WBS), pseudo-linear flow (PLF), pseudo-radial flow (PRF), pseudo-spherical flow (PSF), pseudo-stationary flow (PSS) and apparent no-flow boundary (NFB). The flow regime definitions are further discussed in Section 5.4.3 above.

[2)] For the tests where Q_p was not detected, T_R was assumed to be less than T_M based on the estimated Q/s-measl-L.

6.2.4 Comments on the tests

Short comments on each test follow below. Tests were performed within the interval 106.0–991.0 m in KFM09A. Flow regimes and hydraulic boundaries, as discussed in Section 5.4.3, are in the text referred to as:

WBS = Wellbore storage
PRF = Pseudo-radial flow regime
PLF = Pseudo-linear flow regime
PSF = Pseudo-spherical flow regime
PSS = Pseudo-stationary flow regime
NFB = No-flow boundary
CHB = Constant-head boundary

In almost every test there is a tendency that the pressure below the test section shows an increasing pressure during the whole test time. This increasing pressure is maybe a secondary effect caused by the drilling in the adjacent borehole KFM09B or it can indicate a higher formation pressure in the bedrock. There might be other explanations as well.

106.0–206.0 m

The injection period is clearly dominated by a PSF after about 200 s throughout the period. During the recovery period, WBS and a transition to PSF are present. A high apparent WBS is indicated. The T-value from the injection period is chosen as the most representative value for this section.

206.0–306.0 m

Although large flow rate variations in the beginning, the injection is clearly dominated by a PRF from c 150 s and throughout the period. The recovery is affected by WBS effects and a transition towards a PRF by the end of the period.

306.0-406.0 m

At the beginning of the injection a period of approximately PLF is indicated. The flow then turns into an apparent NFB. The recovery period also seems to start with a short period of approximately PLF and then transits to an apparent NFB. Only limited recovery was obtained (c 12 m) indicating a decreasing fracture aperture away from the borehole. Transient evaluation on the recovery period is regarded to obtain the most representative value of transmissivity.

406.0–506.0 m

The injection period is dominated by a NFB throughout the entire period. The recovery period initially shows signs of an apparent PLF transitioning into an apparent NFB. Only a limited recovery (c 5 m) was observed which may indicate flow in a large fracture of limited extent with decreasing aperture away from the borehole. There are pressure disturbances above and below the test section during this test possibly caused by drilling activities in KFM09B.

506.0–606.0 m

Drilling of the adjacent borehole KFM09B was going on at the time of the injection test. The pressure in the section above is clearly affected by the activity. In addition, some electrical error caused disturbance of the pressure sensors in the borehole which is clearly seen on the overview plot. This problem was however solved a few minutes before the start of the injection, so readings from the flow period and the recovery period are good. The injection period indicates an apparent NFB. After c 150 s of the injection period a change of valves occurred. This caused a temporary pressure increase seen as a gap in the data curve. The recovery period demonstrates an apparent PRF followed by an apparent NFB. Only a limited recovery (c 3.4 m) was observed which may indicate flow in a fracture of limited extent, i.e. decreasing fracture aperture away from the borehole. No transient evaluation can be made from the injection period. An approximate transient evaluation is made from the first part of the recovery period. The stationary evaluation is regarded as the best estimate of the transmissivity in the section.

606.0–706.0 m

Although the injection pressure during this test is slightly unstable due to manual pressure regulation it is not considered to affect the test results. The injection period starts with a transition to a PRF lasting between c 20 and 400 s. After that it turns into an apparent NFB. The recovery begins with WBS followed by a transition towards a PRF which is interrupted by an apparent NFB at the end of the recovery period.

691.0–791.0 m

This test was conducted with the pressure vessel with manual regulation of the pressure although the flow was a little too high for that. During a short time period after about 400 s the pressure drifted away c 4–5 kPa, but this pressure drift was judged to have no effect on the analyses of the test. The injection period transits immediately into a PSF that goes on for the entire period. The recovery starts with a WBS followed by a transition to a possible PSF. There was a pressure interference with the section below which can be seen on the plots. In addition, as can also be seen in the plots, there was some drilling activities started in KFM09B during the recovery of this test. The drilling clearly influenced the pressure above the test section starting when about half of the recovery was completed.

106.0–126.0 m

There are two disturbances on the injection pressure. The first occurs after c 120 s and the s after c 600 s. It is not clear if the disturbances are caused by a real effect from the rock formation or some irregularity in the pressure regulation. However, a PRF is believed to dominate the injection period from c 100 s. The recovery period initially exhibits WBS which then transitions into a PRF lasting from c 200 to 600 s.

126.0–146.0 m

During the first c 400 s of the injection period the flow rate and pressure are somewhat unstable and no flow regime can be determined. Between approximately 550 s and the end of the flow period, however, a PRF may be identified. The recovery period indicates an approximate PLF or possibly an apparent NFB and no unambiguous evaluation of transmissivity can be performed on this period. A residual pressure of c 4 m remained at the end of the recovery period. During the entire test the pressure, in both the section above and below the test section is affected by drilling activities in KFM09B. It is therefore possible that also the test section is affected, and that this could explain the unstable flow and pressure in the beginning of the test. At the time when the test was performed, drilling was conducted at c 121–124 m (borehole length), which is just above the tested section when measured as vertical depth.

146.0–166.0 m

The first c 500 s of the injection period exhibits rather unstable flow rate and pressure and no clear flow regimes can be identified. There are indications of an apparent PRF at the end of the flow period but no good fit using a model for radial flow is possible. An apparent low skin factor may indicate a flow regime of lower dimension than two during the injection period, and transient evaluation with the Ozkan-Raghavan model is used. During the recovery period only a PLF or possibly an apparent NFB is developed. A residual pressure of c 11 m remained at the end of this period, possibly indicating a flow feature of limited extent, i.e. decreasing fracture aperture away from the borehole. No unambiguous transient evaluation of transmissivity is possible on the recovery period. During the entire test the pressure, especially in the section above the test section, is affected by drilling activities in KFM09B.

166.0–186.0 m

The injection period is dominated by a PSF. Evaluation of transmissivity gives rather consistent results for models assuming radial flow and leaky flow, respectively. The recovery period initially exhibits a PLF or possibly WBS transitioning to a possible PRF after c 100 s of the recovery period. The section above the test section is clearly affected by pumping activities in KFM09B for the duration of the test. A possible, but most likely a secondary, effect can also be observed in the section below the test section, indicating that the test section might also be affected by pressure interference from the drilling activities.

186.0–206.0 m

Although the inverse flow rate derivative is quite scattered, the injection period is believed to be dominated by a PSF from c 200 s throughout the period. The injection pressure was not stable until 200 s into the test. Evaluating the injection period using a model for a 3D leaky flow, transmissivity values are similar to those derived with models for radial flow. The recovery period only displays WBS and a transition period and no unambiguous transient evaluation is possible on the recovery period. The pressure above the test section was heavily affected by drilling activities in KFM09B.

206.0–226.0 m

The test section has a very low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, the injection time was shortened. As a result TM, based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section. Since the measurement noise with a zero flow was centred slightly below zero, the flow rate measurement limit was manually elevated $2.43 \cdot 10^{-9}$ m^3/s. The pressure above the test section is clearly affected by the drilling activity in KFM09B.

226.0–246.0 m

The injection period shows a rather well-defined PRF from c 300 s. The recovery period is dominated by WBS and a transition to some other flow regime. No unambiguous transient evaluation can be made on the recovery period. The pressure above the test section is clearly affected by the drilling activity in KFM09B during the test.

238.0–258.0 m

Although the flow rate derivative is rather scattered a PRF is interpreted to dominate the injection period. The derivative is pretty stable between 200 and 800 s, after which time it drops suddenly. This apparent decrease in the derivative may possibly be an effect of the automatic pressure regulation and not necessarily a true characteristic of the formation. During the recovery period only WBS and a transition period is observed. An approximate evaluation using the Dougherty-Babu model during the recovery period is consistent with the evaluation from the injection period. The pressure in the section above the test section is clearly affected by drilling activities in KFM09B for the entire duration of the test. A possible, but most likely secondary, effect can also be observed in the section below the test section.

258.0–278.0 m

The flow rate during the injection period is rather unstable. Still, a transition to a possible PRF is weakly indicated between c 100 and 600 s. After this time, an apparent NFB is indicated. The recovery period exhibits WBS and a transition period towards an assumed PRF from c 200 s until the end of the recovery period. The residual pressure at the end of the recovery period is c 7 m, possibly indicating a hydraulic feature of limited extent, i.e. decreasing fracture aperture away from the borehole. Since the interpretation of the injection period is rather uncertain, the evaluation from the recovery period is considered to provide the most representative value of transmissivity for this section. The pressure in the section above the test section is clearly affected by drilling activities in KFM09B for the duration of the test. A possible, but most likely secondary, effect can also be observed in the section below the test section.

278.0–298.0 m

The pressure above the test section is strongly affected by the progressing drilling activity in KFM09B close to this hole. The injection period shows two separate PRF of which the first has a slightly higher transmissivity than the s. The recovery is clearly indicating a PRF after 600 s, preceded by WBS. The residual pressure at the end of the recovery period is c 6 m, possibly indicating a hydraulic feature of limited extent, i.e. decreasing fracture aperture away from the borehole.

286.0–306.0 m

The injection period is dominated by an intermediate flow regime between PLF and PRF. Evaluation with the Ozkan-Raghavan model for a single fracture and the Hurst-Clark-Brauer model for PLF and PRF, respectively provides consistent results. The recovery indicates WBS and a transition period. Transient evaluations using different models show rather low transmissivity compared to T_M. The pressure above the test section is clearly affected by the drilling activity in KFM09B.

306.0–326.0 m

Both the injection- and recovery period show an early, short PRF followed by an apparent NFB. The high residual pressure at the end of the recovery period is c 13 m, which may indicate a hydraulic feature of limited extent, i.e. decreasing fracture aperture away from the borehole. The pressure above the test section is strongly affected by the ongoing drilling activity in KFM09B close to this borehole.

326.0–346.0 m

The injection period is dominated by a PRF. The recovery period starts with WBS and is then transitioning towards a possible PRF. The pressure above the test section is strongly affected by the ongoing drilling activity in KFM09B close to this borehole.

346.0–366.0 m

The flow rate derivative during the injection period is slowly increasing up to 300 s where it flattens out, which implies a PLF transitioning towards a PRF. The recovery starts with WBS and then transitions towards a possible PRF. The residual pressure at the end of the recovery period was c 4 m. The pressure above the test section is strongly affected by the ongoing drilling activity in KFM09B close to this borehole.

366.0–386.0 m

The injection period is dominated by a well-defined PRF starting after c 200 s and lasts throughout the injection period. The recovery period is also dominated by a well-defined PRF throughout the period. The pressure above the test section is clearly affected by drilling activities in KFM09B.

386.0–406.0 m

The injection period indicates a PLF or possibly an apparent NFB. The recovery period also indicates a PLF, possibly transitioning to an apparent NFB. An approximate transient evaluation was made from the recovery period. The residual pressure at the end of the recovery period is c 11 m, possibly indicating a hydraulic feature of limited extent, i.e. decreasing fracture aperture away from the borehole. The pressure above the test section is clearly affected by drilling activities in KFM09B.

406.0–426.0 m

The injection period indicates a PRF from c 100 s. After c 1,000 s a decrease in the derivative suggests a higher dimensional flow regime, e.g. a PSF. The pressure recovery shows a rather strange behaviour. Initially, a period affected by WBS is shown. After 40 s, the pressure recovery suddenly drops, visible as a knee in the recovery plots. After this time, transition to an apparent NFB is indicated. The responses during the injection- and recovery period are thus not consistent. The residual pressure at the end of the recovery period is c 5.5 m, possibly indicating a hydraulic feature of limited extent, i.e. decreasing fracture aperture away from the borehole. The transmissivity from the steady-state evaluation, $T_{M,}$ is regarded as the representative transmissivity value in the section. The pressure above the test section is strongly affected by the ongoing drilling activity in KFM09B close to this borehole.

426.0–446.0 m

The pressure above the test section is influenced by the drilling in KFM09B close to this borehole. The pressure below the test section was increasing during the entire test sequence. The injection period is dominated by an apparent NFB. By the end of the injection period the flow rate temporarily increased, possibly due to a minor flow in the rock around the packer as reflected by a decreasing (inverse) flow rate derivative. Despite the rather high flow rate during the injection period the pressure only recovered c 5 m from the applied injection head of 22 m water column. This fact may possibly indicate a fracture with a large aperture near the borehole and successively decreasing aperture away from the borehole. The dominating flow regime during the recovery period seems to be an intermediate between PLF and an apparent NFB. Two different models were tested for evaluation of the recovery period. The Dougherty-Babu model and the Ozkan-Raghavan model both give consistent results, which are also consistent with the steady-state transmissivity T_M. However, the evaluations are regarded as uncertain in this borehole section and in particular, the transmissivity value to be selected as the representative one. The transmissivity from the steady-state evaluation (T_M) is chosen as the representative for the section.

446.0–466.0 m

The section above is affected by drilling. It is however possible that some of the pressure increase (c 2.5 kPa) in the section above is caused by interference with the test section. Since the transmissivity above is much higher than in the test section, this relatively small pressure interference may have caused an overestimation of transmissivity in the section 446.0–466.0 m. The time to achieve constant pressure in the test section was relatively long. After this the injection period is clearly dominated by a PRF starting after c 200 s and continuing throughout the injection period. The recovery period starts with a WBS followed by a transition to some other flow regime, possibly a PRF.

466.0–486.0 m

The injection period indicates a PLF and a transition period towards a possible PRF. The recovery period starts with WBS transitioning into an approximate PRF after c 100 s, lasting to c 400 s. After this time a transition to an apparent NFB is indicated. The transient evaluation of the injection period is regarded as uncertain, and hence the transient evaluation of the recovery period is selected as the most representative for the section.

486.0–506.0 m

The injection pressure in this test is somewhat unstable throughout the test. After 12 minutes there was a change from regulation valve 3 to valve 2 which caused an increase of the injection pressure of about 5 kPa. The pressure above the test section is influenced by the drilling in KFM09B right next to this borehole. During the injection period a PLF is dominating. The recovery period is dominated by WBS and a transition period. The residual pressure at the end of the recovery period is c 11 m, indicating a low-transmissivity borehole section.

506.0–526.0 m

There is some interference with the section above the test section during the injection period. The injection indicates a short PRF between 100 and 200 s followed by a transition to a PSF. No unambiguous evaluation could be made on the injection period, neither by the Hurst-Clark-Brauer- or the Hantush’ model. The recovery period starts with initial WBS followed by a transition period, and transient evaluation from the recovery period is regarded as a representative estimate of transmissivity.

526.0–546.0 m

Due to an unfortunate change of valve during the early phase of the injection period, the time to get stabilized pressure became long, but this fact did not affect the possibilities to evaluate the test. The injection period is dominated by an apparent NFB throughout the period. The recovery period, however, is dominated by a PRF from c 100 s throughout the period. Despite the rather high transmissivity, the pressure only recovers c 3 m from the applied head change of c 20 m water column. This fact may possibly indicate a fracture with a large aperture near the borehole and decreasing aperture away from the borehole.

545.0–565.0 m

The test section has a very low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, in accordance with AP PF 400-05-104, the injection time was shortened. As a result, T_M based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section. The period of measured recovery showed a pressure increase indicating that the section is of such low transmissivity that packer expansion affects the pressure throughout the period. Since the measurement noise with a zero flow was centred slightly below zero, the flow rate measurement limit was manually elevated by $3.65 \cdot 10^{-9}$ m^3/s.

566.0–586.0 m

The test section has a very low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, in accordance with AP PF 400-05-104, the injection time was shortened. As a result, TM based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section. The period of measured recovery only showed a pressure increase indicating that the section is of such low transmissivity that packer expansion affects the pressure throughout the period. Since the measurement noise with a zero flow was centred slightly below zero, the flow rate measurement limit was manually elevated by $2.43 \cdot 10^{-9}$ m^3/s.

586.0–606.0 m

The test section has a very low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, in accordance with AP PF 400-05-104, the injection time was shortened. As a result, T_M based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section. The period of measured recovery only showed a pressure increase, indicating that the section is of such low transmissivity that packer expansion affects the pressure throughout the period.

606.0–626.0 m

The injection period is dominated by a PRF between 50 and 300 s transitioning to an apparent NFB. The same flow regimes dominate the recovery period, a PRF between 20 and 200 s (Agarwal time) followed by an apparent NFB.

626.0–646.0 m

During the beginning of the test, a change of valves occurred which makes the time to reach a stable injection pressure somewhat longer than usual. This fact does however not affect the possibility to evaluate the test. Although large flow rate fluctuations, a PRF can be identified after c 200 s lasting throughout the injection period. The recovery period starts with WBS followed by a transition to some other flow regime, possibly a PRF. The evaluation from the recovery period was chosen as the representative.

646.0-666.0 m

Although large flow rate fluctuations, a PRF can be identified after c 50 s lasting throughout the injection period. The recovery period starts with a WBS followed by a transition period.

666.0–686.0 m

The entire injection period is dominated by a PLF. The recovery period is dominated by WBS and a transition phase. The residual pressure at the end of the recovery period is c 11.5 m, indicating a rather tight section.

686.0–706.0 m

This section has a low transmissivity. There is a possible interference with the section above (Pa) during the injection period, but the effects are not noticed until after c 10 minutes of the injection period. The entire injection period is dominated by a PLF. The recovery period is initially dominated by WBS followed by a transition sequence. The transient evaluation on both the injection- and recovery period is uncertain.

691.0–711.0 m

The test section has a low transmissivity. Since the final flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, in accordance with AP PF 400-05-104, the injection time was shortened. As a result, T_M based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section.

711.0–731.0 m

The test section has a very low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, in accordance with AP PF 400-05-104, the injection time was shortened. As a result, T_M based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section. The period of measured recovery only showed a pressure increase, indicating that the section is of such low transmissivity that packer expansion affects the pressure throughout the period. The pressure above the test section is affected by the ongoing drilling in KFM09B close to this borehole.

731.0–751.0 m

Since the flow rate was quite low the automatic regulation system had difficulties of keeping the pressure constant during the entire injection period. Although the pressure was oscillating around an average value, and hence the data, especially the derivative is quite scattered, a PRF is indicated from c 20 s throughout the injection period. The recovery period shows initial WBS and a transition phase. Since the data from the injection period is scattered and the recovery period provides an unambiguous transient evaluation, the value from the recovery period is regarded as the most representative for the section. The pressure in the section above the test section was possibly affected by the drilling of the adjacent borehole KFM9B. It is however possible that some of the pressure changes observed in the section above has to do with interference between the test section and the section above.

751.0–771.0 m

During the injection period an early PLF transitioning towards an approximate PRF is indicated. The transient evaluation using the Hurst-Clark-Brauer model is regarded as giving the best estimate of transmissivity. The recovery period indicates WBS transitioning to some other flow regime. The parameter fitting using the Dougherty-Babu model supports the value obtained from the injection period.

771.0–791.0 m

The injection period indicates a possible PRF from c 100 s until 500 s which is then transitioning to a PSF. During the recovery period only WBS transitioning to some other flow regime is observed. Since the PRF is not obvious and the fitting with the PSF model by Hantush is very good for both the injection- and recovery period the evaluation from the injection period with the Hantush model is chosen as the representative evaluation. Interference with the section below is observed. The pressure in the section above is varying, probably caused by the drilling of the adjacent borehole KFM09B.

106.0–111.0 m

Although the flow rate derivative is rather scattered a PSF is assumed to dominate the injection period. The initial phase of the recovery period displays a flow regime between WBS and a PLF transitioning to a possible PSF which is interrupted by an apparent NFB lasting until the end of the recovery period. The section above the test section is clearly affected by drilling activities in KFM09B. A possible, but most likely a secondary, interference effect can also be observed in the section below the test section.

111.0–116.0 m

Although the data is pretty scattered a PSF is believed to dominate the injection period. During the recovery period an initial WBS develops into a PRF from c 500 s to the end of the recovery period. The transmissivity values determined from the injection- and recovery periods are consistent. The pressure in both the section above and below the test section, are affected by drilling activities in KFM09B.

116.0–121.0 m

During the injection period a PRF is indicated from c 50 s until c 400 s where a s PRF with slightly lower transmissivity starts and continues throughout the period. The recovery period also indicates a PRF from c 30 s until c 400 s. It is then transitioning to a NFB.

121.0–126.0 m

The injection and the recovery periods show similar characteristics with two consecutive periods of PRF. The injection period indicates the first PRF between c 80 s and 350 s, and the s period of PRF lasts from c 700 s to the end of the injection period. The first period of PRF during the recovery period is indicated between c 50 and 250 s. The s period starts shortly after that at c 300 s and lasts until the end of the recovery period. Transmissivity values obtained from the transient evaluation of the recovery period are slightly higher than those from the injection period. The pressure above the test section is affected by drilling activities in KFM09B. Also the pressure below the test section is affected by the drilling activities but only before the start of the injection.

126.0–131.0 m

An apparent NFB is believed to dominate the entire injection period. The pressure exhibits an oscillating behaviour, related to the problems with the pressure regulation, during the first half of the injection period. No good model fit can be made on the injection period however. The recovery period is dominated by a clear PLF. A model fit can be made on the recovery period using a model for one-dimensional flow. The residual pressure is c 13 m at stop of recovery which possibly may indicate a fracture of limited extent, i.e. with decreasing fracture aperture away from the borehole. The pressure above the test section is affected by drilling activities in KFM09B. Also the pressure below the test section is affected by the drilling activities but only before the start of the injection.

128.0–133.0 m

The beginning of the injection period is dominated by a transition period, possibly PLF, up until c 500 s, where a probable PSF develops, lasting to the end of the injection period. The recovery period initially exhibits a PLF which transitions into a possible PRF at c 500 s lasting throughout the recovery period. There are indications of pressure interference in the section below the test section. The pressure increases (c 4 kPa). This is interpreted as an indication of an open hydraulic connection between the two sections. Since the transmissivity below is much higher than in the section, this relatively small pressure interference may have caused an overestimation of transmissivity in the section 128.0–133.0 m. The pressure above the test section is influenced by drilling activities in KFM09B during the test.

133.0–138.0 m

The dominating flow regime during the injection appears to be a PSF. The recovery starts with a short period of WBS, possibly transitioning to an apparent NFB, followed by a transition period by the end. No unambiguous transient evaluation could be performed on either the injection-, or the recovery period. To get consistent transmissivities with the injection period, a very high value on the radius of the fictive standpipe, representing the wellbore storage, must be assumed during the recovery period. Alternatively, an apparent NFB may be assumed. The section above the test section is influenced by the drilling in KFM09B. There is also some interference with the section below during the injection, indicating a possible shortcut flow across the packer.

138.0–143.0 m

The injection pressure was fluctuating a couple of kPa throughout the injection. The injection starts with a transition to a PRF initiated after 100 s lasting the entire injection period. The flow during the recovery is dominated by a transition state and a possible short period of PRF from 300 to 500 s. The pressure in the section above is influenced by the drilling in KFM09B.

141.0–146.0 m

The pressure in the section above is influenced by the drilling in KFM09B. There is some interference with the section below at the time when the injection starts. The flow during the injection starts with a transition state that ends up in a late PRF after about 400 s, continuing throughout the injection period. During the beginning of the recovery period a short PLF is indicated, probably transitioning to an apparent NFB, followed by a short transition period by the end. The residual pressure was c 8 m at stop of recovery, possibly indicating a hydraulic feature of limited extent, i.e. decreasing fracture aperture away from the borehole.

No unambiguous transient evaluation could be performed on the recovery period. To get consistent transmissivities with the injection period, a high value on the radius of the fictive standpipe, representing wellbore storage, must be assumed during the recovery period.

146.0–151.0 m

The pressure in the section above is probably influenced by the drilling in KFM09B. Pressure interference is observed in the interval below the test section during the injection period. The flow during the injection is dominated by an apparent NFB, possibly transitioning to some other flow regime by the end of the period. No transient evaluation can be made on the injection period. The recovery period is dominated by a PLF. The residual pressure was c 17 m at the end of the recovery which fact, together with the observed flow regime during the injection period, possibly indicates a fracture of limited extent, i.e. decreasing fracture aperture away from the borehole. A model for a single fracture was used for the transient evaluation of the recovery period. This value is chosen as most representative for the section.

151.0–156.0 m

The test section has a very low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, in accordance with AP PF 400-05-104, the injection time was shortened. As a result, T_M based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section. The period of measured recovery only showed a pressure increase indicating that the section is of such low transmissivity that packer expansion affects the pressure throughout the period.

156.0–161.0 m

The section above test section is strongly affected by the drilling in KFM09B. There is some pressure interference in the section below during the injection. The injection period indicates a PLF possibly transitioning towards a PRF after c 600 s. Models for linear- and radial flow, respectively give consistent results from the injection period although a very high, negative skin factor is indicated by the latter model. Both the pressure and flow is a little unstable the first minutes during the injection, probably due to a valve change in the beginning of the test period. The recovery is dominated by a PLF/NFB the entire period; no transient evaluation is possible on this period. The residual pressure is c 12 m at the end of recovery. The combined responses during the injection- and recovery periods may indicate a flow feature of limited extent, i.e. decreasing fracture aperture away from the borehole.

161.0–166.0 m

The time to achieve a stable injection pressure was unusually long, since the section had a much lower transmissivity than expected. The injection period shows a rapidly decreasing derivative and hence interpreted as a PSS. No unambiguous transient evaluation could be made on the injection period. The recovery only indicates WBS transitioning to PSS and no unambiguous transient evaluation is possible. Since the transient evaluations during both the injection- and recovery period are uncertain and the flow regime is close to PSS, T_M was considered to be the most representative transmissivity value for this section. The pressure above the test section (Pa) is clearly affected by drilling activities in KFM09B.

166.0–171.0 m

The injection period is dominated by a PSF. Transient evaluation using the Hurst-Clark-Brauer and the Hantush models give similar results. The recovery period shows an initial PLF transitioning to a possible PRF.

171.0–176.0 m

The flow rate during the injection period is quite scattered due to the regulation and the low flow rate. Still, the injection and recovery periods are clearly dominated by a NFB and WBS, respectively, and no transient evaluation is possible. T_M was therefore considered to be the most representative transmissivity value for this section.

176.0–181.0 m

The flow rate data are quite scattered during the injection period. There are signs of a PRF and it is assumed that it dominates the period from 50 s and throughout the period. The first part of the recovery period is dominated by WBS. It eventually transitions to what seems to be a NFB. Hence, no transient evaluation of the recovery period is possible.

181.0–186.0 m

The injection period displays a flat derivative, which should imply a PRF during this period. However, a fit with Hurst-Clark-Brauer model to this period is not possible. An apparent NFB is therefore suspected to dominate the injection. The recovery period only shows WBS. Hence, transient evaluation is not possible of either the injection or the recovery period. T_M was therefore considered to be the most representative transmissivity value for this section.

186.0–191.0 m

A PRF is clearly dominating the injection period. The recovery only displays WBS and a transition to some other flow regime. No transient evaluation gives satisfying results from the recovery period.

191.0–196.0 m

The test section has a low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, the injection time was shortened. As a result T_M, based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section.

196.0–201.0 m

The test section has a low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, the injection time was shortened. As a result T_M, based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section.

201.0–206.0 m

The test section has a very low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, the injection time was shortened. As a result T_M, based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section. The period of measured recovery only showed a pressure increase, indicating that the section is of such low transmissivity that packer expansion affects the pressure throughout the period.

226.0–231.0 m

The test section has a low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, the injection time was shortened. As a result T_M, based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section.

232.0–237.0 m

Both the injection and recovery periods are showing signs of a dominating PSF and give pretty similar results using the Hantush model. The pressure increases (c 2 kPa) in the section below, which might indicate a connection between the two sections. Since the transmissivity below is much higher than in the test section this relatively small pressure interference may have caused an overestimation of transmissivity in the section 232.0–237.0 m.

237.0–242.0 m

The injection is clearly dominated by a PRF from 50 s and throughout the period. The recovery is initially very fast, and a PSF is indicated followed by an increasing derivative which is interpreted as an apparent NFB. The responses during the injection- and recovery periods are thus not consistent. The test is very similar to the test above, and possibly the same connected flow feature is measured in this test and in the previous section.

240.8–245.8 m

A PSF is assumed to dominate the injection period. Transient evaluations using the Hantush and Hurst-Clark-Brauer models give similar results. The recovery only displays WBS and a transition period to some other flow regime. However, a fit with the Dogherthy-Babu model to the recovery supports the evaluations from the injection period.

246.8–251.8 m

The test section has a very low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, in accordance with AP PF 400-05-104, the injection time was shortened. As a result, T_M based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section. The period of measured recovery only showed a pressure increase, indicating that the section is of such low transmissivity that packer expansion affects the pressure throughout the period.

251.5–256.5 m

The test section has a very low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, the injection time was shortened. As a result T_M, based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section. The period of measured recovery only showed a pressure increase, indicating that the section is of such low transmissivity that packer expansion affects the pressure throughout the period.

256.5–261.5 m

The test section has a low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, the injection time was shortened. As a result T_M, based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section.

273.0–278.0 m

Due to a drift in the gas pressure regulator, the pressure in the test section decreased by c 2 kPa. Hence, the flow rate may be affected during the injection period. Still, the injection period indicates two separate periods of PRF. The first has a higher transmissivity than the s. The recovery period shows a WBS transitioning to a PRF between 200 and 600 s. After 600 s of the recovery an increasing derivative could be interpreted as a NFB. On the other hand it could also be interpreted as a transition to a s PRF as in the case of the injection. Also, the transient evaluations of the recovery and the first PRF period of the injection period are very similar.

278.0–283.0 m

Due to a drift in the gas pressure regulator, the pressure in the test section decreased by c 1 kPa. Hence, the flow rate may be slightly affected during the injection period. Still, the injection period clearly shows a PLF followed by a PRF. The PRF transitions after a while to a NFB. The recovery also displays a PLF transitioning to some other flow regime. The end of the recovery has a derivative that is almost flat and may therefore be interpret as a PRF. Transient evaluation using the Hurst-Clark-Brauer (injection), Dougherty-Babu (recovery) and Ozkan-Raghavan (both periods) models all result in similar transmissivities.

283.0–288.0 m

The test section has a low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, the injection time was shortened. As a result T_M, based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section.

288.0–293.0 m

A pressure build-up was observed in the borehole interval below the test section throughout the test. The flow rate is low which results in a scattered derivative. However, a possible PLF is weakly indicated during the injection period. The transient evaluation of the injection period should be regarded as uncertain. The recovery is dominated by WBS throughout the period and no unambiguous transient evaluation is possible. Thus, T_M was considered to be the most representative transmissivity value for this section.

293.0–298.0 m

The pressure above the test section is clearly influenced by the drilling in KFM09B. There is a pressure build-up below the test section throughout the entire test sequence. The dominating flow regime during the injection period is a PRF that starts almost immediately and lasts for the entire injection period. The recovery is initially dominated by WBS. Thereafter, a PRF is indicated that lasts until 300 s where the derivative apparently levels off. However, no good fit to a PRF-model was achieved for the period after 300 s with an apparently flat derivative which possibly could imply some other flow regime than a PRF.

296.0–301.0 m

The test section has a low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, the injection time was shortened. As a result TM, based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section. Since the measurement noise with a zero flow was centred slightly below zero, the flow rate measurement limit was manually elevated by $3.65 \cdot 10^{-9}$ m^3/s.

301.0–306.0 m

The test section has a low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, the injection time was shortened. As a result T_M, based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section.

306.0–311.0 m

The test section has a very low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, the injection time was shortened. As a result T_M, based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section. The period of measured recovery only showed a pressure increase, indicating that the section is of such low transmissivity that packer expansion affects the pressure throughout the period. The section above the test section is affected by the drilling in KFM09B.

311.0–316.0 m

The test section has a low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, the injection time was shortened. As a result T_M, based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section. The section above the test section is affected by the drilling in KFM09B.

316.0–321.0 m

The test section has a low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, the injection time was shortened. As a result T_M, based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section. The section above the test section is affected by the drilling in KFM09B.

321.0–326.0 m

The pressure in the section above is influenced by the drilling in KFM09B. There is also pressure build-up below the test section throughout the entire test sequence. The injection period indicates an early PFR transitioning to an apparent NFB lasting throughout the period. The recovery is dominated by a PLF/NFB. No reliable transient evaluation of the recovery is possible. The residual pressure was c 13.5 m at stop of recovery which may indicate a flow feature of limited extension, i.e. decreasing fracture aperture away from the borehole.

346.0–351.0 m

The test section has a very low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, in accordance with AP PF 400-05-104, the injection time was shortened. As a result, T_M based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section. The period of measured recovery only showed a pressure increase, indicating that the section is of such low transmissivity that packer expansion affects the pressure throughout the period. The section above the test section is affected by the drilling in KFM09B.

351.0–356.0 m

The injection period clearly shows a PRF starting at 30 s, continuing throughout the injection period. The recovery period demonstrates a WBS transitioning to a possible PRF. The pressure in the section below increases during the whole test sequence, probably due to higher formation pressure deeper down in the borehole.

356.0–361.0 m

The test section has a low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, the injection time was shortened. However, it was not until after 18 minutes of the injection period that the flow rate became lower than the detection limit. As a result T_M, based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section. Since the measurement noise with a zero flow was centered slightly below zero, the flow rate measurement limit was manually elevated by $2.43 \cdot 10^{-9}$ m^3/s.

361.0–366.0 m

The flow rate is low, close to the measurement limit and hence the data, especially the flow derivative is quite scattered. Despite this fact a PRF is indicated from c 20 s lasting throughout the injection period. The recovery period shows a WBS transitioning to some other flow regime. No unambiguous transient evaluation could be made from the recovery period. Since the measurement noise with a zero flow was centred slightly below zero, the flow rate measurement limit, as well as the flow data, was manually adjusted (elevated) by $2.43 \cdot 10^{-9}$ m^3/s.

363.0–368.0 m

Due to the low transmissivity of the test section the flow data for the injection period are scattered. Hence a high filter factor for the inversed flow derivative is used to avoid getting negative derivative points. However, the trend is unambiguous and a PRF is indicated from c 80 s throughout the injection period. For the recovery period a WBS is indicated the first 100 s. From 100 s to the end of the recovery period a transition is indicated. No PRF is developed during the recovery period but an unique type curve fit supported by the agreement with the injection period is presented. Transient evaluation of the injection period is considered to be the most representative.

368.0–373.0 m

The test section has a low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, the injection time was shortened. As a result T_M, based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section. Since the measurement noise with a zero flow was centred slightly above zero, the flow rate measurement limit was manually lowered by $3.65 \cdot 10^{-9}$ m^3/s.

371.0–376.0 m

The injection pressure vessel was emptied during the injection period. This caused gas to flow into the injection system with the consequence that the registered flow showed erratic values. In order to avoid the need for rerunning the test the regulator valves were closed manually. Due to this procedure the injection test time was shortened to c 900 s. In spite of the shortened injection period, satisfying transient evaluation was possible. During the injection period a PRF is indicated from c 100 s to 600 s. Due to the procedure described above the scan interval was affected for the recovery period giving sparse data for the first 100 s. The type curve fit for the available data points is very good from c 20 s. From c 200 s to the end of the recovery period a PRF is dominating. Transient evaluation of the injection period is chosen as the best evaluation.

376.0–381.0 m

The test section has a low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, the injection time was shortened. As a result T_M, based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section.

381.0–386.0 m

The test section has a low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, the injection time was shortened. As a result T_M, based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section.

386.0–391.0 m

The injection period only demonstrates an apparent NFB, and no transient evaluation can be made on the period. The recovery period seems to indicate an intermediate flow regime between a PLF and an apparent NFB. The transient evaluation from this period is regarded as rather uncertain; hence T_M is regarded as the most representative value of transmissivity in the section.

391.0–396.0 m

The section above the test section is strongly affected by the drilling in KFM09B. The injection starts with a PRF that transforms into a PSF after about 200 s and lasts during the rest of the injection. The recovery starts with a WBS followed by a transition to some other flow regime. Transient evaluation using the Hurst-Clark-Brauer and the Hantush models, for both the injection and recovery periods, all result in similar transmissivities. However, the Hantush model on the recovery does not converge unless some of the parameters are assumed.

396.0–401.0 m

The test section has a low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, in accordance with AP PF 400-05-104, the injection time was shortened. As a result, T_M based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section. The section above the test section is affected by the drilling in KFM09B.

401.0–406.0 m

The pressure above the test section is influenced by the drilling in the nearby KFM09B. The injection period has a short PRF between c 100–250 s transitioning to an apparent NFB by the end of the period. The recovery starts with a WBS followed by a transition period which is interrupted by an apparent NFB after about 400 s (Agarwal time).

406.0–411.0 m

The test section has a low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, in accordance with AP PF 400-05-104, the injection time was shortened. As a result, T_M based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section. Since the noise level in the flow measurement had been drifted a bit below zero, the Q/s-measl-L chosen for this test was elevated one A/D-level higher to compensate for this drift. The section above the test section is affected by the drilling in KFM09B.

411.0–416.0 m

The injection starts with a short PRF that lasts between 20 and 100 s. The flow is then transitioning to another PRF that starts after c 400 s and lasts throughout the injection period. The flow during the recovery is dominated by an initial short PRF that lasts between 10 and about 100 s (Agarwal time) followed by a transition to an apparent NFB. The residual pressure was c 7 m at the end of the recovery which fact may indicate a flow feature of limited extent, i.e. decreasing fracture aperture away from the borehole. The pressure above the test section is still affected by the drilling in KFM09B.

414.0–419.0 m

Due to the drift of the zero level for the measurements of the flow, a correction of both the rates and Q/s-measl-L by $2.42 \cdot 10^{-9}$ m^3/s was made to get a correct evaluation of the test. The injection has a low but detectable flow and is dominated by a PRF during the entire period. Dominating flow regime during the recovery is WBS followed by a transition period. No unambiguous transient evaluation could be made on the recovery period. Evaluation with the Dougherty-Babu model on the recovery period gives an unreasonably high skin factor. The section above the test section is affected by the drilling in KFM09B.

419.0–424.0 m

The injection starts with a PRF between about 30 and 600 s. The flow then makes a transition into a s PRF that lasts during the rest of the period. Recovery starts with a WBS that goes into a transition phase into a PRF that appears after about 400 s. The pressure above the test section is somewhat effected by the drilling in KFM09B.

421.0–426.0 m

The injection period is dominated by a PRF from c 20 s to the end of the period. For the recovery period there are indications of WBS up to c 20 s transitioning to a PRF from c 30 s throughout the period. A flow regime of higher dimension is only slightly indicated by the end of the period. The interpreted parameters of the injection period are in very good agreement with the interpreted parameters of the recovery period. The representative parameter values are selected from the injection period.

426.0–431.0 m

The test section has a low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, in accordance with AP PF 400-05-104, the injection time was shortened. As a result, T_M based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section.

431.0–436.0 m

The pressure increases (c 5 kPa) in the section below. Since the transmissivity below is lower than in the test section, this relatively small pressure interference should not have a major impact on the test performed in the section. The time to achieve constant pressure was 112 s. The injection period is totally dominated by an apparent NFB and no transient evaluation is possible on this period. The recovery period is dominated by a PLF transitioning towards a possible PRF but interrupted by an apparent NFB after c 300 s. The pressure recovery is only c 5 m which indicates a flow feature of limited extension, i.e. decreasing fracture aperture away from the borehole. The same flow feature is assumed to dominate the responses during the corresponding tests in 20 m and 100 m, respectively. No clear PRF is developed during the recovery period. Hence the steady-state evaluation is considered to be the most representative for this test.

436.0–441.0 m

The test section has a very low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, the injection time was shortened. As a result T_M, based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section. The period of measured recovery only showed a pressure increase, indicating that the section is of such low transmissivity that packer expansion affects the pressure throughout the period.

441.0–446.0 m

The injection period is totally dominated by an apparent NFB. Noticeable is that the final flow is very low (c 12 mL/min) considering the relatively high inital flow. This fact is in agreement with the interpreted flow regimes of both periods. No transient evaluation is possible on the injection period. The recovery period is dominated by a PLF transitioning towards a possible PRF but interrupted by an apparent NFB by the end. The pressure recovery in this rather transmissive section is only c 2 m which indicates a flow feature of limited extension, i.e. decreasing fracture aperture away from the borehole. Only an approximate transient evaluation could be made on the recovery period. Hence the steady-state evaluation is considered to be the most representative for this test.

446.0–451.0 m

After a transition period an apparent NFB dominates the injection period. No unambiguous transient evaluation is possible on this period. The recovery is dominated by a PLF, probably transitioning to an apparent NFB by the end. The pressure recovery is only c 5 m which indicates a flow feature of limited extension, i.e. decreasing fracture aperture away from the borehole. The pressure above the test section is somewhat affected by the drilling in KFM09B.

451.0–456.0 m

This section has a very low but detectable flow. The pressure above the test section is affected by the drilling in KFM09B. The injection period shows a possible PRF transitioning to PSF. During the recovery period WBS is dominating. No unambiguous transient evaluations can be made on either the injection period, or the recovery period. Thus, the stationary evaluation is considered as the most representative for this section.

456.0–461.0 m

The injection period is dominated by a PRF between c 20–600 s transitioning to an apparent NFB by the end. The recovery starts with WBS and a transition period which is interrupted by an apparent NFB. The pressure above the test section is affected by the drilling in KFM09B.

461.0–466.0 m

The test section has a very low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, in accordance with AP PF 400-05-104, the injection time was shortened. As a result, T_M based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section. The period of measured recovery only showed a pressure increase, indicating that the section is of such low transmissivity that packer expansion affects the pressure throughout the period. The section above the test section is affected by the drilling in KFM09B.

471.0–476.0 m

The injection period starts with a PLF and continues until c 1,000 s where an indication of a PSF is noted. The recovery starts with a transition into a PLF that continues for the rest of the period. Transient evaluation using the Hurst-Clark-Brauer (injection), Dougherty-Babu (recovery) and Ozkan-Raghavan (both periods) models all result in similar transmissivities. The pressure above the test section is affected by the drilling in KFM09B.

476.0–481.0 m

During the first part of the injection period a short period of PRF is indicated which is transitioning to an apparent NFB. The recovery period starts with a short WBS and then turns into a transition stage. By the end of the period an apparent NFB is identified. The T-value estimated from the recovery period is similar as for the injection period. The section above the test section is affected by the drilling in KFM09B.

486.0–491.0 m

The test section has a low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, the injection time was shortened. As a result T_M, based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section. Since the measurement noise with a zero flow was centred slightly above zero, the flow rate measurement limit was manually lowered by $3.65 \cdot 10^{-9}$ m^3/s.

491.0–496.0 m

At the beginning of the injection period a short PRF is indicated from c 60–100 s, then transitioning to an apparent NFB to the end of the period. During the recovery period there is initially a WBS up to c 50 s followed by a transition period which is interrupted by an apparent NFB at the end. No PRF is developed during the recovery period. The transient evaluation of the injection period is chosen as the most representative.

496.0–501.0 m

An unfortunate change to the smallest regulation valve half way into the injection period caused the pressure regulation to be unstable during the s half of the period. This contributed to the scattering of data but is not considered to significantly affect the analysis of the test. The injection period shows strong signs of an apparent NFB throughout the period. No unique transient evaluation is possible on this period. The recovery period indicates a PLF transitioning to an apparent NFB and transient evaluation using the Ozkan-Raghavan solution is regarded as the best estimate of transmissivity in the section. The pressure recovery was only c 8 m which might indicate a flow feature of limited extension, i.e. decreasing fracture aperture away from the borehole.

501.0–506.0 m

The test section has a low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, in accordance with AP PF 400-05-104, the injection time was shortened. As a result, T_M based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section.

506.0–511.0 m

This test section has a low but detectable flow. Since the noise level in the flow measurements had drifted a bit below zero, the Q/s-measl-L chosen for this test, as well as the flow data, were set $3.65 \cdot 10^{-9}$ m^3/s higher to compensate for this drift. The injection starts with an apparent NFB transitioning to a PSF after about 200 s. The flow during the recovery is totally dominated by WBS during the entire period. The section above the test section is affected by the drilling in KFM09B.

511.0–516.0 m

The injection period is dominated by a PSF throughout the period. The recovery starts with a WBS followed by a transition period to a possible PSF. No unambiguous transient evaluation can be made on the recovery period. The pressure in the section above the test section is affected by the drilling in KFM09B.

516.0–521.0 m

The injection period is dominated by a transition period towards a PRF. Transient evaluation from the models by Ozkan-Raghavan for a single fracture and Hurst-Clark-Brauer assuming 2D results in similar values of transmissivity. The recovery period starts with WBS that lasts about 30 s, followed by a transition to some other flow regime. The pressure above the test section is disturbed by the drilling in KFM09B.

521.0–526.0 m

The test section has a very low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, the injection time was shortened. As a result T_M, based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section. The period of measured recovery only showed a pressure increase, indicating that the section is of such low transmissivity that packer expansion affects the pressure throughout the period.

526.0–531.0 m

The test section has a very low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, the injection time was shortened. As a result T_M, based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section. The period of measured recovery only showed a pressure increase, indicating that the section is of such low transmissivity that packer expansion affects the pressure throughout the period.

531.0–536.0 m

The injection period is affected by a shift between regulation valves at c 200 s. A strong NFB is indicated for the whole injection period. No unambiguous transient evaluation can be made on the injection period. Hence the recovery period is regarded to give the best estimate of transmissivity. The recovery period indicates an apparent PRF starting at c100 s and continuing almost throughout the recovery period where an apparent NFB is indicated. The total recovery in this rather high-transmissive section is only c 4 m, indicating a flow feature of limited extension, i.e. decreasing fracture aperture away from the borehole.

536.0–541.0 m

The test section has a low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, in accordance with AP PF 400-05-104, the injection time was shortened. As a result, T_M based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section. The section above the test section is affected by the drilling in KFM09B.

541.0–546.0 m

This section has a low but detectable transmissivity. The injection period starts with a short PRF between 10 and 50 s and then it turns into an apparent NFB. The recovery period shows a PLF transitioning to an apparent PRF after c 200 s lasting throughout the recovery period. All the transient evaluations made (one on the injection period and two on the recovery period) result in simular transmissivities. The total recovery in the test section is only c 2 m, indicating a flow feature of limited extension, i.e. decreasing fracture aperture away from the borehole.

561.0–566.0 m

The test section has a very low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, in accordance with AP PF 400-05-104, the injection time was shortened. As a result, T_M based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section. The period of measured recovery only showed a pressure increase, indicating that the section is of such low transmissivity that packer expansion affects the pressure throughout the period. Since the noise level in the flow measurement had drifted a bit below zero, the Q/s-measl-L chosen for this test was set three A/D-levels higher to compensate for this drift. The section above the test section is affected by the drilling in KFM09B.

606.0–611.0 m

The test section has a very low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, in accordance with AP PF 400-05-104, the injection time was shortened. As a result, T_M based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section. The period of measured recovery only showed a pressure increase, indicating that the section is of such low transmissivity that packer expansion affects the pressure throughout the period.

611.0–616.0 m

Both the injection- and recovery period start with a PRF that turns into an apparent NFB after about 200 s and 100 s, respectively. The transient evaluations on both periods give consistent results. The pressure below the test section is still rising during the test period because of the natural formation pressure. The total recovery in the test section is only c 10 m, indicating a flow feature of limited extension, i.e. decreasing fracture aperture away from the borehole.

616.0–621.0 m

The test section has a very low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, in accordance with AP PF 400-05-104, the injection time was shortened. As a result, T_M based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section. The period of measured recovery only showed a pressure increase, indicating that the section is of such low transmissivity that packer expansion affects the pressure throughout the period.

621.0–626.0 m

The injection period in this section begins with a PLF followed by an approximate PRF that starts after about 40 s, lasting until about 400 s when a transition into an apparent NFB commences. The recovery also starts with a PLF for about 80 s, and then develops into a PRF between 60 s and 300 s and finally an apparent NFB is observed. The total recovery in the test section is only c 12 m, indicating a flow feature of limited extension, i.e. decreasing fracture aperture away from the borehole.

626.0–631.0 m

The test section has a low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, in accordance with AP PF 400-05-104, the injection time was shortened. As a result, T_M based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section.

631.0–636.0 m

The injection period starts with an approximate PRF after about 30 s continuing until about 100 s when the flow makes a transition to an apparent NFB. The recovery period begins with WBS that after c 50 s turns into an approximate PRF that continues for the rest of the recovery period.

636.0–641.0 m

The entire injection period is dominated by a PRF. The recovery starts with a WBS followed by a transition to a PRF that begins after about 150 s and continues for the rest of the period. The transient evaluation on the recovery period results in a large apparent skin factor and a T-value higher than the corresponding value from the injection period and from the stationary evaluation. Hence the evaluation on the recovery period is considered uncertain.

641.0–646.0 m

Since the flow rate was very low the data are rather scattered. The injection period indicates a PLF transitioning to a PSF. The recovery period demonstrates WBS transitioning towards a possible PRF. Since the data from the injection is scattered the recovery period is regarded as the most representative for the section.

646.0–651.0 m

The test section has a very low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, in accordance with AP PF 400-05-104, the injection time was shortened. As a result, T_M based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section. The period of measured recovery only showed a pressure increase, indicating that the section is of such low transmissivity that packer expansion affects the pressure throughout the period.

651.0–656.0 m

During the injection period a PRF is identified from c 40 s throughout the injection period. After an initial phase of WBS during the recovery period, a short PRF is observed between 100 and 400 s, then transitioning to some other flow regime, possibly an apparent NFB. The fitting with the Dougherty-Babu model on the recovery period however suggests a large skin factor and a value of transmissivity rather different from the one achieved with the Hurst-Clark-Brauer model on the injection period. This fact makes the evaluation on the recovery period uncertain and hence the transient evaluation of the injection period is regarded as representative for the section.

656.0–661.0 m

The test section has a low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, in accordance with AP PF 400-05-104, the injection time was shortened. As a result, T_M based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section.

661.0–666.0 m

The test section has a very low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, in accordance with AP PF 400-05-104, the injection time was shortened. As a result, T_M based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section. The period of measured recovery only showed a pressure increase, indicating that the section is of such low transmissivity that packer expansion affects the pressure throughout the period.

731.0–736.0 m

The test section has a low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, in accordance with AP PF 400-05-104, the injection time was shortened. As a result, T_M based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section.

736.0–741.0 m

The test section has a low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, in accordance with AP PF 400-05-104, the injection time was shortened. As a result, T_M based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section. The pressure above the test section is affected by the drilling in KFM09B that is performed right next to this hole.

741.0–746.0 m

The injection period in this section starts with a PRF between 40 and 300 s and after that the flow possibly turns into another PRF, with slightly lower transmissivity lasting from 300 s throughout the injection period. The recovery period starts with WBS followed by a transition period that turns into an apparent NFB by the end. The transient evaluation on the recovery period is considered uncertain and results in a high skin factor. The pressure above the test section is affected by the drilling in KFM09B that is performed right next to this borehole.

746.0–751.0 m

The test section has a low transmissivity. Since the flow rate was not detectable, neither steady-state nor transient evaluation of transmissivity was possible. Hence, in accordance with AP PF 400-05-104, the injection time was shortened. As a result, T_M based on Q/s-measl-L, was considered to be the most representative transmissivity value for this section. The pressure above the test section is interfered by the drilling in KFM09B that is performed right next to this hole.

751.0–756.0 m

The injection period starts with a PLF that turns into a short PRF after about 200 s. After c 700 s a transition towards a PSF is observed. The recovery period only indicates a PLF. The pressure above the test section is affected by the drilling in KFM09B that is performed right next to this hole. The pressure increases (c 1.5 kPa) in the section below. Since the transmissivity below is higher than in the test section this relatively small pressure may have caused an overestimation of the transmissivity in the section 751.0–756.0 m.

756.0–761.0 m

The injection period starts with a transition into a PRF after about 70 s lasting throughout the injection period. The recovery period starts with a WBS for about 100 s. After a transition period, an approximate PRF is indicated after c 400 s. The pressure above the test section is interfered by the drilling in KFM09B that is performed right next to this borehole.

761.0–766.0 m

The injection period starts with an approximate PRF transitioning to a PSF by the end. The rather low skin factor might indicate a possible PLF in the beginning of the period, masked by the pressure regulation to a constant pressure. This assumption is also supported by the recovery period with a dominating PLF ending with a transition phase. Evaluations using the Hurst-Clark-Brauer model on the injection and the Dougherty-Babu model and the Ozkan-Raghavan model on the recovery period all result in similar values of transmissivity. The pressure above the test section is interfered by the drilling in KFM09B that is performed right next to this hole. The pressure increases (c 2 kPa) in the section below. Since the transmissivity below is higher than in the test section, this relatively small pressure may have caused an overestimation of the transmissivity in the section 761.0–766.0 m.

766.0–771.0 m

The pressure and the flow were somewhat unstable during the injection period. Despite the unstable pressure it is assumed that the injection period is dominated by a PSF after about 200 s. The recovery period starts with a WBS that at the end turns into a transition state. The evaluation of the recovery period is considered somewhat uncertain since WBS dominates. Drilling is still conducted in KFM09B and affects the pressure above the test section.

771.0–776.0 m

The beginning of the injection period has an unstable flow due to low transmissivity. The injection period is dominated by a PSF after about 200 s and continues for the rest of the injection period. The recovery period begins with a WBS with a transition period to an approximate PRF. The pressure above the test section is affected by the drilling in KFM09B that is performed right next to this borehole.

776.0–781.0 m

The injection period starts with a transition into a PRF after about 100 s which continues for the rest of the injection period. The recovery period begins with a WBS transitioning to an approximate PRF. The evaluations from the two test periods give similar results. Drilling is still conducted in KFM09B and affects the pressure above the test section.

781.0–786.0 m

The injection period starts with a short transition into a PRF after c 30 s lasting until 300 s. Then the flow turns into a PSF for the rest of the injection. However, no unambiguous transient evaluation with the Hantush model, designed for spherical flow, can be made, but when assuming the same T-value as obtained from the Hurst-Clark-Brauer 2D-model the fitting is good. Also when comparing the skin factors from the two models it is noted that the models support each other. Recovery starts with a WBS followed by a transition period after about 100 s to some other flow regime. Drilling is still conducted in KFM09B and affects the pressure above the test section. The pressure increases (c 2 kPa) in the section below. Since the transmissivity below is higher than in the test section this relatively small pressure may have caused an overestimation of the transmissivity in the section 781.0–786.0 m.

786.0–791.0 m

Although the derivative is quite scattered it can be deduced that the injection period is dominated by a PSF starting after about 100 s, continuing throughout the period. The recovery begins with a WBS followed by a transition period. No unambiguous transient evaluation can be made on the recovery period but good agreement with the evaluation of the injection period is obtained if the same value on r/B is used. The pressure above the test section is interfered by the drilling in KFM09B that is performed right next to this borehole.

6.2.5 Flow regimes

As discussed in Section 5.4.4, several of the recovery periods were dominated by wellbore storage effects and no pseudo-radial flow period was reached. On the other hand, some time interval of pseudo-radial flow could in most cases be identified from the injection period. A summary of the frequency of identified flow regimes on different scales is presented in Table 6-3, which shows all identified flow regimes during the tests. For example, a pseudo-radial flow regime (PRF) transitioning to a pseudo-spherical flow regime (PSF) will contribute to one observation of PRF and one observation of PSF. The numbers within parenthesis denote the number of tests where the actual flow regime is the only one present.

It should be noted that the interpretation of flow regimes is only tentative and soley based on visual inspection of the data curves. It should also be observed that the number of tests with a pseudo-linear flow regime during the beginning of the injection period may be under-estimated due to the fact that a certain time is required for achieving a constant pressure, which fact may mask the initial flow regime.

Table 6-3. Interpreted flow regimes during the injection tests in KFM09A.

Borehole	Section length (m)	Number of tests	Number of tests with definable Q_p	Injection period PLF	PRF	PSF	PSS	NFB	Recovery period WBS	PLF	PRF	PSF	PSS	NFB
KFM09A	5	103	64	8(1)	40(24)	17(9)	1(1)	20(10)	37(16)	18(6)	23(3)	4(1)	1(0)	21(0)
KFM09A	20	36	30	9(4)	21(11)	5(2)	0(0)	6(2)	22(14)	5(0)	11(2)	0(0)	0(0)	8(0)
KFM09A	100	7	7	1(0)	2(1)	2(2)	0(0)	4(2)	4(0)	2(0)	3(0)	2(0)	0(0)	4(0)

Table 6-3 shows that a certain period of pseudo-radial flow could be identified from the injection period in c 62% of the tests with a definable final flow rate for KFM09A. This percentage is higher for the tests in 20 m sections compared to the tests in 100 m and 5 m. For the recovery period, the corresponding result is c 37%.

For c 32% of the tests in the borehole, more than one flow regime could be identified. The most common transitions in KFM09A during the injection period were from pseudo-radial flow to an apparent no-flow boundary. Also transitions from PRF to PSF and from an early PRF to another late PRF were quite common. During the recovery period in KFM09A the transition from wellbore storage to pseudo-radial flow was the most frequent transition followed by the transitions PRF->NFB and WBS->NFB.

6.3 Comparison of transmissivity values on different test scales

The transmissivity values considered the most representative, T_R, from the injection tests in KFM09A in the tested sections of 100 m, 20 m and 5 m length, respectively, are shown in Figure 6-2. This figure demonstrates a good agreement between results obtained from tests on different scales in KFM09A. A consistency check of the transmissivity values on the different scales was made by summation of calculated values from smaller scales (20 m and 5 m) and comparing with the estimated values in longer sections (100 m and 20 m).

In Table 6-4, estimated transmissivity values in 100 m and 20 m test sections in KFM09A according to steady-state (T_M) and most representative evaluation (T_R) are listed together with summed transmissivities in 20 m and 5 m sections over the corresponding 100 m and 20 m sections for KFM09A. When the transmissivity values are below the measurement limit (Q_p could not be defined), the most representative transmissivity value, T_R, was considered to be less than T_M, based on Q/s-measl-L, for the test section. The measurement limit values are included in the summed values in Table 6-4. This leads to overestimated values of the summed transmissivities.

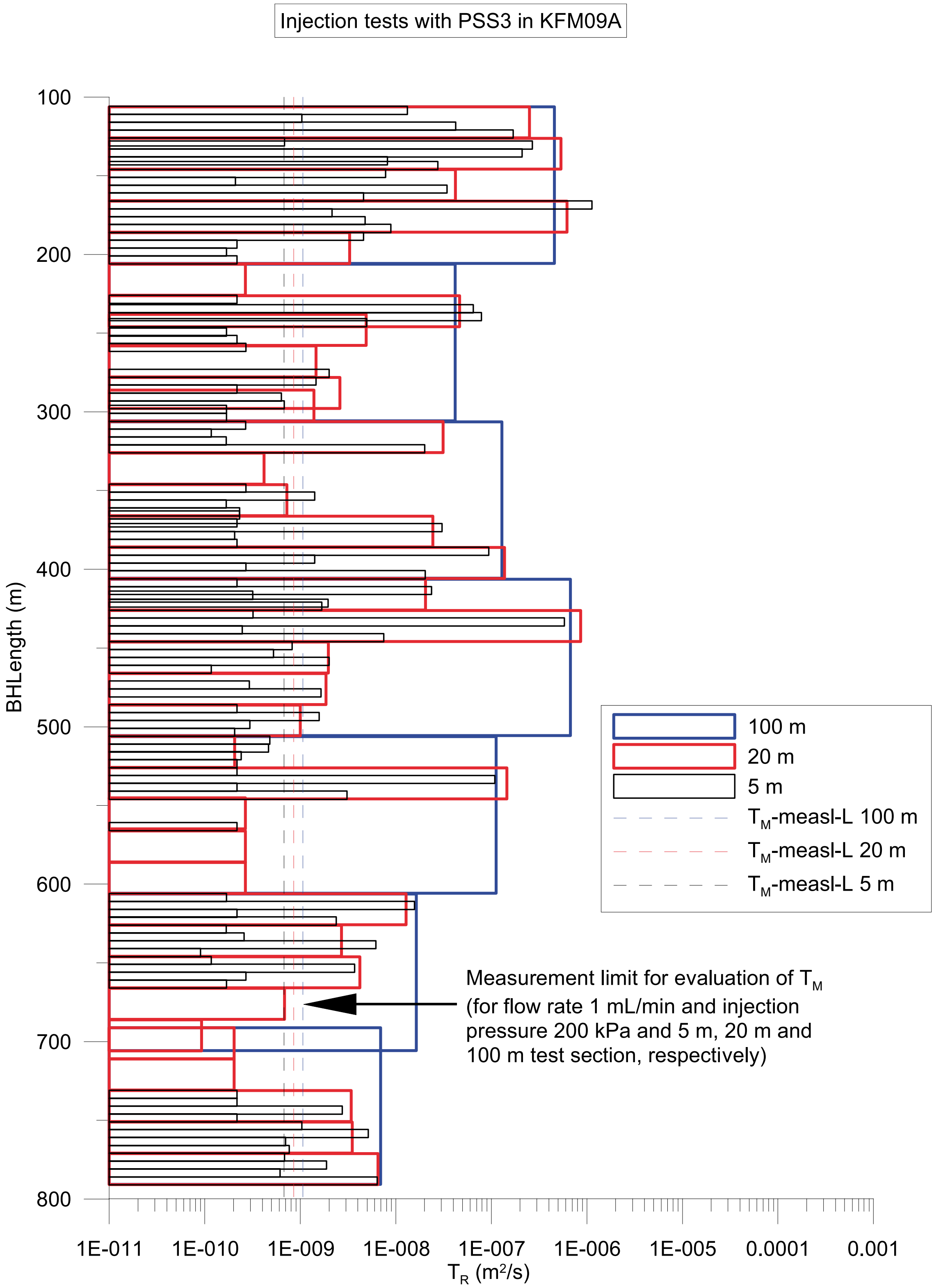

Figure 6-2. *Estimated best representative transmissivity values (T_R) for sections of 100 m, 20 m and 5 m length in borehole KFM09A. Estimated transmissivity values for the lower standard measurement limit from stationary evaluation (T_M-measl-L) for different test section lengths are also shown.*

Table 6-4. Estimated transmissivity values in 100 m and 20 m test sections together with summed up transmissivity values in 20 m and 5 m sections in the corresponding borehole intervals from the injection tests in KFM09A.

Bore-hole Idcode	Secup inj.test (m)	Seclow inj.test (m)	L_w (m)	T_M inj. tests (m^2/ s)	T_R inj. tests (m^2/s)	SUM T_M (20m) inj. tests (m^2/s)	SUM T_R (20m) inj. tests (m^2/s)	SUM T_M (5m) inj. tests (m^2/s)	SUM T_R (5m) inj. tests (m^2/s)
KFM09A	106.0	206.0	100.0	4.89E–06	4.56E–07	4.24E–06	1.45E–06	3.74E–06	1.94E–06
KFM09A	206.0	306.0	100.0	7.69E–08	4.19E–08	7.15E–08 [1)]	5.72E–08 [1)]	1.25E–07	1.55E–07
KFM09A	306.0	406.0	100.0	2.46E–07	1.29E–07	2.20E–07	1.95E–07	1.94E–07	1.70E–07
KFM09A	406.0	506.0	100.0	6.74E–07	6.74E–07	8.92E–07	8.86E–07	6.27E–07	6.27E–07
KFM09A	506.0	606.0	100.0	1.13E–07	1.13E–07	1.49E–07 [1)]	1.46E–07 [1)]	1.13E–07	1.14E–07
KFM09A	606.0	706.0	100.0	3.56E–08	1.64E–08	3.49E–08 [2)]	2.05E–08 [2)]	3.57E–08	2.93E–08
KFM09A	691.0	791.0	100.0	6.09E–08	6.92E–09	6.39E–08	1.39E–08	6.65E–08	2.06E–08
KFM09A	106.0	126.0	20.0	4.06E–07	2.51E–07			3.82E–07	2.26E–07
KFM09A	126.0	146.0	20.0	1.28E–06	5.35E–07			1.28E–06 [1)]	5.16E–07 [1)]
KFM09A	146.0	166.0	20.0	2.52E–07	4.22E–08			2.18E–07	4.70E–08
KFM09A	166.0	186.0	20.0	2.29E–06	6.19E–07			1.86E–06	1.15E–06
KFM09A	186.0	206.0	20.0	4.82E–09	3.28E–09			5.21E–09	5.19E–09
KFM09A	206.0	226.0	20.0	<2.66E–10	<2.66E–10			–	–
KFM09A	226.0	246.0	20.0	4.83E–08	4.65E–08			1.15E–07 [2)]	1.49E–07 [2)]
KFM09A	238.0	258.0	20.0	1.20E–08	4.90E–09			1.31E–08 [2)]	5.33E–09 [2)]
KFM09A	258.0	278.0	20.0	2.61E–09	1.46E–09			2.63E–09 [2), 3)]	2.27E–09 [2), 3)]
KFM09A	278.0	298.0	20.0	5.37E–09	2.59E–09			5.83E–09 [2)]	3.00E–09 [2)]
KFM09A	286.0	306.0	20.0	2.95E–09	1.39E–09			2.13E–09 [2)]	1.65E–09 [2)]
KFM09A	306.0	326.0	20.0	1.43E–08	3.12E–08			1.25E–08 [2)]	2.06E–08 [2)]
KFM09A	326.0	346.0	20.0	1.06E–09	4.17E–10			–	–
KFM09A	346.0	366.0	20.0	2.18E–09	7.25E–10			3.03E–09 [2)]	2.08E–09 [2)]
KFM09A	366.0	386.0	20.0	6.50E–08	2.44E–08			6.00E–08 [2)]	3.14E–08 [2)]
KFM09A	386.0	406.0	20.0	1.38E–07	1.38E–07			1.18E–07	1.16E–07
KFM09A	406.0	426.0	20.0	2.04E–08	2.04E–08			2.07E–08	2.79E–08
KFM09A	426.0	446.0	20.0	8.60E–07	8.60E–07			5.91E–07	5.91E–07
KFM09A	446.0	466.0	20.0	3.16E–09	1.97E–09			4.78E–09 [3)]	3.46E–09 [3)]
KFM09A	466.0	486.0	20.0	2.37E–09	1.86E–09			3.87E–09 [3)]	1.94E–09 [3)]
KFM09A	486.0	506.0	20.0	5.86E–09	1.00E–09			6.03E–09	2.30E–09
KFM09A	506.0	526.0	20.0	2.33E–09	2.06E–10			3.12E–09	1.40E–09
KFM09A	526.0	546.0	20.0	1.45E–07	1.45E–07			1.09E–07 [3)]	1.12E–07 [3)]
KFM09A	545.0	565.0	20.0	<2.66E–10	<2.66E–10			2.18E–10 [2), 3)]	2.18E–10 [2), 3)]
KFM09A	566.0	586.0	20.0	<2.66E–10	<2.66E–10			–	–
KFM09A	586.0	606.0	20.0	<2.66E–10	<2.66E–10			–	–
KFM09A	606.0	626.0	20.0	2.43E–08	1.28E–08			2.29E–08	1.84E–08
KFM09A	626.0	646.0	20.0	4.21E–09	2.70E–09			7.04E–09	6.71E–09
KFM09A	646.0	666.0	20.0	5.22E–09	4.21E–09			5.78E–09	4.26E–09
KFM09A	666.0	686.0	20.0	6.82E–10	6.82E–10			–	–
KFM09A	686.0	706.0	20.0	5.10E–10	9.24E–11			–	–
KFM09A	691.0	711.0	20.0	<2.02E–10	<2.02E–10			–	–
KFM09A	711.0	731.0	20.0	<2.02E–10	<2.02E–10			–	–
KFM09A	731.0	751.0	20.0	3.01E–09	3.41E–09			4.28E–09	3.40E–09
KFM09A	751.0	771.0	20.0	1.82E–08	3.50E–09			1.85E–08	7.65E–09
KFM09A	771.0	791.0	20.0	4.23E–08	6.54E–09			4.37E–08	9.54E–09

[1)] Partly overlapping sections.

[2)] Partly overlapping sections and measured intervals not identical.

[3)] Interval only partly measured.

n.m. = not measured.

In Figure 6-3, transmissivity values considered as the most representative for 100 m and 20 m sections (T_R–100 m and T_R–20 m, respectively) in KFM09A are plotted versus the sum of the transmissivity values considered most representative in 5 m sections in the corresponding intervals (SUM T_R–5 m). The lower measurement limit of T_M for the different section lengths (Q_p=1mL/min and an assumed pressure difference of 200 kPa) together with the cumulative measurement limit for the sum of 5 m sections are also shown in the figure.

Figure 6-3 indicates a relatively good agreement between estimated transmissivity values in longer sections and summed transmissivity values in corresponding 5 m sections for the injection tests. However, a majority of the data points are located below the straight line, indicating that the sum of the transmissivity from the shorter sections is generally higher than the estimated transmissivity in longer sections. Some of the sections are partly overlapping, resulting in an overestimation when summing the sections together. Also interference between adjacent sections can contribute to an overestimation of the sum of transmissivity when summing the transmissivity from several sections together. Since the measurement limit values are summed up, the sum of T in shorter sections can become higher than the estimated transmissivity value in the longer section, for very low conductive sections. There might also be other reasons for discrepancies.

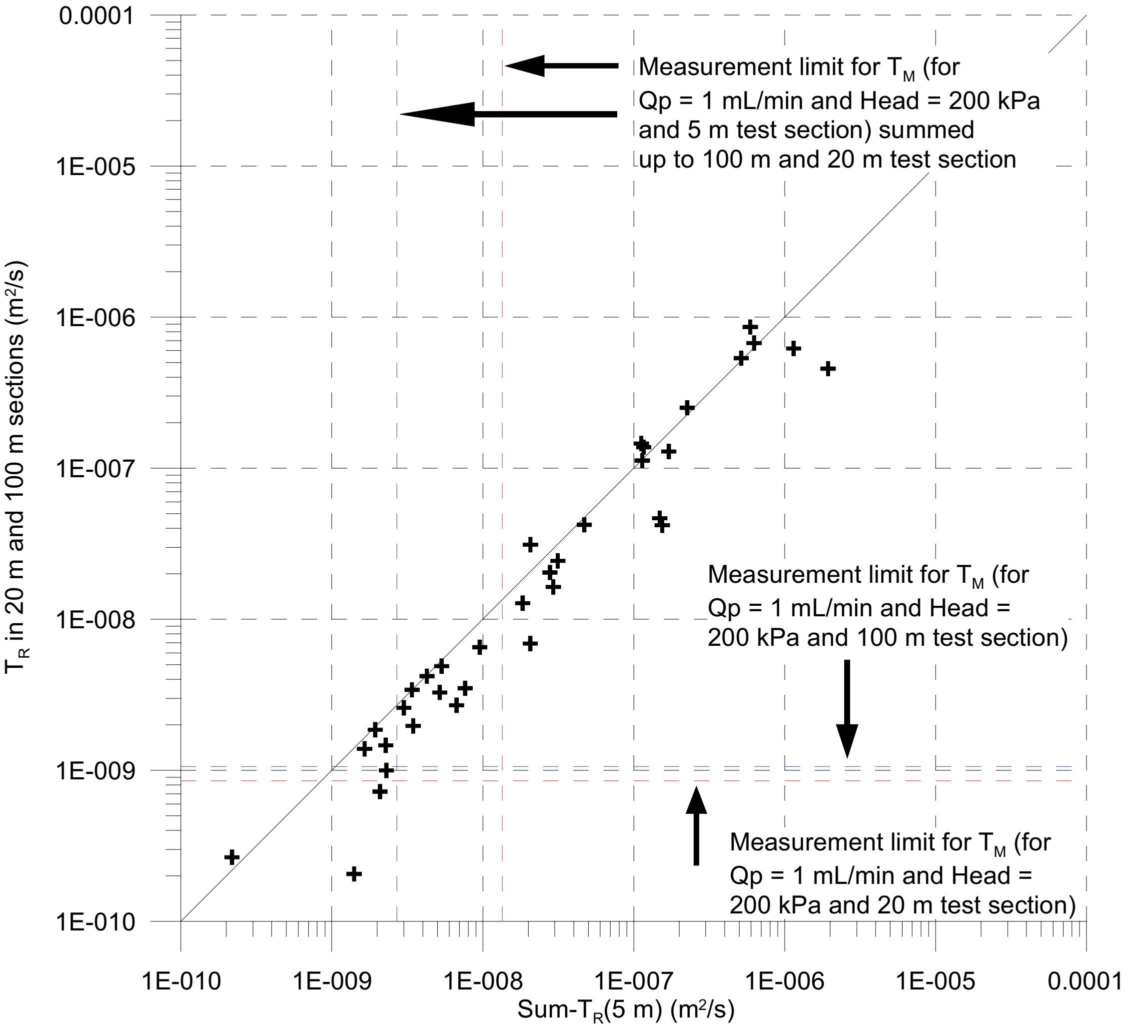

Figure 6-3. *Transmissivity values considered most representative (T_R) for 100 m and 20 m sections versus the sum of most representative transmissivity values (T_R) in 5 m sections in the corresponding borehole intervals from the injection tests in KFM09A together with the standard lower measurement limit at different scales.*

Interference is specially noticed between the 5 m sections 751.0–756.0 m and 756.0–761.0 m and between 761.0–766.0 and 766.0–771.0 m all within the same 20 m section 751.0–771.0 m. Another section where interference is noticed is between sections 226.0–232.0 m and 232.0–237.0 m.

In Table 6-5 a comparison of the sum of estimated transmissivity values from injection tests with different section lengths in KFM09A is presented. It should be observed that the summed transmissivity values only include the tests actually performed for each section length. However, the most conductive sections are measured. It is also important to point out that this is a very rough way of comparing the tests in different test scales since no consideration to overlapping sections are made. The tendency that the sum of transmissivity of shorter sections is bigger than the transmissivity in corresponding longer sections can however be seen on T_R in Table 6-5.

The total transmissivity of KFM09A is dominated by the intervals between 166.0–171.0 m and 431.0–436.0 m.

Table 6-5. Comparison of calculated transmissivity values from tests with different section lengths in borehole KFM09A.

Sum of T (m^2/s)	Borehole interval (m) 106.00–791.00 [1)]
$\sum T_M$(100 m)	6.09E–06
$\sum T_R$(100 m)	1.44E–06
$\sum T_M$(20 m)	5.67E–06
$\sum T_R$(20 m)	2.77E–06
$\sum T_M$(5 m)	4.90E–06
$\sum T_R$(5 m)	3.05E–06

[1)] Tests measured with all section lengths contain partly overlapping sections.

6.4 Basic statistics of hydraulic conductivity distributions in different scales

Some basic statistical parameters were calculated for the steady-state hydraulic conductivity (K_M) distributions in different scales (100 m, 20 m and 5 m) from the injection tests in borehole KFM09A. The hydraulic conductivity is obtained by dividing the transmissivity by the section length, in this case T_M/L_w. Results from tests where Q_p was below the estimated test-specific measurement limit were not included in the statistical analyses of K_M. The same basic statistical parameters were derived for the hydraulic conductivity considered most representative (K_R=T_R/L_w), including all tests. In the statistical analysis, the logarithm (base 10) of K_M and K_R was used. Selected results are shown in Table 6-6. It should be noted that the statistics for the different section lengths is based on different borehole intervals.

Table 6-6. Basic statistical parameters for steady-state hydraulic conductivity (K_M) and hydraulic conductivity considered most representative (K_R) in borehole KFM09A. L_w=section length, m=arithmetic mean, s=standard deviation.

Parameter	Unit	KFM09A L_w=100 m	KFM09A L_w=20 m	KFM09A L_w=5 m
Measured borehole interval	m	106.0–791.0 [2]	106.0–791.0 [3),4]	106.0–791.0 [5), 6), 7]
Number of tests	–	7	36	104
N:o of tests below E.L.M.L.[1]	–	0	6	39
m ($Log_{10}(K_M)$)	Log10(m/s)	–8.69	–9.10	–8.85
s ($Log_{10}(K_M)$)	–	0.74	0.99	0.86
m ($Log_{10}(K_R)$)	Log10(m/s)	–9.10	–9.66	–9.59
s ($Log_{10}(K_R)$)	–	0.73	1.12	0.96

1) Number of tests where Q_p could not be defined (E.L.M.L. = estimated test-specific lower measurement limit).

2) Sections 606.0–706.0 m and 691.0–791.0 m partly overlapping.

3) Intervals 226.0–258.0 m, 278.0–306.0 m, 526.0–565.0 m and 686.0–711.0 m contain partly overlapping 20 m sections.

4) The section 565.0–566.0 m was not measured with 20 m-section.

5) The interval 206.0–226.0 m, 261.5–273.0 m, 326.0–346.0 m, 466.0–471.0 m, 481.0–486.0 m, 546.0–561.0 m, 566.0–606.0 m and 666.0–731.0 m were not measured with the 5 m section.

6) The following sections are partly overlapping: 126.0–131.0 and 128.0–133.0 m, 138.0–143.0 and 141.0–146.0 m, 237.0–242.0 and 240.8–245.8 m, 246.8–251.8 and 251.5–256.5 m, 293.0–298.0 and 296.0–301.0 m, 361.0–366.0 and 363.0–368.0 m, 368.0–373.0 and 371.0–376.0 m, 411.0–416.0 and 414.0–419.0 m, 419.0–424.0 and 421.0–426.0 m.

7) Sections between 231.0–232.0 m and 245.8–246.8 m were not measured due to packer positioning difficulties, no visible fractures are seen within the intervals.

7 References

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APPENDIX 1. File description table

Bh id	Test section		Test type	Test no	Test start Date, time	Test stop Date, time	Data files of raw and primary data	Parameters in file	Comments
idcode	(m)	(m)	(1-6)[1)]		YYYYMMDD hh:mm	YYYYMMDD hh:mm	__Borehole id_secup_date and time of test start		
KFM09A	106.00	206.00	3	1	2005-11-17 16:09	2005-11-17 17:59	__KFM09A_0106.00_200511171609.ht2	P, Q, Te	
KFM09A	206.00	306.00	3	1	2005-11-17 19:03	2005-11-17 20:53	__KFM09A_0206.00_200511171903.ht2	P, Q, Te	
KFM09A	306.00	406.00	3	1	2005-11-17 21:47	2005-11-17 23:36	__KFM09A_0306.00_200511172147.ht2	P, Q, Te	
KFM09A	406.00	506.00	3	1	2005-11-18 09:59	2005-11-18 11:49	__KFM09A_0406.00_200511180959.ht2	P, Q, Te	
KFM09A	506.00	606.00	3	1	2005-11-18 13:32	2005-11-18 14:28	__KFM09A_0506.00_200511181332.ht2	P, Q, Te	Interrupted [2)]
KFM09A	506.00	606.00	3	2	2005-11-21 12:52	2005-11-21 15:13	__KFM09A_0506.00_200511211252.ht2	P, Q, Te	
KFM09A	606.00	706.00	3	1	2005-11-21 06:14	2005-11-21 08:03	__KFM09A_0606.00_200511210614.ht2	P, Q, Te	
KFM09A	691.00	791.00	3	1	2005-11-21 08:51	2005-11-21 10:40	__KFM09A_0691.00_200511210851.ht2	P, Q, Te	
KFM09A	106.00	126.00	3	1	2005-11-28 16:44	2005-11-28 18:19	__KFM09A_0106.00_200511281644.ht2	P, Q, Te	
KFM09A	126.00	146.00	3	1	2005-11-29 06:29	2005-11-29 07:43	__KFM09A_0126.00_200511290629.ht2	P, Q, Te	
KFM09A	146.00	166.00	3	1	2005-11-29 08:20	2005-11-29 09:35	__KFM09A_0146.00_200511290820.ht2	P, Q, Te	
KFM09A	166.00	186.00	3	1	2005-11-29 10:00	2005-11-29 11:15	__KFM09A_0166.00_200511291000.ht2	P, Q, Te	
KFM09A	186.00	206.00	3	1	2005-11-29 12:14	2005-11-29 13:31	__KFM09A_0186.00_200511291214.ht2	P, Q, Te	
KFM09A	206.00	226.00	3	1	2005-11-29 14:01	2005-11-29 14:47	__KFM09A_0206.00_200511291401.ht2	P, Q, Te	
KFM09A	226.00	246.00	3	1	2005-11-29 15:38	2005-11-29 16:56	__KFM09A_0226.00_200511291538.ht2	P, Q, Te	
KFM09A	238.00	258.00	3	1	2005-11-29 17:18	2005-11-29 18:37	__KFM09A_0238.00_200511291718.ht2	P, Q, Te	
KFM09A	258.00	278.00	3	1	2005-11-29 18:58	2005-11-29 20:17	__KFM09A_0258.00_200511291858.ht2	P, Q, Te	
KFM09A	278.00	298.00	3	1	2005-11-29 21:03	2005-11-29 22:25	__KFM09A_0278.00_200511292103.ht2	P, Q, Te	
KFM09A	286.00	306.00	3	1	2005-11-29 22:41	2005-11-29 23:57	__KFM09A_0286.00_200511292241.ht2	P, Q, Te	
KFM09A	306.00	326.00	3	1	2005-11-30 06:29	2005-11-30 07:48	__KFM09A_0306.00_200511300629.ht2	P, Q, Te	
KFM09A	326.00	346.00	3	1	2005-11-30 08:16	2005-11-30 09:35	__KFM09A_0326.00_200511300816.ht2	P, Q, Te	
KFM09A	346.00	366.00	3	1	2005-11-30 10:06	2005-11-30 11:22	__KFM09A_0346.00_200511301006.ht2	P, Q, Te	
KFM09A	366.00	386.00	3	1	2005-11-30 12:06	2005-11-30 13:23	_KFM09A_0366.00_200511301206.ht2	P, Q, Te	
KFM09A	386.00	406.00	3	1	2005-11-30 13:50	2005-11-30 15:08	__KFM09A_0386.00_200511301350.ht2	P, Q, Te	
KFM09A	406.00	426.00	3	1	2005-11-30 15:30	2005-11-30 16:47	__KFM09A_0406.00_200511301530.ht2	P, Q, Te	
KFM09A	426.00	446.00	3	1	2005-11-30 18:03	2005-11-30 17:43	__KFM09A_0426.00_200511301710.ht2	P, Q, Te	Interrupted [2)]
KFM09A	426.00	446.00	3	2	2005-11-30 18:18	2005-11-30 19:38	__KFM09A_0426.00_200511301818.ht2	P, Q, Te	
KFM09A	446.00	466.00	3	1	2005-11-30 20:03	2005-11-30 21:45	__KFM09A_0446.00_200511302003.ht2	P, Q, Te	
KFM09A	466.00	486.00	3	1	2005-11-30 22:03	2005-11-30 23:20	__KFM09A_0466.00_200511302203.ht2	P, Q, Te	
KFM09A	486.00	506.00	3	1	2005-12-01 08:06	2005-12-01 09:34	__KFM09A_0486.00_200512010806.ht2	P, Q, Te	
KFM09A	506.00	526.00	3	1	2005-12-01 10:01	2005-12-01 11:22	__KFM09A_0506.00_200512011001.ht2	P, Q, Te	
KFM09A	526.00	546.00	3	1	2005-12-01 11:41	2005-12-01 13:46	__KFM09A_0526.00_200512011141.ht2	P, Q, Te	
KFM09A	545.00	565.00	3	1	2005-12-01 14:21	2005-12-01 15:09	__KFM09A_0545.00_200512011421.ht2	P, Q, Te	
KFM09A	566.00	586.00	3	1	2005-12-01 15:34	2005-12-01 16:17	__KFM09A_0566.00_200512011534.ht2	P, Q, Te	
KFM09A	586.00	606.00	3	1	2005-12-02 07:55	2005-12-02 08:37	__KFM09A_0586.00_200512020755.ht2	P, Q, Te	

Bh id	Test section		Test type	Test no	Test start Date, time	Test stop Date, time	Data files of raw and primary data	Parameters in file	Comments
idcode	(m)	(m)	(1-6)[1)]		YYYYMMDD hh:mm	YYYYMMDD hh:mm	__Borehole id_secup_date and time of test start		
KFM09A	606.00	626.00	3	1	2005-12-02 08:58	2005-12-02 10:22	__KFM09A_0606.00_200512020858.ht2	P, Q, Te	
KFM09A	626.00	646.00	3	1	2005-12-02 10:43	2005-12-02 12:05	__KFM09A_0626.00_200512021043.ht2	P, Q, Te	
KFM09A	646.00	666.00	3	1	2005-12-02 13:12	2005-12-02 14:35	__KFM09A_0646.00_200512021312.ht2	P, Q, Te	
KFM09A	666.00	686.00	3	1	2005-12-02 14:57	2005-12-02 16:13	__KFM09A_0666.00_200512021457.ht2	P, Q, Te	
KFM09A	686.00	706.00	3	1	2005-12-05 08:22	2005-12-05 09:53	__KFM09A_0686.00_200512050822.ht2	P, Q, Te	
KFM09A	691.00	711.00	3	1	2005-12-05 10:10	2005-12-05 11:12	__KFM09A_0691.00_200512051010.ht2	P, Q, Te	
KFM09A	711.00	731.00	3	1	2005-12-05 12:46	2005-12-05 13:30	__KFM09A_0711.00_200512051246.ht2	P, Q, Te	
KFM09A	731.00	751.00	3	1	2005-12-05 13:49	2005-12-05 15:12	__KFM09A_0731.00_200512051349.ht2	P, Q, Te	
KFM09A	751.00	771.00	3	1	2005-12-05 15:30	2005-12-05 16:54	__KFM09A_0751.00_200512051530.ht2	P, Q, Te	
KFM09A	771.00	791.00	3	1	2005-12-05 18:09	2005-12-05 19:26	__KFM09A_0771.00_200512051809.ht2	P, Q, Te	
KFM09A	106.00	111.00	3	1	2005-12-07 07:32	2005-12-07 08:52	__KFM09A_0106.00_200512070732.ht2	P, Q, Te	
KFM09A	111.00	116.00	3	1	2005-12-07 09:08	2005-12-07 10:24	__KFM09A_0111.00_200512070908.ht2	P, Q, Te	
KFM09A	116.00	121.00	3	1	2005-12-07 10:38	2005-12-07 12:39	__KFM09A_0116.00_200512071038.ht2	P, Q, Te	Interrupted [2)]
KFM09A	116.00	121.00	3	2	2005-12-21 15:48	2005-12-08 17:51	__KFM09A_0116.00_200512211548.ht2	P, Q, Te	
KFM09A	121.00	126.00	3	1	2005-12-07 12:52	2005-12-07 14:09	__KFM09A_0121.00_200512071252.ht2	P, Q, Te	
KFM09A	126.00	131.00	3	1	2005-12-07 14:26	2005-12-07 16:04	__KFM09A_0126.00_200512071426.ht2	P, Q, Te	
KFM09A	128.00	133.00	3	1	2005-12-07 16:21	2005-12-07 17:40	__KFM09A_0128.00_200512071621.ht2	P, Q, Te	
KFM09A	133.00	138.00	3	1	2005-12-07 17:58	2005-12-07 19:16	__KFM09A_0133.00_200512071758.ht2	P, Q, Te	
KFM09A	138.00	143.00	3	1	2005-12-07 19:42	2005-12-07 21:13	__KFM09A_0138.00_200512071942.ht2	P, Q, Te	
KFM09A	141.00	146.00	3	1	2005-12-07 21:27	2005-12-07 22:45	__KFM09A_0141.00_200512072127.ht2	P, Q, Te	
KFM09A	146.00	151.00	3	1	2005-12-07 23:02	2005-12-08 00:17	__KFM09A_0146.00_200512072302.ht2	P, Q, Te	
KFM09A	151.00	156.00	3	1	2005-12-08 06:16	2005-12-08 06:59	__KFM09A_0151.00_200512080616.ht2	P, Q, Te	
KFM09A	156.00	161.00	3	1	2005-12-08 07:10	2005-12-08 08:26	__KFM09A_0156.00_200512080710.ht2	P, Q, Te	
KFM09A	161.00	166.00	3	1	2005-12-08 08:36	2005-12-08 09:52	__KFM09A_0161.00_200512080836.ht2	P, Q, Te	
KFM09A	166.00	171.00	3	1	2005-12-08 10:03	2005-12-08 11:19	__KFM09A_0166.00_200512081003.ht2	P, Q, Te	
KFM09A	171.00	176.00	3	1	2005-12-08 12:12	2005-12-08 13:29	__KFM09A_0171.00_200512081212.ht2	P, Q, Te	
KFM09A	176.00	181.00	3	1	2005-12-08 13:43	2005-12-08 14:57	__KFM09A_0176.00_200512081343.ht2	P, Q, Te	
KFM09A	181.00	186.00	3	1	2005-12-08 15:13	2005-12-08 16:28	__KFM09A_0181.00_200512081513.ht2	P, Q, Te	
KFM09A	186.00	191.00	3	1	2005-12-08 16:36	2005-12-08 17:51	__KFM09A_0186.00_200512081636.ht2	P, Q, Te	
KFM09A	191.00	196.00	3	1	2005-12-08 18:03	2005-12-08 18:50	__KFM09A_0191.00_200512081803.ht2	P, Q, Te	
KFM09A	196.00	201.00	3	1	2005-12-08 19:02	2005-12-08 19:47	__KFM09A_0196.00_200512081902.ht2	P, Q, Te	
KFM09A	201.00	206.00	3	1	2005-12-08 19:57	2005-12-08 20:39	__KFM09A_0201.00_200512081957.ht2	P, Q, Te	
KFM09A	226.00	231.00	3	1	2005-12-08 20:58	2005-12-08 21:40	__KFM09A_0226.00_200512082058.ht2	P, Q, Te	
KFM09A	232.00	237.00	3	1	2005-12-08 21:54	2005-12-08 23:08	__KFM09A_0232.00_200512082154.ht2	P, Q, Te	
KFM09A	237.00	242.00	3	1	2005-12-08 23:21	2005-12-09 00:35	__KFM09A_0237.00_200512082321.ht2	P, Q, Te	
KFM09A	240.80	245.80	3	1	2005-12-09 08:08	2005-12-09 09:24	__KFM09A_0240.80_200512090808.ht2	P, Q, Te	
KFM09A	246.80	251.80	3	1	2005-12-21 13:55	2005-12-21 14:35	__KFM09A_0246.80_200512211355.ht2	P, Q, Te	

Bh id	Test section		Test type	Test no	Test start Date, time	Test stop Date, time	Data files of raw and primary data	Parameters in file	Comments
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KFM09A	251.50	256.50	3	1	2005-12-09 09:40	2005-12-09 10:22	__KFM09A_0251.50_200512090940.ht2	P, Q, Te	
KFM09A	256.50	261.50	3	1	2005-12-09 10:34	2005-12-09 11:18	__KFM09A_0256.50_200512091034.ht2	P, Q, Te	
KFM09A	273.00	278.00	3	1	2005-12-09 11:30	2005-12-09 13:22	__KFM09A_0273.00_200512091130.ht2	P, Q, Te	
KFM09A	278.00	283.00	3	1	2005-12-09 13:34	2005-12-09 14:48	__KFM09A_0278.00_200512091334.ht2	P, Q, Te	
KFM09A	283.00	288.00	3	1	2005-12-09 15:04	2005-12-09 15:51	__KFM09A_0283.00_200512091504.ht2	P, Q, Te	
KFM09A	288.00	293.00	3	1	2005-12-09 16:00	2005-12-09 17:15	__KFM09A_0288.00_200512091600.ht2	P, Q, Te	
KFM09A	293.00	298.00	3	1	2005-12-12 08:21	2005-12-12 09:42	__KFM09A_0293.00_200512120821.ht2	P, Q, Te	
KFM09A	296.00	301.00	3	1	2005-12-21 12:39	2005-12-21 13:28	__KFM09A_0296.00_200512211239.ht2	P, Q, Te	
KFM09A	301.00	306.00	3	1	2005-12-21 11:45	2005-12-21 12:29	__KFM09A_0301.00_200512211145.ht2	P, Q, Te	
KFM09A	306.00	311.00	3	1	2005-12-12 09:58	2005-12-12 10:39	__KFM09A_0306.00_200512120958.ht2	P, Q, Te	
KFM09A	311.00	316.00	3	1	2005-12-12 10:49	2005-12-12 12:33	__KFM09A_0311.00_200512121049.ht2	P, Q, Te	
KFM09A	316.00	321.00	3	1	2005-12-12 12:43	2005-12-12 13:31	__KFM09A_0316.00_200512121243.ht2	P, Q, Te	
KFM09A	321.00	326.00	3	1	2005-12-12 13:44	2005-12-12 15:02	__KFM09A_0321.00_200512121344.ht2	P, Q, Te	
KFM09A	346.00	351.00	3	1	2005-12-12 15:31	2005-12-12 16:14	__KFM09A_0346.00_200512121531.ht2	P, Q, Te	
KFM09A	351.00	356.00	3	1	2005-12-21 10:04	2005-12-21 11:19	__KFM09A_0351.00_200512211004.ht2	P, Q, Te	
KFM09A	356.00	361.00	3	1	2005-12-21 08:54	2005-12-21 09:50	__KFM09A_0356.00_200512210854.ht2	P, Q, Te	
KFM09A	361.00	366.00	3	1	2005-12-21 07:28	2005-12-21 08:43	__KFM09A_0361.00_200512210728.ht2	P, Q, Te	
KFM09A	363.00	368.00	3	1	2005-12-12 16:39	2005-12-12 17:54	__KFM09A_0363.00_200512121639.ht2	P, Q, Te	
KFM09A	368.00	373.00	3	1	2005-12-13 06:27	2005-12-13 07:24	__KFM09A_0368.00_200512130627.ht2	P, Q, Te	
KFM09A	371.00	376.00	3	1	2005-12-13 07:35	2005-12-13 08:48	__KFM09A_0371.00_200512130735.ht2	P, Q, Te	
KFM09A	376.00	381.00	3	1	2005-12-13 09:02	2005-12-13 09:58	__KFM09A_0376.00_200512130902.ht2	P, Q, Te	
KFM09A	381.00	386.00	3	1	2005-12-13 10:10	2005-12-13 11:25	__KFM09A_0381.00_200512131010.ht2	P, Q, Te	
KFM09A	386.00	391.00	3	1	2005-12-13 11:57	2005-12-13 13:16	__KFM09A_0386.00_200512131157.ht2	P, Q, Te	
KFM09A	391.00	396.00	3	1	2005-12-13 13:28	2005-12-13 14:48	__KFM09A_0391.00_200512131328.ht2	P, Q, Te	
KFM09A	396.00	401.00	3	1	2005-12-13 15:06	2005-12-13 15:49	__KFM09A_0396.00_200512131506.ht2	P, Q, Te	
KFM09A	401.00	406.00	3	1	2005-12-13 16:00	2005-12-13 17:15	__KFM09A_0401.00_200512131600.ht2	P, Q, Te	
KFM09A	406.00	411.00	3	1	2005-12-13 17:25	2005-12-13 18:18	__KFM09A_0406.00_200512131725.ht2	P, Q, Te	
KFM09A	411.00	416.00	3	1	2005-12-13 18:36	2005-12-13 19:50	__KFM09A_0411.00_200512131836.ht2	P, Q, Te	
KFM09A	414.00	419.00	3	1	2005-12-13 20:06	2005-12-13 21:22	__KFM09A_0414.00_200512132006.ht2	P, Q, Te	
KFM09A	419.00	424.00	3	1	2005-12-13 21:32	2005-12-13 22:46	__KFM09A_0419.00_200512132132.ht2	P, Q, Te	
KFM09A	421.00	426.00	3	1	2005-12-13 22:55	2005-12-14 00:09	__KFM09A_0421.00_200512132255.ht2	P, Q, Te	
KFM09A	426.00	431.00	3	1	2005-12-14 06:51	2005-12-14 07:59	__KFM09A_0426.00_200512140651.ht2	P, Q, Te	
KFM09A	431.00	436.00	3	1	2005-12-14 08:11	2005-12-14 09:31	__KFM09A_0431.00_200512140811.ht2	P, Q, Te	
KFM09A	436.00	441.00	3	1	2005-12-14 09:47	2005-12-14 10:29	__KFM09A_0436.00_200512140947.ht2	P, Q, Te	
KFM09A	441.00	446.00	3	1	2005-12-14 10:44	2005-12-14 12:00	__KFM09A_0441.00_200512141044.ht2	P, Q, Te	
KFM09A	446.00	451.00	3	1	2005-12-14 12:13	2005-12-14 14:04	__KFM09A_0446.00_200512141213.ht2	P, Q, Te	
KFM09A	451.00	456.00	3	1	2005-12-14 14:22	2005-12-14 15:38	__KFM09A_0451.00_200512141422.ht2	P, Q, Te	
KFM09A	456.00	461.00	3	1	2005-12-14 15:55	2005-12-14 17:12	__KFM09A_0456.00_200512141555.ht2	P, Q, Te	

Bh id	Test section		Test type	Test no	Test start Date, time	Test stop Date, time	Data files of raw and primary data	Parameters in file	Comments
idcode	(m)	(m)	(1-6)1)		YYYYMMDD hh:mm	YYYYMMDD hh:mm	__Borehole id_secup_date and time of test start		
KFM09A	461.00	466.00	3	1	2005-12-14 17:32	2005-12-14 18:15	__KFM09A_0461.00_200512141732.ht2	P, Q, Te	
KFM09A	471.00	476.00	3	1	2005-12-14 18:35	2005-12-14 19:50	__KFM09A_0471.00_200512141835.ht2	P, Q, Te	
KFM09A	476.00	481.00	3	1	2005-12-14 20:01	2005-12-14 21:23	__KFM09A_0476.00_200512142001.ht2	P, Q, Te	
KFM09A	486.00	491.00	3	1	2005-12-14 21:40	2005-12-14 22:31	__KFM09A_0486.00_200512142140.ht2	P, Q, Te	
KFM09A	491.00	496.00	3	1	2005-12-14 22:58	2005-12-15 00:12	__KFM09A_0491.00_200512142258.ht2	P, Q, Te	
KFM09A	496.00	501.00	3	1	2005-12-15 06:33	2005-12-15 07:57	__KFM09A_0496.00_200512150633.ht2	P, Q, Te	
KFM09A	501.00	506.00	3	1	2005-12-15 08:14	2005-12-15 09:00	__KFM09A_0501.00_200512150814.ht2	P, Q, Te	
KFM09A	506.00	511.00	3	1	2005-12-20 19:00	2005-12-20 20:23	__KFM09A_0506.00_200512201900.ht2	P, Q, Te	
KFM09A	511.00	516.00	3	1	2005-12-20 20:50	2005-12-20 22:05	__KFM09A_0511.00_200512202050.ht2	P, Q, Te	
KFM09A	516.00	521.00	3	1	2005-12-20 22:14	2005-12-20 23:28	__KFM09A_0516.00_200512202214.ht2	P, Q, Te	
KFM09A	521.00	526.00	3	1	2005-12-15 09:25	2005-12-15 10:11	__KFM09A_0521.00_200512150925.ht2	P, Q, Te	
KFM09A	526.00	531.00	3	1	2005-12-15 10:26	2005-12-15 11:07	__KFM09A_0526.00_200512151026.ht2	P, Q, Te	
KFM09A	531.00	536.00	3	1	2005-12-15 11:23	2005-12-15 12:44	__KFM09A_0531.00_200512151123.ht2	P, Q, Te	
KFM09A	536.00	541.00	3	1	2005-12-15 13:19	2005-12-15 14:03	__KFM09A_0536.00_200512151319.ht2	P, Q, Te	
KFM09A	541.00	546.00	3	1	2005-12-15 14:14	2005-12-15 15:28	__KFM09A_0541.00_200512151414.ht2	P, Q, Te	
KFM09A	561.00	566.00	3	1	2005-12-20 17:14	2005-12-20 17:58	__KFM09A_0561.00_200512201714.ht2	P, Q, Te	
KFM09A	606.00	611.00	3	1	2005-12-15 16:19	2005-12-15 17:00	__KFM09A_0606.00_200512151619.ht2	P, Q, Te	
KFM09A	611.00	616.00	3	1	2005-12-15 17:19	2005-12-15 18:35	__KFM09A_0611.00_200512151719.ht2	P, Q, Te	
KFM09A	616.00	621.00	3	1	2005-12-15 18:50	2005-12-15 19:31	__KFM09A_0616.00_200512151850.ht2	P, Q, Te	
KFM09A	621.00	626.00	3	1	2005-12-15 19:44	2005-12-15 21:03	__KFM09A_0621.00_200512151944.ht2	P, Q, Te	
KFM09A	626.00	631.00	3	1	2005-12-15 21:14	2005-12-15 22:01	__KFM09A_0626.00_200512152114.ht2	P, Q, Te	
KFM09A	631.00	636.00	3	1	2005-12-15 22:08	2005-12-15 23:33	__KFM09A_0631.00_200512152208.ht2	P, Q, Te	
KFM09A	636.00	641.00	3	1	2005-12-15 23:43	2005-12-16 00:58	__KFM09A_0636.00_200512152343.ht2	P, Q, Te	
KFM09A	641.00	646.00	3	1	2005-12-16 08:21	2005-12-16 09:36	__KFM09A_0641.00_200512160821.ht2	P, Q, Te	
KFM09A	646.00	651.00	3	1	2005-12-16 09:55	2005-12-16 10:38	__KFM09A_0646.00_200512160955.ht2	P, Q, Te	
KFM09A	651.00	656.00	3	1	2005-12-16 10:53	2005-12-16 12:10	__KFM09A_0651.00_200512161053.ht2	P, Q, Te	
KFM09A	656.00	661.00	3	1	2005-12-16 12:21	2005-12-16 13:20	__KFM09A_0656.00_200512161221.ht2	P, Q, Te	
KFM09A	661.00	666.00	3	1	2005-12-16 13:31	2005-12-16 14:14	__KFM09A_0661.00_200512161331.ht2	P, Q, Te	
KFM09A	731.00	736.00	3	1	2005-12-19 08:19	2005-12-19 09:01	__KFM09A_0731.00_200512190819.ht2	P, Q, Te	
KFM09A	736.00	741.00	3	1	2005-12-19 09:15	2005-12-19 09:56	__KFM09A_0736.00_200512190915.ht2	P, Q, Te	
KFM09A	741.00	746.00	3	1	2005-12-19 10:11	2005-12-19 11:30	__KFM09A_0741.00_200512191011.ht2	P, Q, Te	
KFM09A	746.00	751.00	3	1	2005-12-19 11:44	2005-12-19 12:36	__KFM09A_0746.00_200512191144.ht2	P, Q, Te	
KFM09A	751.00	756.00	3	1	2005-12-19 12:50	2005-12-19 14:05	__KFM09A_0751.00_200512191250.ht2	P, Q, Te	
KFM09A	756.00	761.00	3	1	2005-12-19 14:20	2005-12-19 15:42	__KFM09A_0756.00_200512191420.ht2	P, Q, Te	
KFM09A	761.00	766.00	3	1	2005-12-19 15:56	2005-12-19 17:16	__KFM09A_0761.00_200512191556.ht2	P, Q, Te	
KFM09A	766.00	771.00	3	1	2005-12-20 06:55	2005-12-20 08:10	__KFM09A_0766.00_200512200655.ht2	P, Q, Te	
KFM09A	771.00	776.00	3	1	2005-12-20 08:29	2005-12-20 09:46	__KFM09A_0771.00_200512200829.ht2	P, Q, Te	
KFM09A	776.00	781.00	3	1	2005-12-20 10:06	2005-12-20 11:24	__KFM09A_0776.00_200512201006.ht2	P, Q, Te	

Bh id	Test section		Test type	Test no	Test start Date, time	Test stop Date, time	Data files of raw and primary data	Parameters in file	Comments
idcode	(m)	(m)	(1-6)[1]		YYYYMMDD hh:mm	YYYYMMDD hh:mm	__Borehole id_secup_date and time of test start		
KFM09A	781.00	786.00	3	1	2005-12-20 11:35	2005-12-20 12:58	__KFM09A_0781.00_200512201135.ht2	P, Q, Te	
KFM09A	786.00	791.00	3	1	2005-12-20 13:11	2005-12-20 14:28	__KFM09A_0786.00_200512201311.ht2	P, Q, Te	

[1] Injection test
[2] The tests were interrupted for various reasons or did not provide satisfying data for the evaluation and were hence re-performed later

Appendix 2.1. General test data

Borehole:	KFM09A
Testtype:	CHir (Constant Head injection and recovery)
Field crew:	C. Hjerne, K. Gokall-Norman, T. Svensson, A. Lindquist, J. Harrström, E. Gustavsson
General comment:	

Test section secup	**Test section seclow**	**Test start**	**Start of flow period**	**Stop of flow period**	**Test stop**	**Total flow time t_p**	**Total recovery time t_F**
(m)	(m)	YYYYMMDD hh:mm	YYYYMMDD hh:mm:ss	YYYYMMDD hh:mm:ss	YYYYMMDD hh:mm	(min)	(min)
106.00	206.00	20051117 16:09	20051117 16:57:06	20051117 17:27:25	20051117 17:59	30	30
206.00	306.00	20051117 19:03	20051117 19:50:48	20051117 20:21:10	20051117 20:53	30	30
306.00	406.00	20051117 21:47	20051117 22:34:02	20051117 23:04:29	20051117 23:36	30	30
406.00	506.00	20051118 09:59	20051118 10:46:49	20051118 11:17:10	20051118 11:49	30	30
506.00	606.00	20051121 12:52	20051121 14:11:02	20051121 14:41:23	20051121 15:13	30	30
606.00	706.00	20051121 06:14	20051121 07:00:34	20051121 07:30:54	20051121 08:03	30	30
691.00	791.00	20051121 08:51	20051121 09:37:30	20051121 10:07:51	20051121 10:40	30	30
106.00	126.00	20051128 16:44	20051128 17:36:29	20051128 17:56:45	20051128 18:19	20	20
126.00	146.00	20051129 06:29	20051129 07:01:05	20051129 07:21:21	20051129 07:43	20	20
146.00	166.00	20051129 08:20	20051129 08:53:25	20051129 09:13:42	20051129 09:35	20	20
166.00	186.00	20051129 10:00	20051129 10:33:21	20051129 10:53:39	20051129 11:15	20	20
186.00	206.00	20051129 12:14	20051129 12:48:51	20051129 13:09:11	20051129 13:31	20	20
206.00	226.00	20051129 14:01	20051129 14:36:49	20051129 14:40:14	20051129 14:47	3	5
226.00	246.00	20051129 15:38	20051129 16:13:49	20051129 16:34:11	20051129 16:56	20	20
238.00	258.00	20051129 17:18	20051129 17:54:33	20051129 18:14:55	20051129 18:37	20	20
258.00	278.00	20051129 18:58	20051129 19:35:15	20051129 19:55:42	20051129 20:17	20	20
278.00	298.00	20051129 21:03	20051129 21:42:40	20051129 22:03:04	20051129 22:25	20	20
286.00	306.00	20051129 22:41	20051129 23:15:24	20051129 23:35:54	20051129 23:57	21	20
306.00	326.00	20051130 06:29	20051130 07:05:44	20051130 07:26:04	20051130 07:48	20	20
326.00	346.00	20051130 08:16	20051130 08:53:03	20051130 09:13:26	20051130 09:35	20	20
346.00	366.00	20051130 10:06	20051130 10:40:24	20051130 11:00:46	20051130 11:22	20	20
366.00	386.00	20051130 12:06	20051130 12:41:16	20051130 13:01:46	20051130 13:23	21	20
386.00	406.00	20051130 13:50	20051130 14:25:53	20051130 14:46:29	20051130 15:08	21	20
406.00	426.00	20051130 15:30	20051130 16:04:48	20051130 16:25:26	20051130 16:47	21	20
426.00	446.00	20051130 18:18	20051130 18:55:34	20051130 19:16:08	20051130 19:38	21	20
446.00	466.00	20051130 20:03	20051130 21:02:55	20051130 21:23:31	20051130 21:45	21	20
466.00	486.00	20051130 22:03	20051130 22:37:39	20051130 22:58:37	20051130 23:20	21	19
486.00	506.00	20051201 08:06	20051201 08:51:37	20051201 09:11:58	20051201 09:34	20	20
506.00	526.00	20051201 10:01	20051201 10:39:48	20051201 11:00:08	20051201 11:22	20	20
526.00	546.00	20051201 11:41	20051201 13:03:33	20051201 13:23:52	20051201 13:46	20	20
545.00	565.00	20051201 14:21	20051201 14:59:12	20051201 15:02:07	20051201 15:09	3	5
566.00	586.00	20051201 15:34	20051201 16:08:01	20051201 16:10:17	20051201 16:17	2	5
586.00	606.00	20051202 07:55	20051202 08:28:21	20051202 08:29:58	20051202 08:37	2	5
606.00	626.00	20051202 08:58	20051202 09:40:01	20051202 10:00:18	20051202 10:22	20	20
626.00	646.00	20051202 10:43	20051202 11:22:44	20051202 11:43:05	20051202 12:05	20	20
646.00	666.00	20051202 13:12	20051202 13:52:57	20051202 14:13:15	20051202 14:35	20	20
666.00	686.00	20051202 14:57	20051202 15:30:57	20051202 15:51:01	20051202 16:13	20	20
686.00	706.00	20051205 08:22	20051205 09:10:31	20051205 09:30:35	20051205 09:53	20	20
691.00	711.00	20051205 10:10	20051205 10:52:46	20051205 11:05:04	20051205 11:12	12	5
711.00	731.00	20051205 12:46	20051205 13:20:23	20051205 13:22:52	20051205 13:30	2	5
731.00	751.00	20051205 13:49	20051205 14:29:26	20051205 14:49:46	20051205 15:12	20	20
751.00	771.00	20051205 15:30	20051205 16:12:15	20051205 16:32:33	20051205 16:54	20	20
771.00	791.00	20051205 18:09	20051205 18:44:18	20051205 19:04:38	20051205 19:26	20	20
106.00	111.00	20051207 07:32	20051207 08:10:17	20051207 08:30:41	20051207 08:52	20	20
111.00	116.00	20051207 09:08	20051207 09:42:13	20051207 10:02:37	20051207 10:24	20	20
116.00	121.00	20051221 15:48	20051221 16:27:38	20051221 16:47:54	20051208 17:51	20	20
121.00	126.00	20051207 12:52	20051207 13:26:31	20051207 13:46:51	20051207 14:09	20	20
126.00	131.00	20051207 14:26	20051207 15:21:48	20051207 15:42:09	20051207 16:04	20	20
128.00	133.00	20051207 16:21	20051207 16:58:15	20051207 17:18:34	20051207 17:40	20	20
133.00	138.00	20051207 17:58	20051207 18:34:22	20051207 18:54:23	20051207 19:16	20	20
138.00	143.00	20051207 19:42	20051207 20:30:41	20051207 20:50:56	20051207 21:13	20	20
141.00	146.00	20051207 21:27	20051207 22:03:25	20051207 22:23:49	20051207 22:45	20	20
146.00	151.00	20051207 23:02	20051207 23:35:21	20051207 23:55:41	20051208 00:17	20	20
151.00	156.00	20051208 06:16	20051208 06:49:42	20051208 06:51:37	20051208 06:59	2	5
156.00	161.00	20051208 07:10	20051208 07:44:24	20051208 08:04:38	20051208 08:26	20	20
161.00	166.00	20051208 08:36	20051208 09:10:22	20051208 09:30:41	20051208 09:52	20	20
166.00	171.00	20051208 10:03	20051208 10:36:39	20051208 10:56:56	20051208 11:19	20	20
171.00	176.00	20051208 12:12	20051208 12:47:14	20051208 13:07:30	20051208 13:29	20	20

Test section secup	Test section seclow	Test start	Start of flow period	Stop of flow period	Test stop	Total flow time t_p	Total recovery time t_F
(m)	(m)	YYYYMMDD hh:mm	YYYYMMDD hh:mm:ss	YYYYMMDD hh:mm:ss	YYYYMMDD hh:mm	(min)	(min)
176.00	181.00	20051208 13:43	20051208 14:15:22	20051208 14:35:42	20051208 14:57	20	20
181.00	186.00	20051208 15:13	20051208 15:45:32	20051208 16:05:52	20051208 16:28	20	20
186.00	191.00	20051208 16:36	20051208 17:09:19	20051208 17:29:36	20051208 17:51	20	20
191.00	196.00	20051208 18:03	20051208 18:35:40	20051208 18:42:32	20051208 18:50	7	5
196.00	201.00	20051208 19:02	20051208 19:35:04	20051208 19:39:45	20051208 19:47	5	5
201.00	206.00	20051208 19:57	20051208 20:30:56	20051208 20:32:09	20051208 20:39	1	5
226.00	231.00	20051208 20:58	20051208 21:30:25	20051208 21:32:31	20051208 21:40	2	5
232.00	237.00	20051208 21:54	20051208 22:26:14	20051208 22:46:32	20051208 23:08	20	20
237.00	242.00	20051208 23:21	20051208 23:52:47	20051209 00:13:05	20051209 00:35	20	20
240.80	245.80	20051209 08:08	20051209 08:41:39	20051209 09:01:58	20051209 09:24	20	20
246.80	251.80	20051221 13:55	20051221 14:26:40	20051221 14:28:04	20051221 14:35	1	5
251.50	256.50	20051209 09:40	20051209 10:12:05	20051209 10:14:57	20051209 10:22	3	5
256.50	261.50	20051209 10:34	20051209 11:06:25	20051209 11:10:31	20051209 11:18	4	5
273.00	278.00	20051209 11:30	20051209 12:39:59	20051209 13:00:19	20051209 13:22	20	20
278.00	283.00	20051209 13:34	20051209 14:05:39	20051209 14:26:00	20051209 14:48	20	20
283.00	288.00	20051209 15:04	20051209 15:36:41	20051209 15:44:08	20051209 15:51	7	5
288.00	293.00	20051209 16:00	20051209 16:33:16	20051209 16:53:38	20051209 17:15	20	20
293.00	298.00	20051212 08:21	20051212 08:59:52	20051212 09:20:12	20051212 09:42	20	20
296.00	301.00	20051221 12:39	20051221 13:11:23	20051221 13:21:20	20051221 13:28	10	5
301.00	306.00	20051221 11:45	20051221 12:18:01	20051221 12:21:31	20051221 12:29	4	5
306.00	311.00	20051212 09:58	20051212 10:30:37	20051212 10:31:58	20051212 10:39	1	5
311.00	316.00	20051212 10:49	20051212 12:23:33	20051212 12:25:31	20051212 12:33	2	5
316.00	321.00	20051212 12:43	20051212 13:19:35	20051212 13:23:52	20051212 13:31	4	5
321.00	326.00	20051212 13:44	20051212 14:20:06	20051212 14:40:29	20051212 15:02	20	20
346.00	351.00	20051212 15:31	20051212 16:05:39	20051212 16:06:46	20051212 16:14	1	5
351.00	356.00	20051221 10:04	20051021 10:36:43	20051021 10:56:56	20051221 11:19	20	20
356.00	361.00	20051221 08:54	20051221 09:25:06	20051221 09:43:27	20051221 09:50	18	5
361.00	366.00	20051221 07:28	20051221 08:00:40	20051221 08:20:51	20051221 08:43	20	20
363.00	368.00	20051212 16:39	20051212 17:11:54	20051212 17:32:16	20051212 17:54	20	20
368.00	373.00	20051213 06:27	20051213 07:15:59	20051213 07:17:12	20051213 07:24	1	5
371.00	376.00	20051213 07:35	20051213 08:09:41	20051213 08:23:48	20051213 08:48	14	20
376.00	381.00	20051213 09:02	20051213 09:37:12	20051213 09:51:20	20051213 09:58	14	5
381.00	386.00	20051213 10:10	20051213 10:42:36	20051213 11:02:40	20051213 11:25	20	20
386.00	391.00	20051213 11:57	20051213 12:33:30	20051213 12:53:52	20051213 13:16	20	20
391.00	396.00	20051213 13:28	20051213 14:05:53	20051213 14:26:16	20051213 14:48	20	20
396.00	401.00	20051213 15:06	20051213 15:37:15	20051213 15:41:39	20051213 15:49	4	5
401.00	406.00	20051213 16:00	20051213 16:33:21	20051213 16:53:44	20051213 17:15	20	20
406.00	411.00	20051213 17:25	20051213 17:56:34	20051213 18:10:55	20051213 18:18	14	5
411.00	416.00	20051213 18:36	20051213 19:07:32	20051213 19:27:56	20051213 19:50	20	20
414.00	419.00	20051213 20:06	20051213 20:39:31	20051213 20:59:55	20051213 21:22	20	20
419.00	424.00	20051213 21:32	20051213 22:04:11	20051213 22:24:35	20051213 22:46	20	20
421.00	426.00	20051213 22:55	20051213 23:26:44	20051213 23:47:06	20051214 00:09	20	20
426.00	431.00	20051214 06:51	20051214 07:32:04	20051214 07:52:07	20051214 07:59	20	5
431.00	436.00	20051214 08:11	20051214 08:49:02	20051214 09:09:24	20051214 09:31	20	20
436.00	441.00	20051214 09:47	20051214 10:20:56	20051214 10:22:10	20051214 10:29	1	5
441.00	446.00	20051214 10:44	20051214 11:18:15	20051214 11:38:42	20051214 12:00	20	20
446.00	451.00	20051214 12:13	20051214 13:21:31	20051214 13:41:55	20051214 14:04	20	20
451.00	456.00	20051214 14:22	20051214 14:56:20	20051214 15:16:46	20051214 15:38	20	20
456.00	461.00	20051214 15:55	20051214 16:30:00	20051214 16:50:24	20051214 17:12	20	20
461.00	466.00	20051214 17:32	20051214 18:04:52	20051214 18:07:43	20051214 18:15	3	5
471.00	476.00	20051214 18:35	20051214 19:08:00	20051214 19:28:26	20051214 19:50	20	20
476.00	481.00	20051214 20:01	20051214 20:40:37	20051214 21:00:58	20051214 21:23	20	20
486.00	491.00	20051214 21:40	20051214 22:17:49	20051214 22:23:53	20051214 22:31	6	5
491.00	496.00	20051214 22:58	20051214 23:29:36	20051214 23:49:58	20051215 00:12	20	20
496.00	501.00	20051215 06:33	20051215 07:15:10	20051215 07:35:32	20051215 07:57	20	20
501.00	506.00	20051215 08:14	20051215 08:47:17	20051215 08:53:08	20051215 09:00	6	5
506.00	511.00	20051220 19:00	20051220 19:41:12	20051220 20:01:35	20051220 20:23	20	20
511.00	516.00	20051220 20:50	20051220 21:22:36	20051220 21:42:55	20051220 22:05	20	20
516.00	521.00	20051220 22:14	20051220 22:45:57	20051220 23:06:17	20051220 23:28	20	20
521.00	526.00	20051215 09:25	20051215 10:01:53	20051215 10:03:44	20051215 10:11	2	5
526.00	531.00	20051215 10:26	20051215 10:58:38	20051215 10:59:49	20051215 11:07	1	5
531.00	536.00	20051215 11:23	20051215 12:01:54	20051215 12:22:16	20051215 12:44	20	20
536.00	541.00	20051215 13:19	20051215 13:52:58	20051215 13:56:08	20051215 14:03	3	5
541.00	546.00	20051215 14:14	20051215 14:46:13	20051215 15:06:37	20051215 15:28	20	20
561.00	566.00	20051220 17:14	20051220 17:49:31	20051220 17:50:36	20051220 17:58	1	5
606.00	611.00	20051215 16:19	20051215 16:50:43	20051215 16:52:47	20051215 17:00	2	5
611.00	616.00	20051215 17:19	20051215 17:52:51	20051215 18:13:12	20051215 18:35	20	20
616.00	621.00	20051215 18:50	20051215 19:21:48	20051215 19:23:40	20051215 19:31	2	5
621.00	626.00	20051215 19:44	20051215 20:21:06	20051215 20:41:34	20051215 21:03	20	20

Test section **secup**	**Test section** **seclow**	**Test start**	**Start of flow period**	**Stop of flow period**	**Test stop**	**Total flow time** t_p	**Total recovery time** t_F
(m)	(m)	YYYYMMDD hh:mm	YYYYMMDD hh:mm:ss	YYYYMMDD hh:mm:ss	YYYYMMDD hh:mm	(min)	(min)
626.00	631.00	20051215 21:14	20051215 21:45:46	20051215 21:54:10	20051215 22:01	8	5
631.00	636.00	20051215 22:08	20051215 22:51:11	20051215 23:11:40	20051215 23:33	20	20
636.00	641.00	20051215 23:43	20051216 00:15:28	20051216 00:35:56	20051216 00:58	20	20
641.00	646.00	20051216 08:21	20051216 08:53:39	20051216 09:14:01	20051216 09:36	20	20
646.00	651.00	20051216 09:55	20051216 10:28:16	20051216 10:31:02	20051216 10:38	3	5
651.00	656.00	20051216 10:53	20051216 11:27:51	20051216 11:48:20	20051216 12:10	20	20
656.00	661.00	20051216 12:21	20051216 13:03:34	20051216 13:12:30	20051216 13:20	9	5
661.00	666.00	20051216 13:31	20051216 14:04:48	20051216 14:06:57	20051216 14:14	2	5
731.00	736.00	20051219 08:19	20051219 08:52:49	20051219 08:54:27	20051219 09:01	2	5
736.00	741.00	20051219 09:15	20051219 09:46:55	20051219 09:49:06	20051219 09:56	2	5
741.00	746.00	20051219 10:11	20051219 10:47:39	20051219 11:08:09	20051219 11:30	21	20
746.00	751.00	20051219 11:44	20051219 12:22:11	20051219 12:29:10	20051219 12:36	7	5
751.00	756.00	20051219 12:50	20051219 13:23:07	20051219 13:43:35	20051219 14:05	20	20
756.00	761.00	20051219 14:20	20051219 15:00:30	20051219 15:20:59	20051219 15:42	20	20
761.00	766.00	20051219 15:56	20051219 16:33:37	20051219 16:54:07	20051219 17:16	21	20
766.00	771.00	20051220 06:55	20051220 07:28:05	20051220 07:48:28	20051220 08:10	20	20
771.00	776.00	20051220 08:29	20051220 09:04:02	20051220 09:24:27	20051220 09:46	20	20
776.00	781.00	20051220 10:06	20051220 10:41:52	20051220 11:02:21	20051220 11:24	20	20
781.00	786.00	20051220 11:35	20051220 12:15:53	20051220 12:36:19	20051220 12:58	20	20
786.00	791.00	20051220 13:11	20051220 13:46:19	20051220 14:06:43	20051220 14:28	20	20
506.00 [1)]	606.00	20051118 13:32	20051118 14:18:02	20051118 14:26:00	20051118 14:28	8	0
426.00 [1)]	446.00	20051130 17:10	20051130 17:43:55	20051130 17:56:57	20051130 18:03	13	4
116.00 [1)]	121.00	20051207 10:38	20051207 12:36:48	20051207 12:38:34	20051207 12:39	2	0

[1)] The tests were interrupted for various reasons or did not provide satisfying data for the evaluation and were hence re-performed later

Appendix 2.2 Pressure and flow data

Summary of pressure and flow data for all tests in KFM09A

Test section		Pressure			Flow		
secup	seclow	p_i	p_p	p_F	Q_p 1)	Q_m 2)	V_p 2)
(m)	(m)	(kPa)	(kPa)	(kPa)	(m^3/s)	(m^3/s)	(m^3)
106.00	206.00	929.78	1114.19	948.54	7.07E-05	9.33E-05	1.70E-01
206.00	306.00	1746.27	1963.05	1759.94	1.31E-06	1.62E-06	2.95E-03
306.00	406.00	2542.61	2753.18	2631.48	4.06E-06	7.19E-06	1.31E-02
406.00	506.00	3314.26	3517.7	3472.12	1.07E-05	3.77E-05	6.87E-02
506.00	606.00	4075.97	4296.2	4263.63	1.94E-06	8.12E-06	1.48E-02
606.00	706.00	4781.92	4987.26	4843.19	5.72E-07	8.03E-07	1.46E-03
691.00	791.00	5371.98	5548.07	5405.64	8.41E-07	1.23E-06	2.24E-03
106.00	126.00	939.44	1152.92	946.07	8.47E-06	9.98E-06	1.22E-02
126.00	146.00	1108.5	1324.71	1158.02	2.71E-05	4.44E-05	5.40E-02
146.00	166.00	1277.24	1460	1389.29	4.5E-06	1.26E-05	1.54E-02
166.00	186.00	1439.66	1628.85	1451.67	4.24E-05	4.98E-05	6.07E-02
186.00	206.00	1609	1908.7	1627.19	1.41E-07	1.63E-07	1.99E-04
206.00	226.00	1799.82	1971.07	1959.47			
226.00	246.00	1936.29	2142.18	1942.92	9.72E-07	1.18E-06	1.45E-03
238.00	258.00	2036.61	2246.5	2073.17	2.46E-07	3.84E-07	4.70E-04
258.00	278.00	2205.79	2409.18	2271.89	5.18E-08	9.9E-08	1.22E-04
278.00	298.00	2363.51	2574.6	2423.68	1.11E-07	1.57E-07	1.92E-04
286.00	306.00	2426.85	2640.1	2497.64	6.13E-08	9.62E-08	1.19E-04
306.00	326.00	2588.71	2788.52	2720.63	2.78E-07	6.73E-07	8.23E-04
326.00	346.00	2751.68	2952.8	2816.12	2.09E-08	4.56E-08	5.58E-05
346.00	366.00	2908.57	3113.84	2949.69	4.37E-08	5.89E-08	7.20E-05
366.00	386.00	3063.39	3264.59	3103.70	1.28E-06	1.6E-06	1.98E-03
386.00	406.00	3219.88	3419.73	3326.14	2.69E-06	5.5E-06	6.80E-03
406.00	426.00	3378.16	3578.01	3432.11	3.99E-07	4.89E-07	6.05E-04
426.00	446.00	3545.41	3765.49	3714.71	1.85E-05	4.93E-05	6.10E-02
446.00	466.00	3693.33	3922.81	3730.72	7.09E-08	9.94E-08	1.23E-04
466.00	486.00	3856.58	4029.33	3923.36	4E-08	7.55E-08	9.52E-05
486.00	506.00	4001.32	4206.1	4108.27	1.17E-07	2.67E-07	3.27E-04
506.00	526.00	4171.74	4362.23	4210.38	4.34E-08	7.76E-08	9.50E-05
526.00	546.00	4303.1	4508.03	4472.57	2.91E-06	9.83E-06	1.20E-02
545.00	565.00	4514.1	4661.19	4675.69			
566.00	586.00	4631.11	4820.31	4823.61			
586.00	606.00	4765.93	4982.58	4989.21			
606.00	626.00	4896.47	5096.82	4980.92	4.76E-07	7.39E-07	9.01E-04
626.00	646.00	5050.61	5258.42	5072.55	8.54E-08	1.15E-07	1.41E-04
646.00	666.00	5186.25	5389.93	5211.64	1.04E-07	1.27E-07	1.55E-04
666.00	686.00	5355.15	5533.99	5469.96	1.19E-08	3.11E-08	3.74E-05
686.00	706.00	5498.11	5687.43	5619.55	9.44E-09	2.33E-08	2.81E-05
691.00	711.00	5561.73	5724.42	5713.38			
711.00	731.00	5679.43	5864.34	5869.58			
731.00	751.00	5782.93	5995.56	5819.36	6.26E-08	8.05E-08	9.84E-05
751.00	771.00	5915.12	6118.38	1406.62	3.61E-07	1.07E-07	1.31E-04
771.00	791.00	6056.14	6271.55	1456.30	8.9E-07	4.69E-05	5.72E-02
106.00	111.00	948.9	1151.62	995.96	5.7E-07	6.88E-07	8.42E-04
111.00	116.00	993.19	1200.74	1037.91	6E-08	7.52E-08	9.20E-05
116.00	121.00	1025.62	1225.72	1627.41	2.15E-06	1.42E-07	1.73E-04
121.00	126.00	1074.34	1252.7	1076.55	5.98E-06	6.93E-06	8.47E-03
126.00	131.00	1121.53	1323.83	1249.86	3.85E-08	1.12E-07	1.37E-04
128.00	133.00	1131.88	1348.66	1163.76	1.74E-05	2.61E-05	3.18E-02
133.00	138.00	1174.24	1409.45	1217.29	1.66E-05	2.67E-05	3.21E-02
138.00	143.00	1215.08	1415.79	1219.50	3.09E-07	3.51E-07	4.28E-04
141.00	146.00	1240.89	1466.23	1321.06	1.24E-06	2.35E-06	2.88E-03
146.00	151.00	1284.09	1510.35	1450.22	1.33E-06	5.33E-06	6.51E-03
151.00	156.00	1349.21	1565.72	1571.10			
156.00	161.00	1365.5	1573.1	1482.79	4.26E-06	1.07E-05	1.31E-02
161.00	166.00	1408	1586.5	1406.62	1.02E-07	1.07E-07	1.31E-04
166.00	171.00	1447.05	1626.8	1456.30	4.09E-05	4.69E-05	5.72E-02
171.00	176.00	1496.45	1703.03	1687.02	5.5E-08	8.37E-07	1.03E-03
176.00	181.00	1534	1734.49	1557.86	2.91E-07	3.41E-07	4.15E-04
181.00	186.00	1575.38	1803.9	1780.30	2.5E-07	1.9E-06	2.35E-03
186.00	191.00	1616.92	1832.6	1627.41	1.23E-07	1.42E-07	1.73E-04
191.00	196.00	1677.49	1875.23	1828.87			
196.00	201.00	1710.62	1916.5	1891.79			
201.00	206.00	1766.78	1957.48	1965.21			
226.00	231.00	1961.89	2161.15	2158.94			

Test section		Pressure			Flow		
secup	seclow	p_i	p_p	p_F	Q_p 1)	Q_m 2)	V_p 2)
(m)	(m)	(kPa)	(kPa)	(kPa)	(m^3/s)	(m^3/s)	(m^3)
232.00	237.00	1992.95	2191.65	1995.02	8.39E-07	8.63E-07	1.05E-03
237.00	242.00	2032.55	2232.77	2040.28	1.7E-06	1.86E-06	2.27E-03
240.80	245.80	2060.01	2263.69	2071.18	3.22E-07	4.57E-07	5.58E-04
246.80	251.80	2184.89	2323.99	2971.99			
251.50	256.50	2217.45	2385.25	2408.43			
256.50	261.50	2239.39	2427.2	2424.45			
273.00	278.00	2328.68	2560.78	2393.53	6.8E-08	1E-07	1.22E-04
278.00	283.00	2369.8	2576.3	2435.48	9.75E-08	1.44E-07	1.76E-04
283.00	288.00	2409.26	2618.73	2574.58			
288.00	293.00	2459.9	2659.88	2540.35	1.57E-08	2.83E-08	3.40E-05
293.00	298.00	2493.43	2728	2549.74	3.38E-08	4.1E-08	5.00E-05
296.00	301.00	2521.45	2730.23	3349.53			
301.00	306.00	2567.81	2767.21	3301.51			
306.00	311.00	2678.48	2831.8	2864.35			
311.00	316.00	2652.96	2872.36	2868.77			
316.00	321.00	2674.48	2942.73	2935.01			
321.00	326.00	2712.56	2913.42	2845.04	2.98E-07	6.68E-07	8.16E-04
346.00	351.00	3017.39	3117.02	3125.44			
351.00	356.00	2958.18	3169.22	3512.92	5.07E-08	6.9E-08	8.44E-05
356.00	361.00	2991.17	3206.99	3532.23			
361.00	366.00	3026.221	3242.46	3698.38	1.76E-08	9.48E-09	1.14E-05
363.00	368.00	3062.65	3254.73	3095.07	1.17E-08	1.62E-08	1.95E-05
368.00	373.00	3128.47	3316.41	3294.88			
371.00	376.00	3108.19	3309.5	3140.33	1.47E-06	2.13E-06	2.12E-03
376.00	381.00	3174.01	3361.53	3334.08			
381.00	386.00	3234.58	3403.07	3284.95			
386.00	391.00	3226.58	3437.98	3349.53	2.47E-06	5.33E-06	6.53E-03
391.00	396.00	3274.47	3481.73	3301.51	1.66E-07	1.87E-07	2.29E-04
396.00	401.00	3321.1	3524.5	3485.87			
401.00	406.00	3346.08	3547.69	3369.95	4.26E-07	4.98E-07	6.09E-04
406.00	411.00	3392.03	3584.11	3550.45			
411.00	416.00	3426.25	3621.31	3496.35	3.7E-07	5.52E-07	6.76E-04
414.00	419.00	3460.47	3654.12	3480.91	1.3E-08	1.05E-08	1.27E-05
419.00	424.00	3488.626	3692.58	3512.92	5.68E-08	6.9E-08	8.44E-05
421.00	426.00	3515	3708.32	3532.23	5.78E-08	7.13E-08	8.73E-05
426.00	431.00	3560.79	3773.3	3698.38			
431.00	436.00	3579.7	3802.83	3753.02	1.61E-05	5.02E-05	6.15E-02
436.00	441.00	3649.79	3829.74	3837.47			
441.00	446.00	3661.4	3888.2	3871.14	2.09E-07	1.94E-06	2.41E-03
446.00	451.00	3702.236	3909.77	3866.72	3.75E-08	1.55E-07	1.90E-04
451.00	456.00	3761.02	3951.96	3840.22	1.24E-08	1.48E-08	1.78E-05
456.00	461.00	3787.78	3990.92	3815.94	6.76E-08	5.9E-08	7.22E-05
461.00	466.00	3916.81	4031.76	4071.50			
471.00	476.00	3902.457	4111.1	3964.42	5.28E-08	7.96E-08	9.75E-05
476.00	481.00	3964.425	4153.74	4008.03	4.27E-08	5.18E-08	6.33E-05
486.00	491.00	4047.08	4229.36	4217.76			
491.00	496.00	4063.22	4261.51	4095.23	7.8E-08	1.03E-07	1.26E-04
496.00	501.00	4090.13	4297.53	4222.18	6.24E-08	1.75E-07	2.15E-04
501.00	506.00	4165.19	4330.23	4289.52			
506.00	511.00	4215.56	4366.8	4289.52	1.64E-08	1.77E-08	2.13E-05
511.00	516.00	4232.67	4403.23	4229.36	2.98E-08	2.82E-08	3.44E-05
516.00	521.00	4254.199	4440.03	4285.67	1.94E-08	2.24E-08	2.70E-05
521.00	526.00	4405.3	4484.51	4539.01			
526.00	531.00	4442.14	4520.81	4592.00			
531.00	536.00	4354.65	4571.03	4535.15	2.91E-06	1.06E-05	1.30E-02
536.00	541.00	4479.13	4594.76	4560.54			
541.00	546.00	4437.45	4632.29	4613.53	8.67E-09	5.55E-08	6.67E-05
561.00	566.00	4726.95	4774.42	4801.19			
606.00	611.00	5042.26	5120.24	5224.00			
611.00	616.00	4956.43	5148.26	5044.06	3.96E-07	6.14E-07	7.50E-04
616.00	621.00	5077.59	5206.34	5272.02			
621.00	626.00	5032.46	5244.56	5127.97	1.53E-07	2.22E-07	2.73E-04
626.00	631.00	5085.18	5263.75	5233.38			
631.00	636.00	5136.79	5301.28	5249.39	1.17E-08	2.06E-08	2.47E-05
636.00	641.00	5144.52	5335.36	5146.73	1.35E-07	1.34E-07	1.64E-04
641.00	646.00	5195.3	5374.69	5235.59	1.27E-08	9.09E-07	1.11E-03
646.00	651.00	5309.69	5410.56	5419.40			
651.00	656.00	5248.56	5444.23	5280.30	1.27E-07	2.02E-05	9.65E-03
656.00	661.00	5344.46	5486.74	5472.94			
661.00	666.00	5426.71	5523.99	5534.21			
731.00	736.00	5867.31	6009.44	5986.26			

Test section		Pressure			Flow		
secup	seclow	p_i	p_p	p_F	Q_p [1)]	Q_m [2)]	V_p [2)]
(m)	(m)	(kPa)	(kPa)	(kPa)	(m^3/s)	(m^3/s)	(m^3)
736.00	741.00	5860.27	6044.22	5996.20			
741.00	746.00	5881.11	6078.44	5914.50	8.87E-08	7.57E-08	9.31E-05
746.00	751.00	5928.44	6112.66	6074.02			
751.00	756.00	5957.42	6143.29	6000.07	7.95E-08	1.26E-07	1.55E-04
756.00	761.00	5986.68	6192.63	6040.91	2.15E-07	3.66E-07	4.51E-04
761.00	766.00	6021.04	6221.97	6050.29	1.07E-07	1.57E-07	1.92E-04
766.00	771.00	6049.32	6239.82	6077.34	5.47E-08	7.57E-08	9.27E-05
771.00	776.00	6086.85	6319.41	6096.65	5.99E-08	6.39E-08	7.84E-05
776.00	781.00	6119.15	6309.34	6137.49	1.15E-07	1.4E-07	1.71E-04
781.00	786.00	6152.12	6325.44	6168.40	1.85E-07	2.36E-07	2.90E-04
786.00	791.00	6184.96	6388.23	6192.69	7.06E-07	9.09E-07	1.11E-03
506.00 [3)]	606.00	4063.27	4265.15	4264.74			
426.00 [3)]	446.00	3535.19	3703.67	3675.53			
116.00 [3)]	121.00	1074.89	1242.69	1074.34			

[1)] No value indicates a flow below measurement limit (measurement limit is unique for each test but nominally 1.67 E-8 m^3/s).
[2)] No value indicates that the parameter could not be calculated due to low and uncertain flow rates during a major part of flow period
[3)] The tests were interrupted for various reasons or did not provide satisfying data for the evaluation and were hence re-performed later.

p_i	Pressure in test section before start of flow period
p_p	Pressure in test section before stop of flow period
p_F	Pressure in test section at the end of recovery period
Q_p	Flow rate just before stop of flow period
Q_m	Mean (arithmetic) flow rate during flow period
V_p	Total volume injected during the flow period

Appendix 3. Test diagrams – Injection Tests

In the following pages diagrams are presented for all test sections. A linear diagram of pressure and flow rate is presented for each test. For most tests are lin-log and log-log diagrams presented, from injection and recovery period respectively.

Nomenclature for Aqtesolv:

T	=	transmissivity (m^2/s)
S	=	storativity (-)
K_z/K_r	=	ratio of hydraulic conductivities in the vertical and radial direction (set to 1)
Sw	=	skin factor
r(w)	=	borehole radius (m)
r(c)	=	effective casing radius (m)
C	=	well loss constant (set to 0)
r/B	=	leakage factor (-)

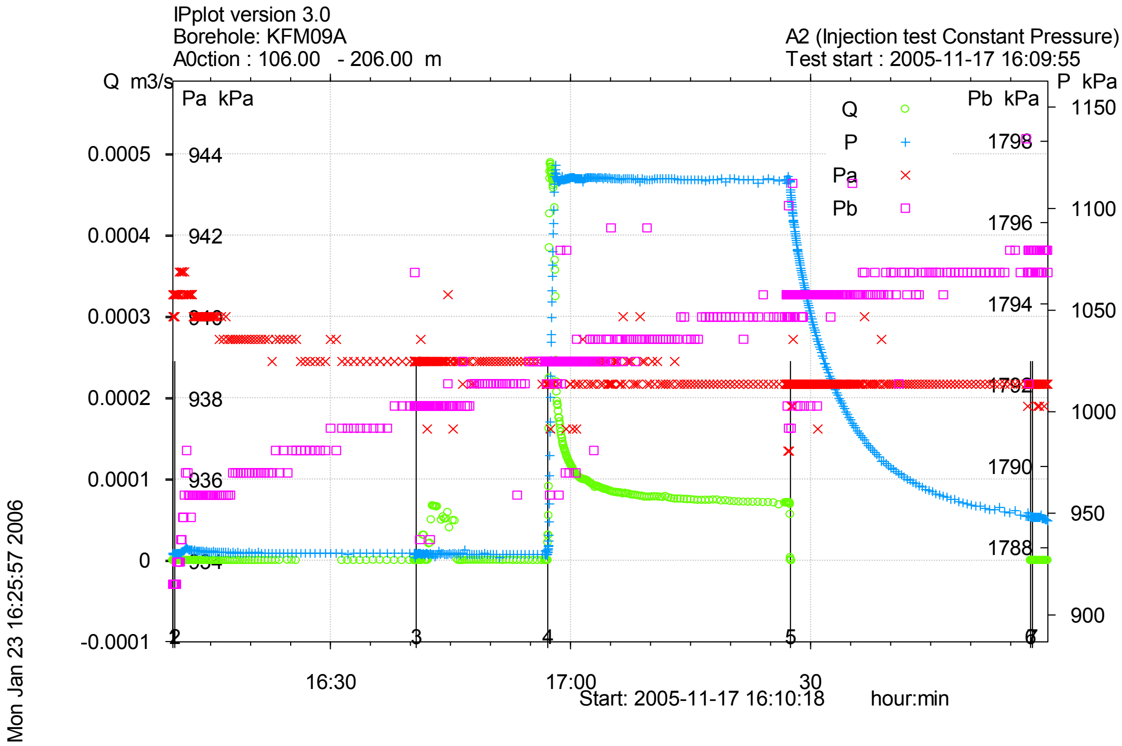


Figure A3-2. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 106.0-206.0 m in borehole KFM09A.*

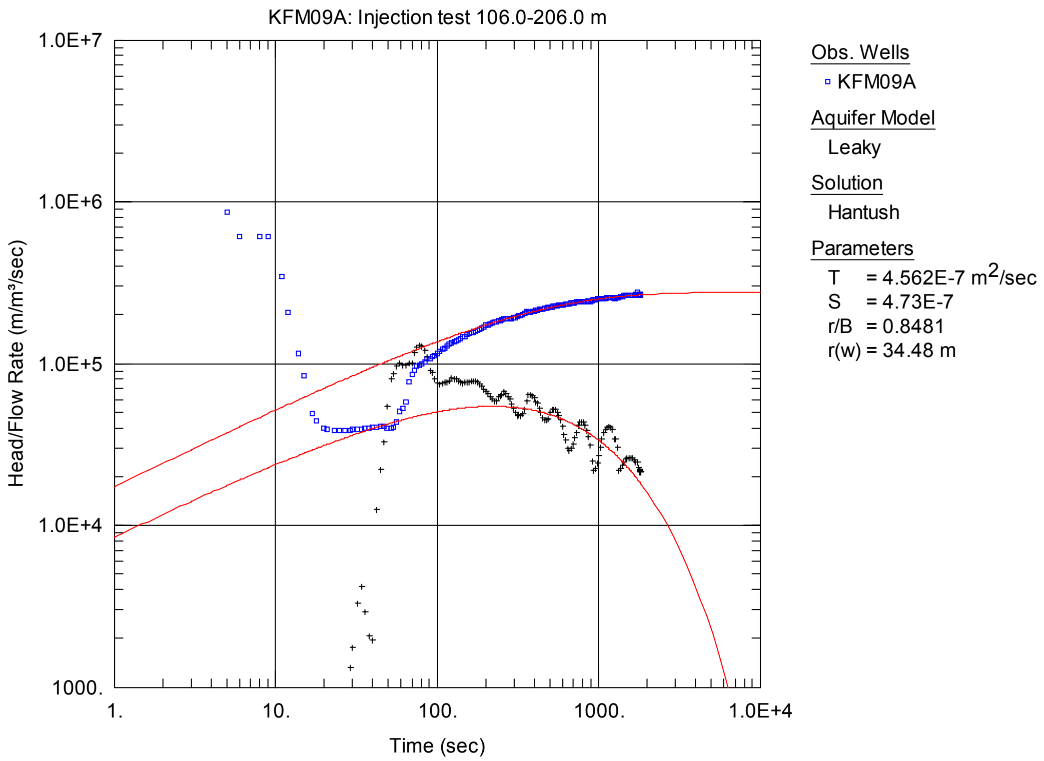


Figure A3-3. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 106.0-206.0 m in KFM09A.*

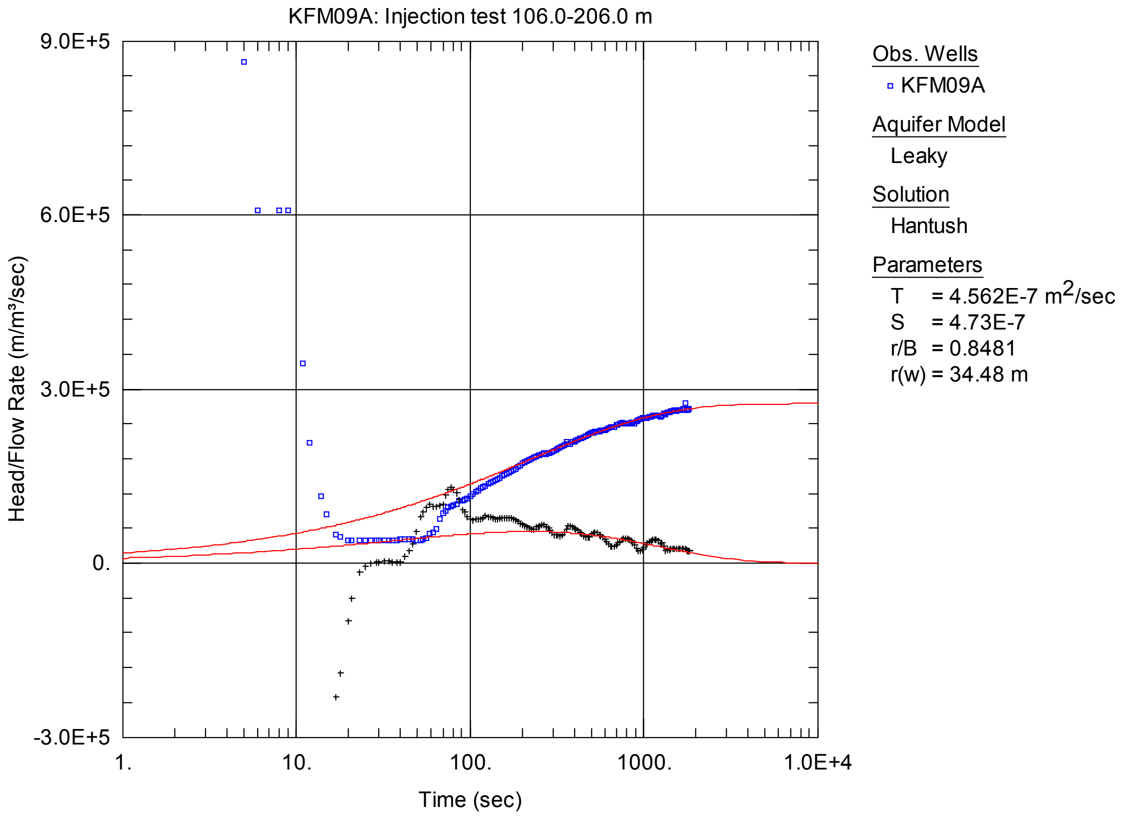


Figure A3-4. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 106.0-206.0 m in KFM09A.*

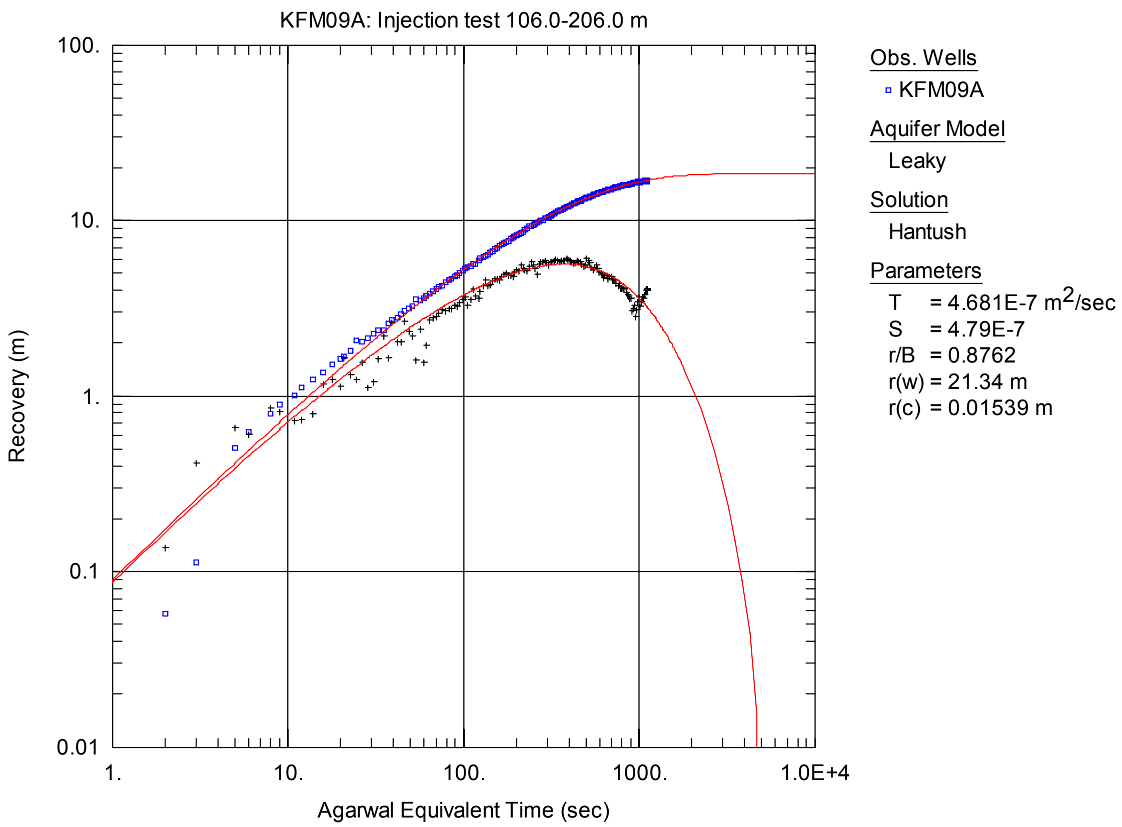


Figure A3-5. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 106.0-206.0 m in KFM09A.*

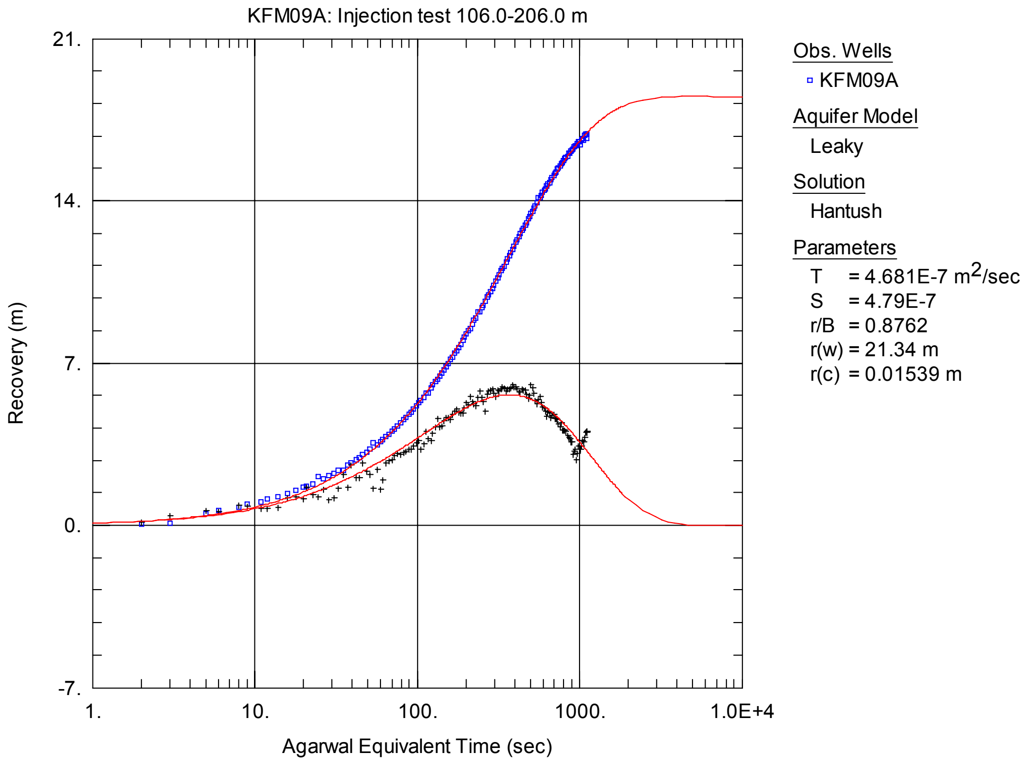


Figure A3-6. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 106.0-206.0 m in KFM09A.*

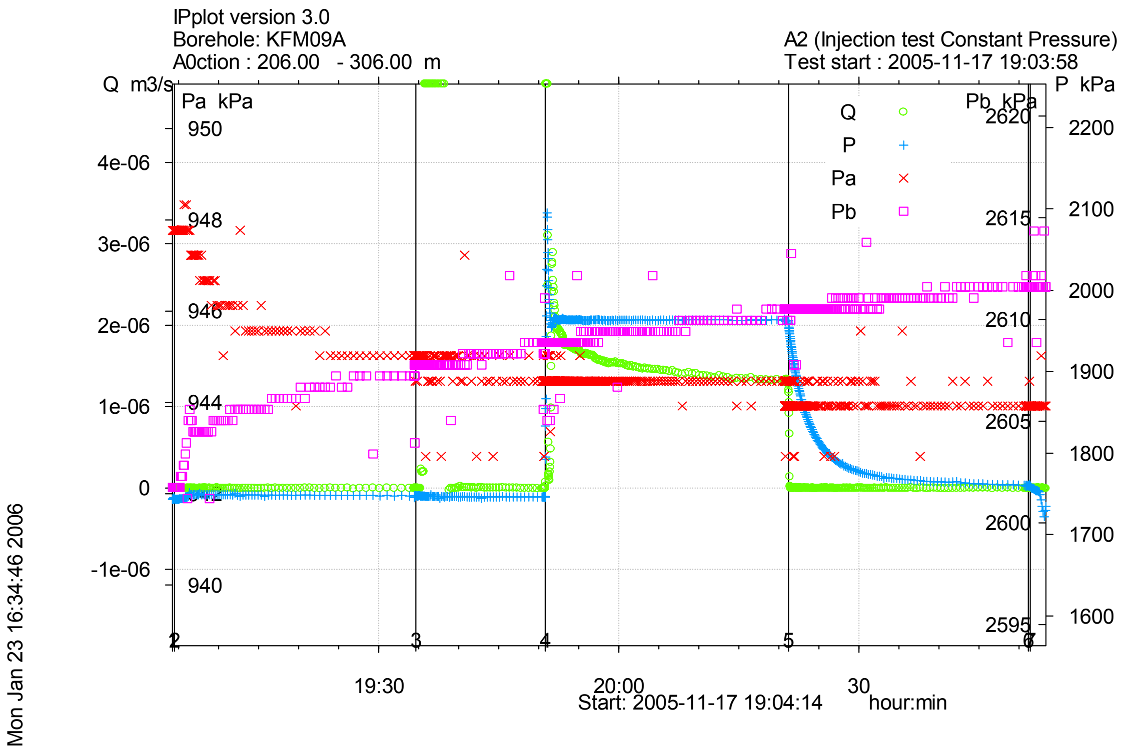


Figure A3-7. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 206.0-306.0 m in borehole KFM09A.*

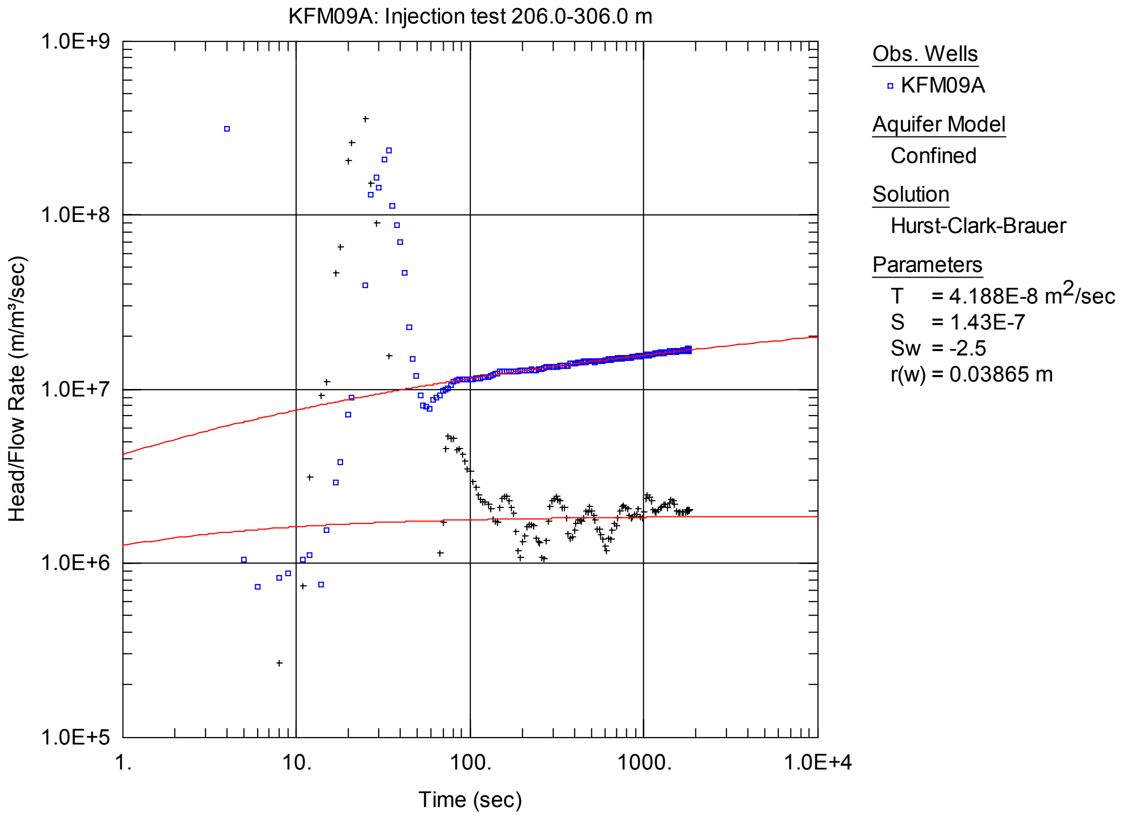


Figure A3-8. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 206.0-306.0 m in KFM09A.*

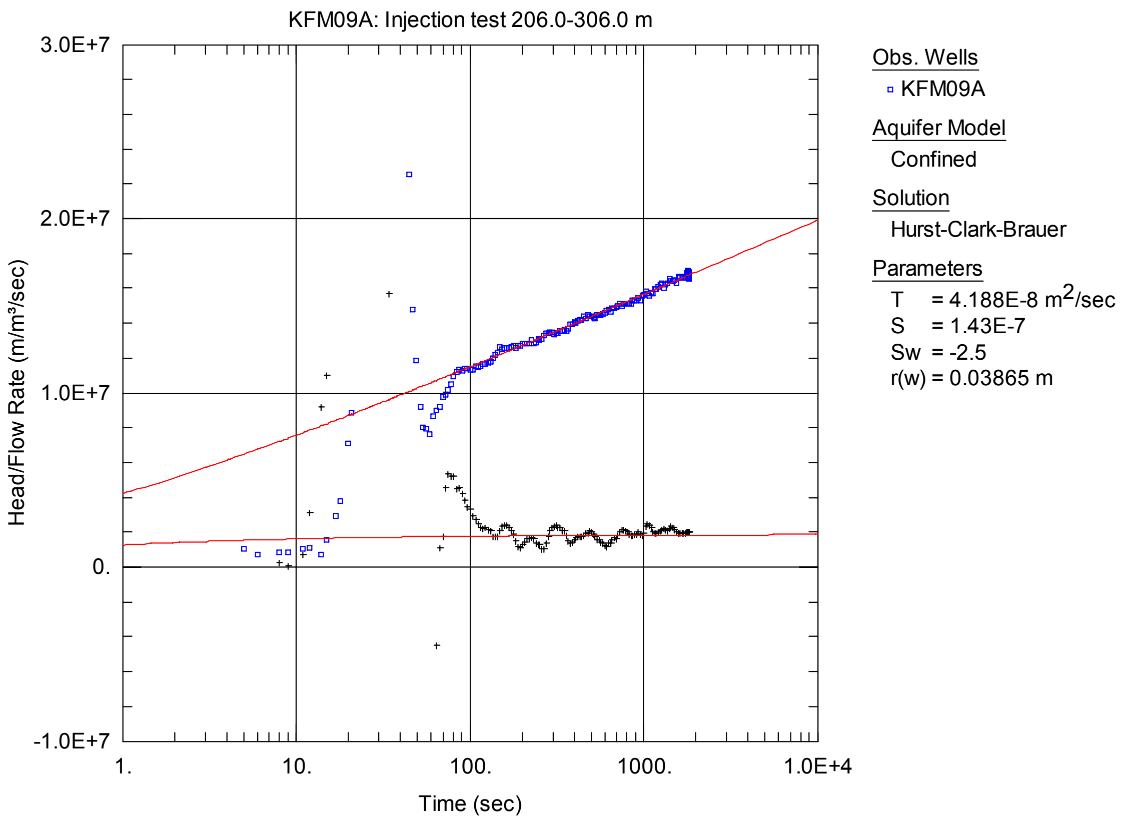


Figure A3-9. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 206.0-306.0 m in KFM09A.*

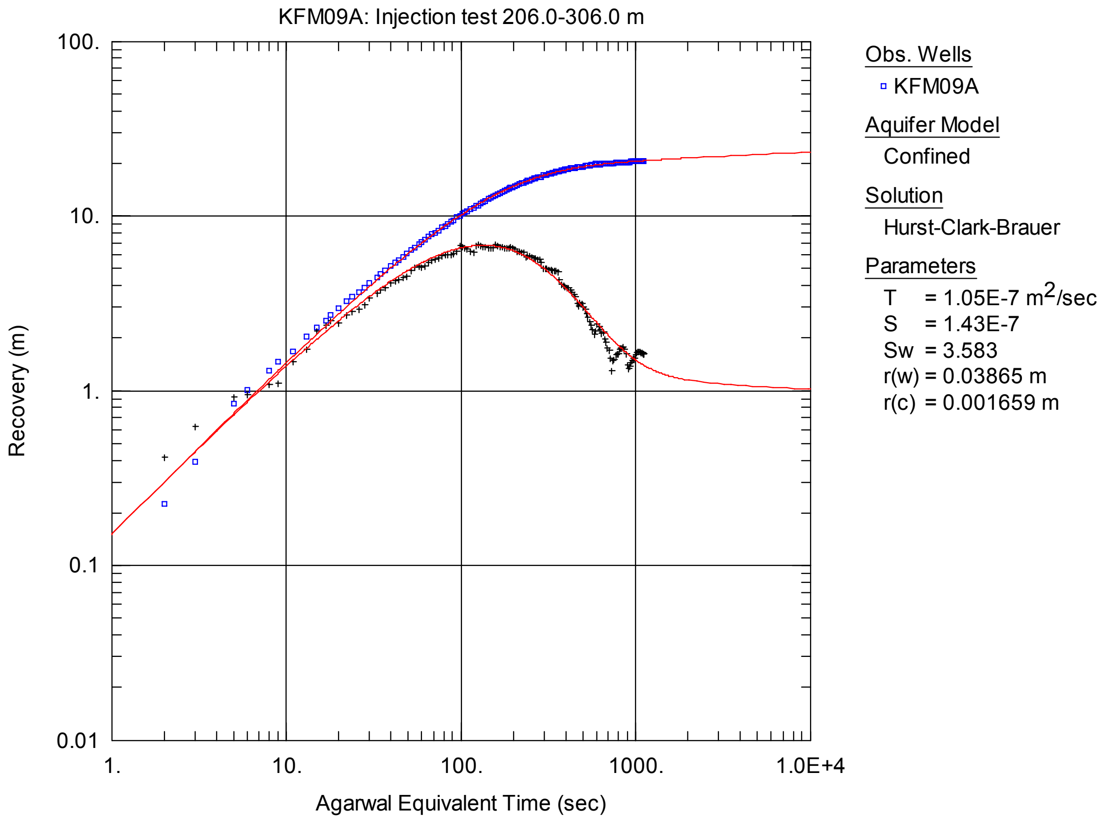


Figure A3-10. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 206.0-306.0 m in KFM09A.*

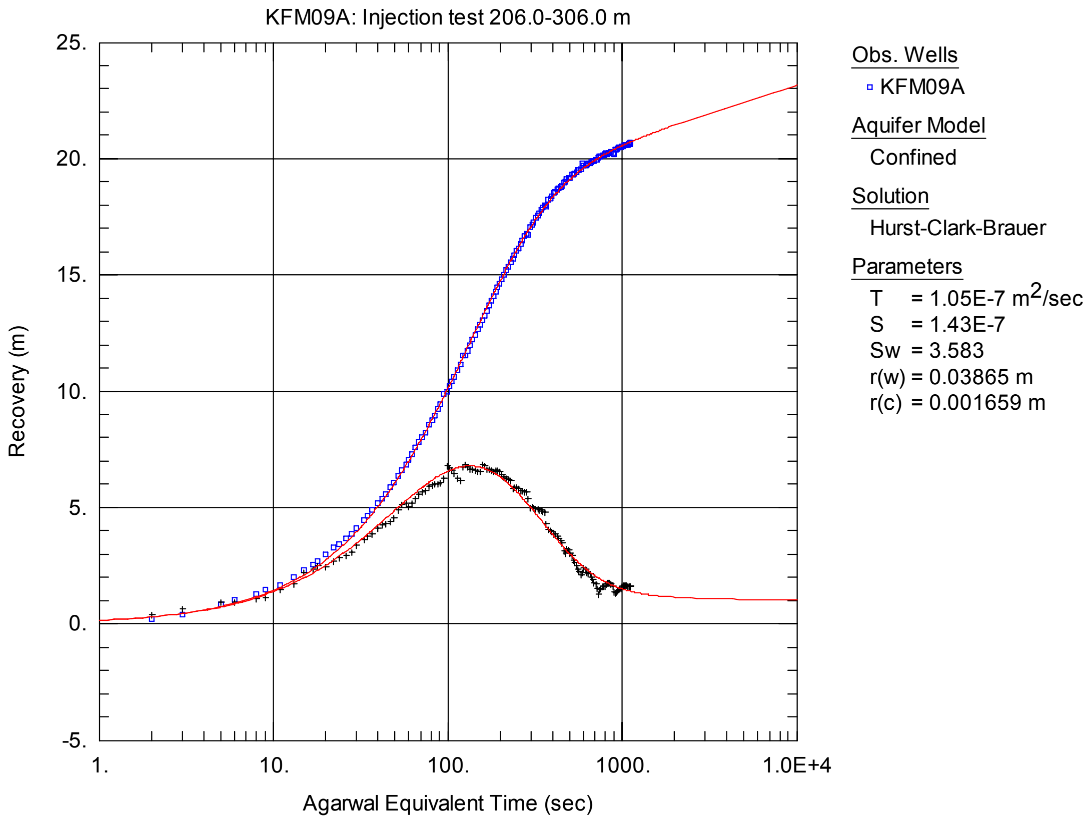


Figure A3-11. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 206.0-306.0 m in KFM09A.*

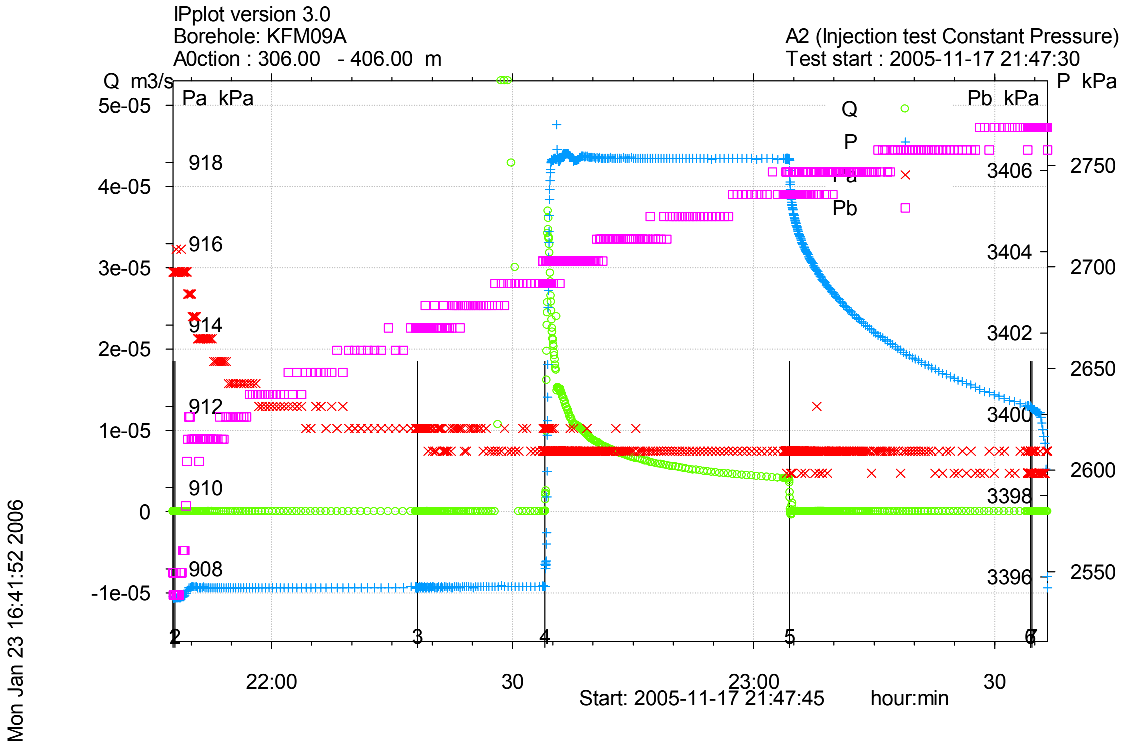


__Figure A3-12.__ Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 306.0-406.0 m in borehole KFM09A.

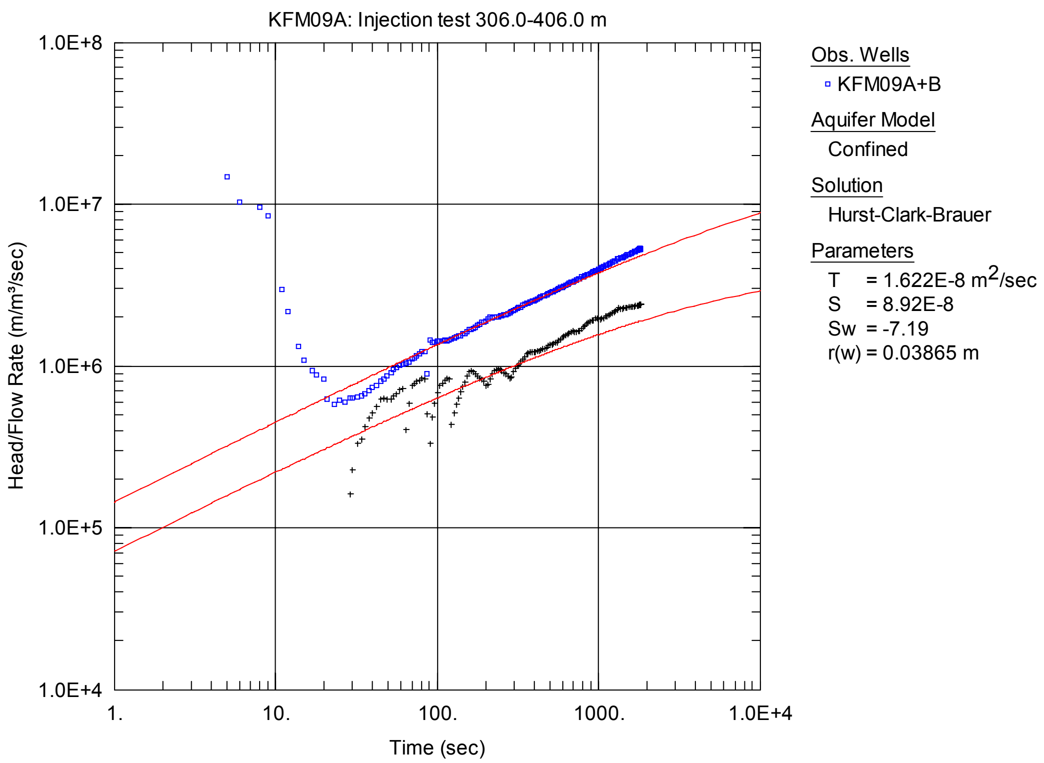


__Figure A3-13.__ Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 306.0-406.0 m in KFM09A.

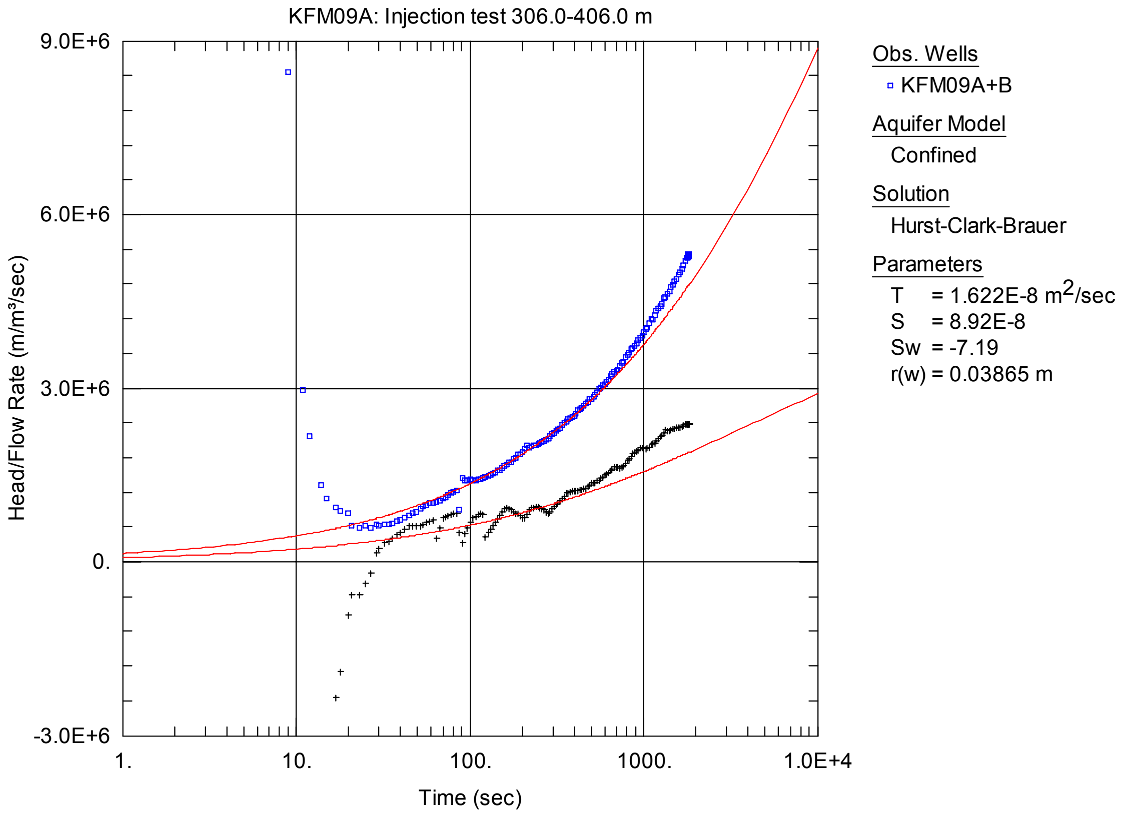


Figure A3-14. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 306.0-406.0 m in KFM09A.*

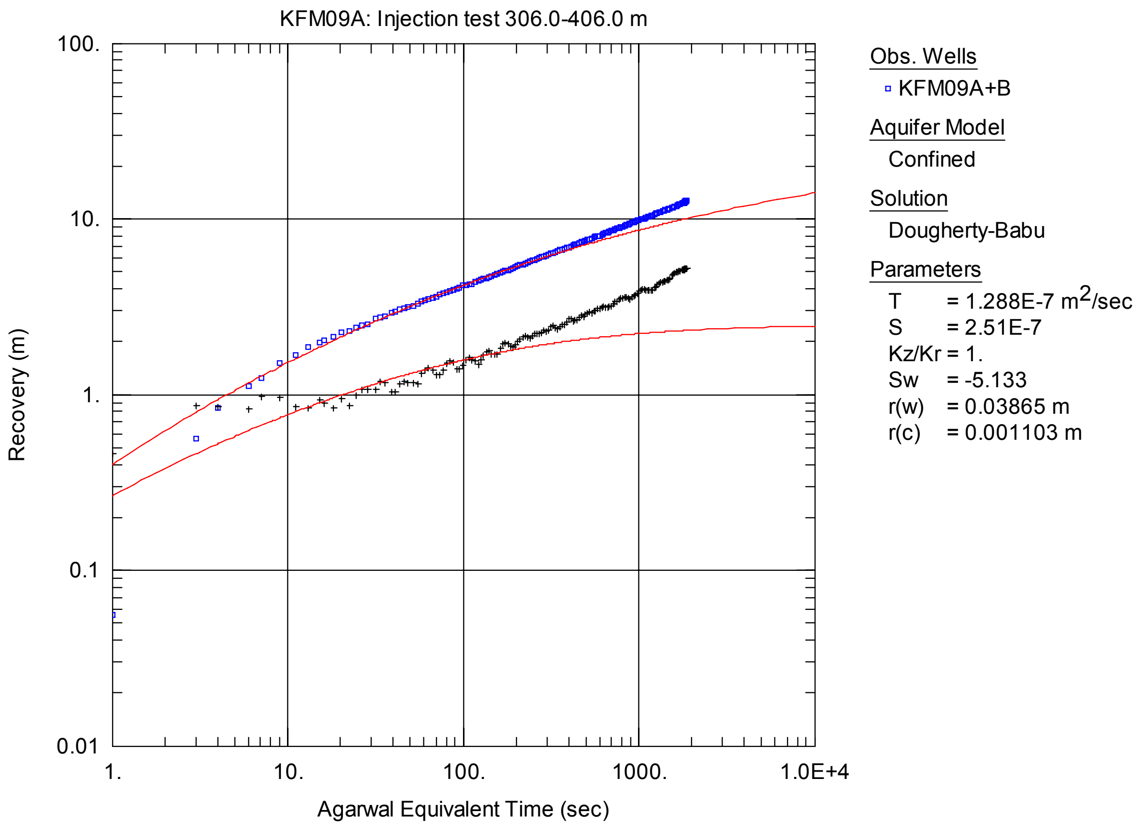


Figure A3-15. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 306.0-406.0x m in KFM09A.*

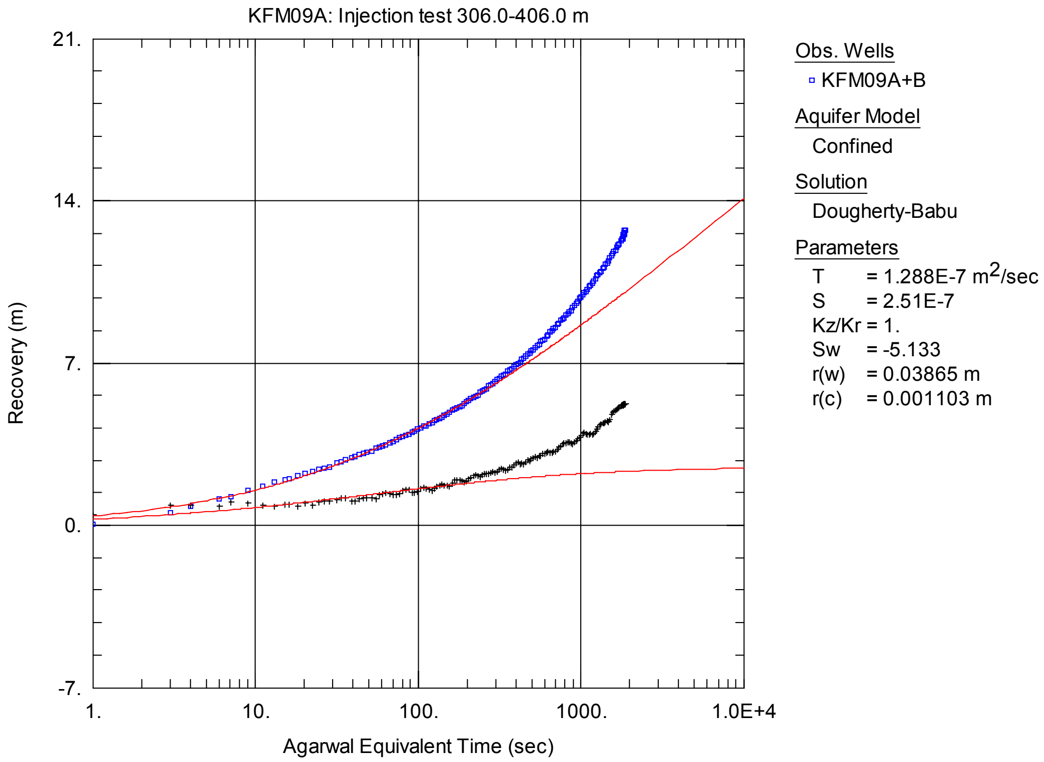


Figure A3-16. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 306.0-406.0 m in KFM09A.*

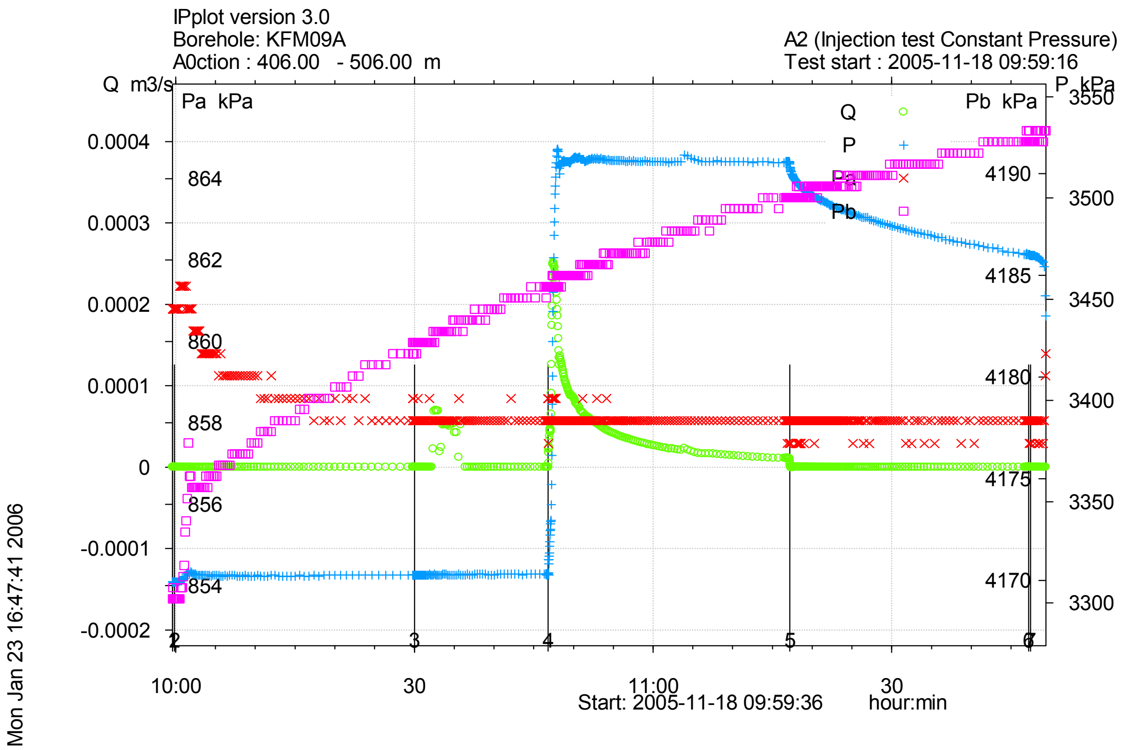


Figure A3-17. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 406.0-506.0 m in borehole KFM09A.*

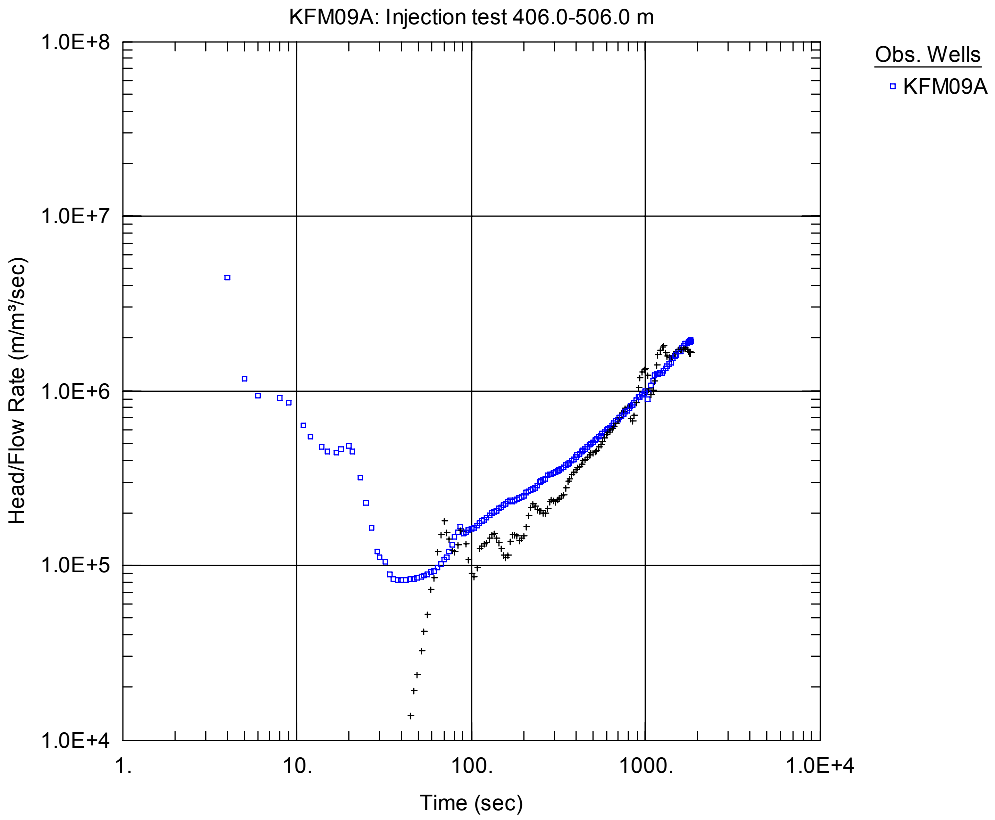


Figure A3-18. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 406.0-506.0 m in KFM09A.*

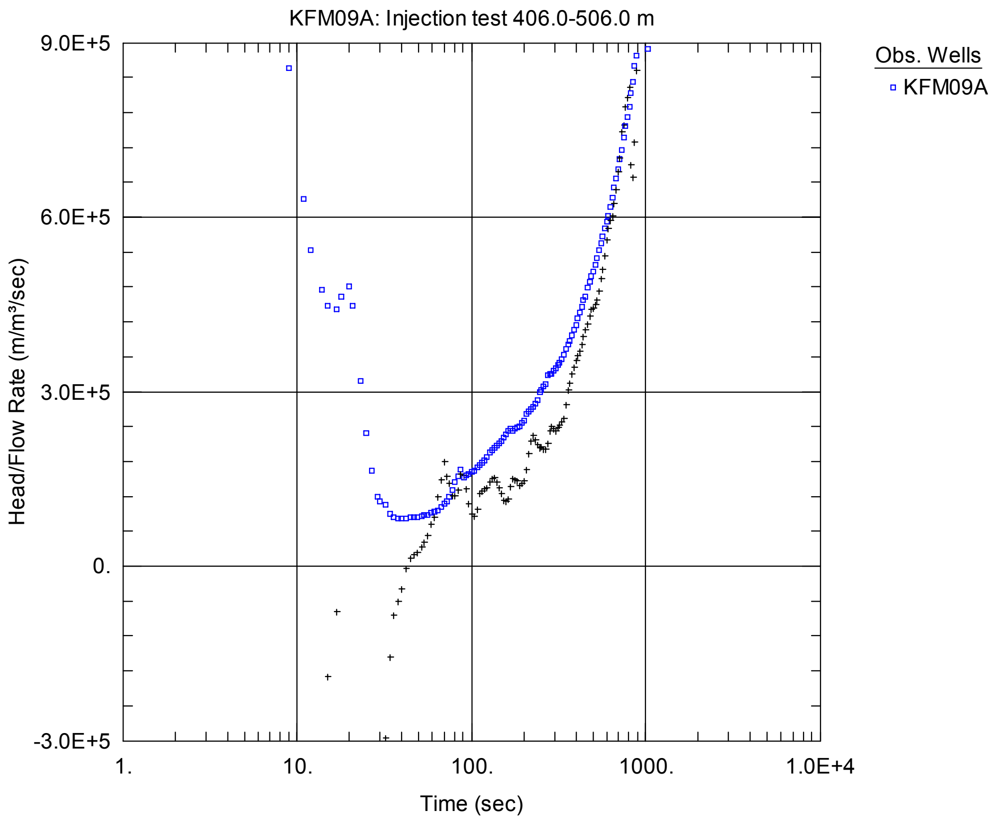


Figure A3-19. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 406.0-506.0 m in KFM09A.*

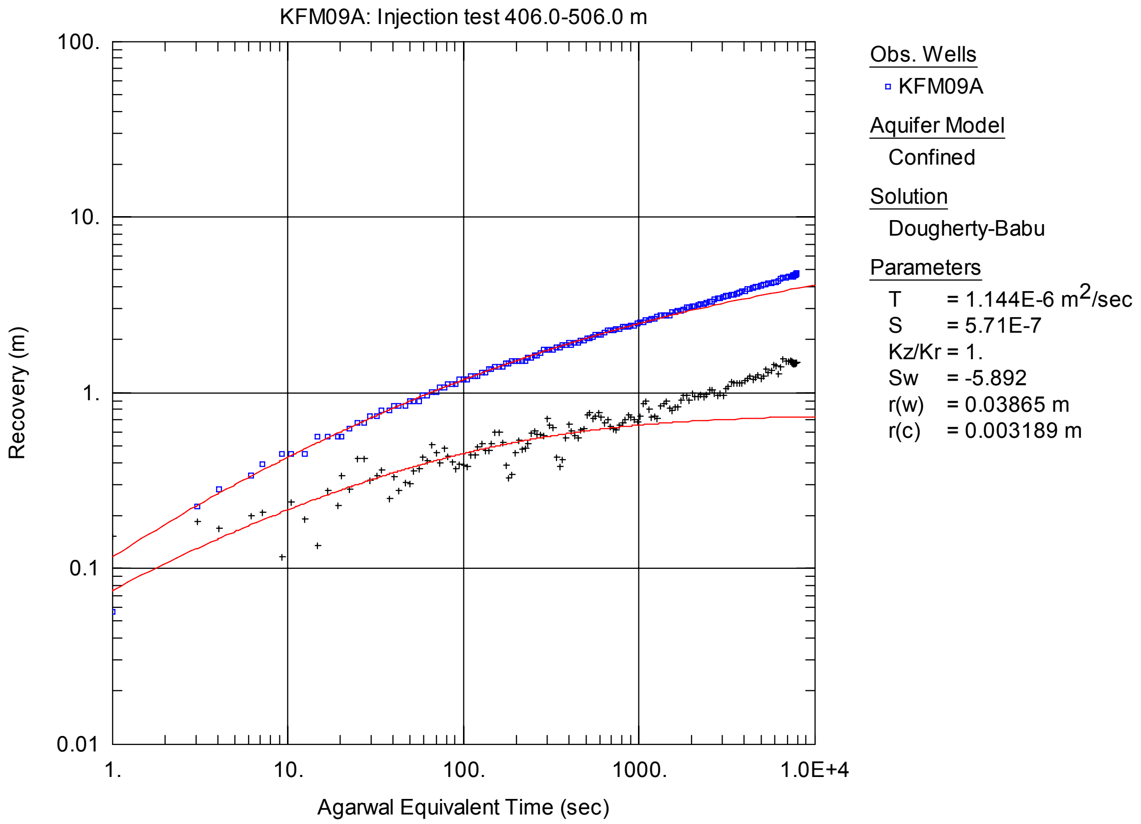


Figure A3-20. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 406.0-506.0 m in KFM09A.*

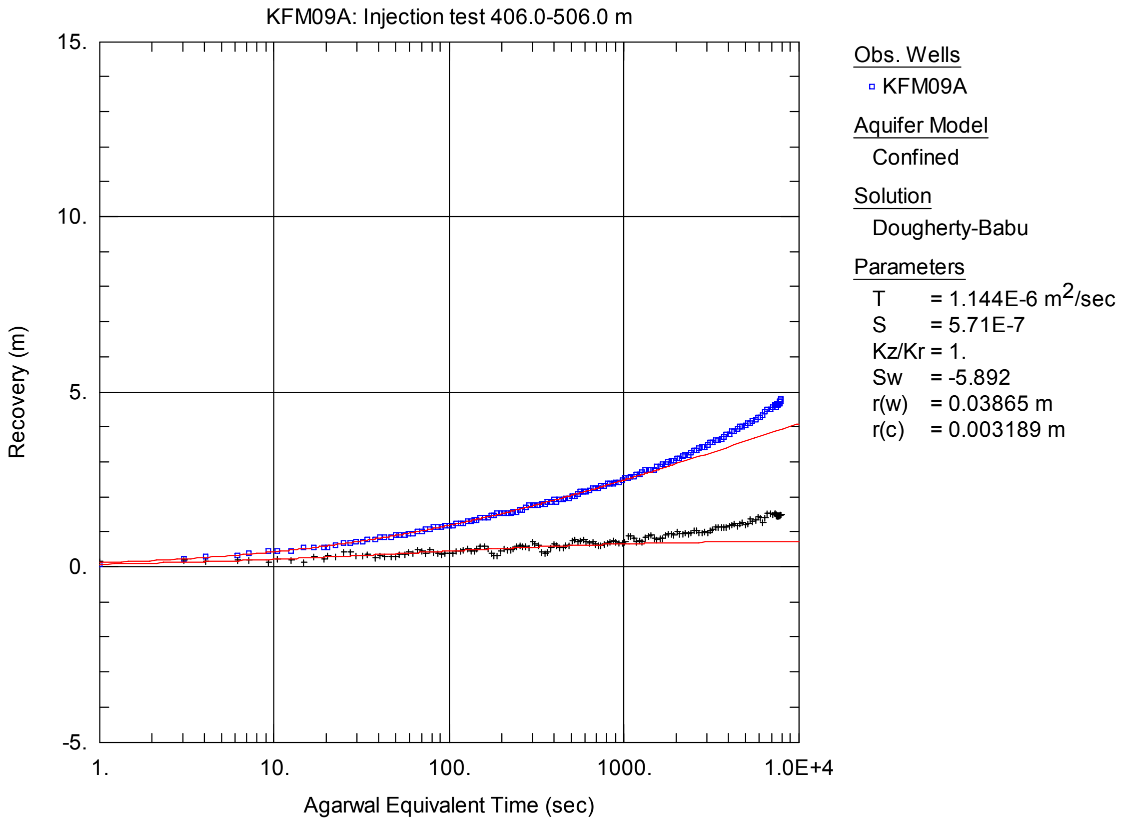


Figure A3-21. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 406.0-506.0 m in KFM09A.*

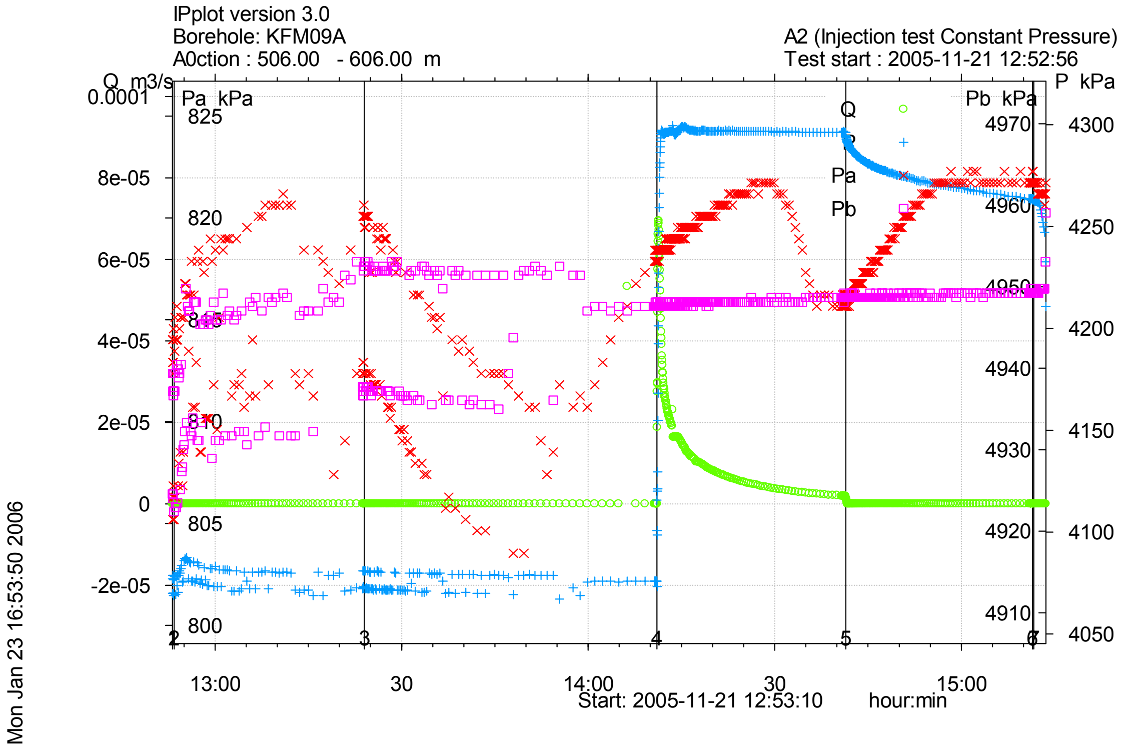


Figure A3-22. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 506.0-606.0 m in borehole KFM09A.*

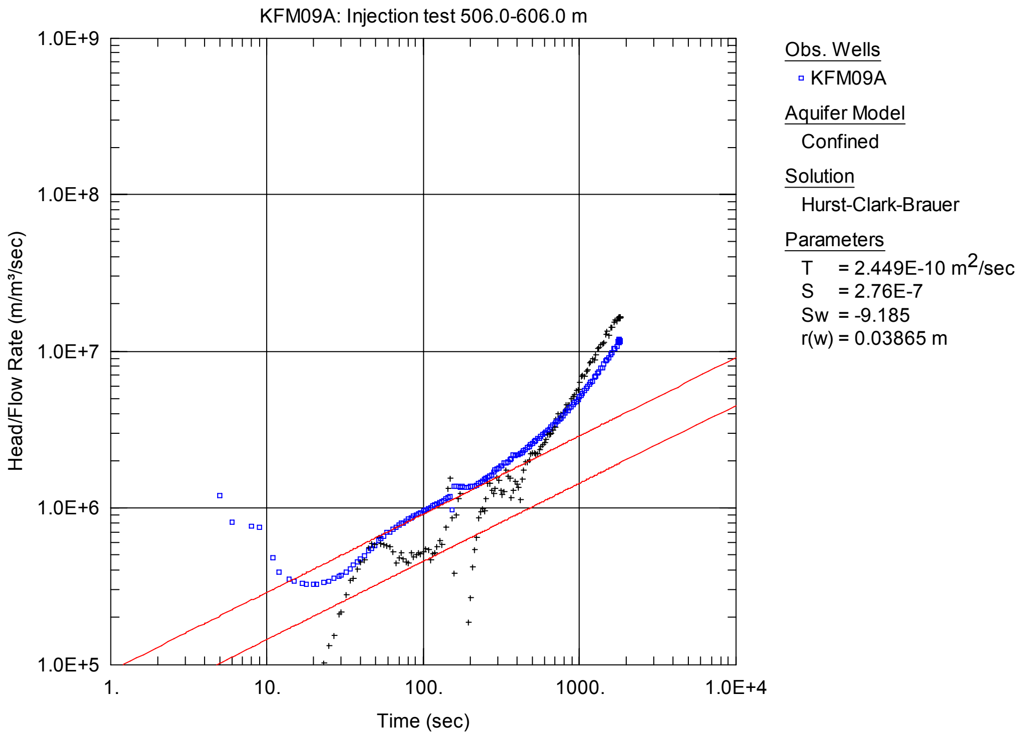


Figure A3-23. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 506.0-606.0 m in KFM09A. No unambiguous transit evaluation of transmissivity on this period is possible.*

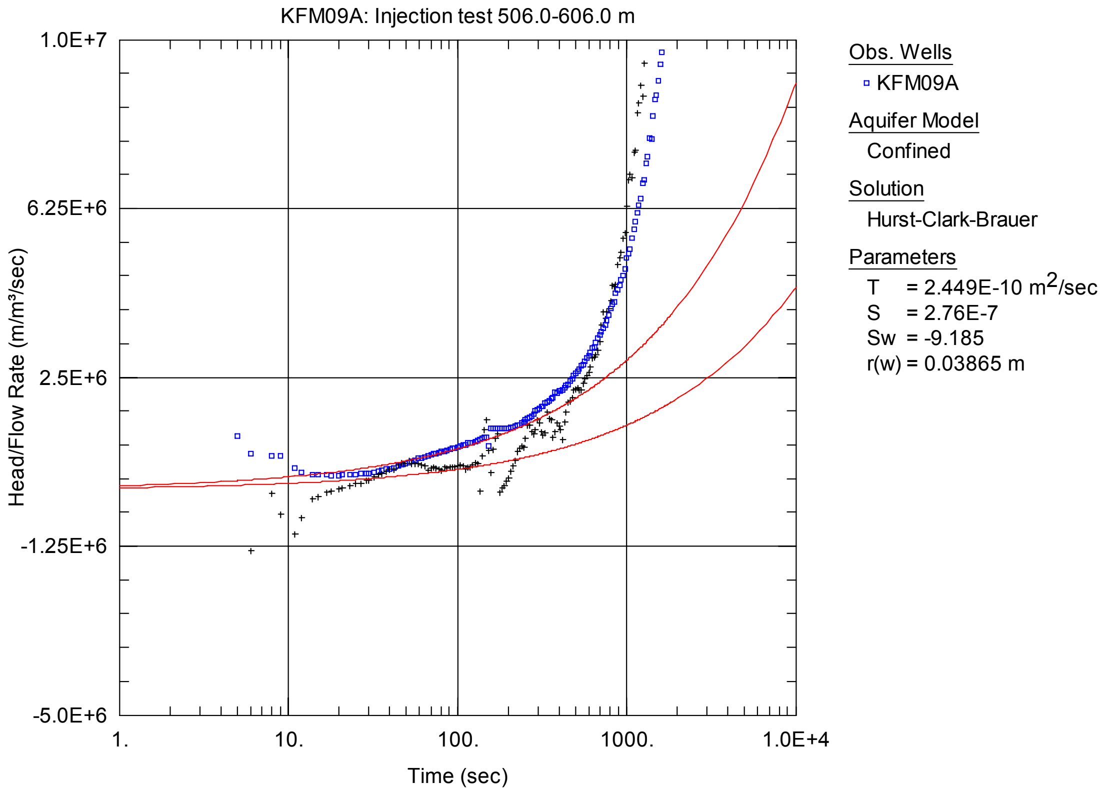


__Figure A3-24.__ Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 506.0-606.0 m in KFM09A. No unambiguous transit evaluation of transmissivity on this period is possible.

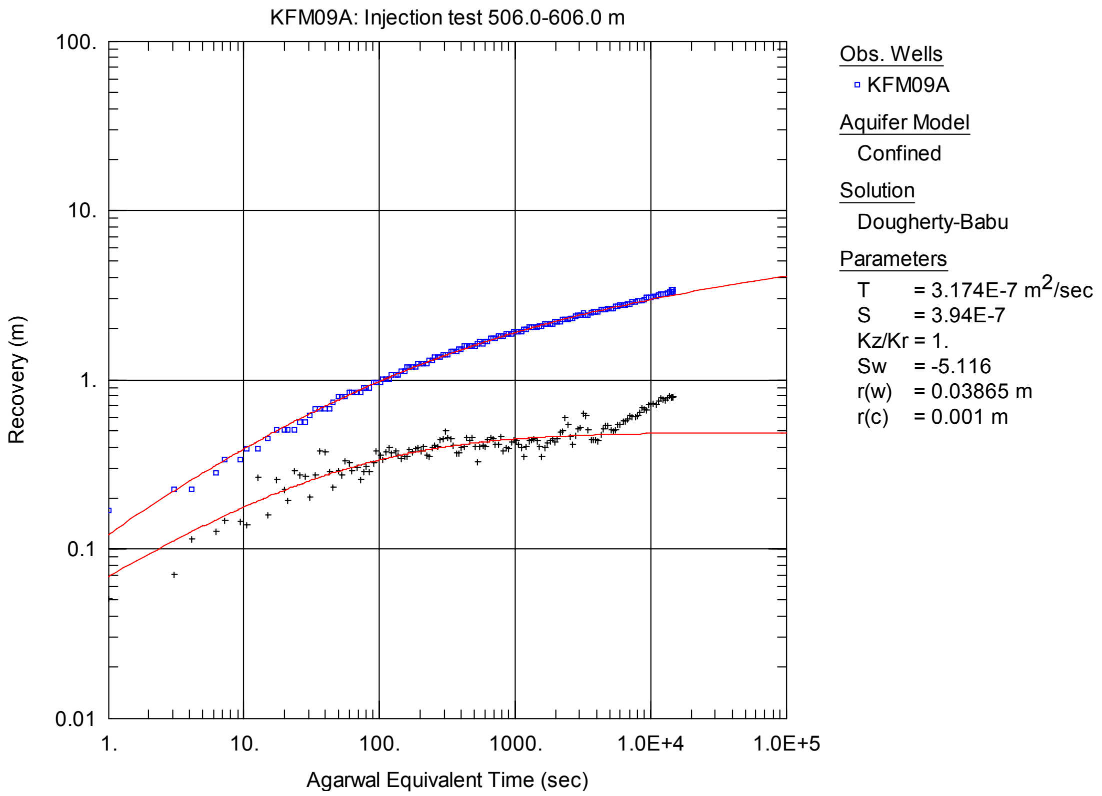


__Figure A3-25.__ Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 506.0-606.0 m in KFM09A.

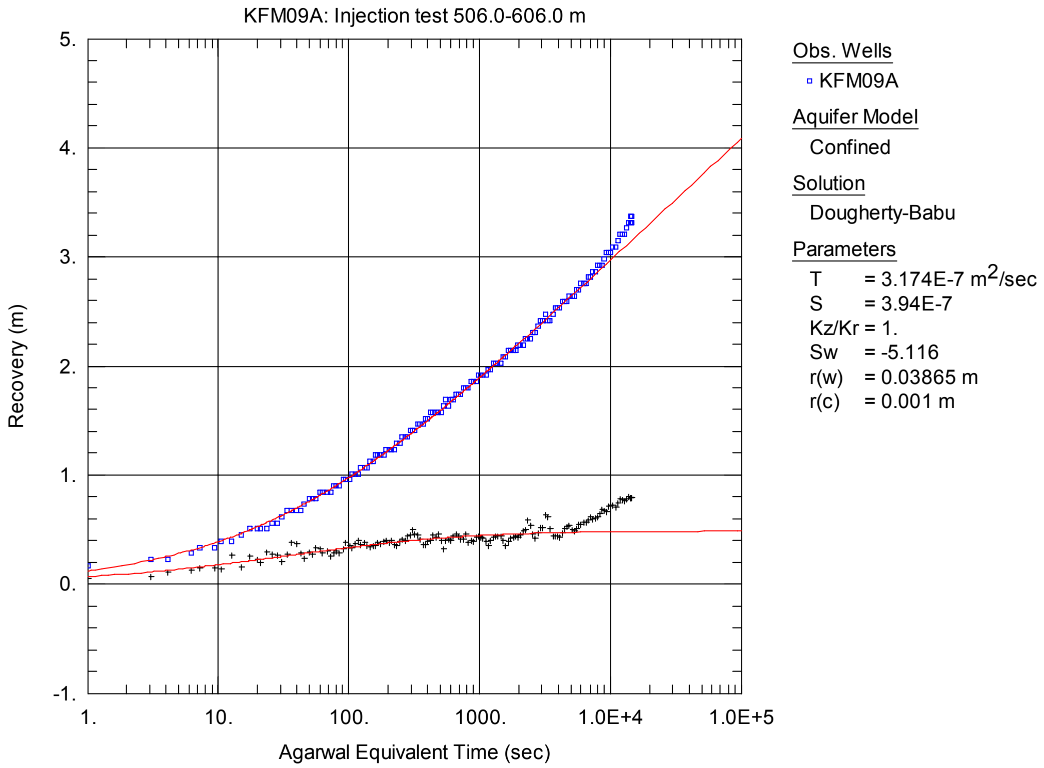


Figure A3-26. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 506.0-606.0 m in KFM09A.*

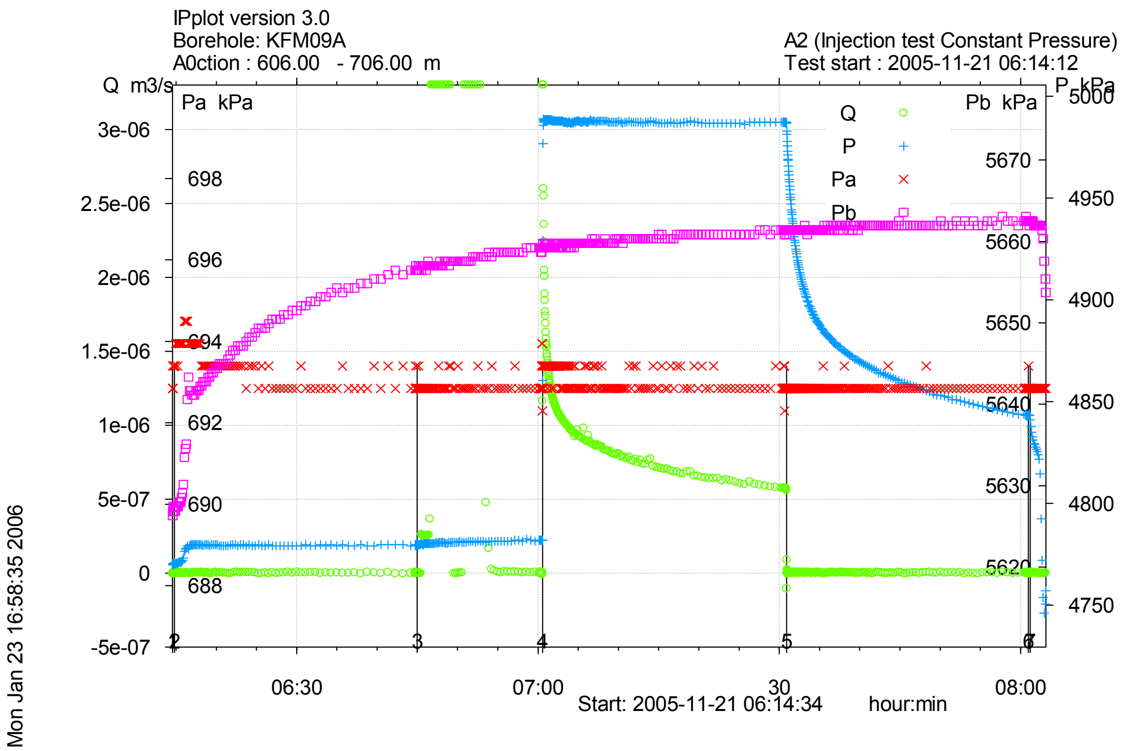


Figure A3-27. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 606.0-706.0 m in borehole KFM09A.*

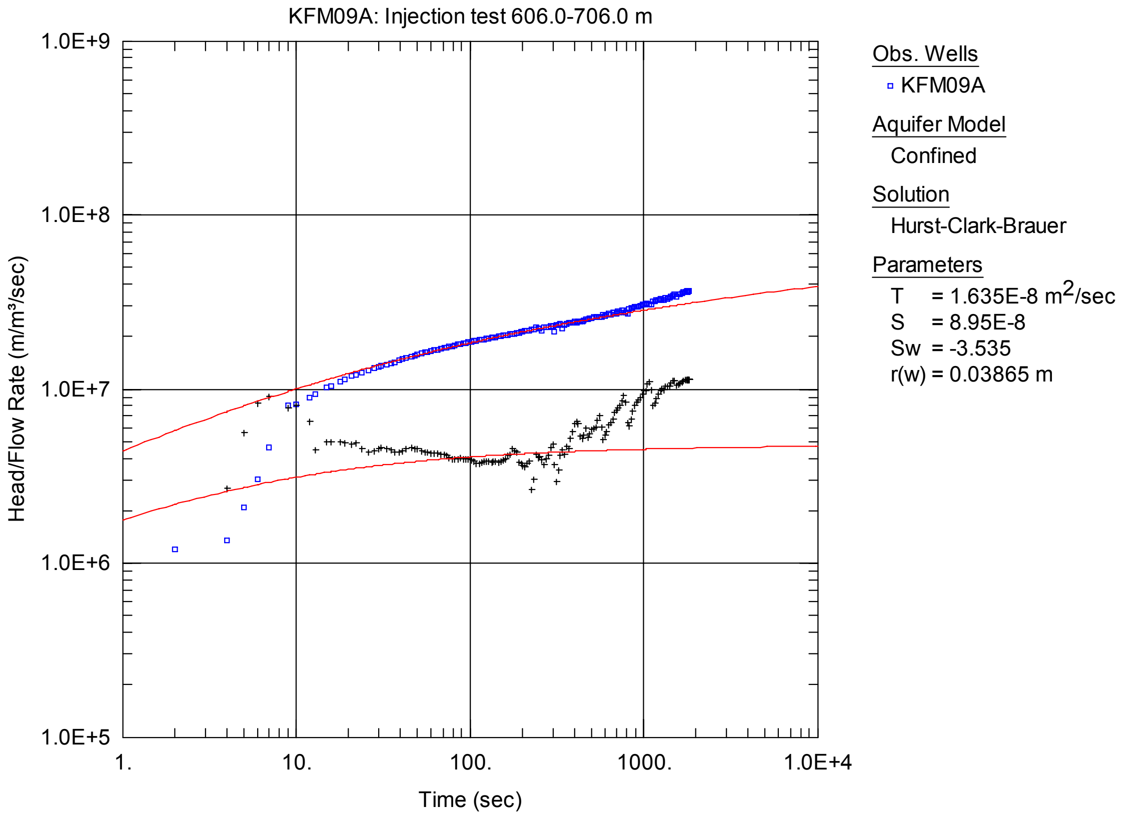


Figure A3-28. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 606.0-706.0 m in KFM09A.*

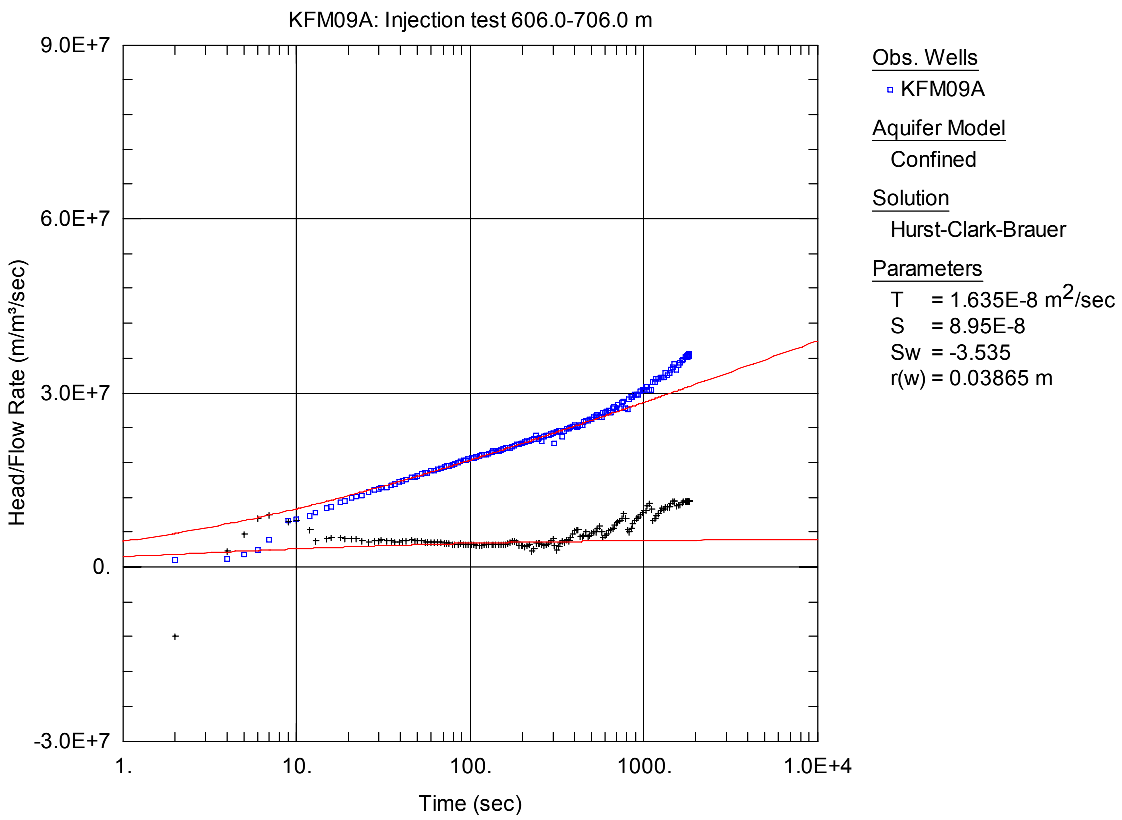


Figure A3-29. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 606.0-706.0 m in KFM09A.*

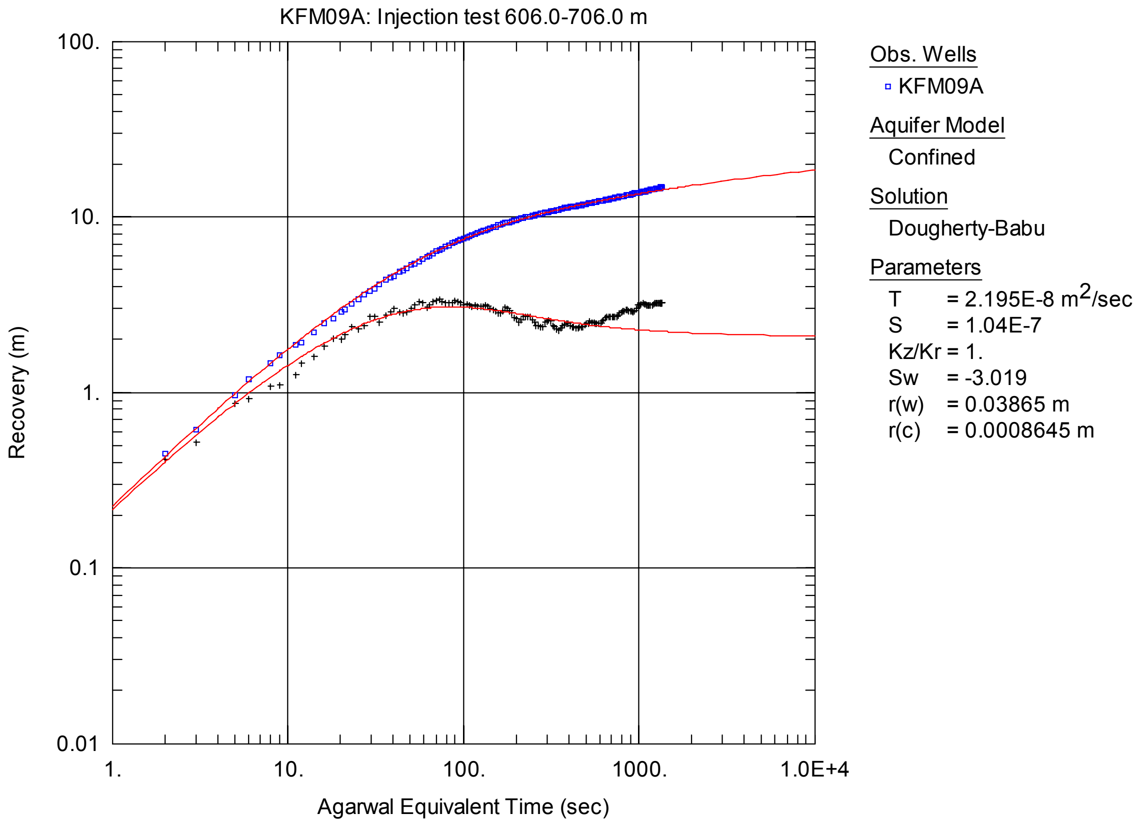


Figure A3-30. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 606.0-706.0 m in KFM09A.*

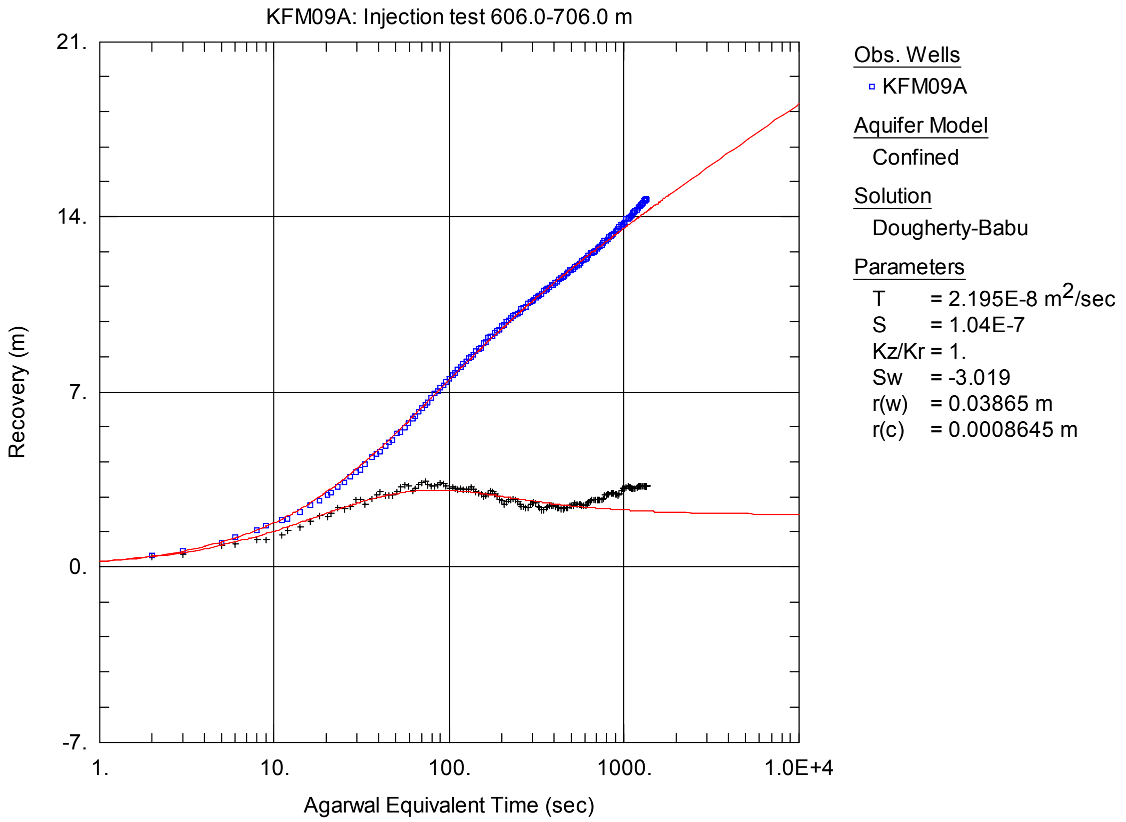


Figure A3-31. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 606.0-706.0 m in KFM09A.*

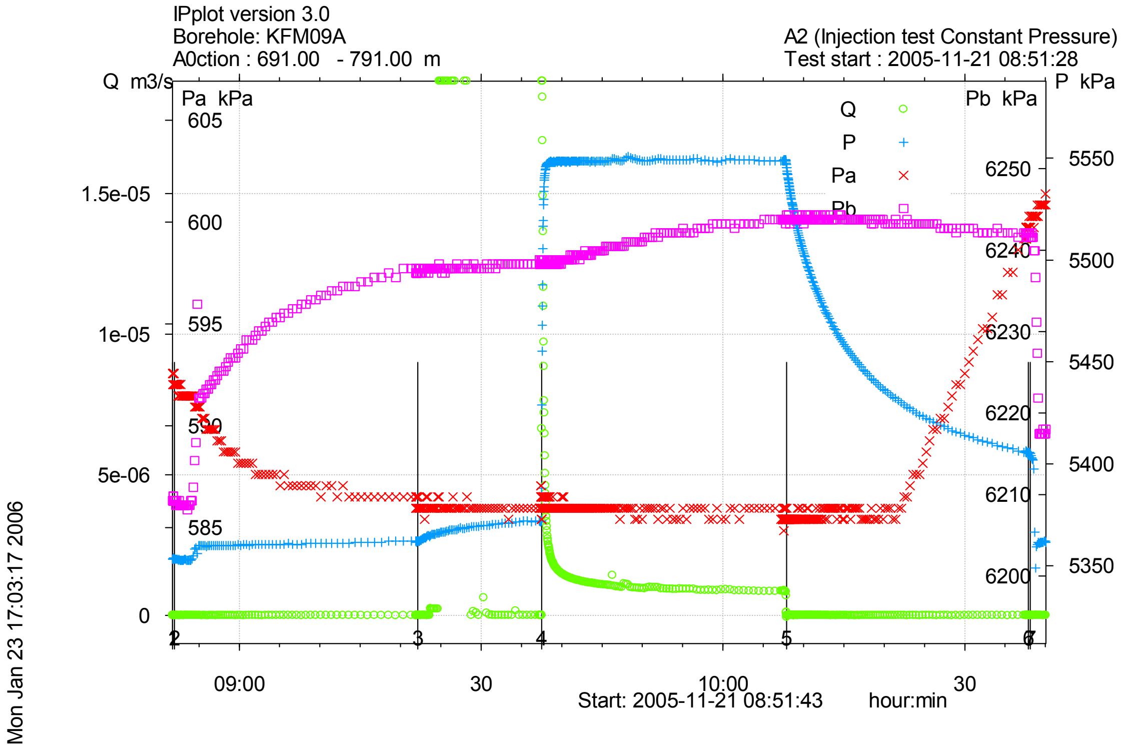


Figure A3-32. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 691.0-791.0 m in borehole KFM09A.

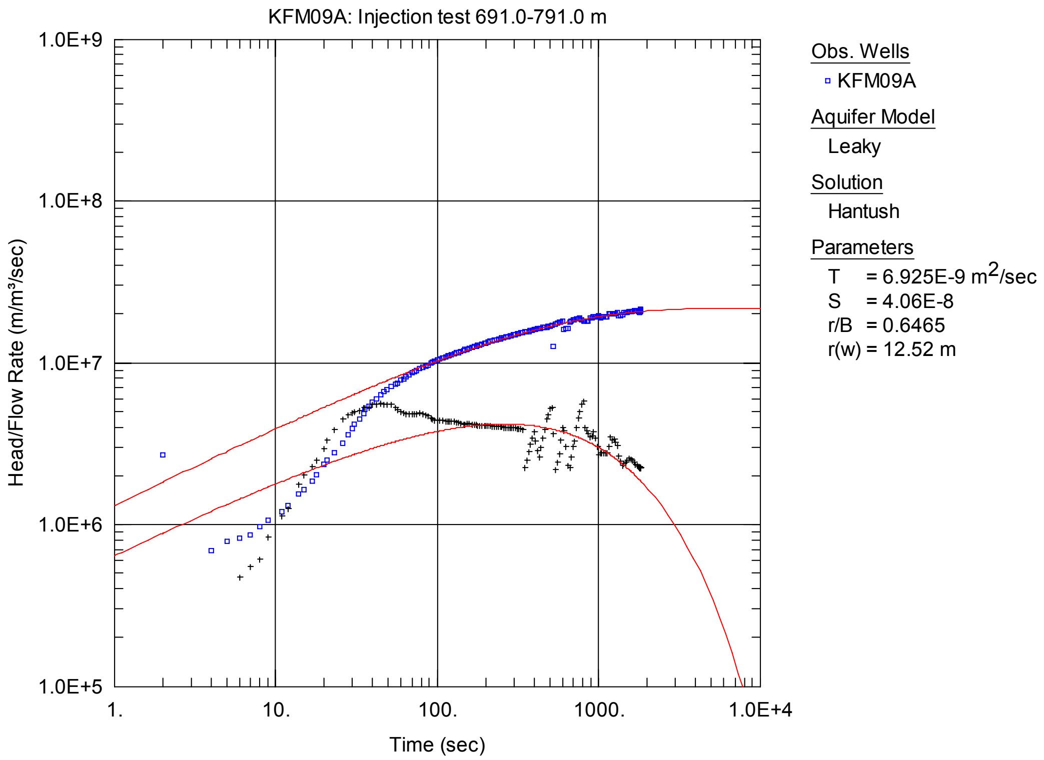


Figure A3-33. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 691.0-791.0 m in KFM09A.

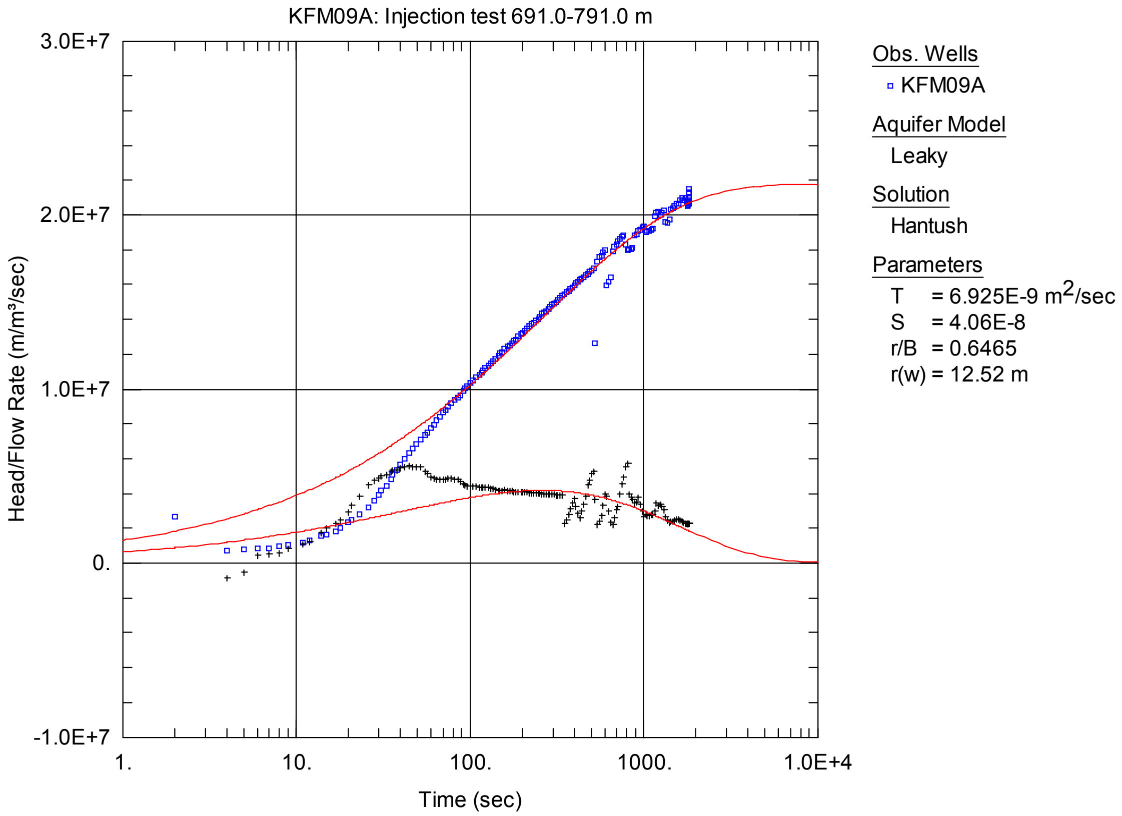


Figure A3-34. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 691.0-791.0 m in KFM09A.*

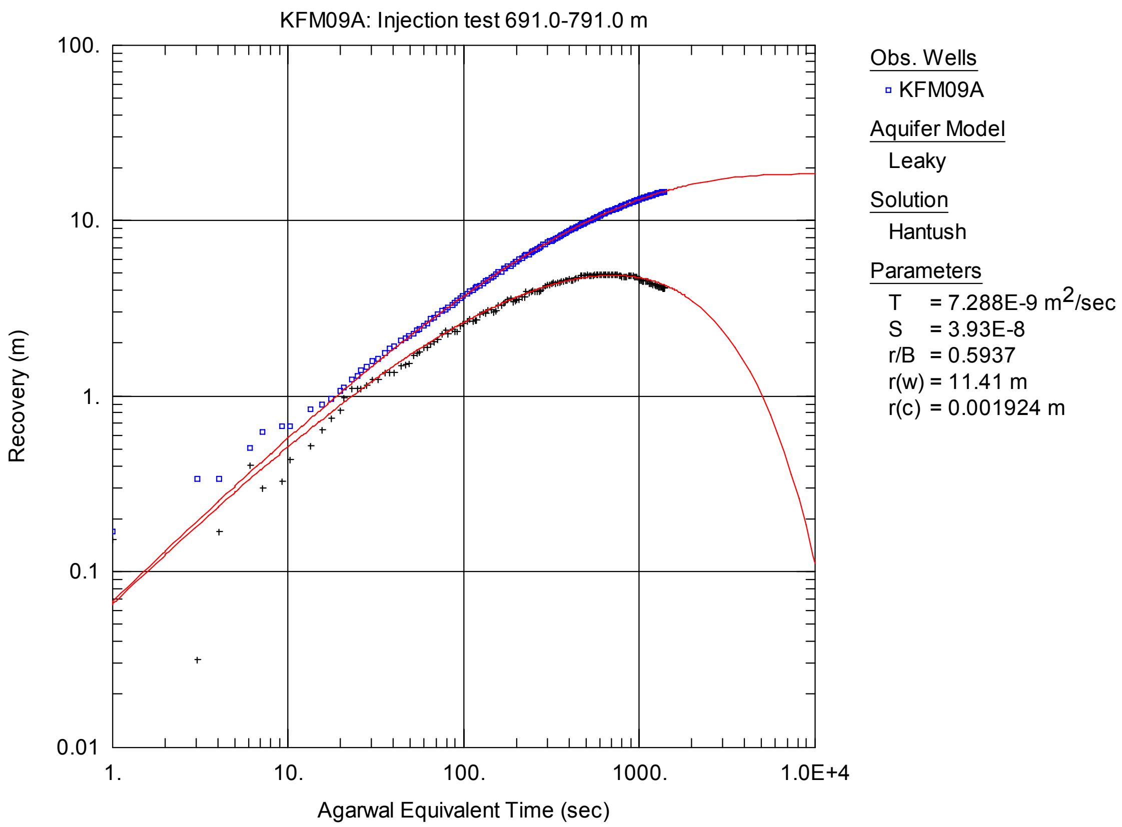


Figure A3-35. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 691.0-791.0 m in KFM09A.*

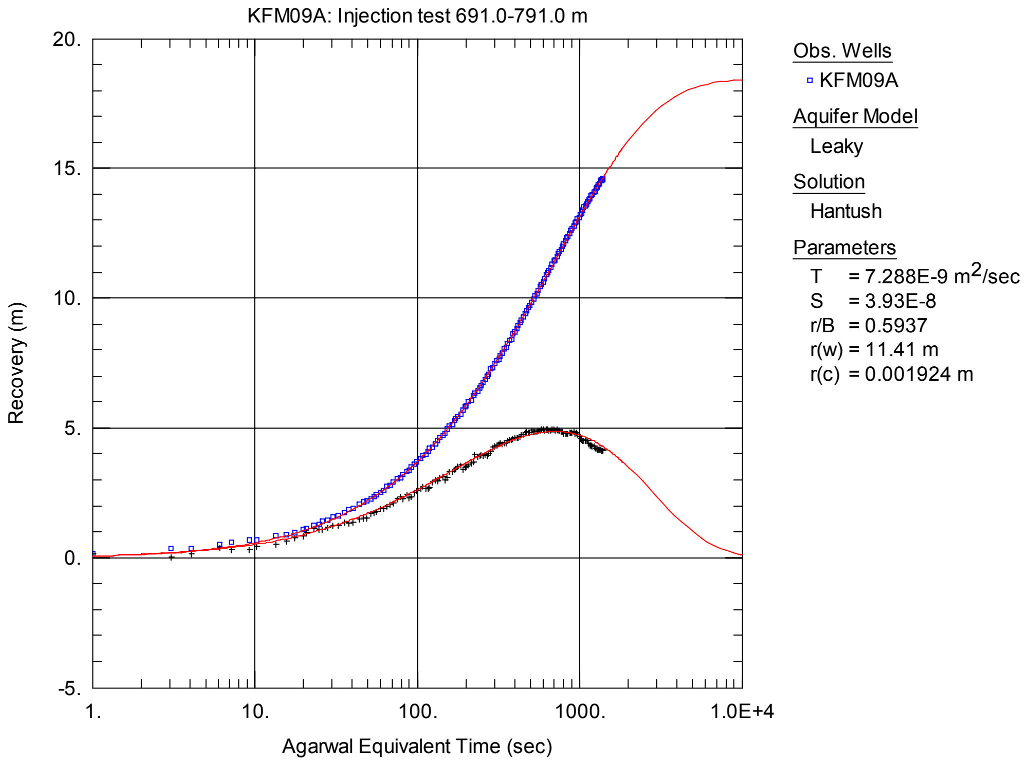


Figure A3-36. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 691.0-791.0 m in KFM09A.*

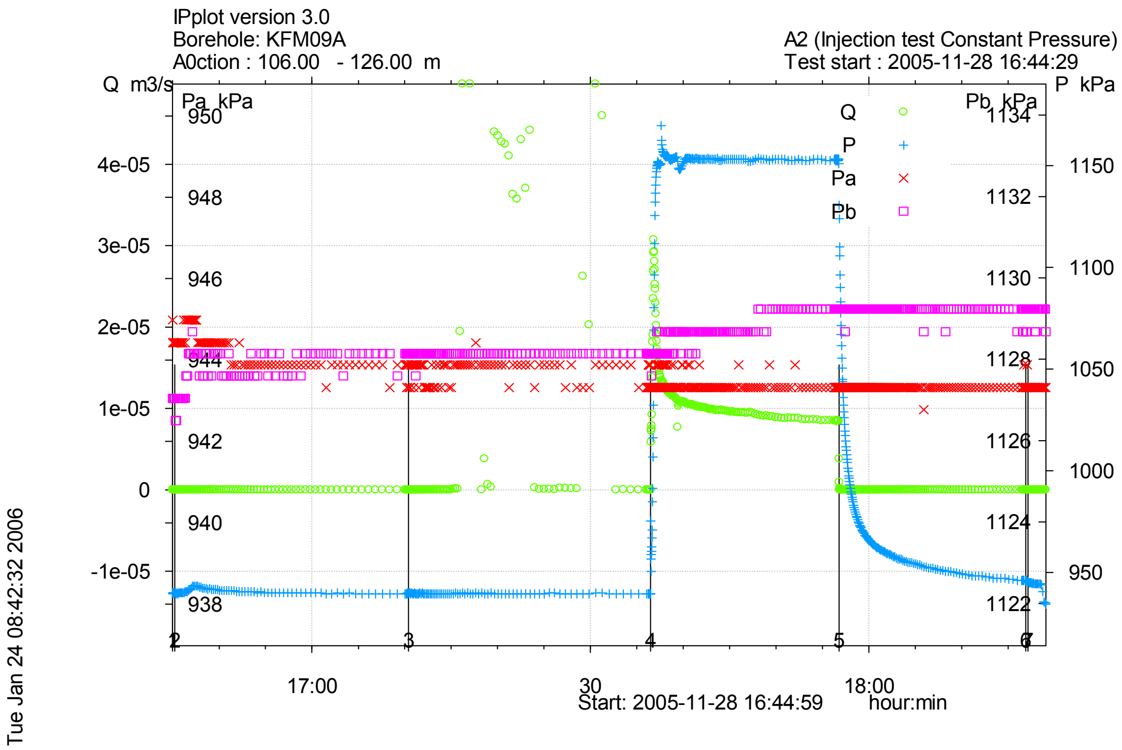


Figure A3-37. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 106.0-126.0 m in borehole KFM09A.*

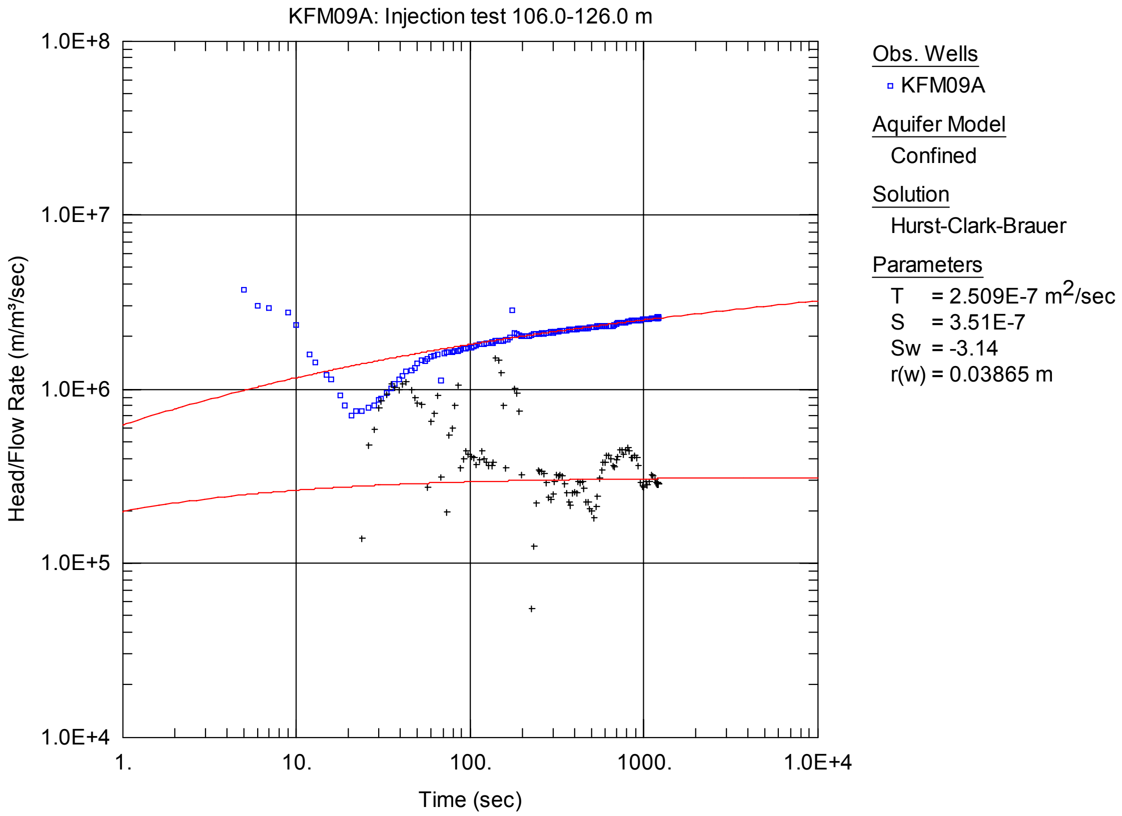


Figure A3-38. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 106.0-126.0 m in KFM09A.*

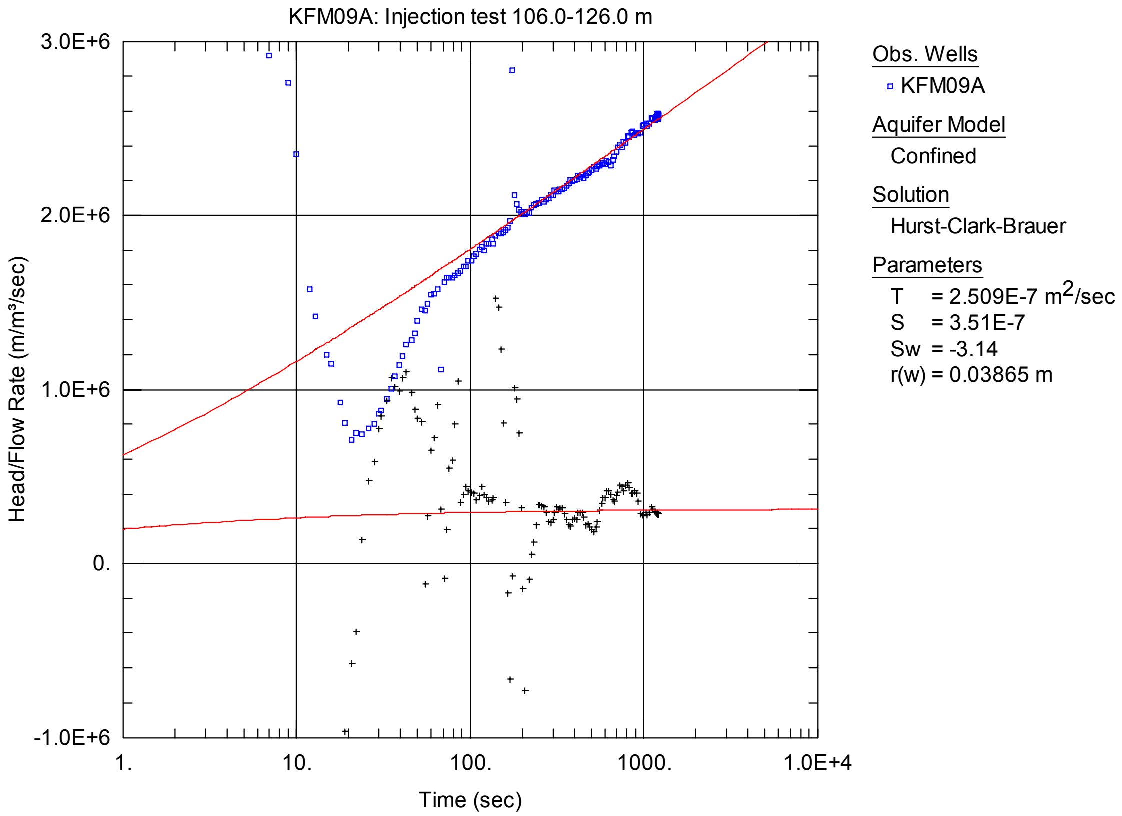


Figure A3-39. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 106.0-126.0 m in KFM09A.*

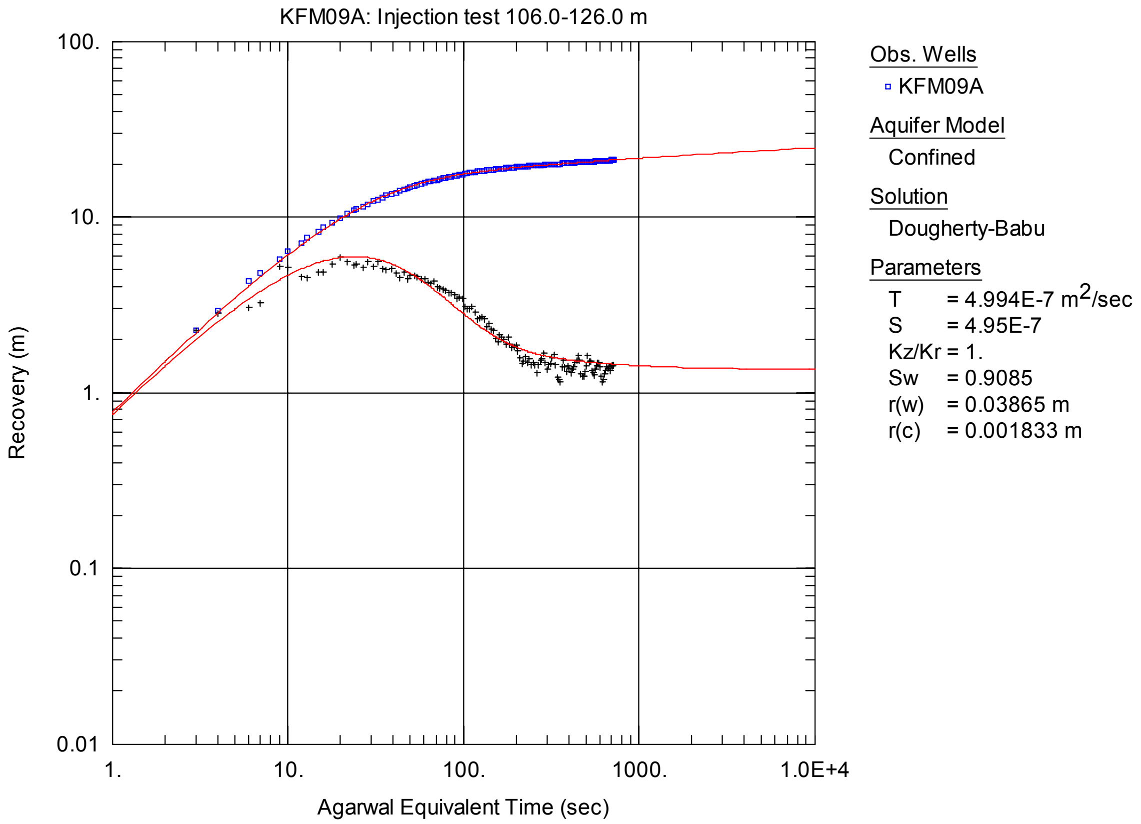


Figure A3-40. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 106.0-126.0 m in KFM09A.*

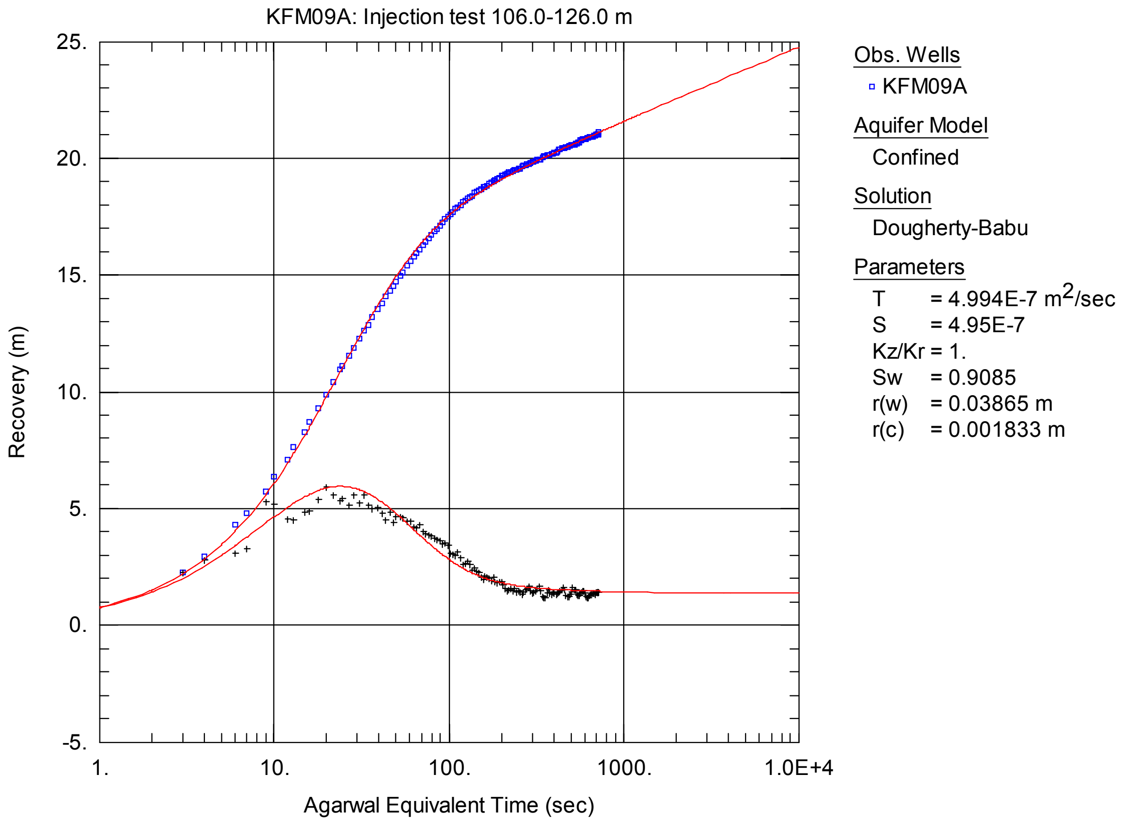


Figure A3-41. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 106.0-126.0 m in KFM09A.*

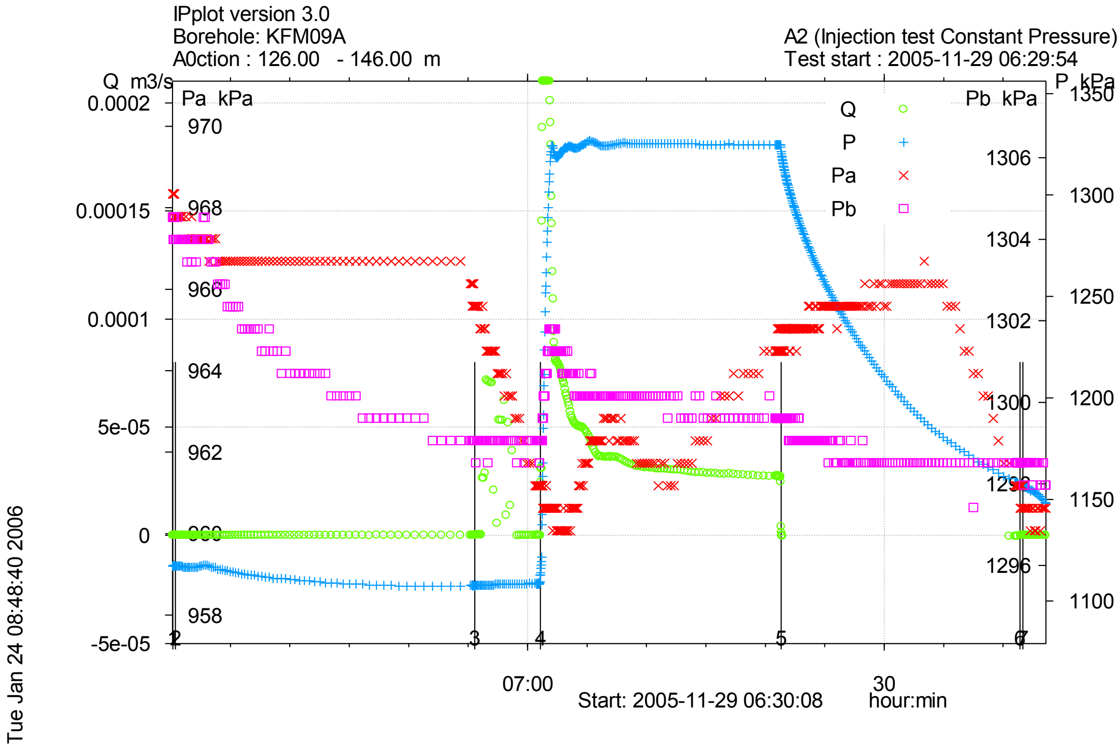


***Figure A3-42.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 126.0-146.0 m in borehole KFM09A.*

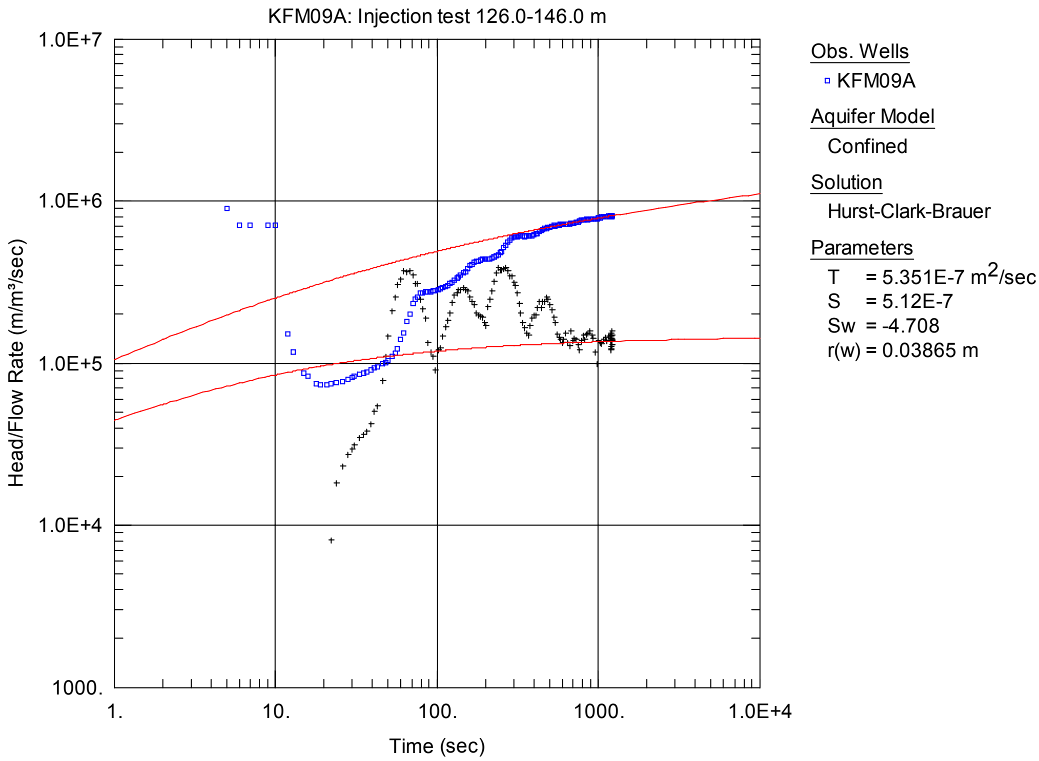


***Figure A3-43.** Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 126.0-146.0 m in KFM09A.*

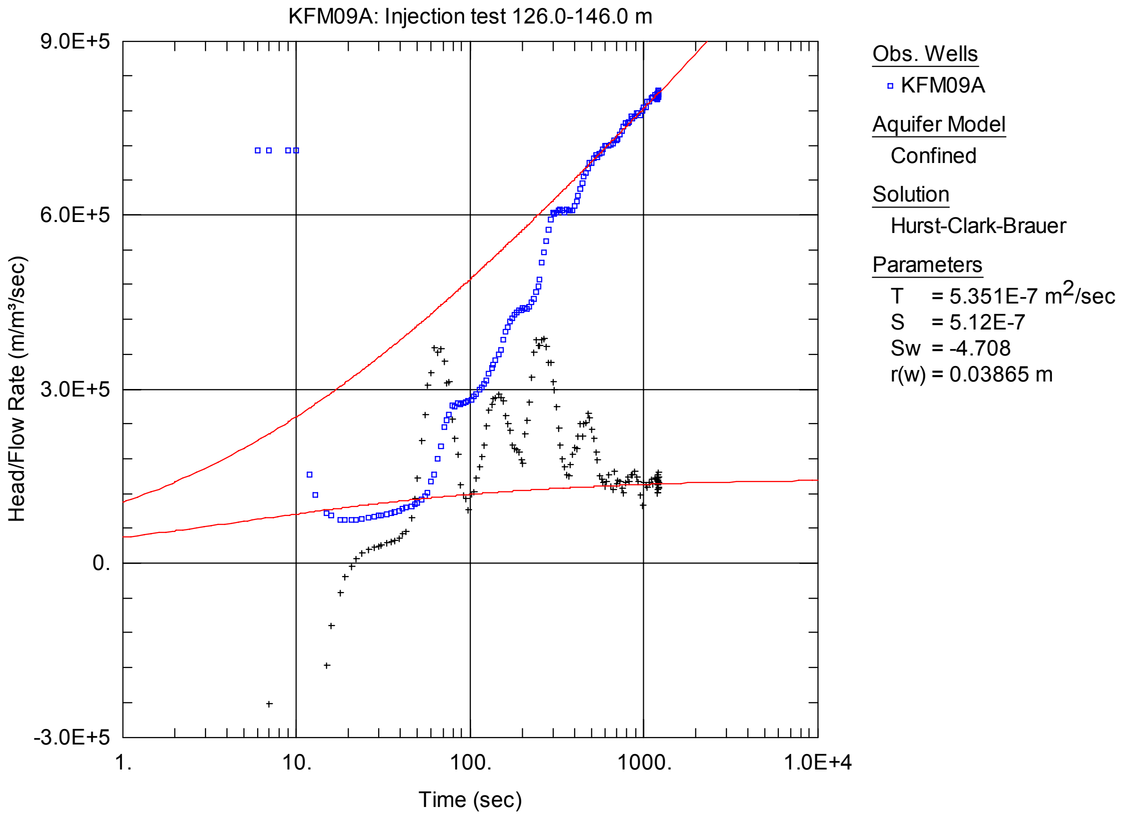


Figure A3-44. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 126.0-146.0 m in KFM09A.*

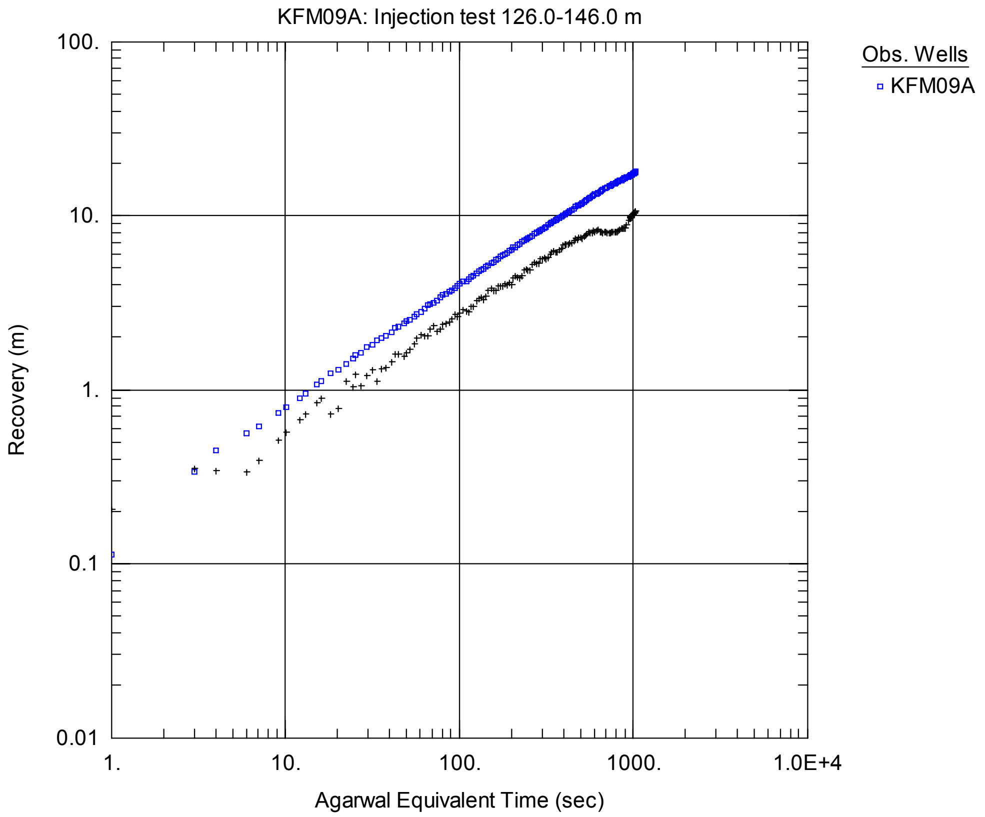


Figure A3-45. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 126.0-146.0 m in KFM09A.*

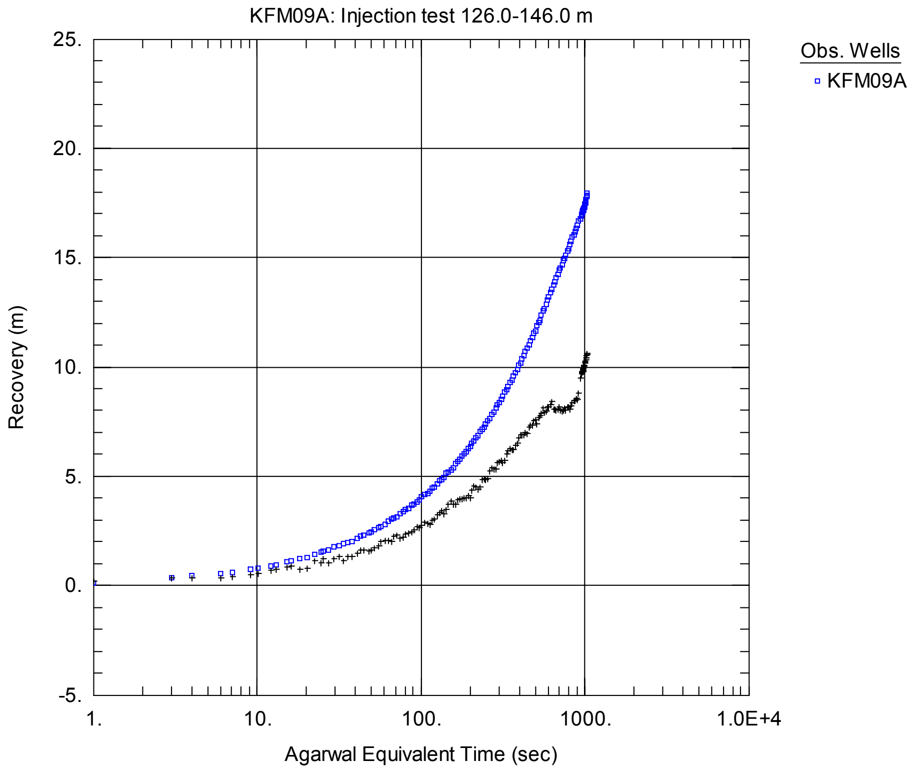


Figure A3-46. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 126.0-146.0 m in KFM09A.*

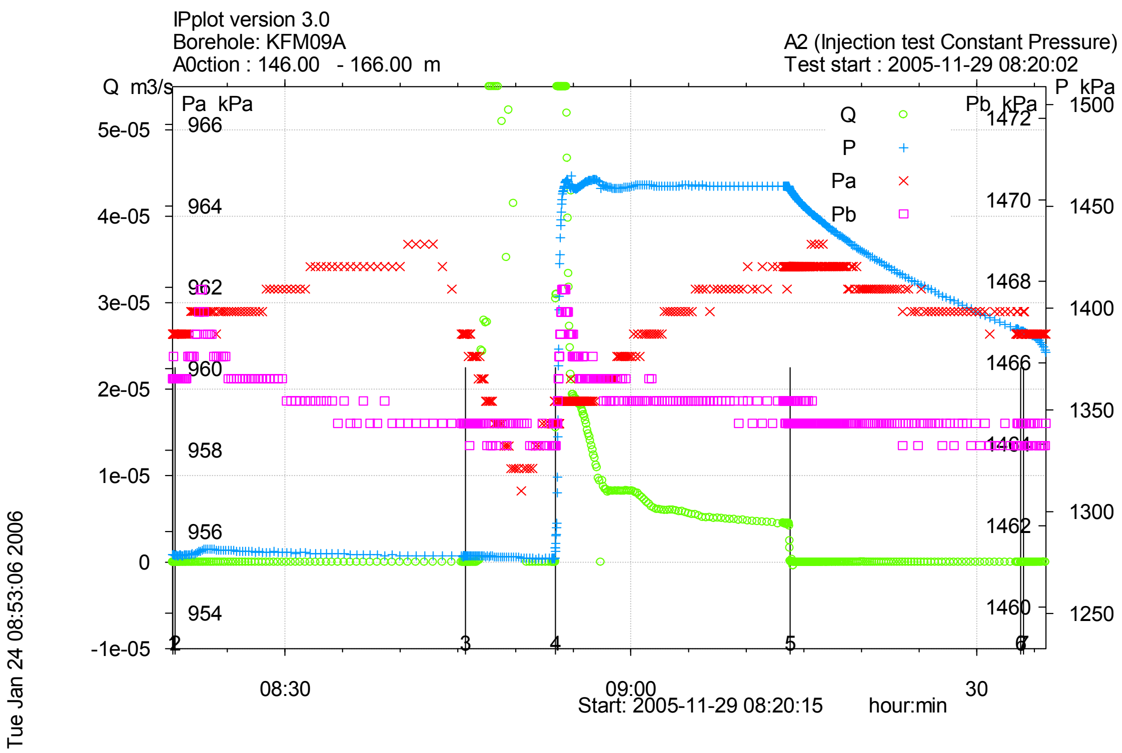


Figure A3-47. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 146.0-166.0 m in borehole KFM09A.*

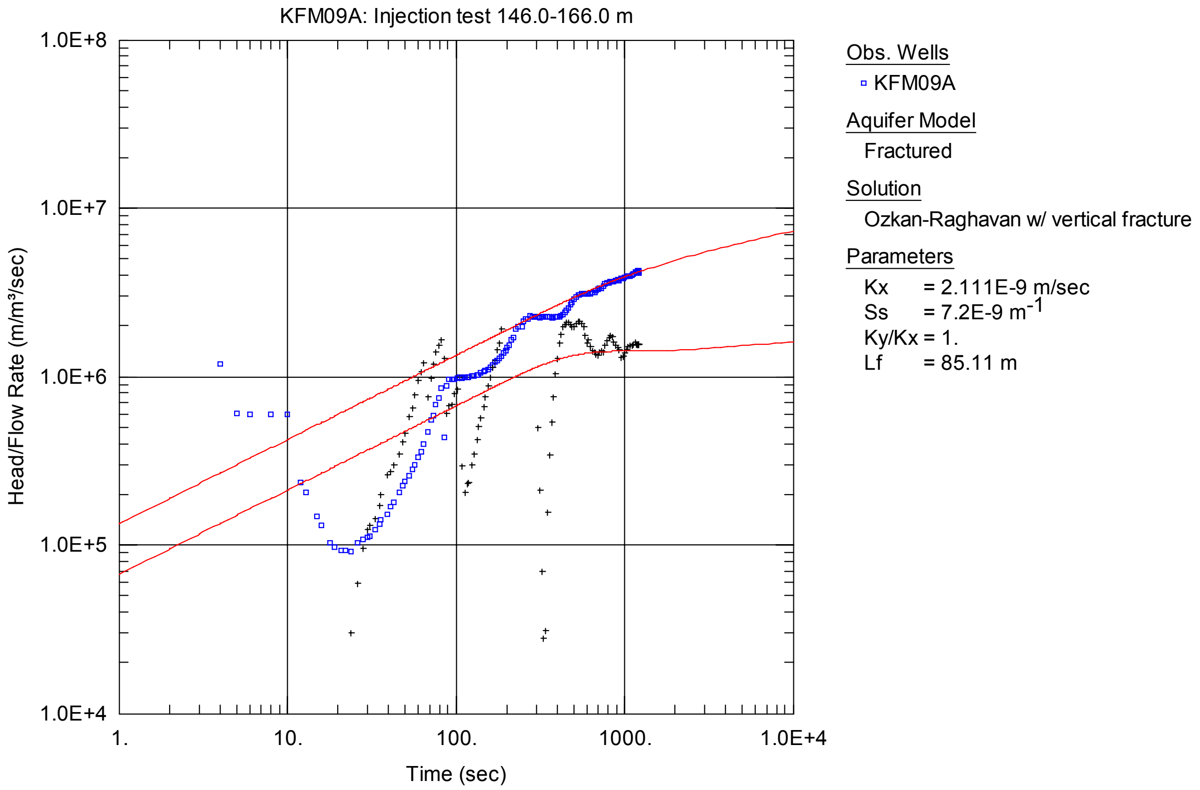


Figure A3-48. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 146.0-166.0 m in KFM09A.*

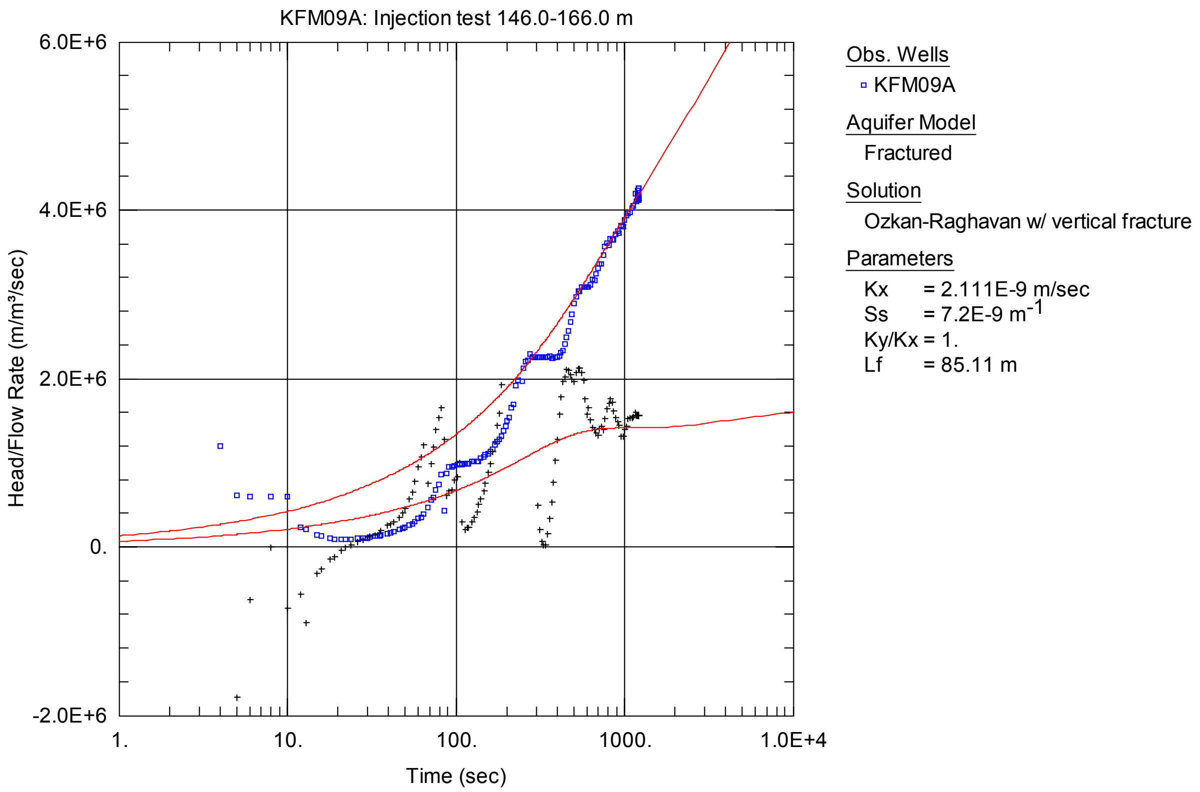


Figure A3-49. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 146.0-166.0 m in KFM09A.*

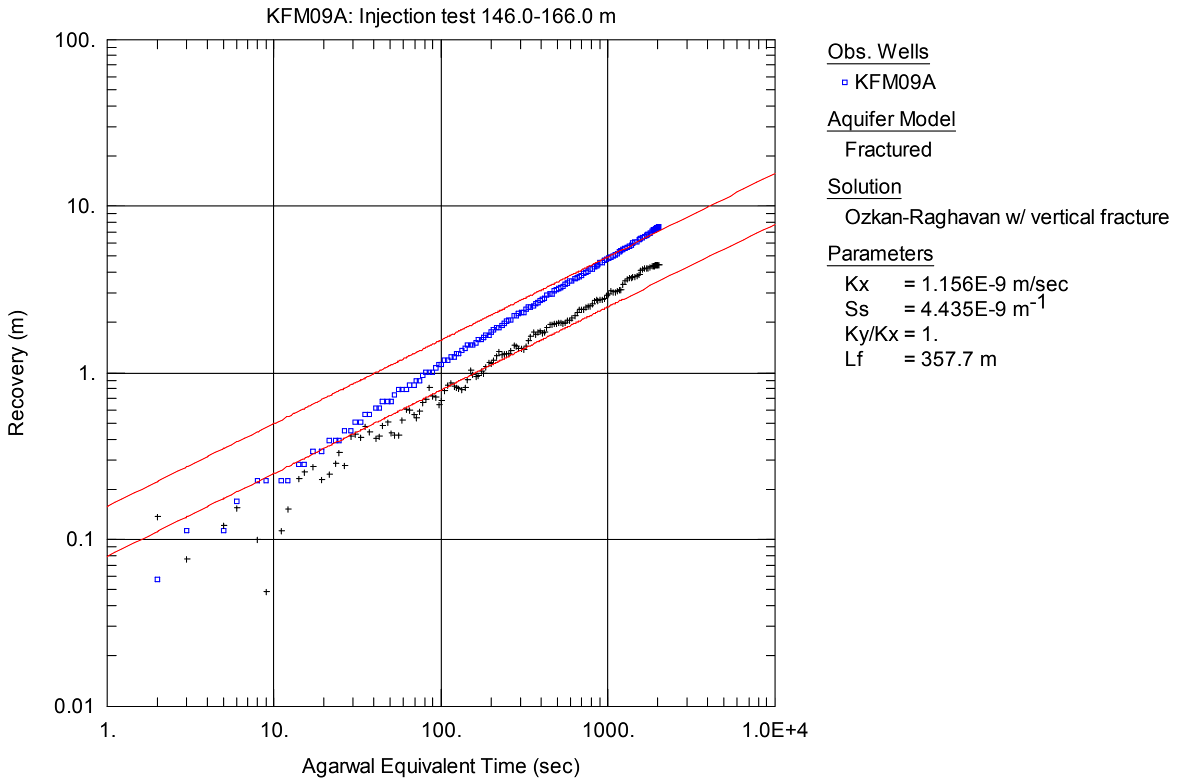


Figure A3-50. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 146.0-166.0 m in KFM09A. No unambiguous transient evaluation of transmissivity on this period is possible.*

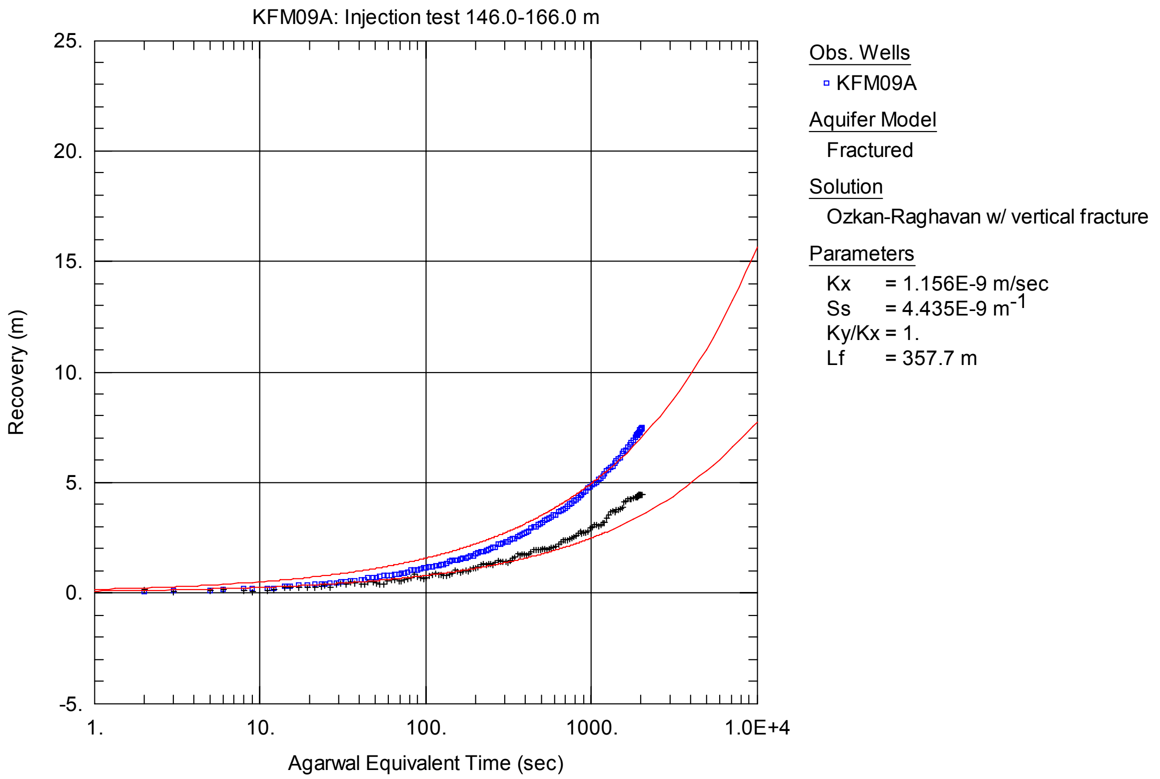


Figure A3-51. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 146.0-166.0 m in KFM09A. No unambiguous transient evaluation of transmissivity on this period is possible.*

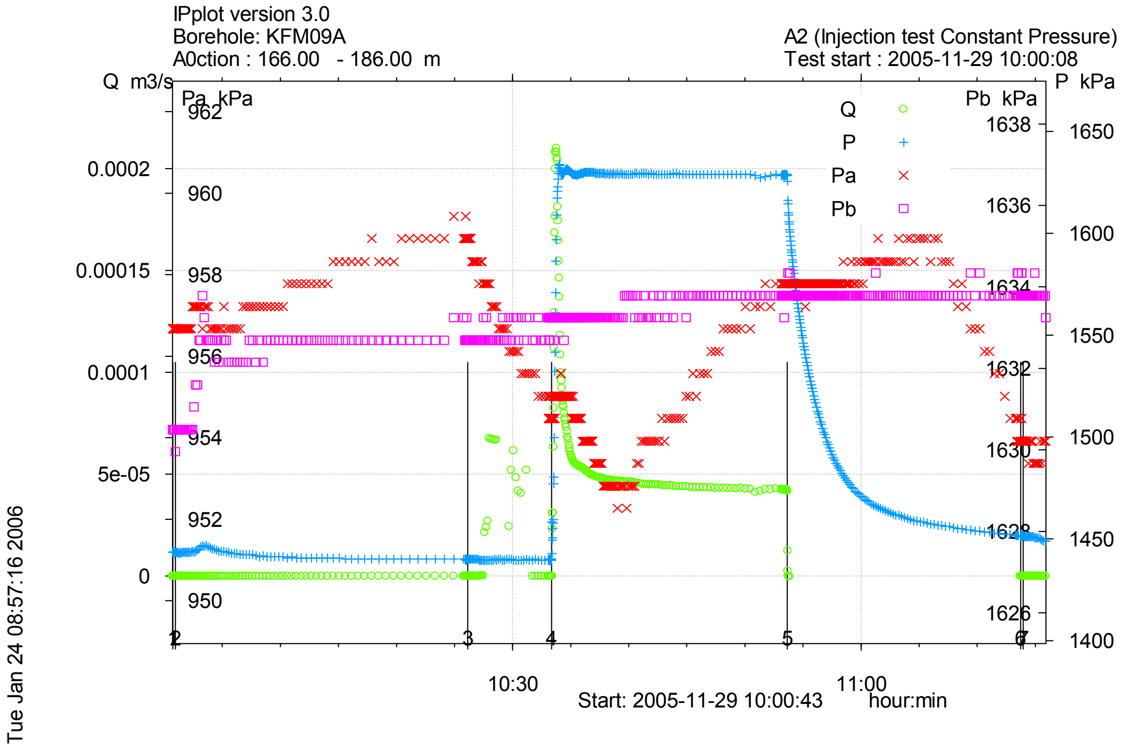


Figure A3-52. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 166.0-186.0 m in borehole KFM09A.*

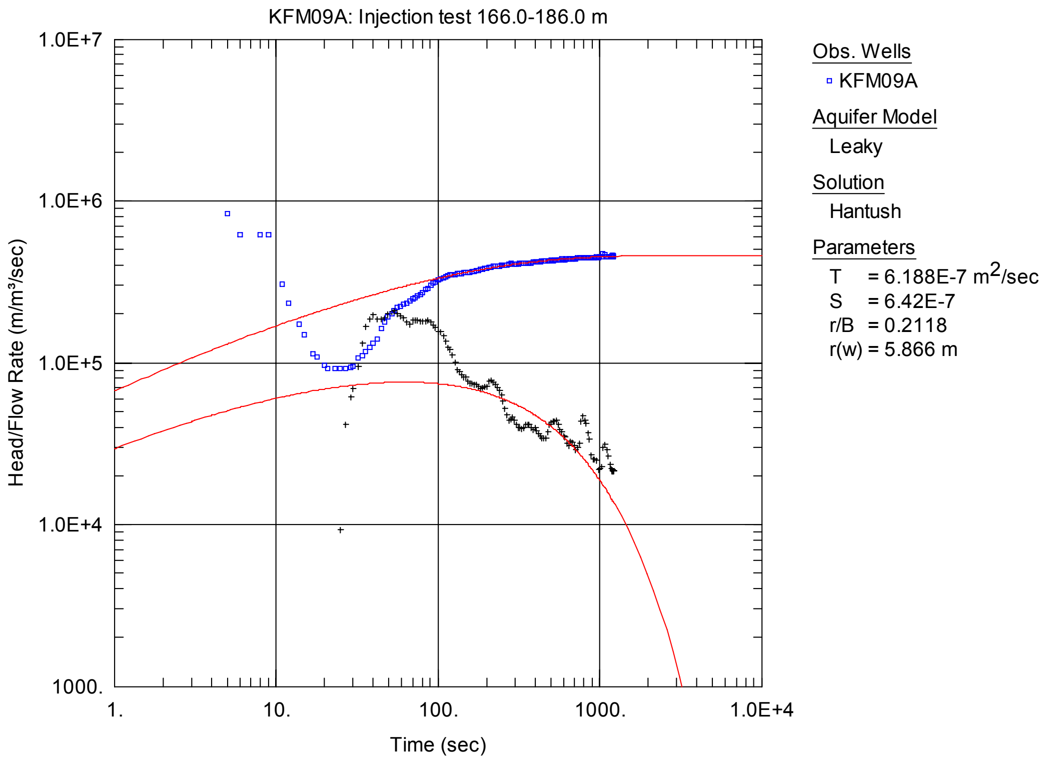


Figure A3-53. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 166.0-186.0 m in KFM09A.*

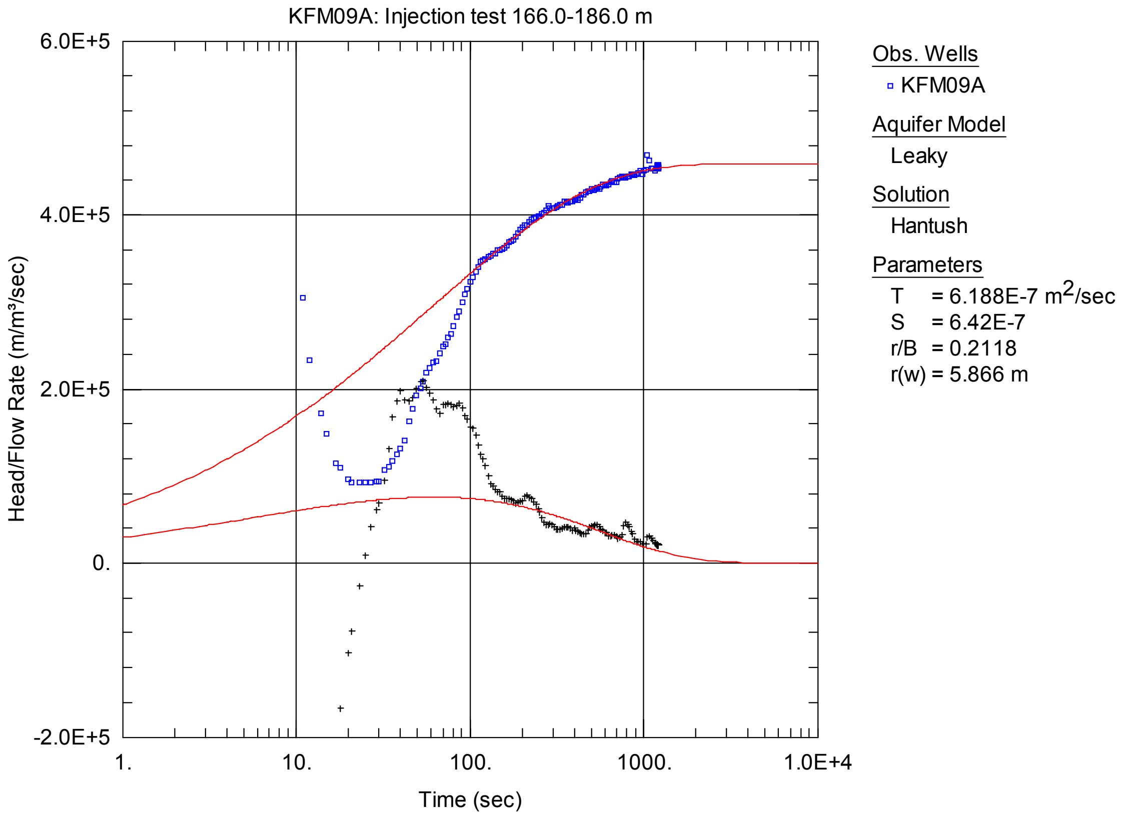


Figure A3-54. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 166.0-186.0 m in KFM09A.*

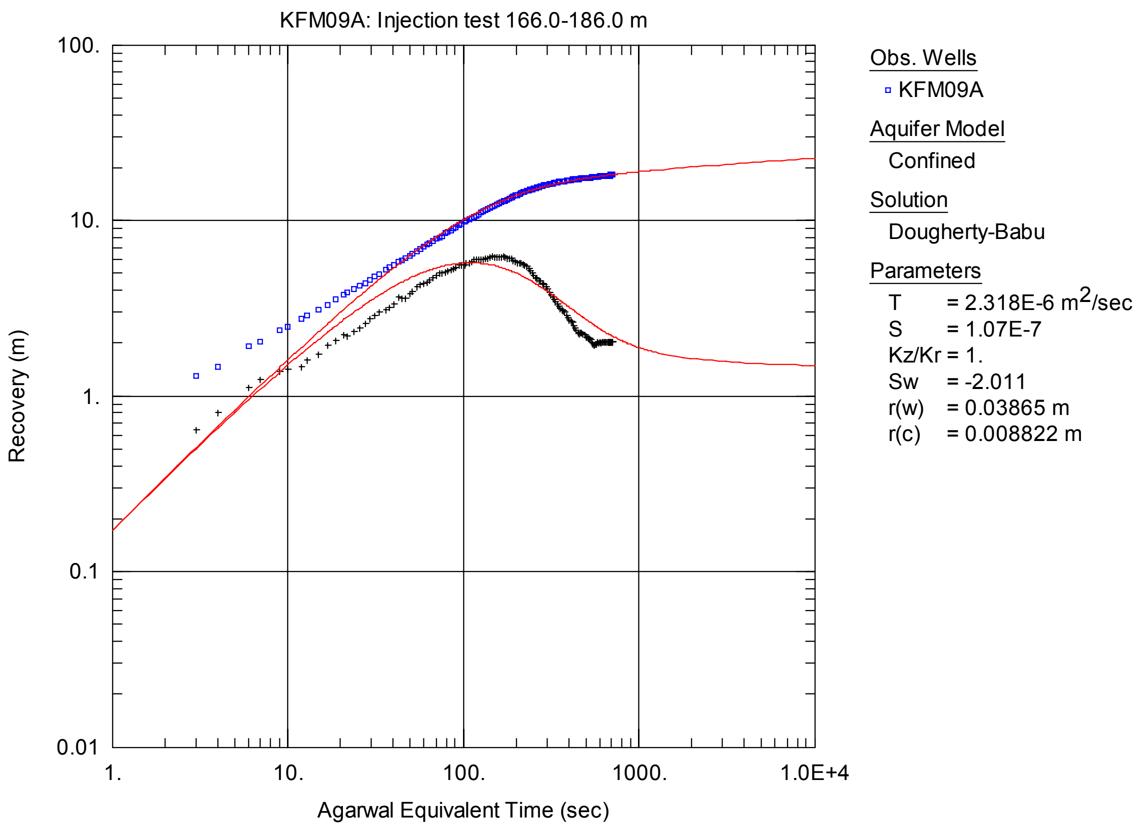


Figure A3-55. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 166.0-186.0 m in KFM09A.*

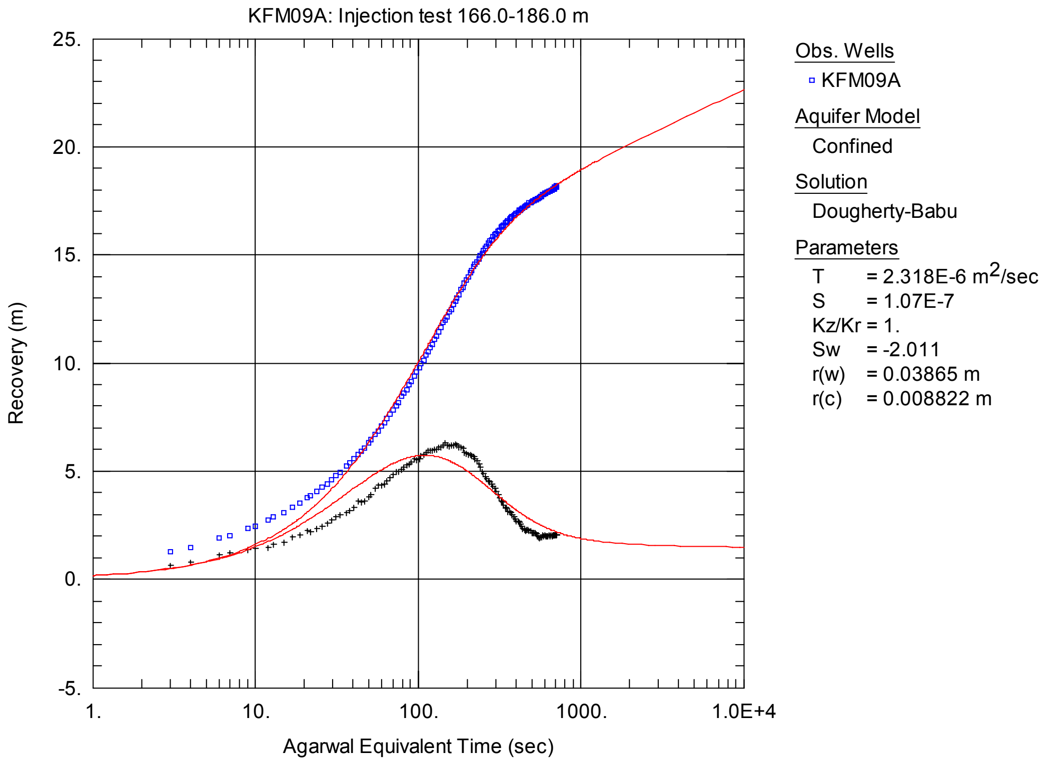


Figure A3-56. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 166.0-186.0 m in KFM09A.*

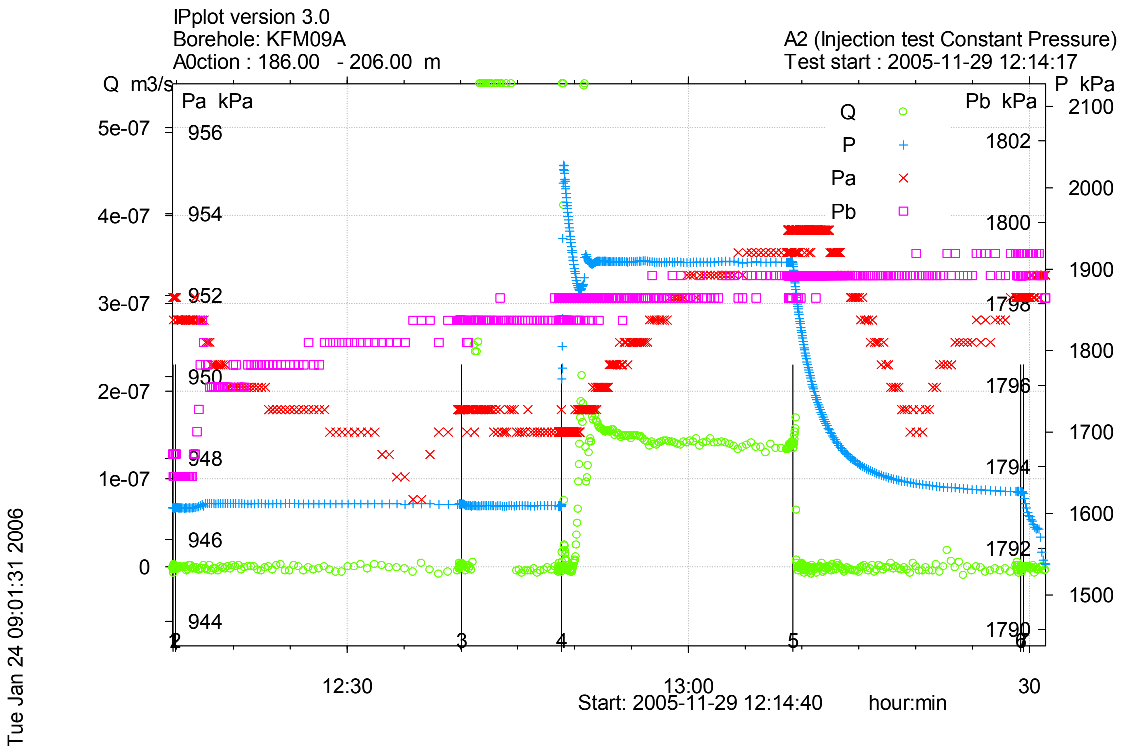


Figure A3-57. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 186.0-206.0 m in borehole KFM09A.*

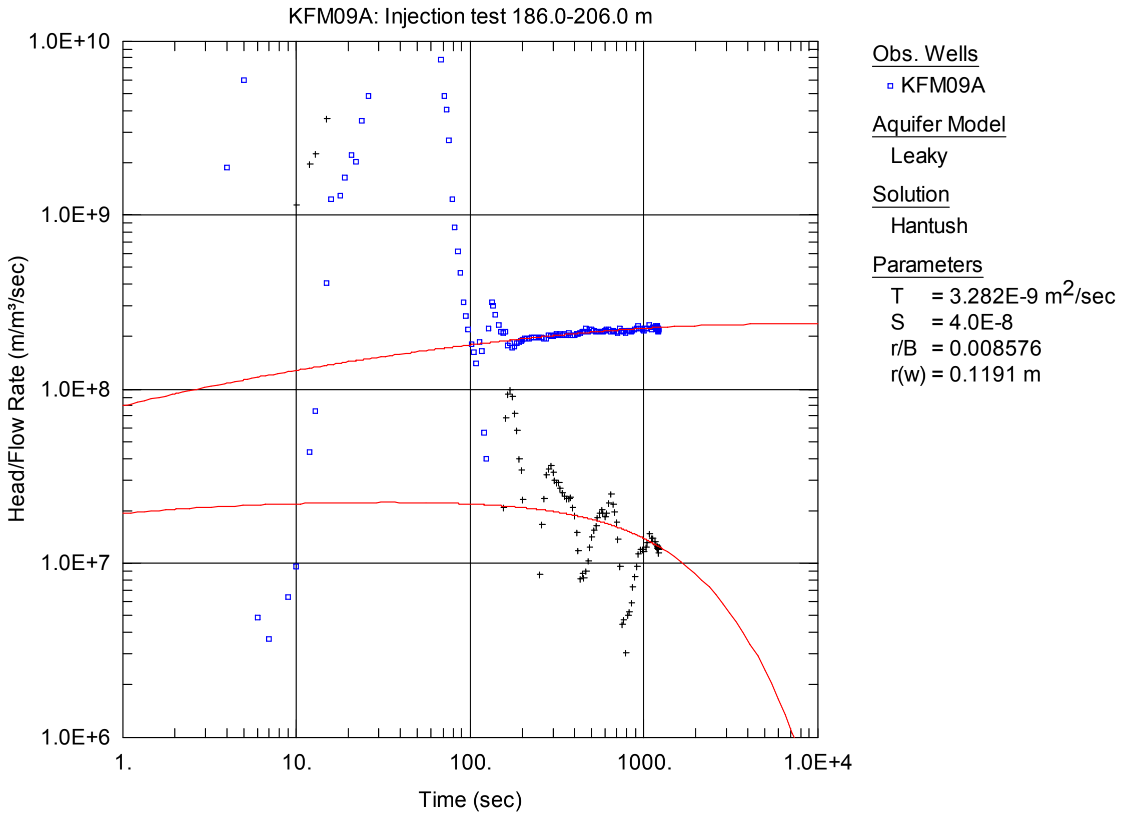


Figure A3-58. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 186.0-206.0 m in KFM09A.*

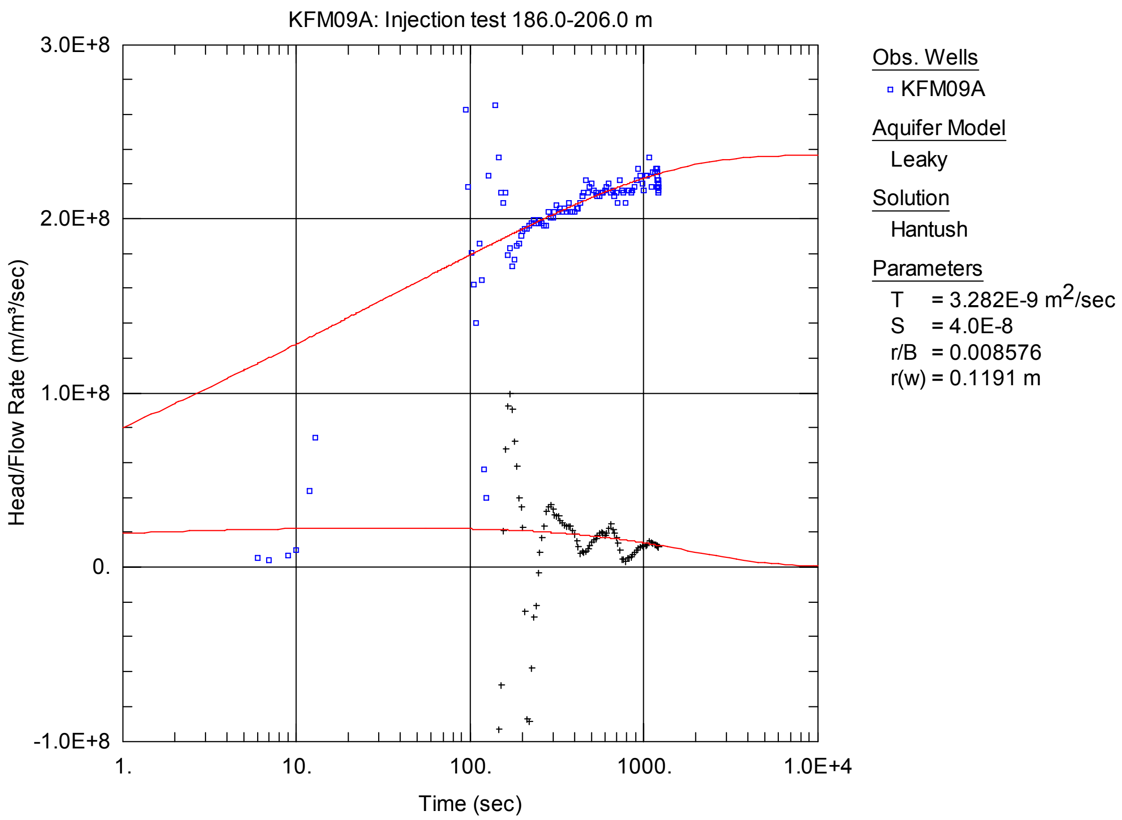


Figure A3-59. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 186.0-206.0 m in KFM09A.*

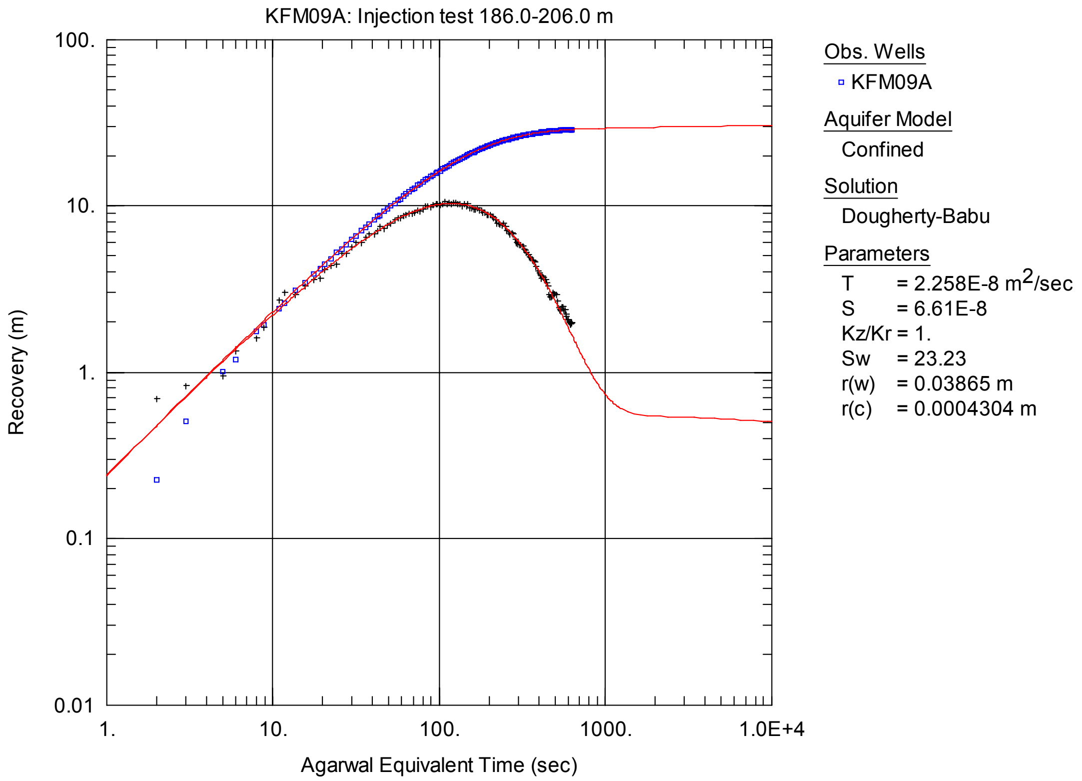


Figure A3-60. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 186.0-206.0 m in KFM09A. The transient evaluation on the recovery period is not regarded as representative.*

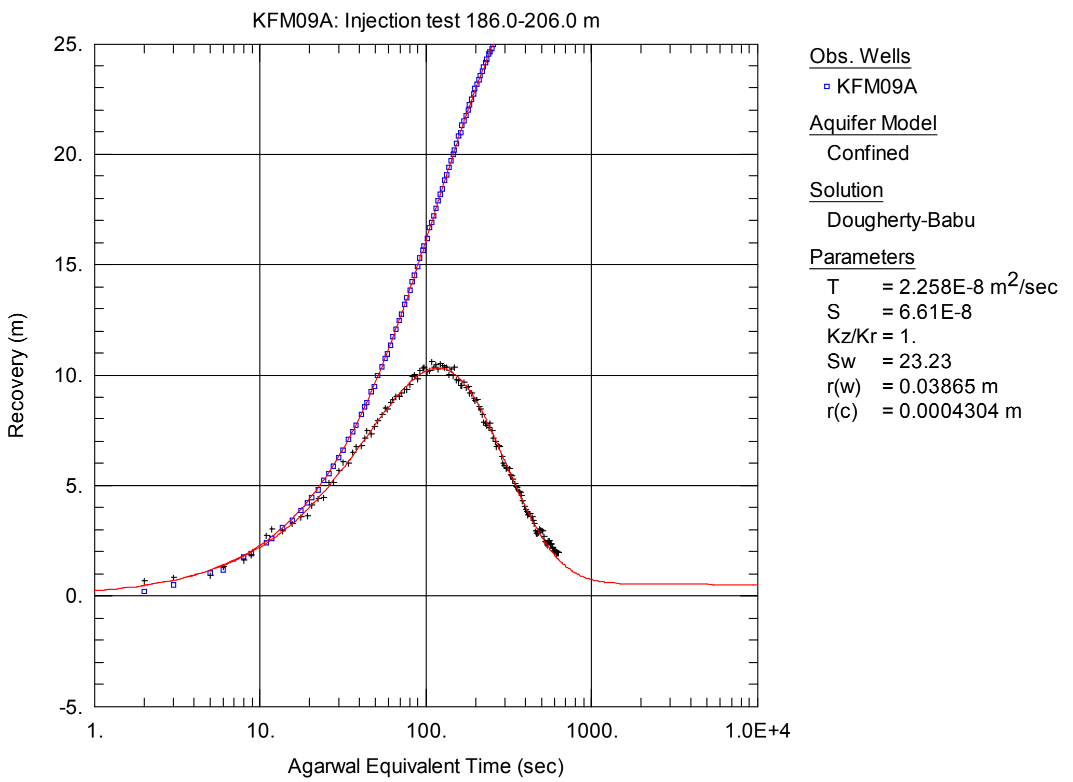


Figure A3-61. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in 186.0-206.0 m in KFM09A. The transient evaluation on the recovery period is not regarded as representative.*

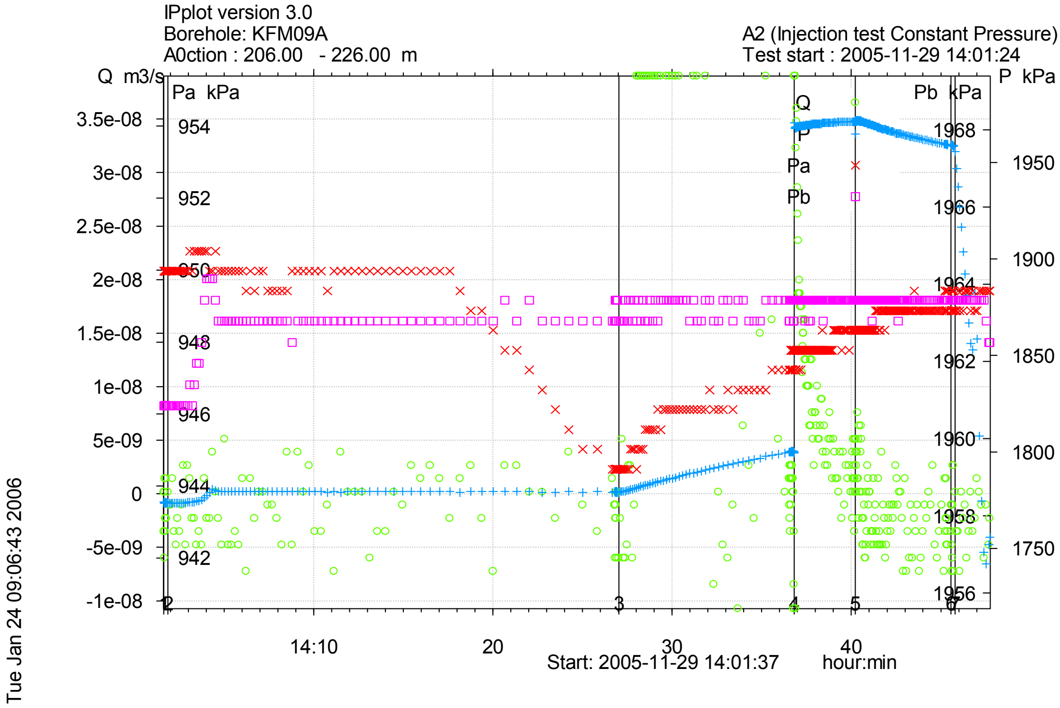


Figure A3-62. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 206.0-226.0 m in borehole KFM09A.*

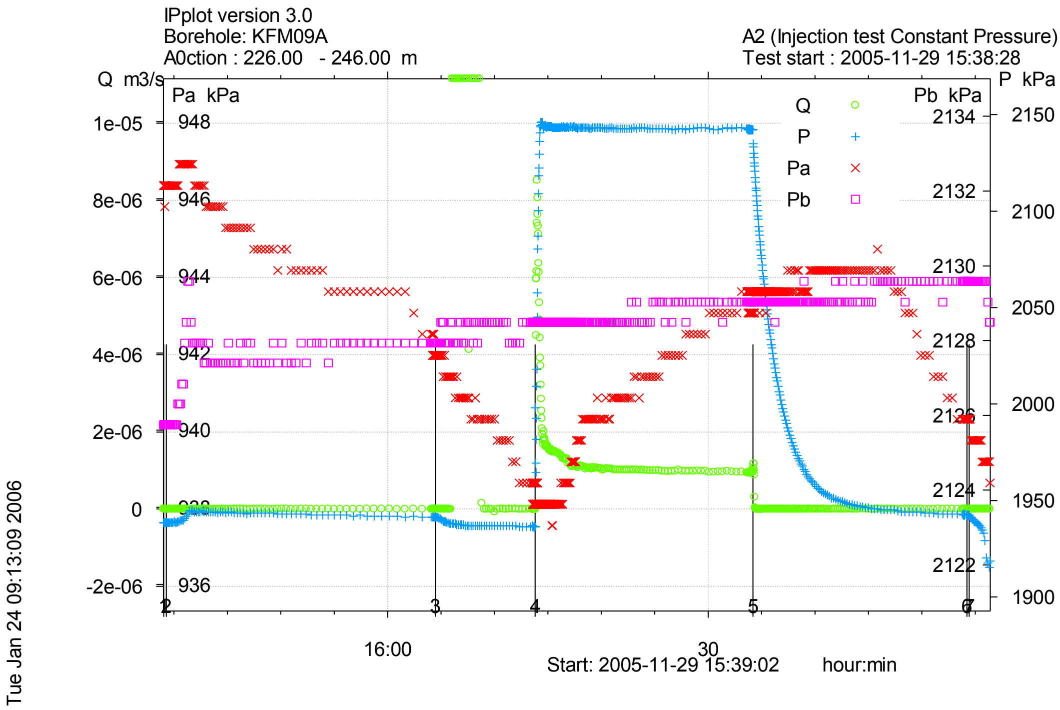


Figure A3-63. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 226.0-246.0 m in borehole KFM09A.*

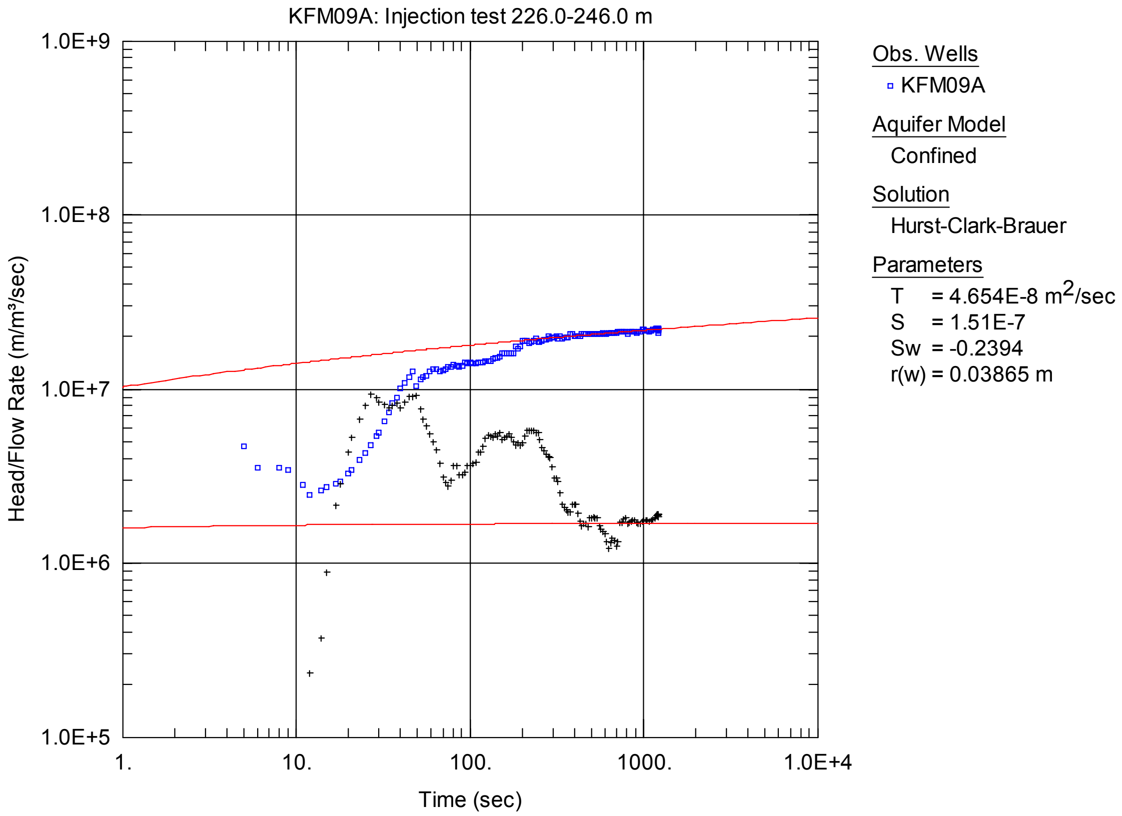


Figure A3-64. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 226.0-246.0 m in KFM09A.*

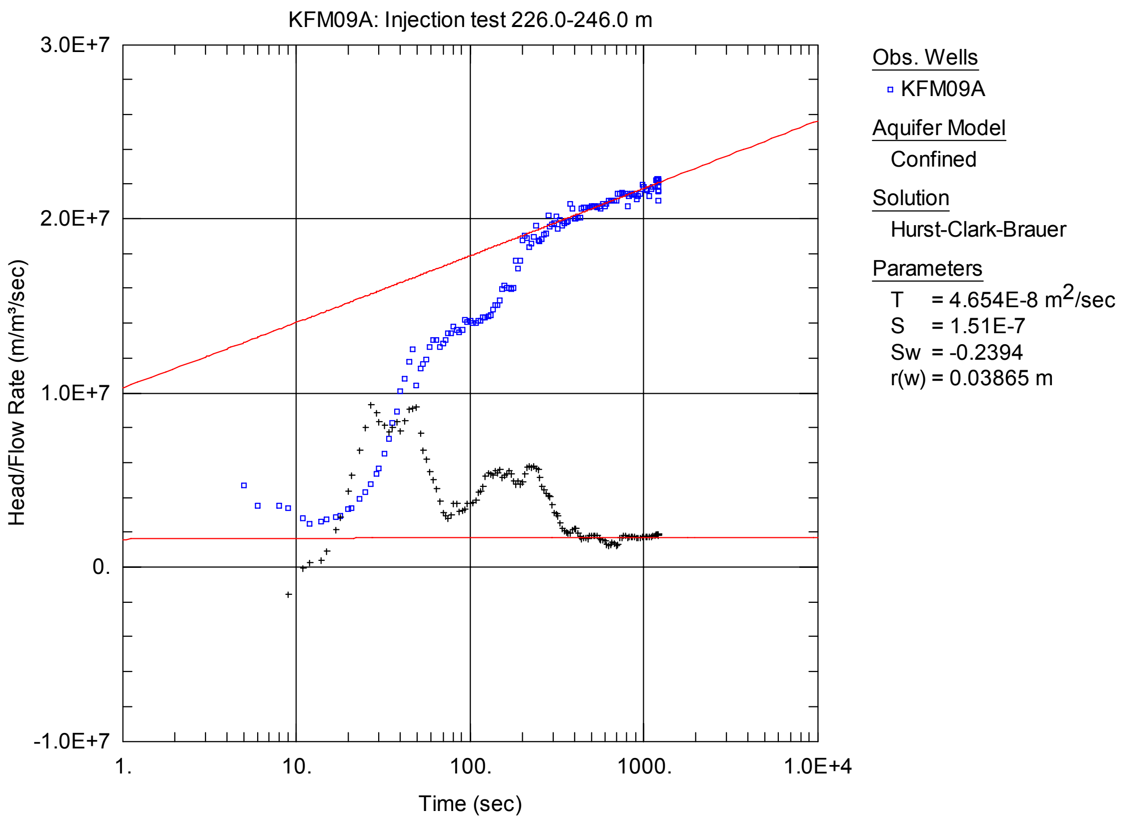


Figure A3-65. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 226.0-246.0 m in KFM09A.*

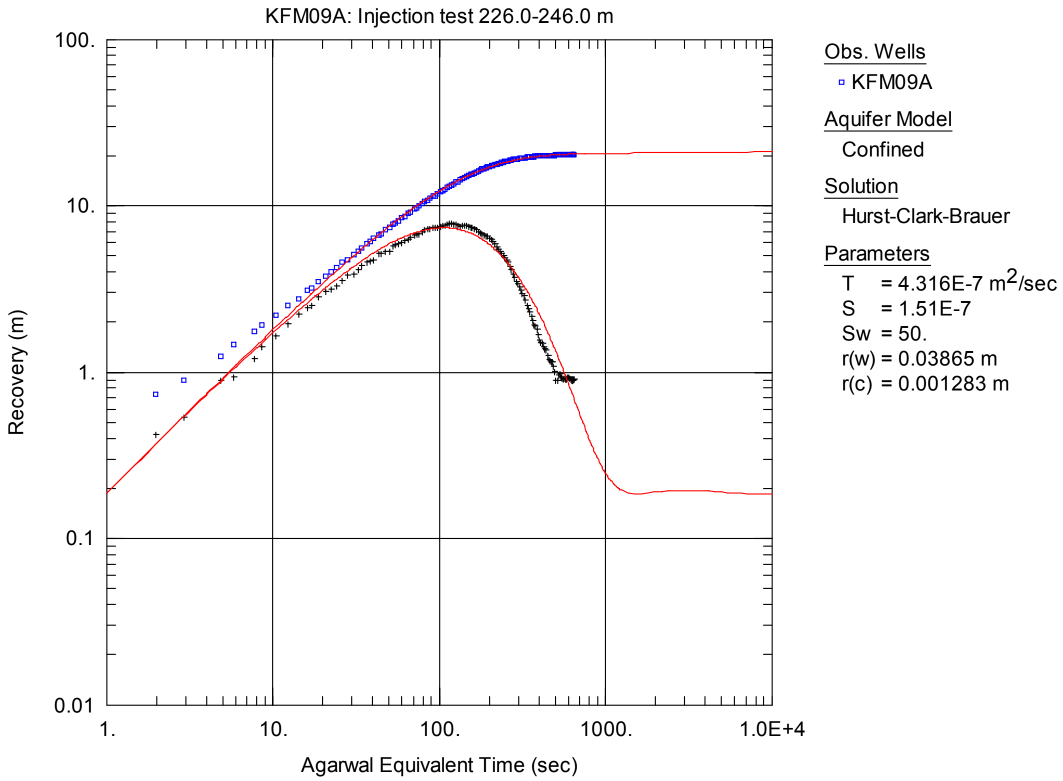


Figure A3-66. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in 226.0-246.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.*

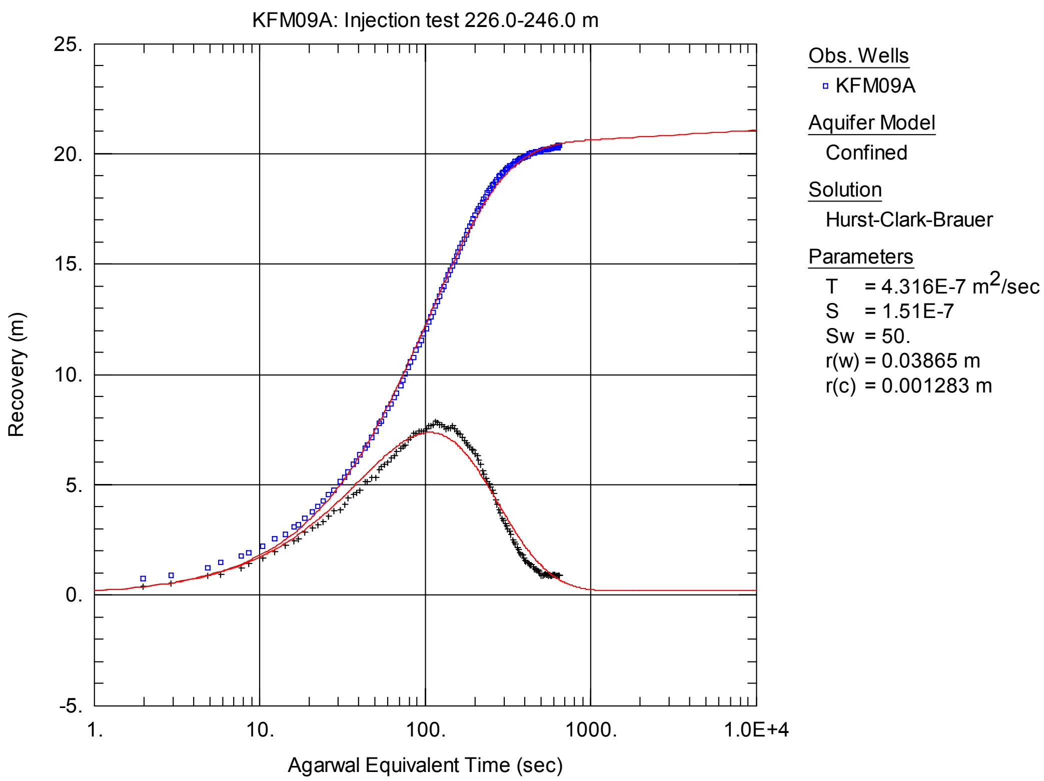


Figure A3-67. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 226.0-246.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period*

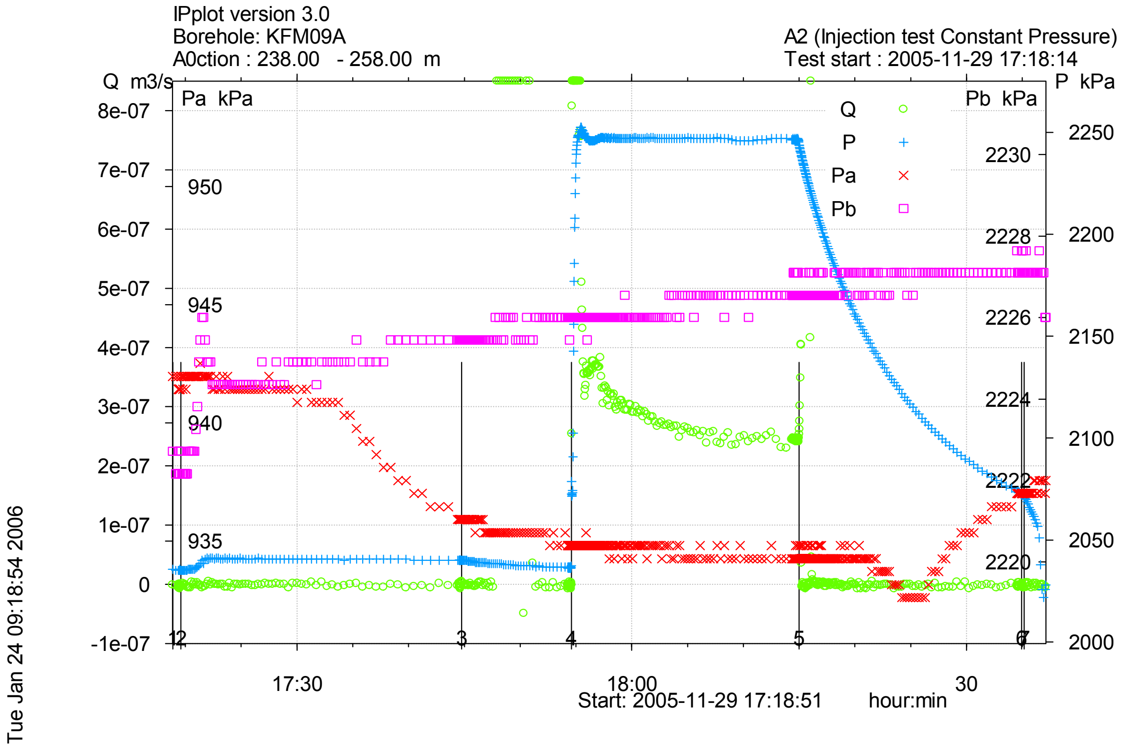


Figure A3-68. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 238.0-258.0 m in borehole KFM09A.*

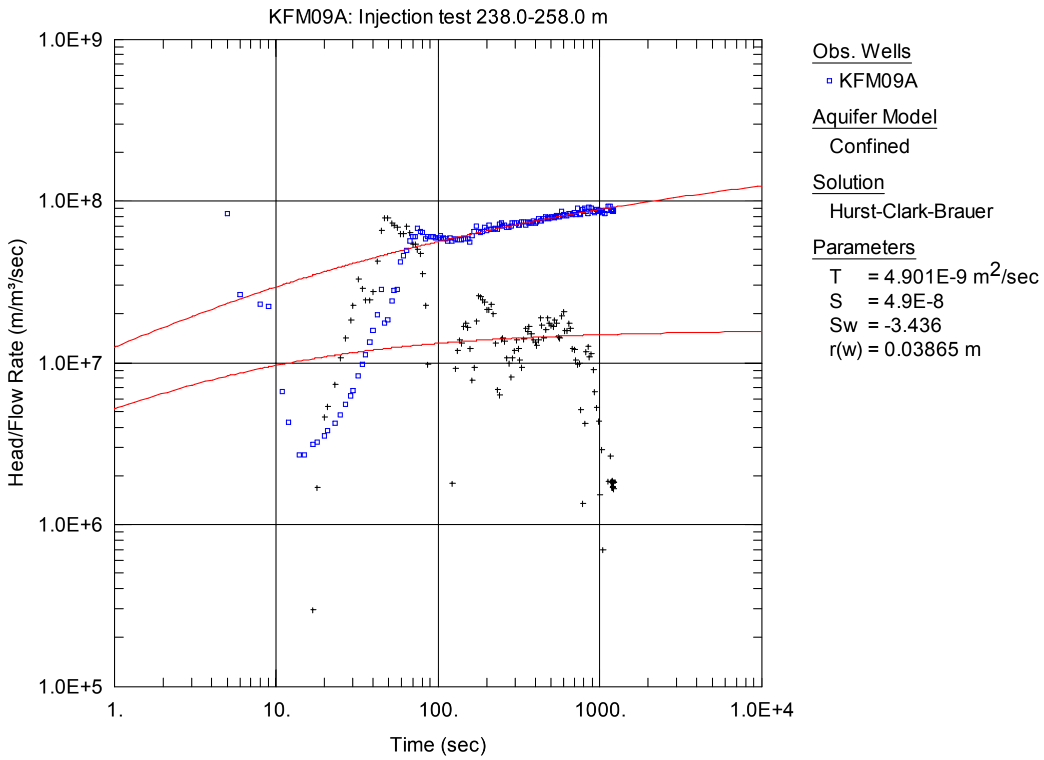


Figure A3-69. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 238.0-258.0 m in KFM09A.*

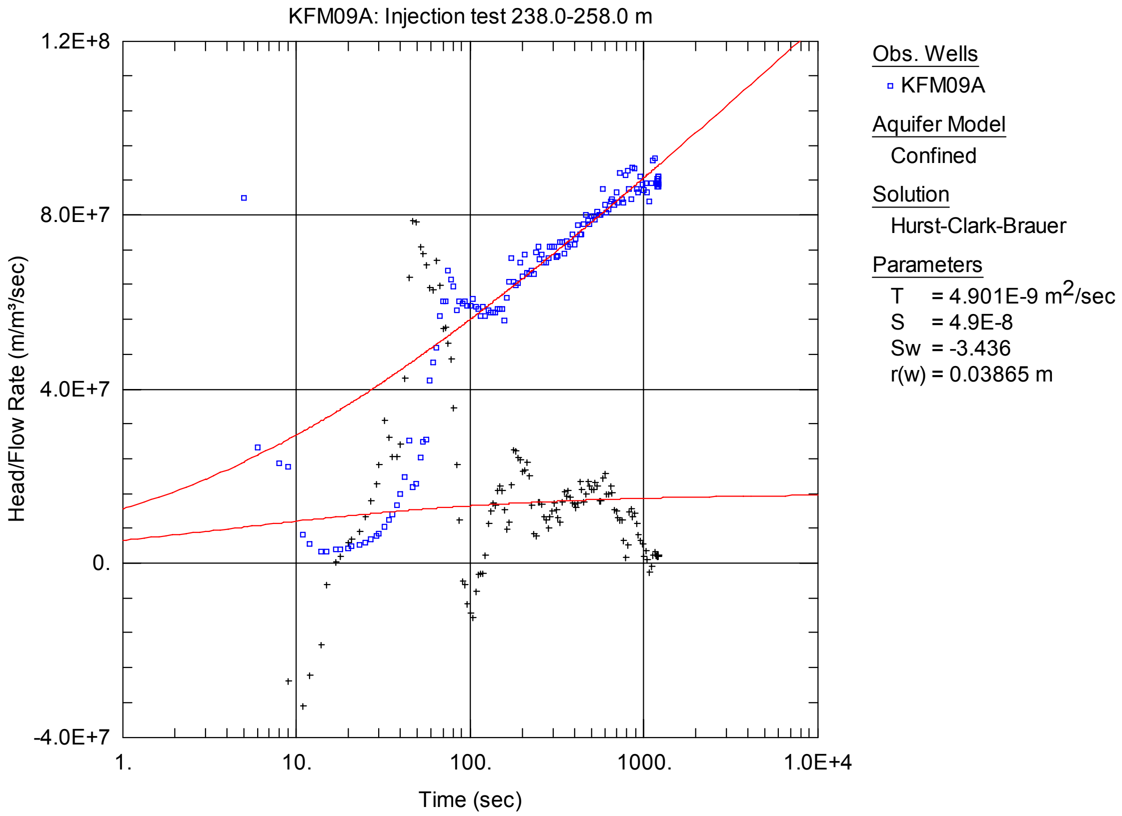


Figure A3-70. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 238.0-258.0 m in KFM09A.*

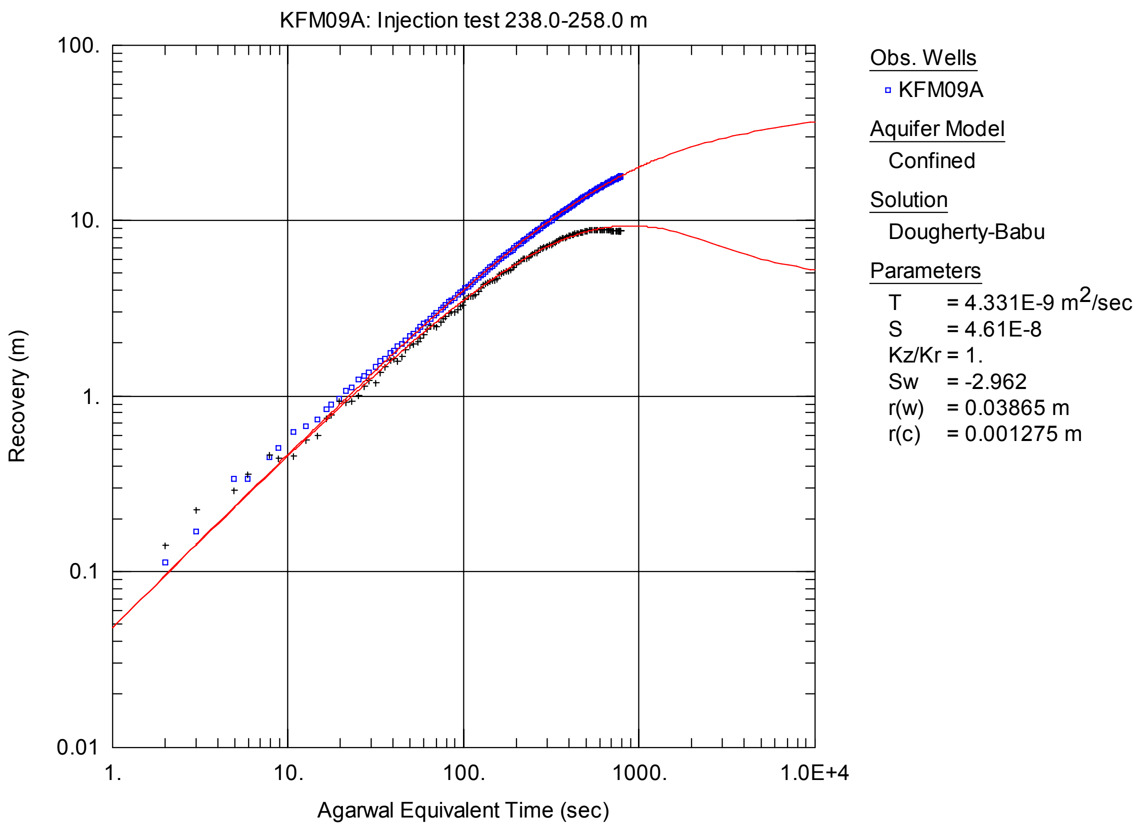


Figure A3-71. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 238.0-258.0 m in KFM09A.*

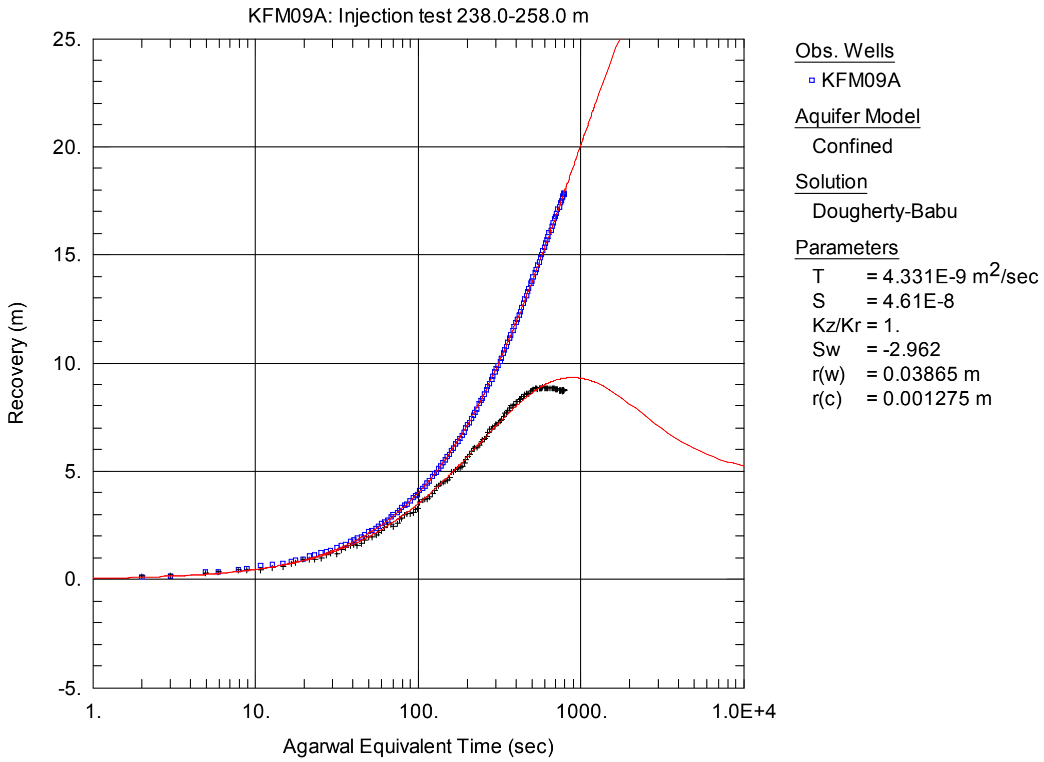


Figure A3-72. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in 238.0-258.0 m in KFM09A.*

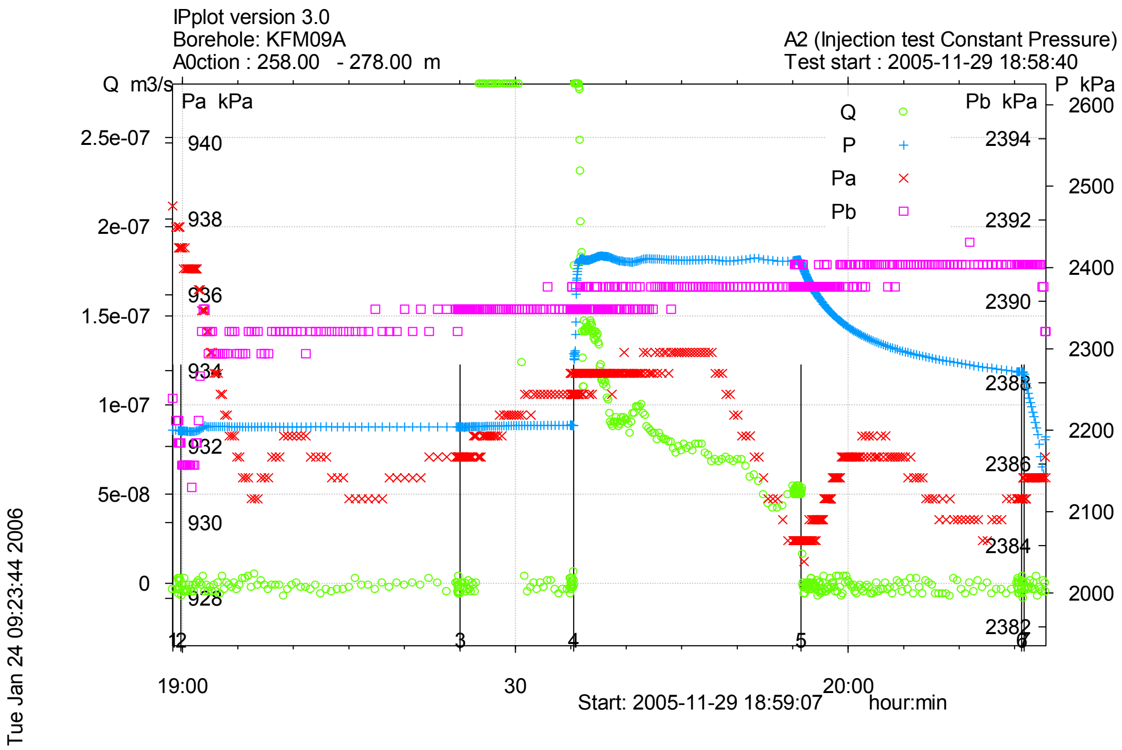


Figure A3-73. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 258.0-278.0 m in borehole KFM09A.*

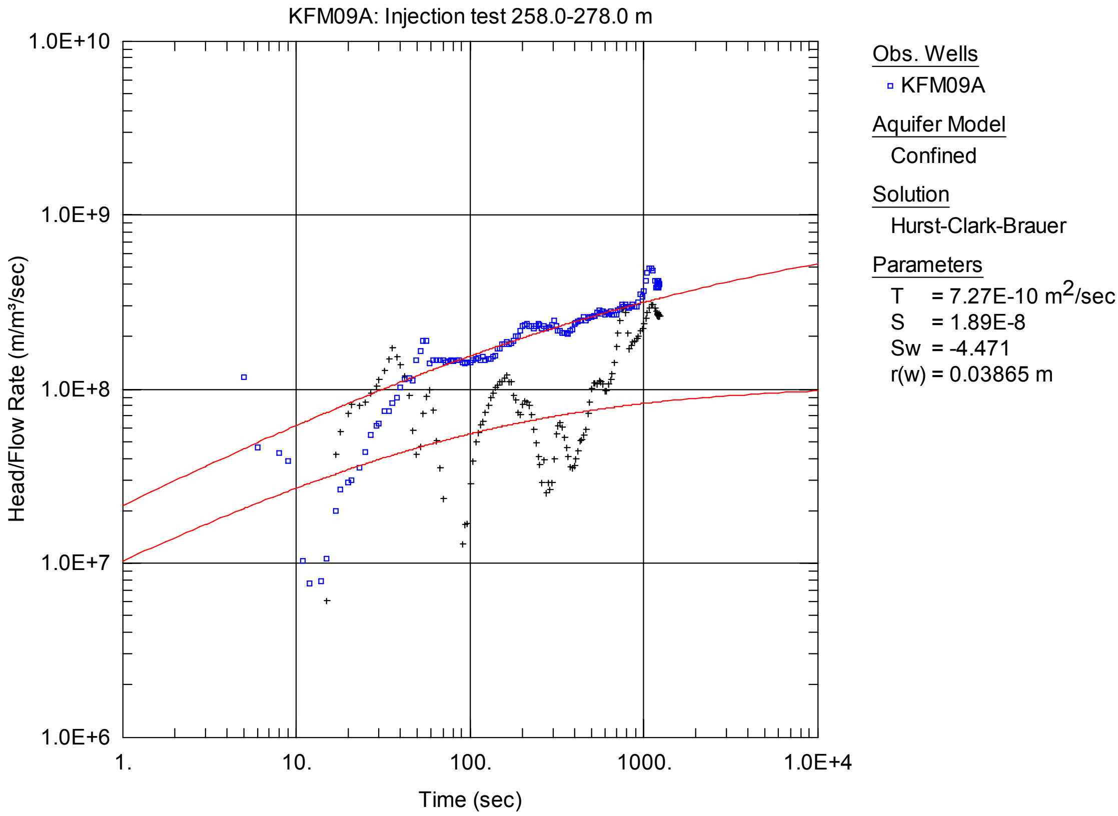


Figure A3-74. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 258.0-278.0 m in KFM09A.*

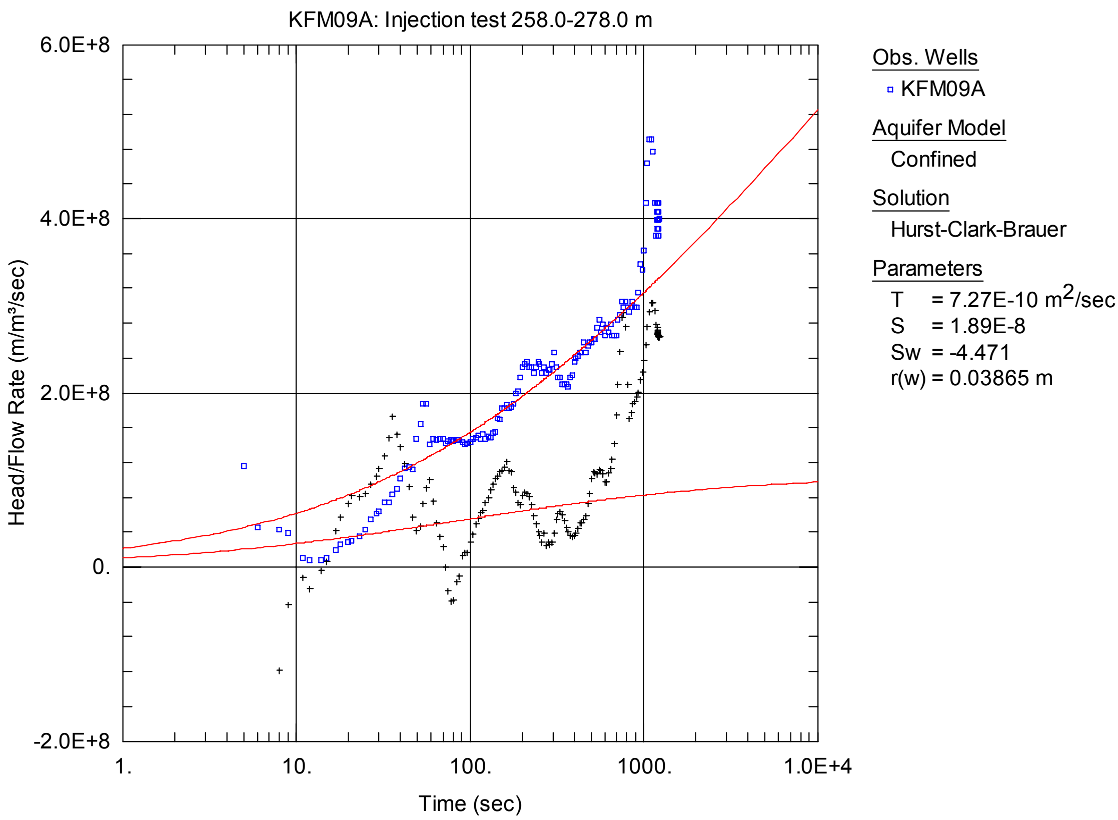


Figure A3-75. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 258.0-278.0 m in KFM09A.*

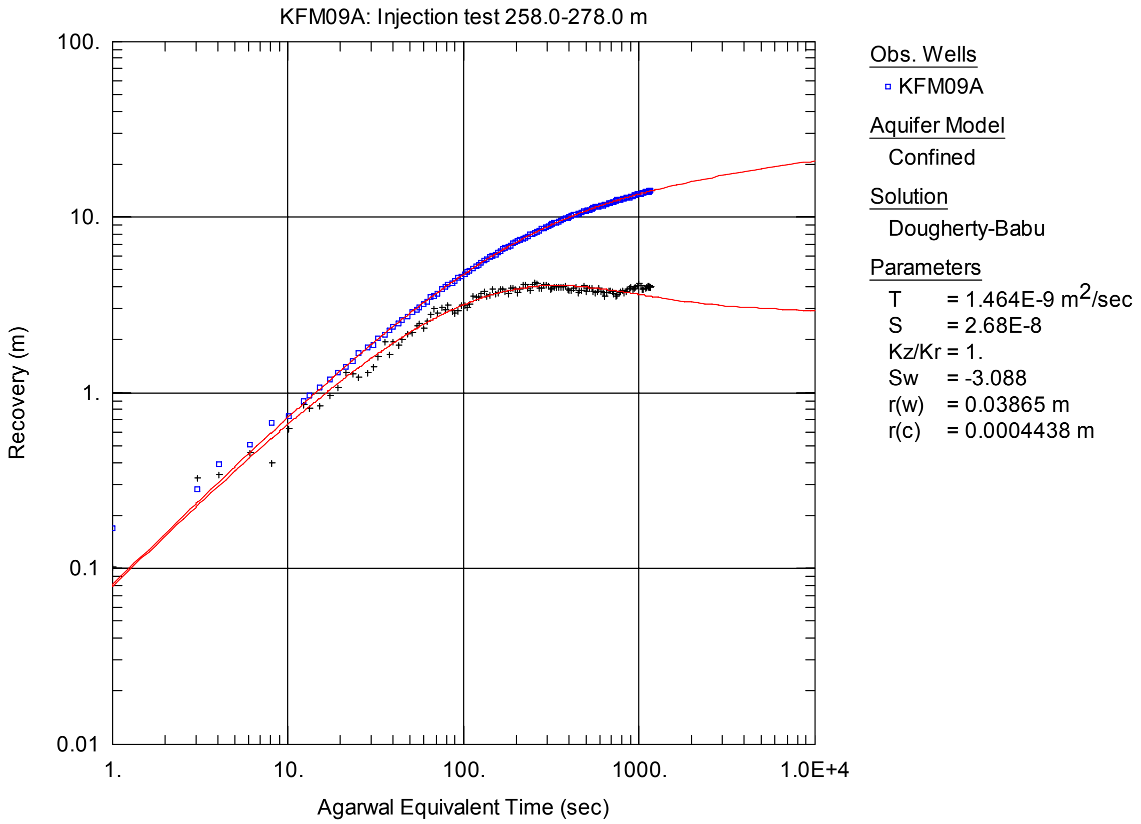


Figure A3-76. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 258.0-278.0 m in KFM09A.*

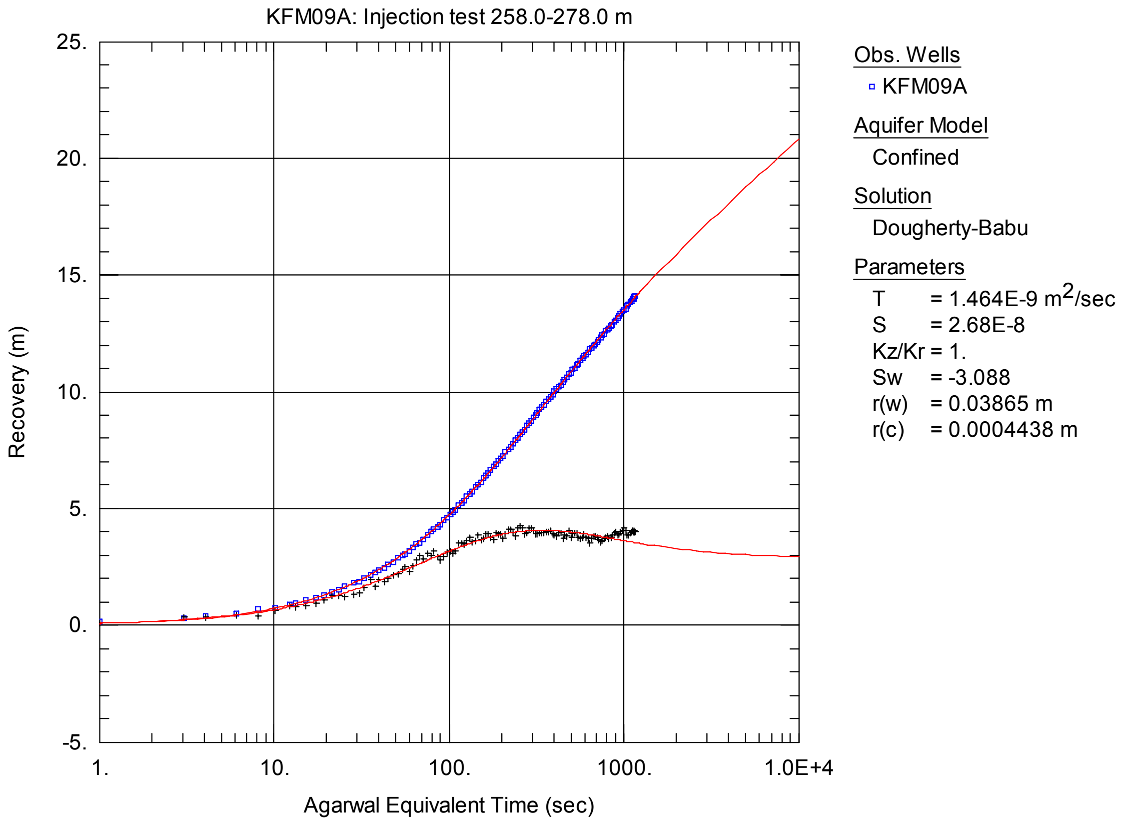


Figure A3-77. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 258.0-278.0 m in KFM09A.*

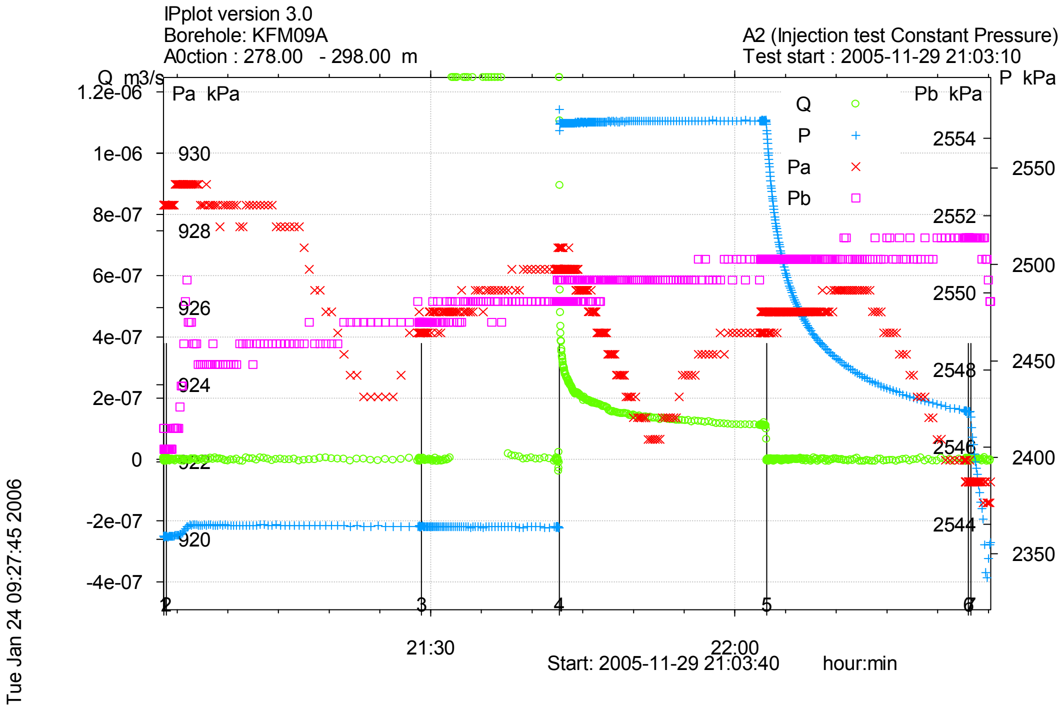


__Figure A3-78.__ Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 278.0-298.0 m in borehole KFM09A.

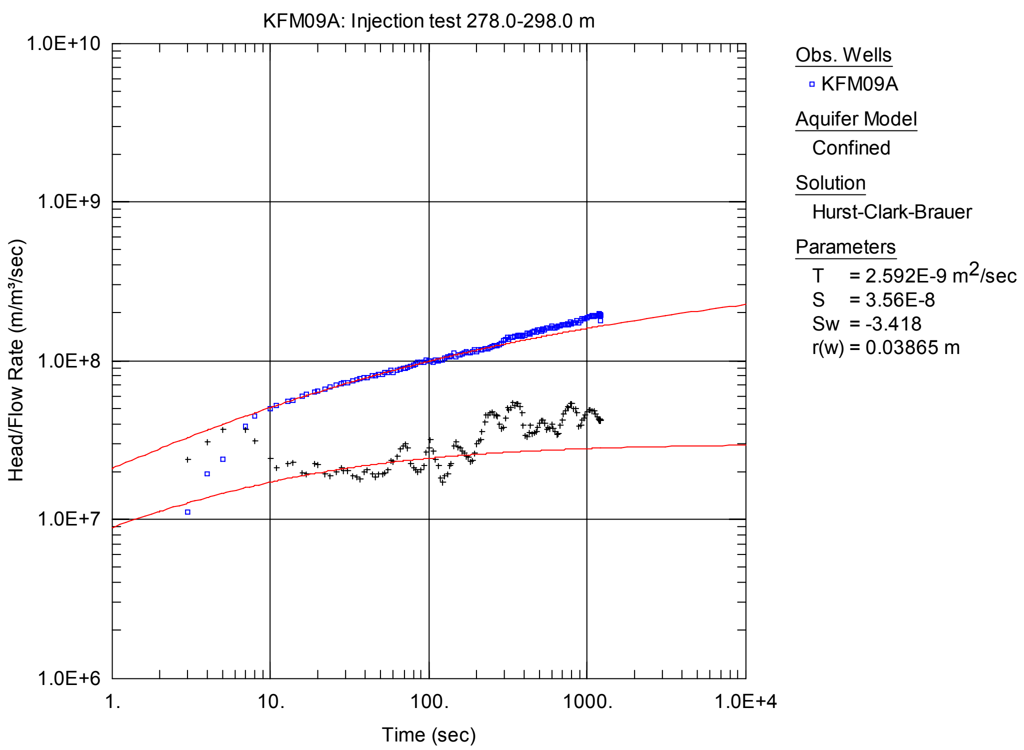


__Figure A3-79.__ Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 278.0-298.0 m in KFM09A. This plot shows the first of two different PRF:s during the injection period in this section.

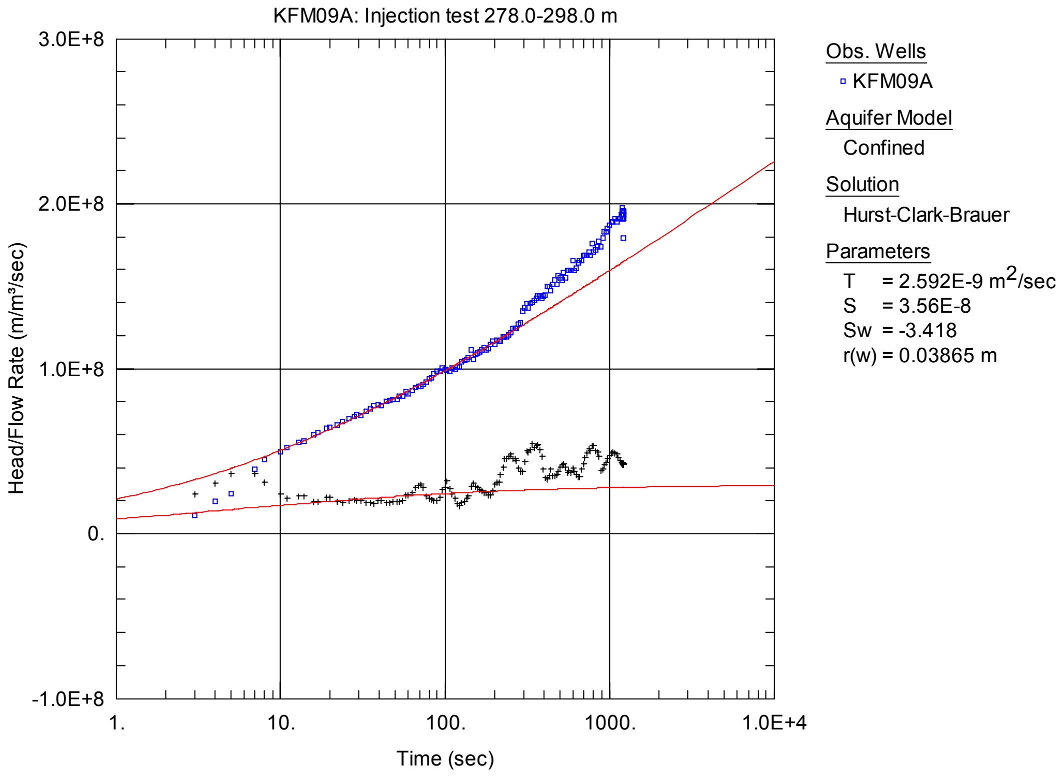


Figure A3-80. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 278.0-298.0x m in KFM09A. This plot shows the first of two different PRF:s during the injection period in this section.*

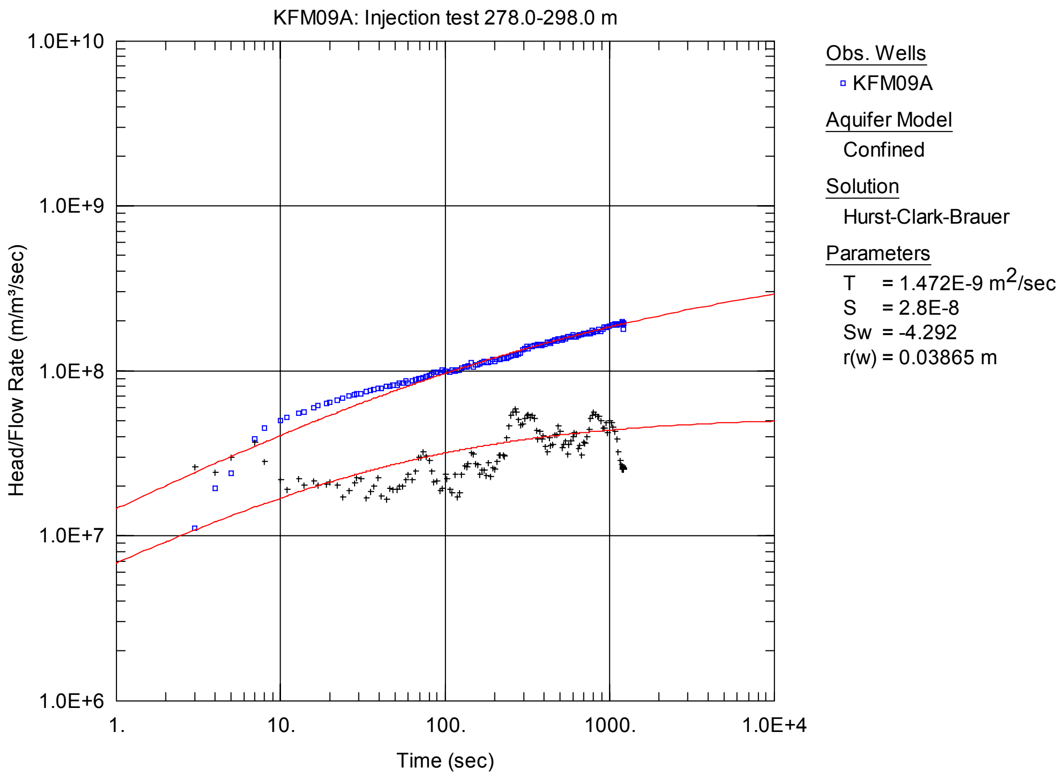


Figure A3-81. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 278.0-298.0 m in KFM09A. This plot shows the second of two different PRF:s during the injection period in this section.*

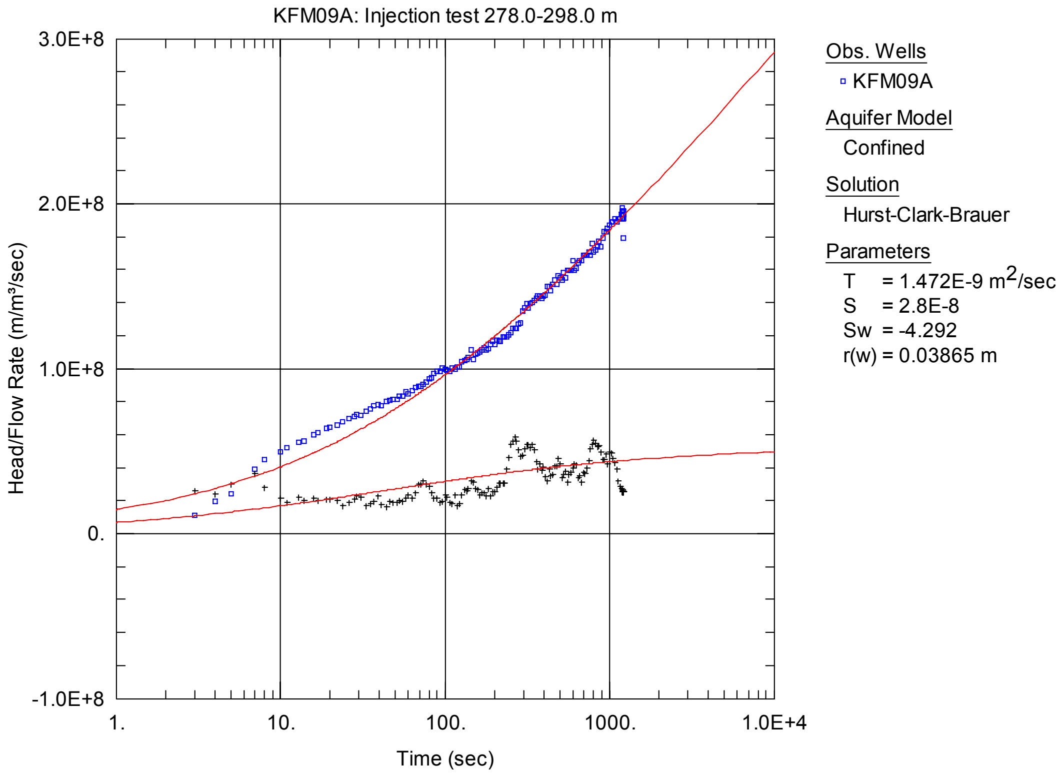


Figure A3-82. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 278.0-298.0 m in KFM09A. This plot shows the second of two different PRF:s during the injection period in this section.*

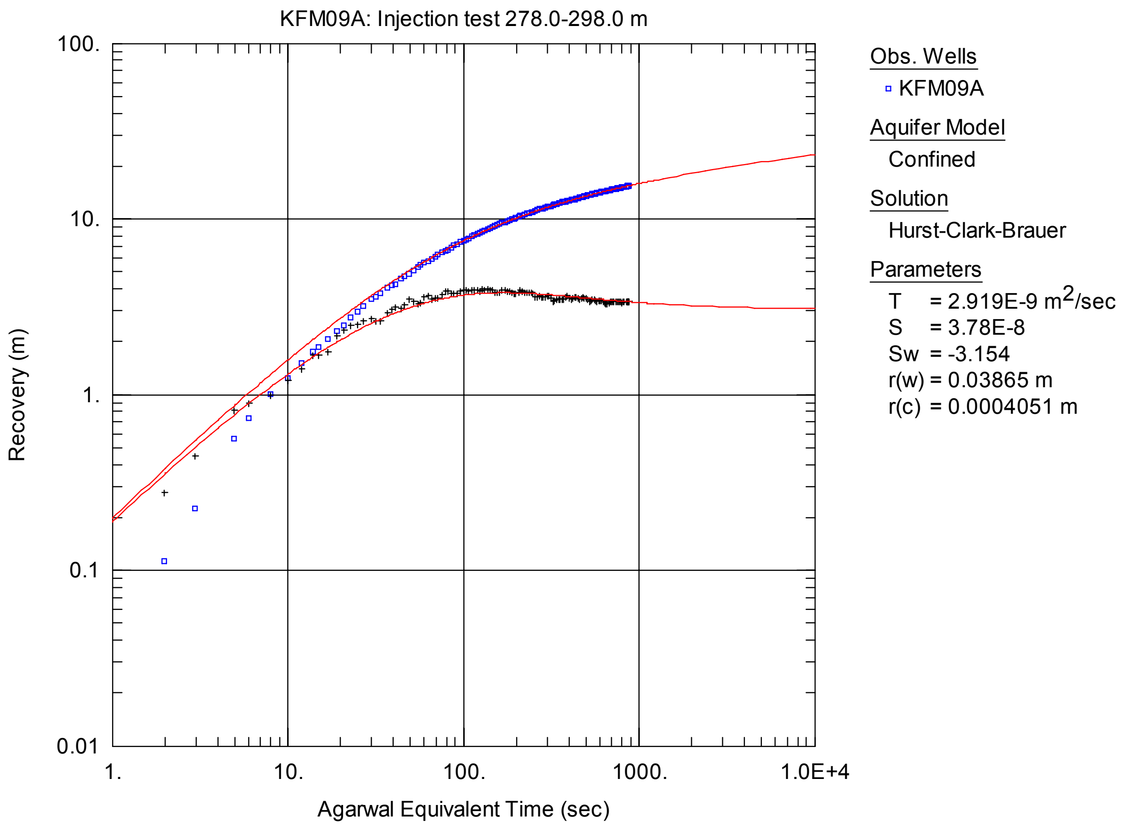


Figure A3-83. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 278.0-298.0 m in KFM09A.*

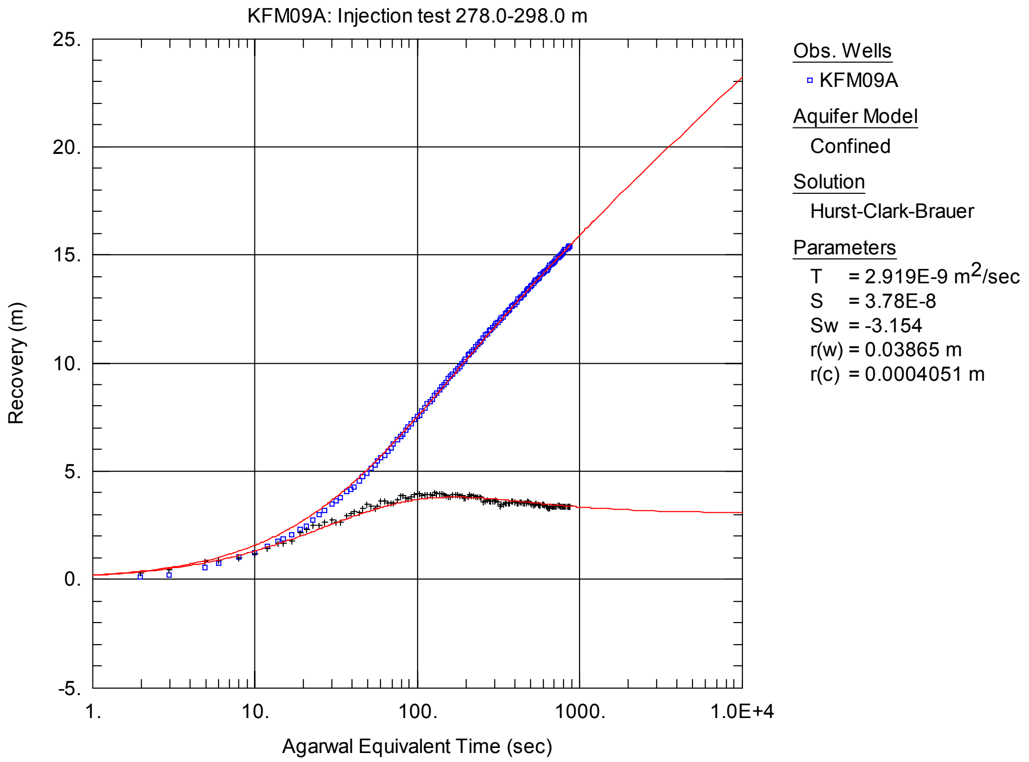


Figure A3-84. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in 278.0-298.0 m in KFM09A.*

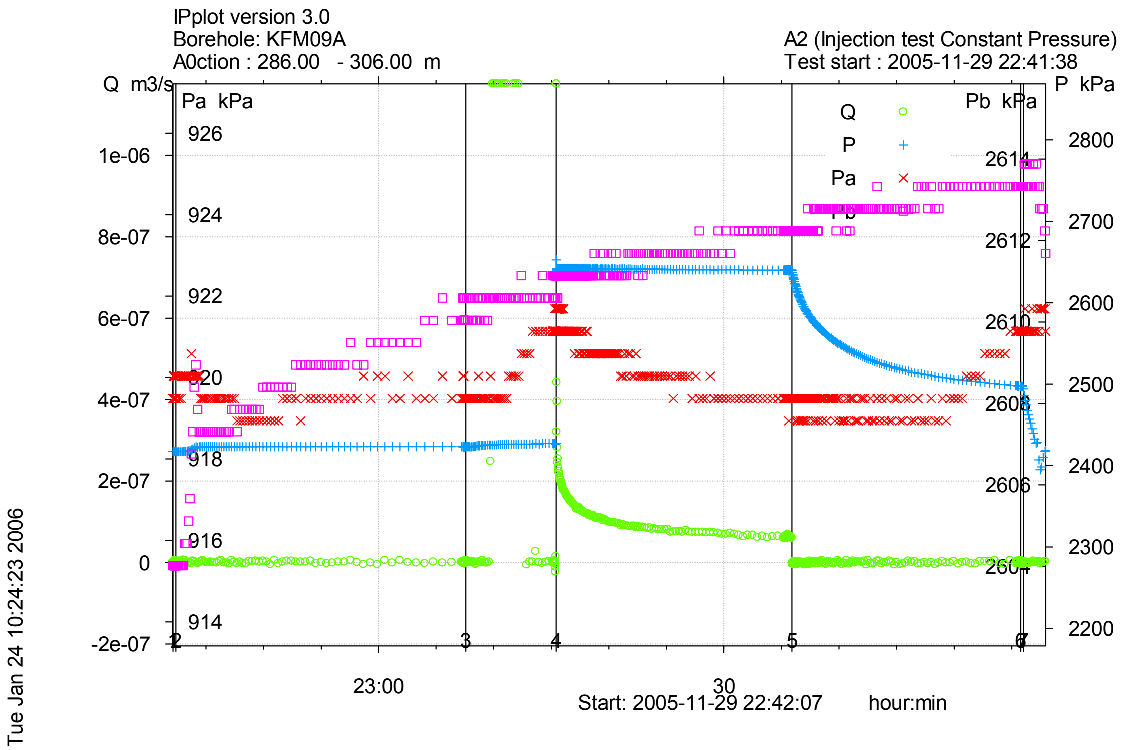


Figure A3-85. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 286.0-306.0 m in borehole KFM09A.*

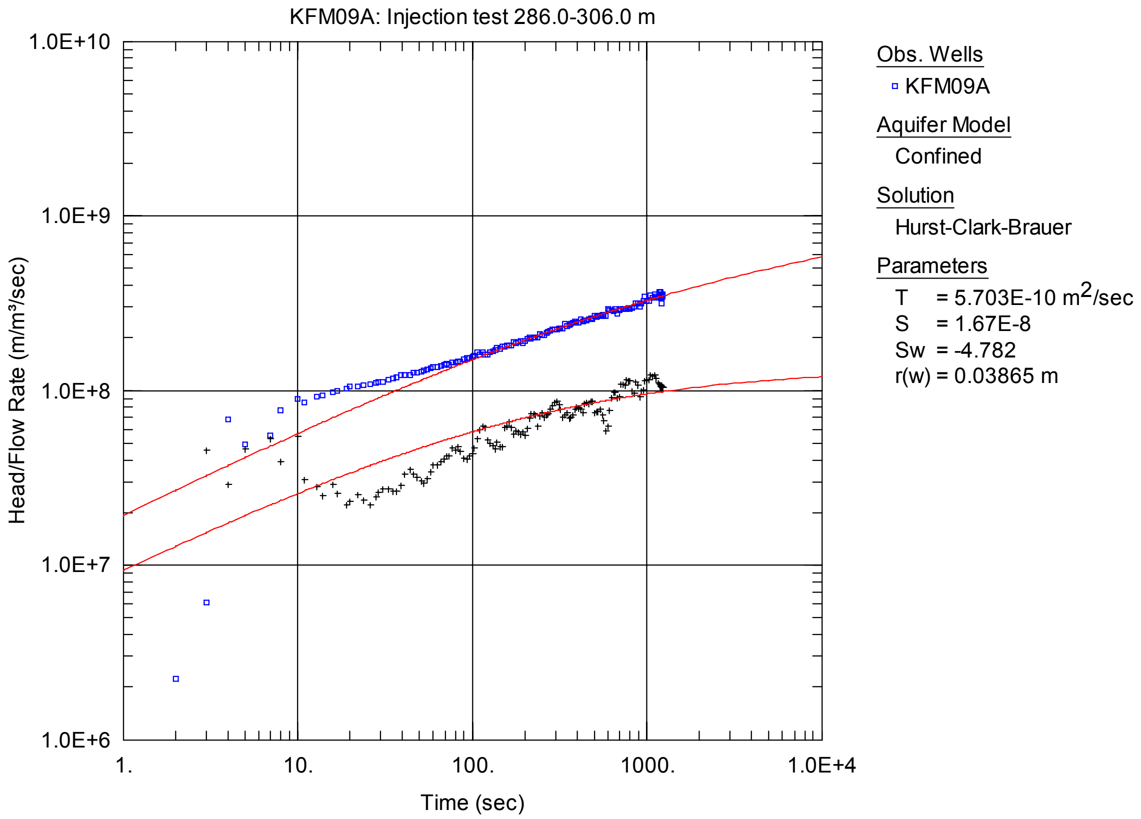


Figure A3-86. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 286.0-306.0 m in KFM09A.*

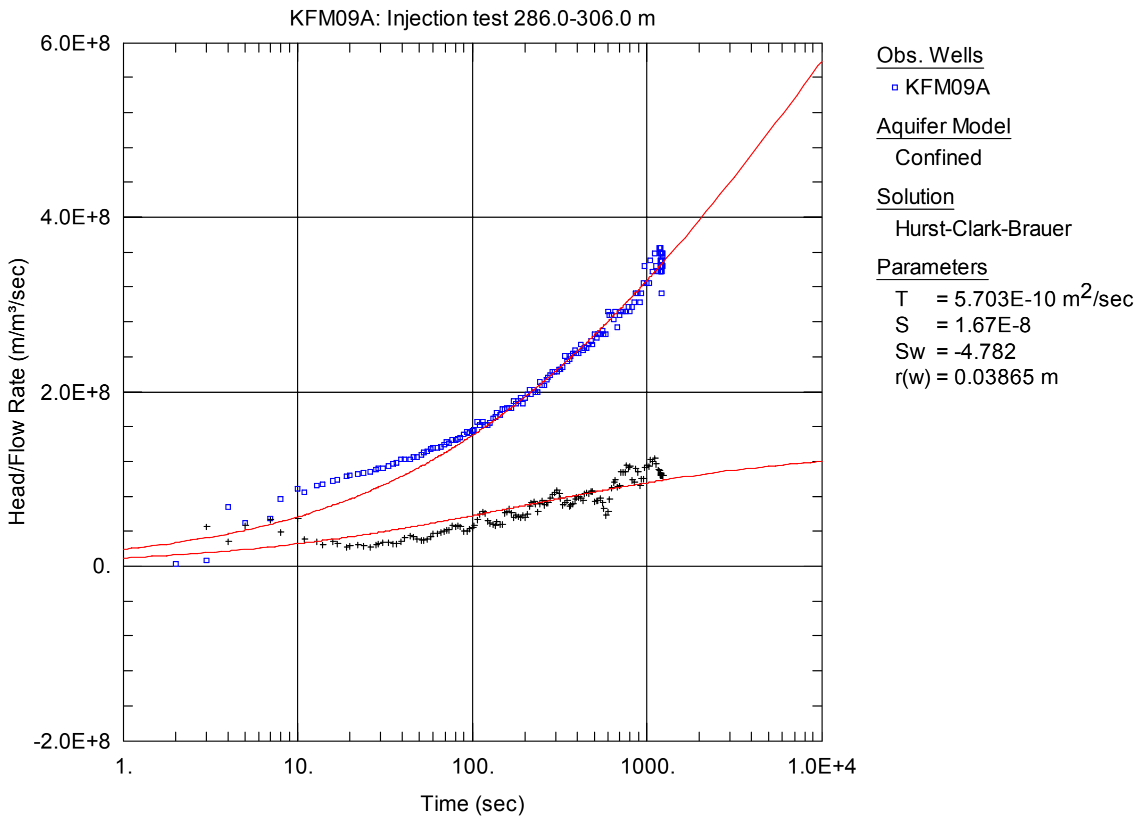


Figure A3-87. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 286.0-306.0 m in KFM09A.*

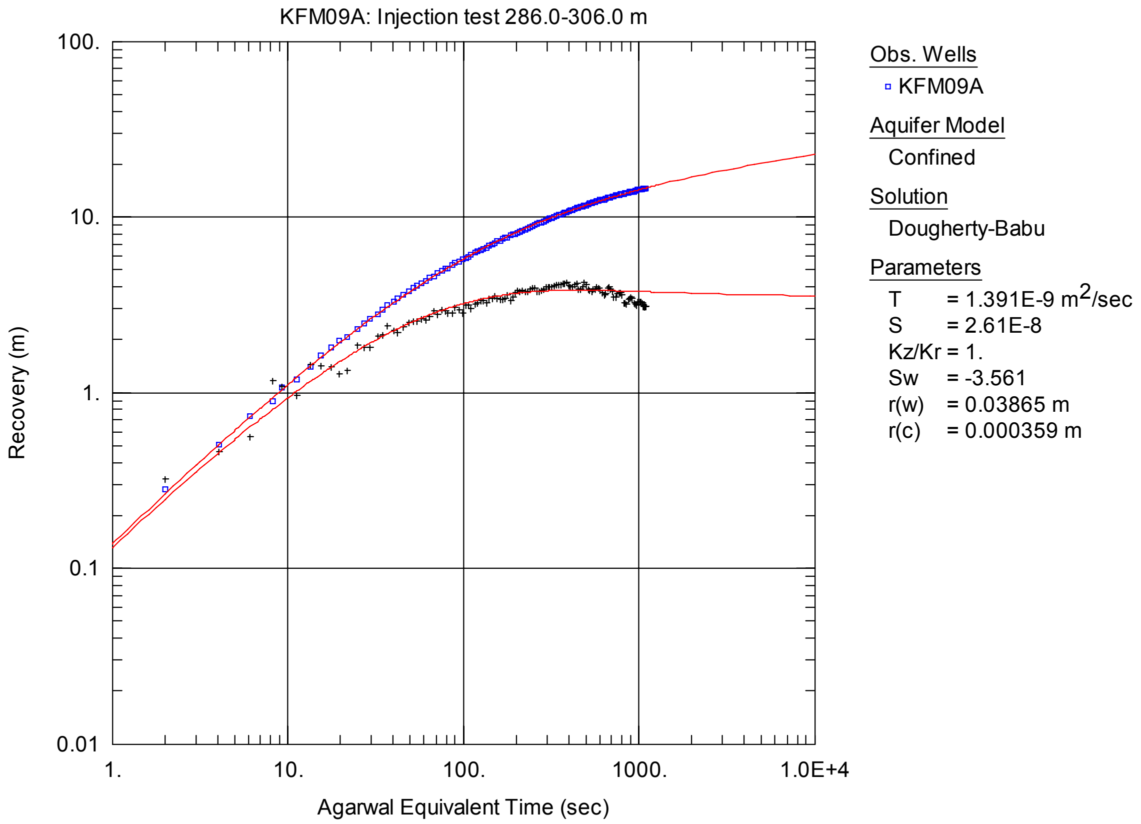


Figure A3-88. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 286.0-306.0 m in KFM09A.*

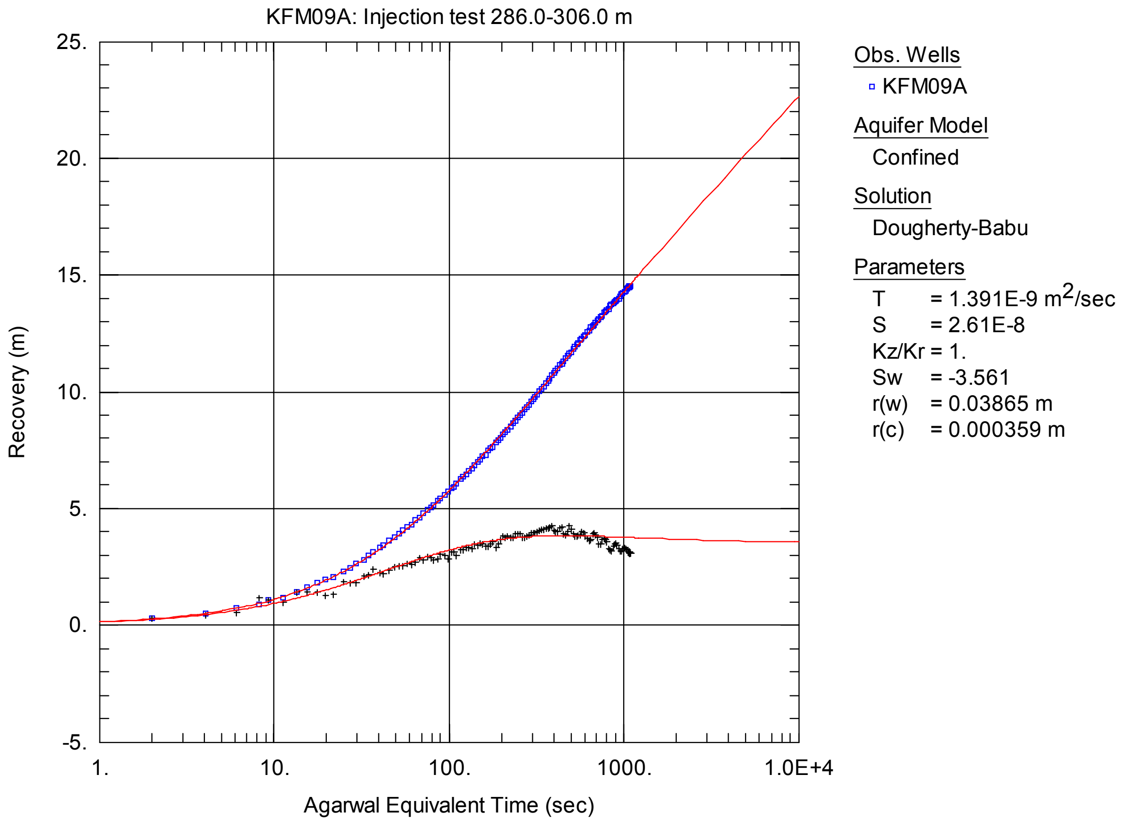


Figure A3-89. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 286.0-306.0 m in KFM09A.*

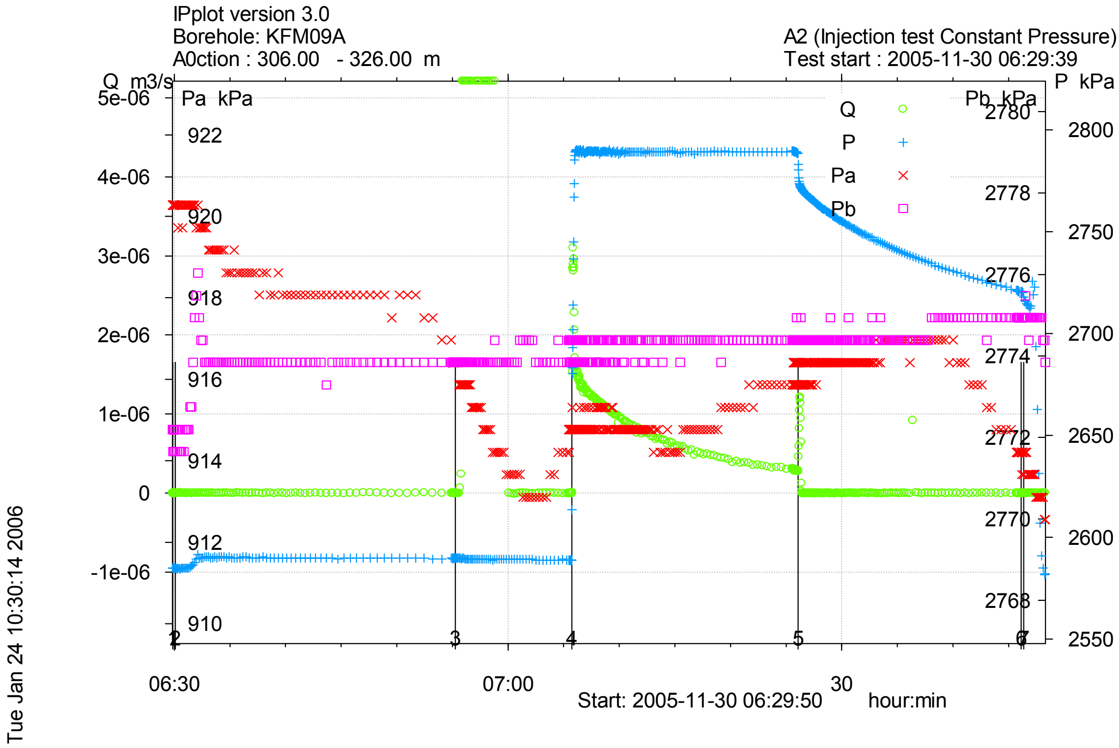


Figure A3-90. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 306.0-326.0 m in borehole KFM09A.*

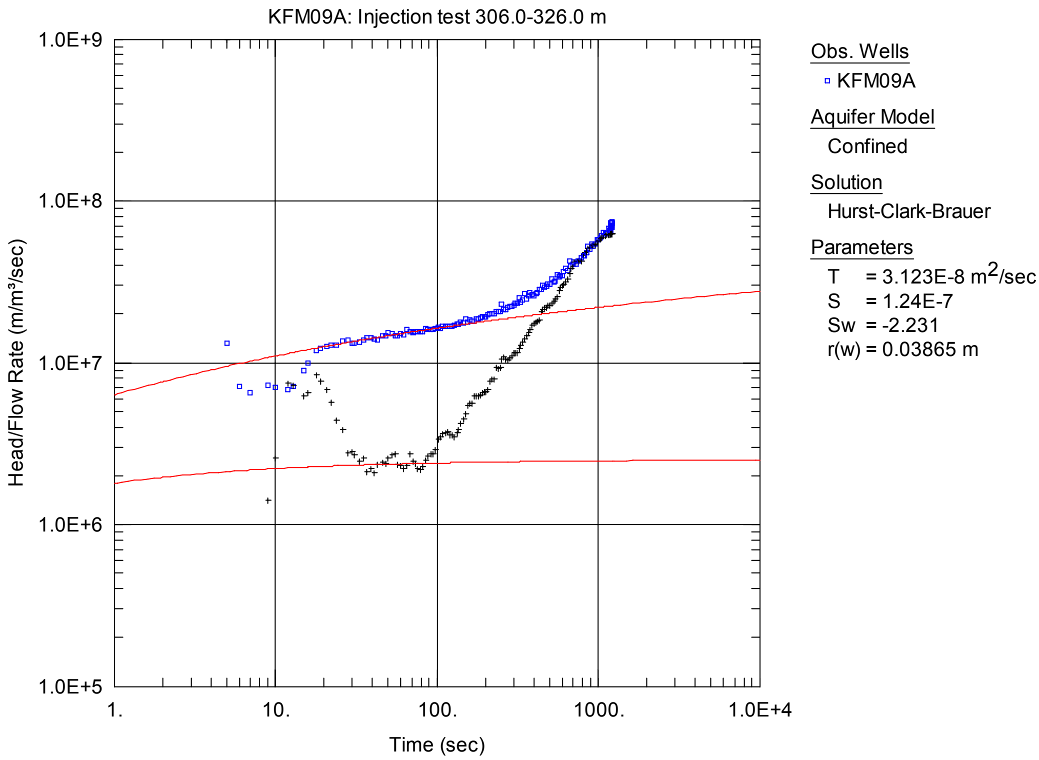


Figure A3-91. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 306.0-326.0 m in KFM09A.*

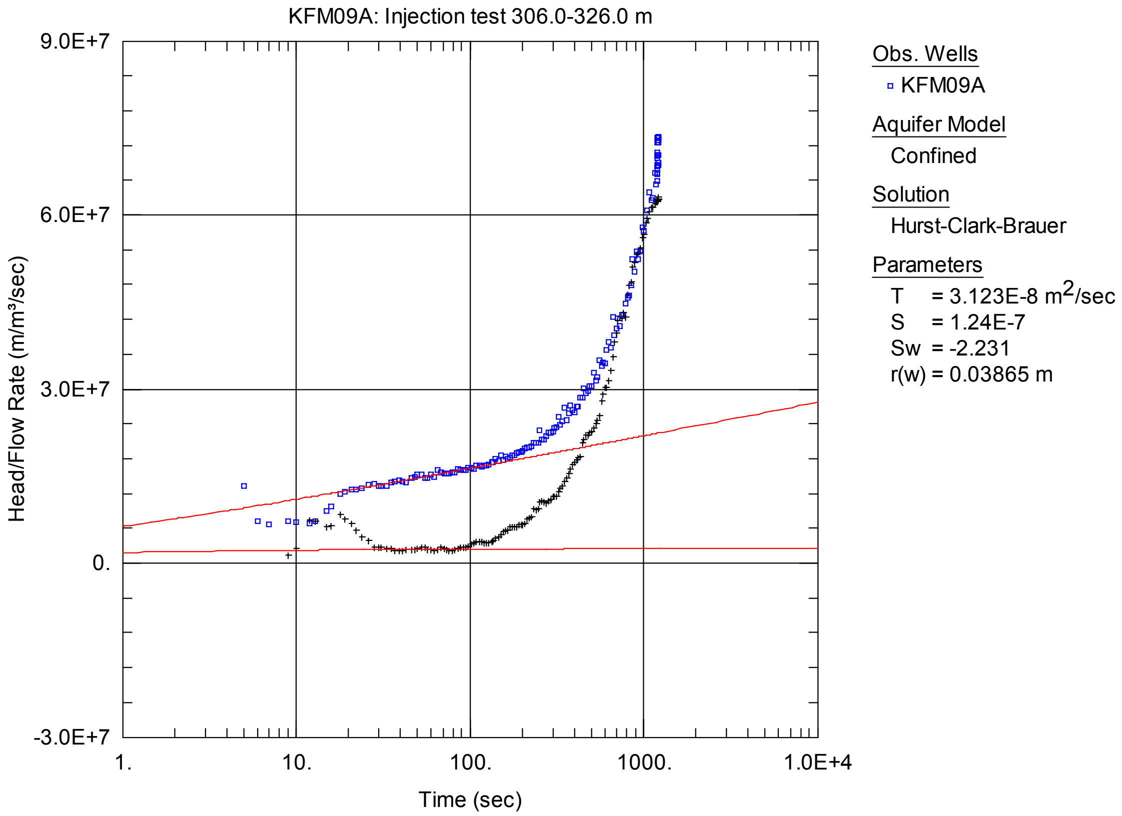


Figure A3-92. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 306.0-326.0 m in KFM09A.*

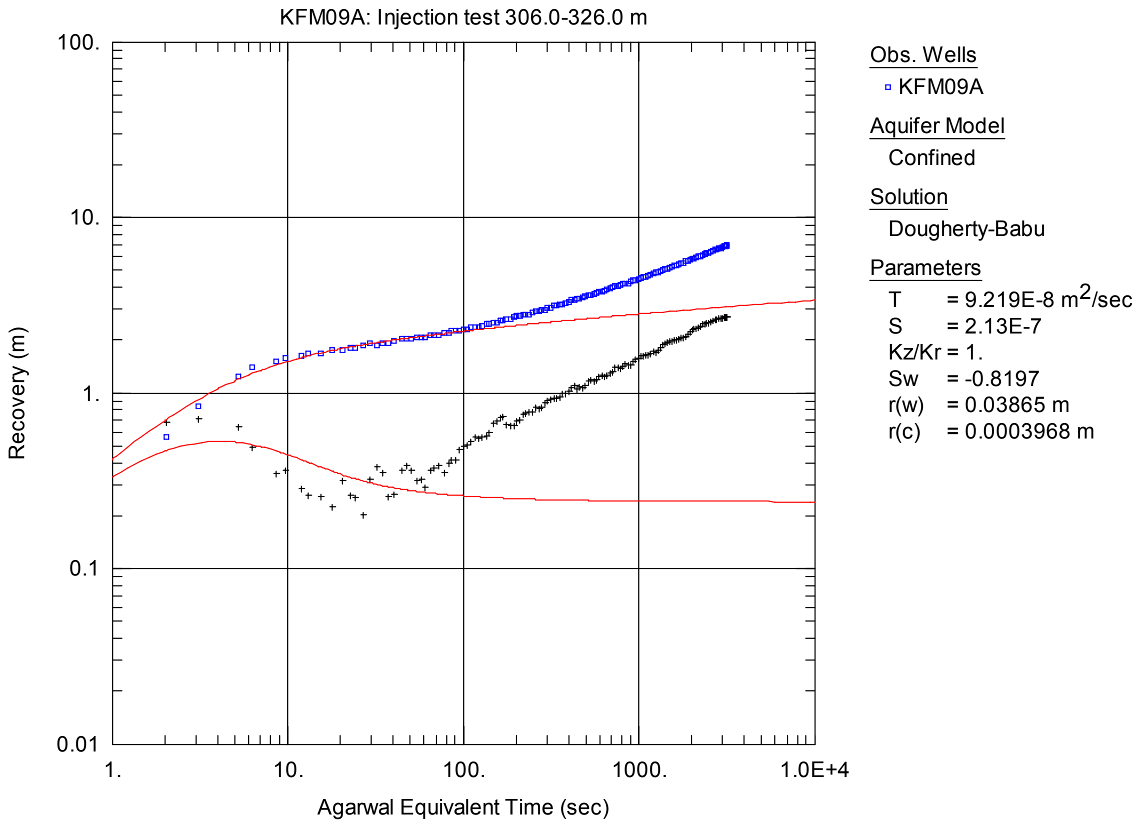


Figure A3-93. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 306.0-326.0 m in KFM09A.*

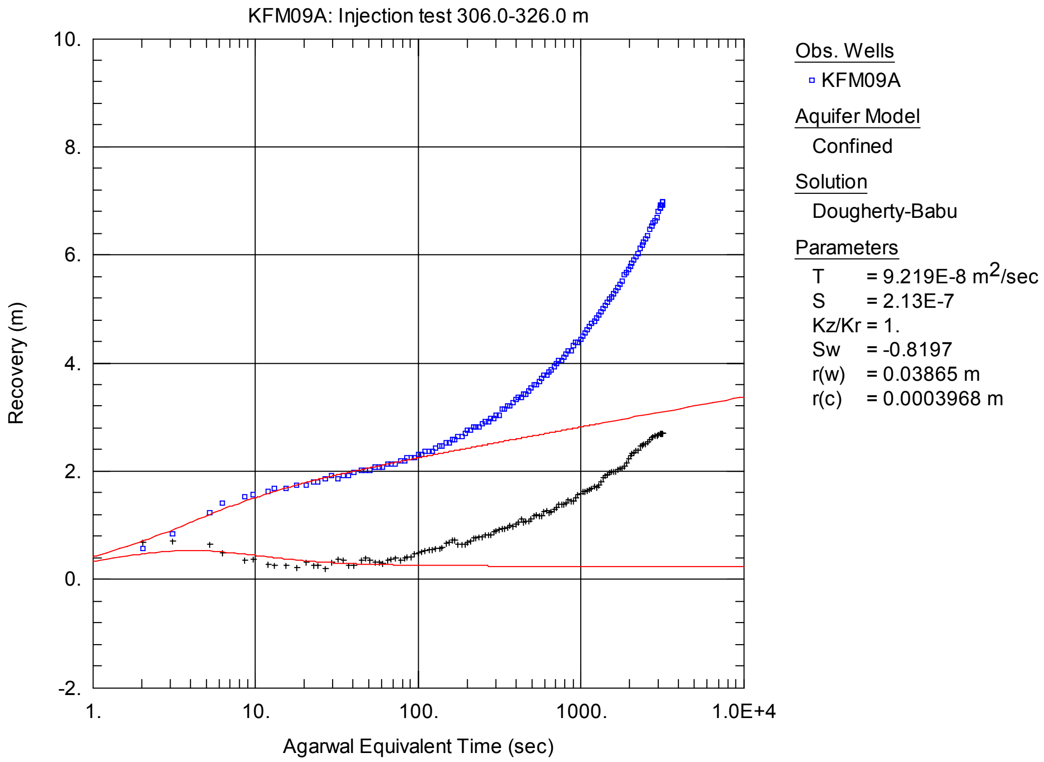


Figure A3-94. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 306.0-326.0 m in KFM09A.*

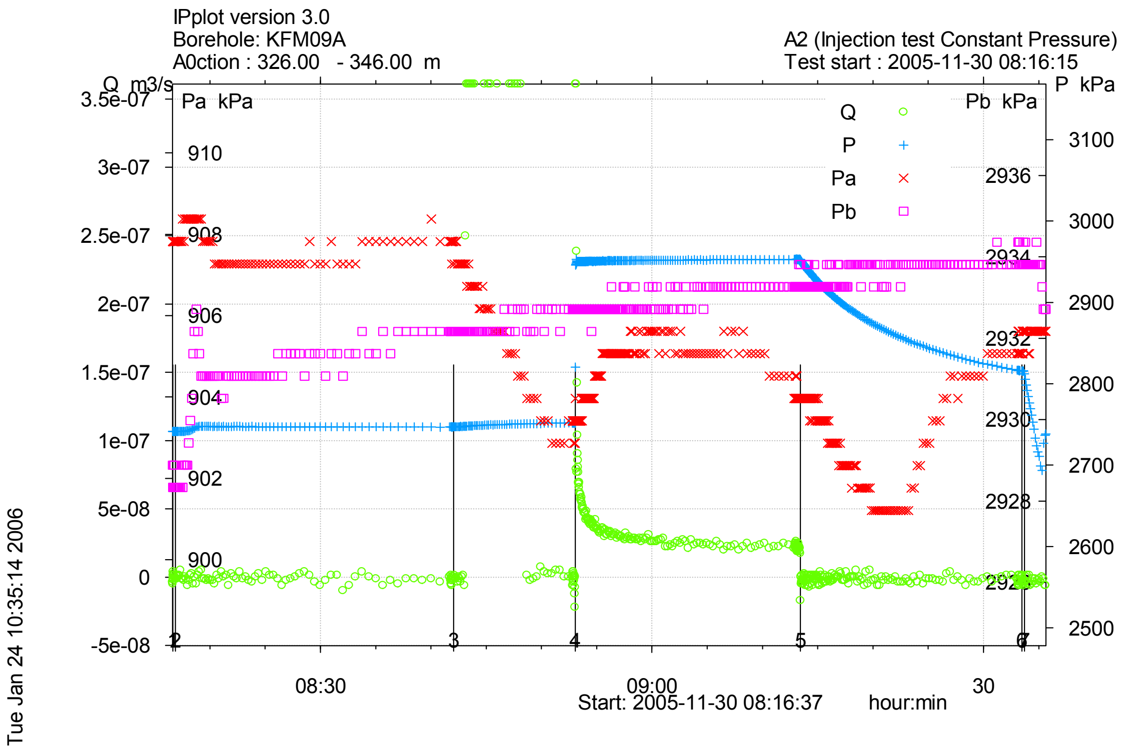


Figure A3-95. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 326.0-346.0 m in borehole KFM09A.*

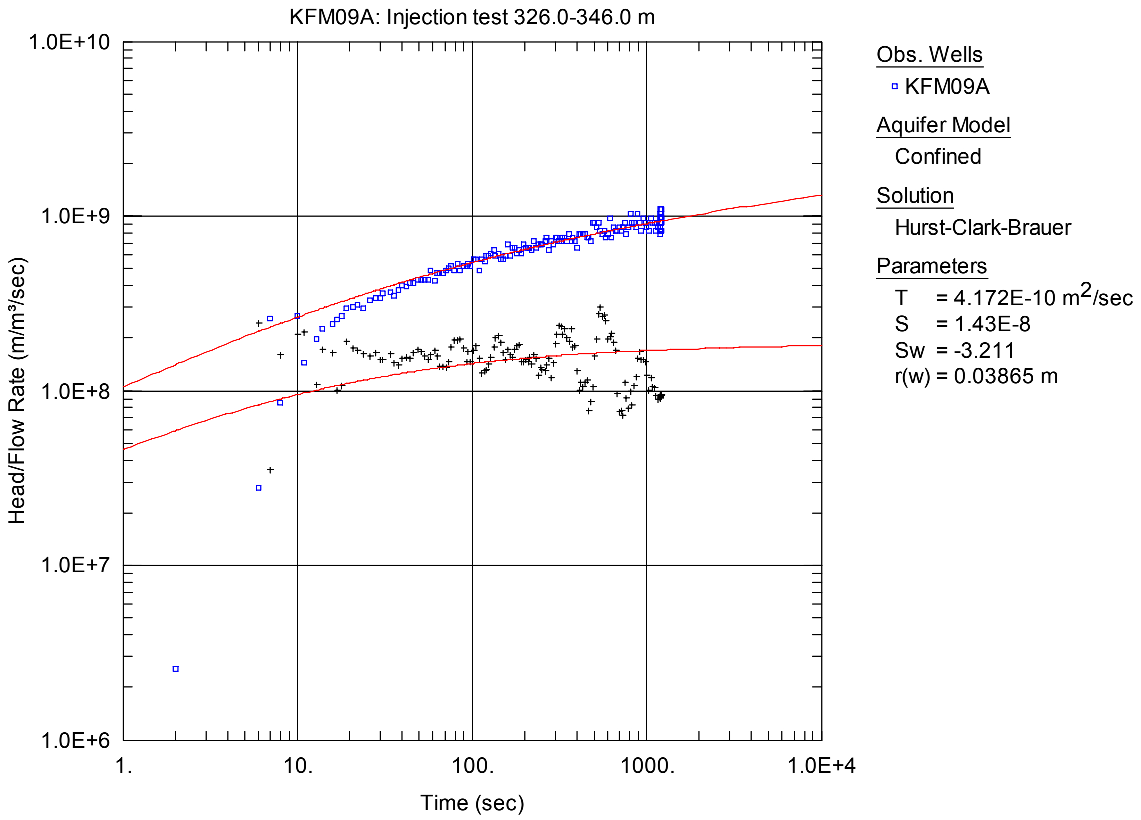


Figure A3-96. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in 326.0-346.0 m in KFM09A.*

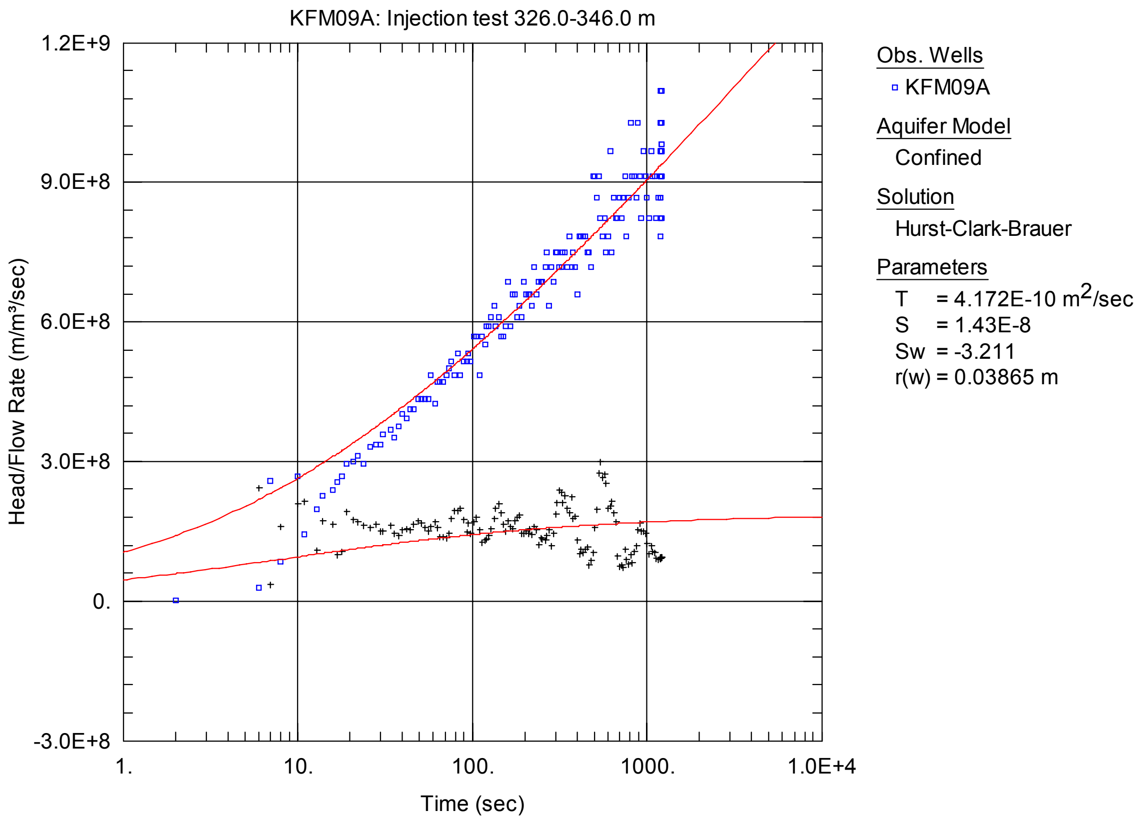


Figure A3-97. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 326.0-346.0 m in KFM09A.*

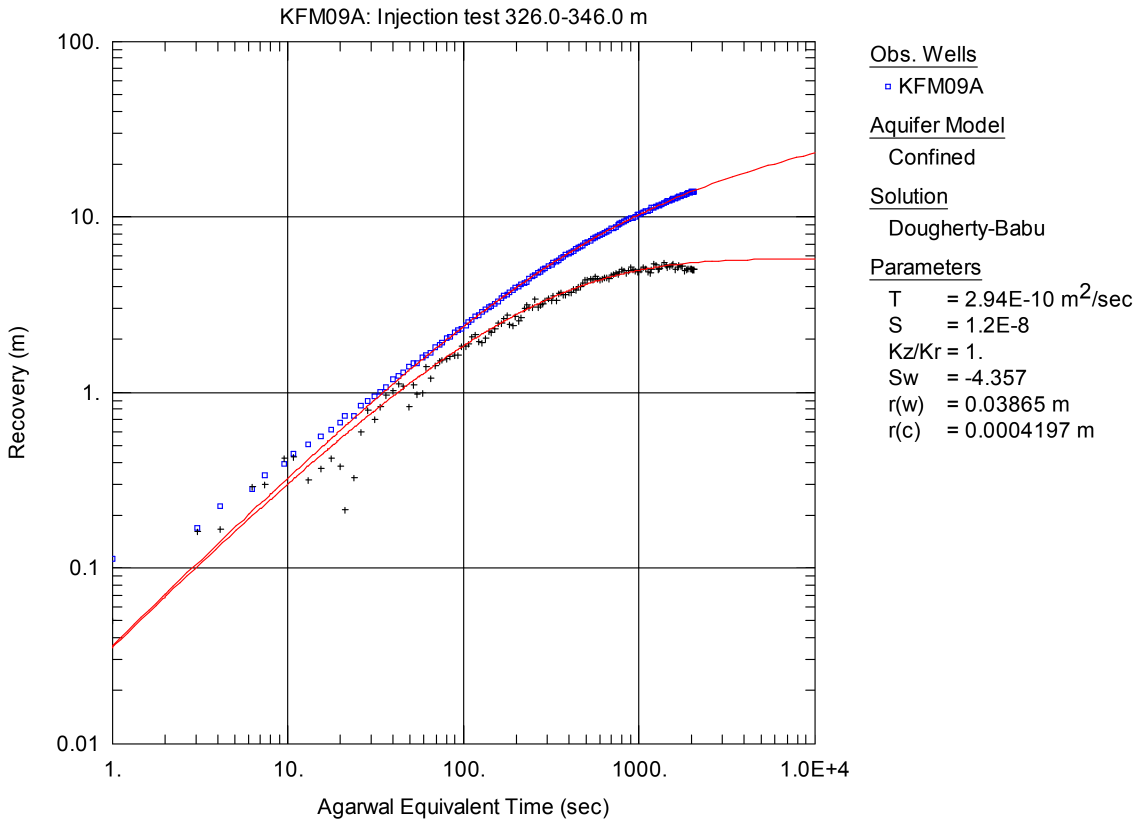


Figure A3-98. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 326.0-346.0 m in KFM09A.*

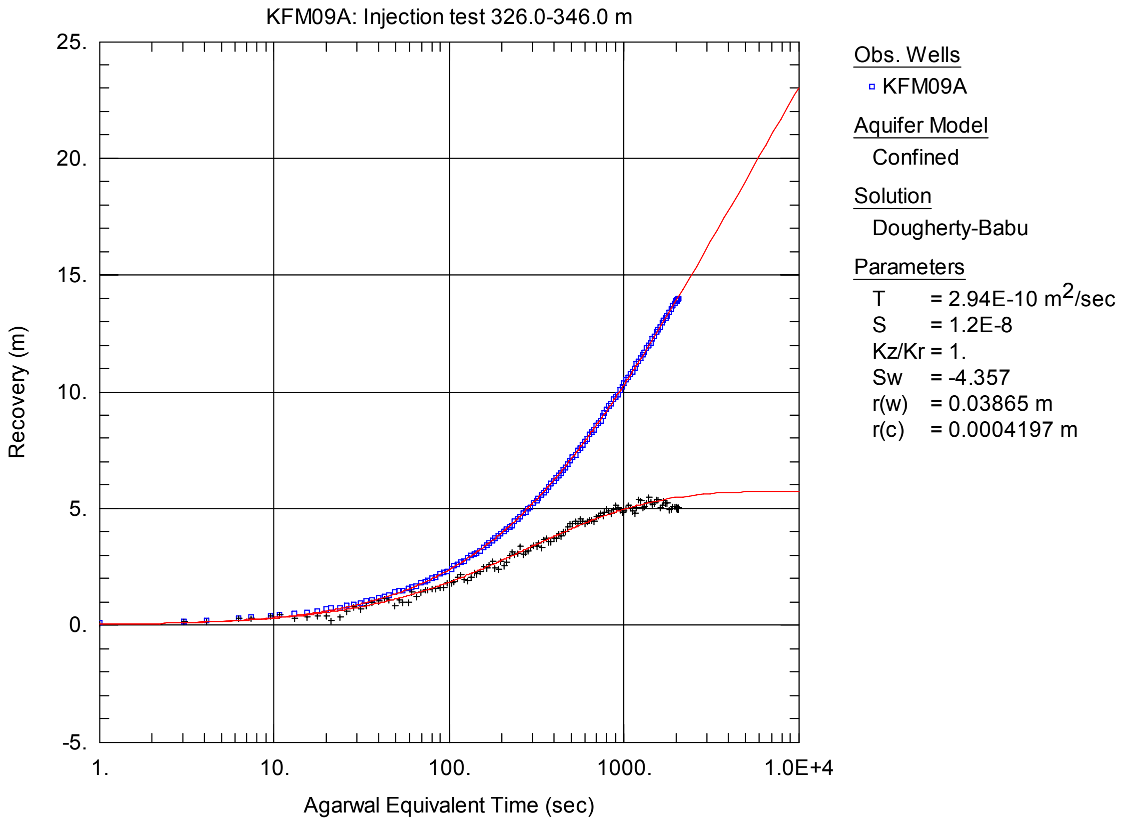


Figure A3-99. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 326.0-346.0 m in KFM09A.*

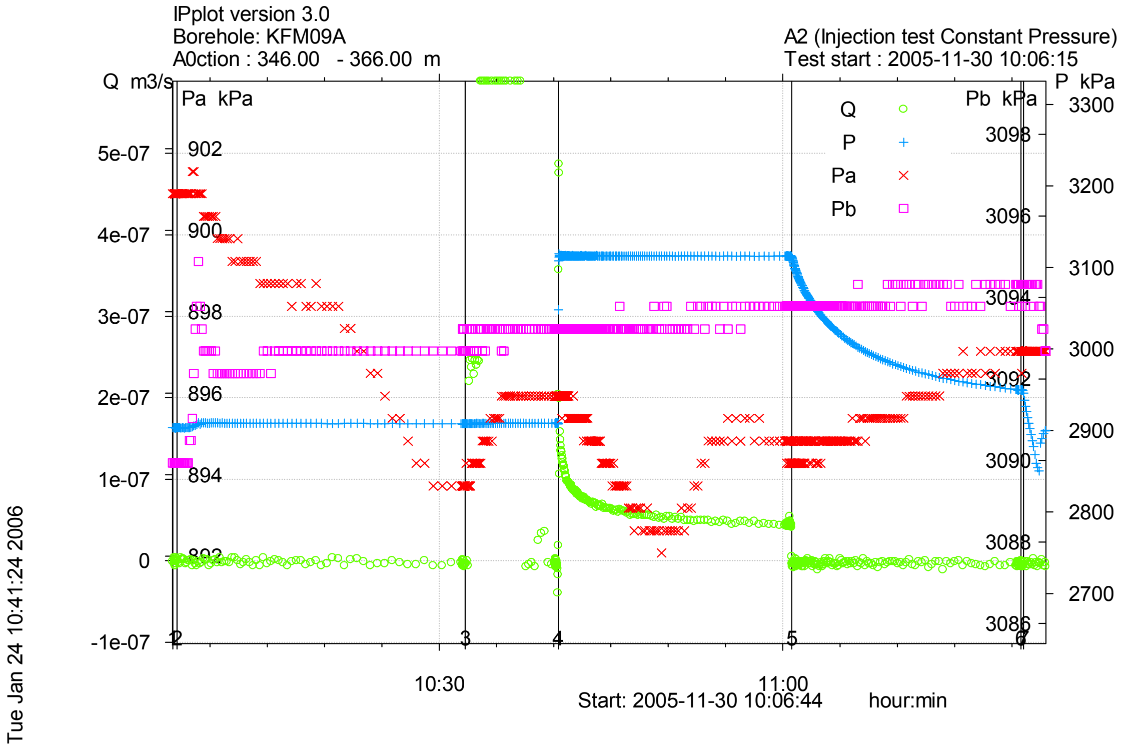


Figure A3-100. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 346.0-366.0 m in borehole KFM09A.

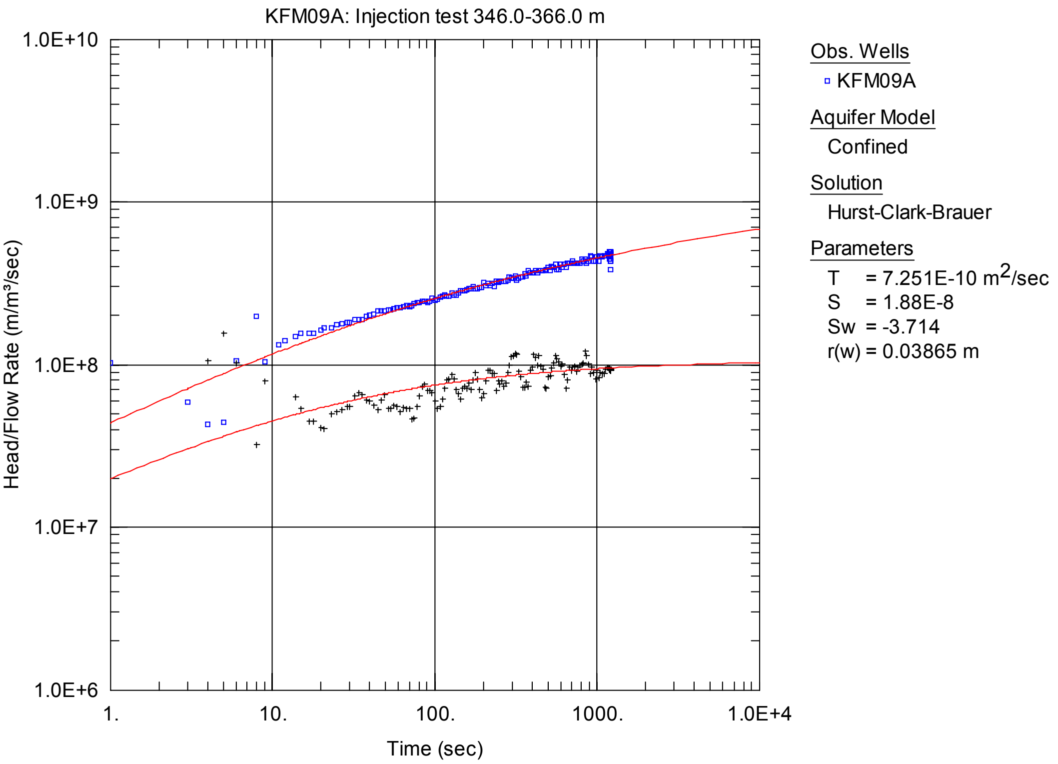


Figure A3-101. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 346.0-366.0 m in KFM09A.

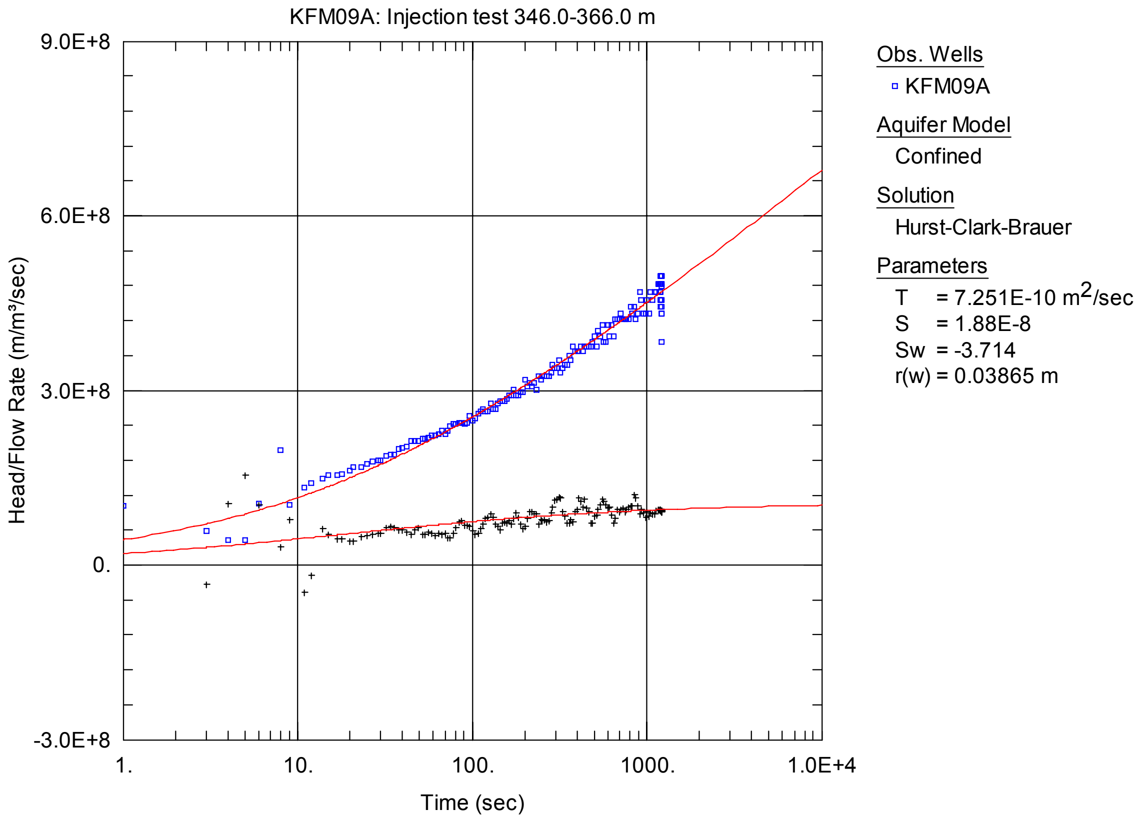


Figure A3-102. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in 346.0-366.0 m in KFM09A.*

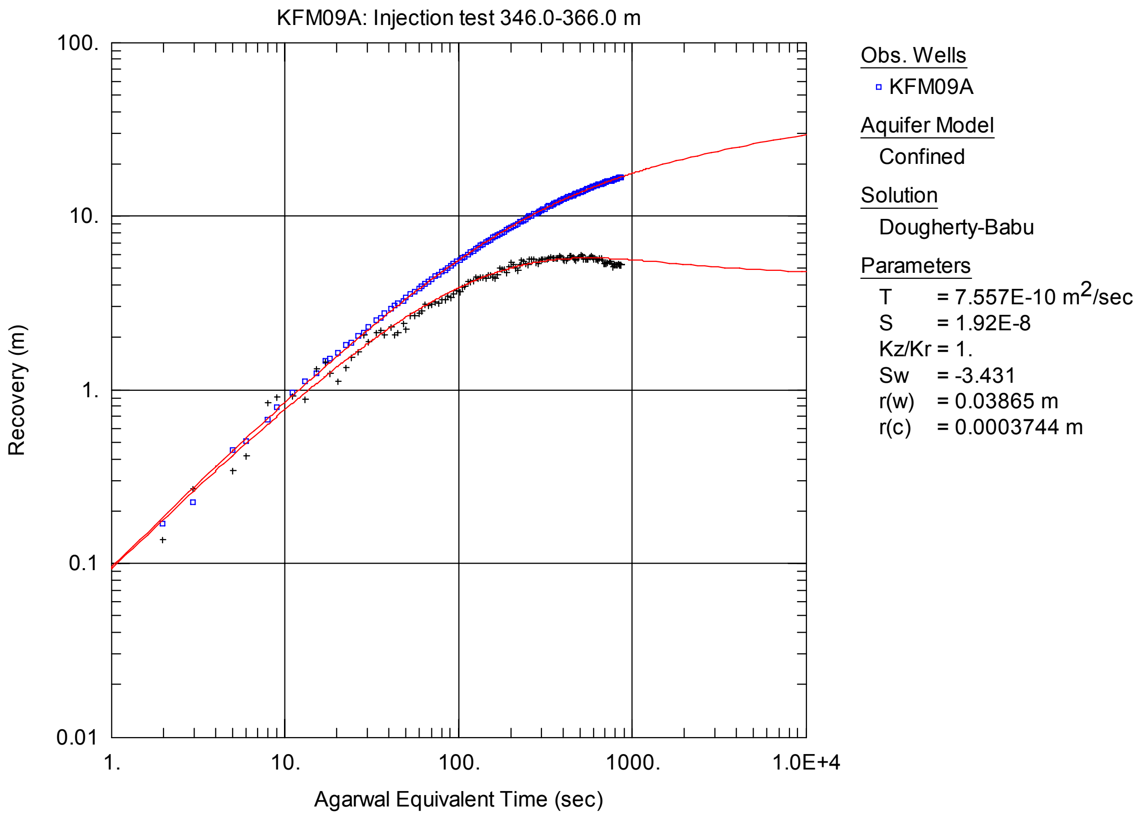


Figure A3-103. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 346.0-366.0 m in KFM09A.*

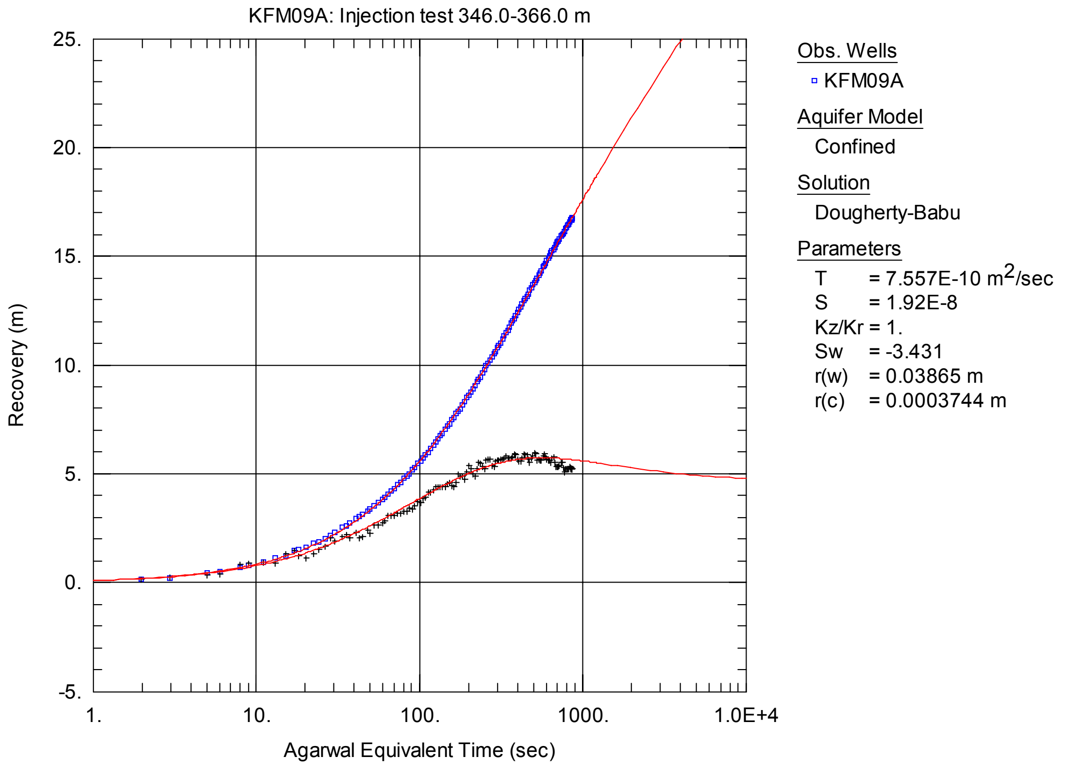


Figure A3-104. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 346.0-366.0 m in KFM09A.*

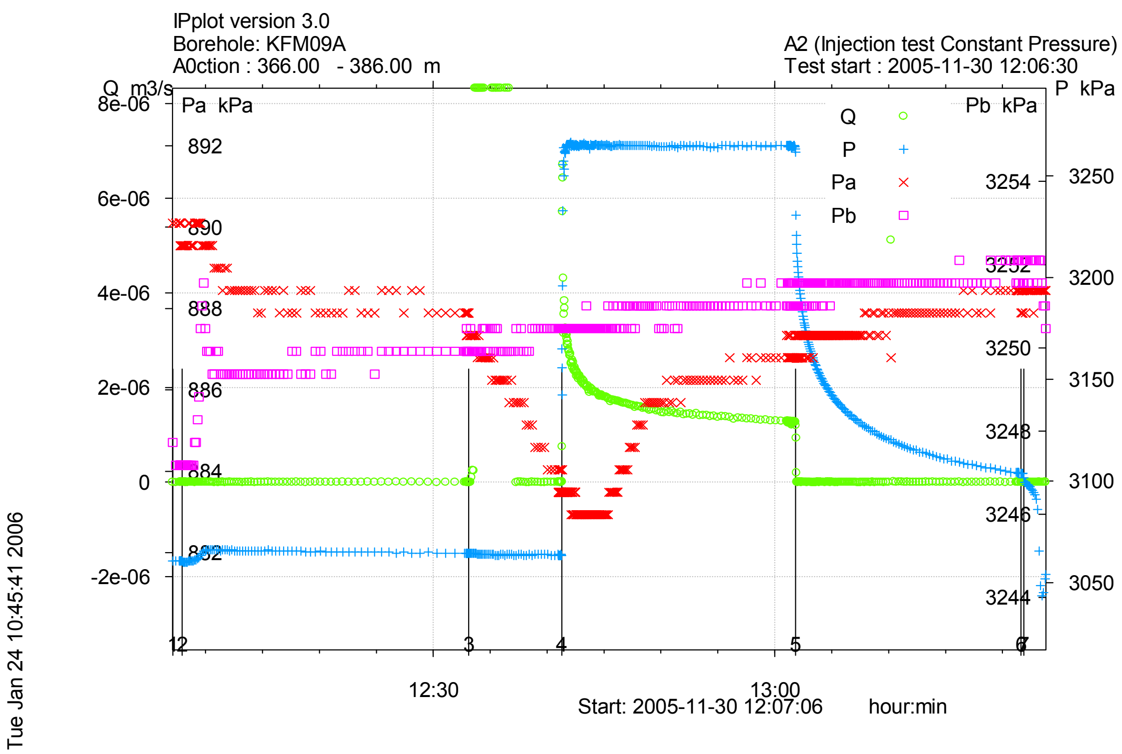


Figure A3-105. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 366.0-386.0 m in borehole KFM09A.*

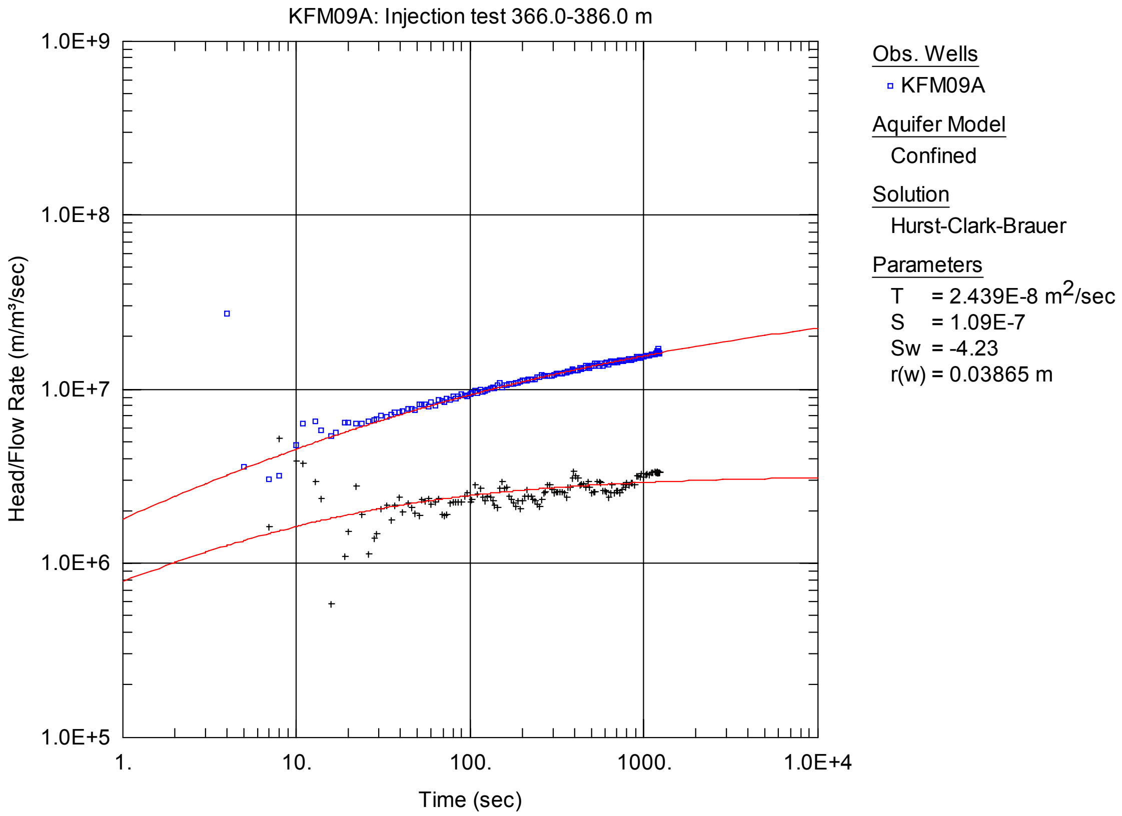


Figure A3-106. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 366.0-386.0 m in KFM09A.*

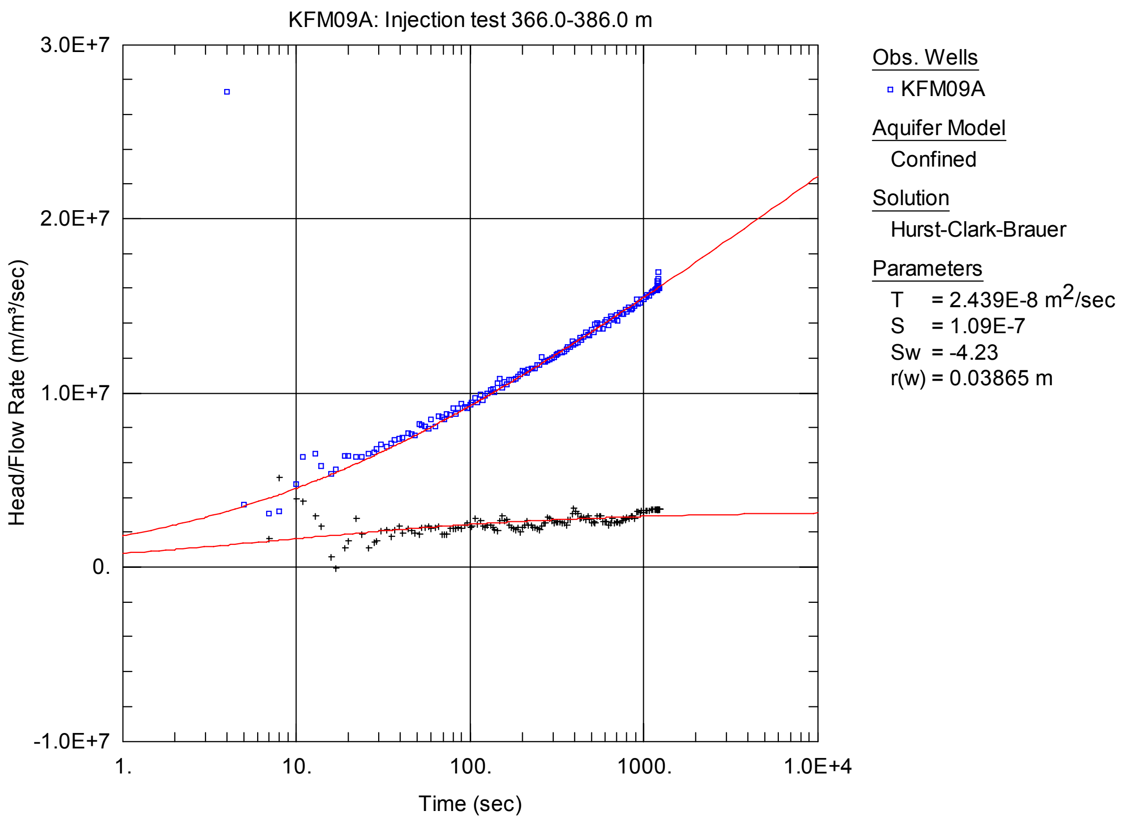


Figure A3-107. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 366.0-386.0 m in KFM09A.*

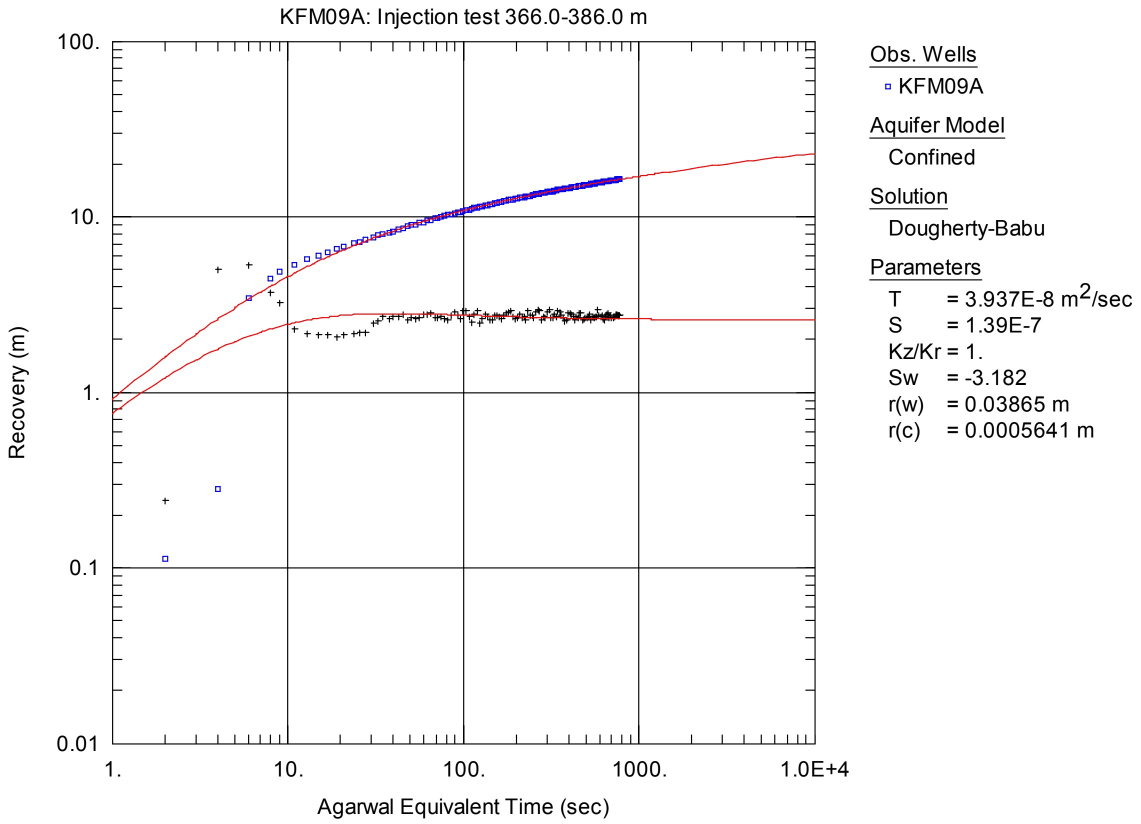


Figure A3-108. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 366.0-386.0 m in KFM09A.*

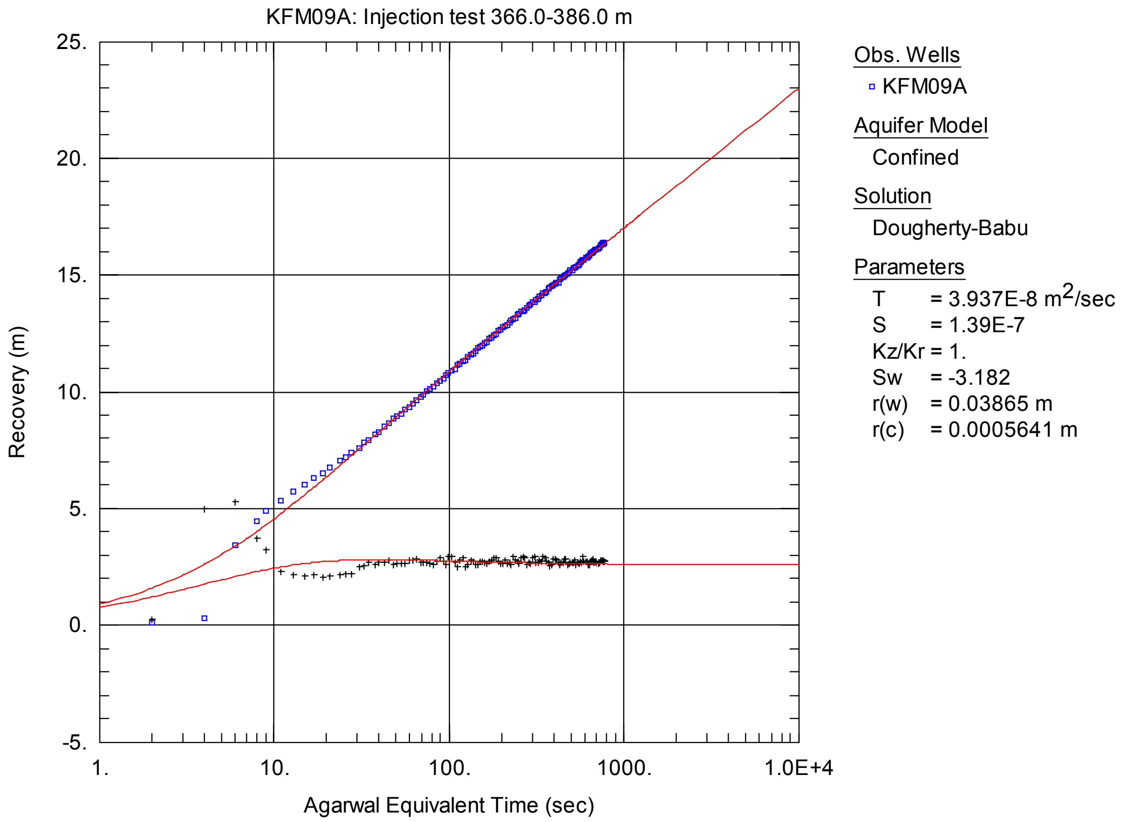


Figure A3-109. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 366.0-386.0 m in KFM09A.*

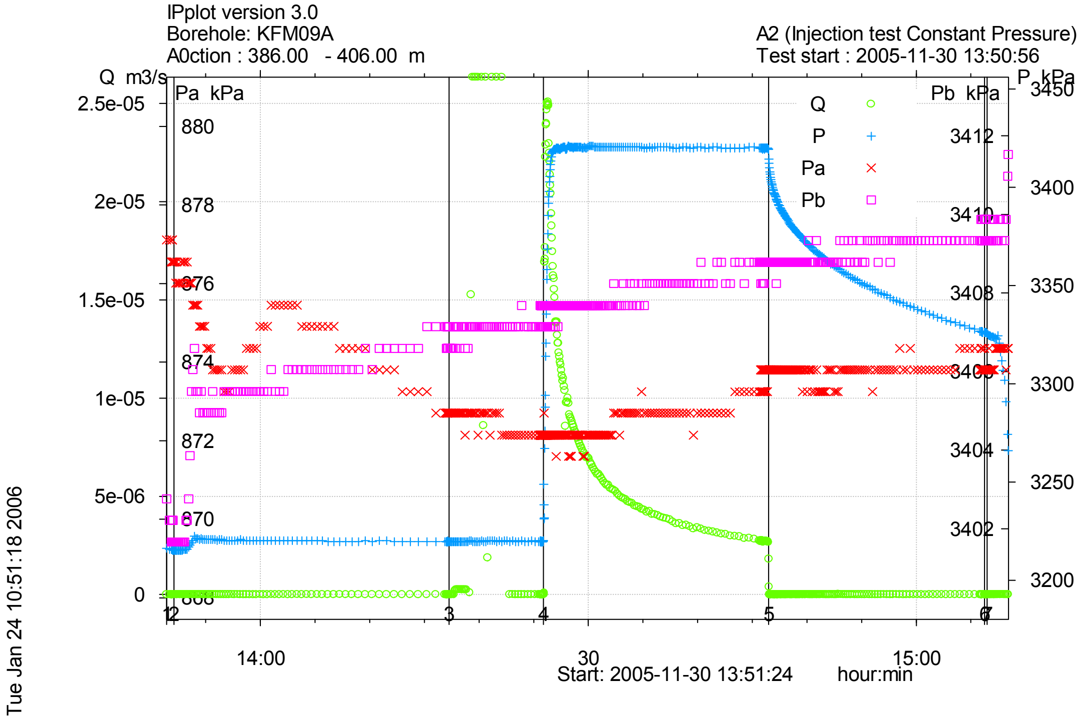


Figure A3-110. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 386.0-406.0 m in borehole KFM09A.

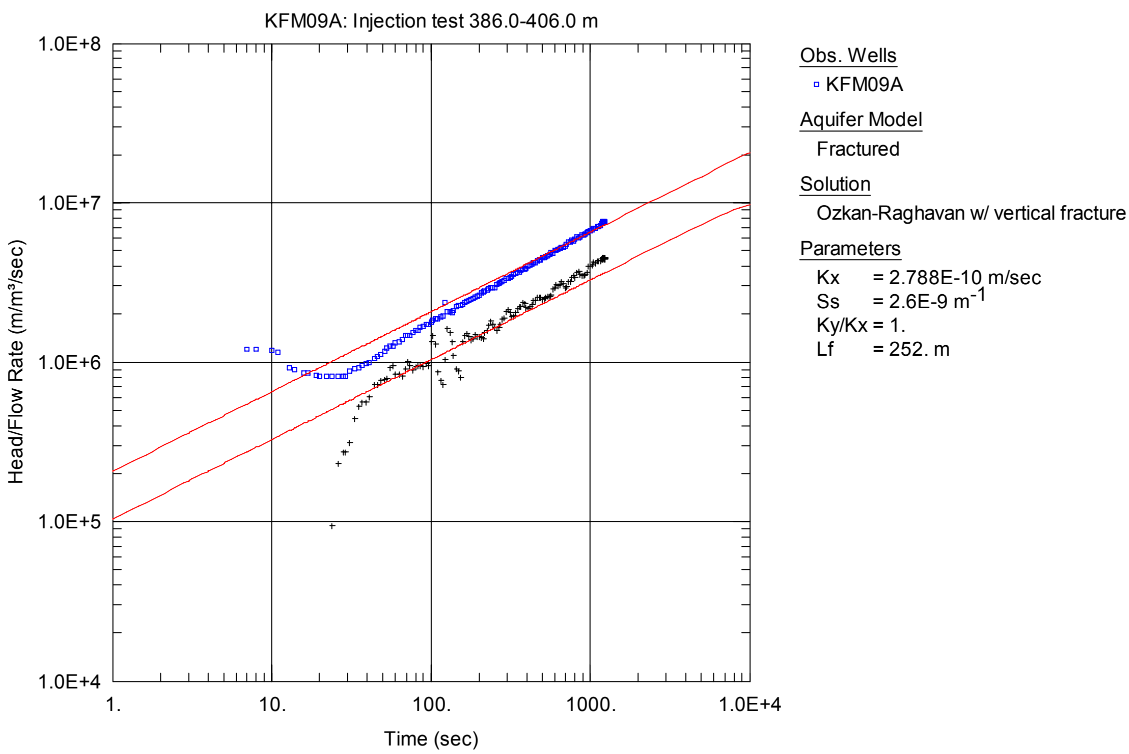


Figure A3-111. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 386.0-406.0 m in KFM09A. No transient evaluation is possible on the injection period.

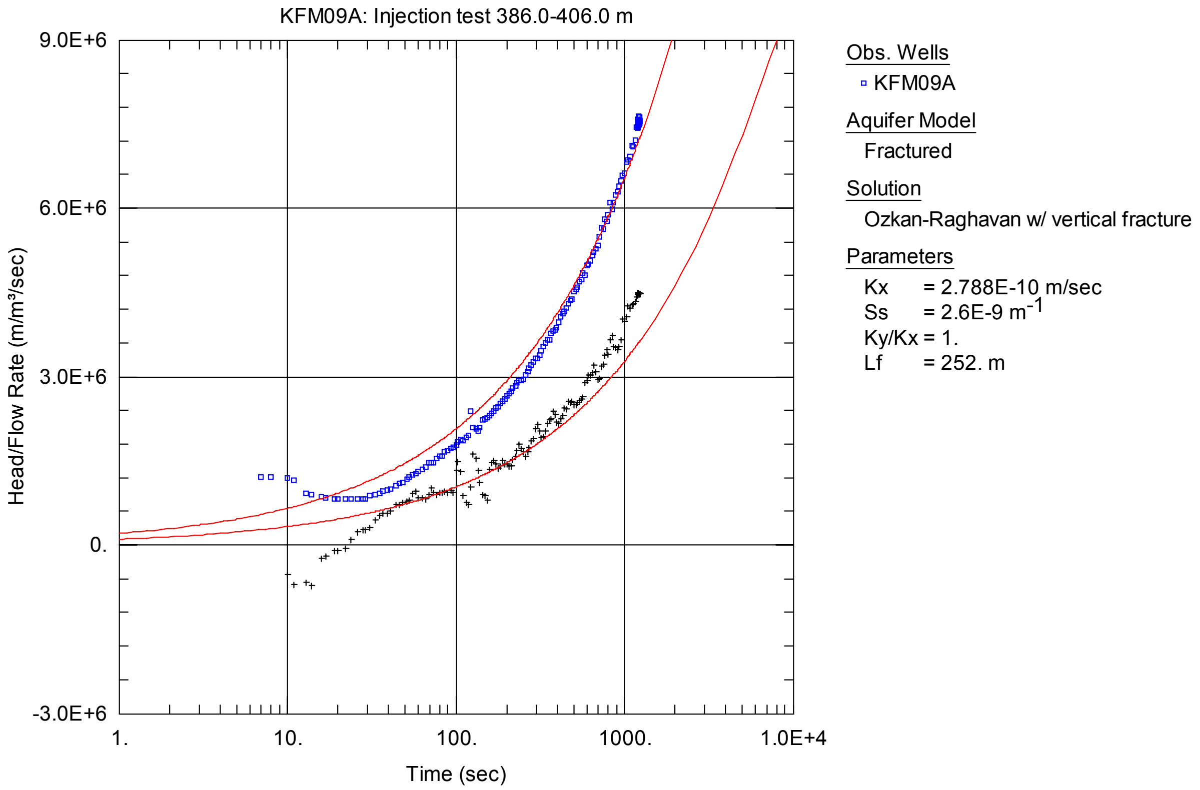


Figure A3-112. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 386.0-406.0 m in KFM09A. No transient evaluation is possible on the injection period.*

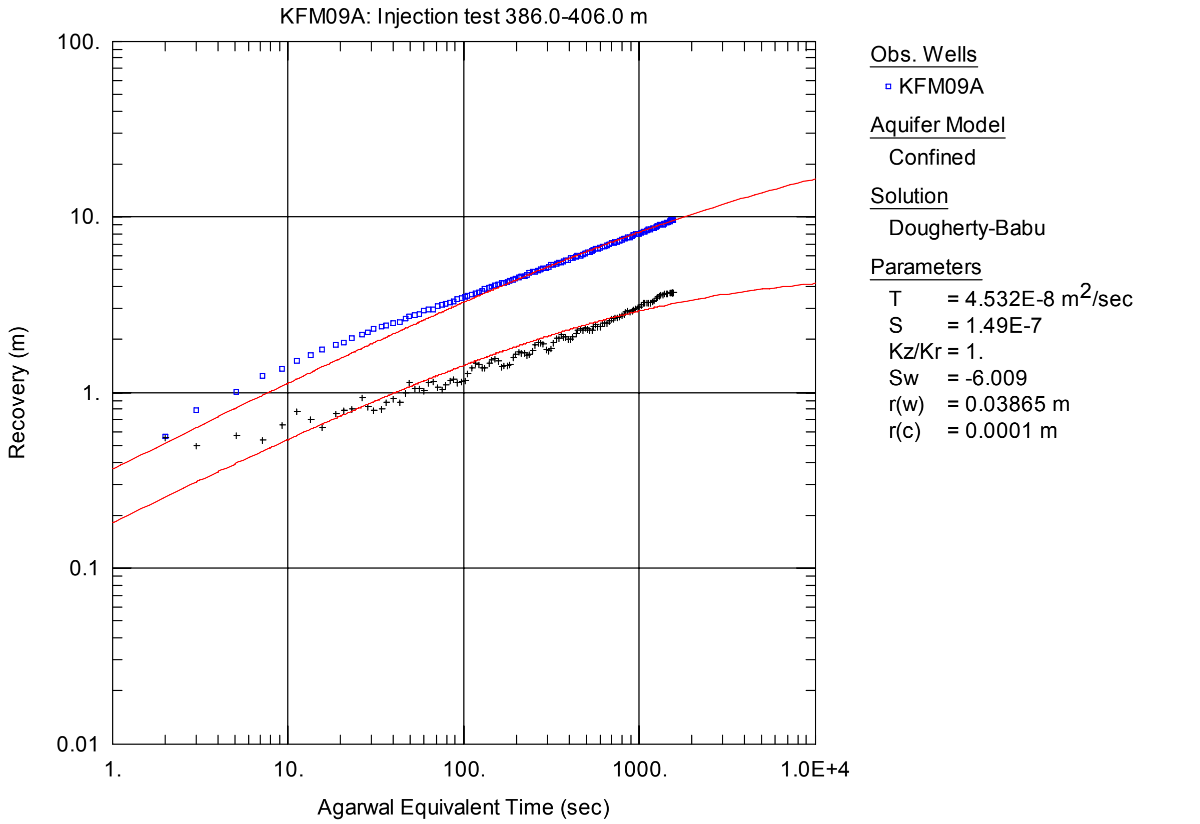


Figure A3-113. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 386.0-406.0 m in KFM09A.*

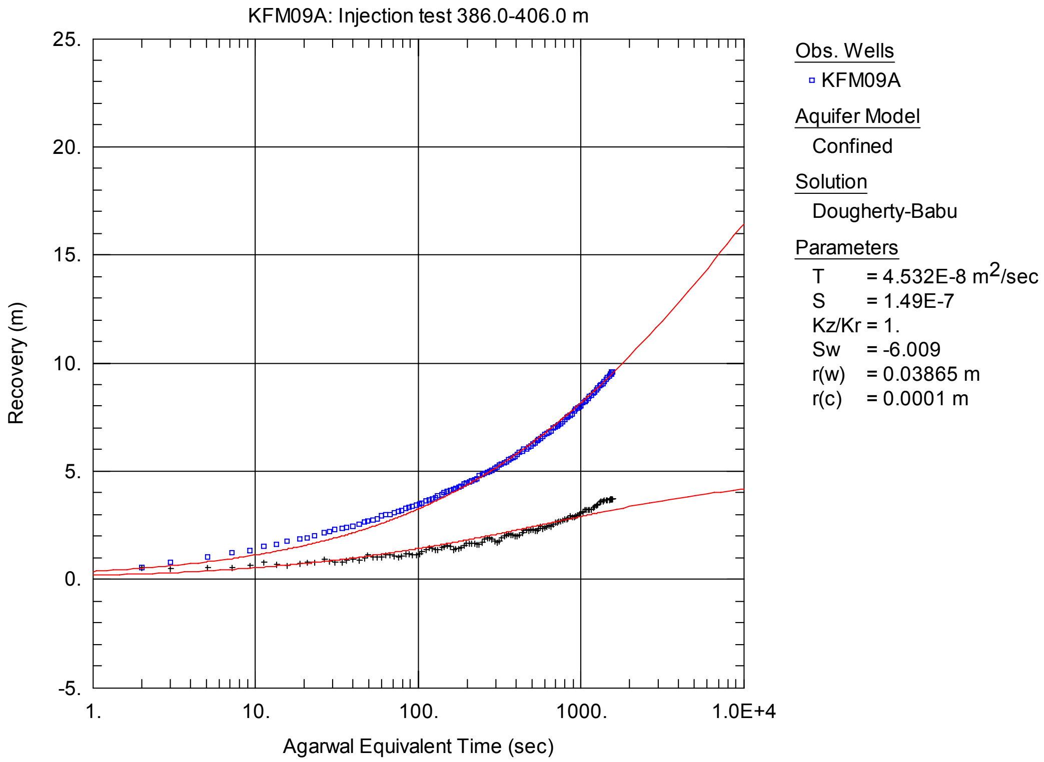


Figure A3-114. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in 386.0-406.0 m in KFM09A.*

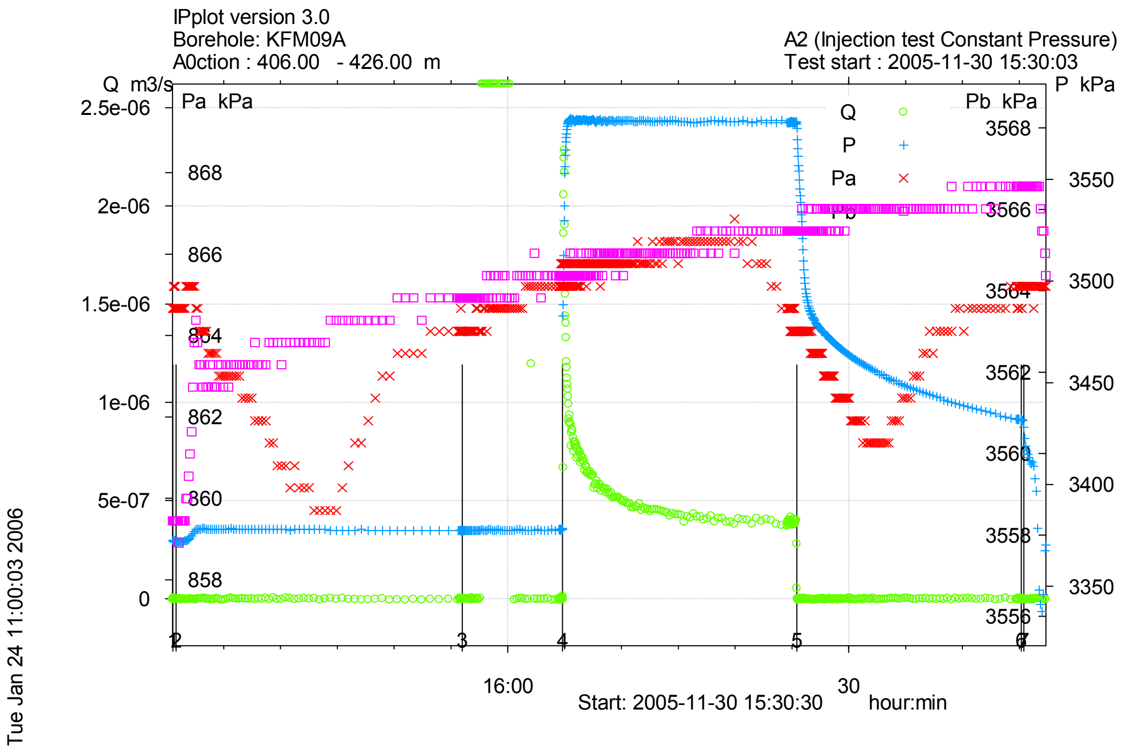


Figure A3-115. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 406.0-426.0 m in borehole KFM09A.*

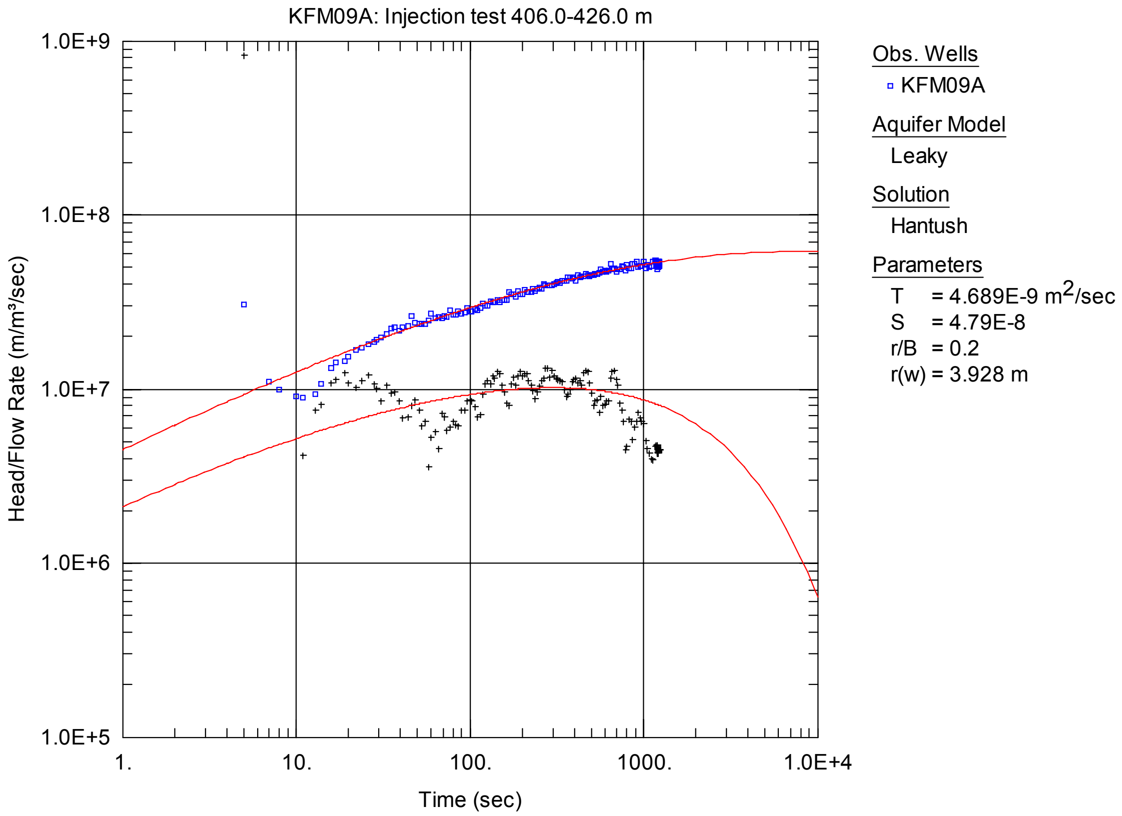


Figure A3-116. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 406.0-426.0 m in KFM09A.*

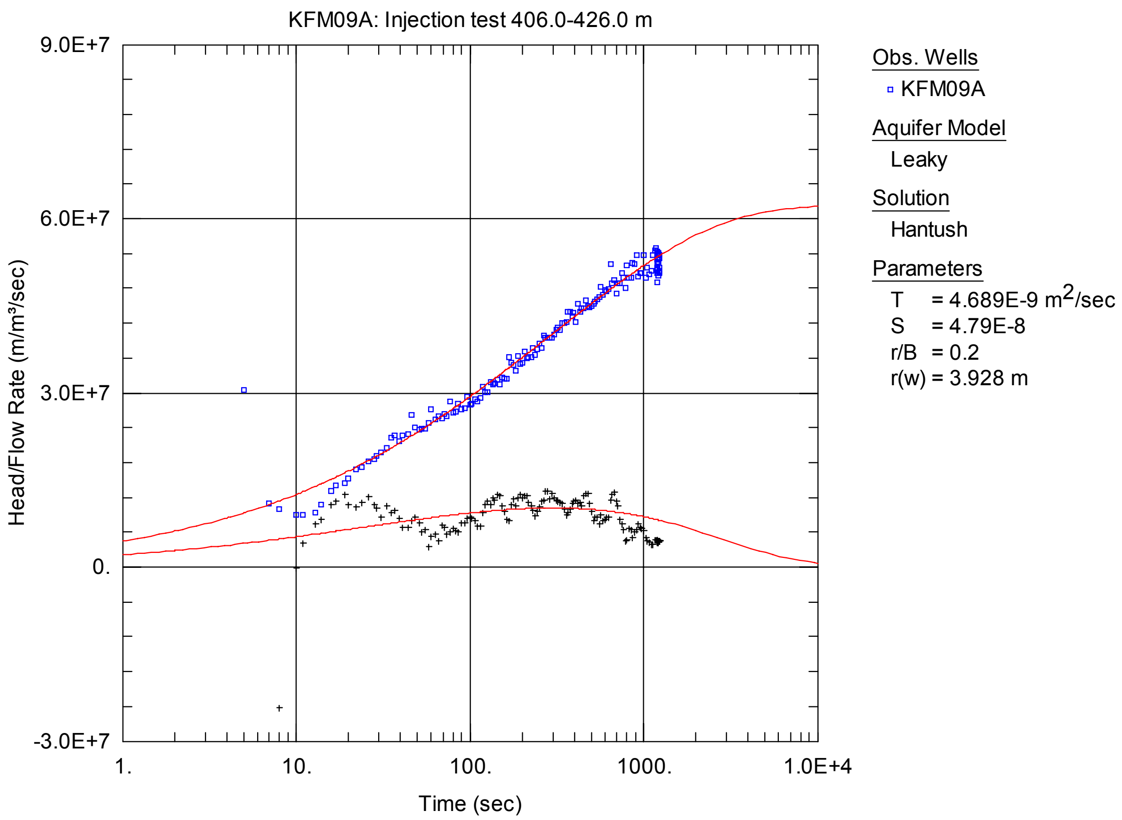


Figure A3-117. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 406.0-426.0 m in KFM09A.*

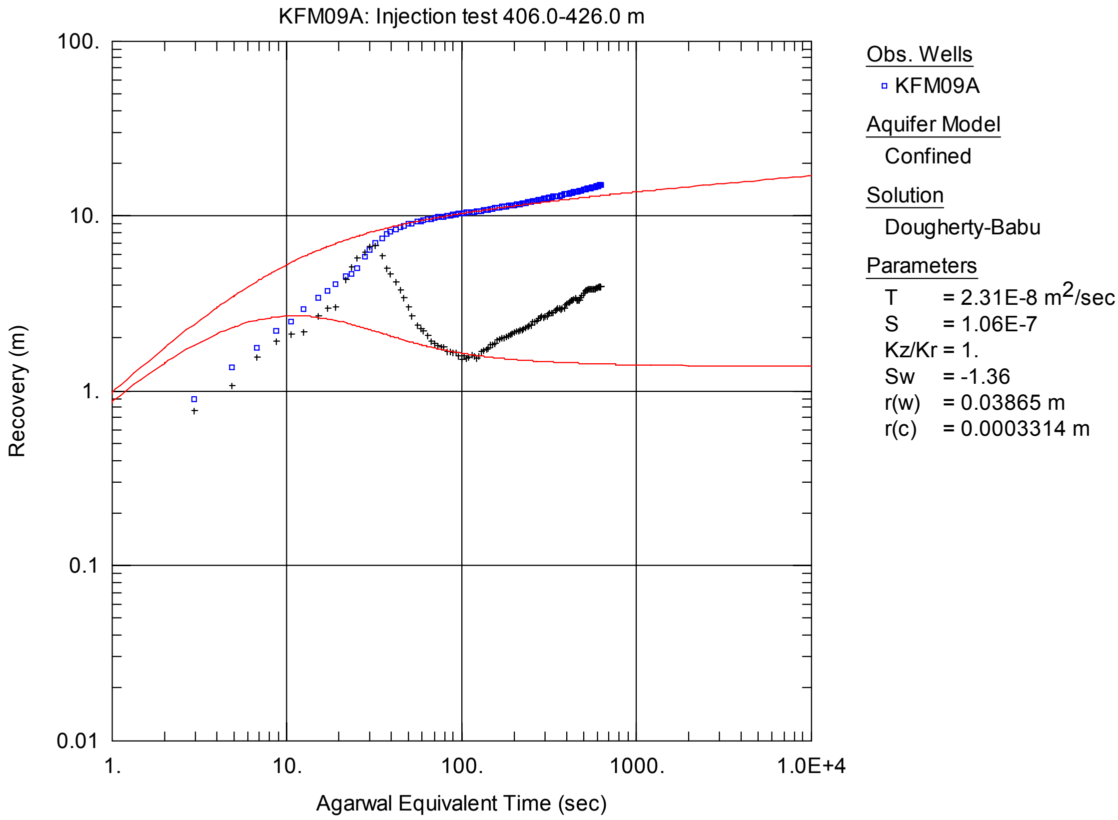


Figure A3-118. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 406.0-426.0 m in KFM09A.*

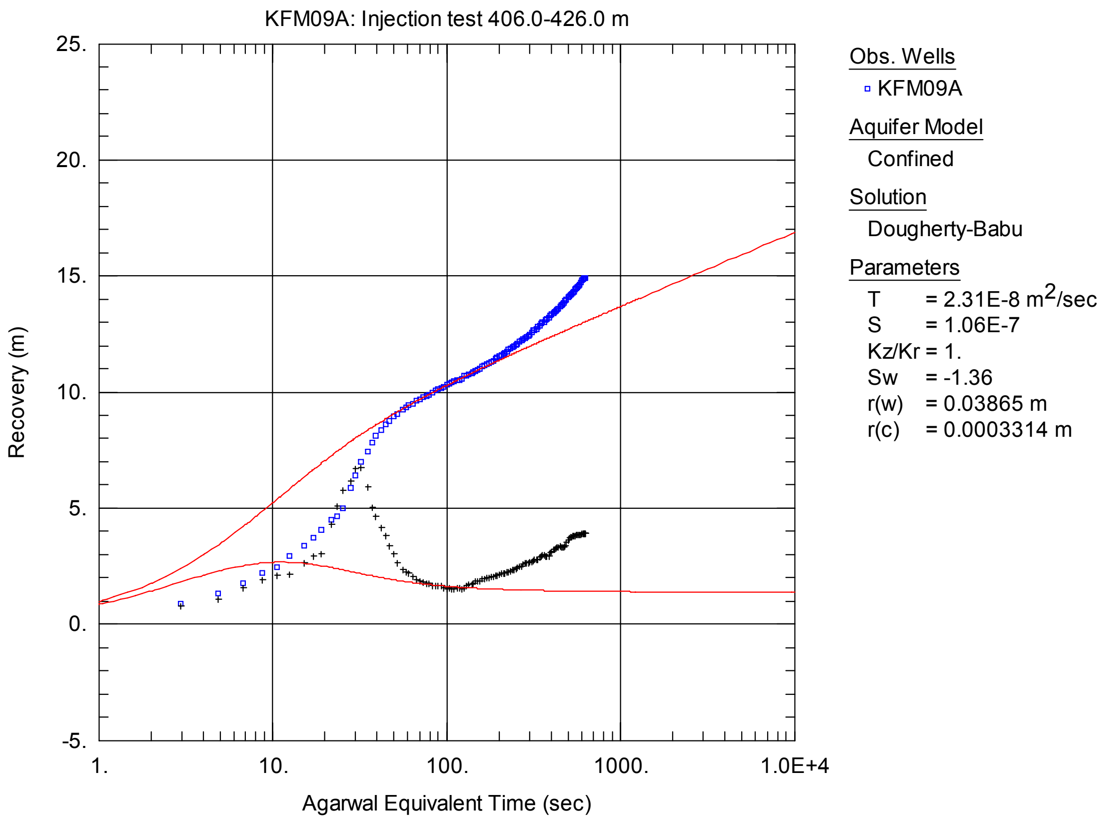


Figure A3-119. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 406.0-426.0 m in KFM09A.*

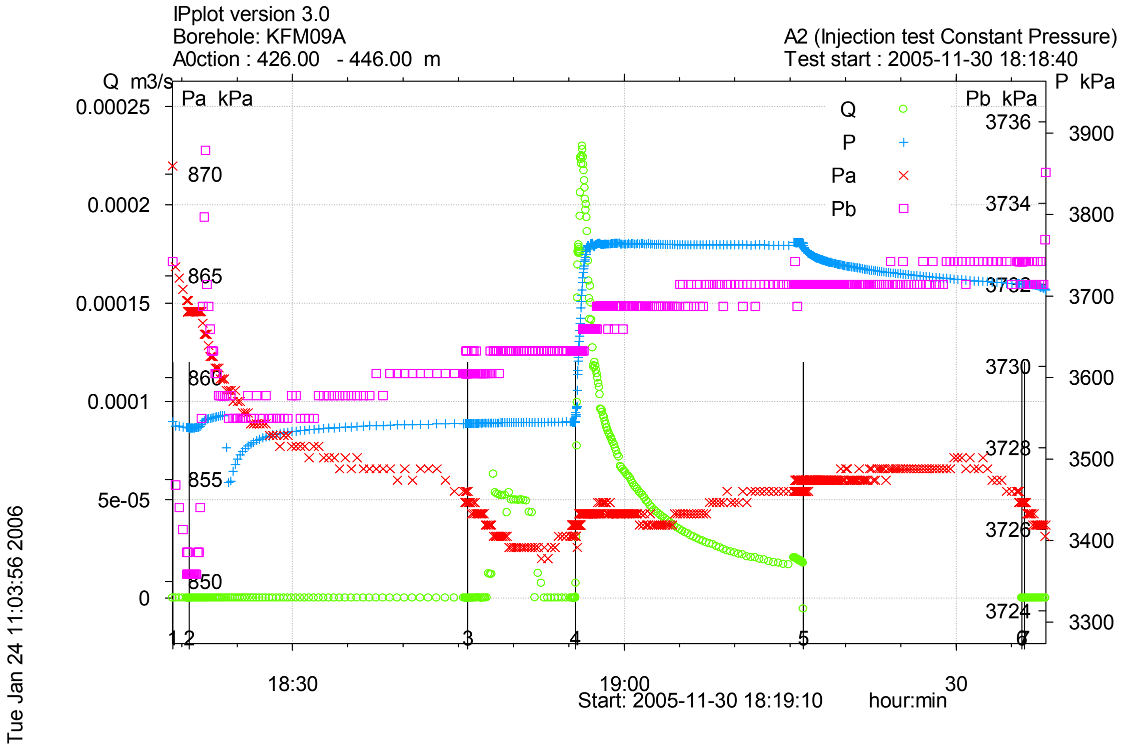


Figure A3-120. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in 426.0-446.0 m in borehole KFM09A.*

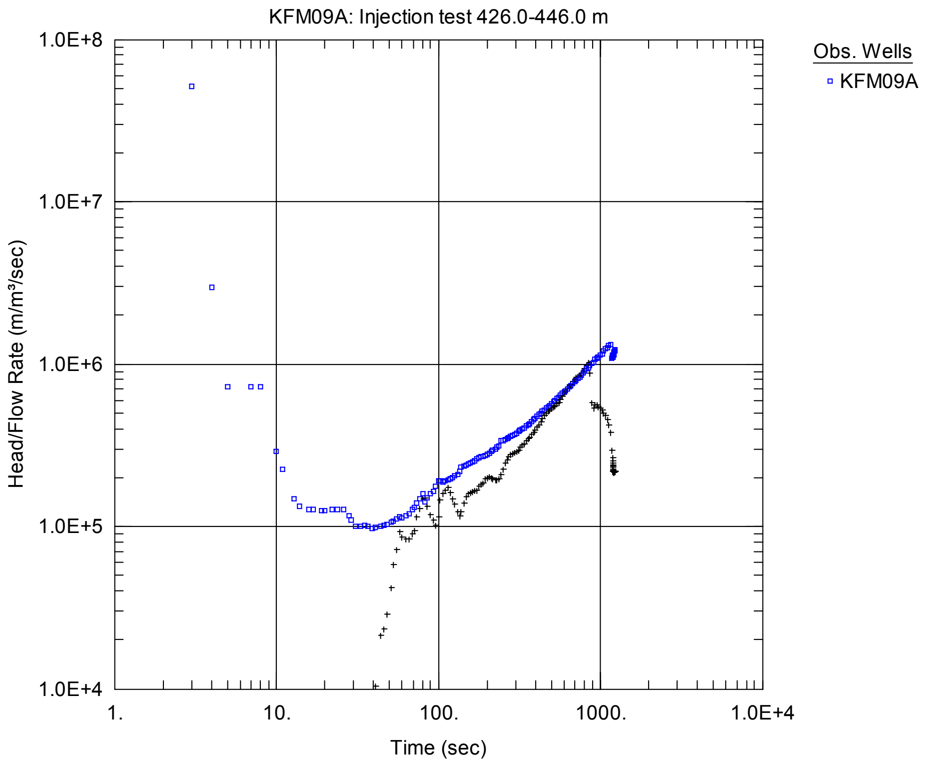


Figure A3-121. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 426.0-446.0 m in KFM09A.*

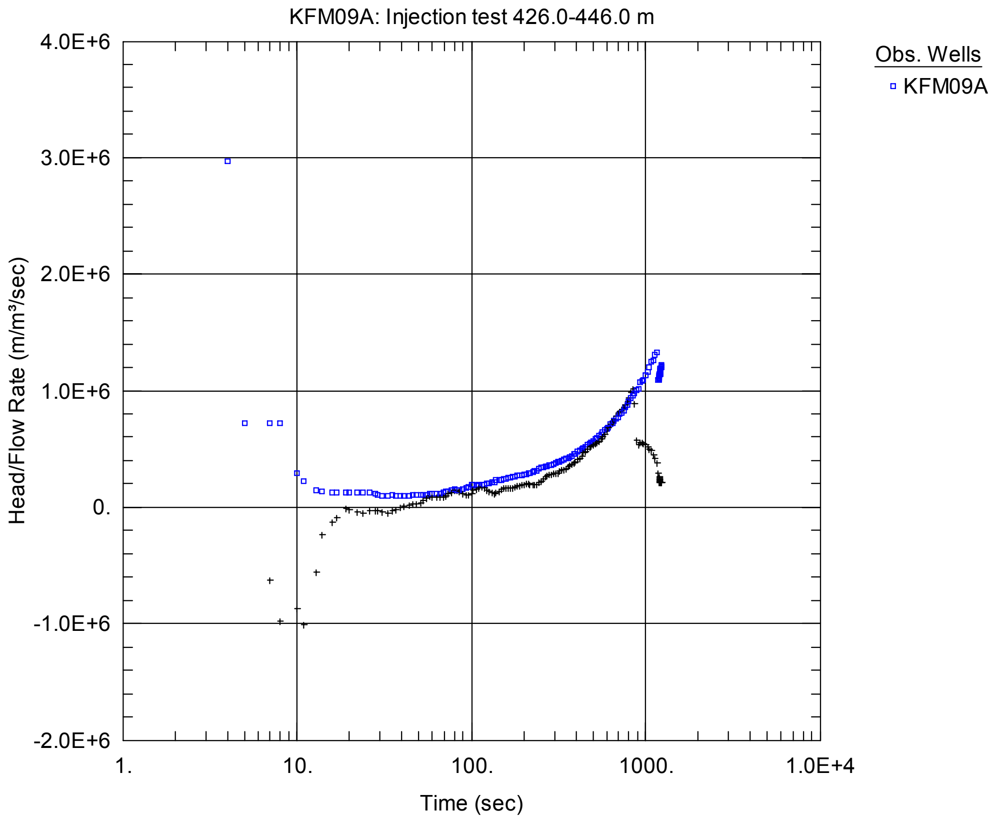


Figure A3-122. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 426.0-446.0 m in KFM09A.*

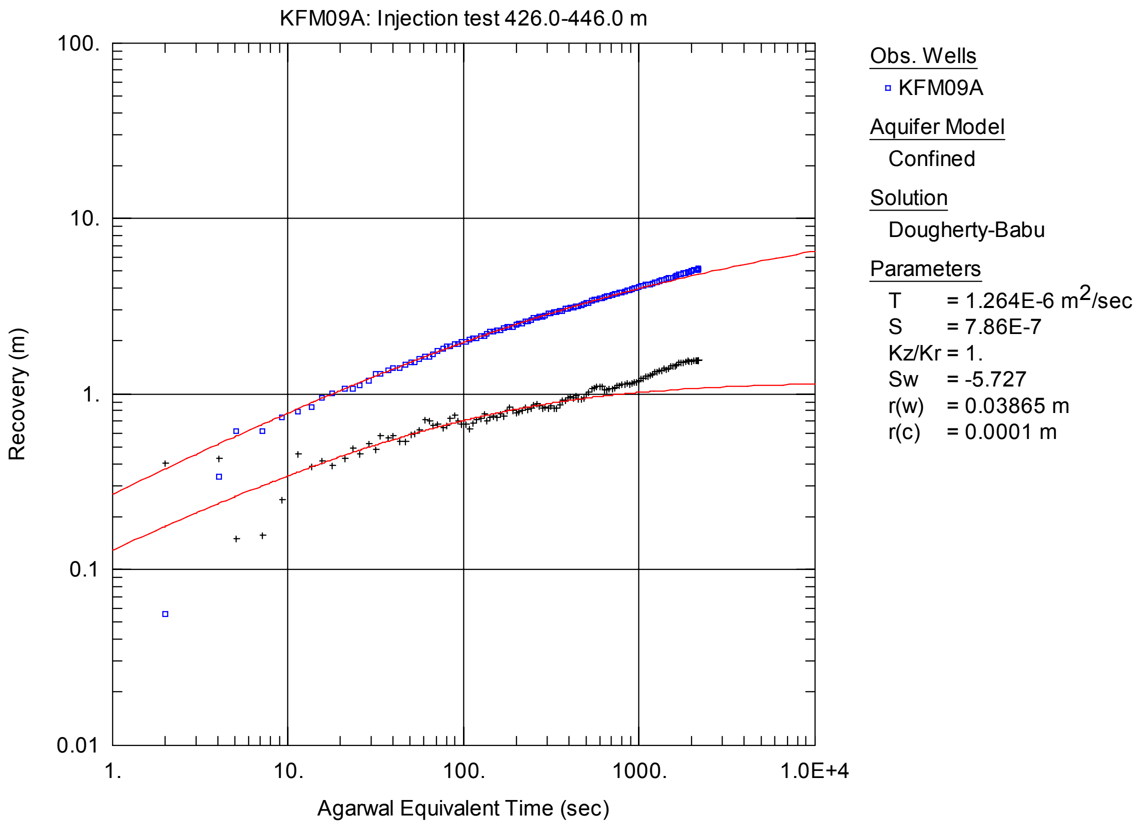


Figure A3-123. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 426.0-446.0 m in KFM09A.*

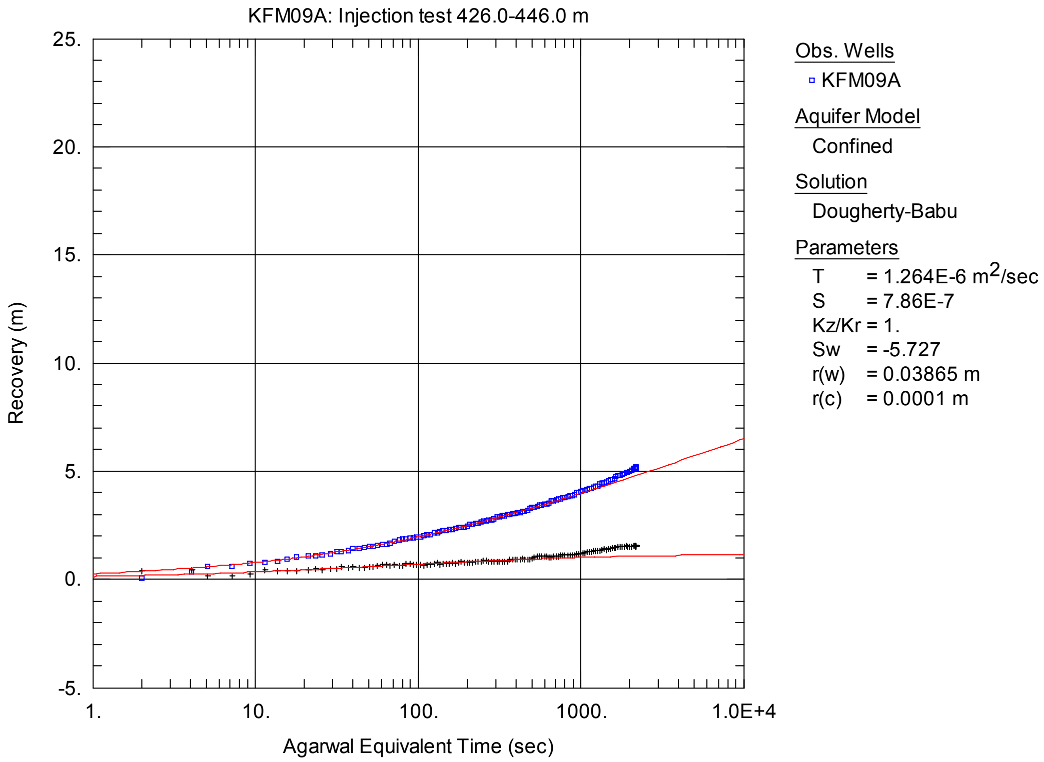


Figure A3-124. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 426.0-446.0 m in KFM09A.*

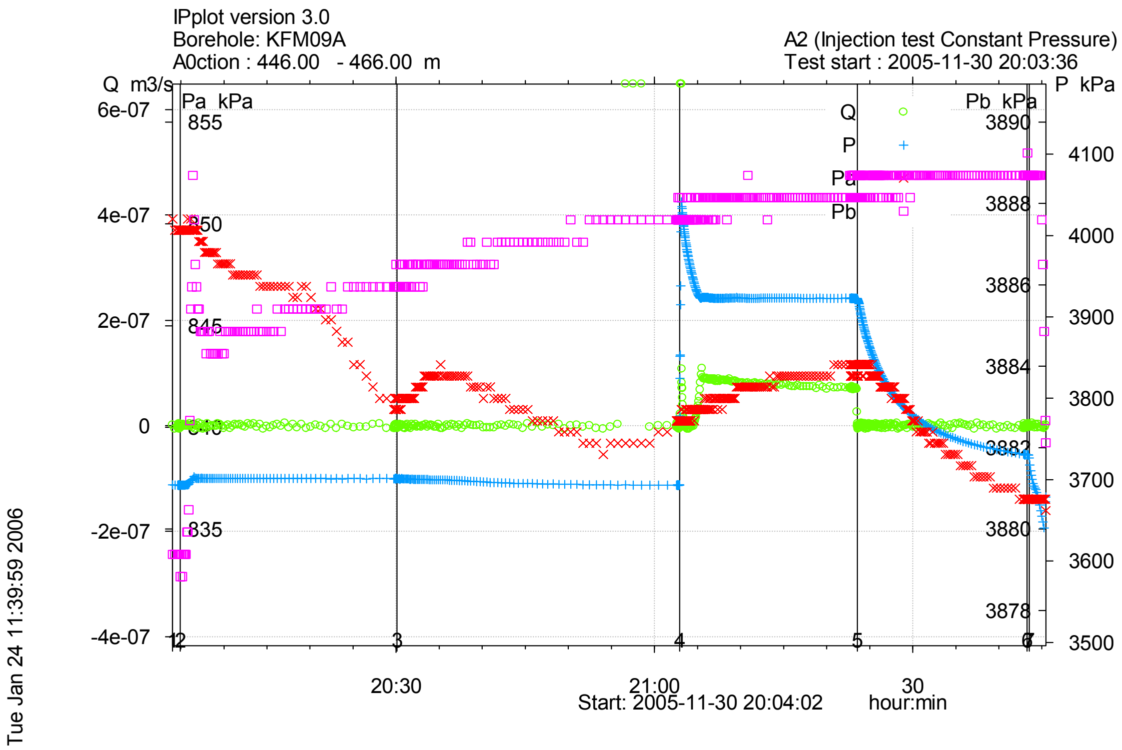


Figure A3-125. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 446.0-466.0 m in borehole KFM09A.*

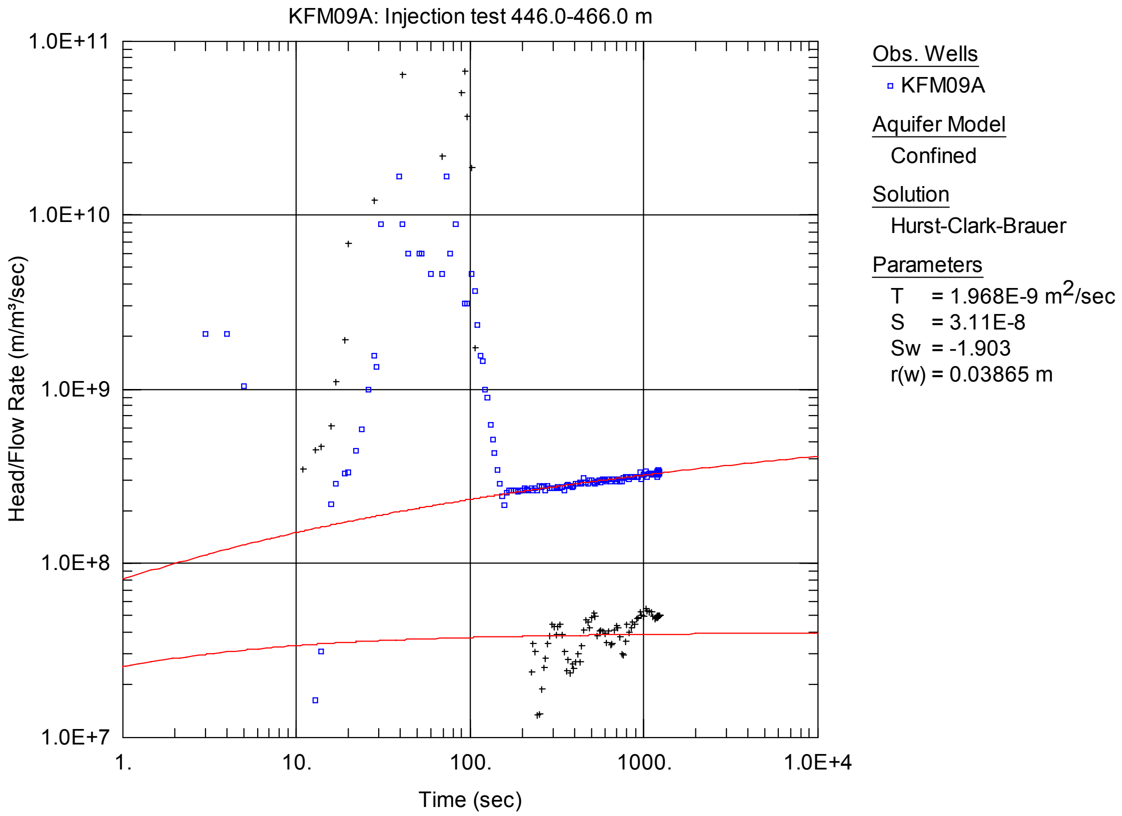


Figure A3-126. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 446.0-466.0 m in KFM09A.*

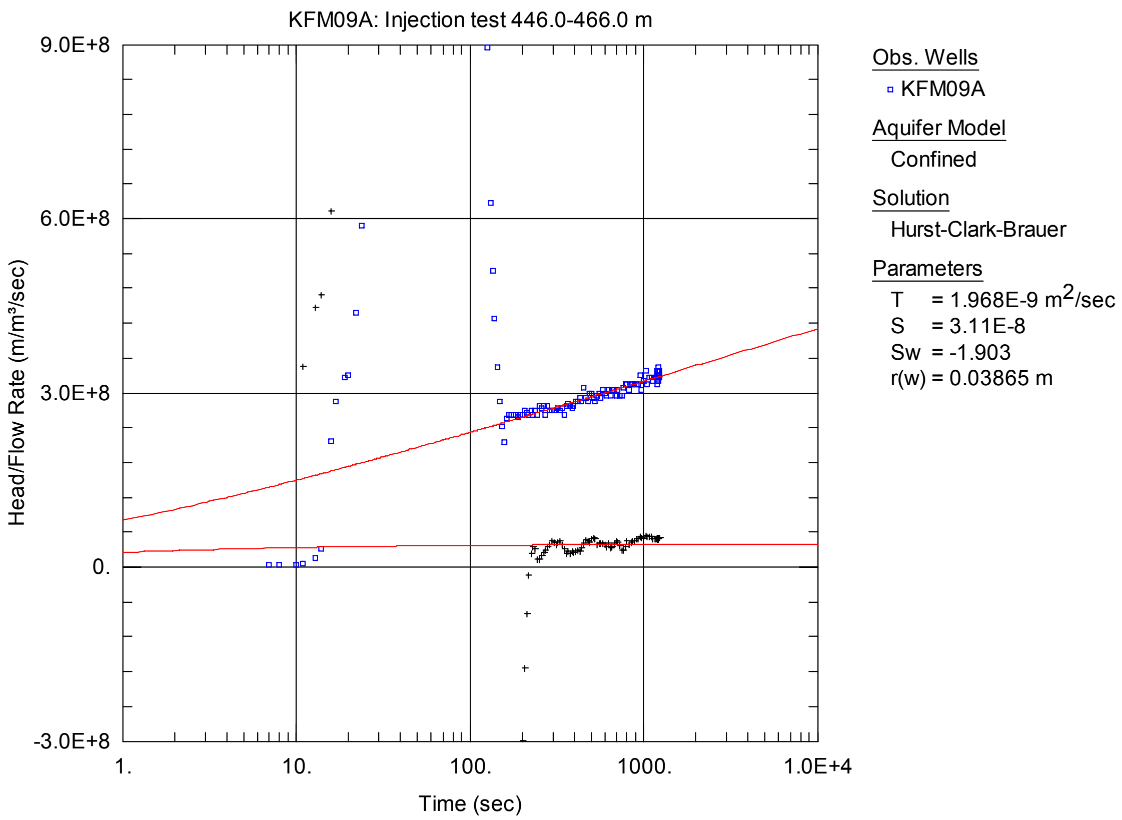


Figure A3-127. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 446.0-466.0 m in KFM09A.*

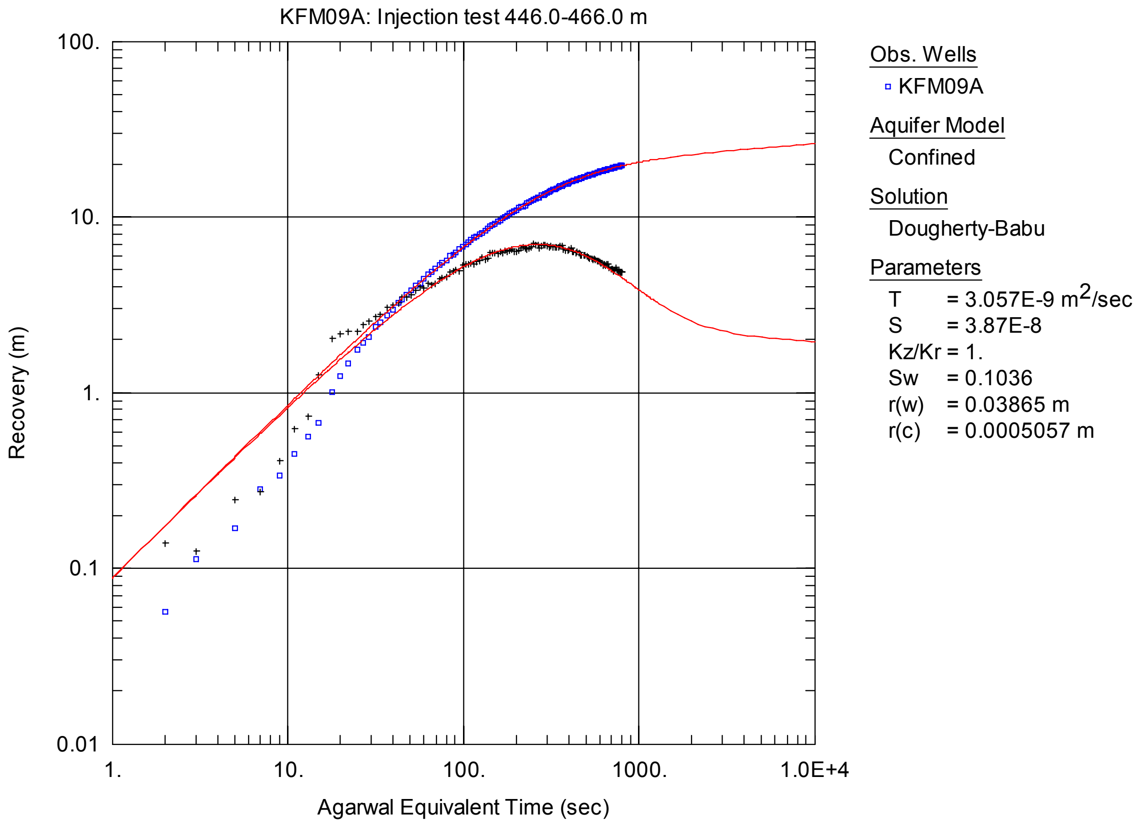


Figure A3-128. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in 446.0-466.0 m in KFM09A.*

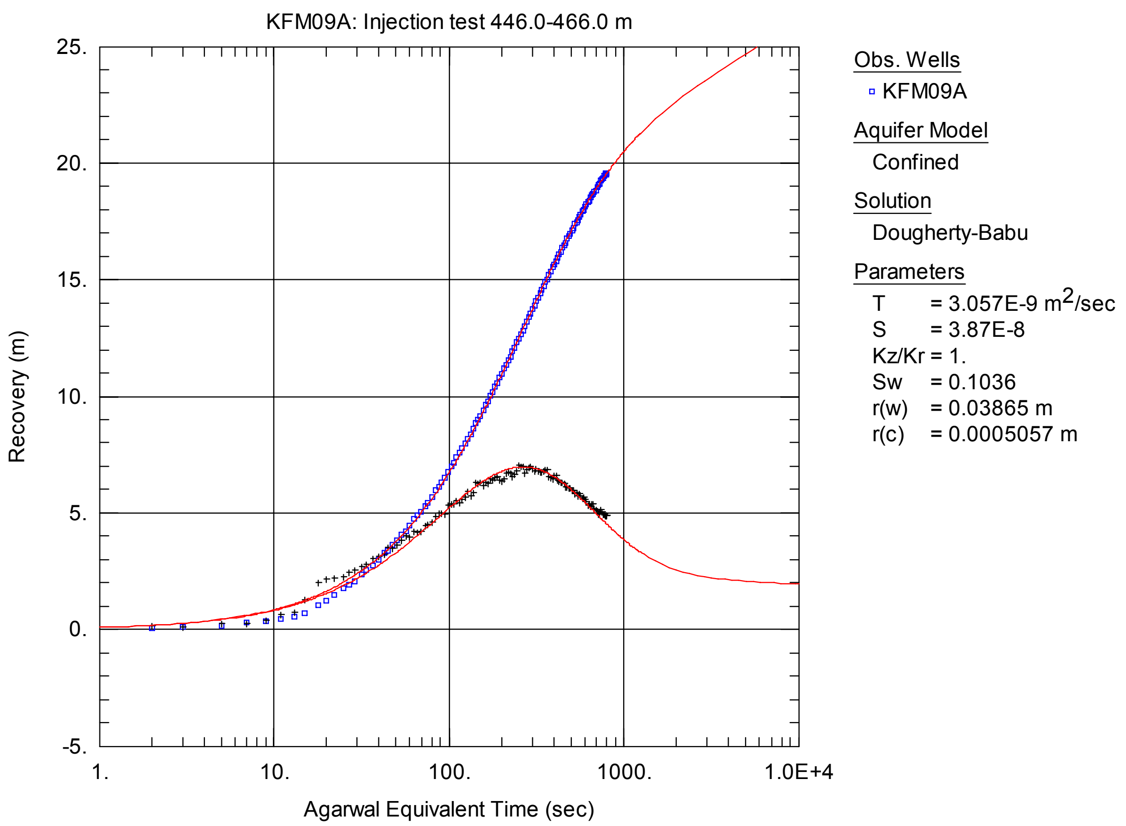


Figure A3-129. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 446.0-466.0 m in KFM09A.*

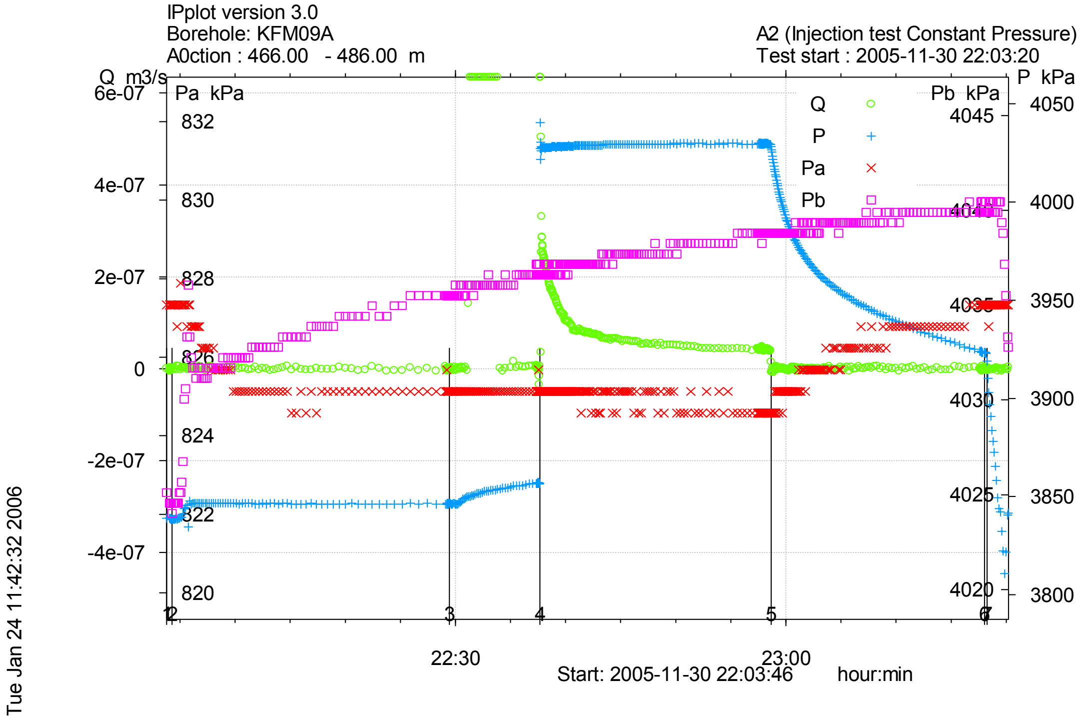


Figure A3-130. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 466.0-486.0 m in borehole KFM09A.*

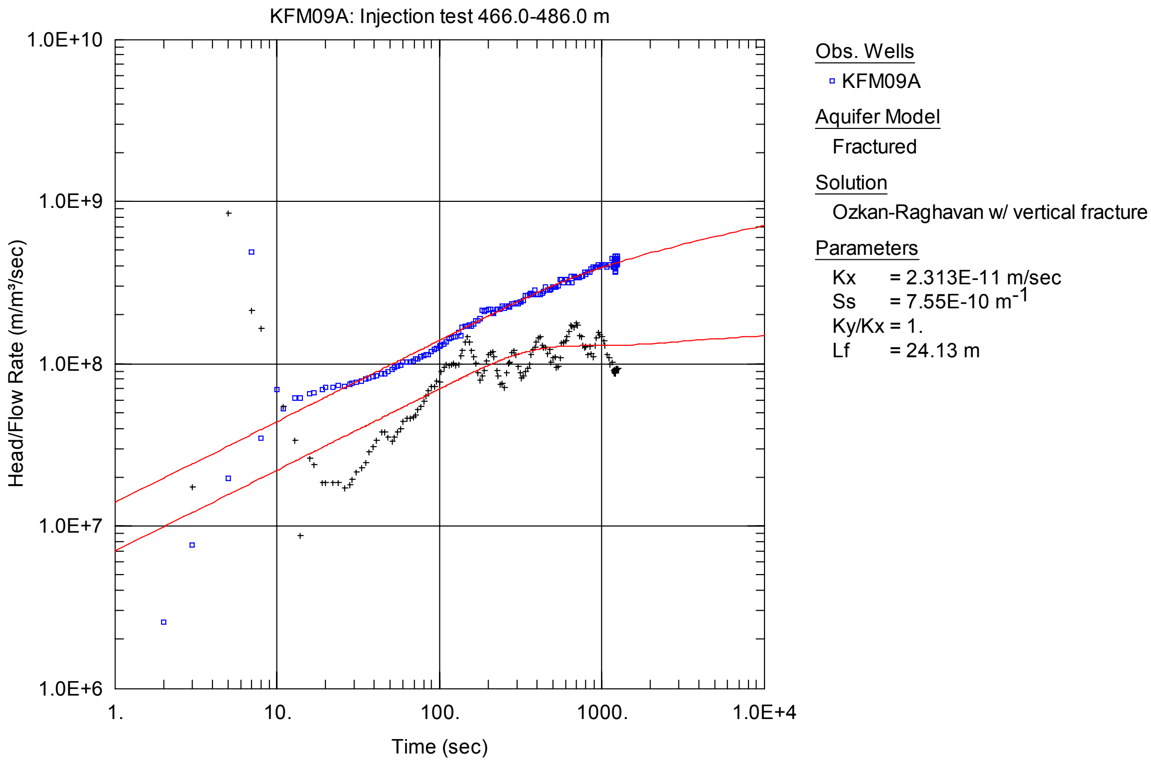


Figure A3-131. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 466.0-486.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

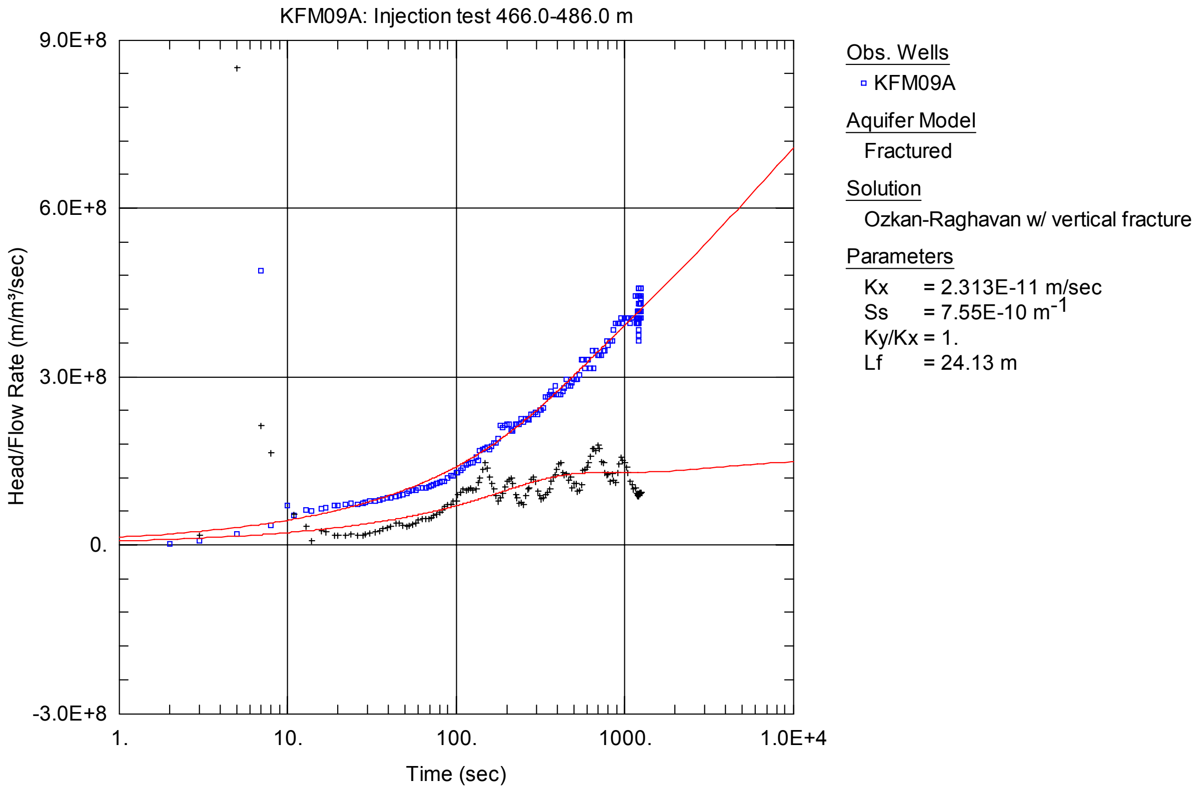


Figure A3-132. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 466.0-486.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

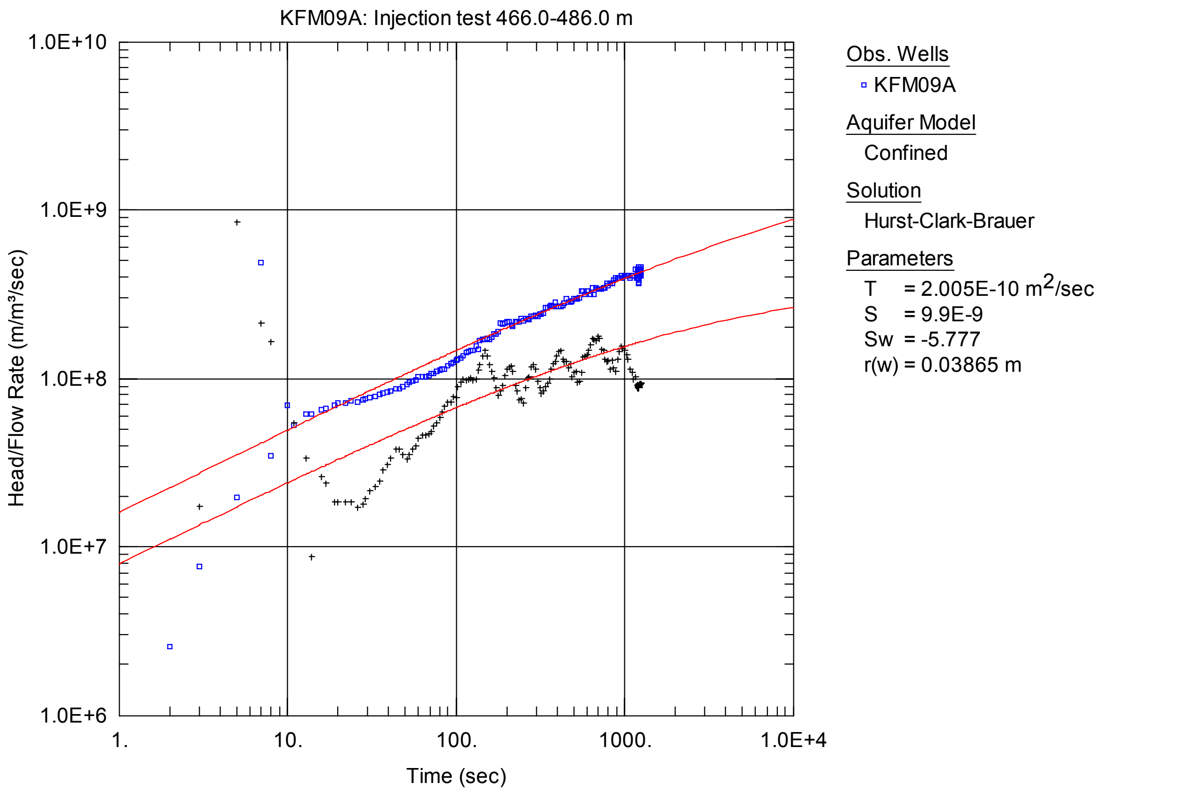


Figure A3-133. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 466.0-486.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for pseudo-radial flow.*

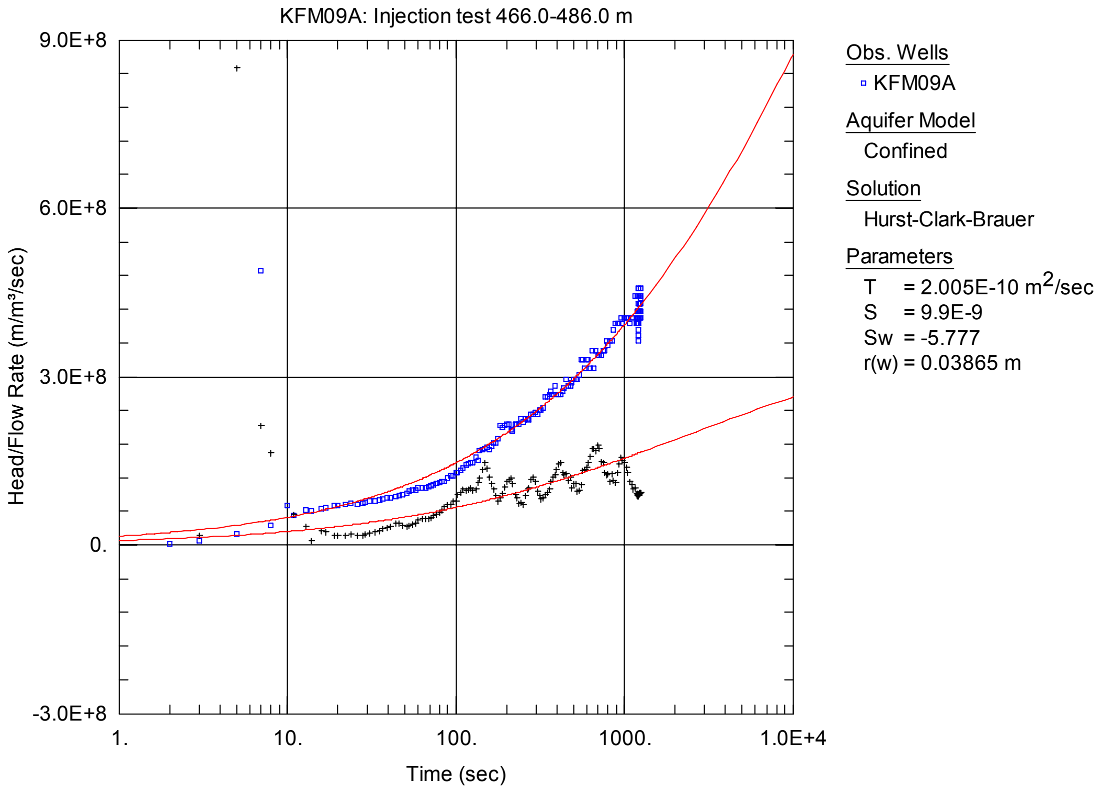


Figure A3-134. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 466.0-486.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for pseudo-radial flow.*

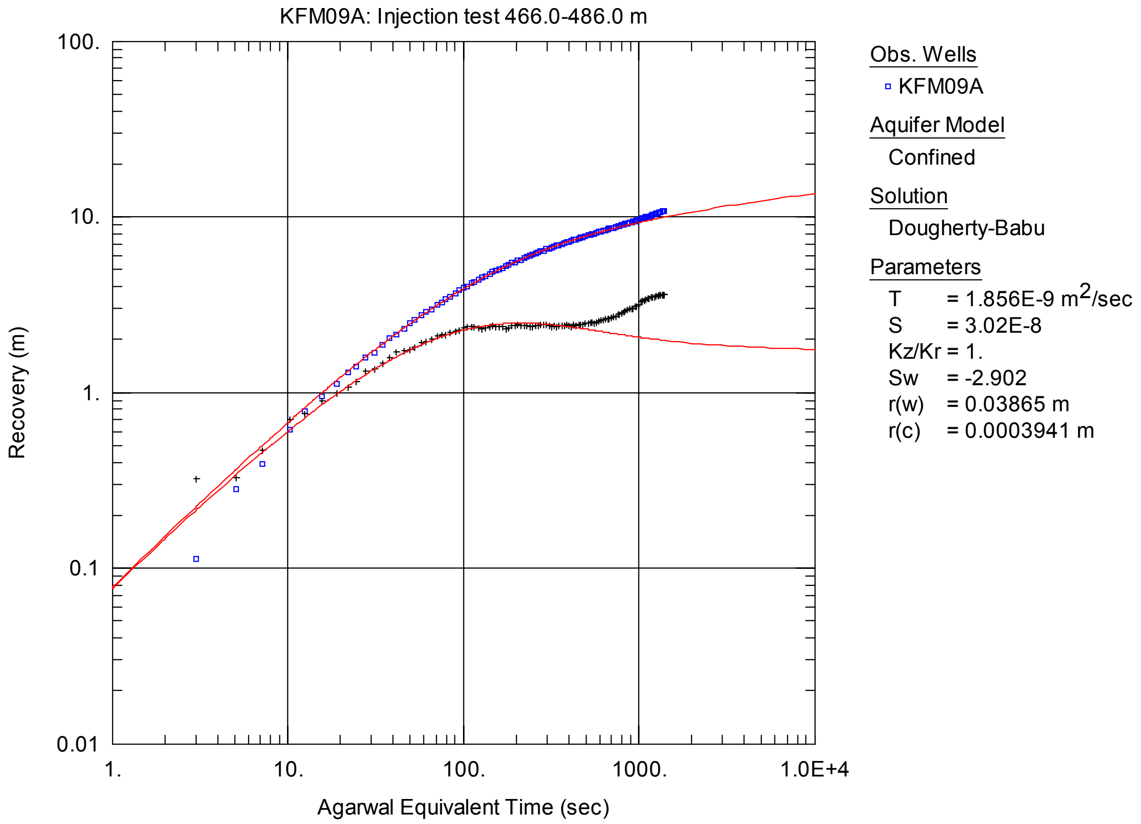


Figure A3-135. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 466.0-486.0 m in KFM09A.*

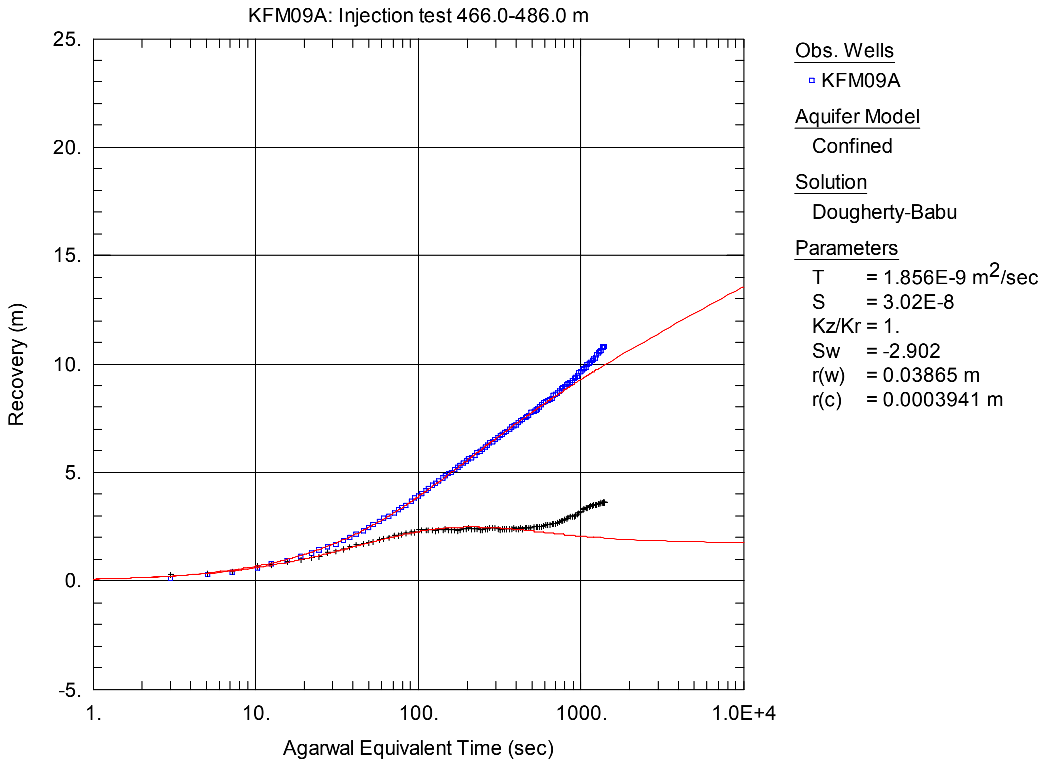


Figure A3-136. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 466.0-486.0 m in KFM09A.*

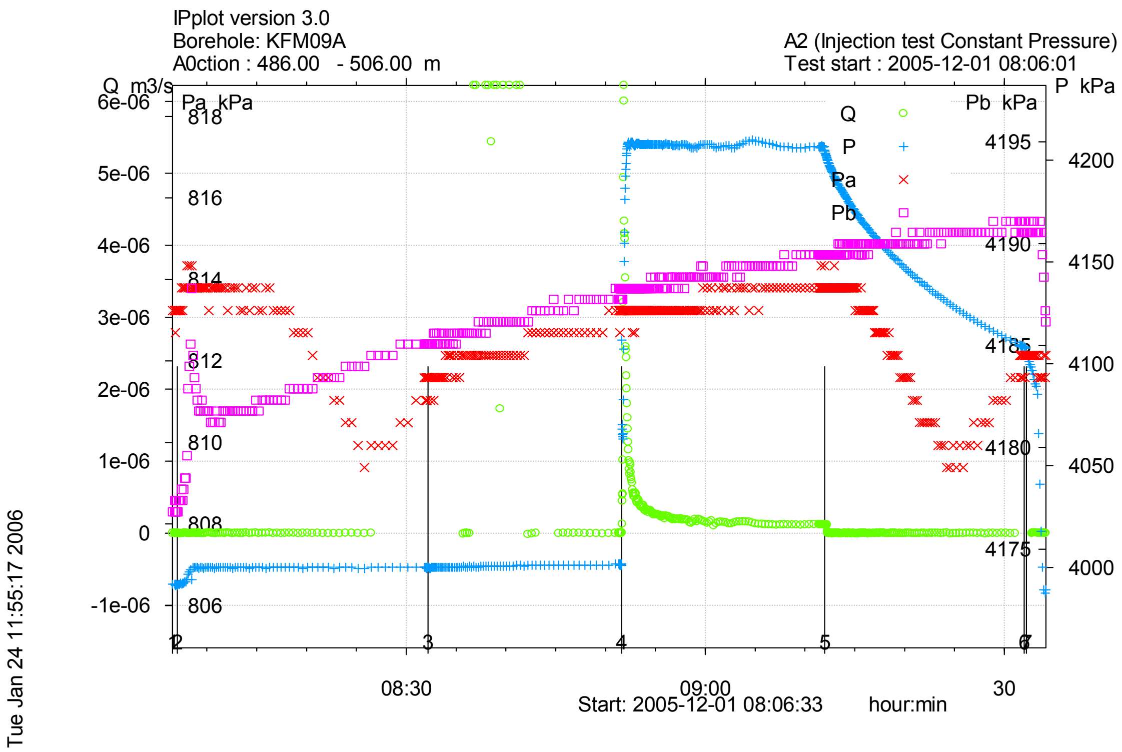


Figure A3-137. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 486.0-506.0 m in borehole KFM09A.*

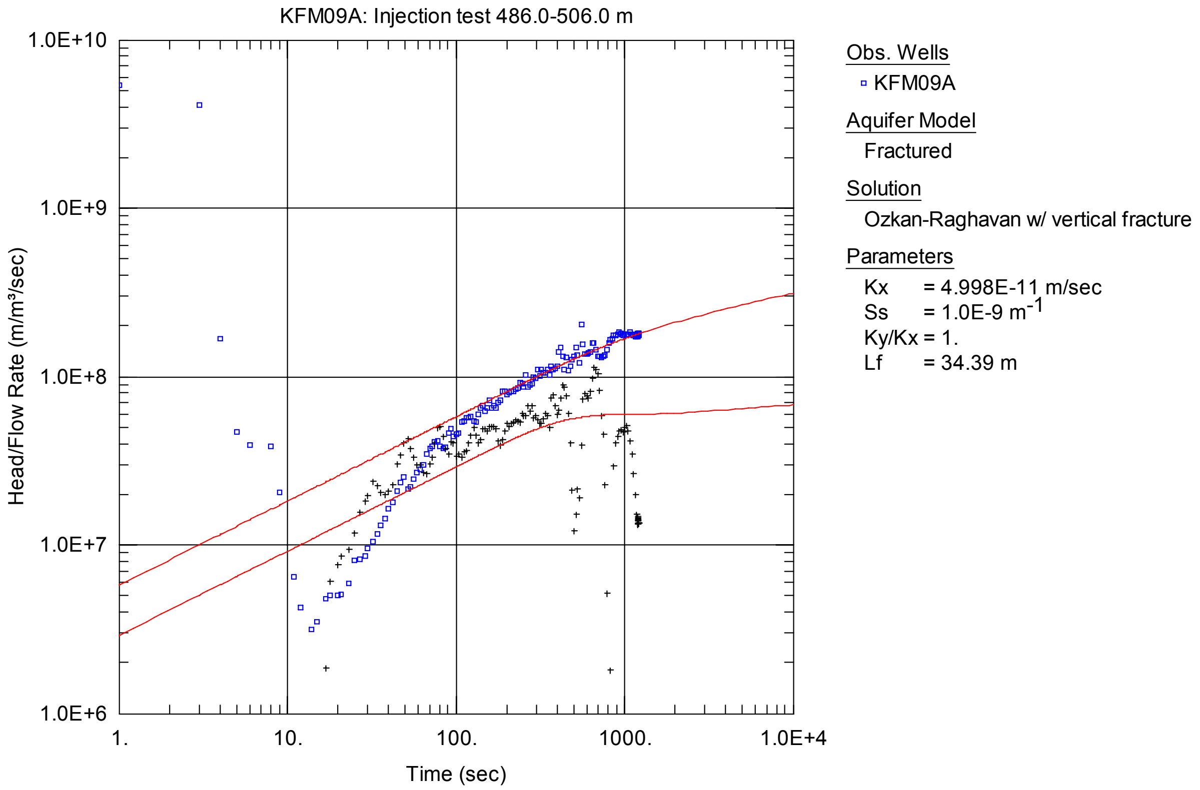


Figure A3-138. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 486.0-506.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

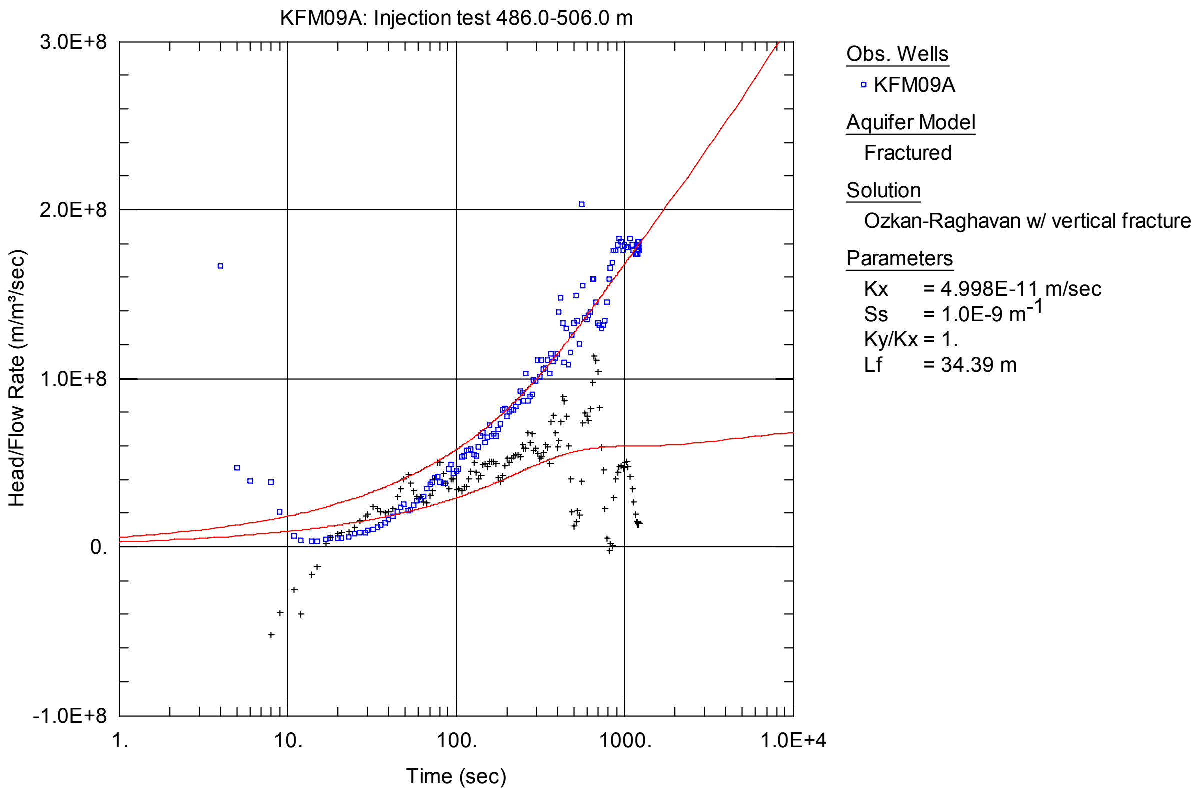


Figure A3-139. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 486.0-506.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

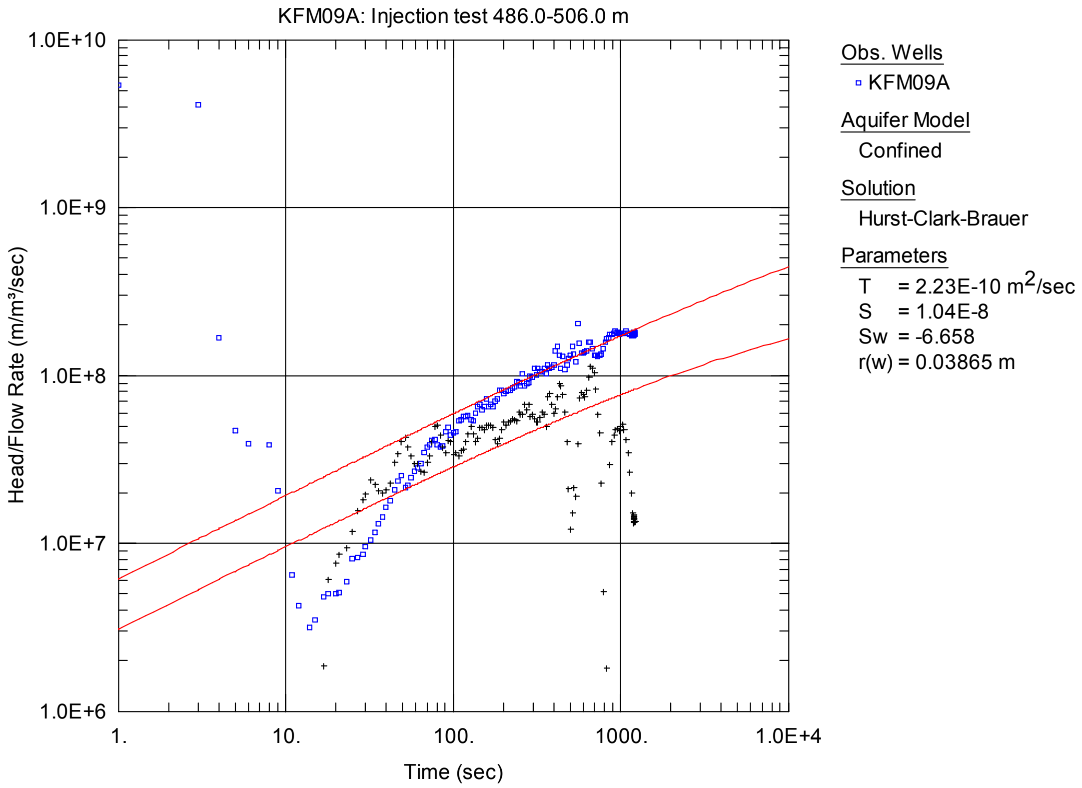


Figure A3-140. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 486.0-506.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for pseudo-radial flow.*

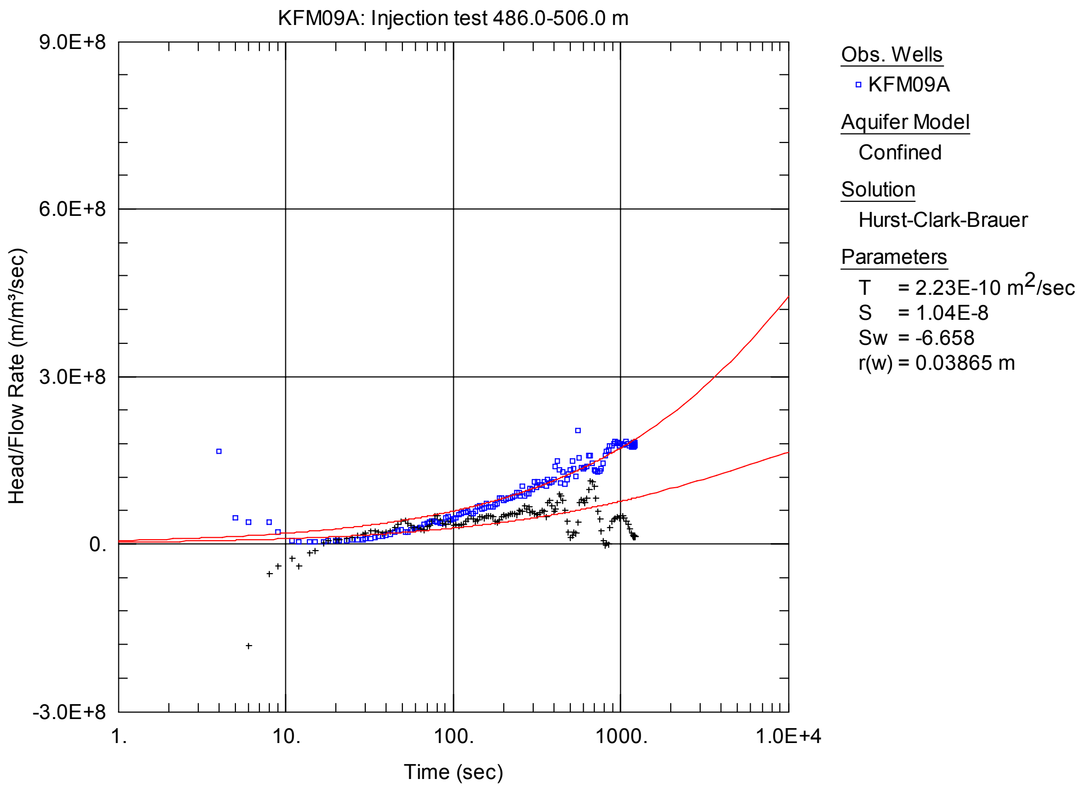


Figure A3-141. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 486.0-506.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for pseudo-radial flow.*

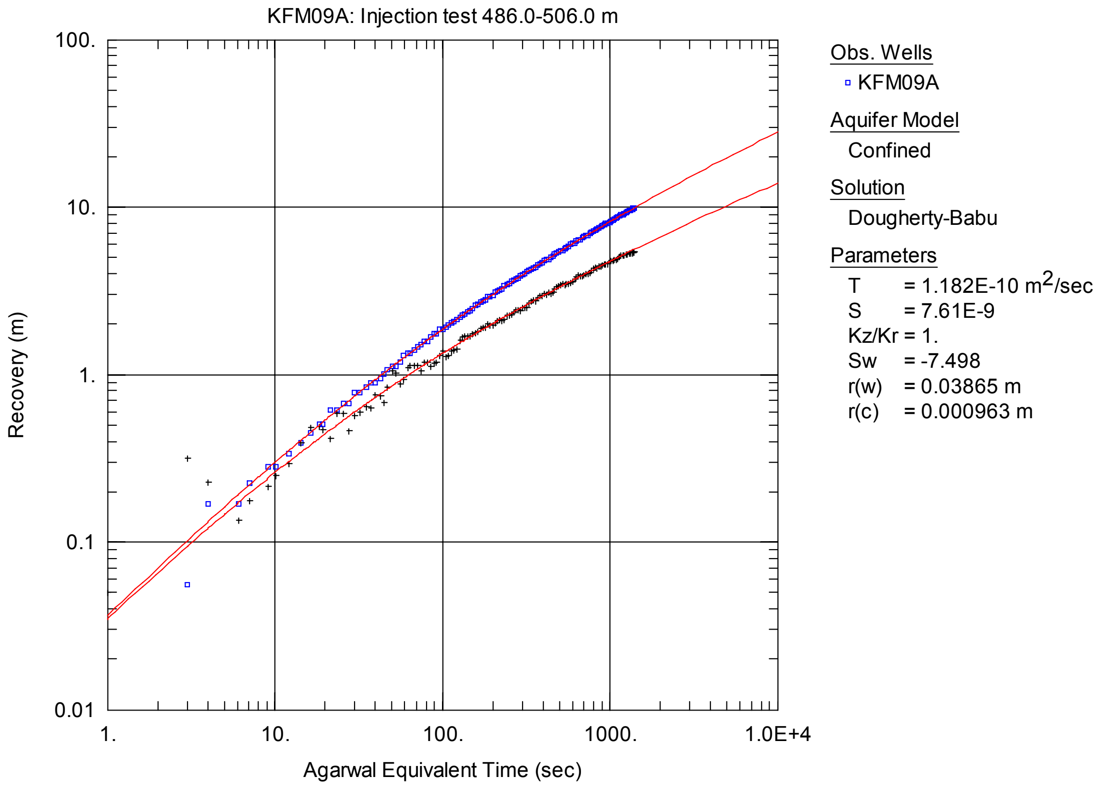


Figure A3-142. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 486.0-506.0 m in KFM09A. The transient evaluation on the recovery period is not regarded as representative.*

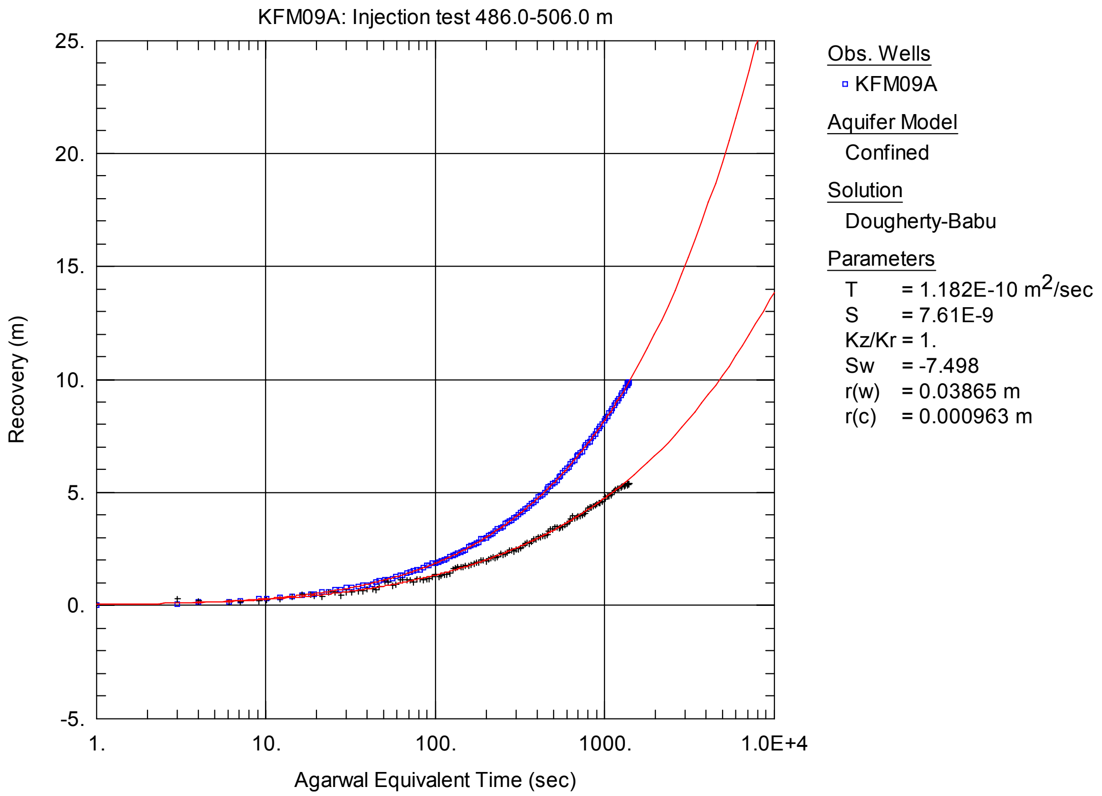


Figure A3-143. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 486.0-506.0 m in KFM09A. The transient evaluation on the recovery period is not regarded as representative.*

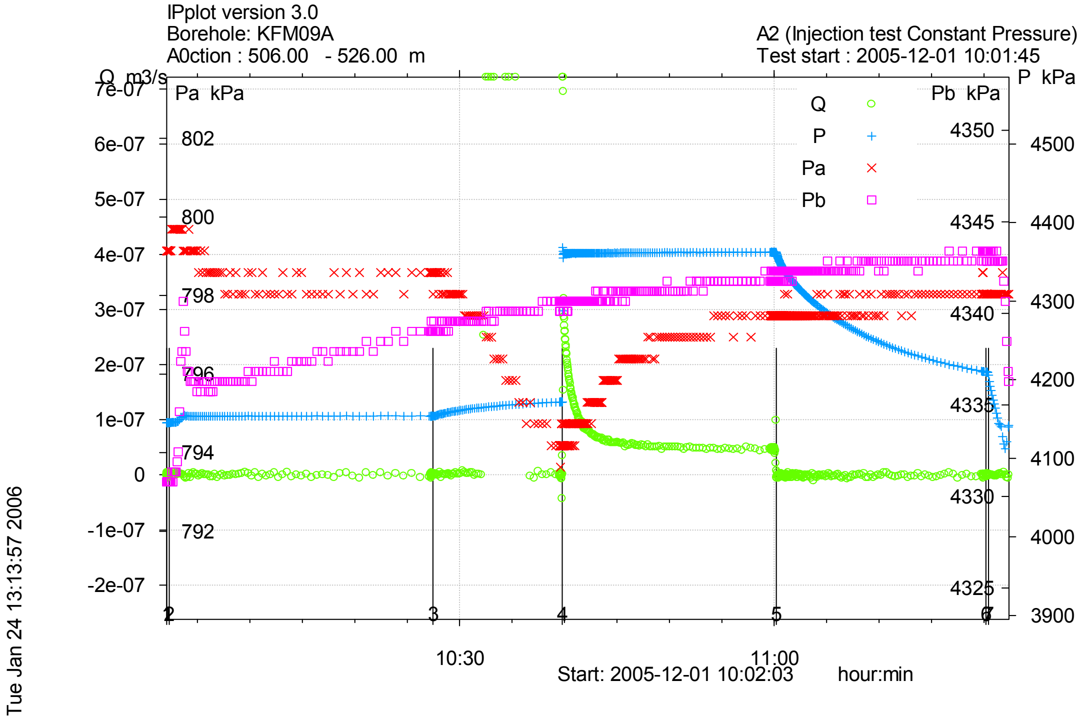


Figure A3-144. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 506.0-526.0 m in borehole KFM09A.

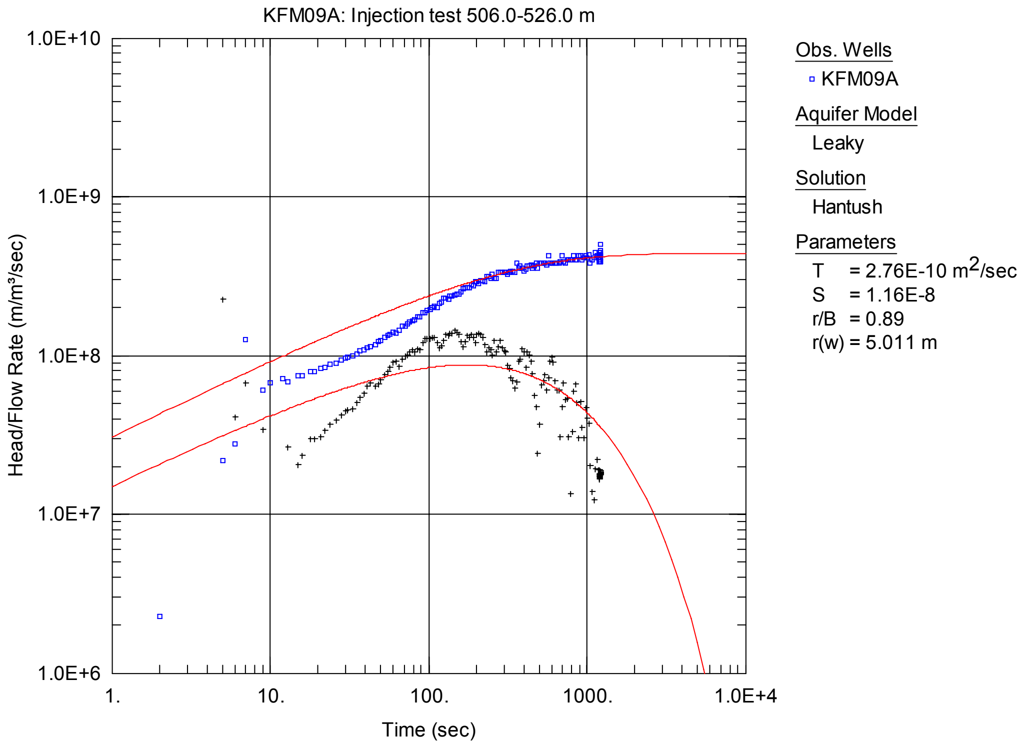


Figure A3-145. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 506.0-526.0 m in KFM09A. No unambiguous evaluation could be made on the injection period.

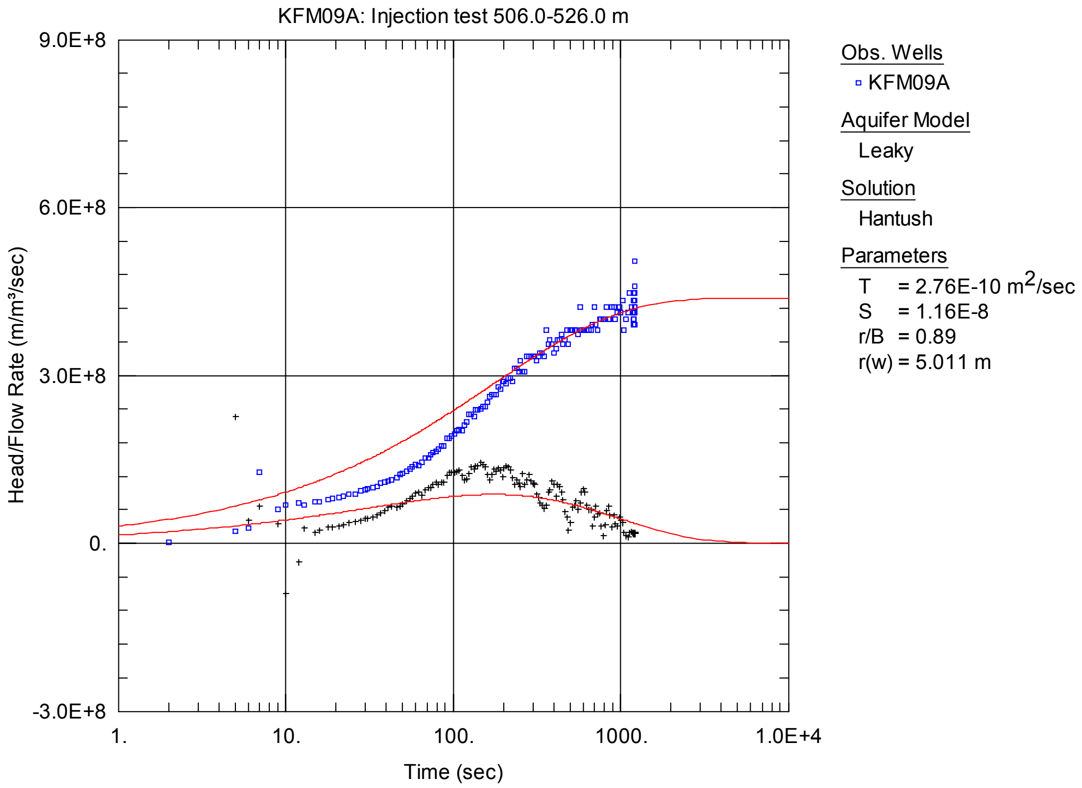


Figure A3-146. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 506.0-526.0 m in KFM09A. No unambiguous evaluation could be made on the injection period.*

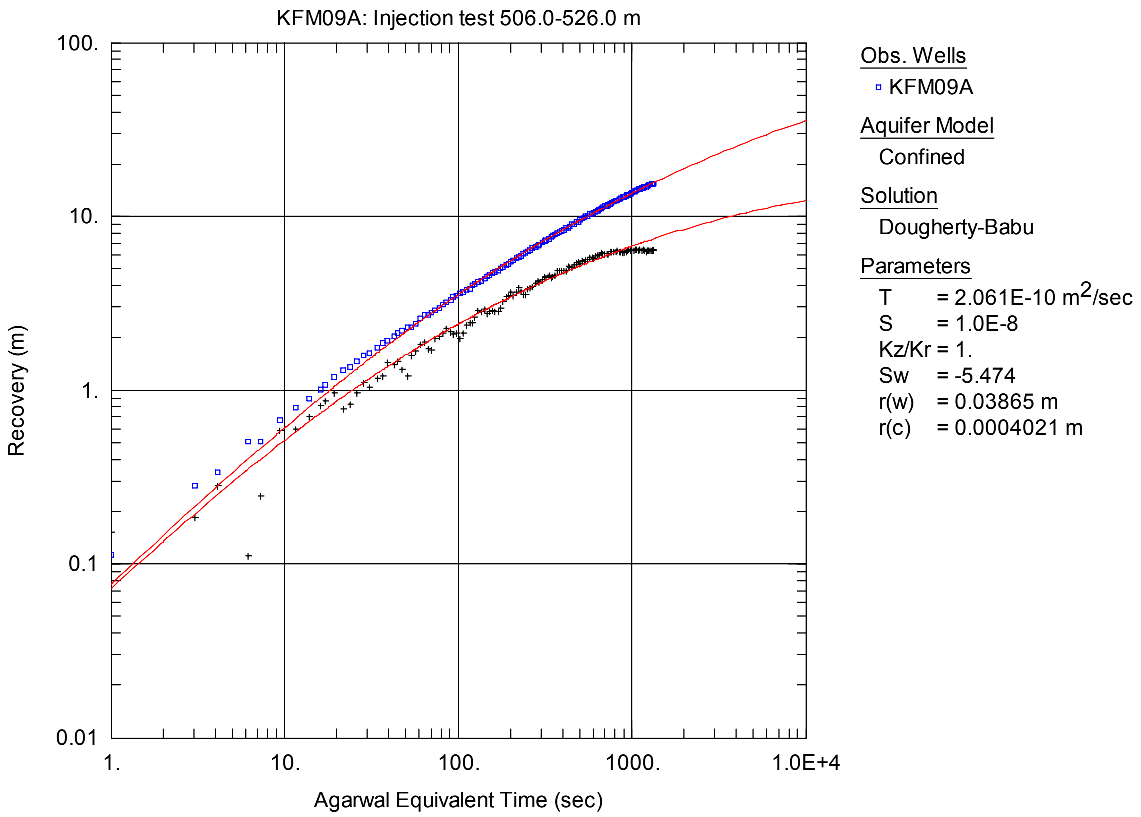


Figure A3-147. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 506.0-526.0 m in KFM09A.*

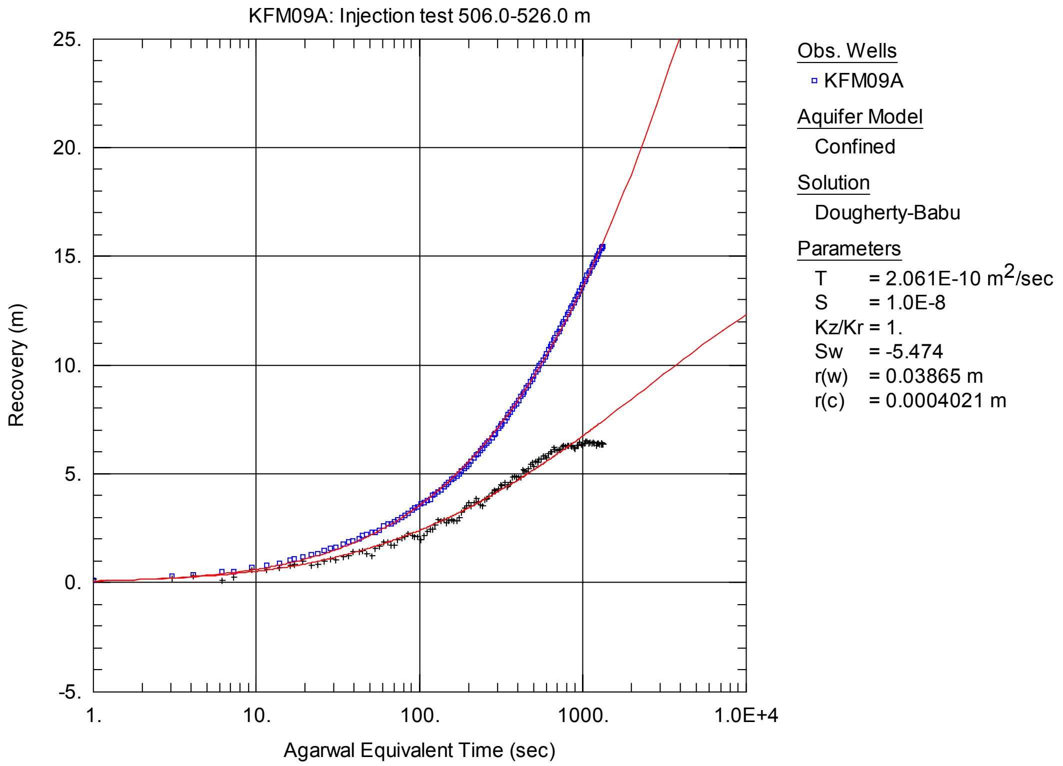


Figure A3-148. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 506.0-526.0 m in KFM09A.*

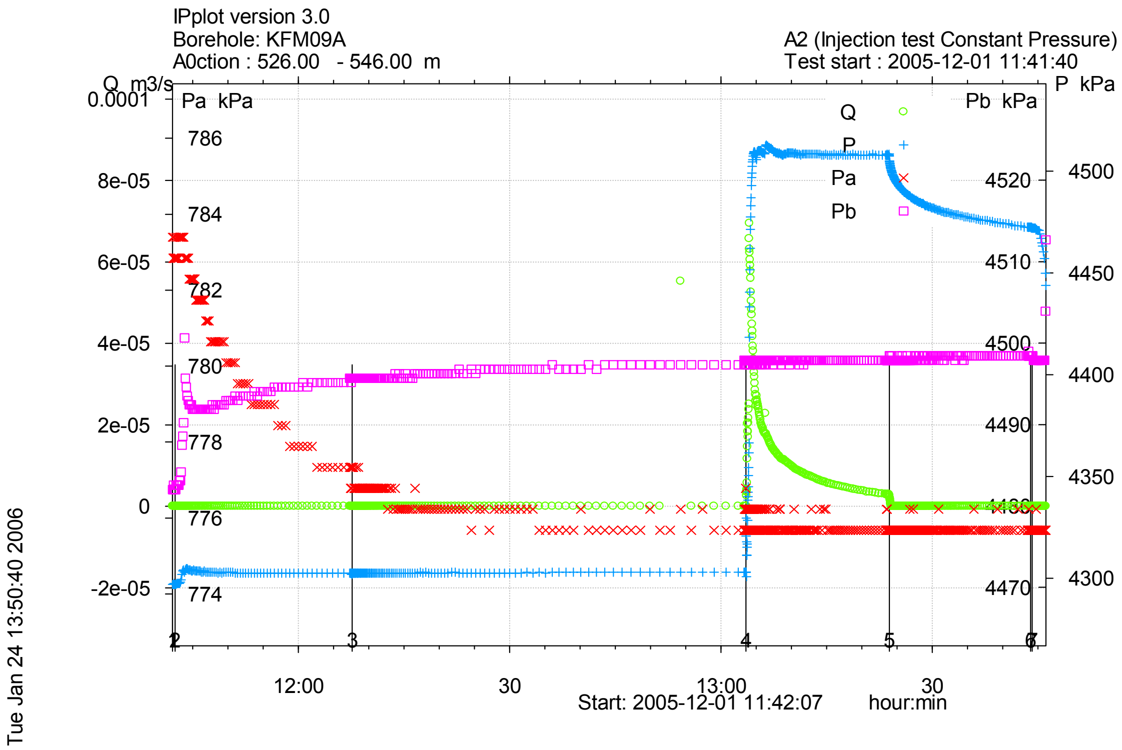


Figure A3-149. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 526.0-546.0 m in borehole KFM09A.*

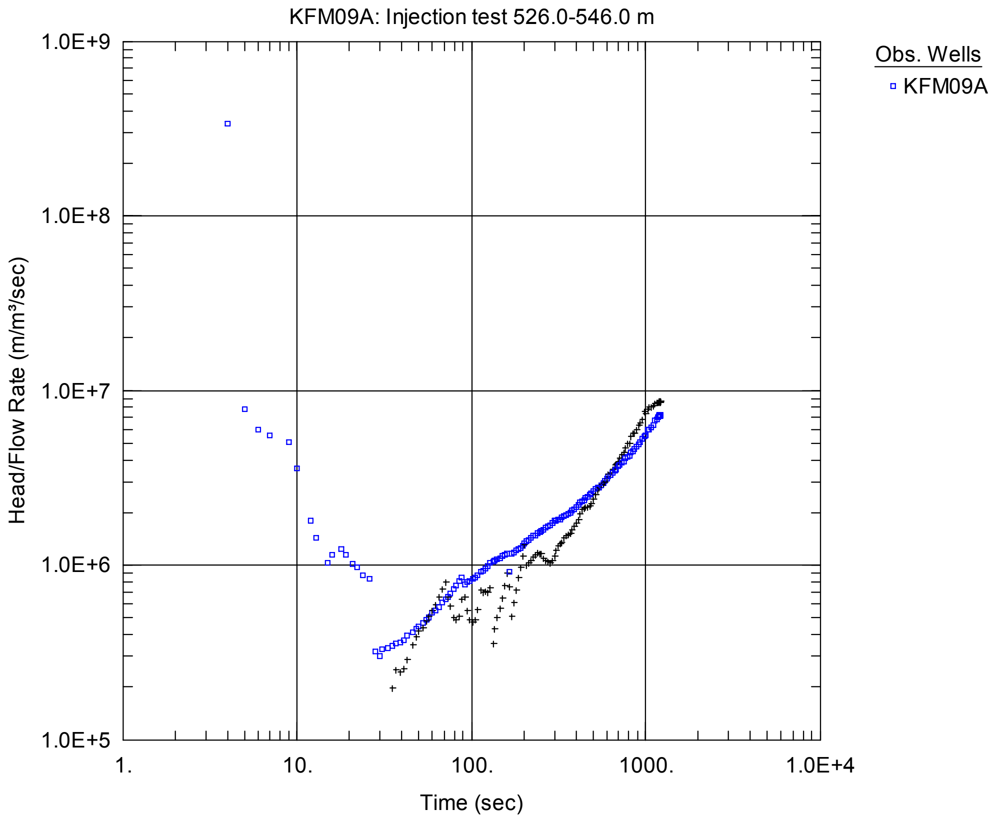


Figure A3-150. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 526.0-546.0 m in KFM09A.*

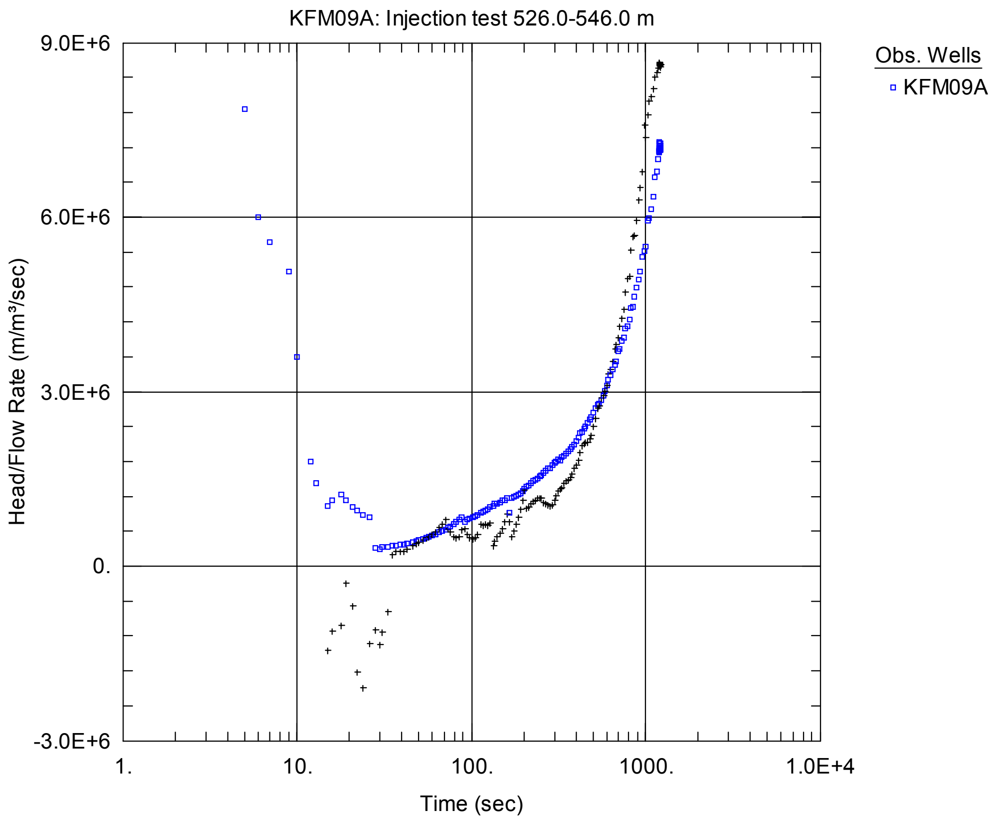


Figure A3-151. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 526.0-546.0 m in KFM09A.*

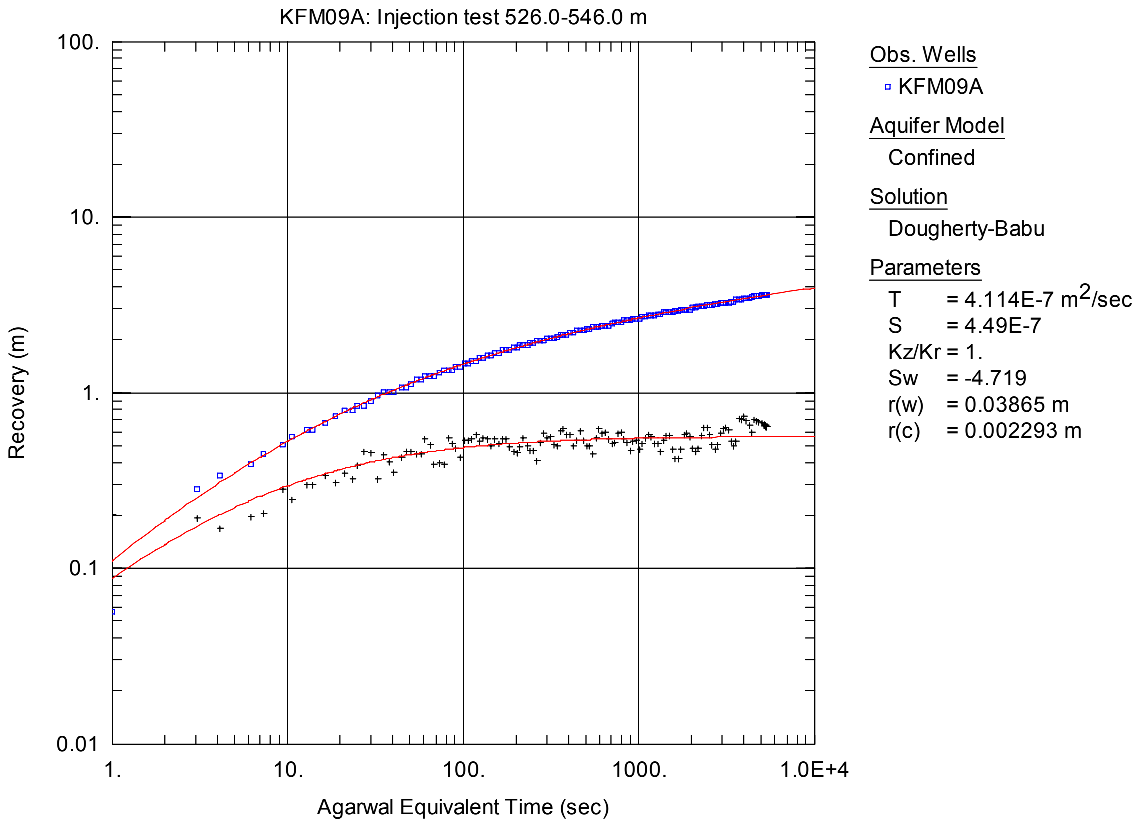


Figure A3-152. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 526.0-546.0 m in KFM09A.*

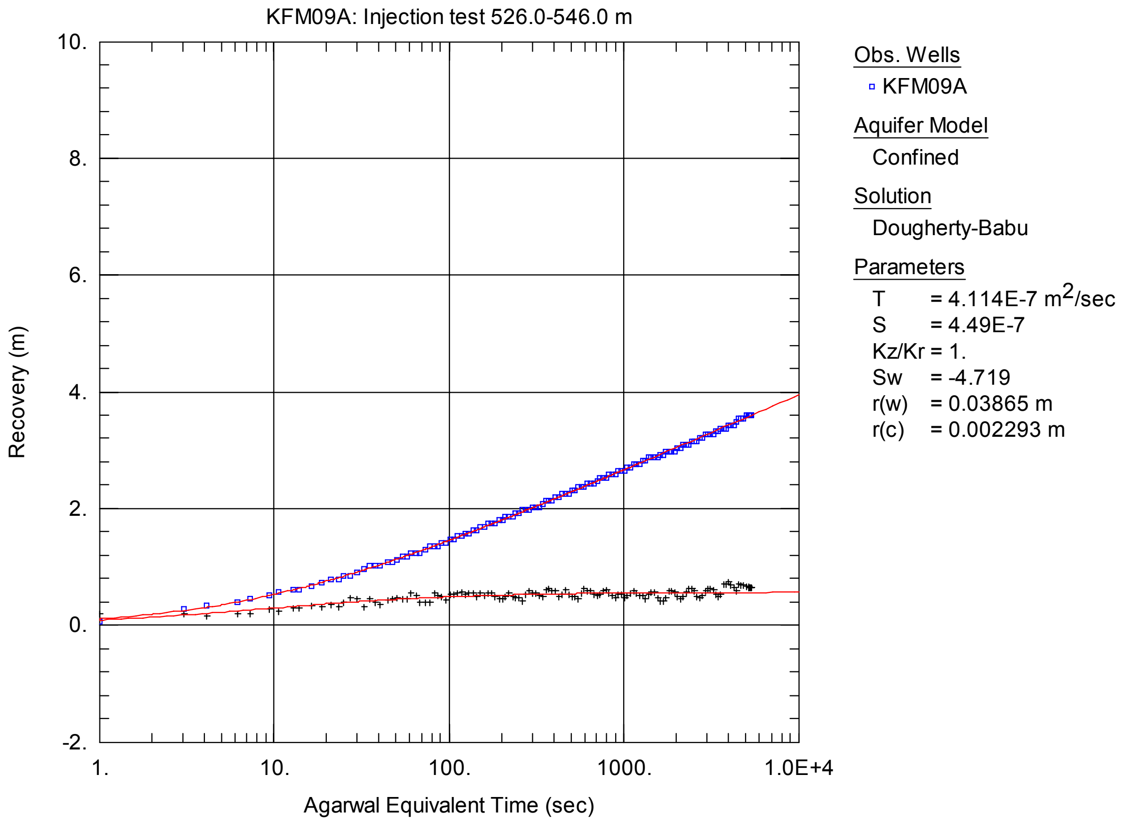


Figure A3-153. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 526.0-546.0 m in KFM09A.*

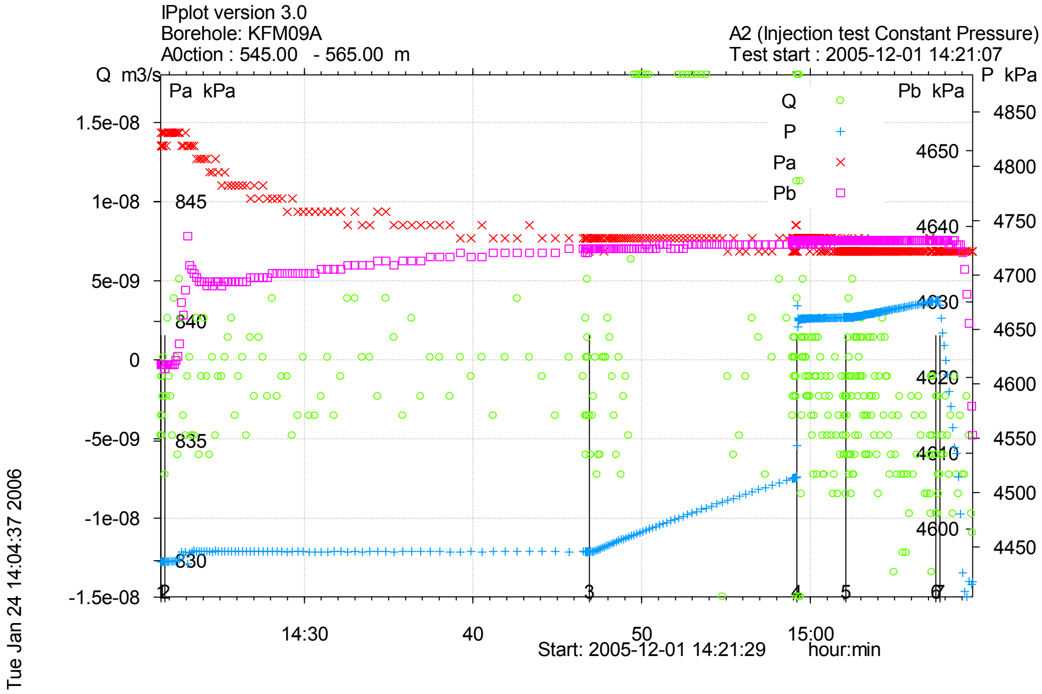


Figure A3-154. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 545.0-565.0 m in borehole KFM09A.*

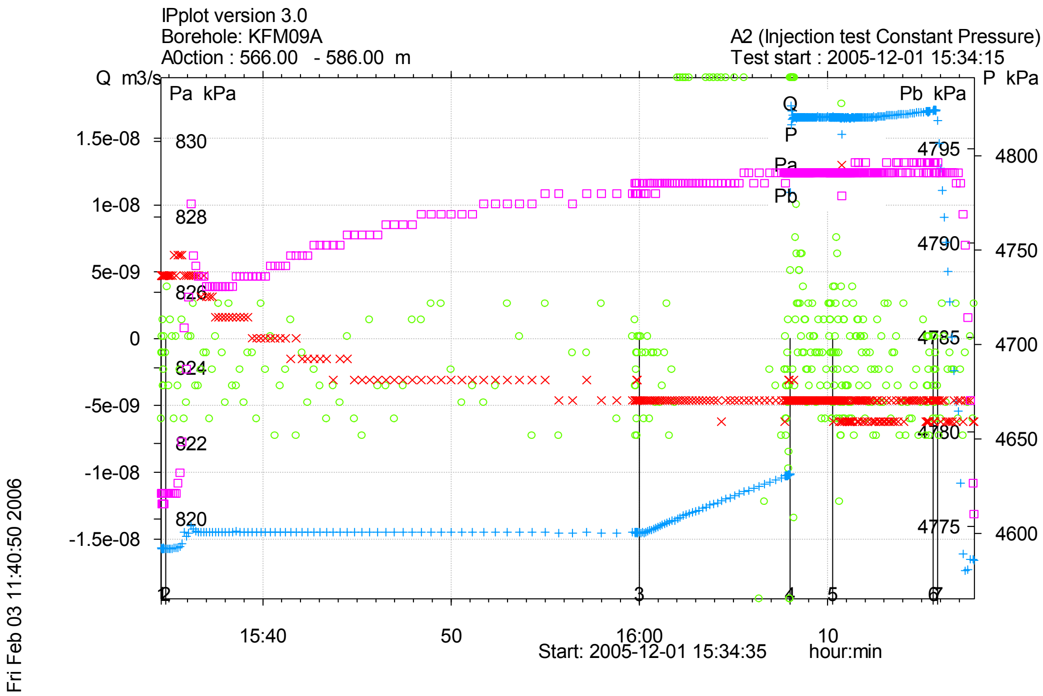


Figure A3-155. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 566.0-586.0 m in borehole KFM09A.*

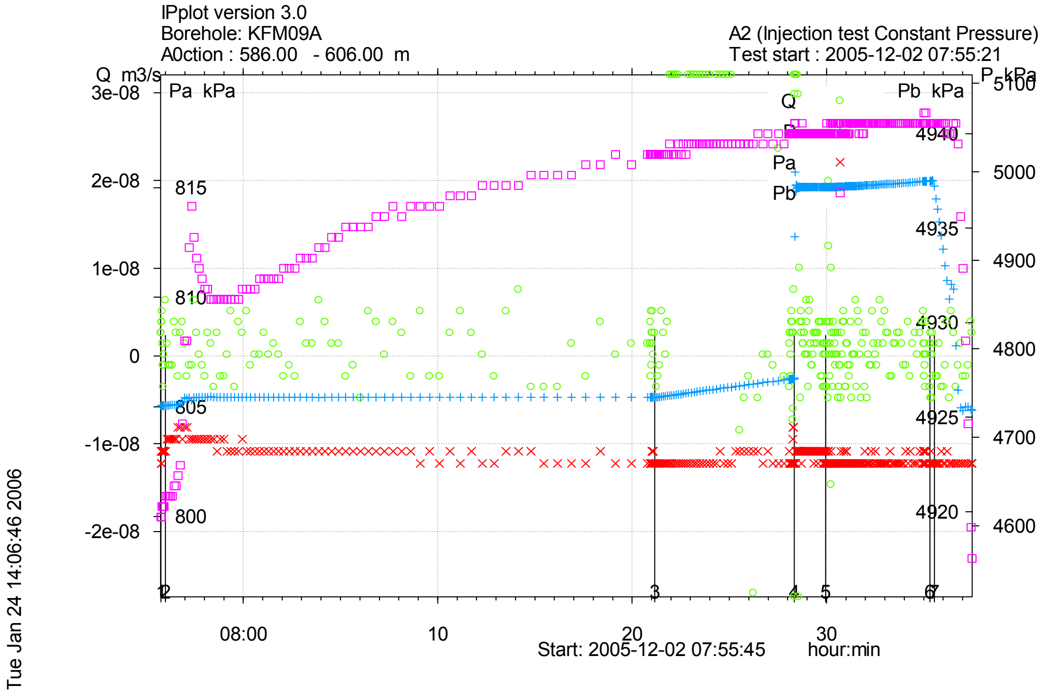


Figure A3-156. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 586.0-606.0 m in borehole KFM09A.*

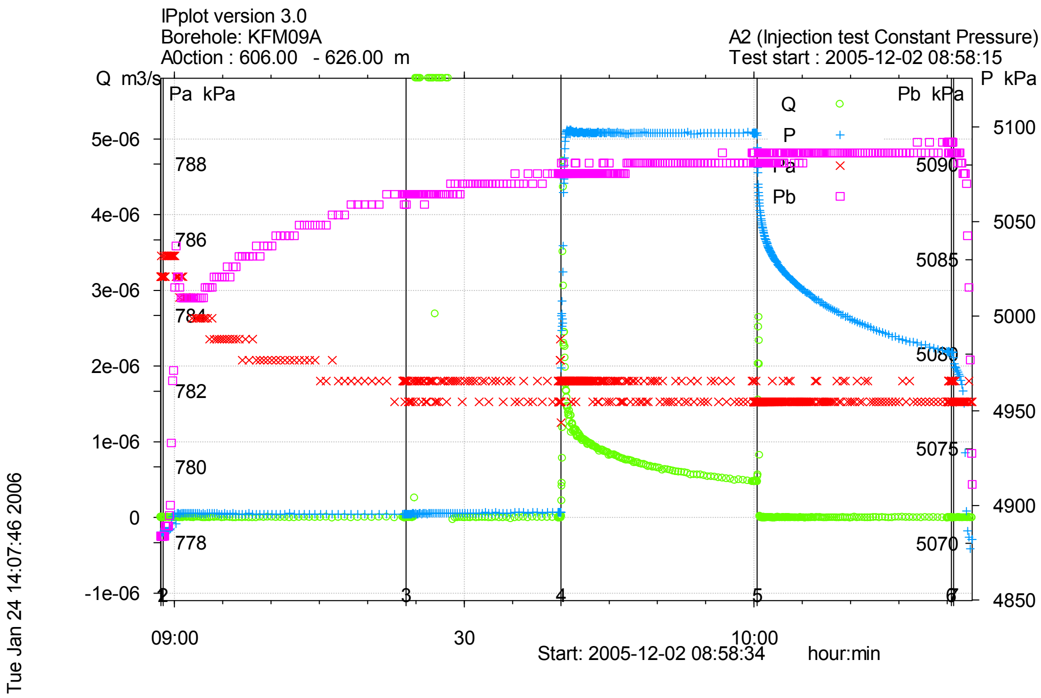


Figure A3-157. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 606.0-626.0 m in borehole KFM09A.*

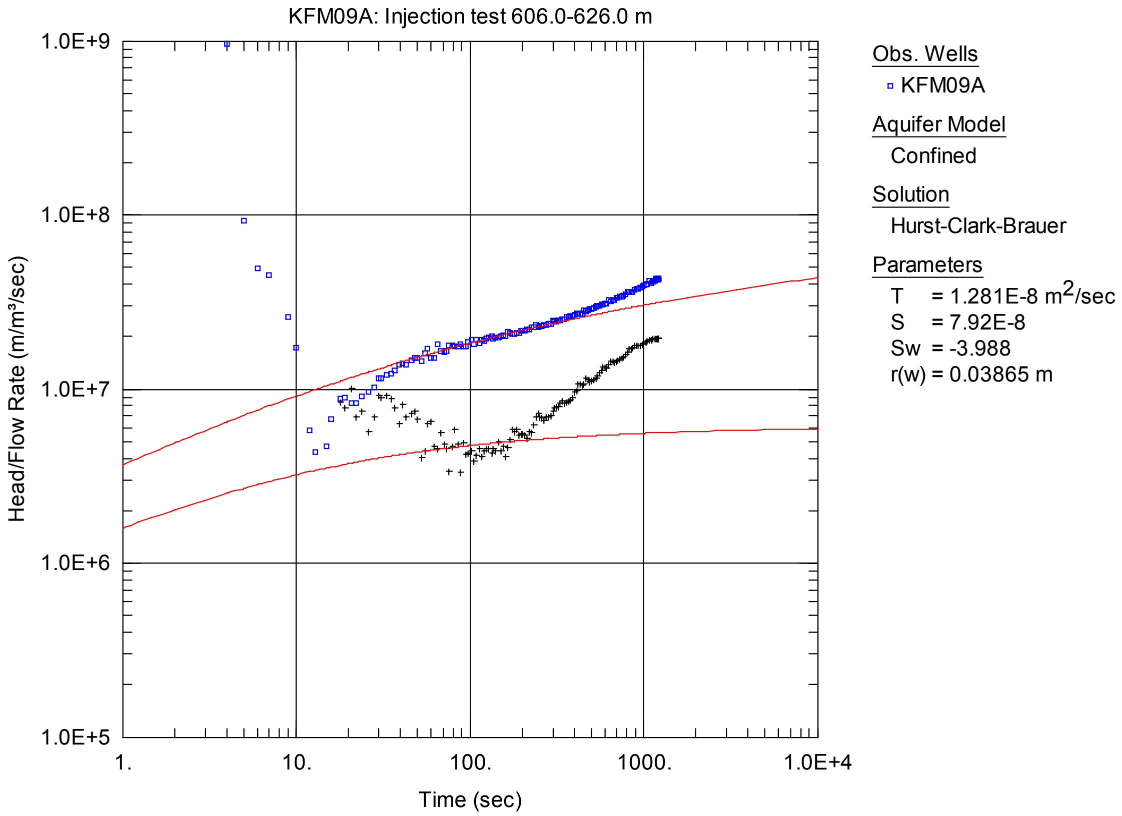


Figure A3-158. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 606.0-626.0 m in KFM09A.*

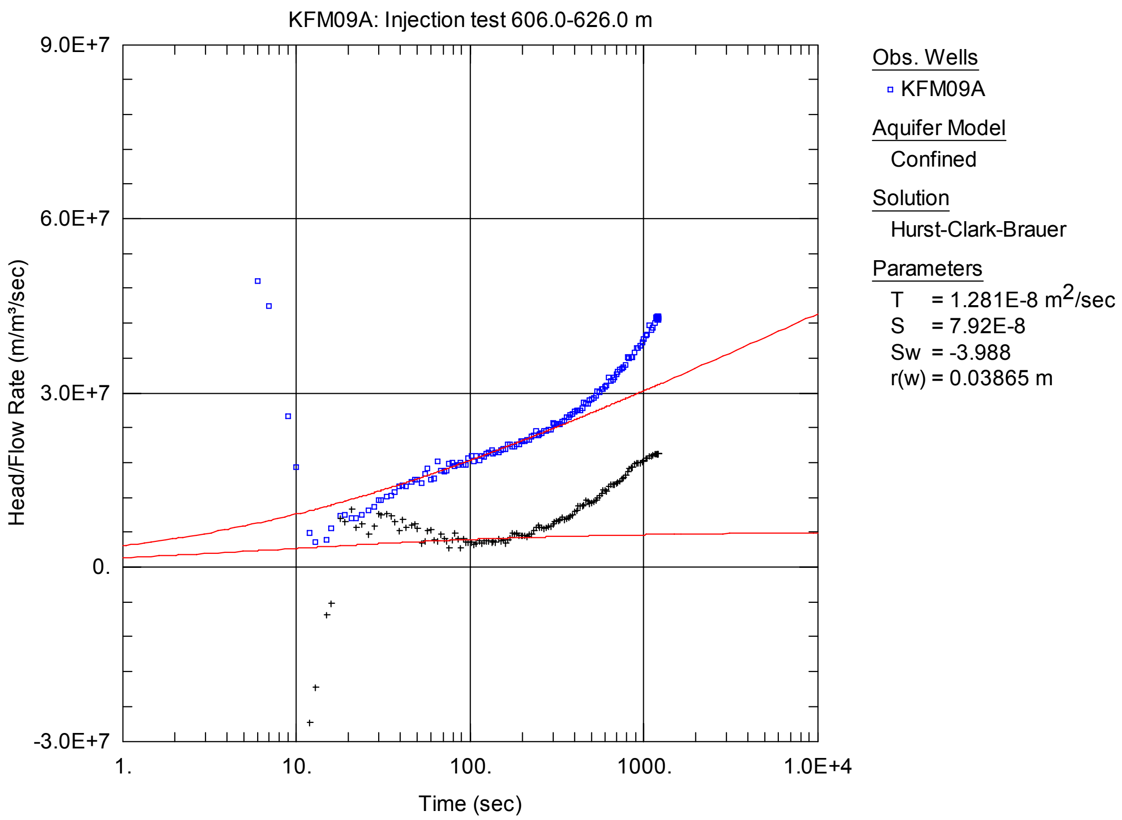


Figure A3-159. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 606.0-626.0 m in KFM09A.*

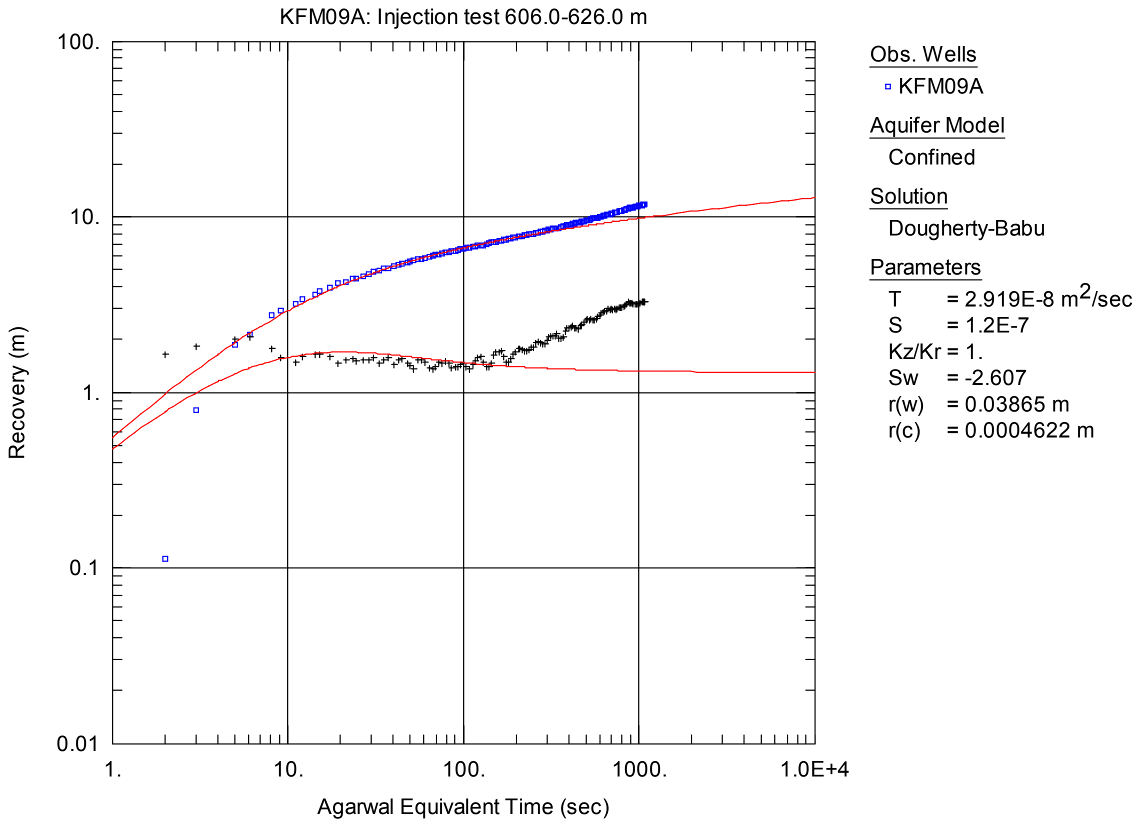


Figure A3-160. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 606.0-626.0 m in KFM09A.*

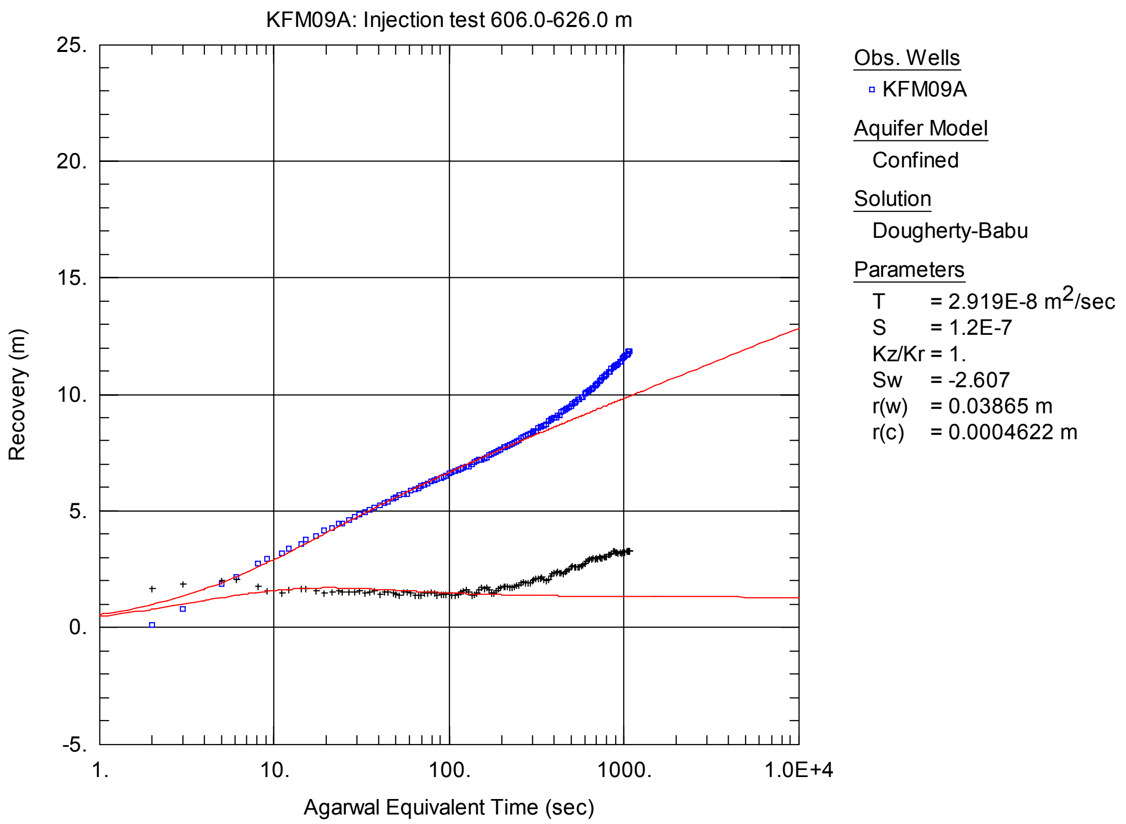


Figure A3-161. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 606.0-626.0 m in KFM09A.*

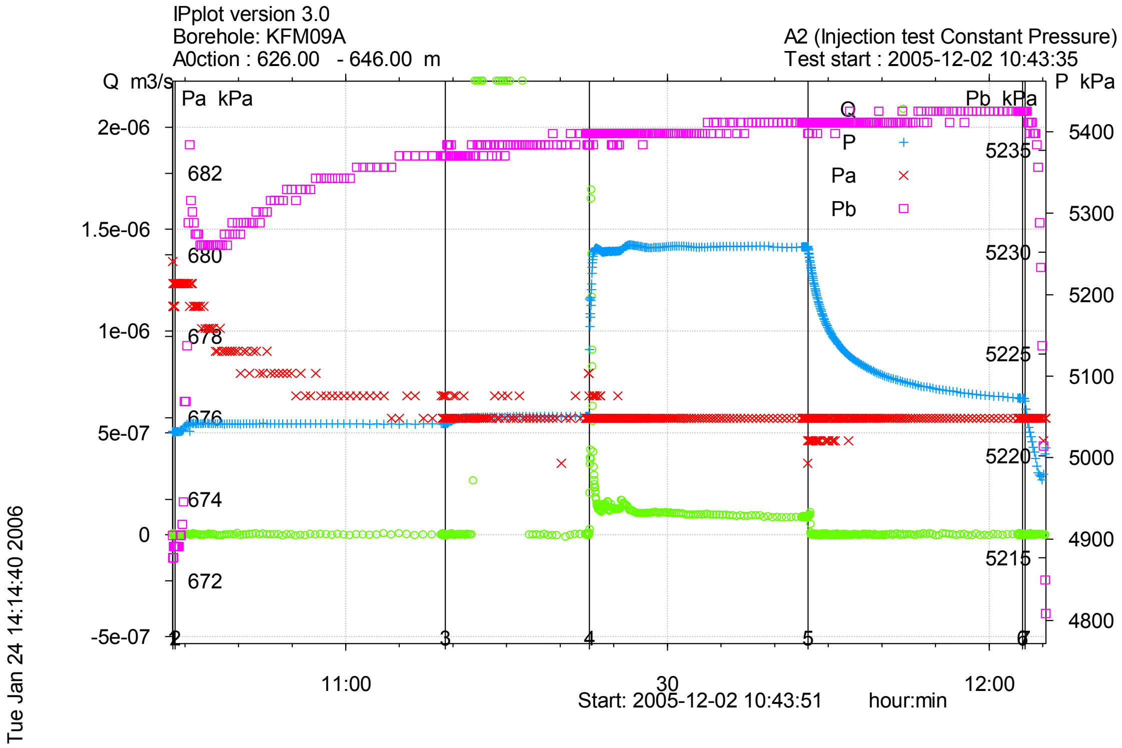


Figure A3-162. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in 626.0-646.0 m in borehole KFM09A.

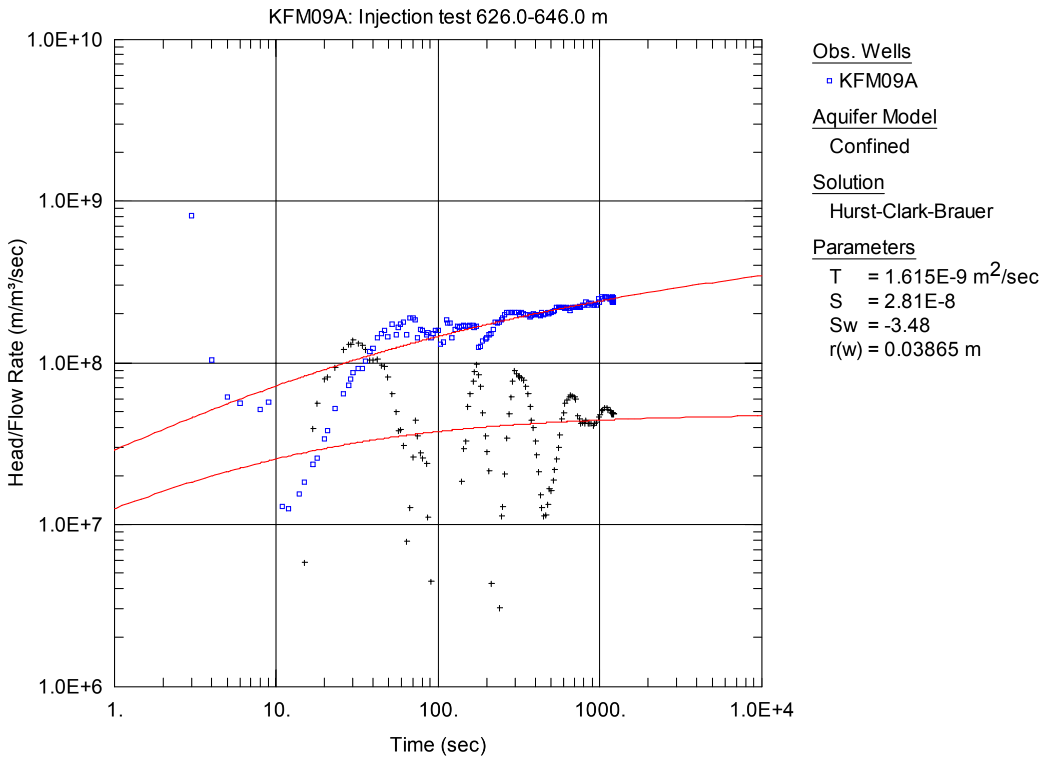


Figure A3-163. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 626.0-646.0 m in KFM09A.

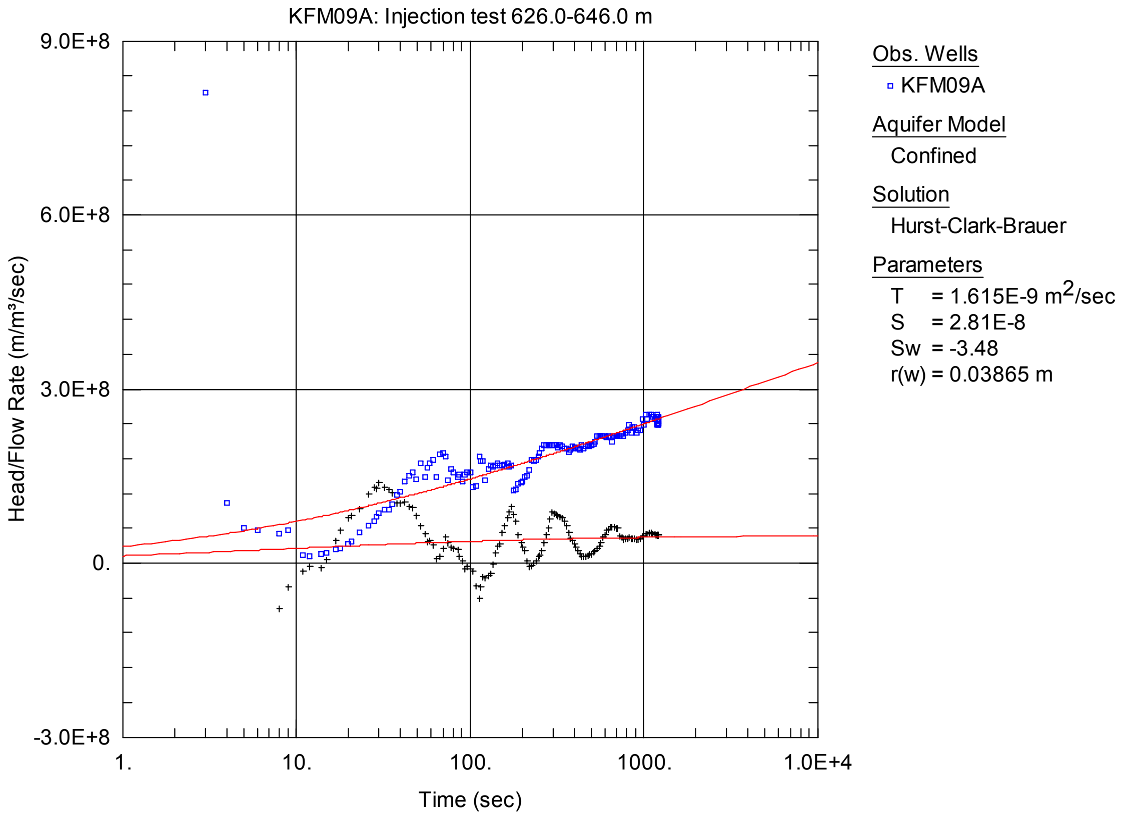


Figure A3-164. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in 626.0-646.0 m in KFM09A.*

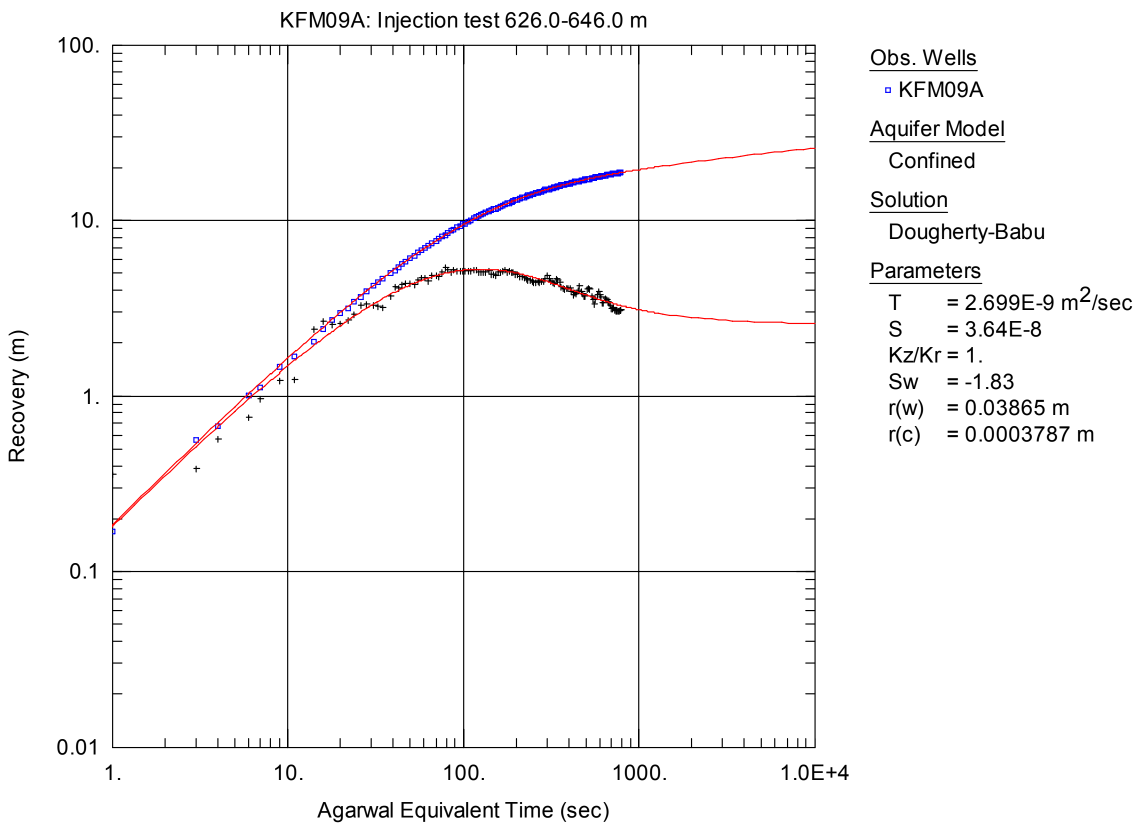


Figure A3-165. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 626.0-646.0 m in KFM09A.*

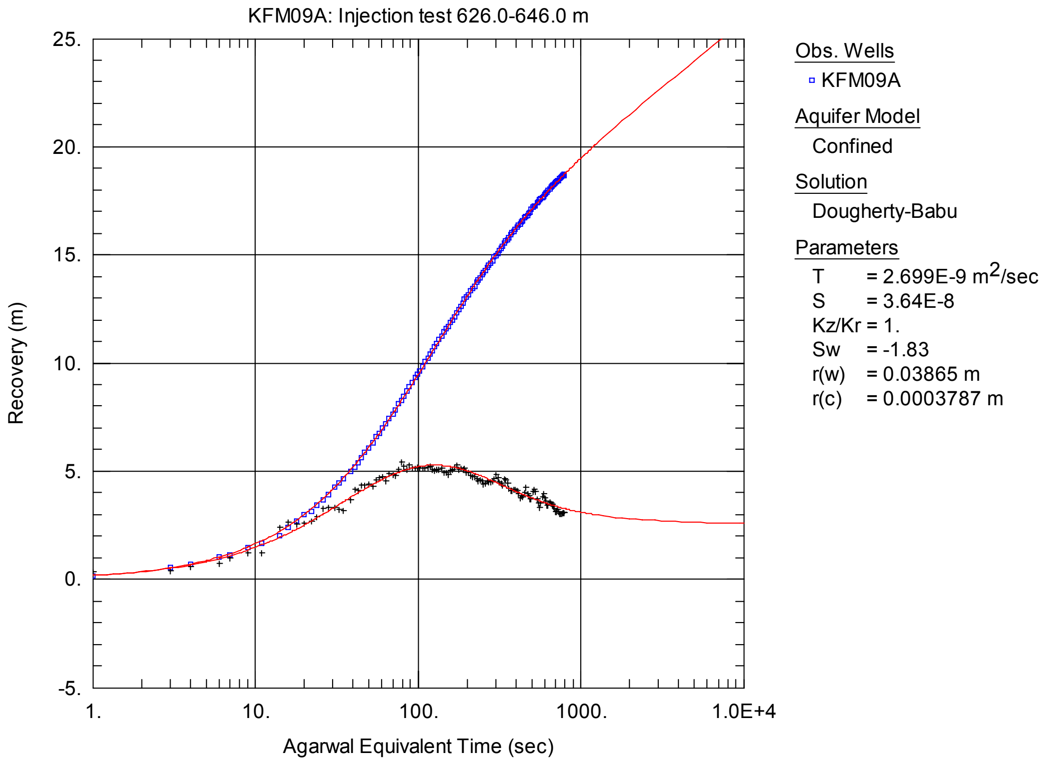


Figure A3-166. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 626.0-646.0 m in KFM09A.*

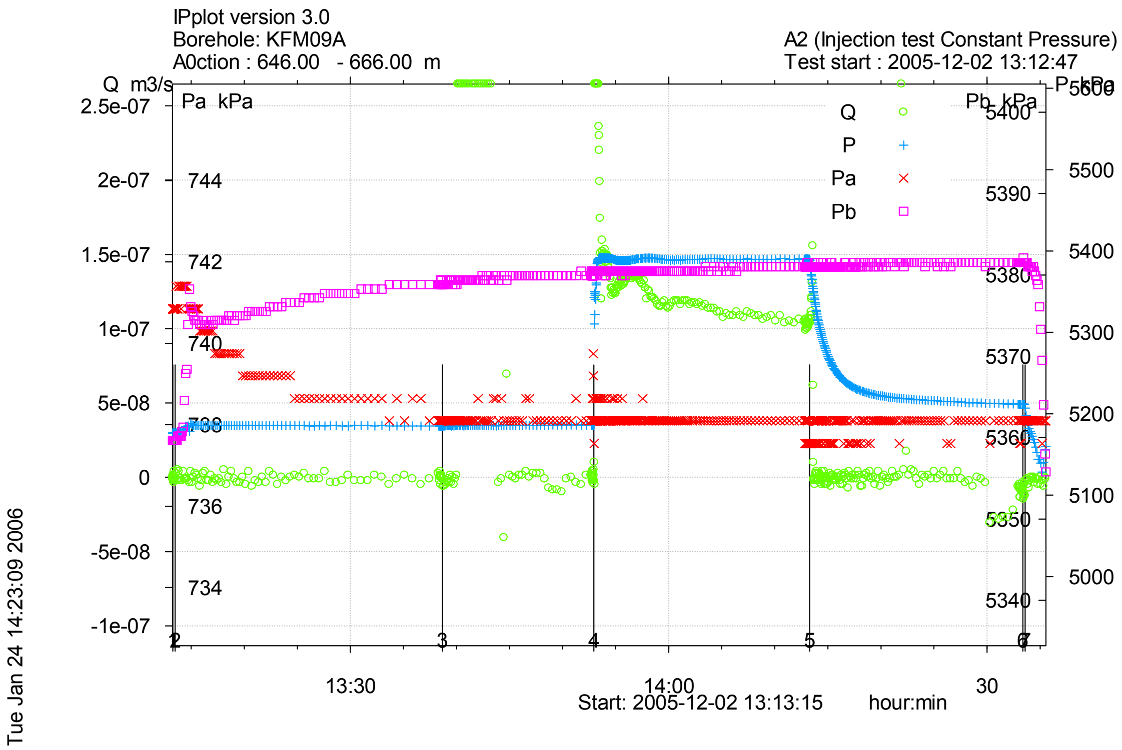


Figure A3-167. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 646.0-666.0 m in borehole KFM09A.*

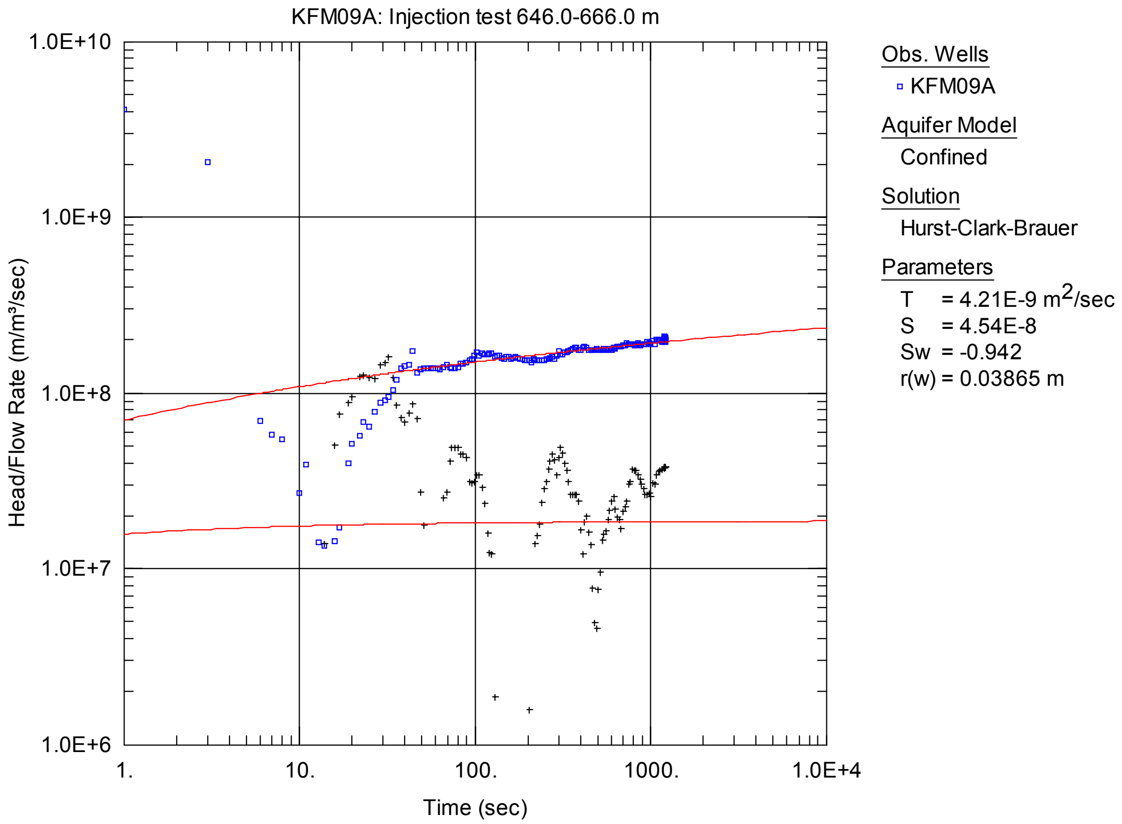


Figure A3-168. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 646.0-666.0 m in KFM09A.*

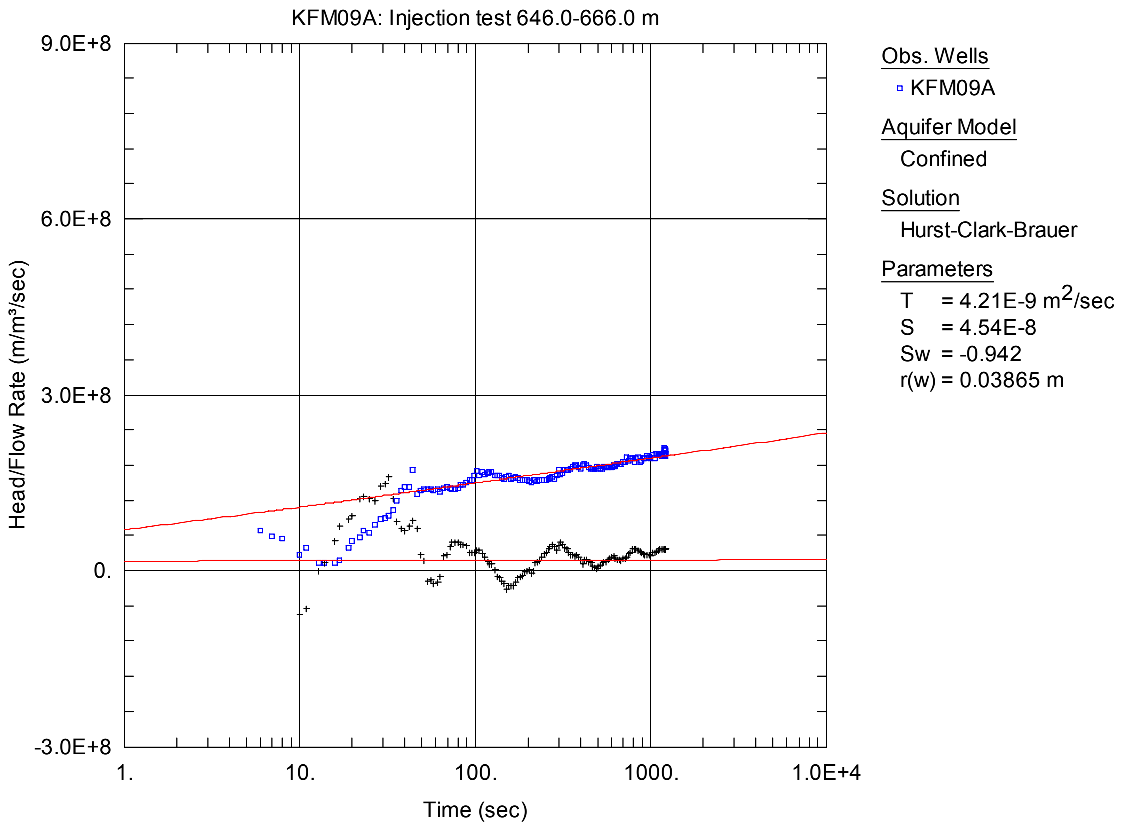


Figure A3-169. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 646.0-666.0m in KFM09A.*

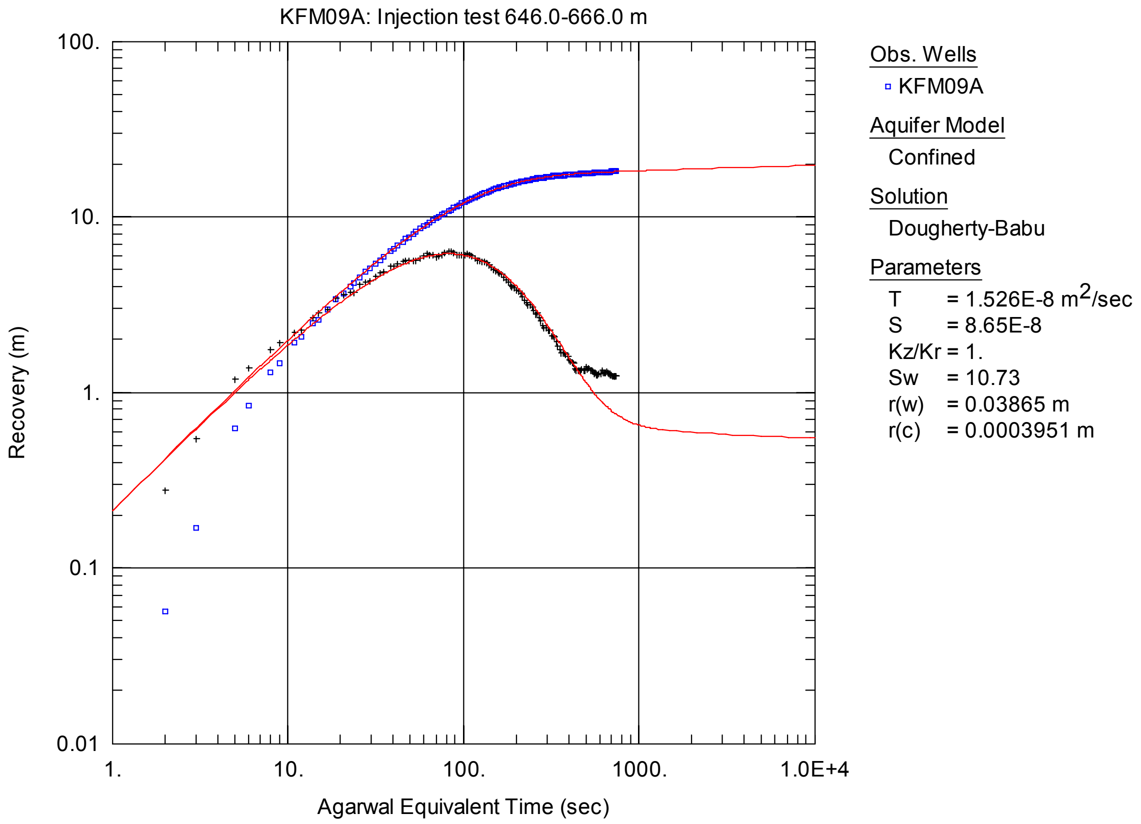


Figure A3-170. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 646.0-666.0 m in KFM09A.*

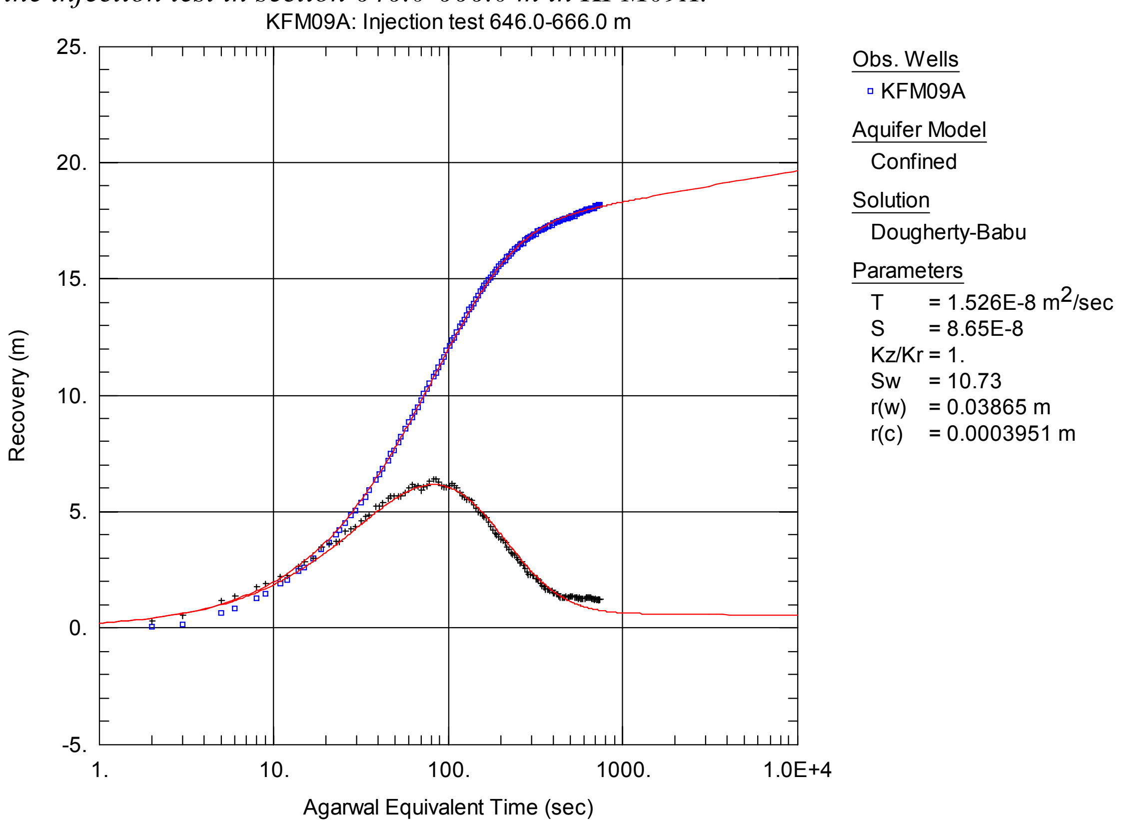


Figure A3-171. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 646.0-666.0 m in KFM09A.*

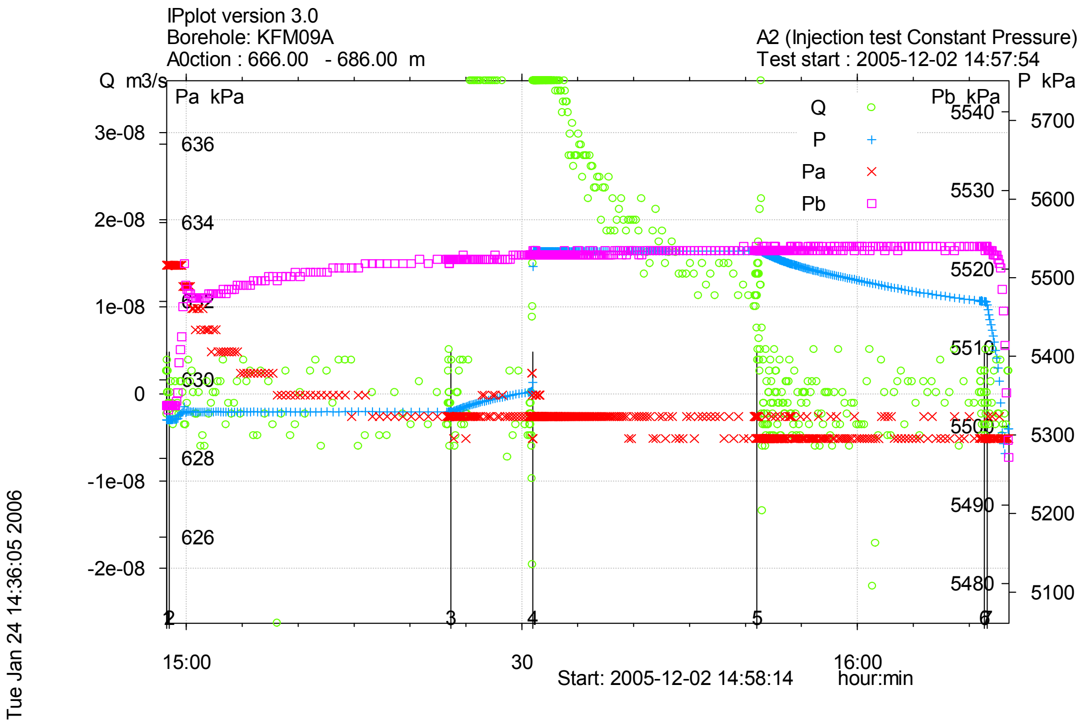


Figure A3-172. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 666.0-686.0 m in borehole KFM09A.*

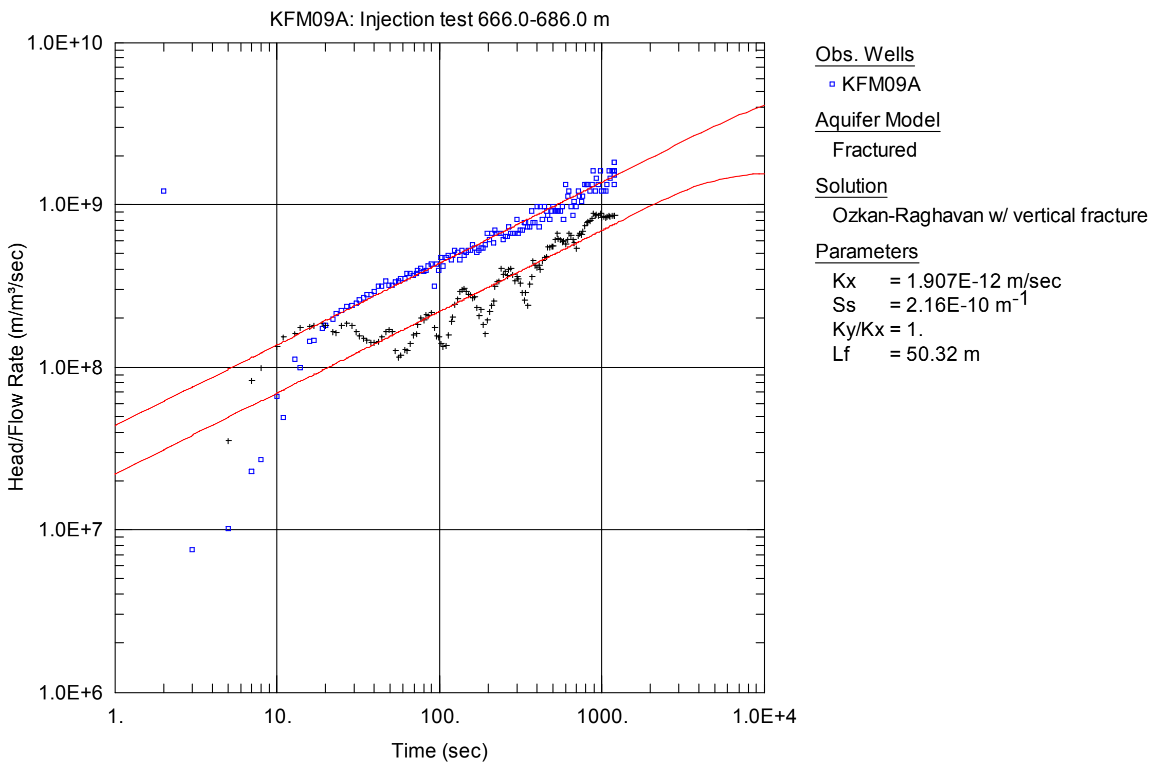


Figure A3-173. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 666.0-686.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

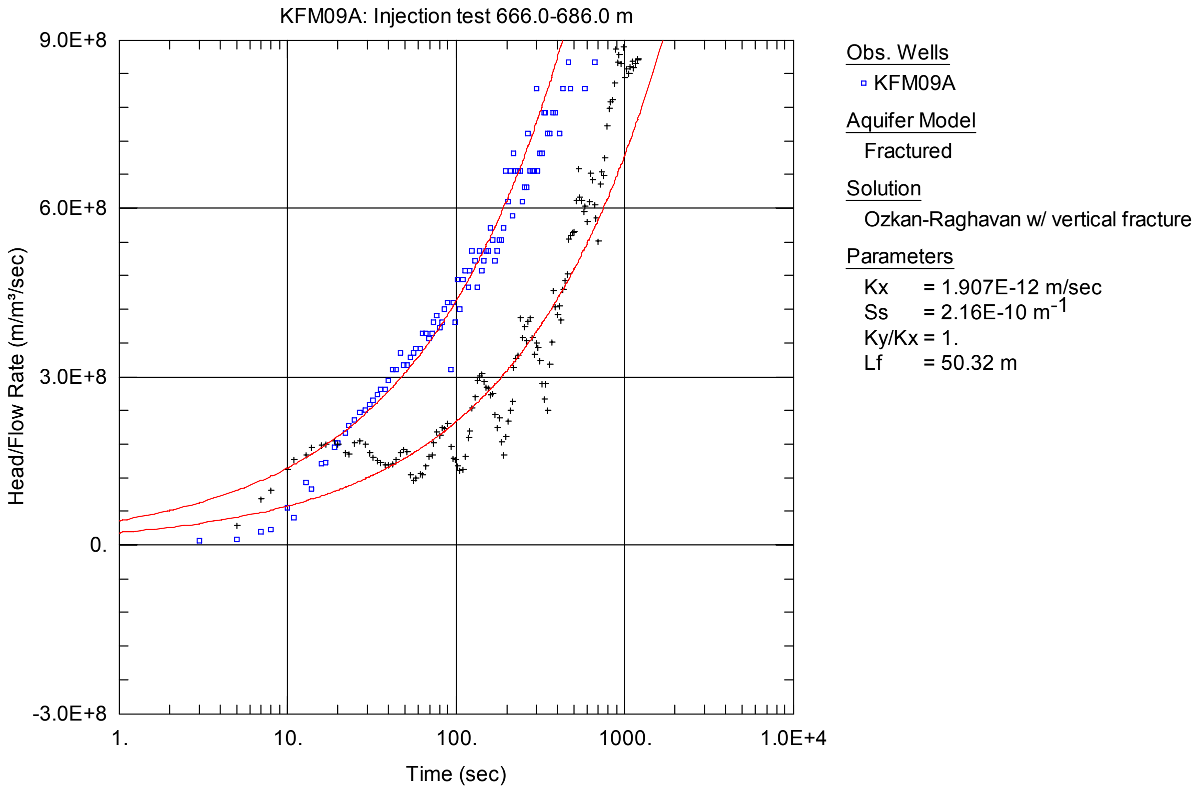


Figure A3-174. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 666.0-686.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

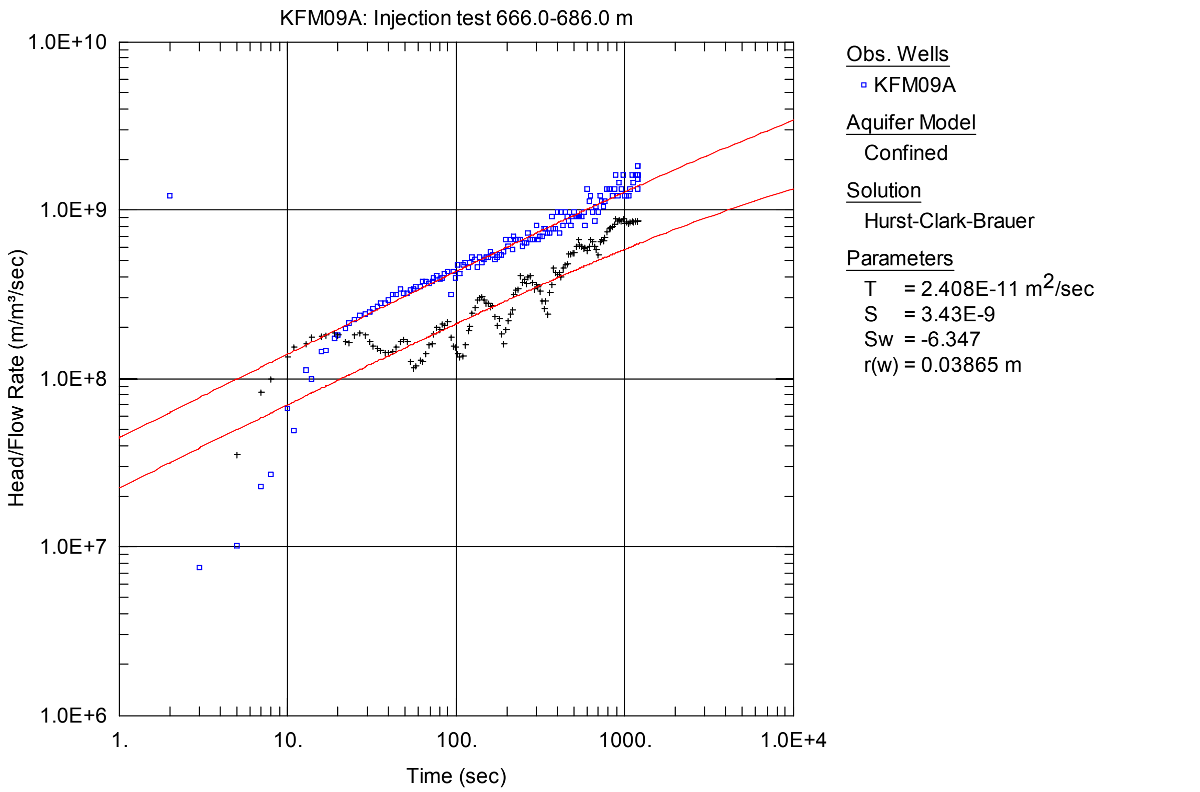


Figure A3-175. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 666.0-686.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for pseudo-radial flow.*

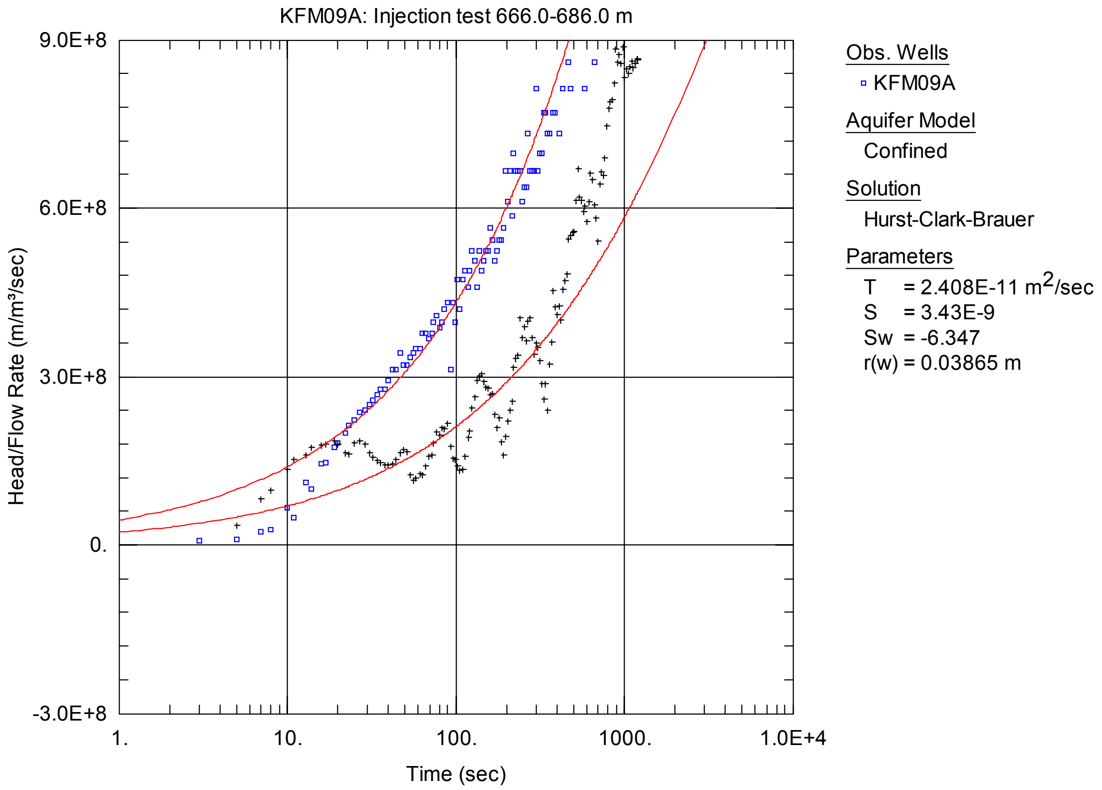


Figure A3-176. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 666.0-686.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for pseudo-radial flow.*

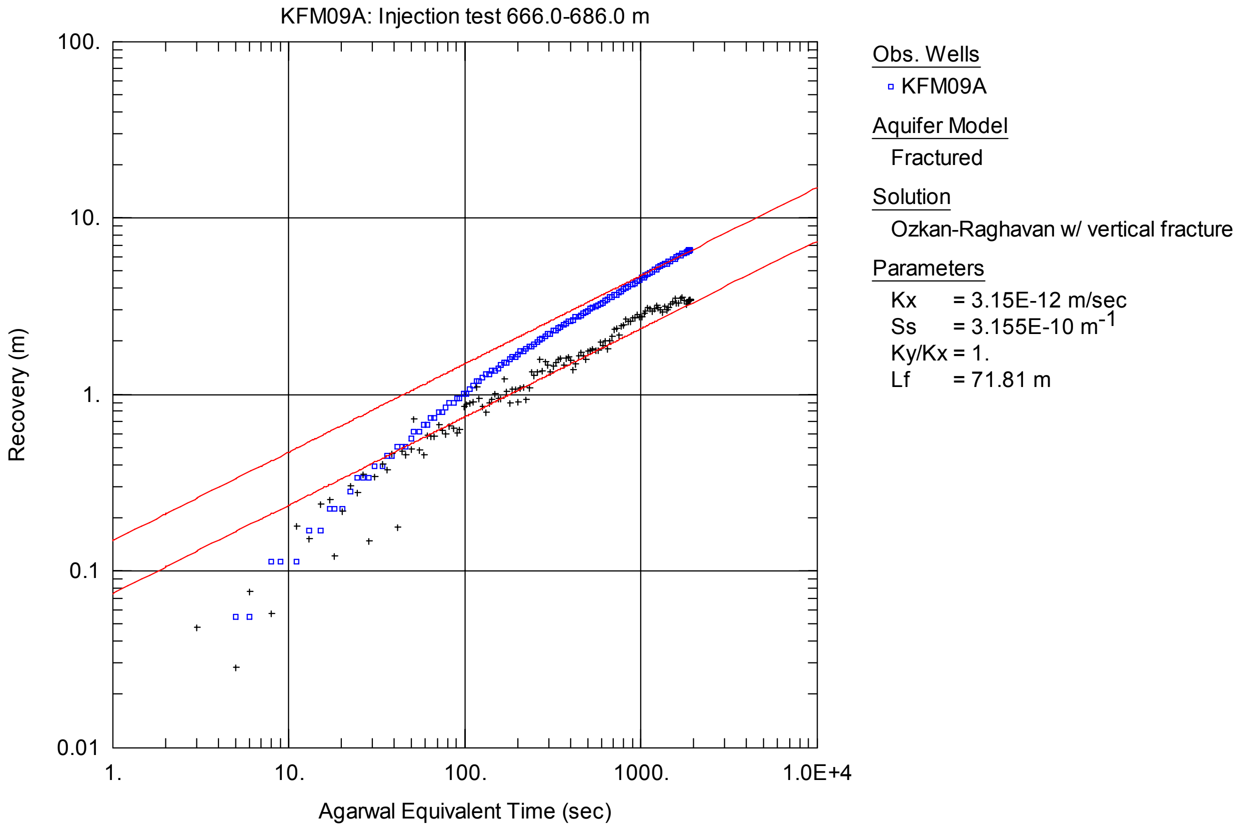


Figure A3-177. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 666.0-686.0 m in KFM09A.*

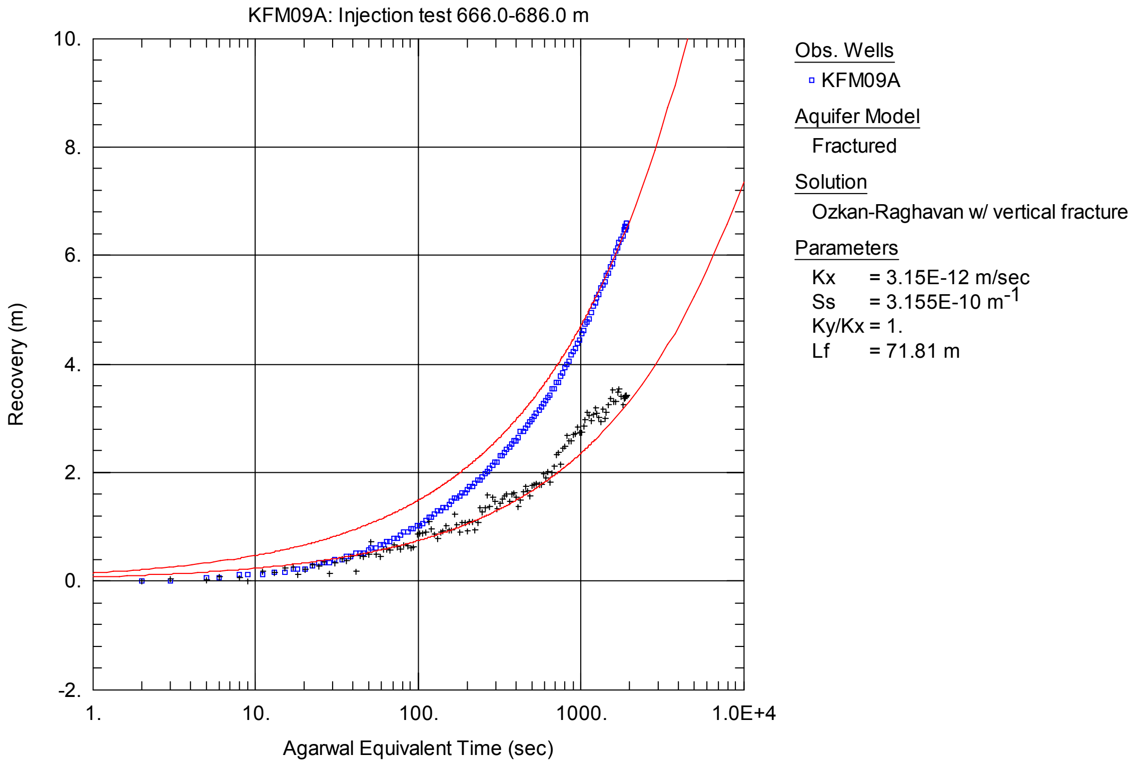


Figure A3-178. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 666.0-686.0 m in KFM09A.*

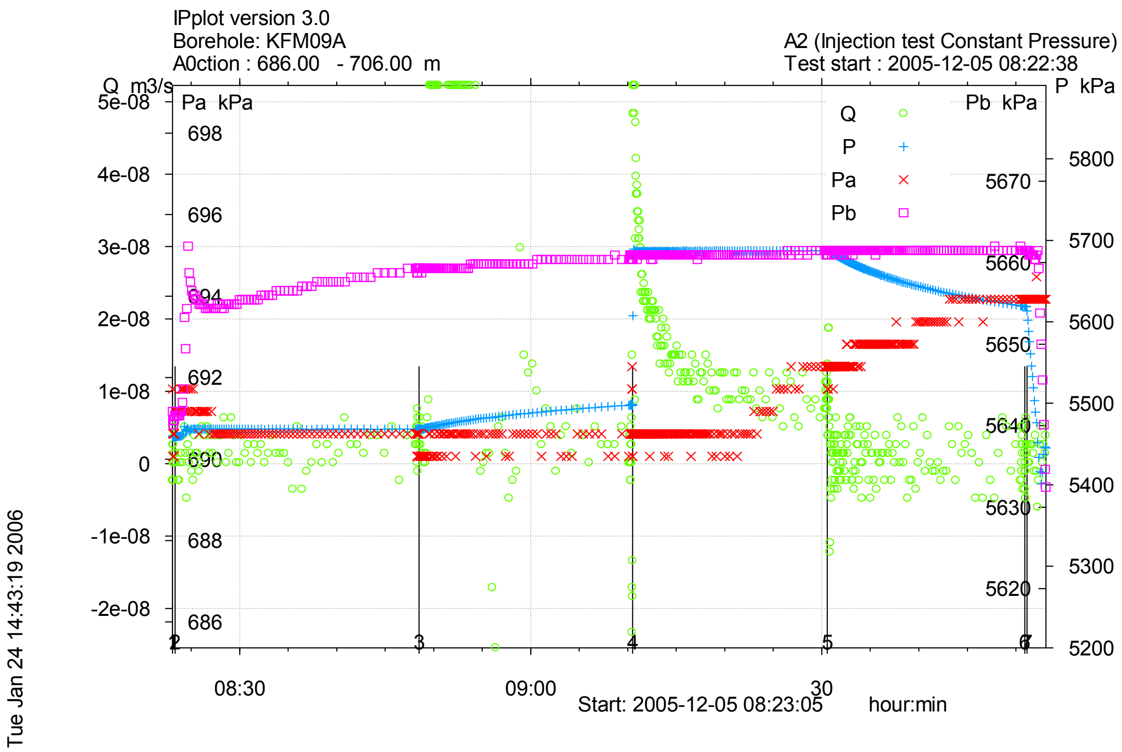


Figure A3-179. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 686.0-706.0 m in borehole KFM09A.*

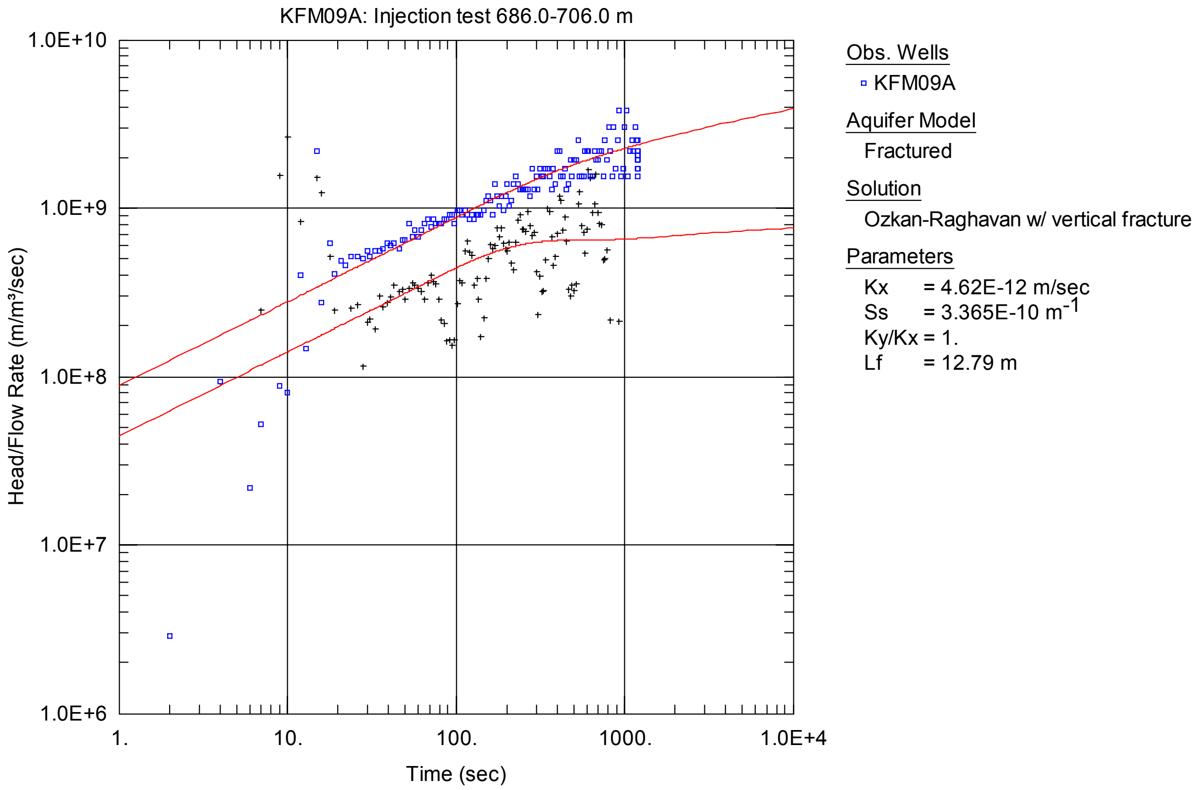


Figure A3-180. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 686.0-706.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

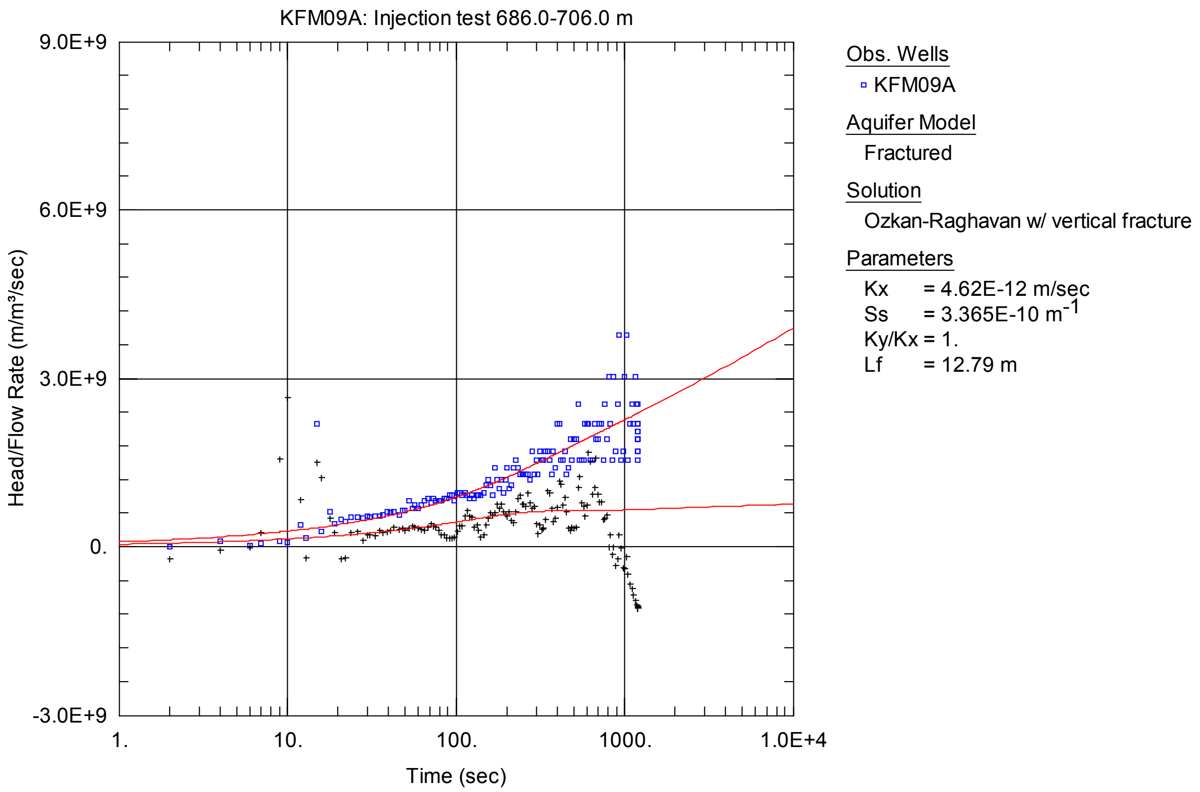


Figure A3-181. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 686.0-706.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

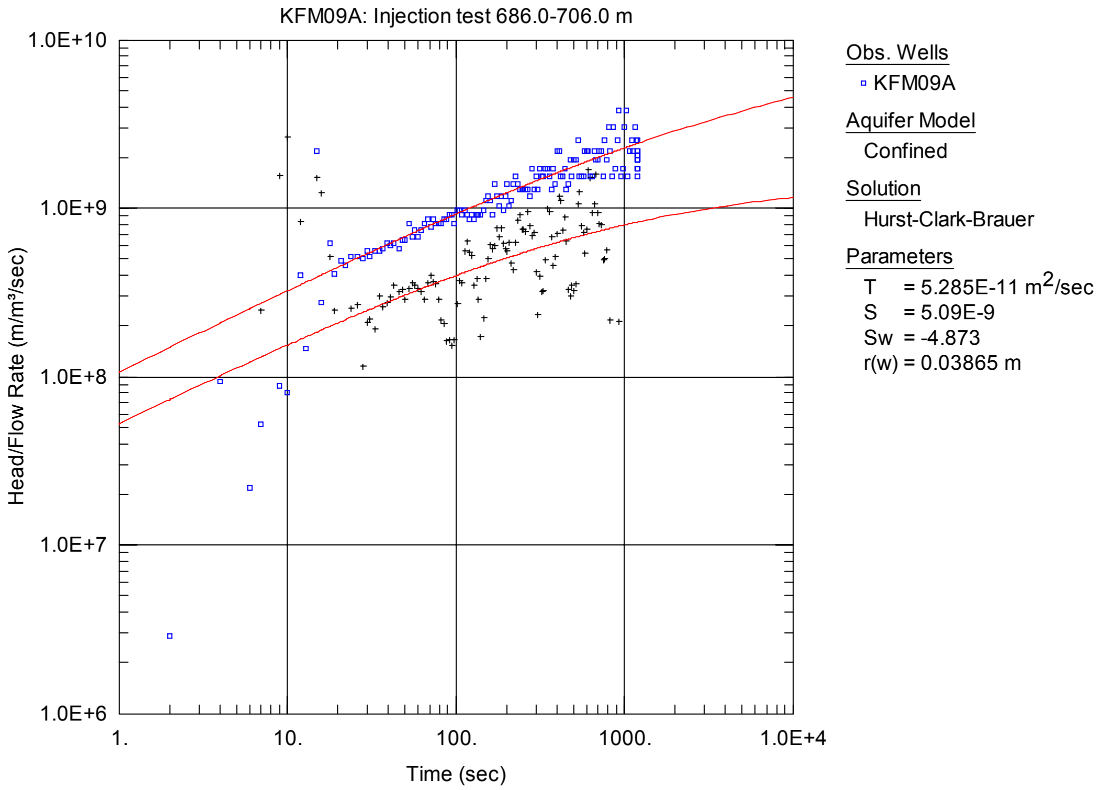


Figure A3-182. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 686.0-706.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for pseudo-radial flow.*

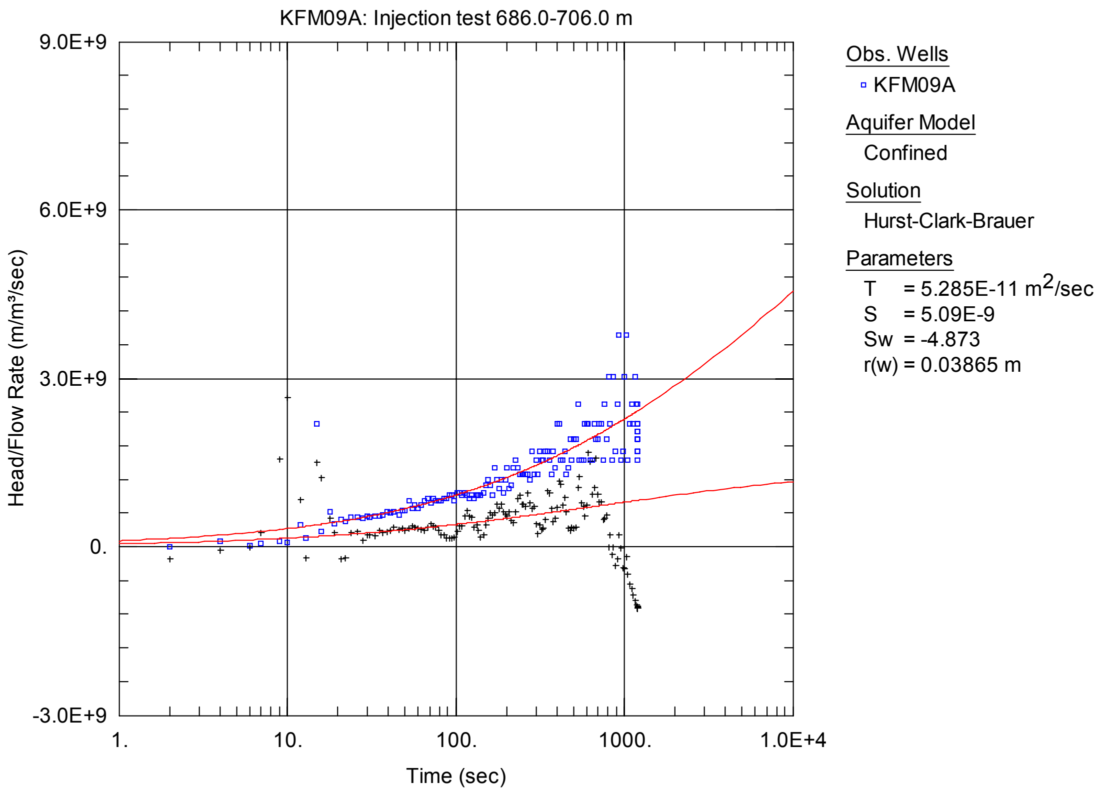


Figure A3-183. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 686.0-706.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for pseudo-radial flow.*

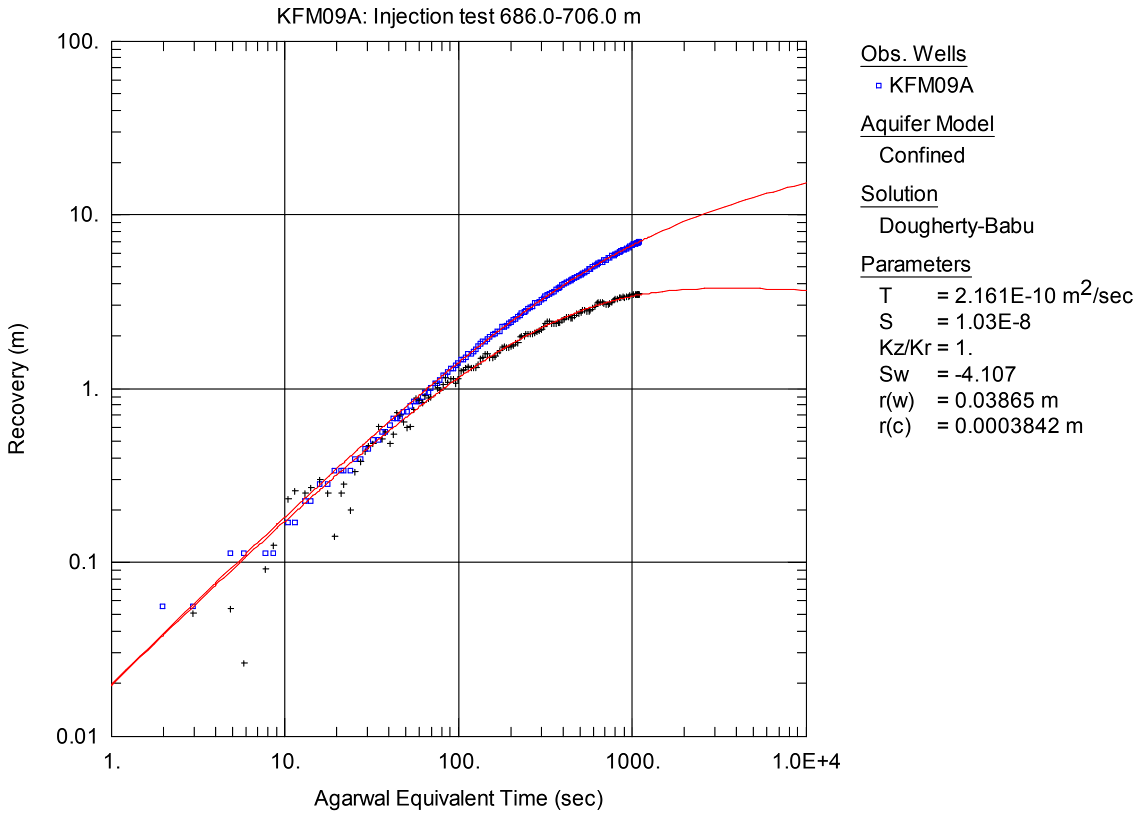


Figure A3-184. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 686.0-706.0m in KFM09A.*

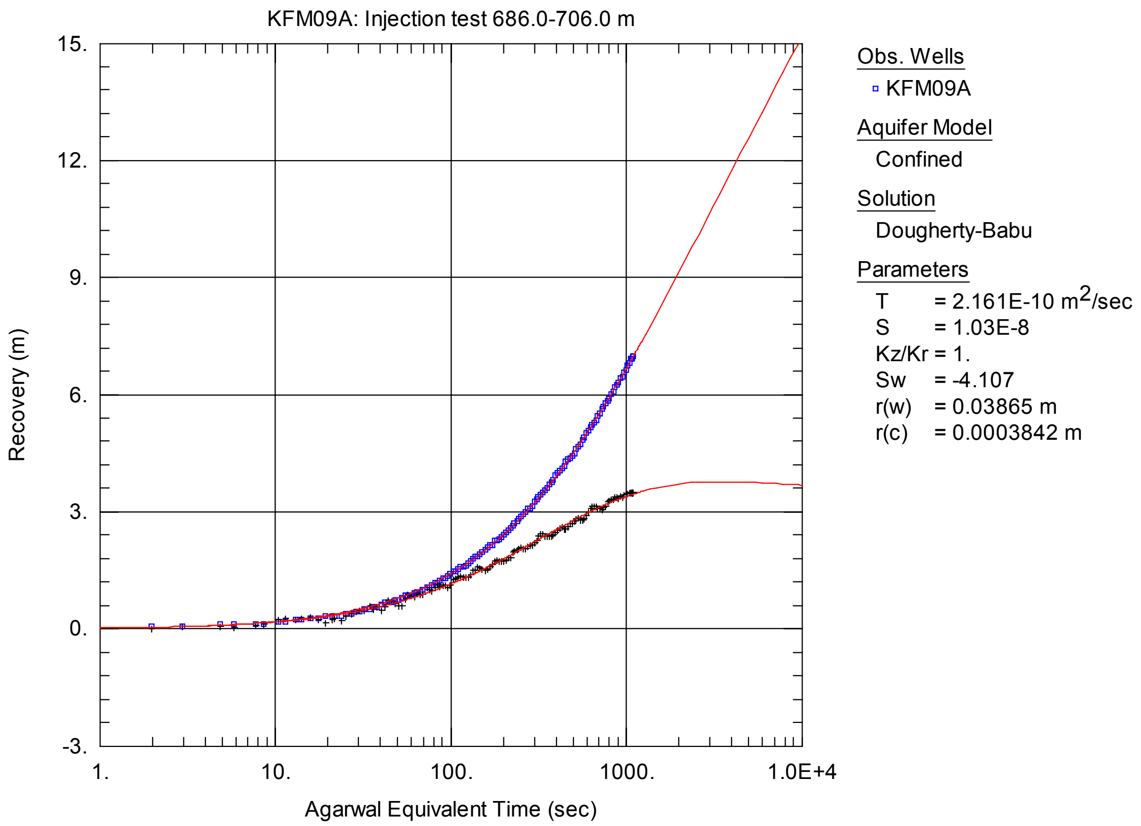


Figure A3-185. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 686.0-706.0 m in KFM09A.*

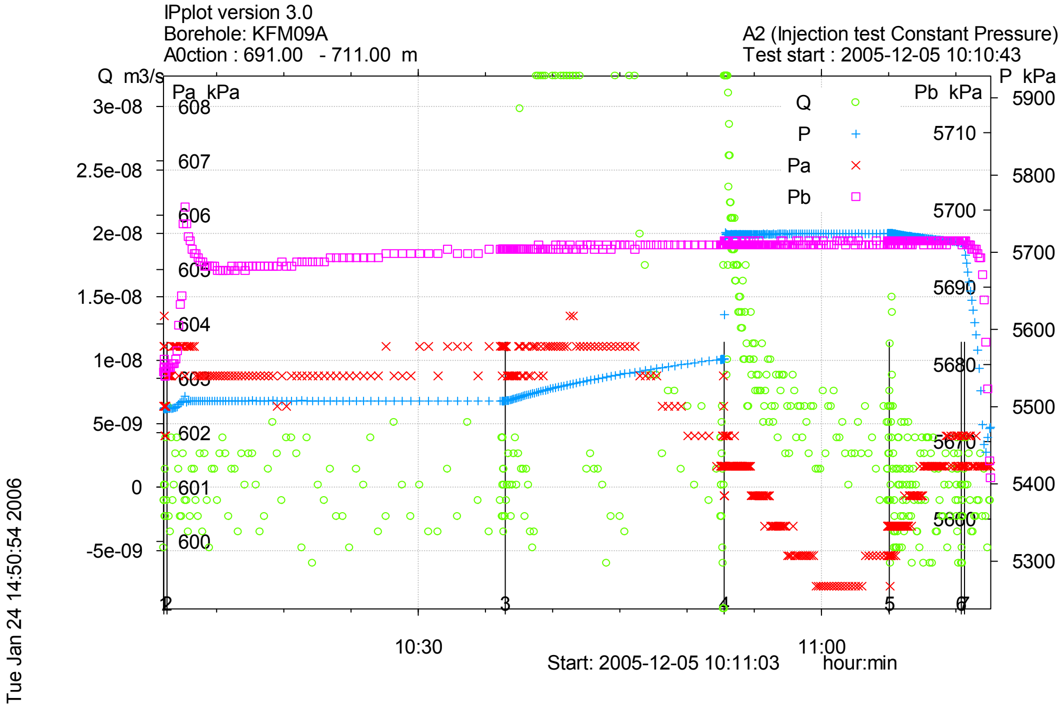


Figure A3-186. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 691.0-711.0 m in borehole KFM09A.*

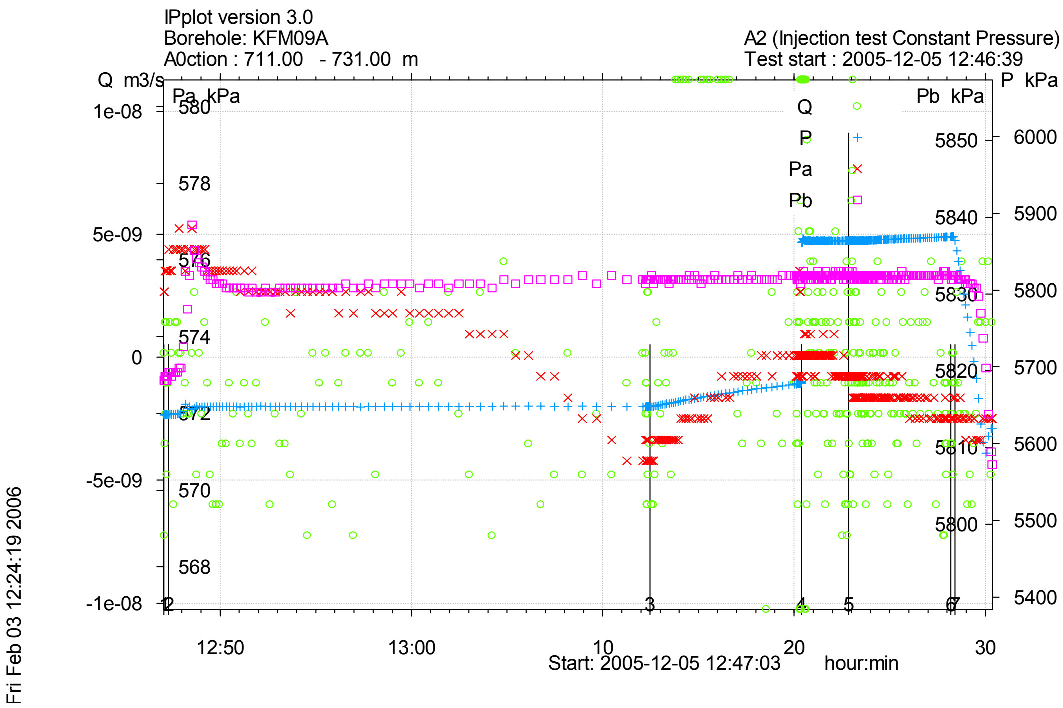


Figure A3-187. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 711.0-731.0 m in borehole KFM09A.*

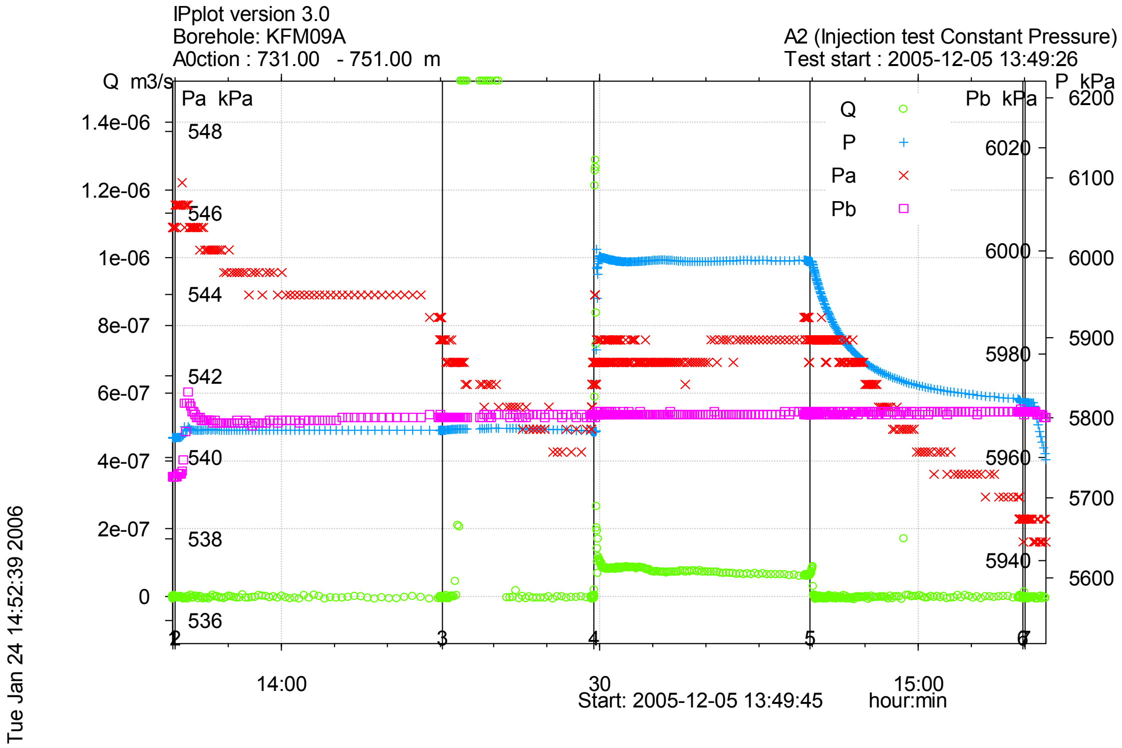


Figure A3-188. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 731.0-751.0 m in borehole KFM09A.

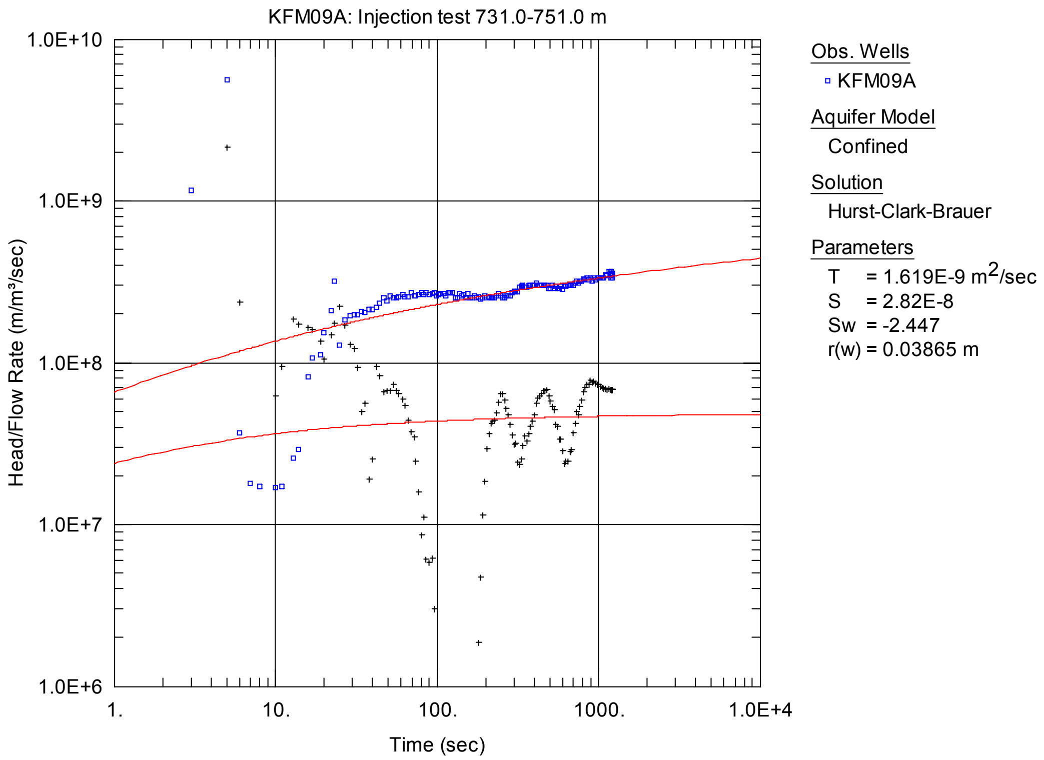


Figure A3-189. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 731.0-751.0 m in KFM09A.

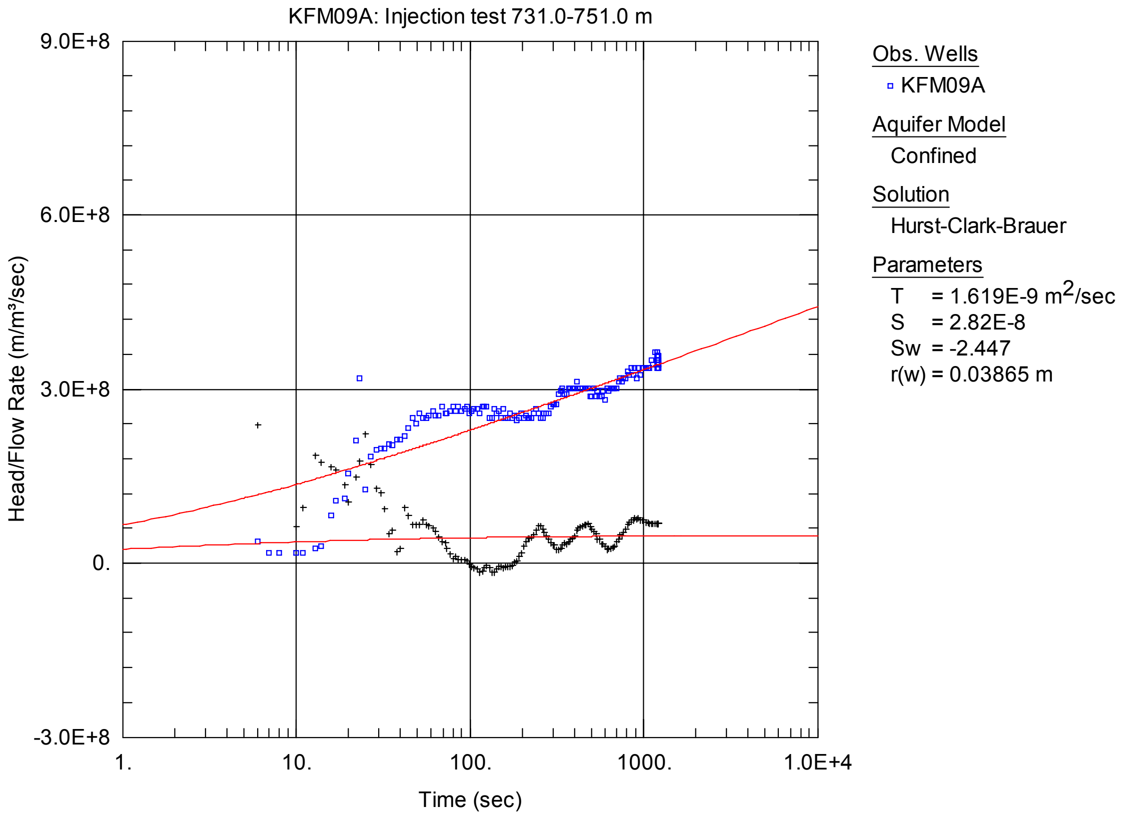


Figure A3-190. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 731.0-751.0 m in KFM09A.*

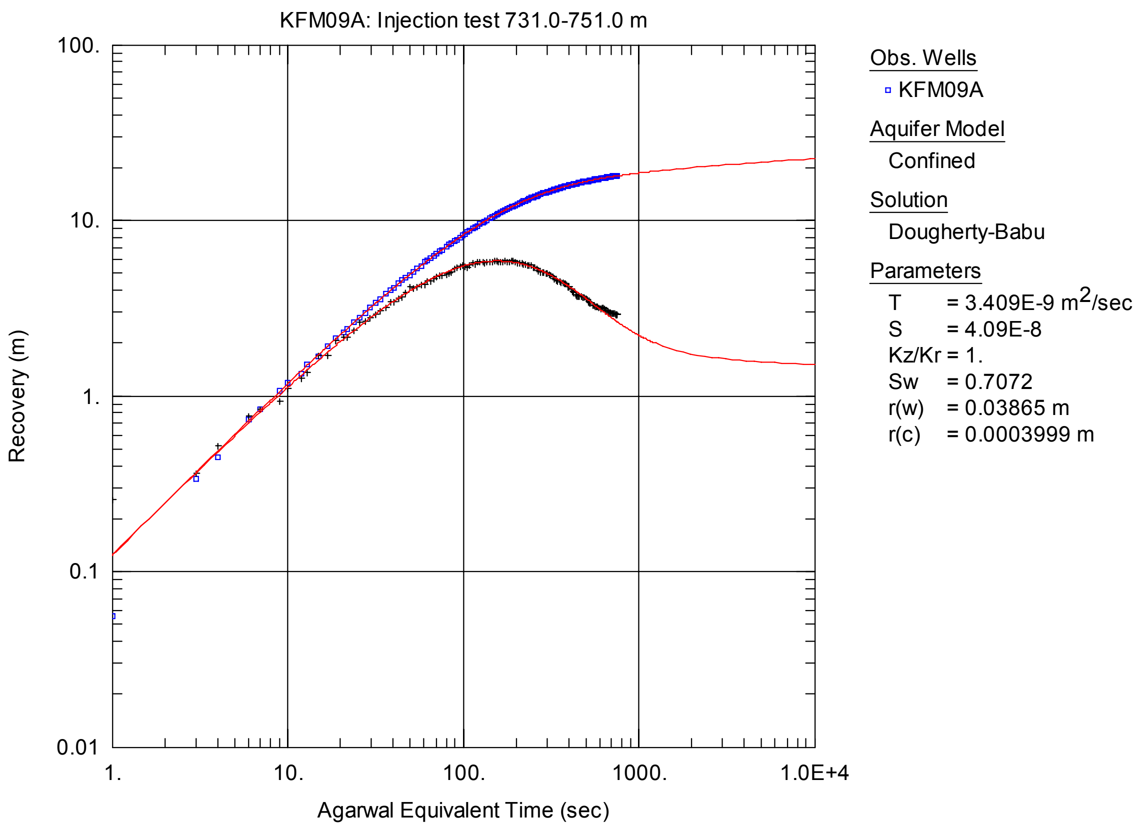


Figure A3-191. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in 731.0-751.0 m in KFM09A.*

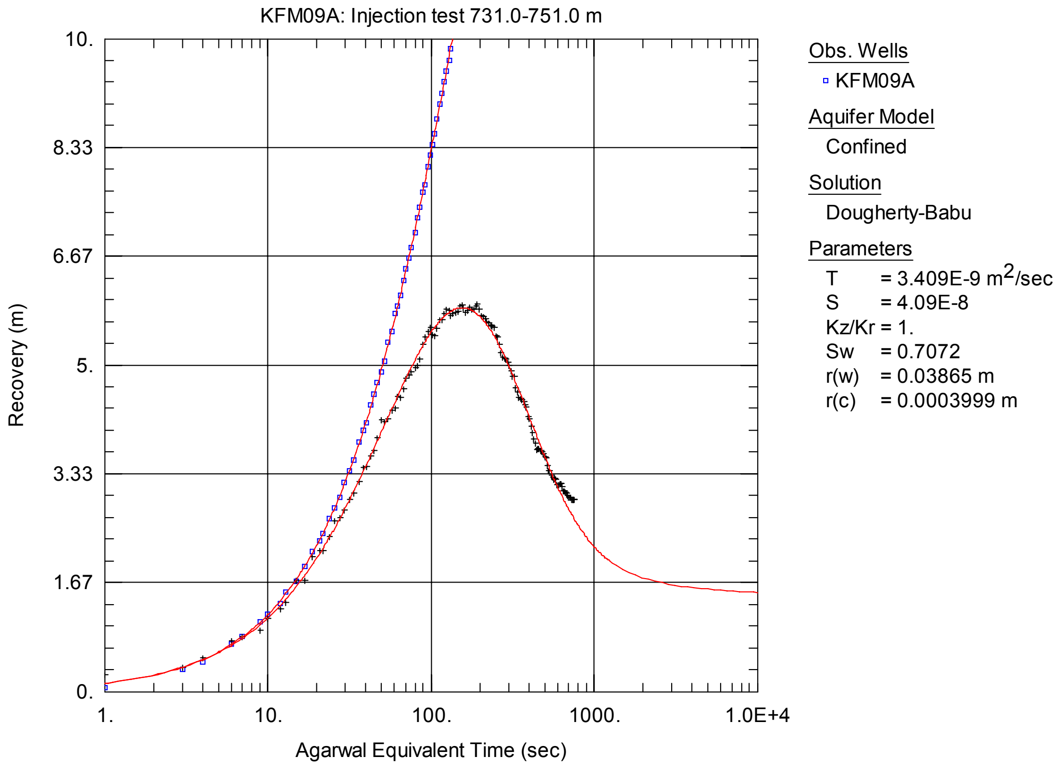


Figure A3-192. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 731.0-751.0 m in KFM09A.*

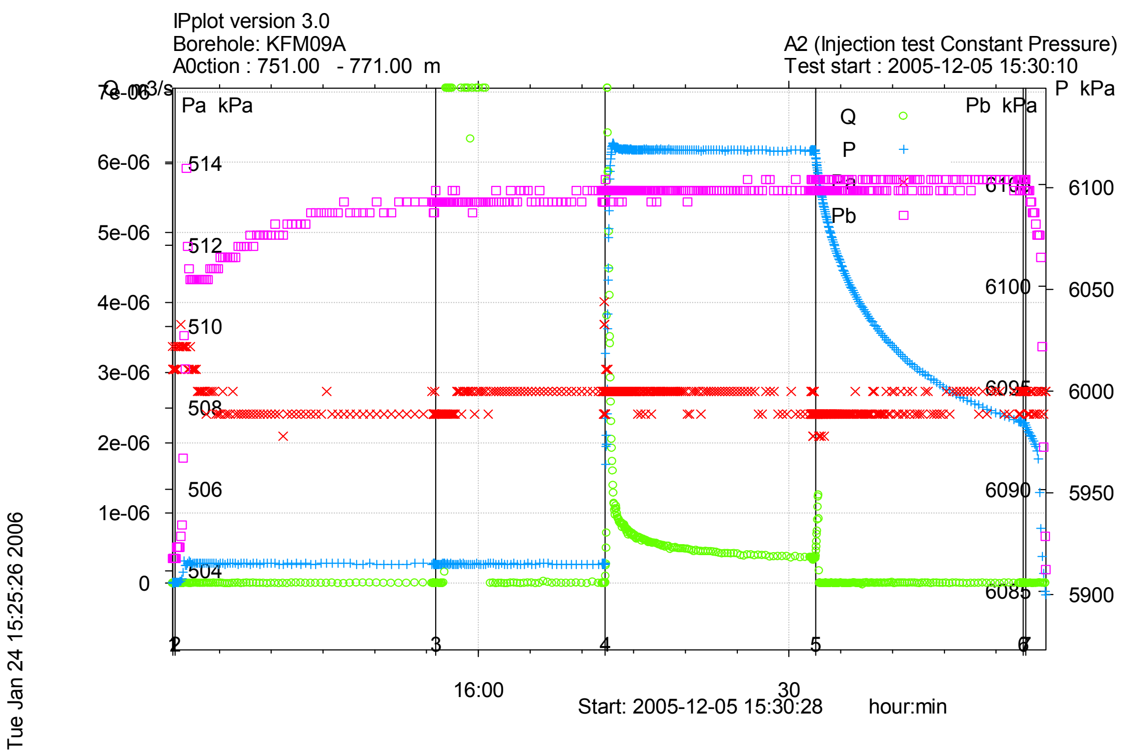


Figure A3-193. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 751.0-771.0 m in borehole KFM09A.*

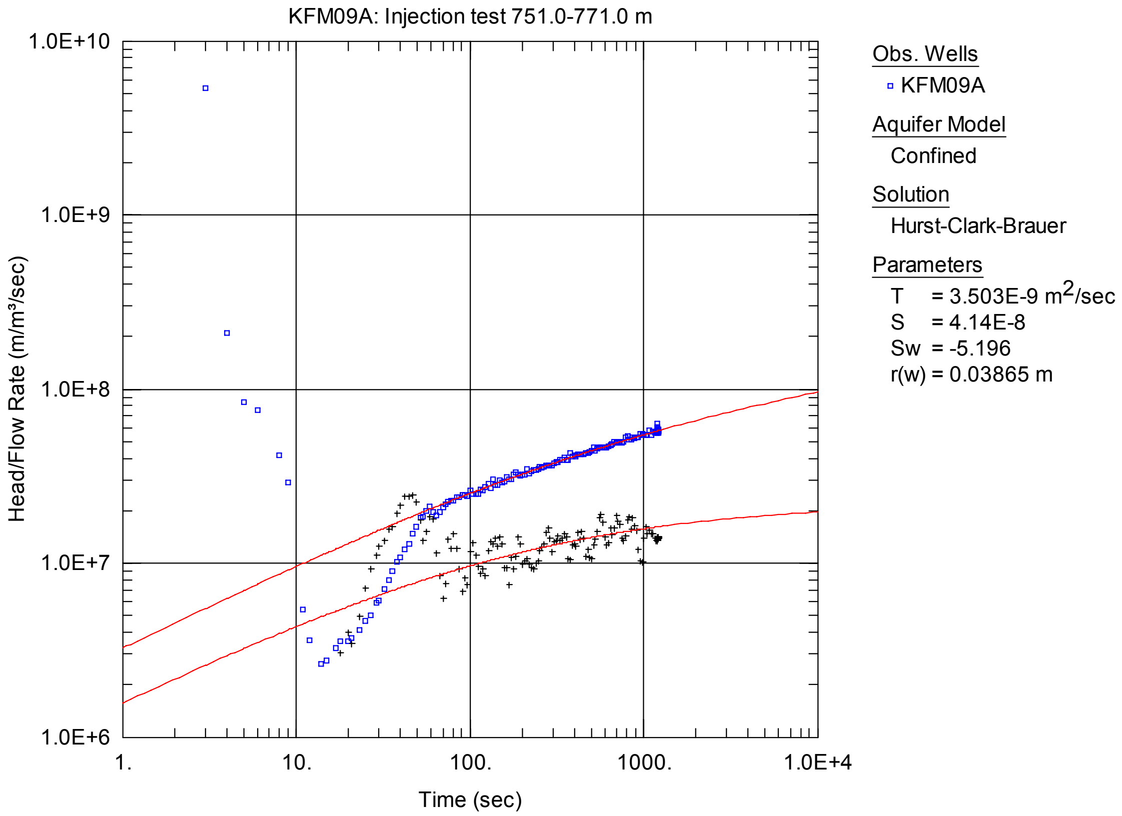


Figure A3-194. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 751.0-771.0 m in KFM09A.*

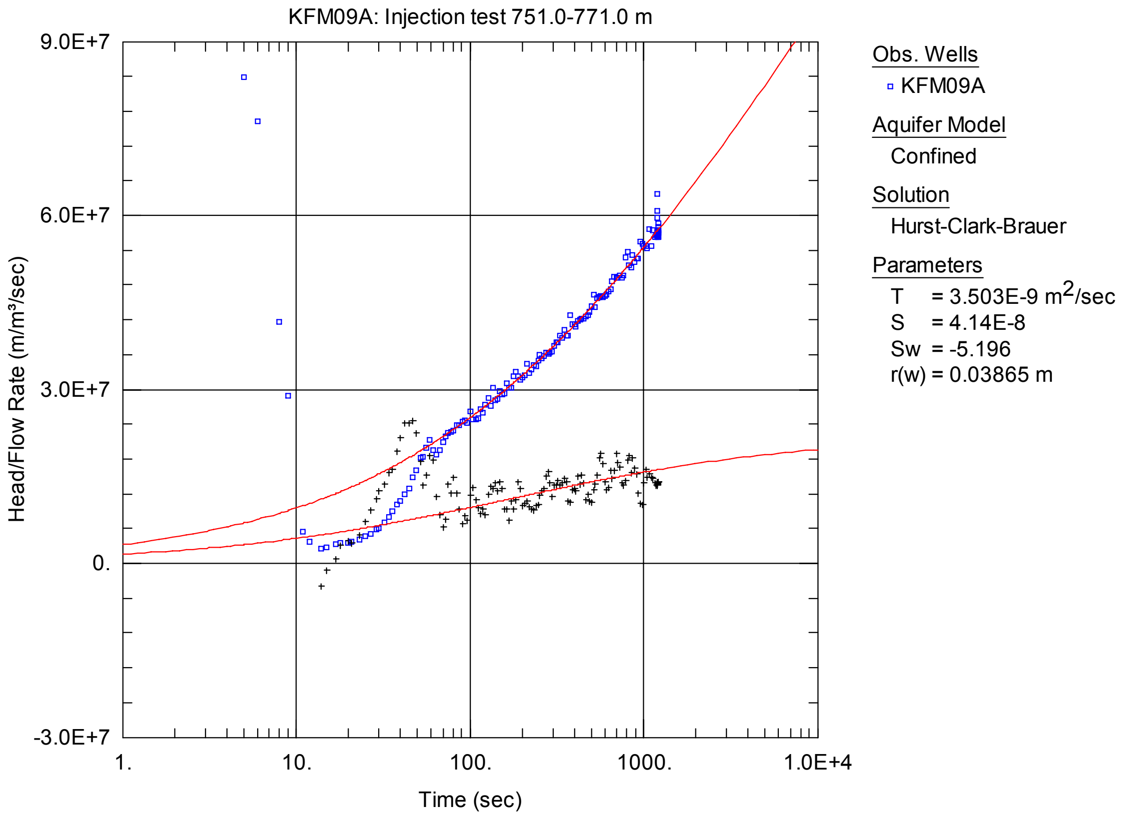


Figure A3-195. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in 751.0-771.0 m in KFM09A.*

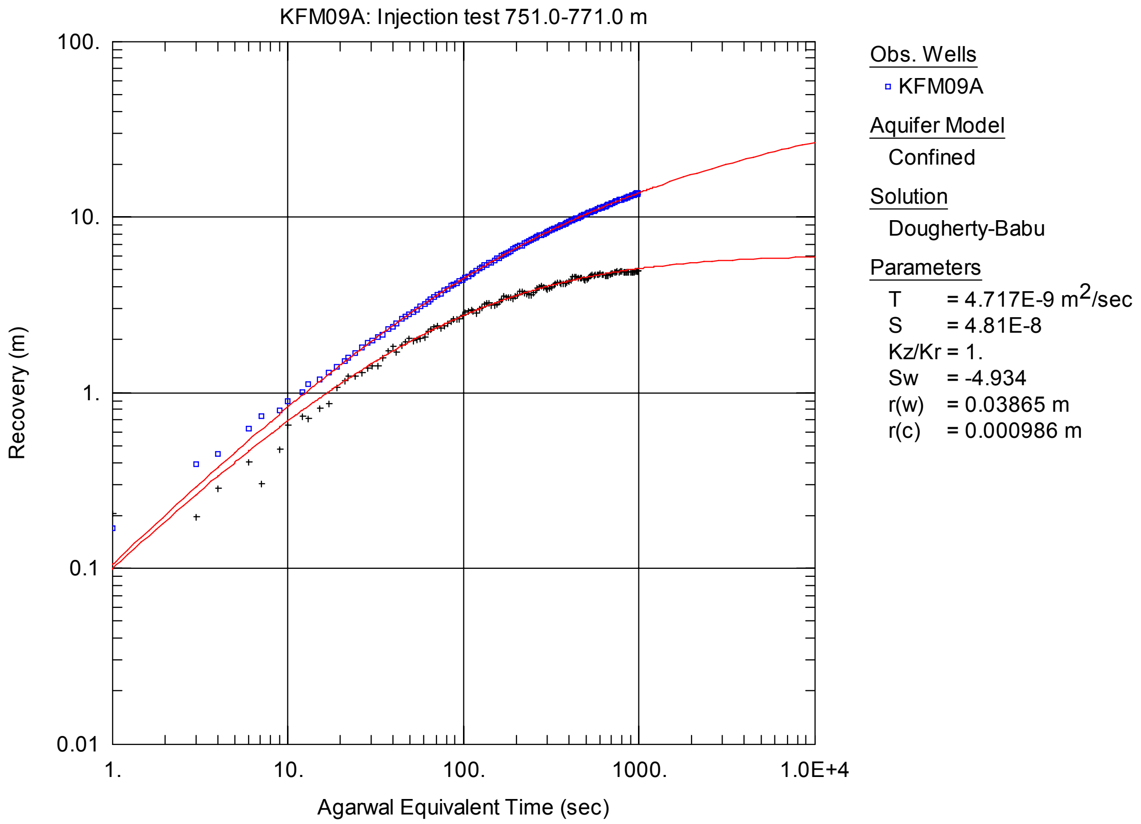


Figure A3-196. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 751.0-771.0 m in KFM09A.*

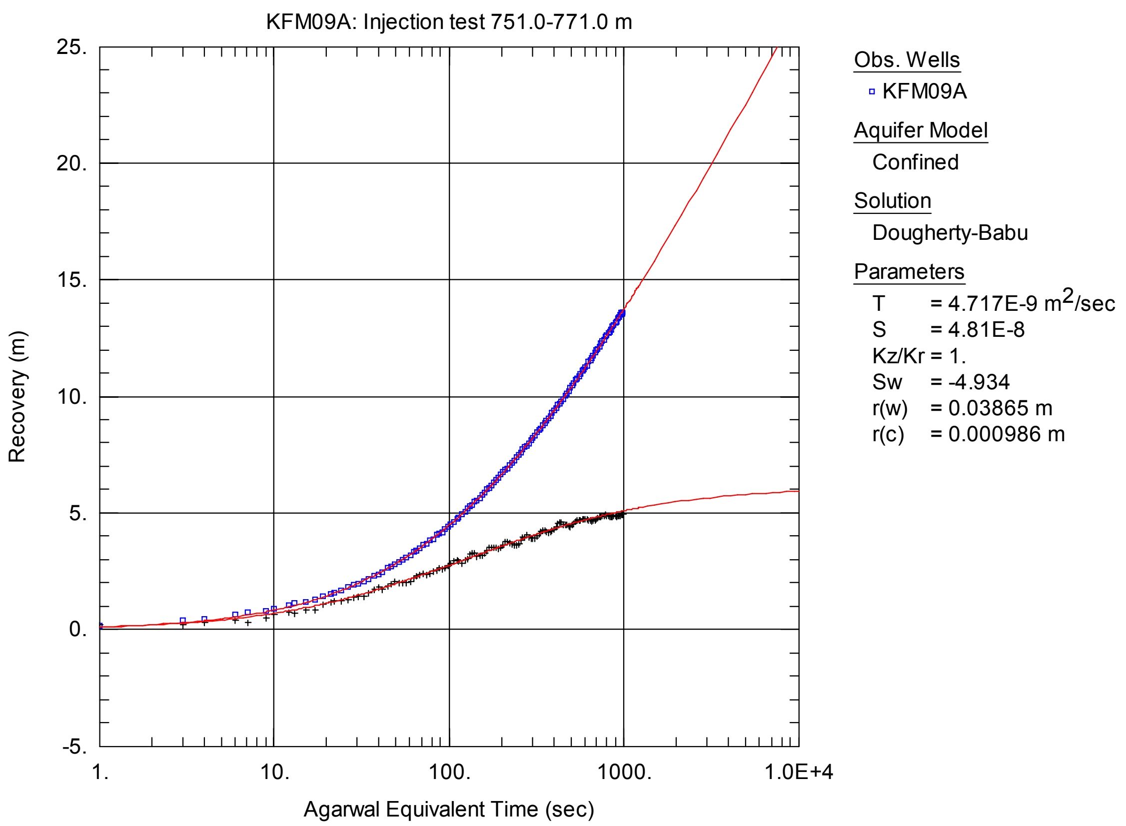


Figure A3-197. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 751.0-771.0 m in KFM09A.*

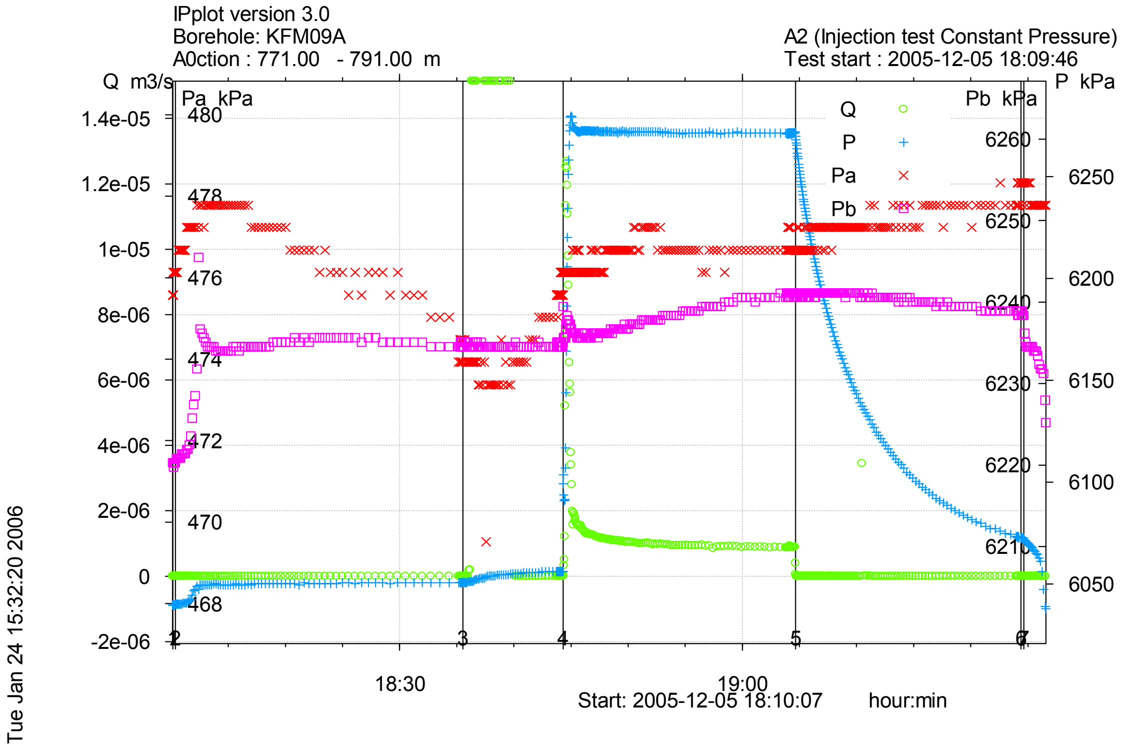


Figure A3-198. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 771.0-791.0 m in borehole KFM09A.*

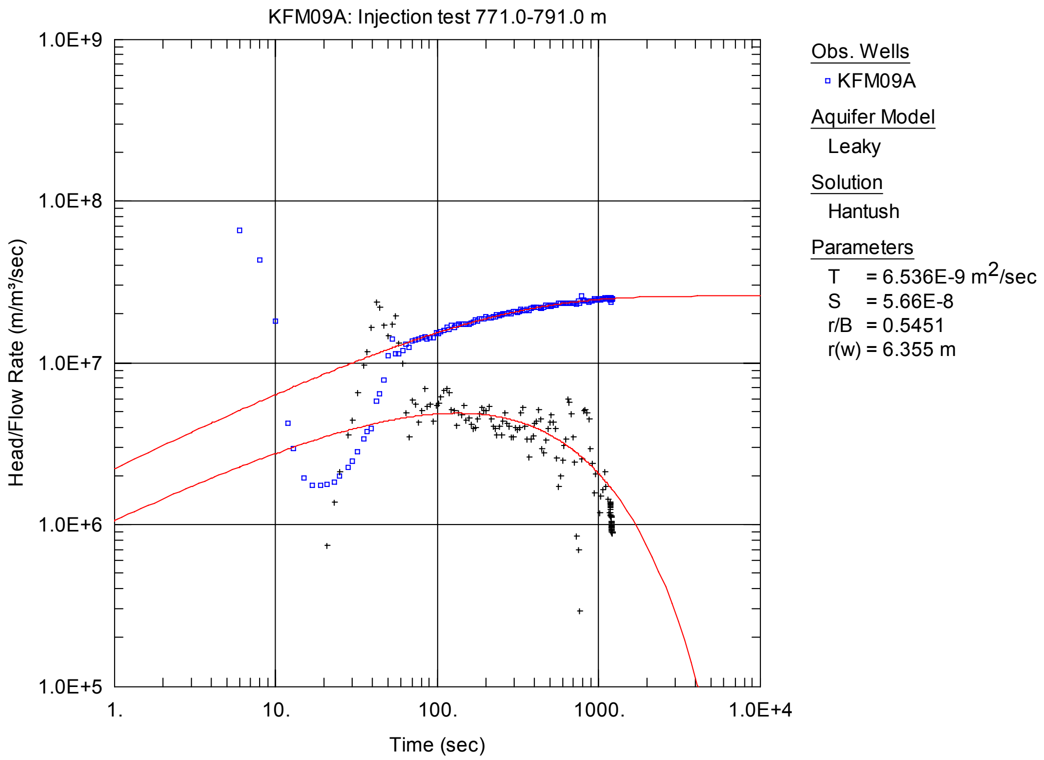


Figure A3-199. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 771.0-791.0 m in KFM09A.*

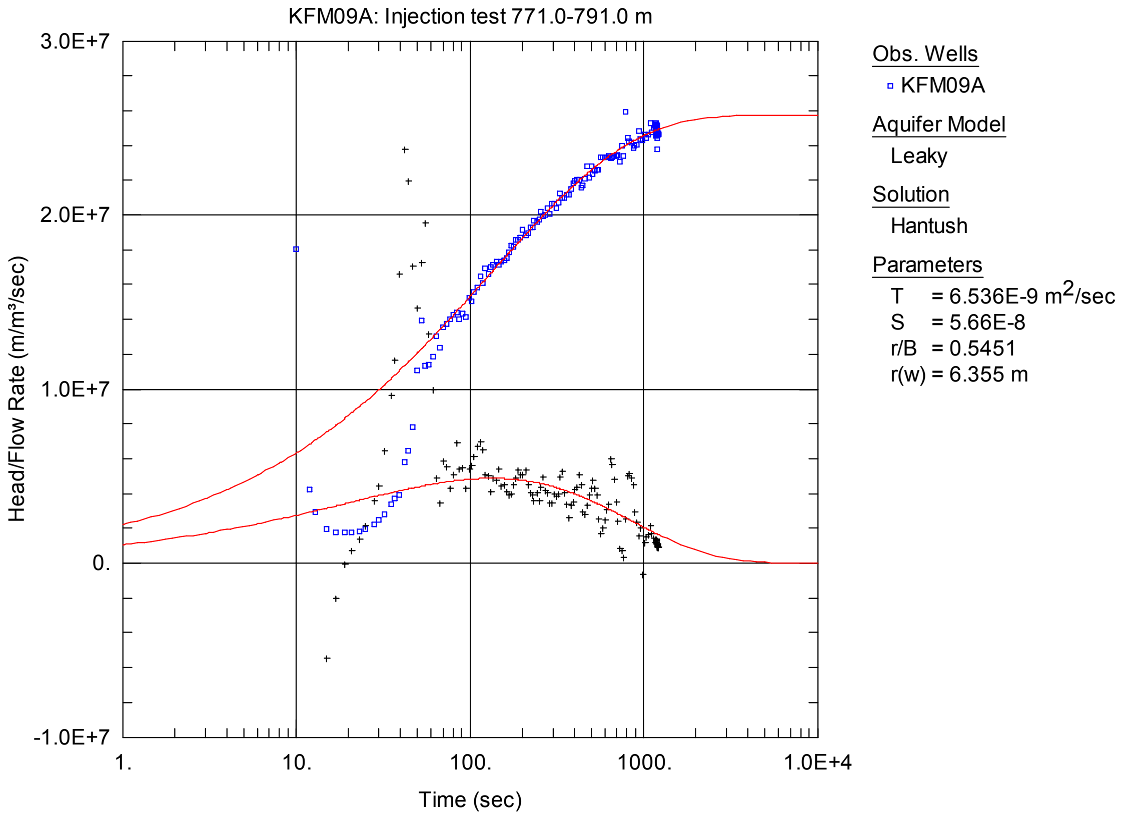


Figure A3-200. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 771.0-791.0 m in KFM09A.*

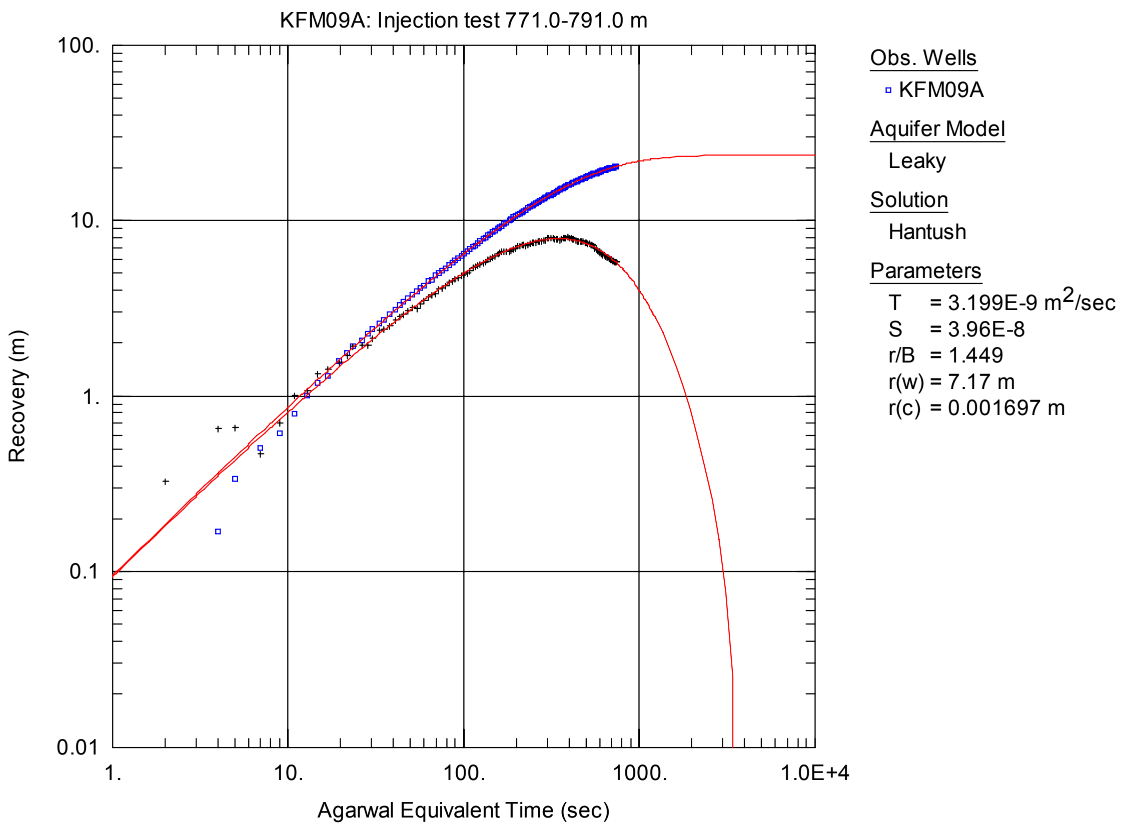


Figure A3-201. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 771.0-791.0 m in KFM09A.*

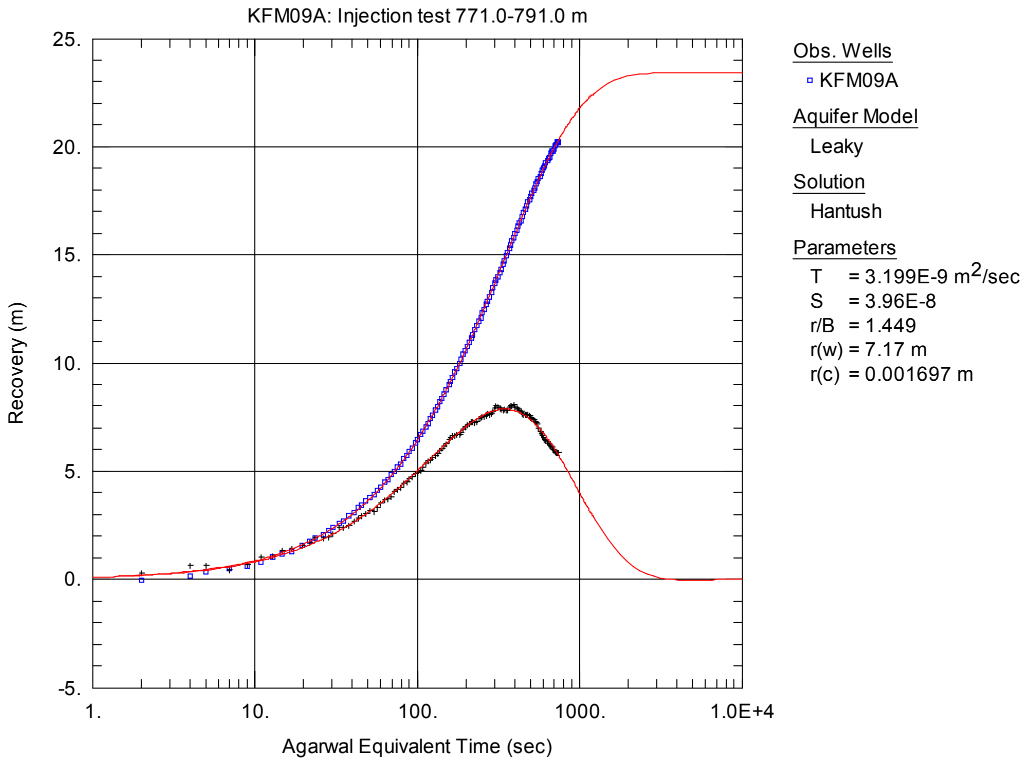


Figure A3-202. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 771.0-791.0 m in KFM09A.*

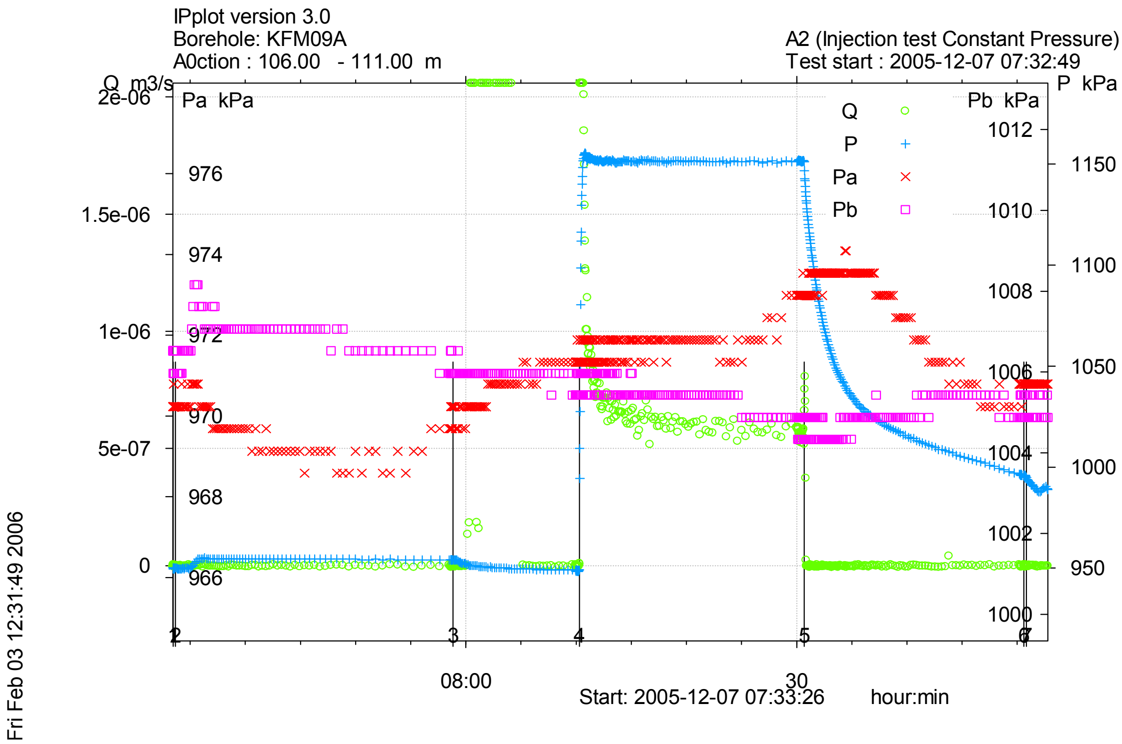


Figure A3-203. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 106.0-111.0 m in borehole KFM09A.*

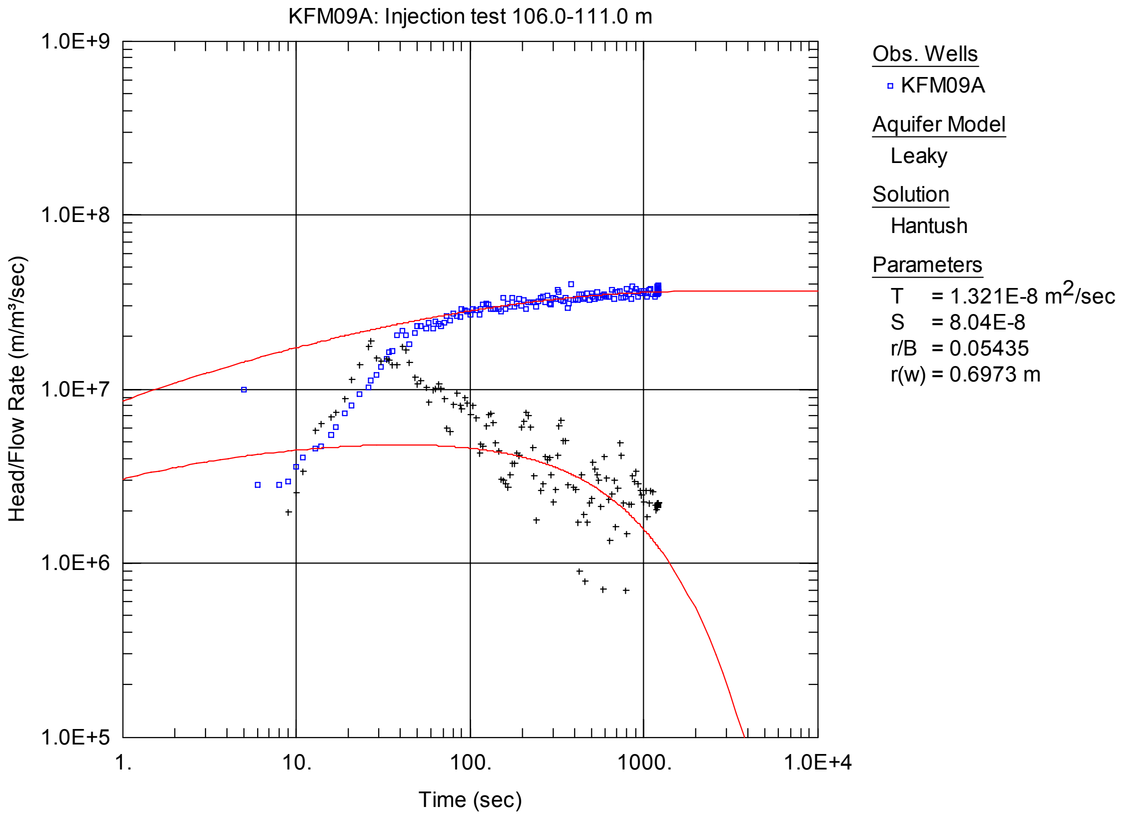


Figure A3-204. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 106.0-111.0 m in KFM09A.*

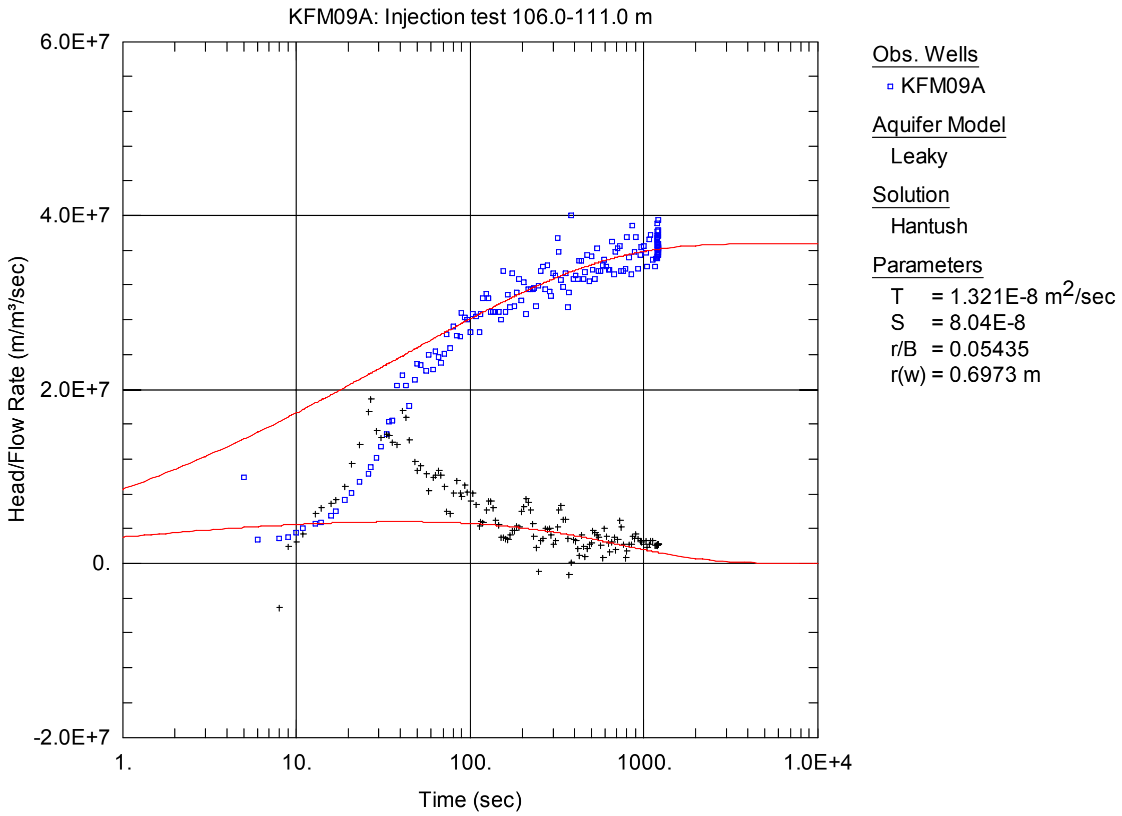


Figure A3-205. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 106.0-111.0 m in KFM09A.*

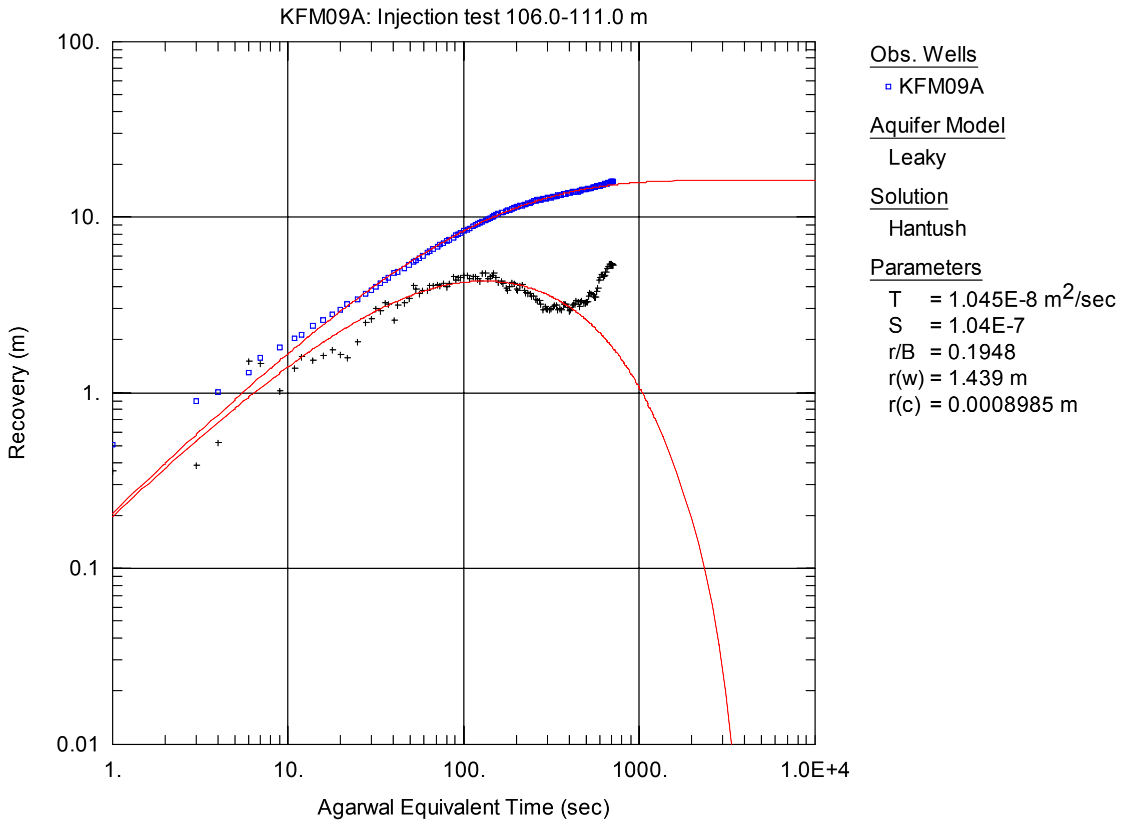


Figure A3-206. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 106.0-111.0 m in KFM09A.*

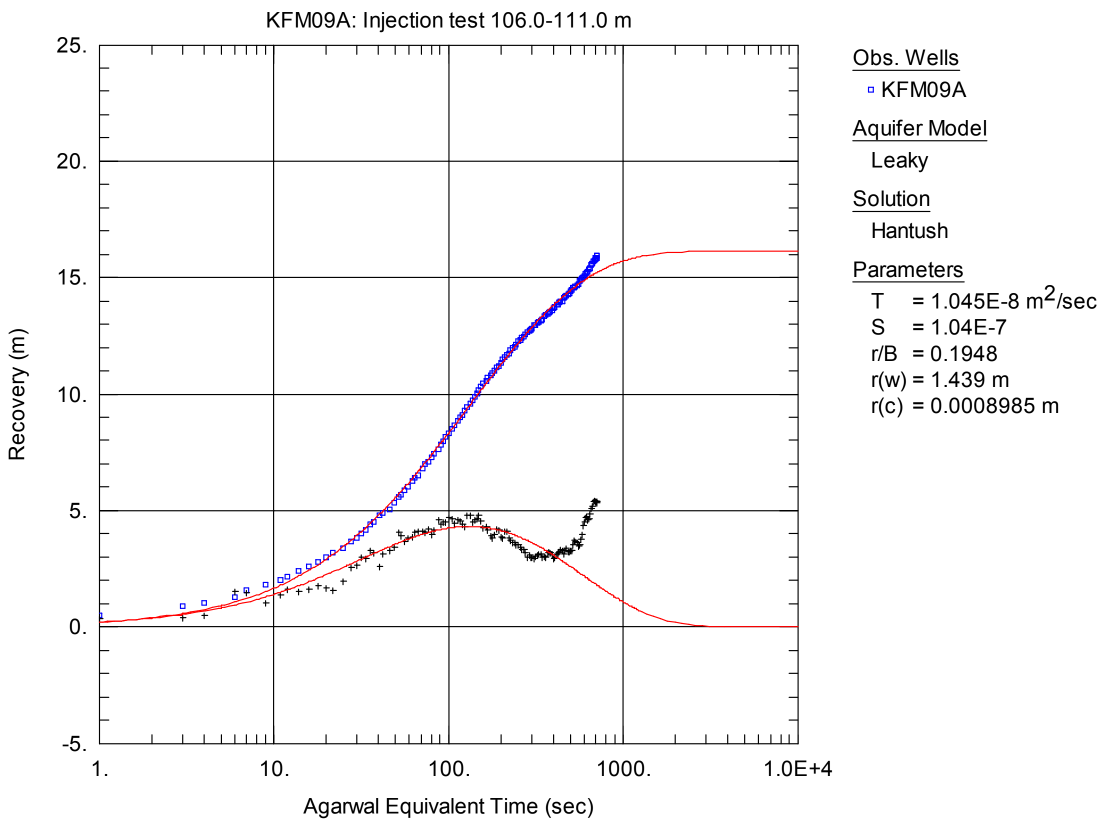


Figure A3-207. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 106.0-111.0 m in KFM09A.*

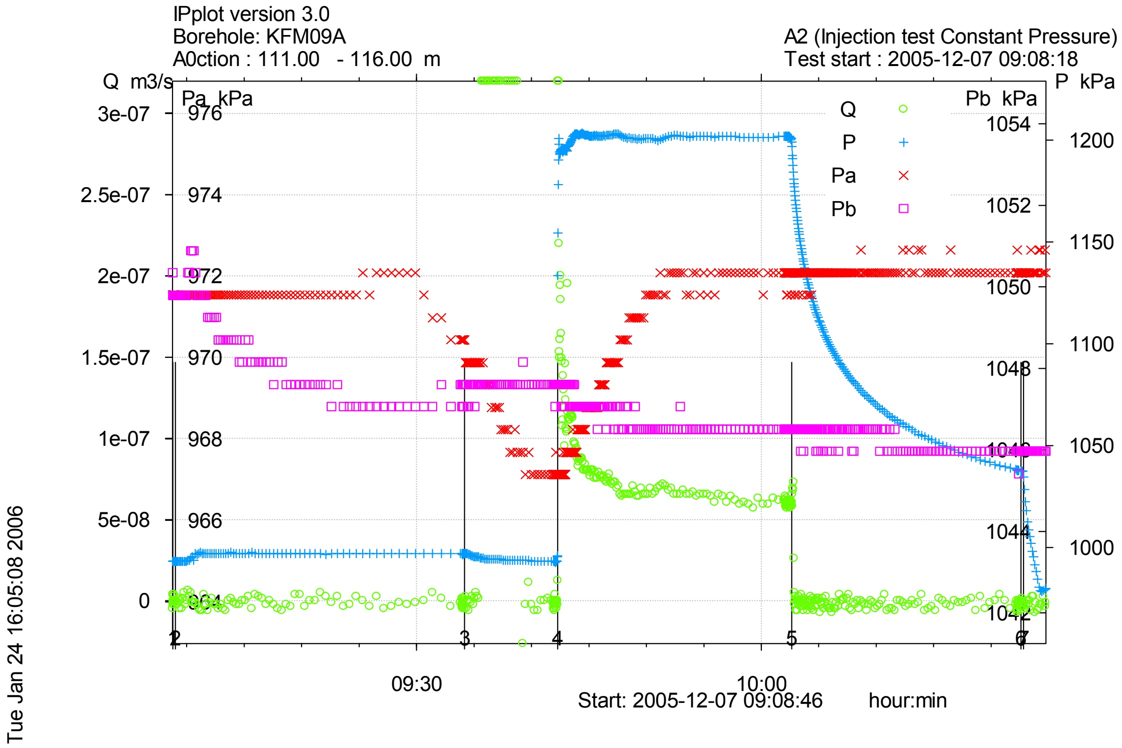


Figure A3-208. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 111.0-116.0 m in borehole KFM09A.*

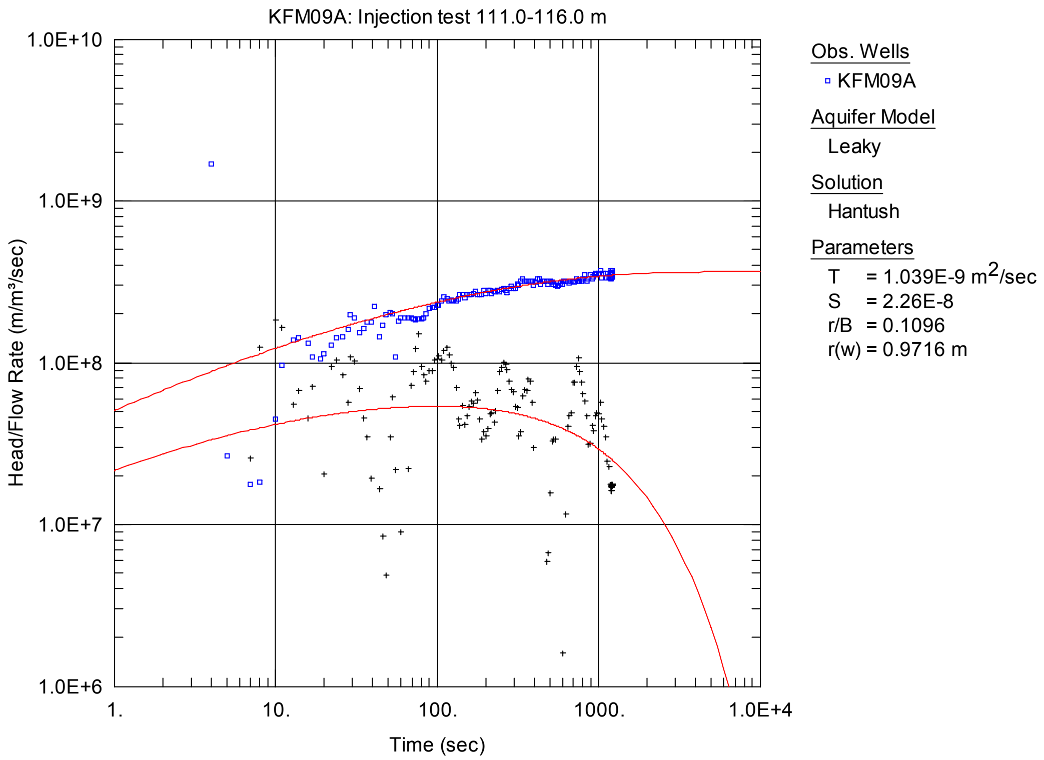


Figure A3-209. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 111.0-116.0 m in KFM09A.*

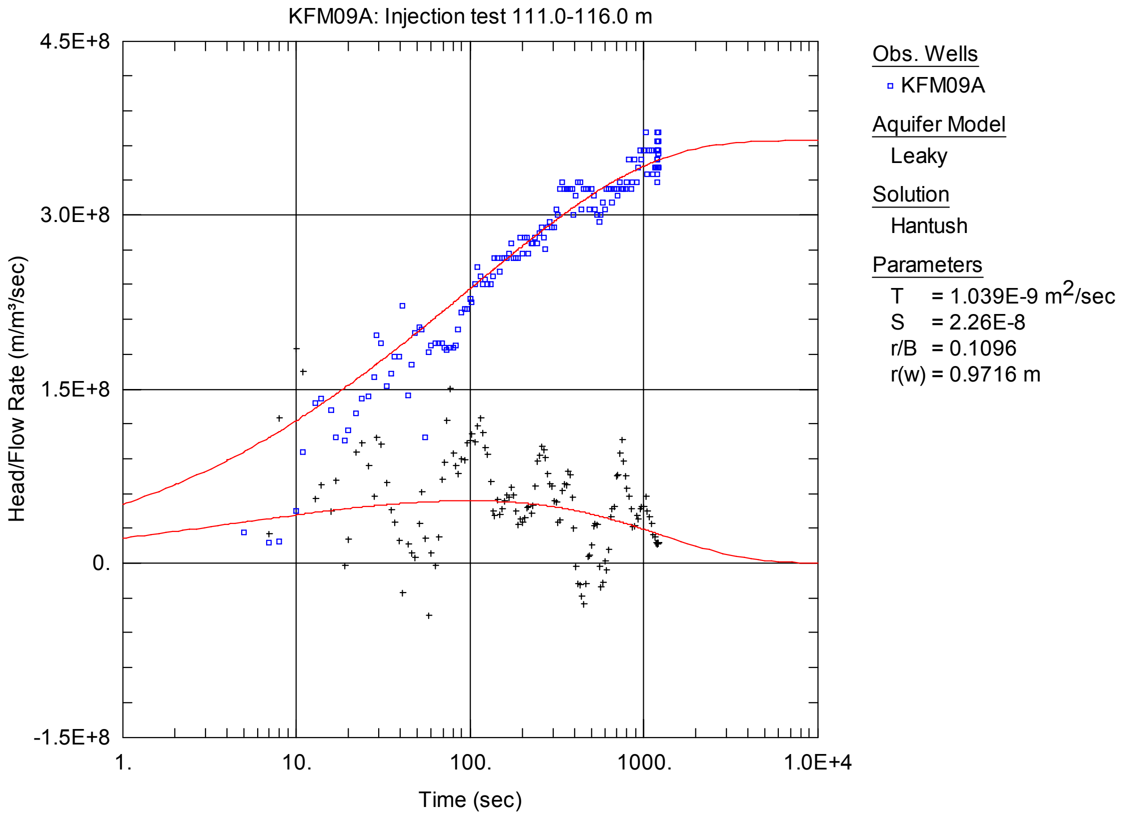


Figure A3-210. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 111.0-116.0 m in KFM09A.*

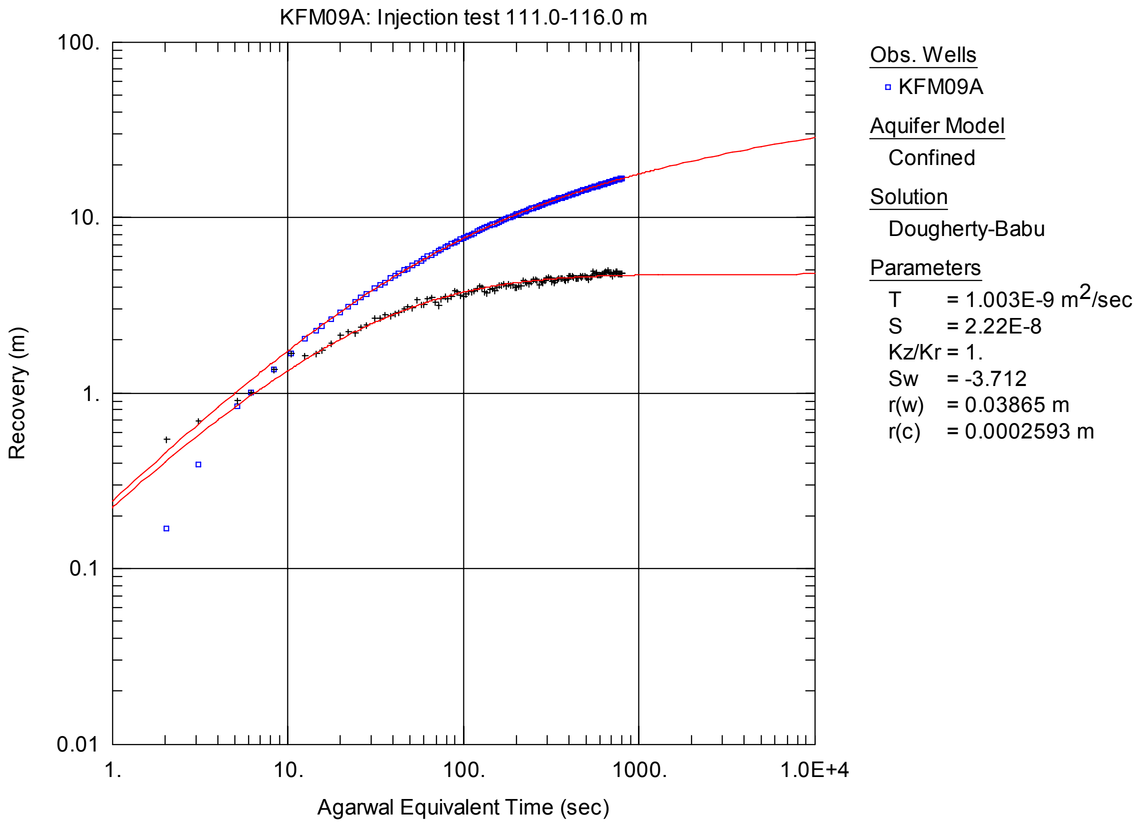


Figure A3-211. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 111.0-116.0 m in KFM09A.*

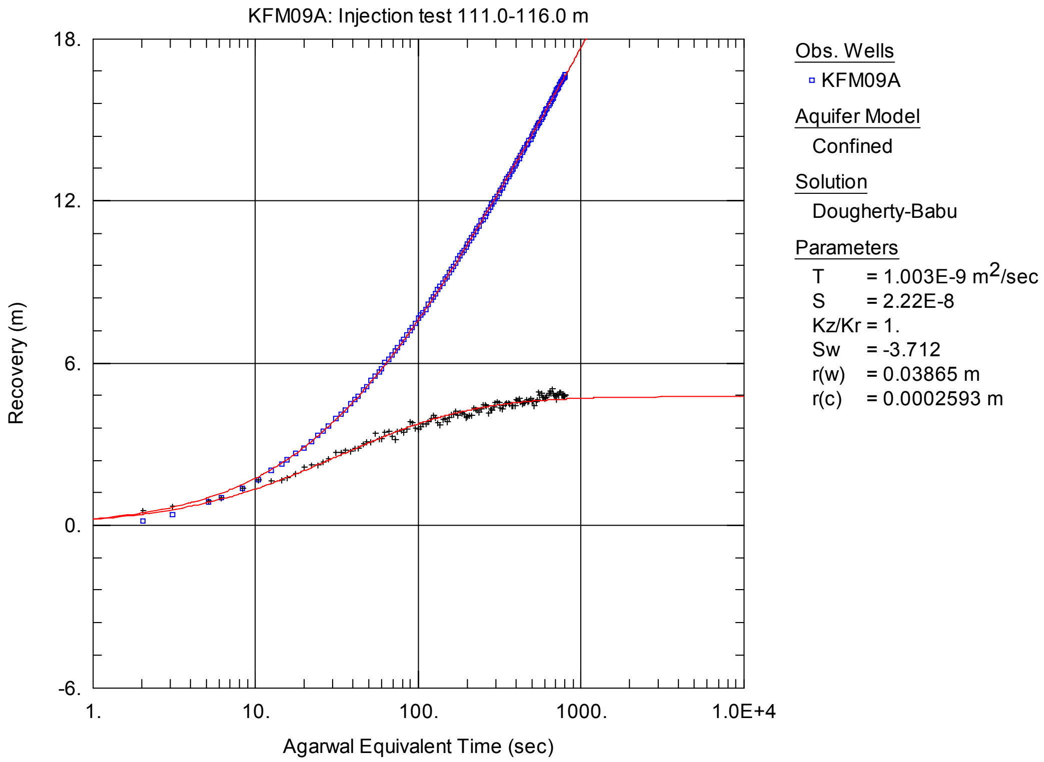


Figure A3-212. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 111.0-116.0 m in KFM09A.*

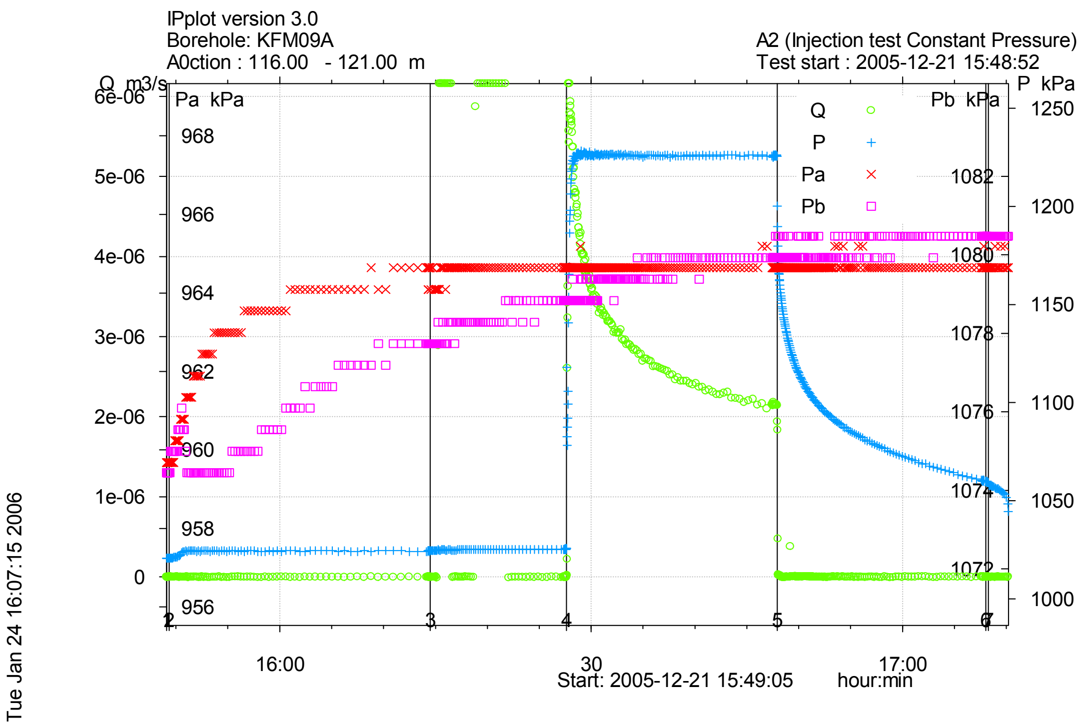


Figure A3-213. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 116.0-121.0 m in borehole KFM09A.*

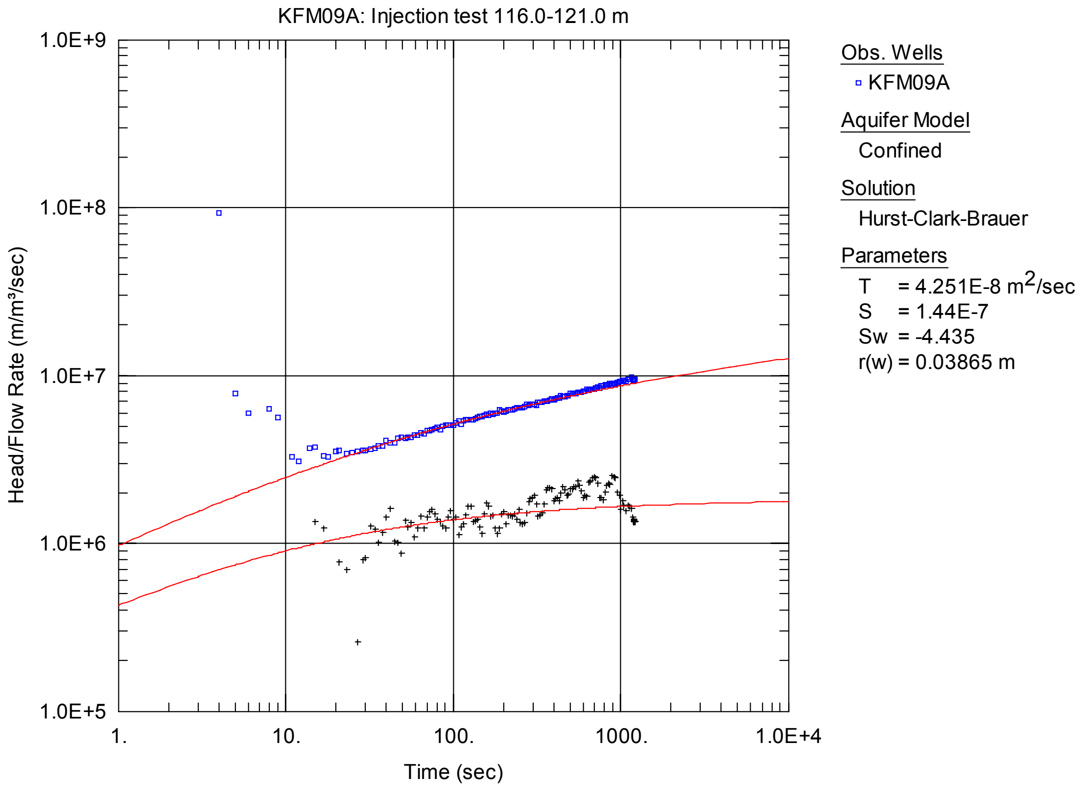


Figure A3-214. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 116.0-121.0 m in KFM09A. This plot shows the first of two different PRF:s during the injection period in this section.*

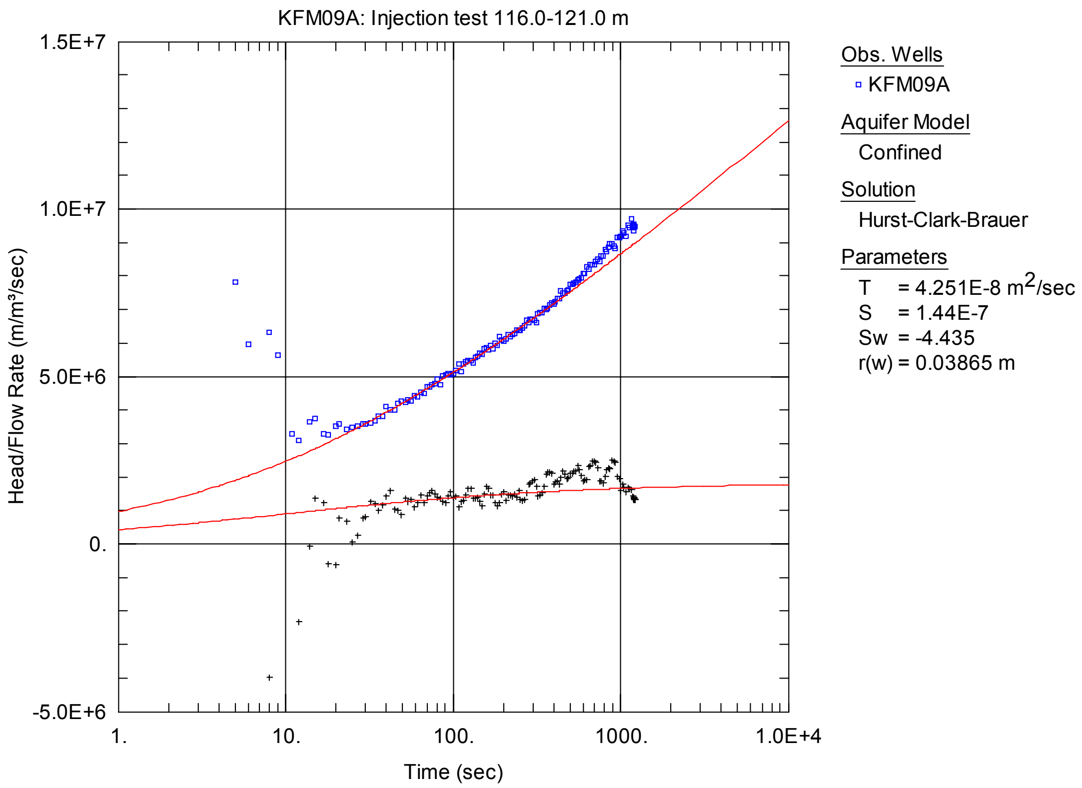


Figure A3-215. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 116.0-121.0 m in KFM09A. This plot shows the first of two different PRF:s during the injection period in this section.*

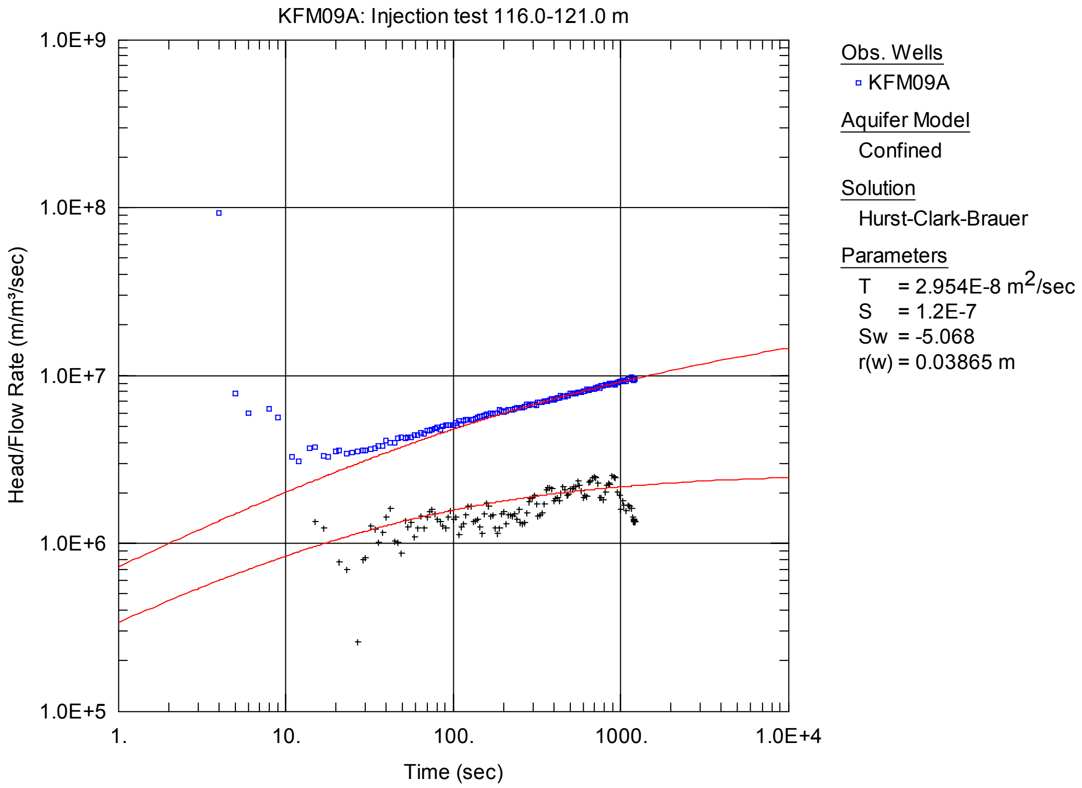


Figure A3-216. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 116.0-121.0 m in KFM09A. This plot shows a fit to the second of two different PRF:s during the injection period in this section.*

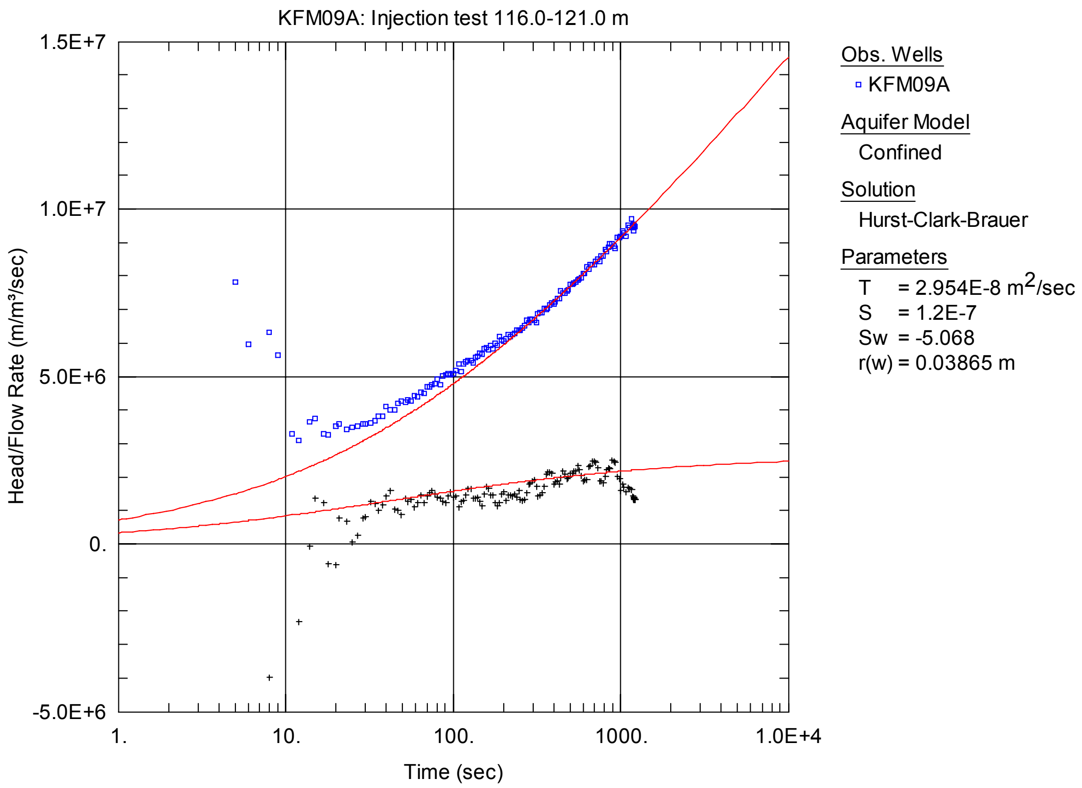


Figure A3-217. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 116.0-121.0 m in KFM09A. This plot shows a fit to the second of two different PRF:s during the injection period in this section.*

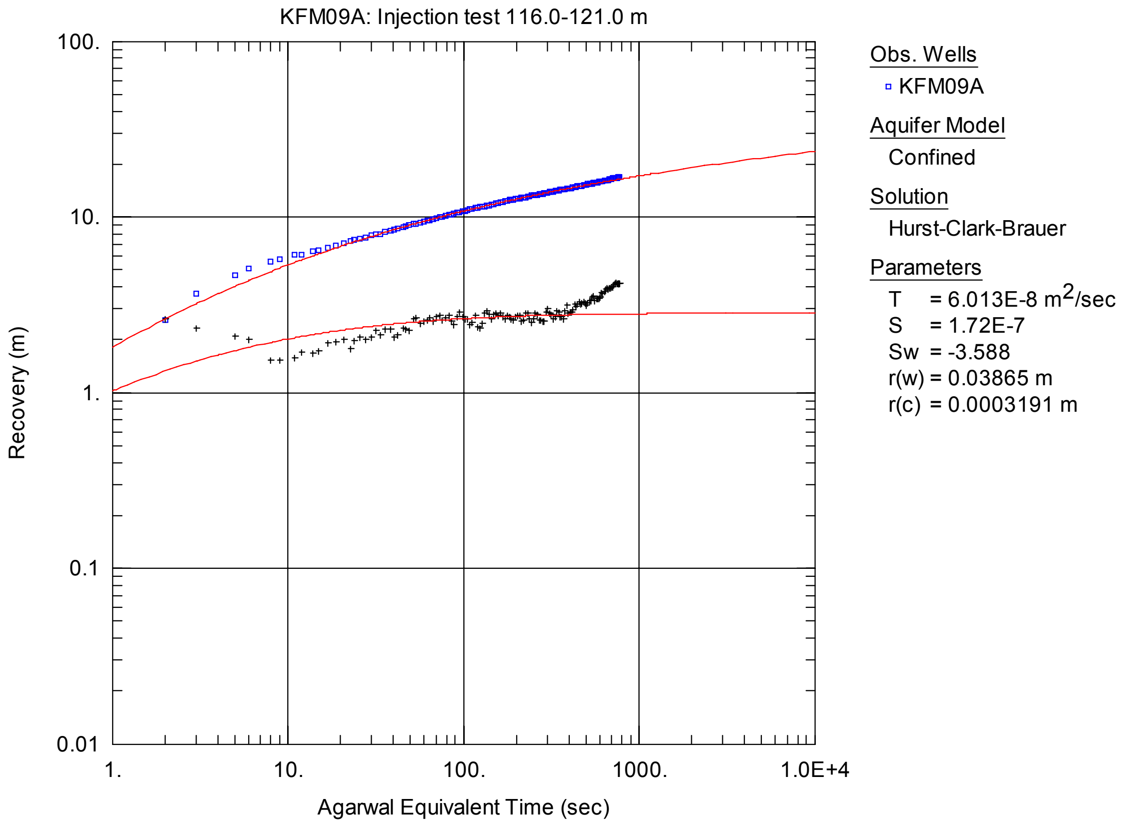


***Figure A3-218.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 116.0-121.0 m in KFM09A.*

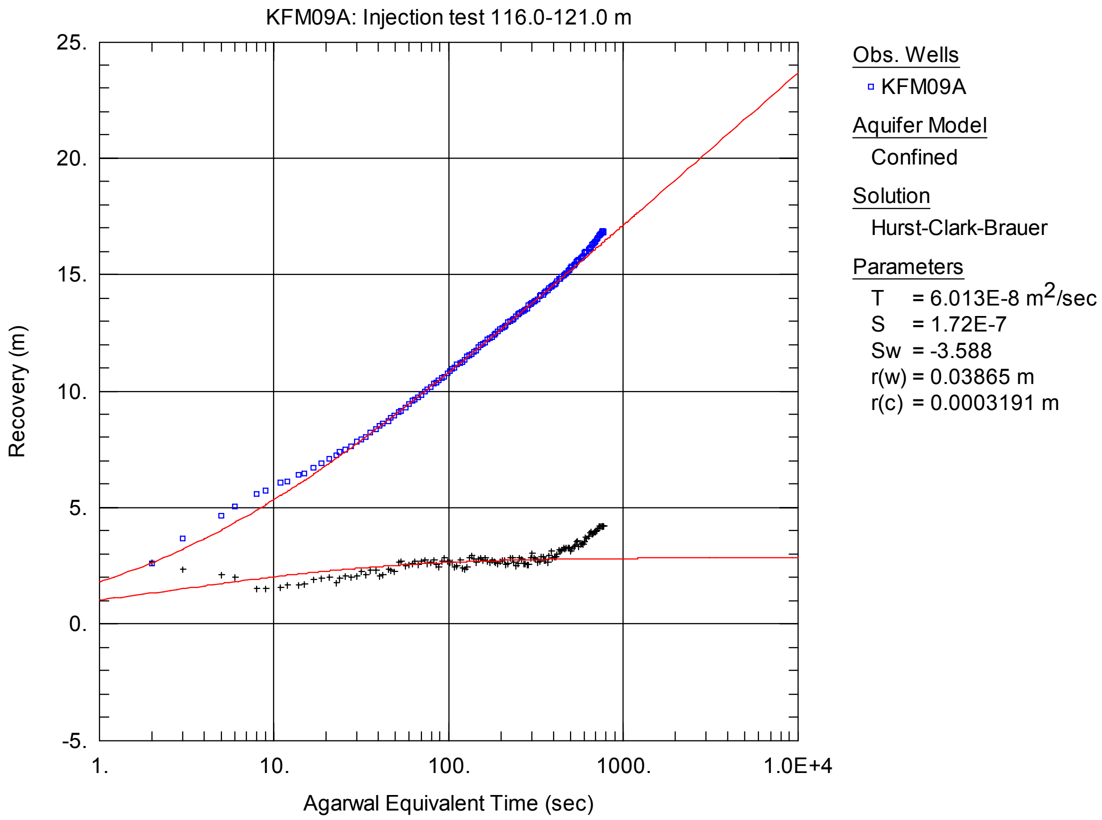


***Figure A3-219.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 116.0-121.0 m in KFM09A.*

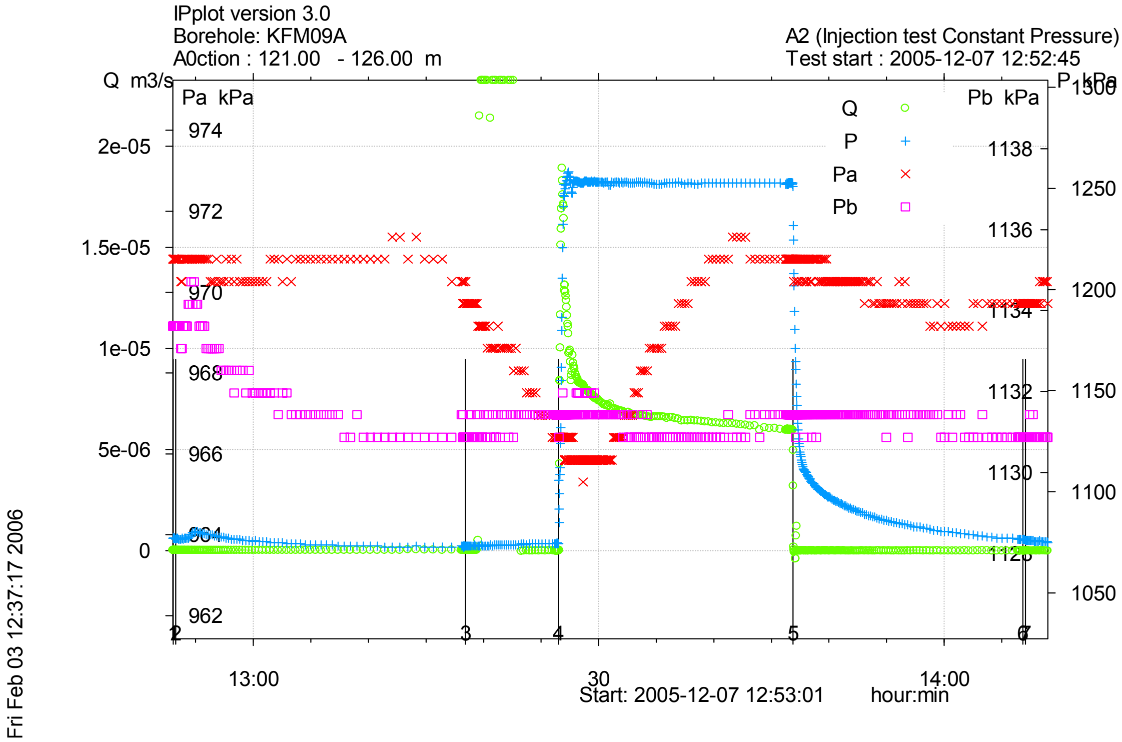


Figure A3-220. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 121.0-126.0 m in borehole KFM09A.*

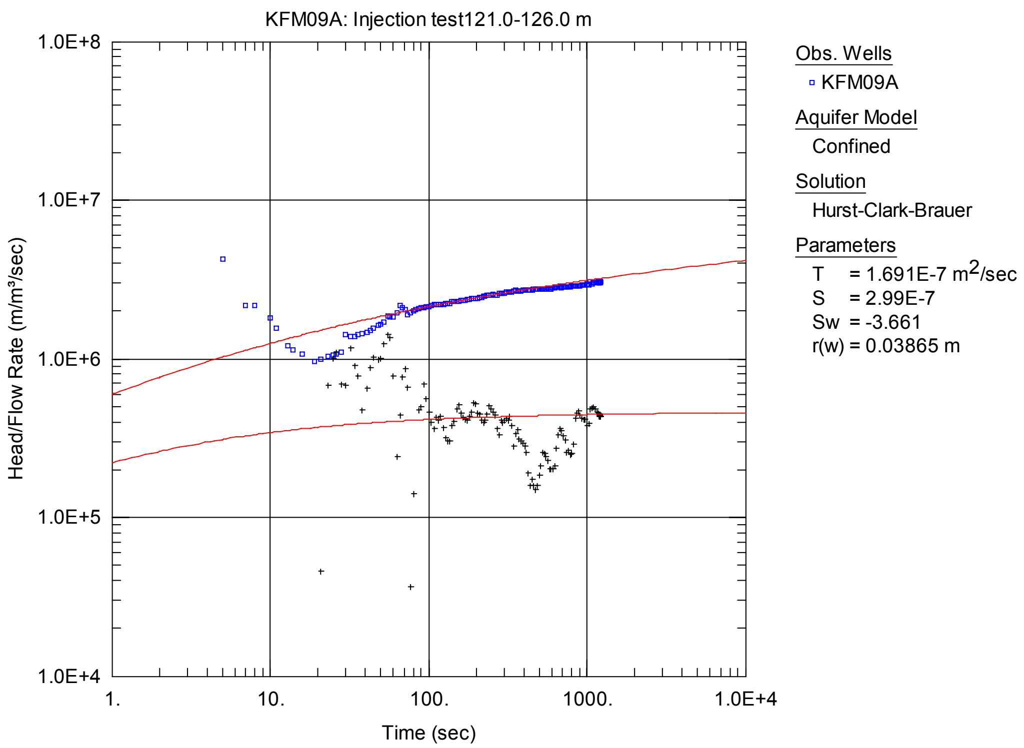


Figure A3-221. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 121.0-126.0 m in KFM09A. This plot shows a fit to the first of two different PRF:s during the injection period in this section.*

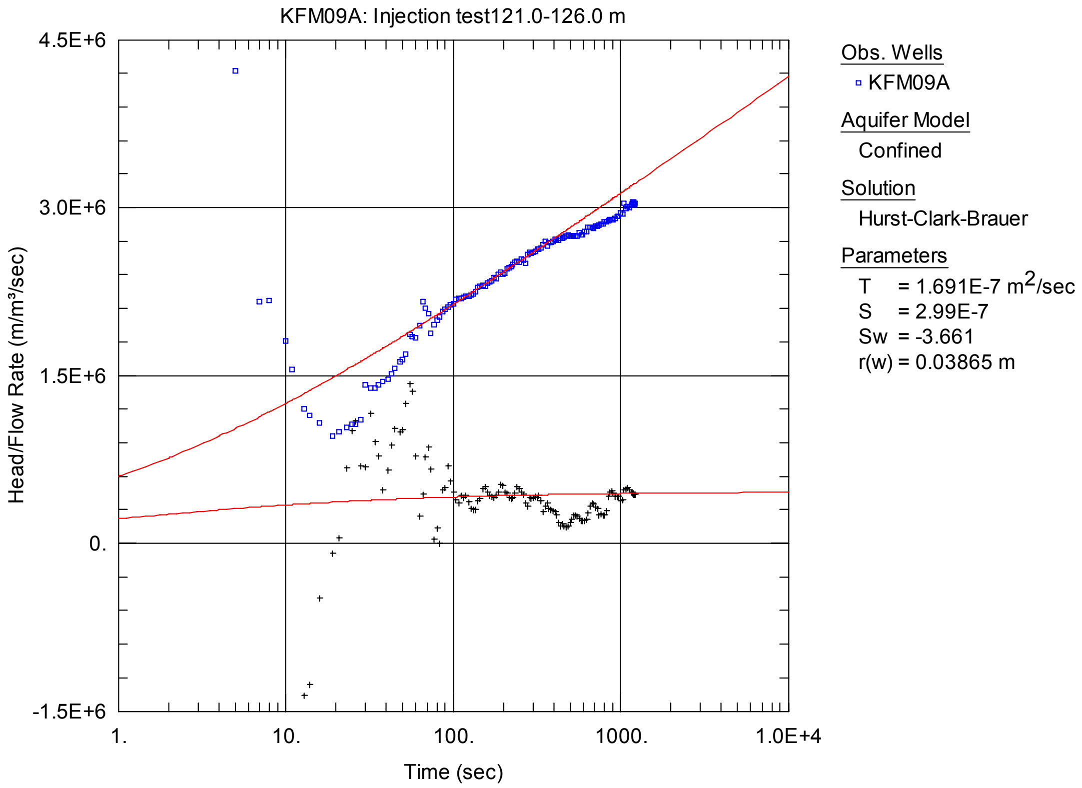


***Figure A3-222.** Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 121.0-126.0 m in KFM09A. This plot shows a fit to the first of two different PRF:s during the injection period in this section.*

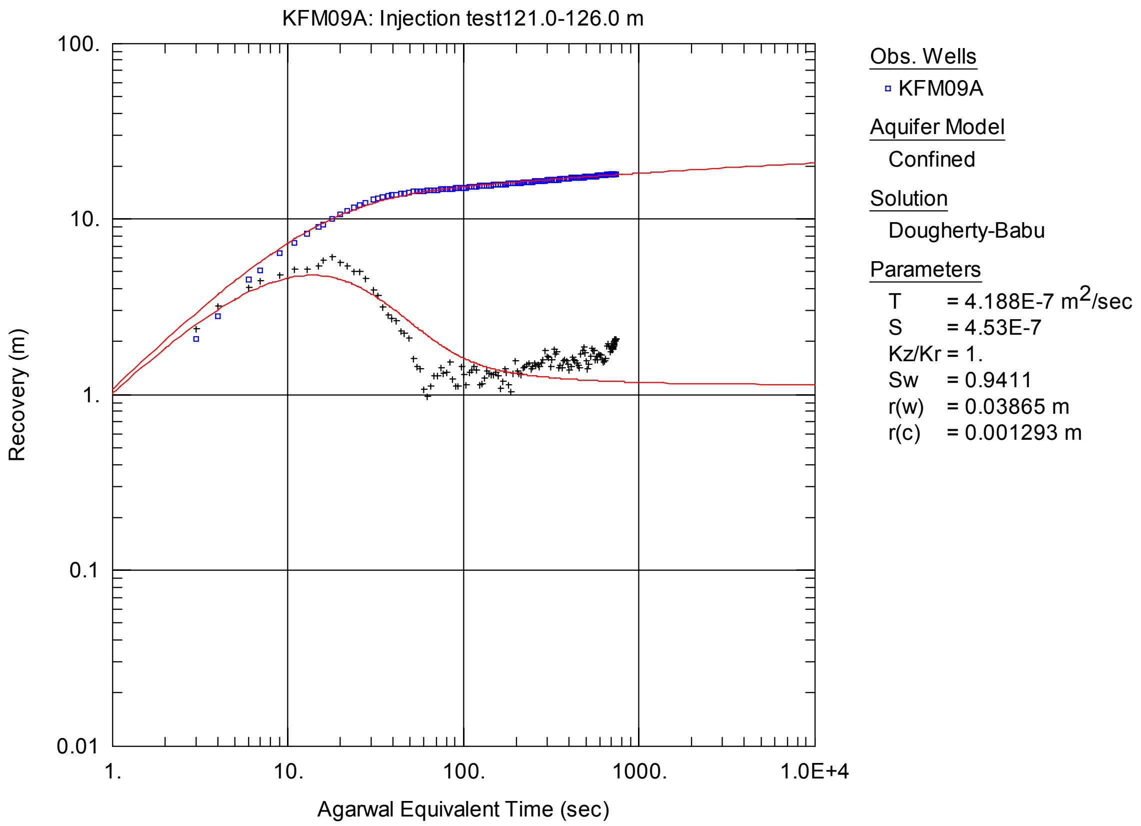


***Figure A3-223.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 121.0-126.0 m in KFM09A.*

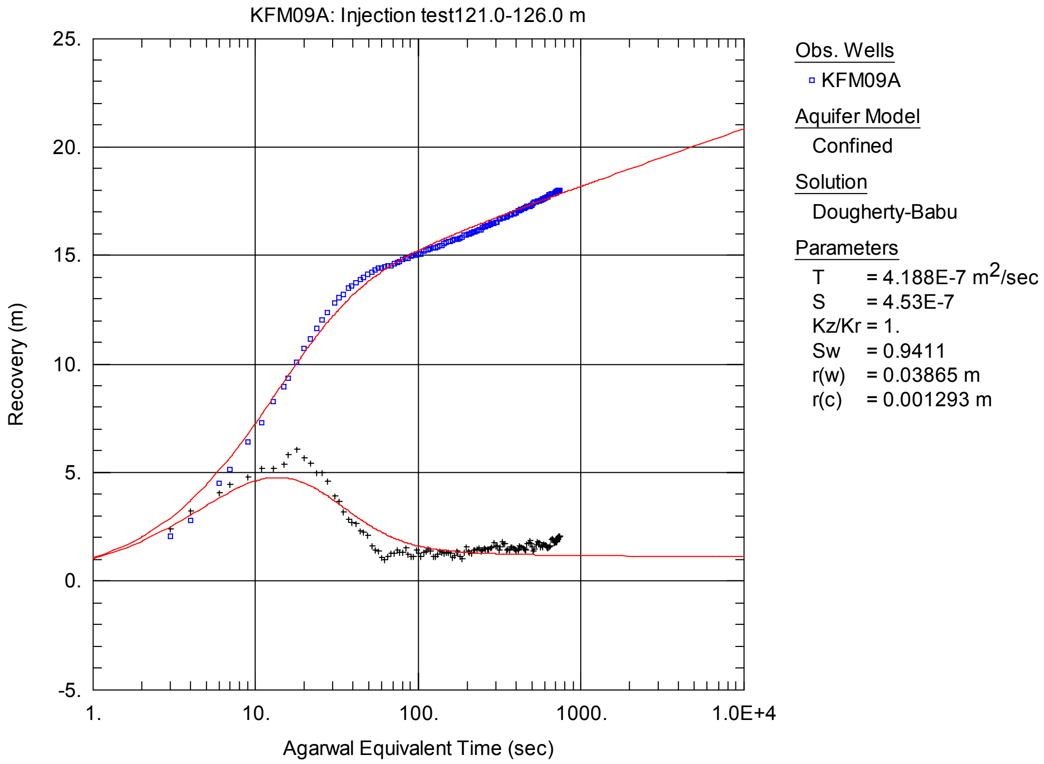


***Figure A3-224.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 121.0-126.0 m in KFM09A.*

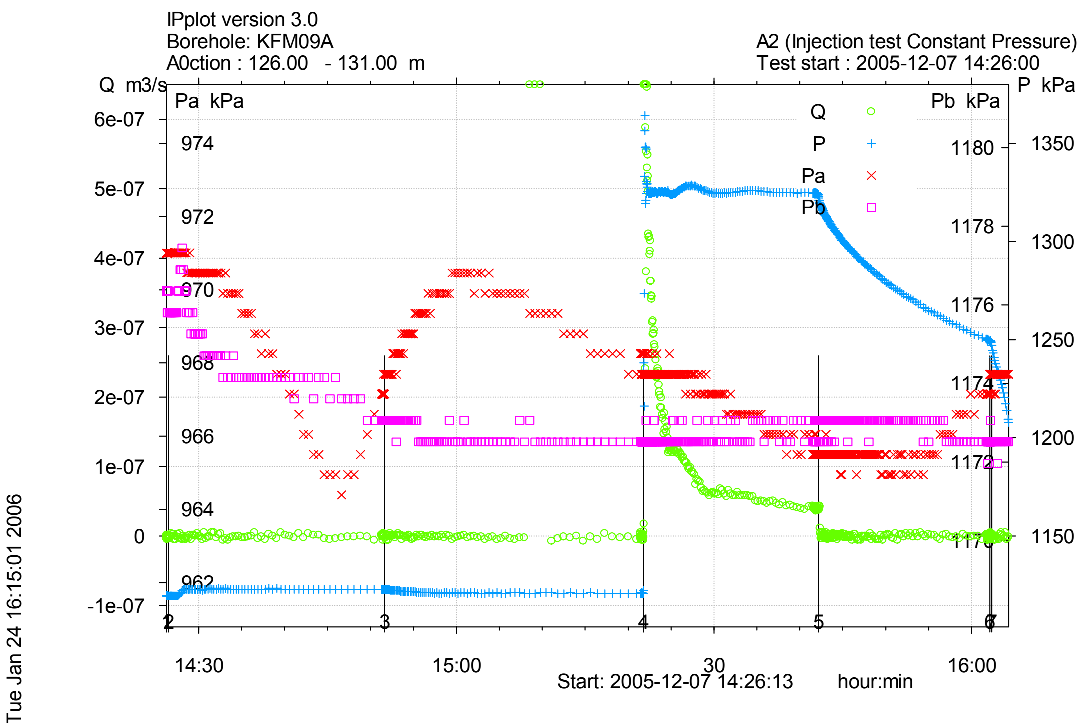


***Figure A3-225.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 126.0-131.0 m in borehole KFM09A.*

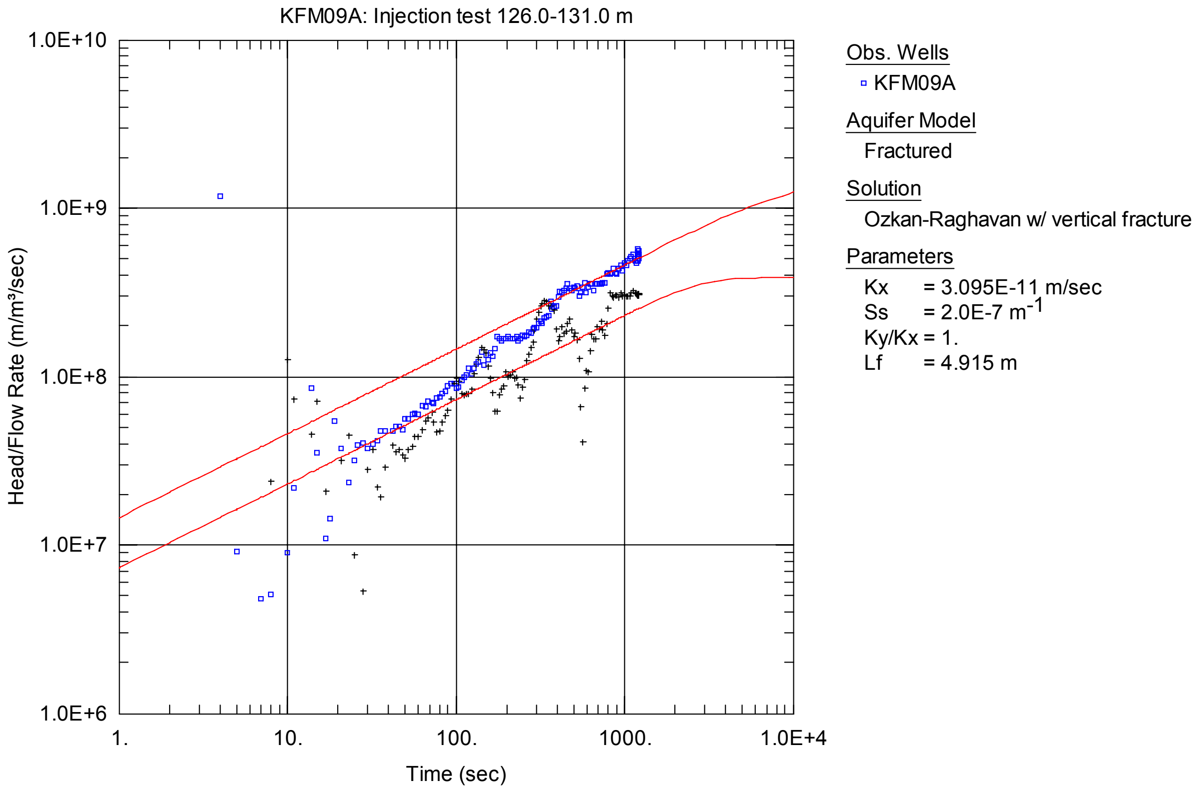


Figure A3-226. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 126.0-131.0 m in KFM09A. No unambiguous transient evaluation is possible on the injection period.*

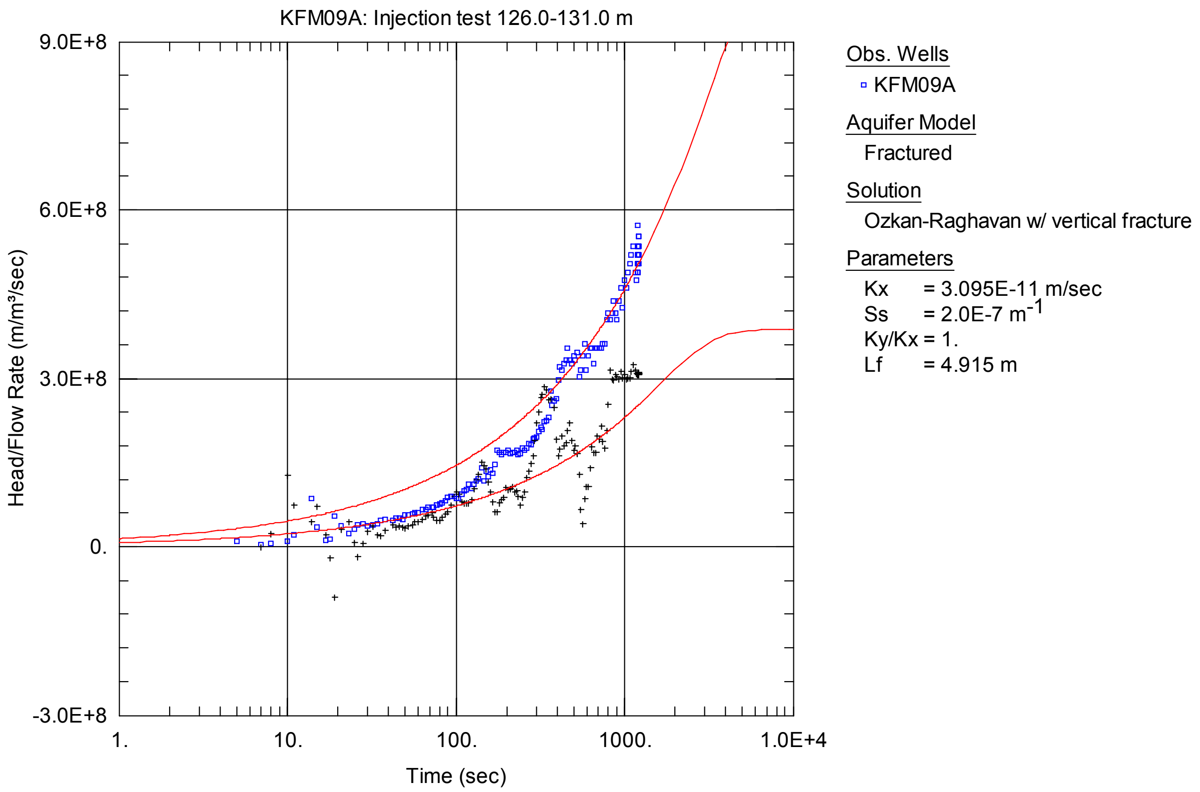


Figure A3-227. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 126.0-131.0 m in KFM09A. No unambiguous transient evaluation is possible on the injection period.*

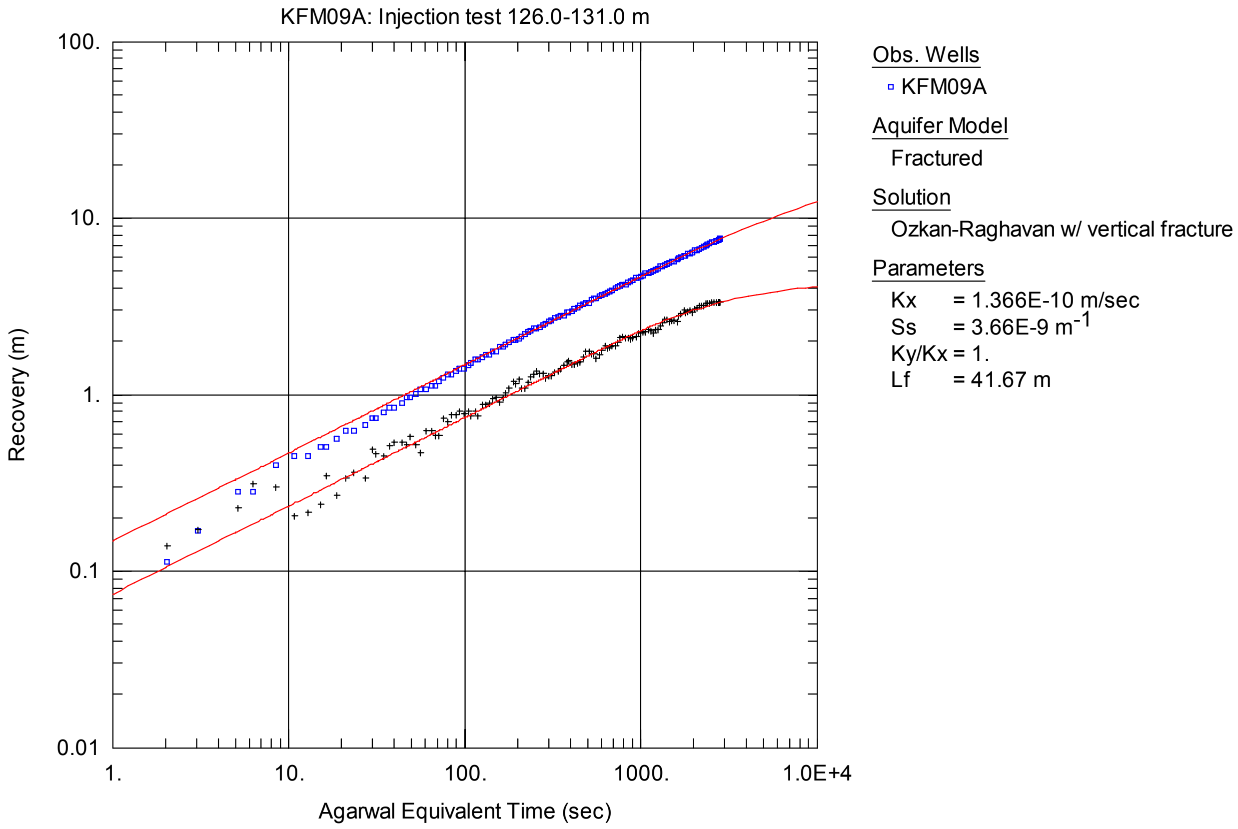


Figure A3-228. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 126.0-131.0 m in KFM09A.*

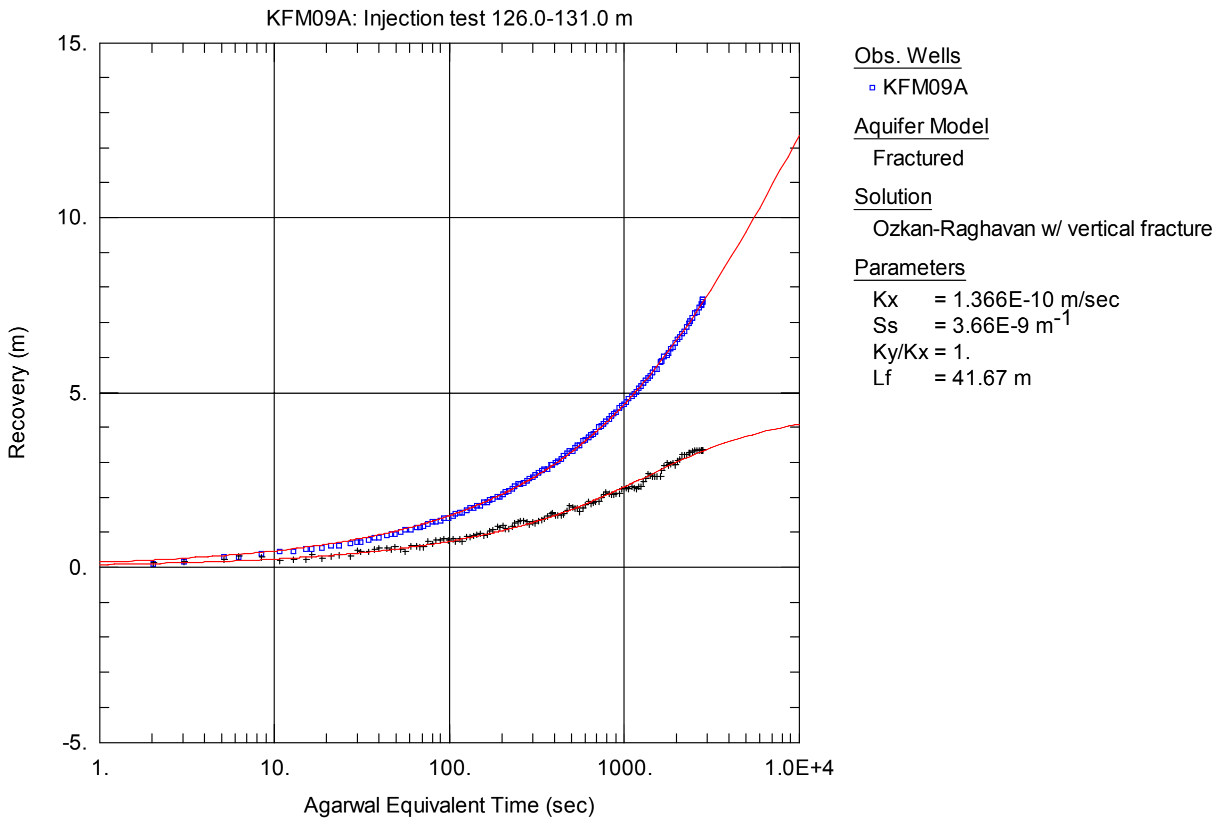


Figure A3-229. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 126.0-131.0 m in KFM09A.*

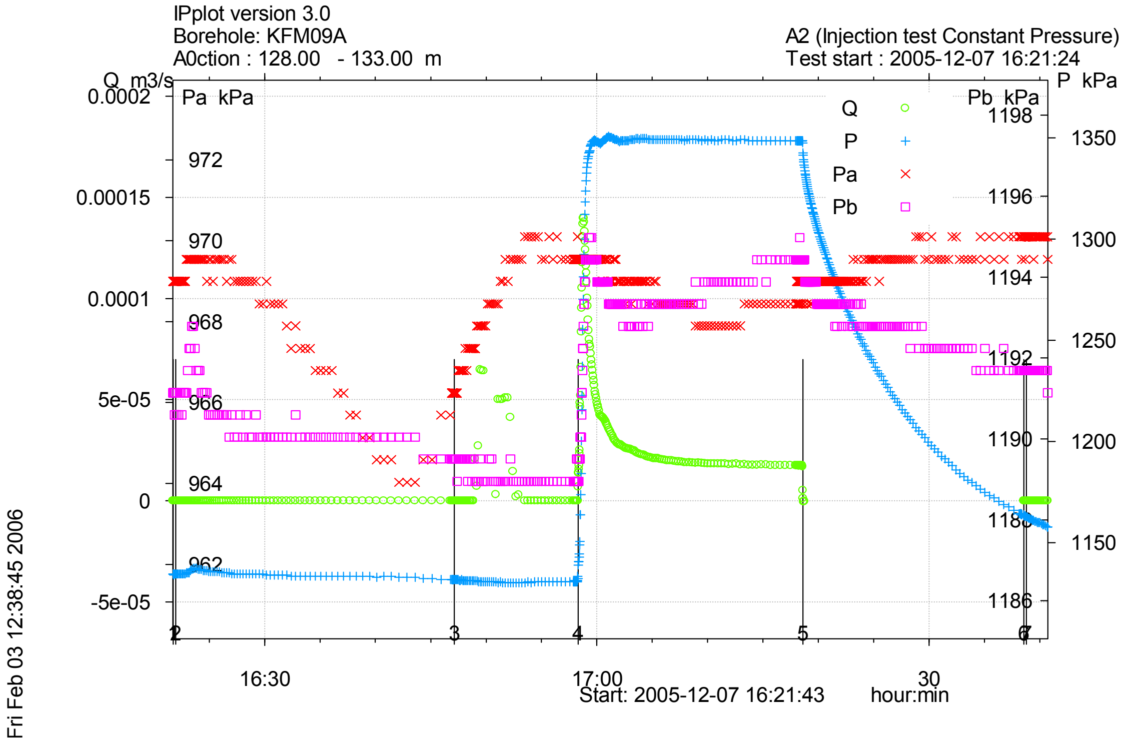


Figure A3-230. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 128.0-133.0 m in borehole KFM09A.*

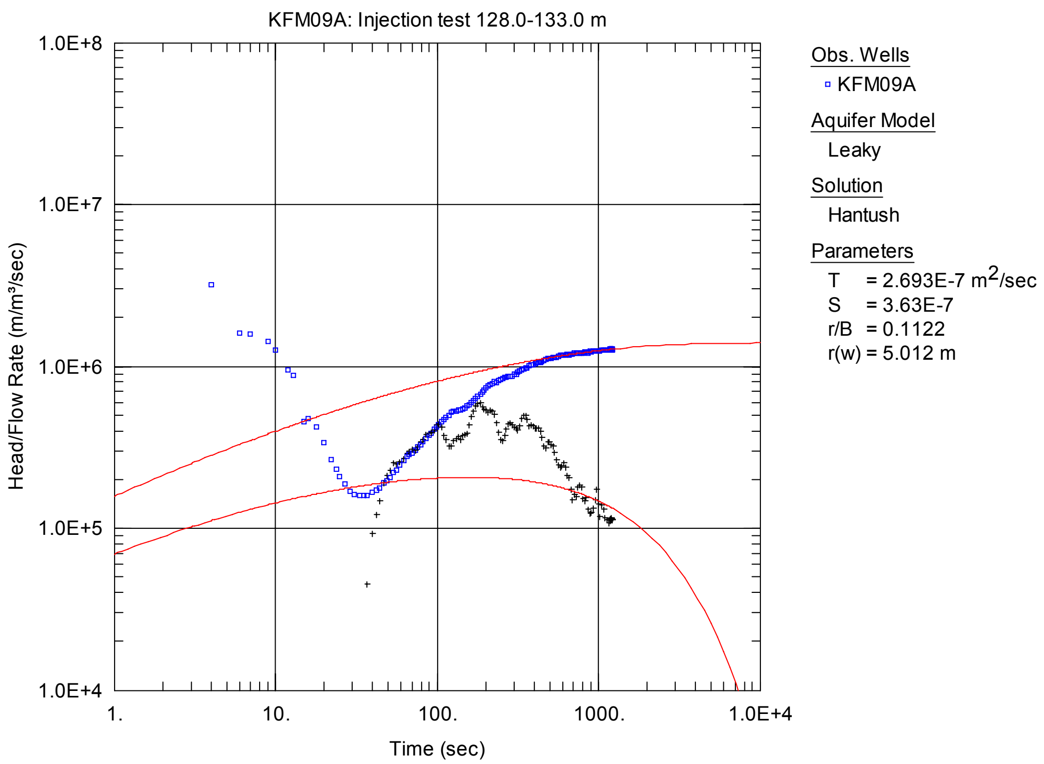


Figure A3-231. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 128.0-133.0 m in KFM09A.*

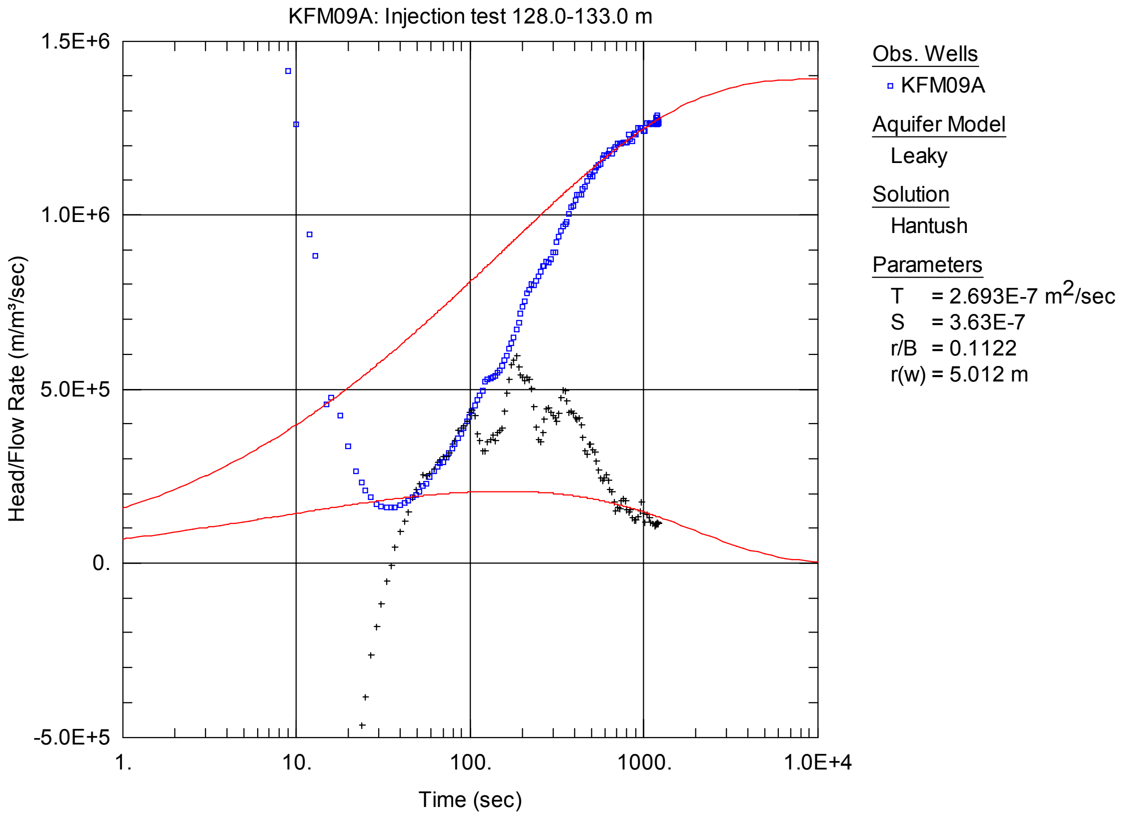


***Figure A3-232.** Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 128.0-133.0 m in KFM09A.*

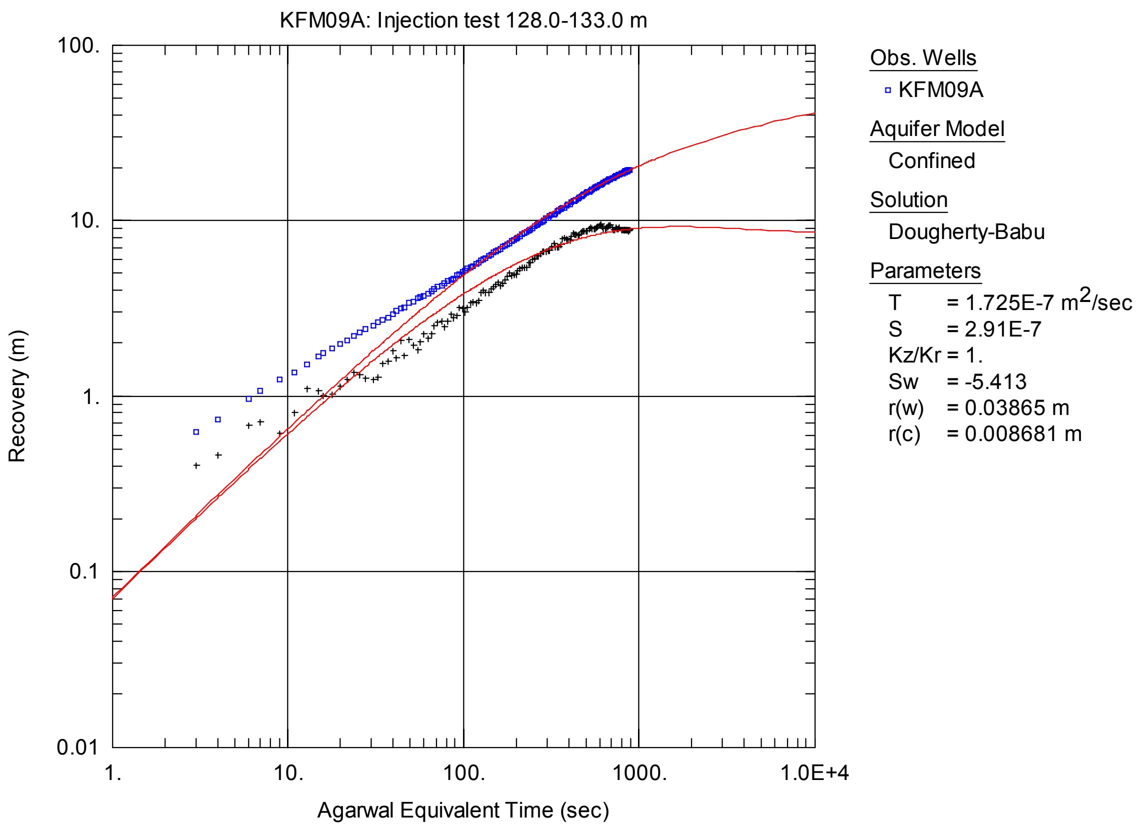


***Figure A3-233.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 128.0-133.0 m in KFM09A.*

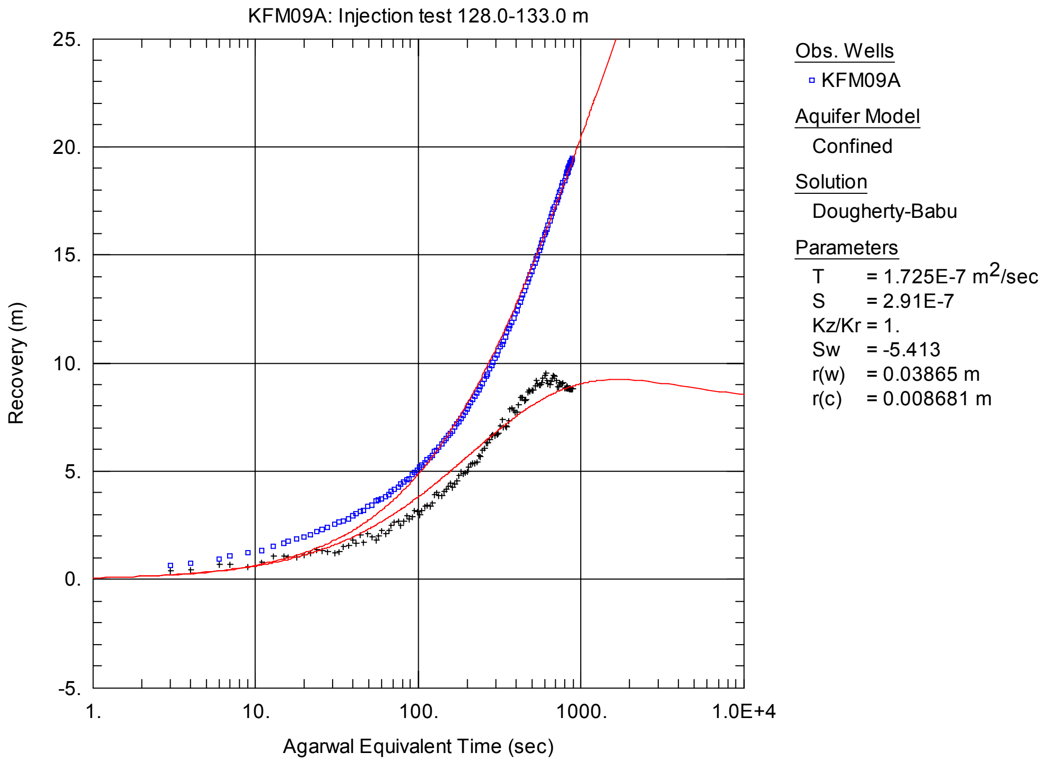


Figure A3-234. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 128.0-133.0 m in KFM09A.*

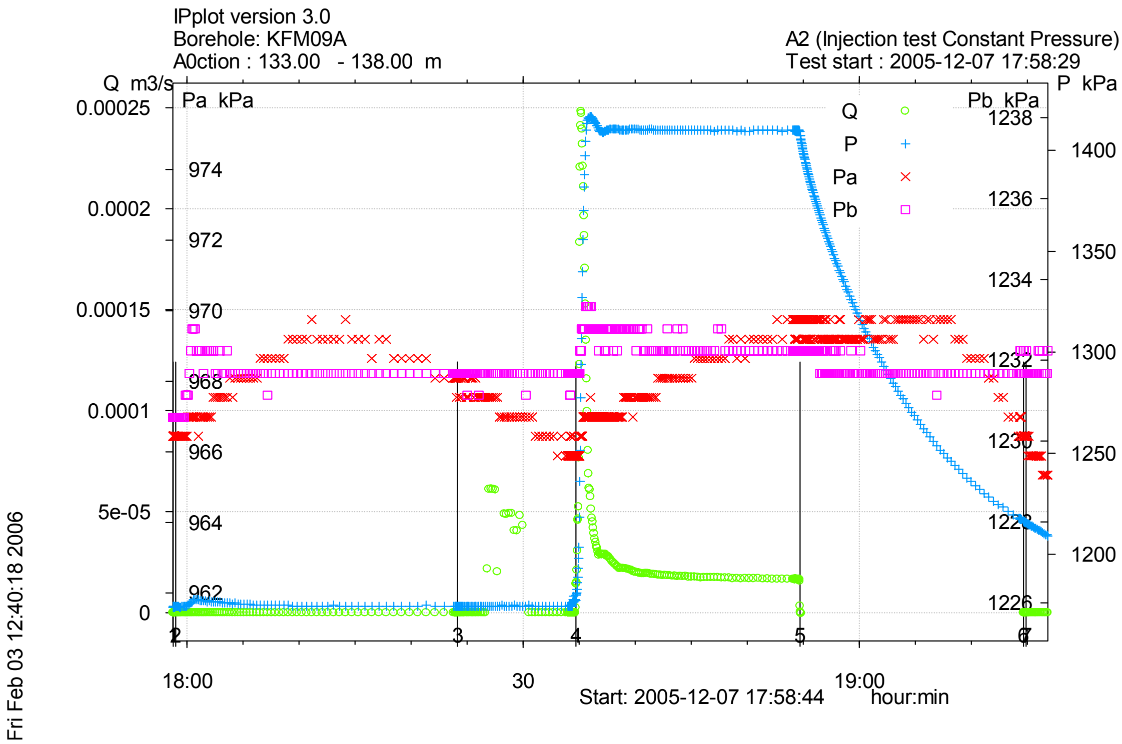


Figure A3-235. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 133.0-138.0 m in borehole KFM09A.*

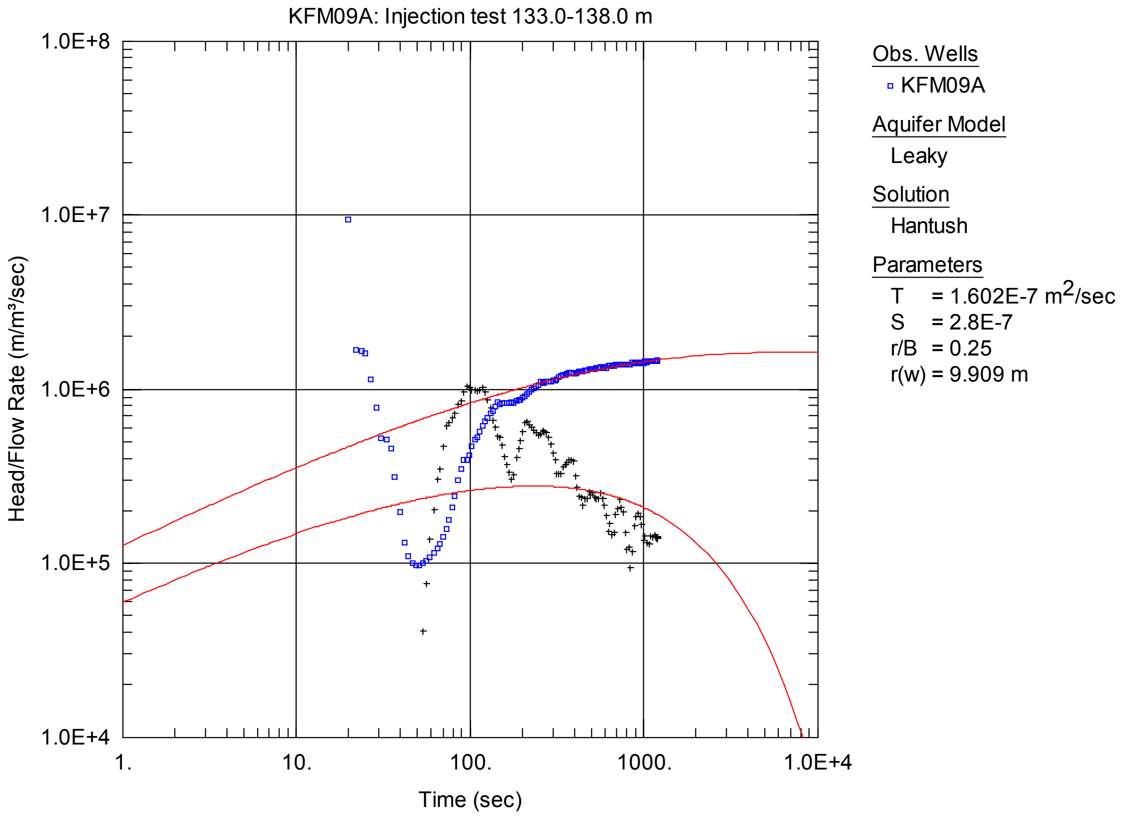


Figure A3-236. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 133.0-138.0 m in KFM09A.*

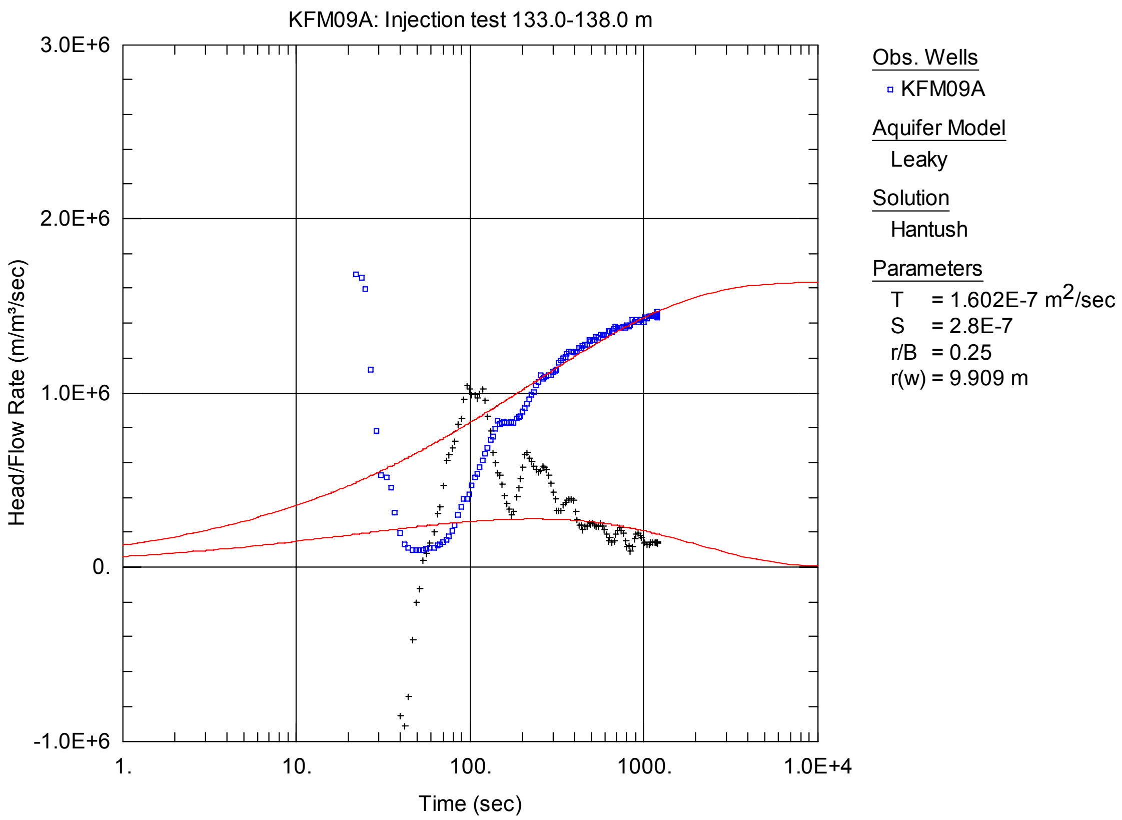


Figure A3-237. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 133.0-138.0 m in KFM09A.*

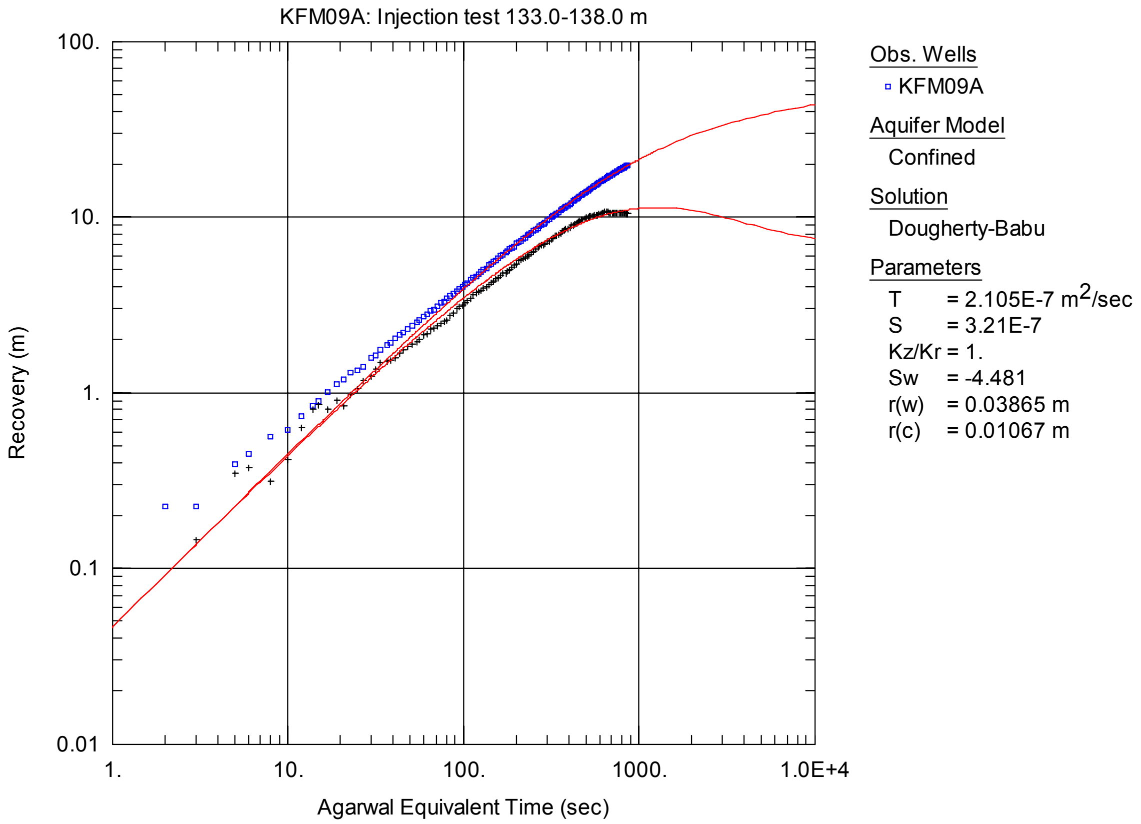


Figure A3-238. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 133.0-138.0 m in KFM09A.*

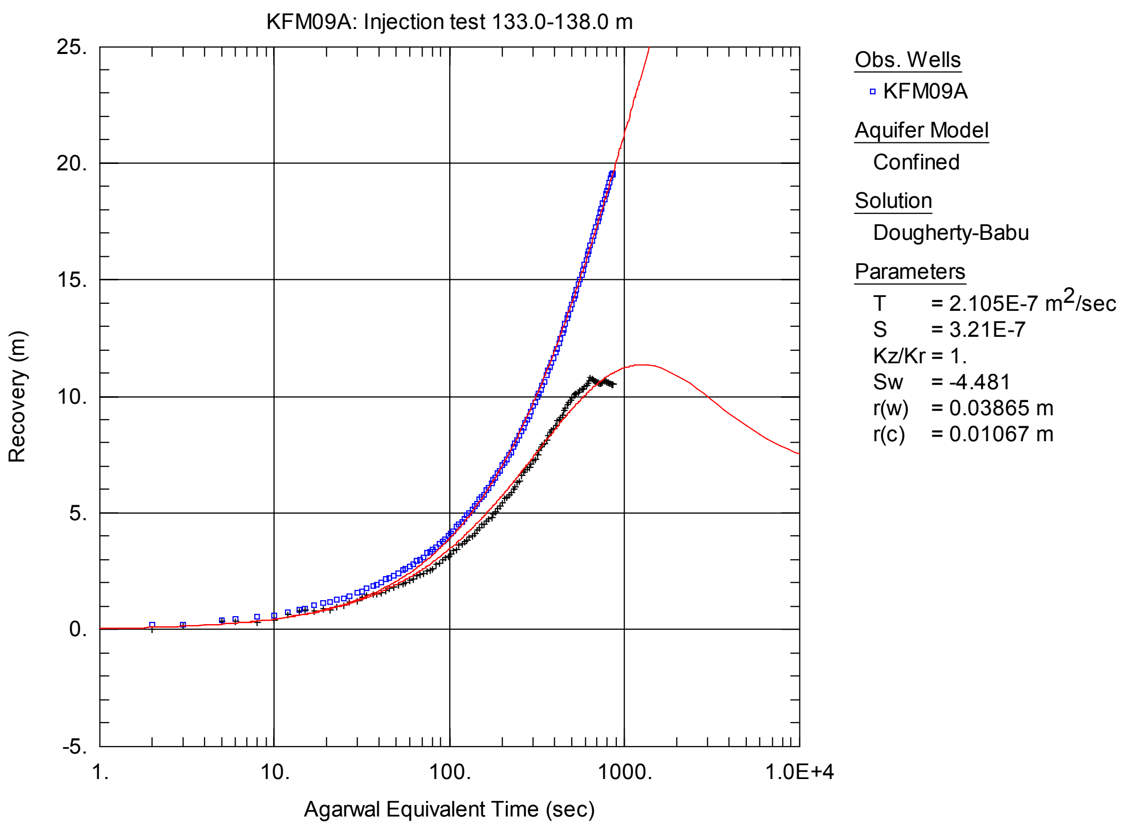


Figure A3-239. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 133.0-138.0 m in KFM09A.*

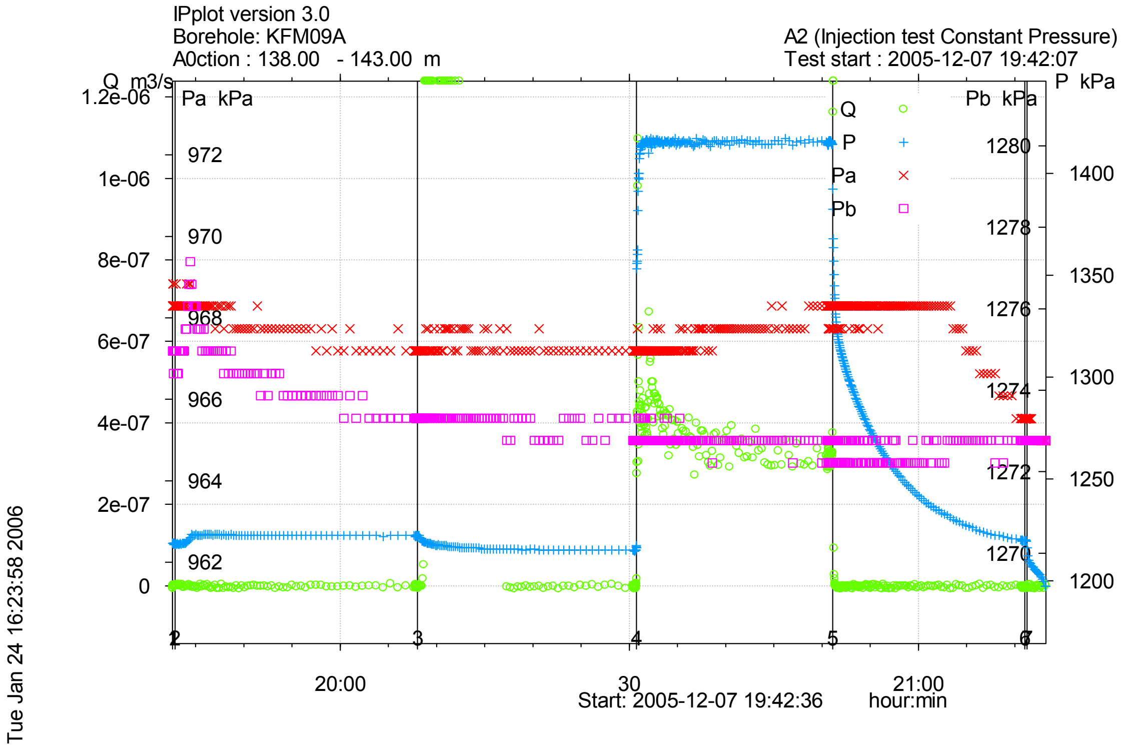


Figure A3-240. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 138.0-143.0 m in borehole KFM09A.*

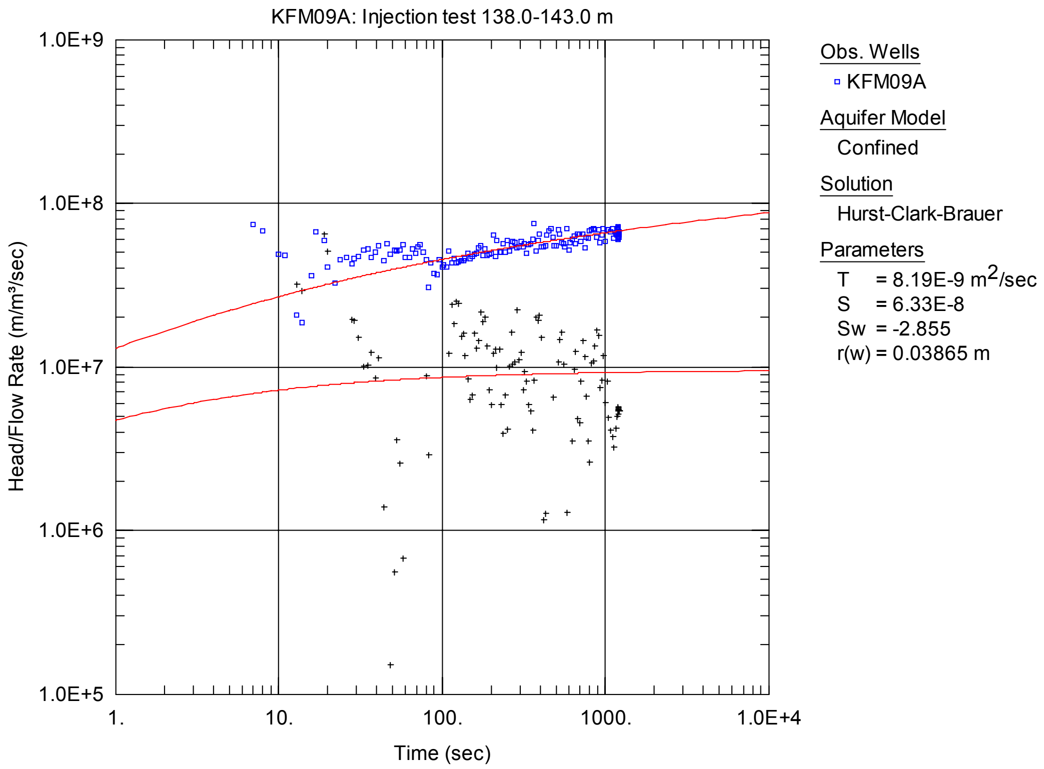


Figure A3-241. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 138.0-143.0 m in KFM09A.*

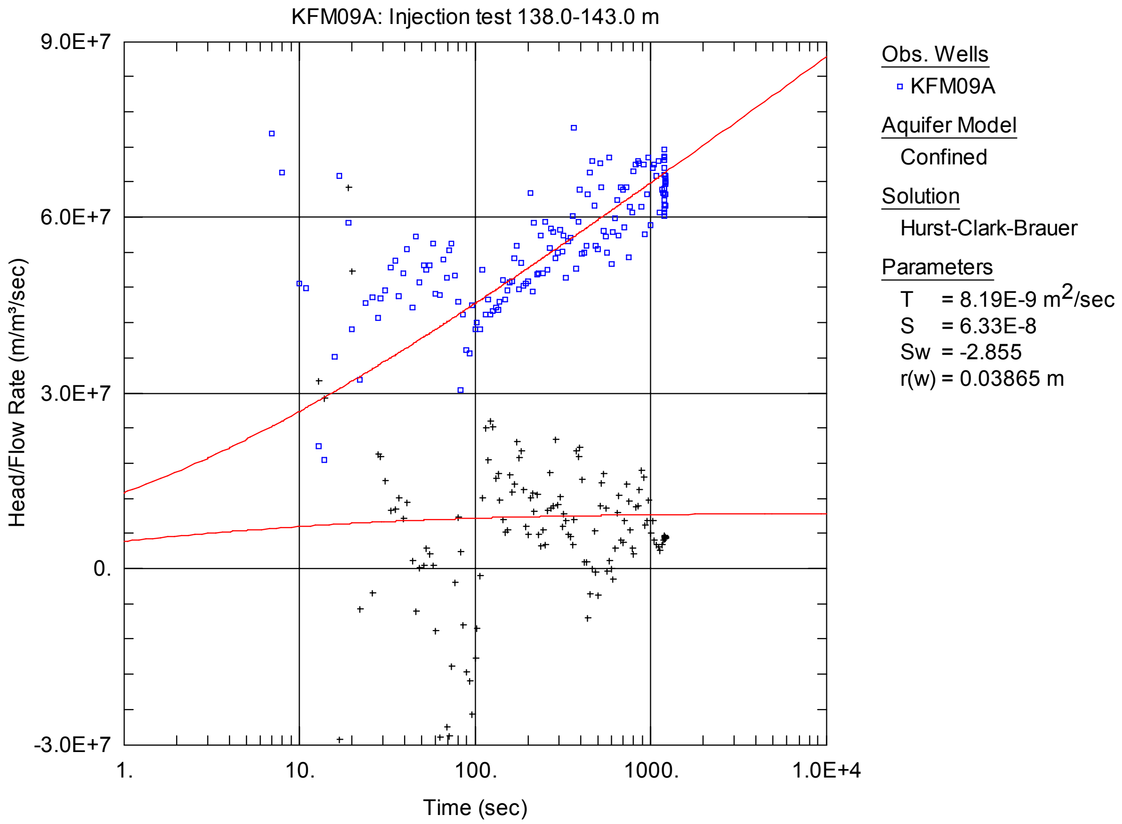


***Figure A3-242.** Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 138.0-143.0 m in KFM09A.*

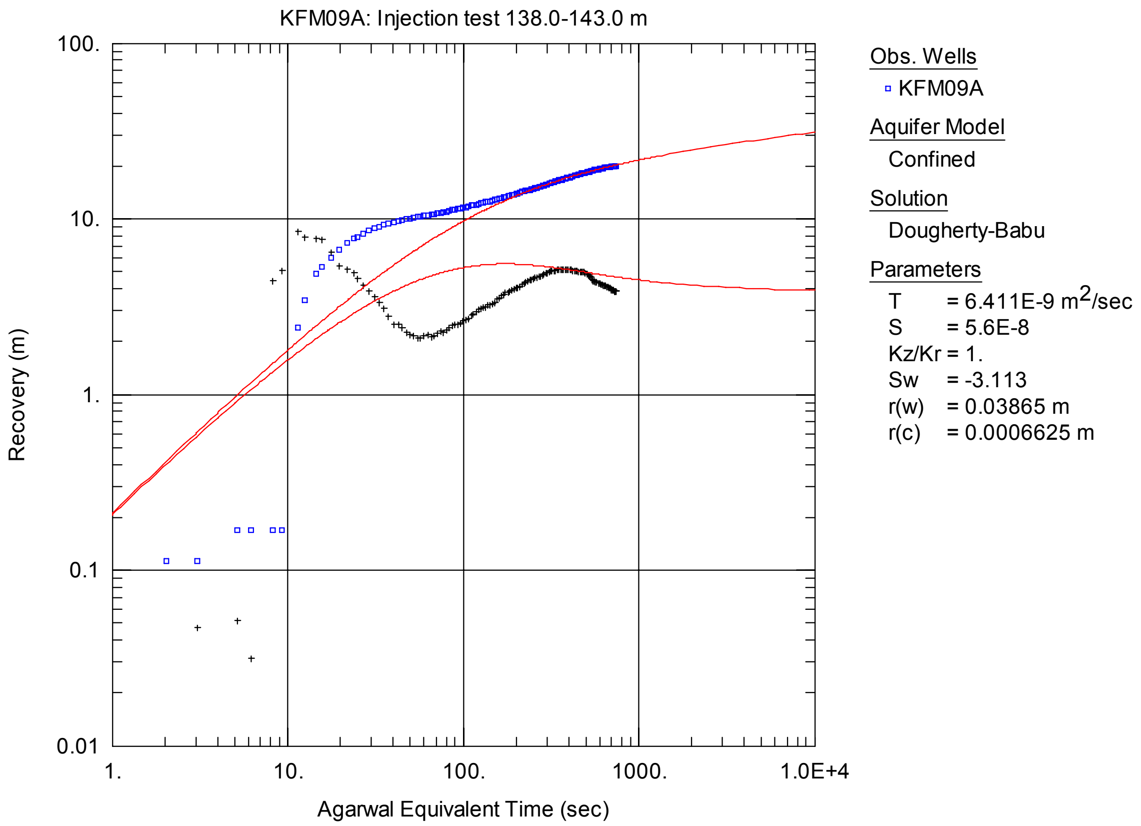


***Figure A3-243.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 138.0-143.0 m in KFM09A.*

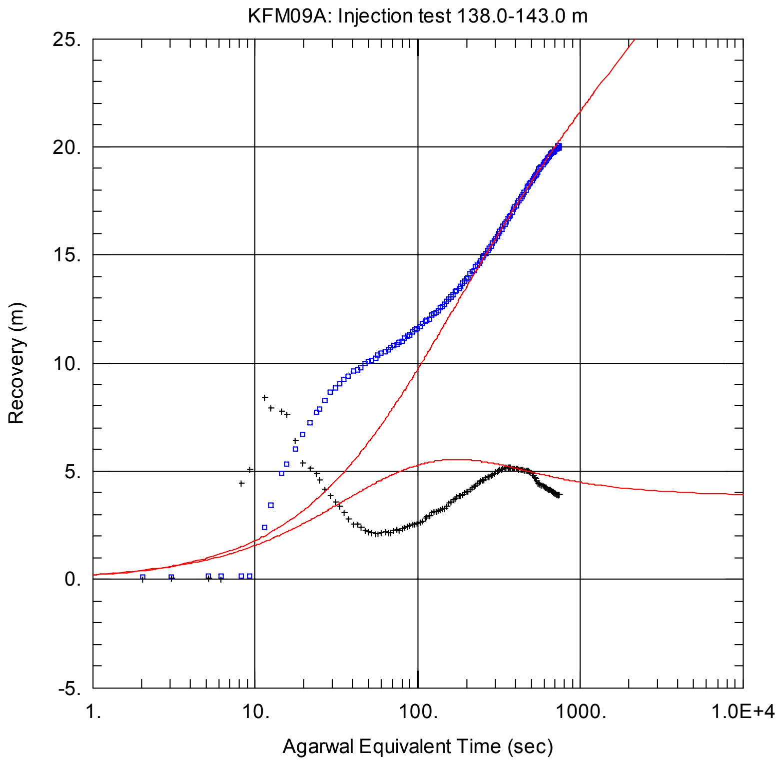


Figure A3-244. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 138.0-143.0 m in KFM09A.*

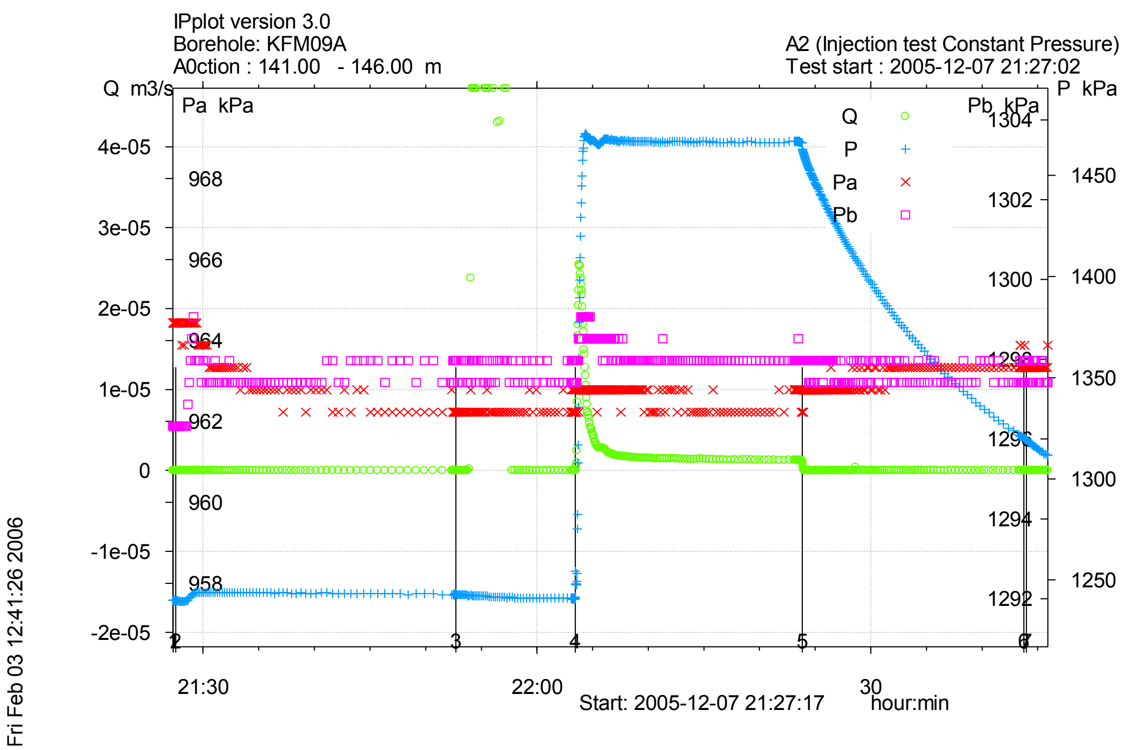


Figure A3-245. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 141.0-146.0 m in borehole KFM09A.*

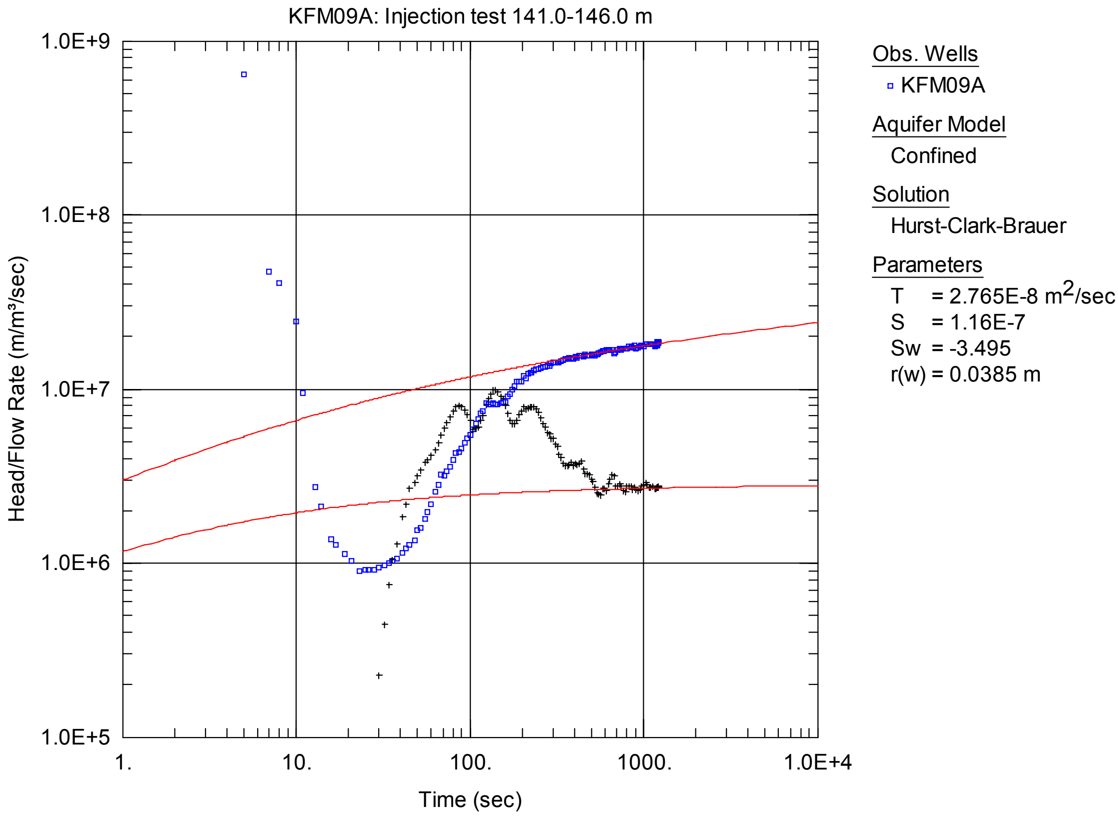


***Figure A3-246.** Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 141.0-146.0 m in KFM09A.*

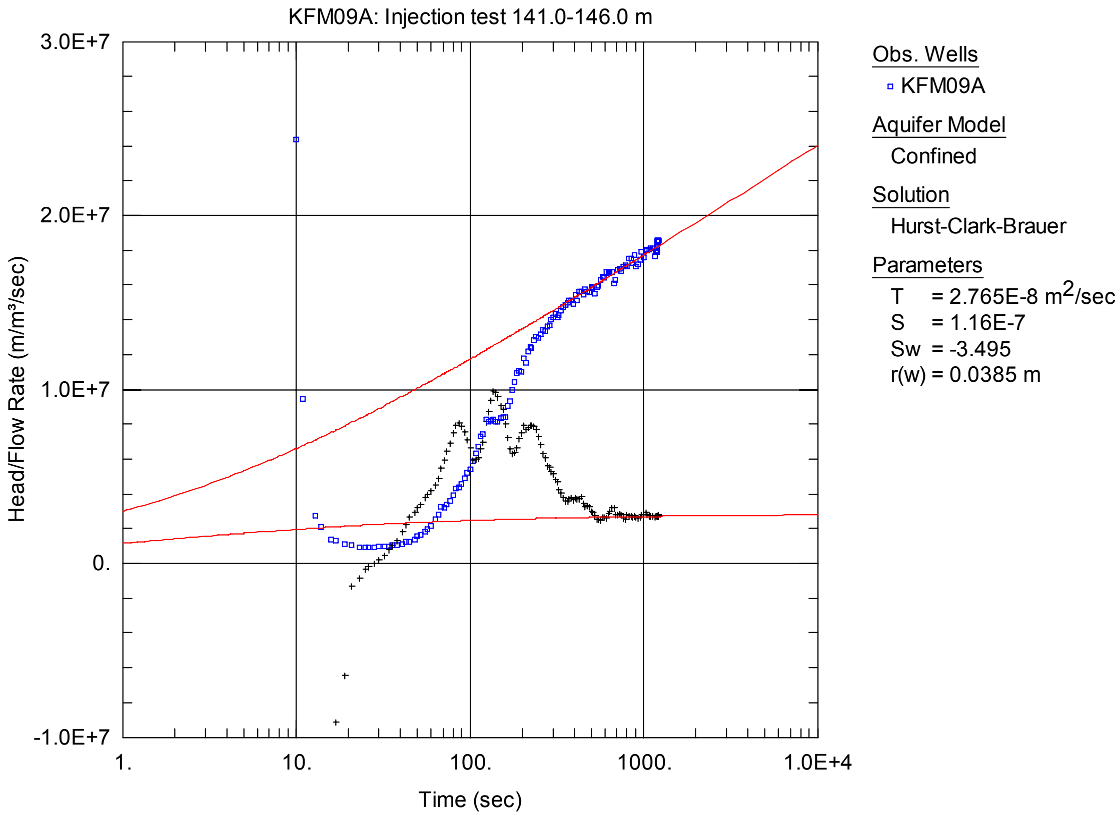


***Figure A3-247.** Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 141.0-146.0 m in KFM09A.*

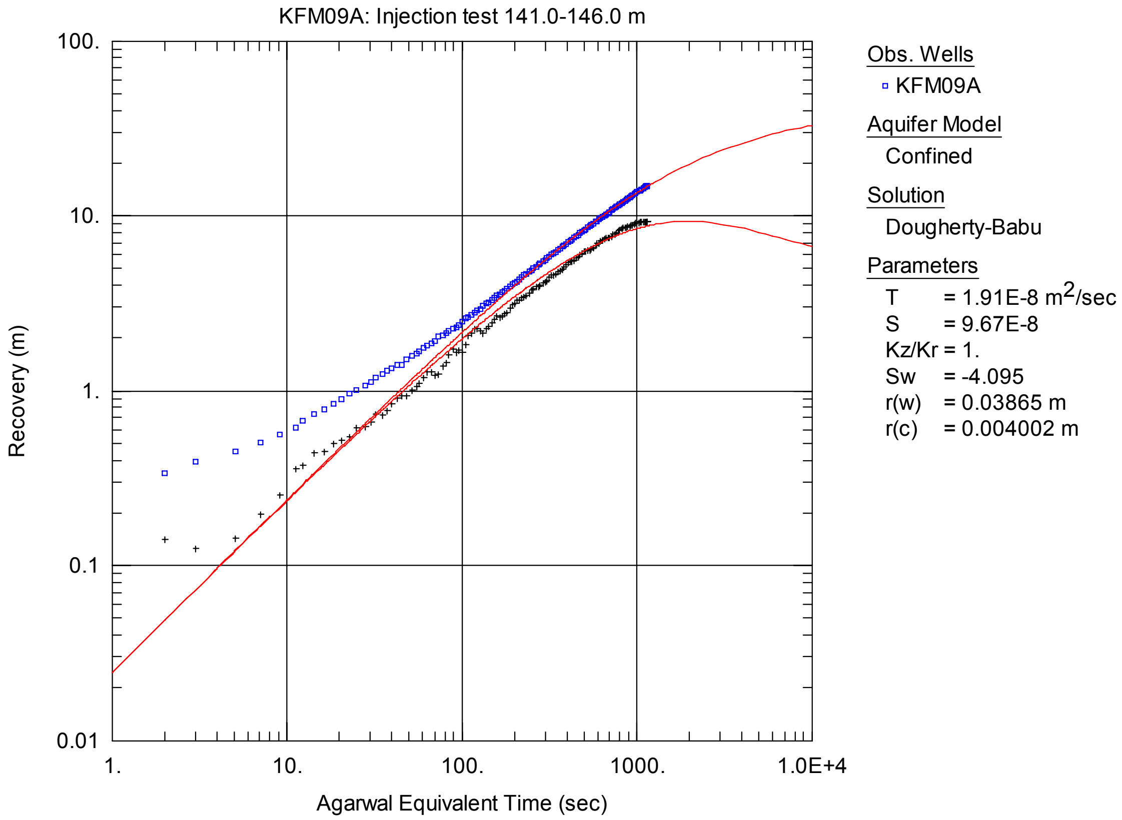


Figure A3-248. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 141.0-146.0 m in KFM09A.*

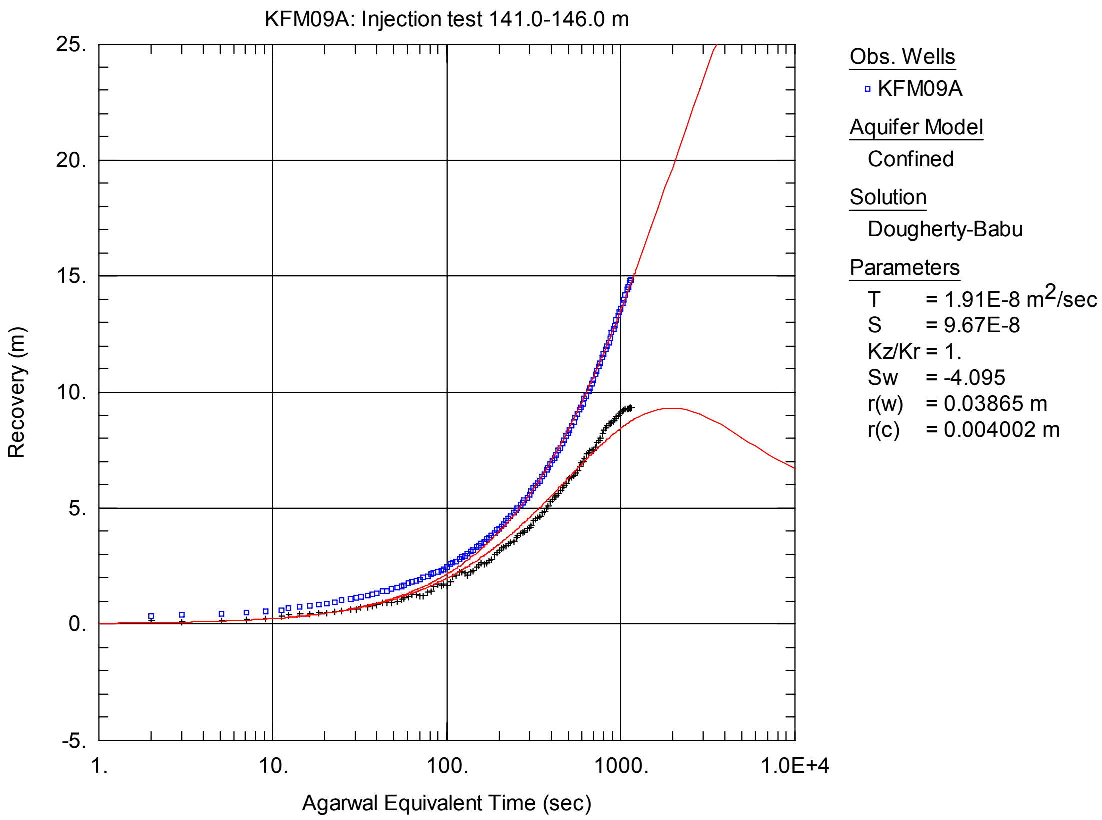


Figure A3-249. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 141.0-146.0 m in KFM09A.*

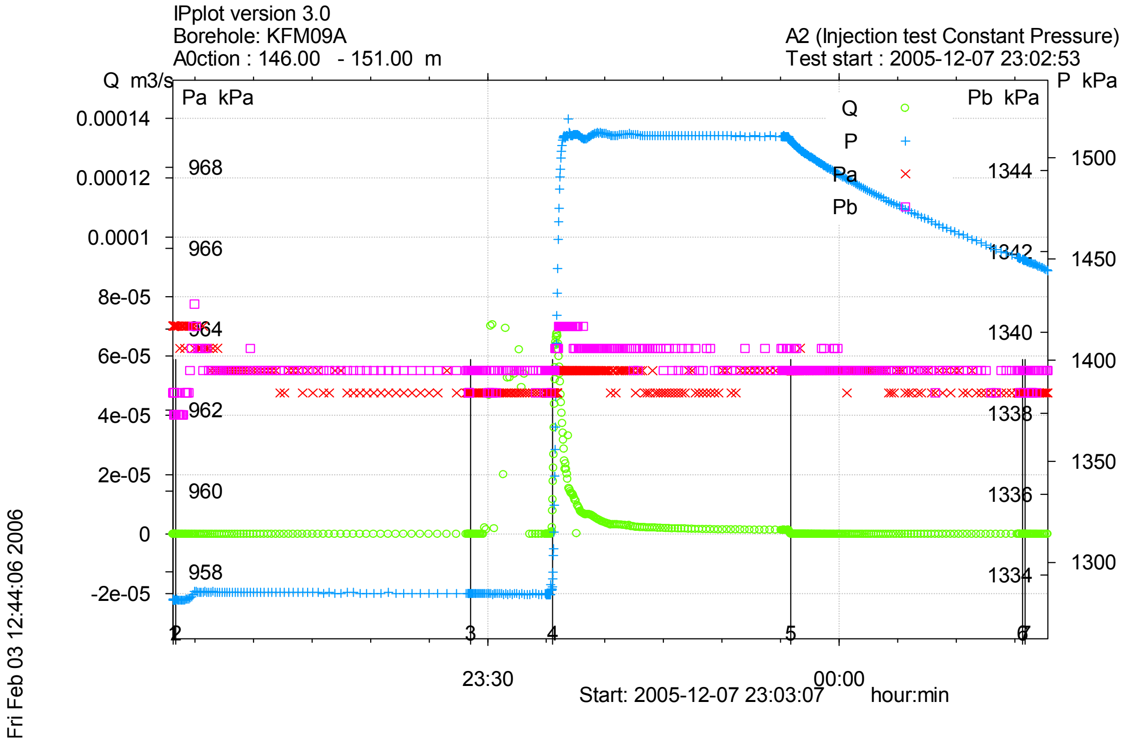


Figure A3-250. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 146.0-151.0 m in borehole KFM09A.*

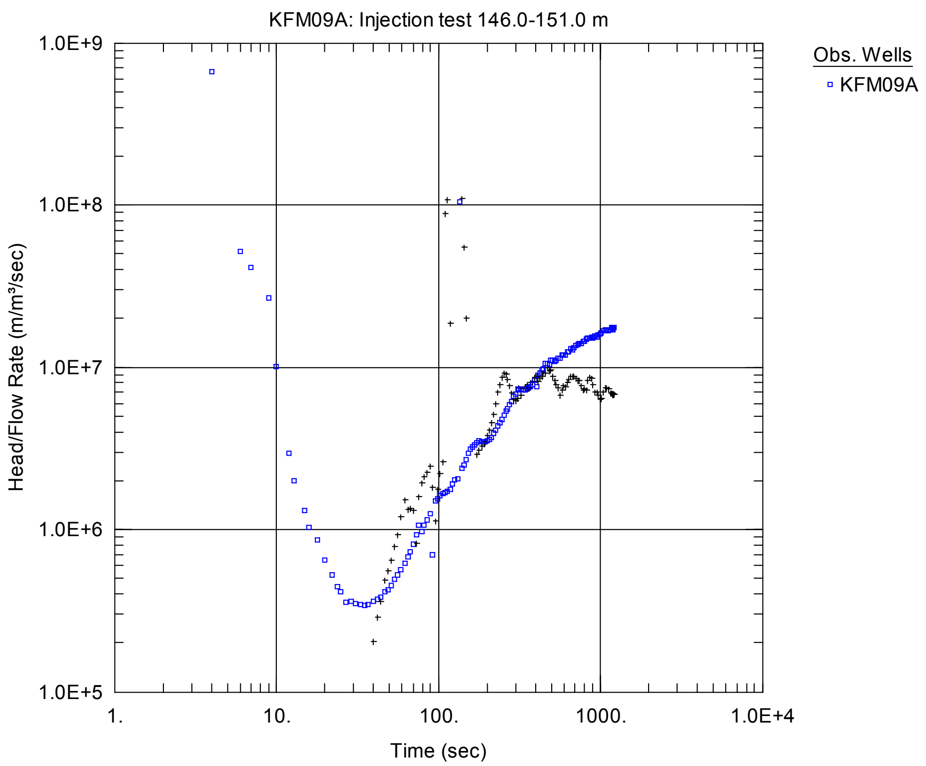


Figure A3-251. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 146.0-151.0 m in KFM09A.*

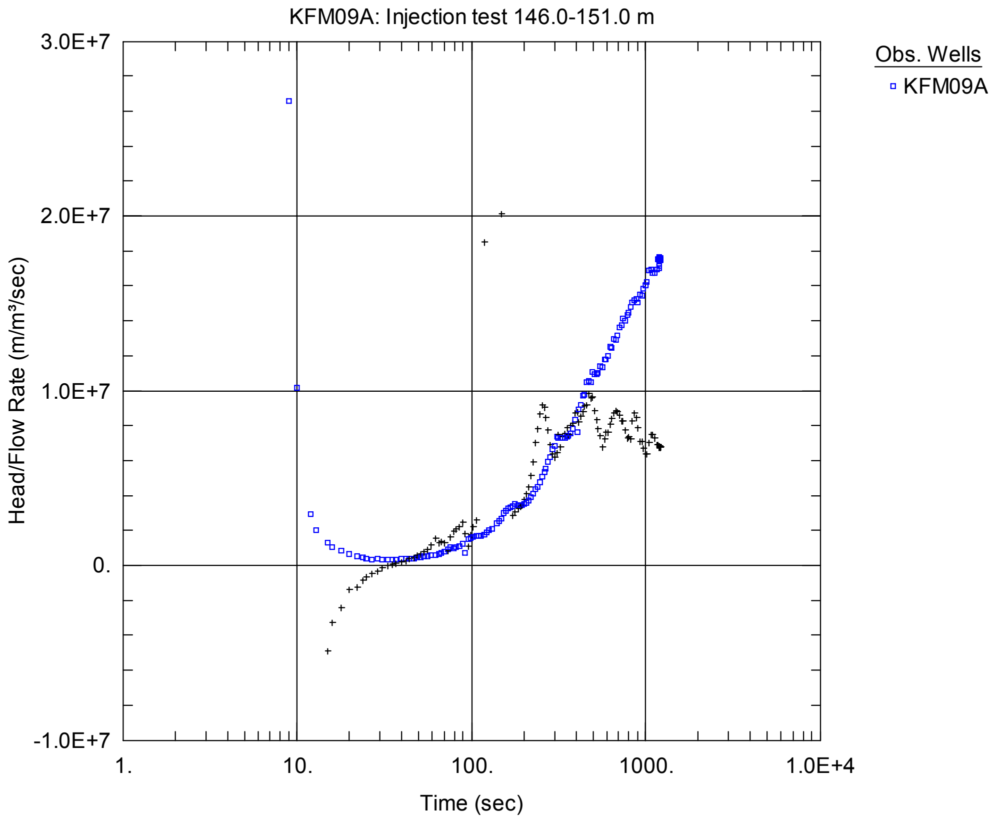


__Figure A3-252.__ Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 146.0-151.0 m in KFM09A.

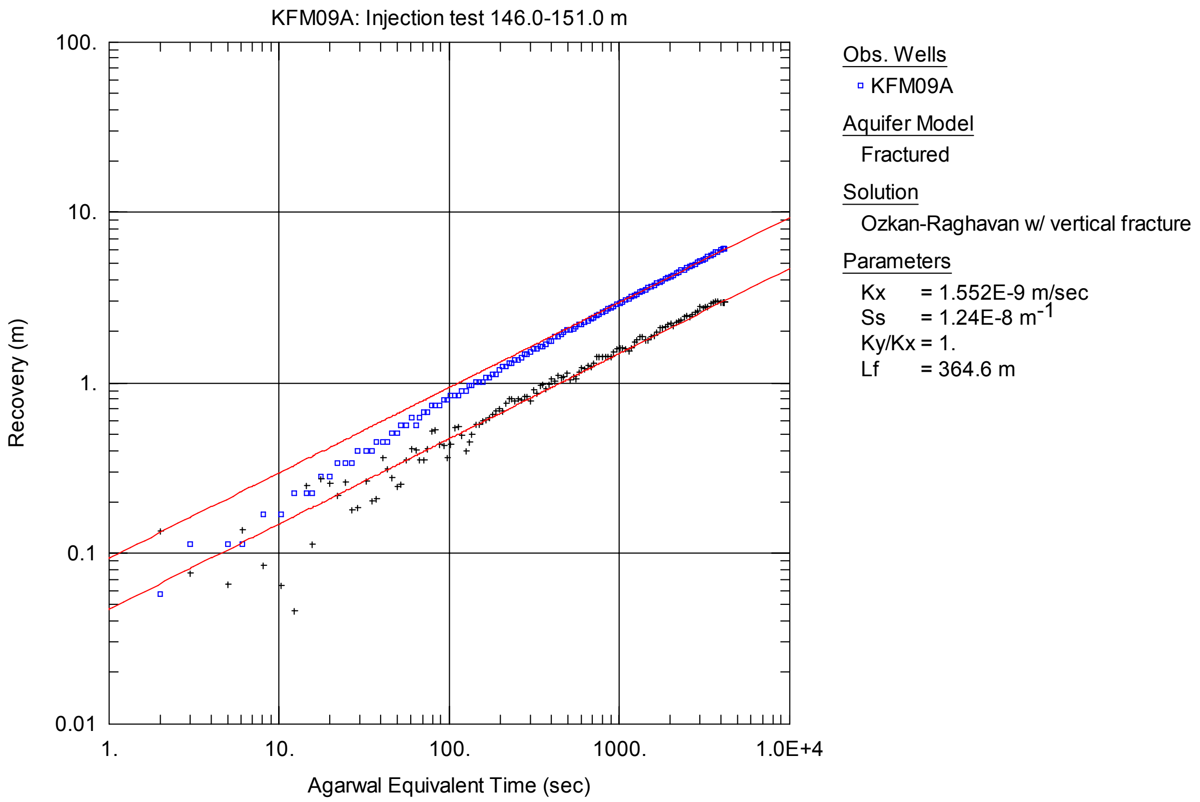


__Figure A3-253.__ Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 146.0-151.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.

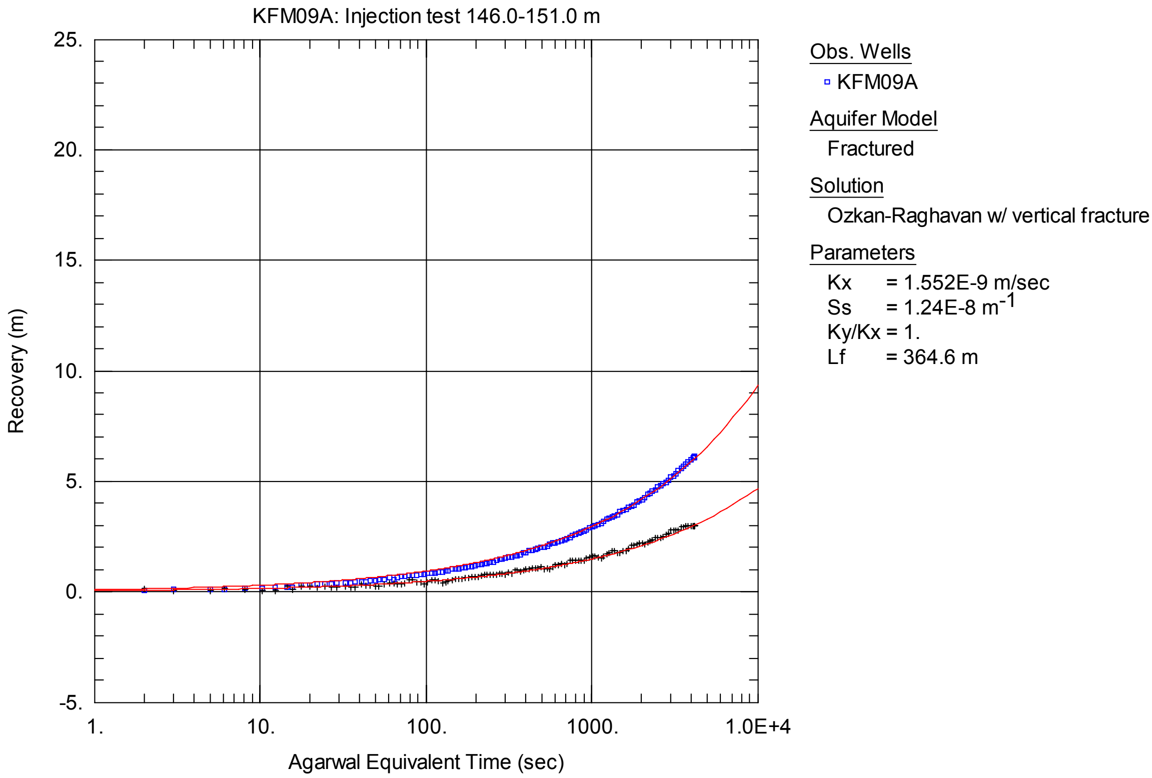


Figure A3-254. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 146.0-151.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

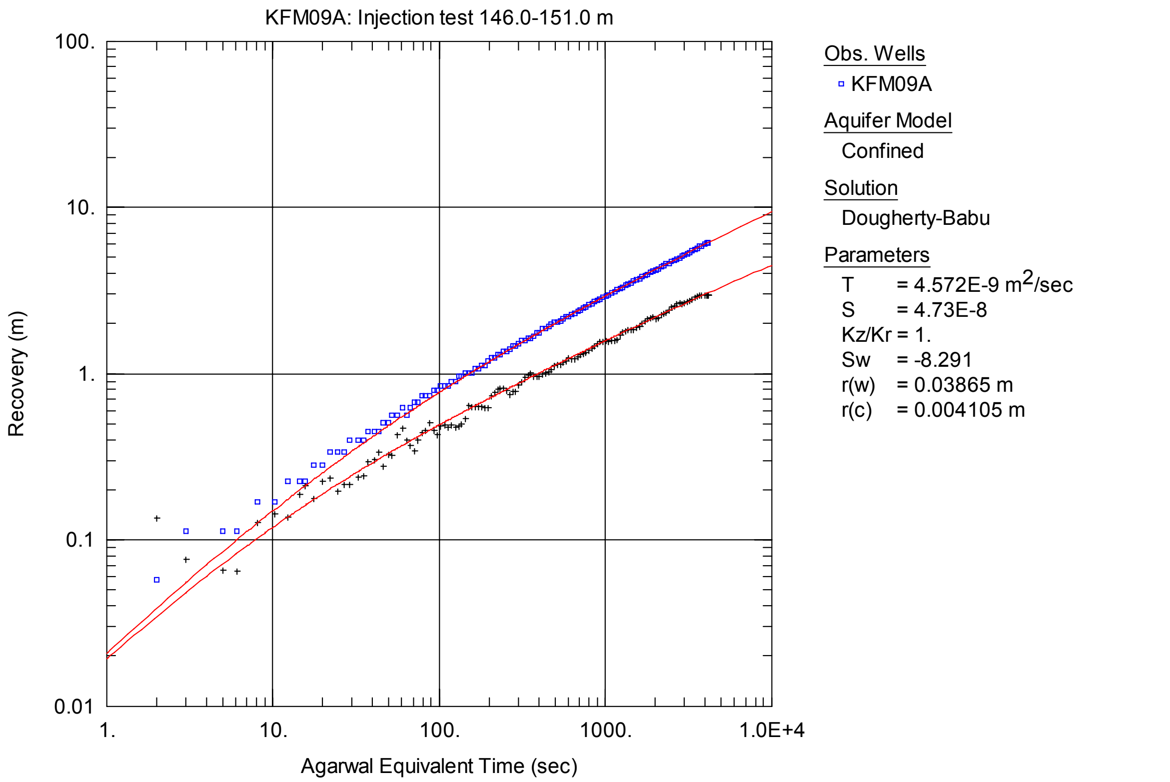


Figure A3-255. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 146.0-151.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

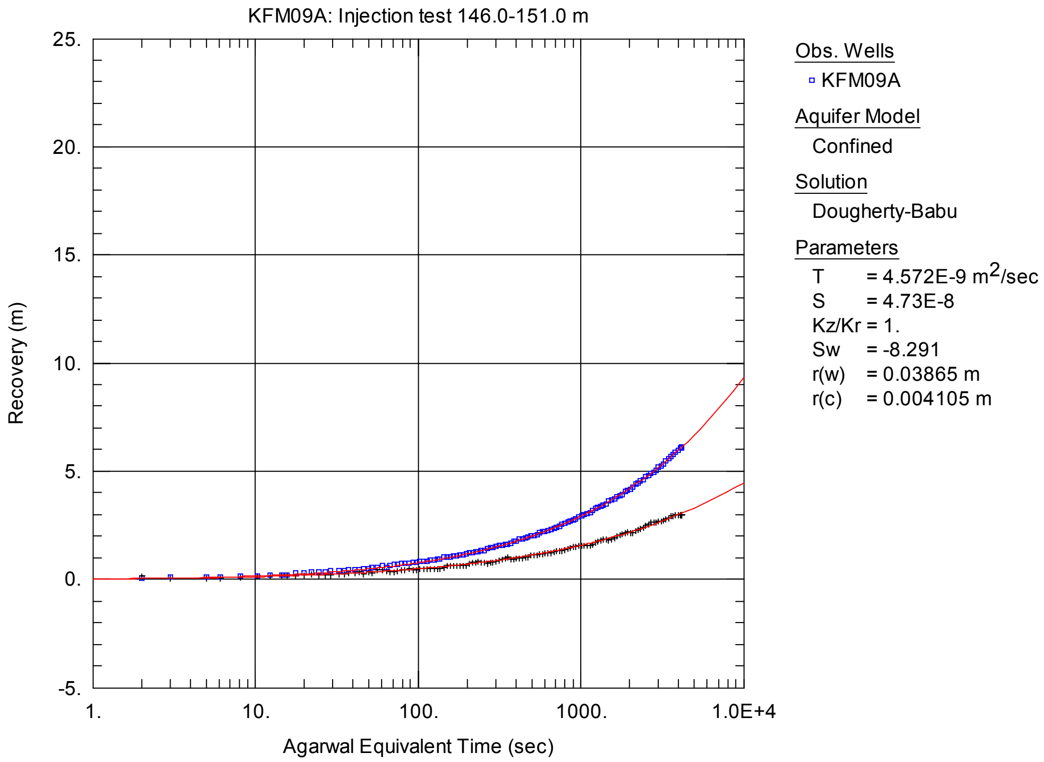


Figure A3-256. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 146.0-151.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

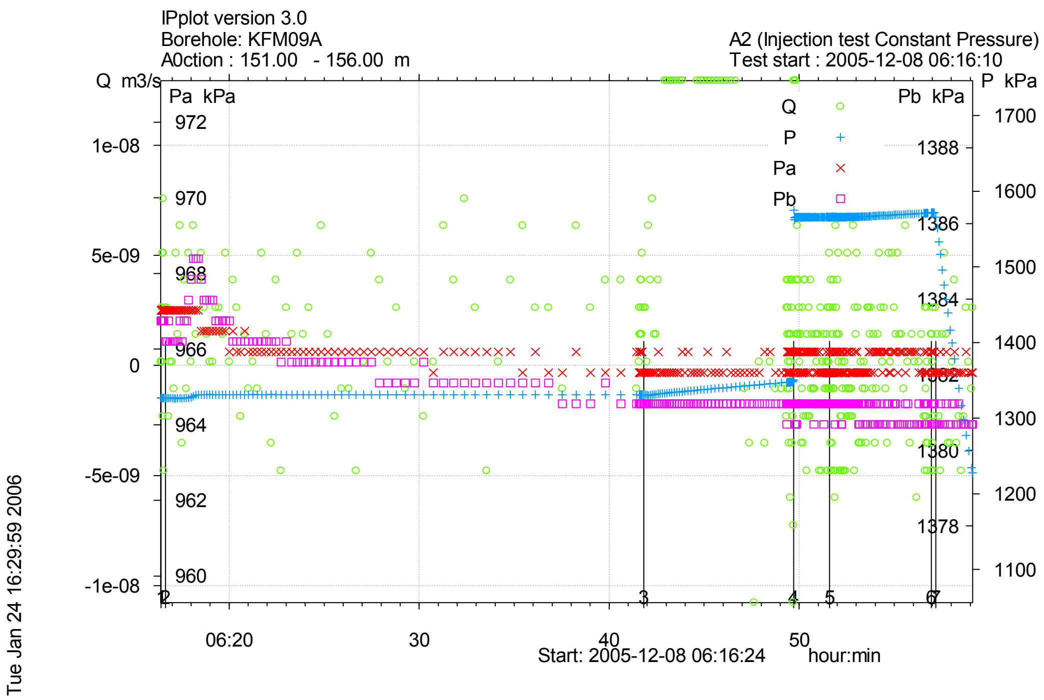


Figure A3-257. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 151.0-156.0 m in borehole KFM09A.*

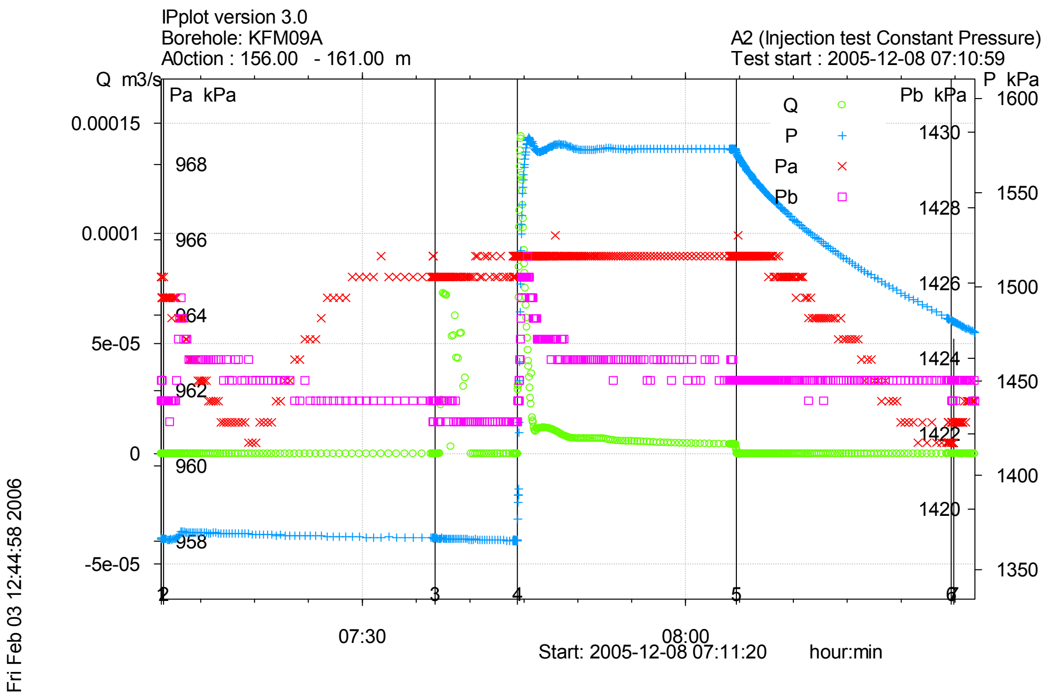


Figure A3-258. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 156.0-161.0 m in borehole KFM09A.*

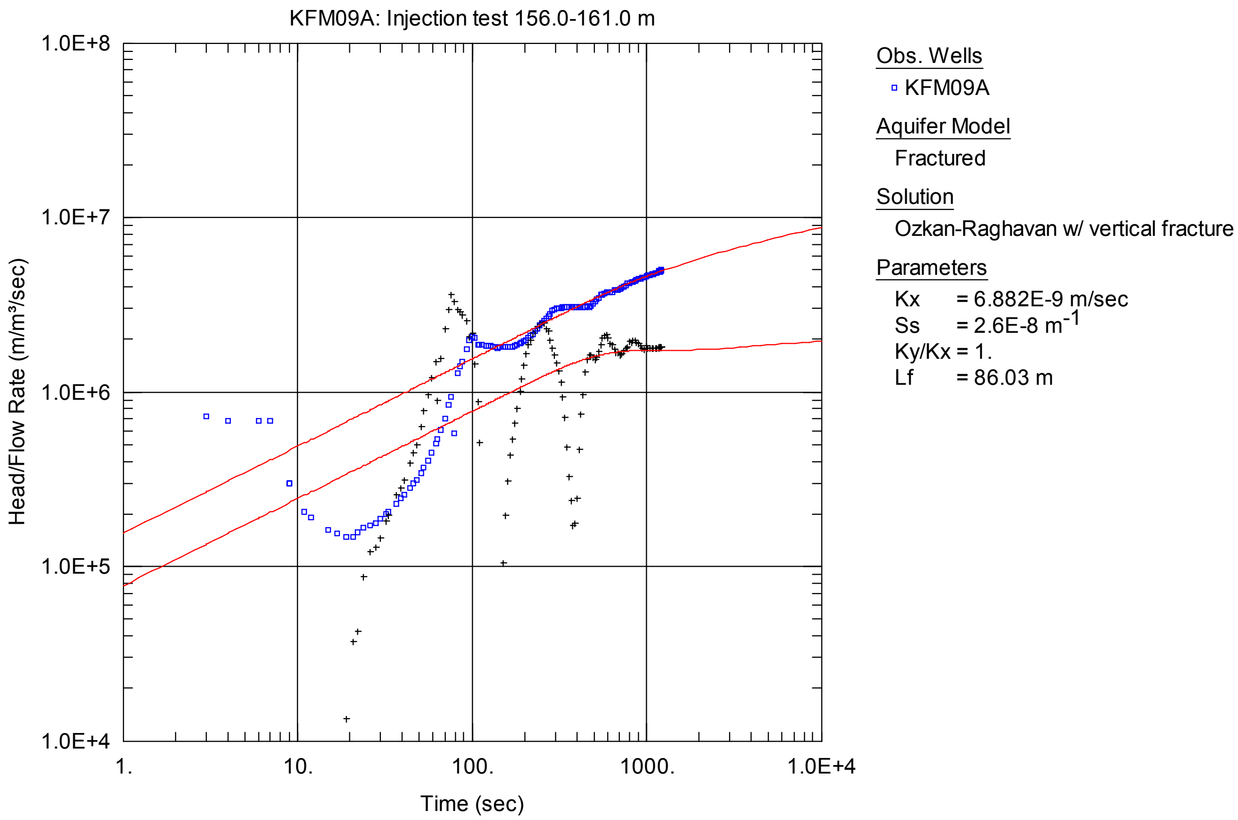


Figure A3-259. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 156.0-161.0 m in KFM09A.*

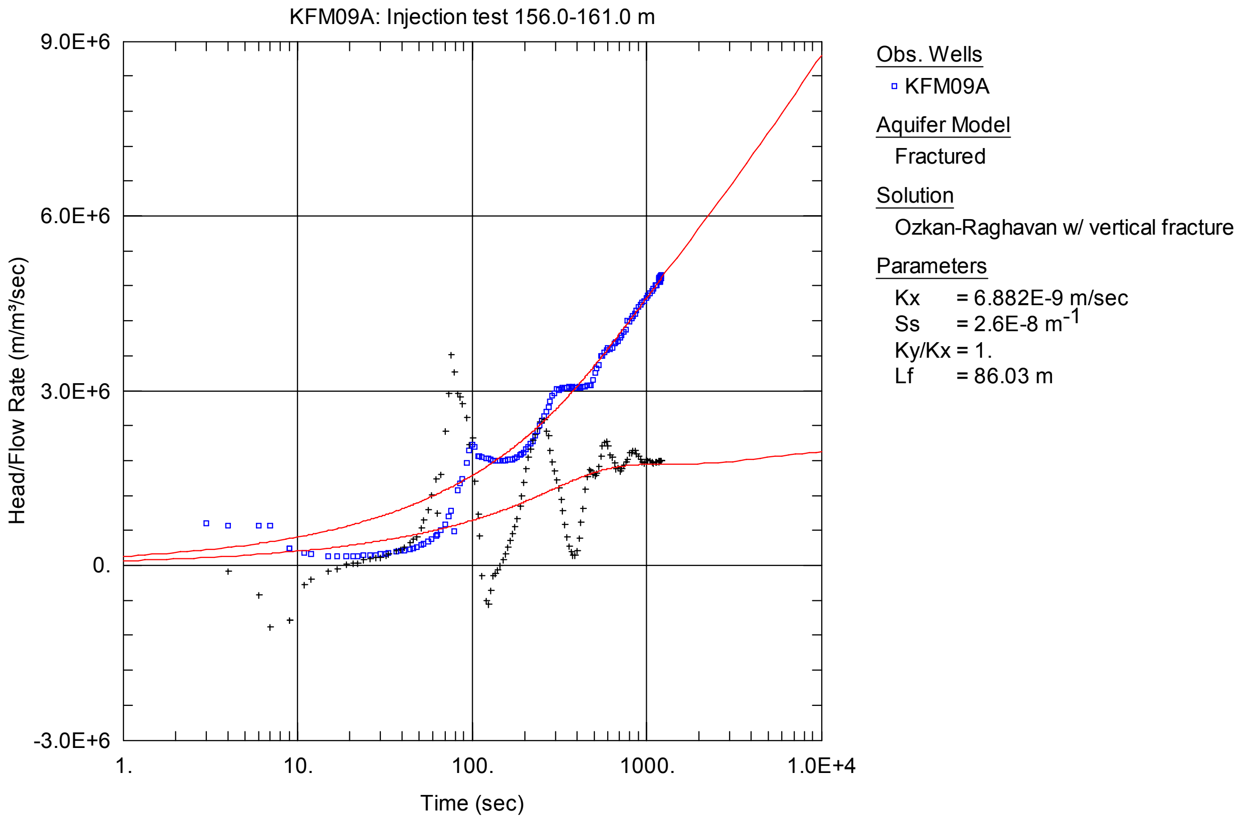


Figure A3-260. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 156.0-161.0 m in KFM09A.*

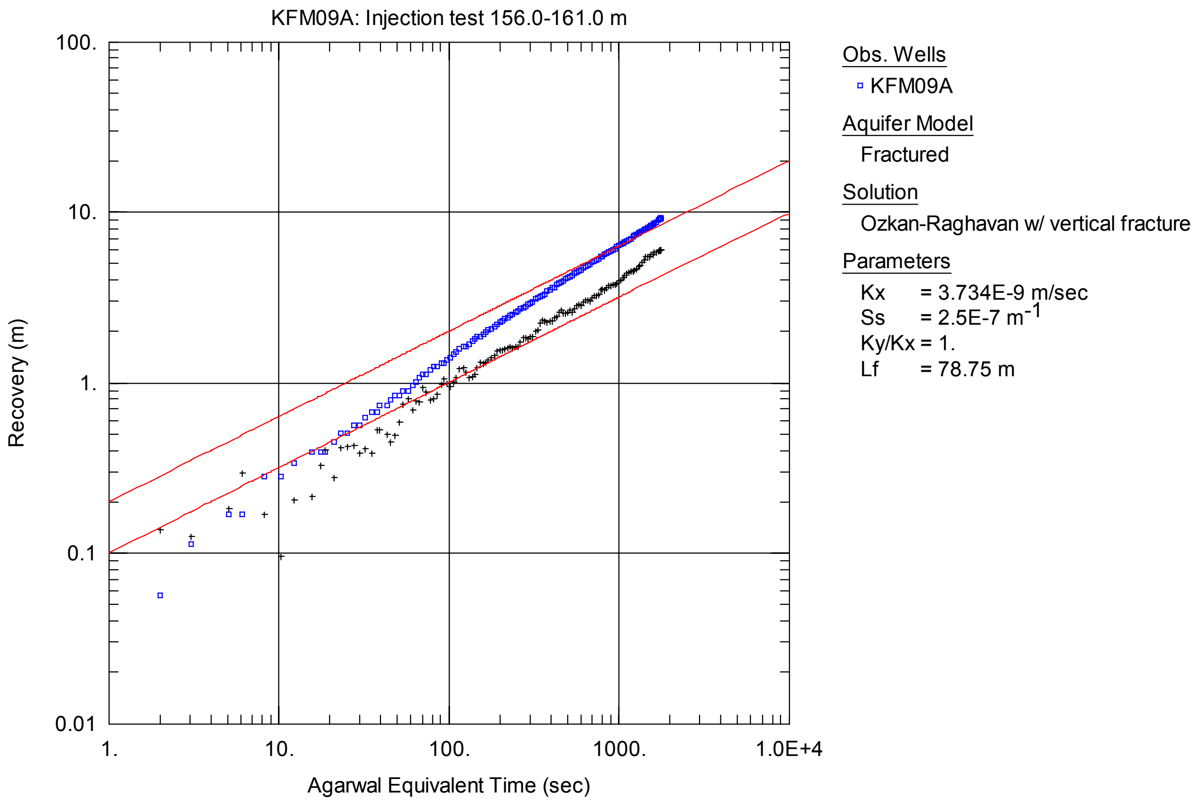


Figure A3-261. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 156.0-161.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.*

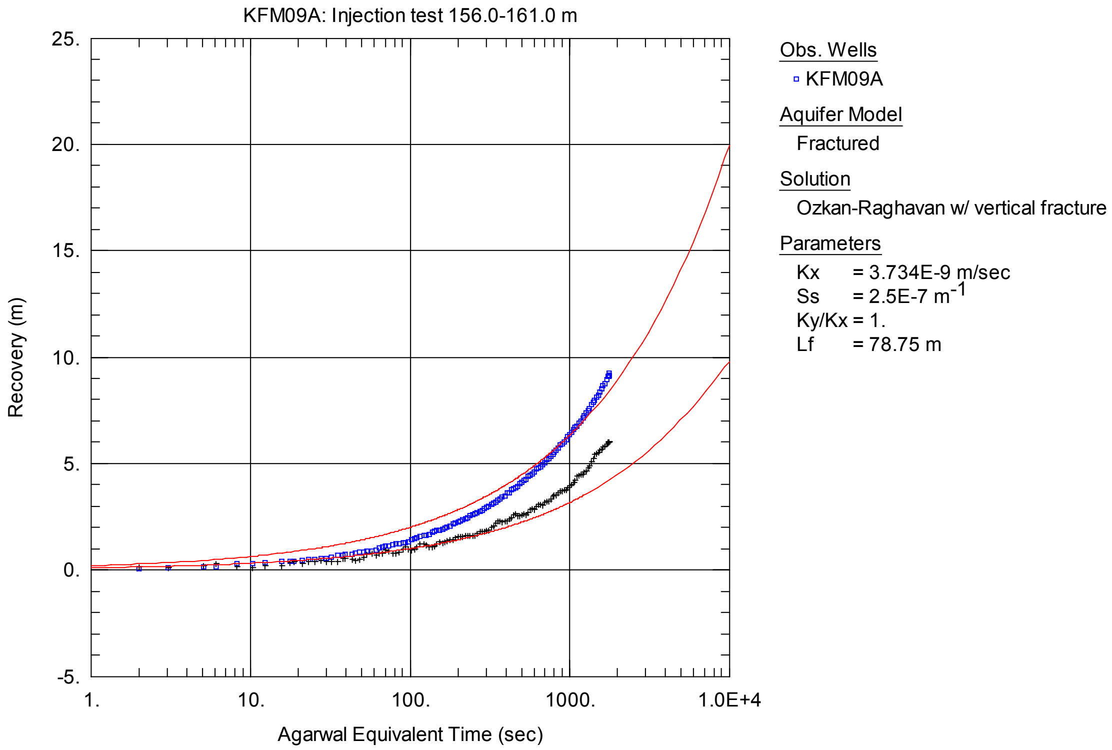


__Figure A3-262.__ Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 156.0-161.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.

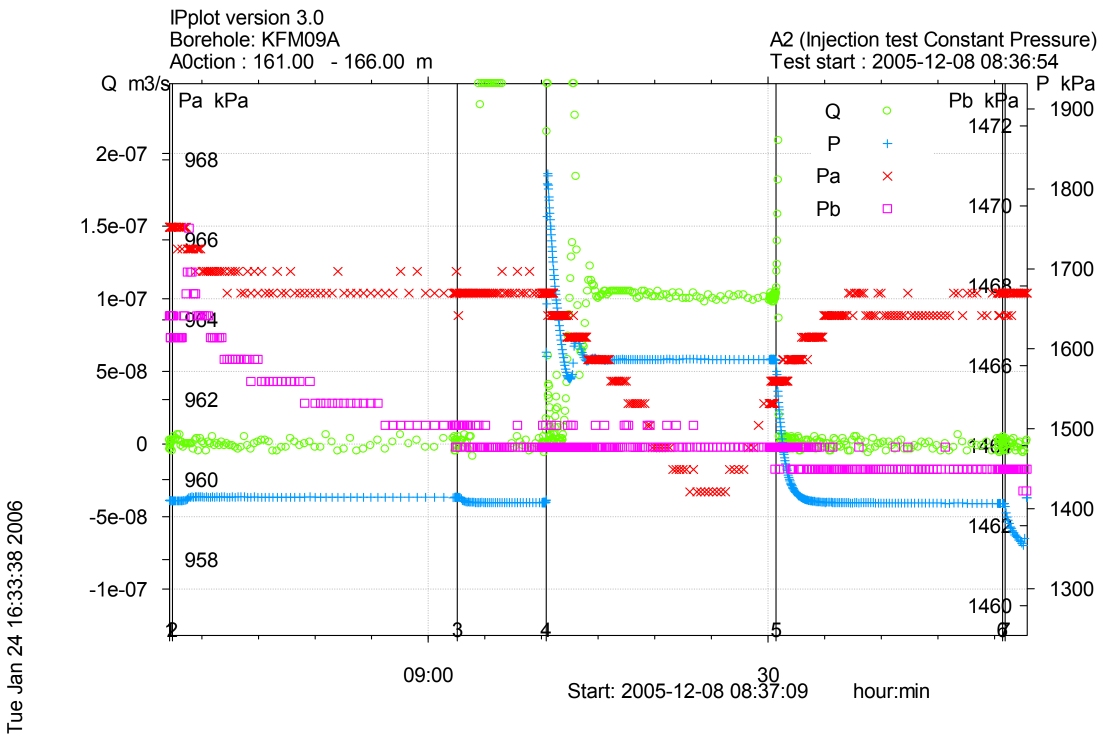


__Figure A3-263.__ Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 161.0-166.0 m in borehole KFM09A.

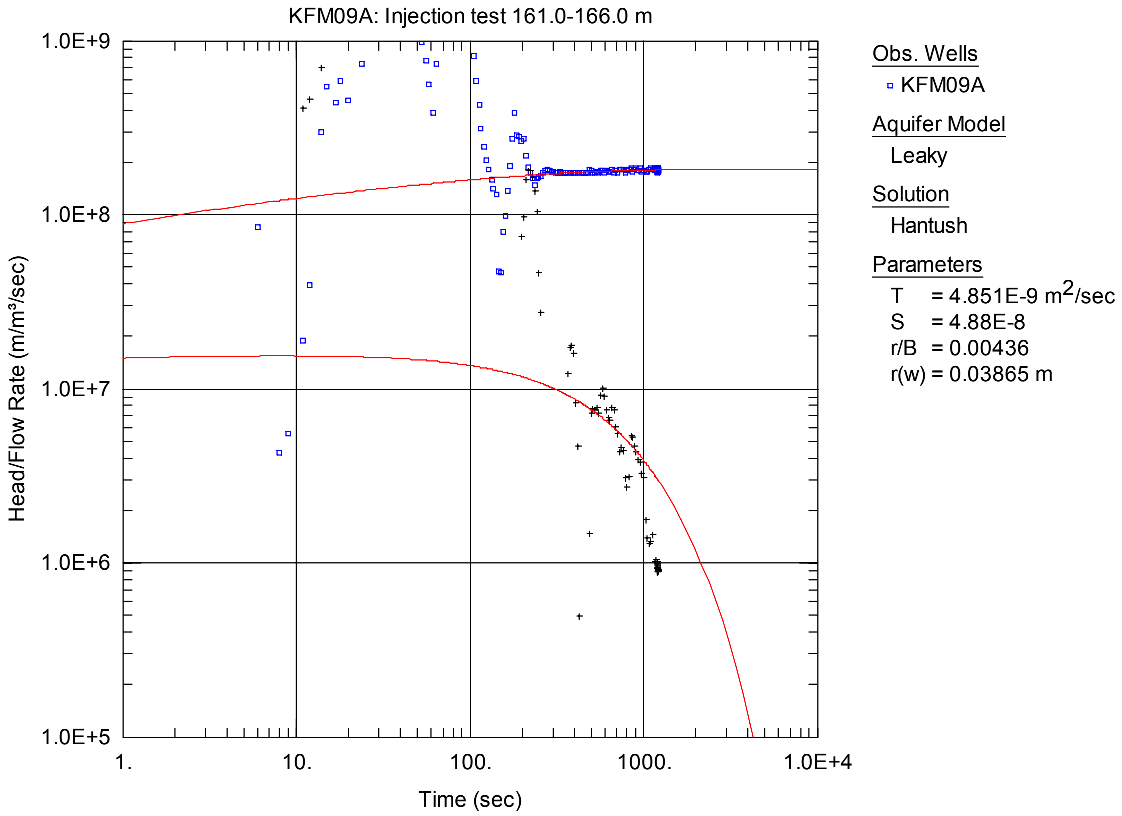


***Figure A3-264.** Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 161.0-166.0 m in KFM09A.*

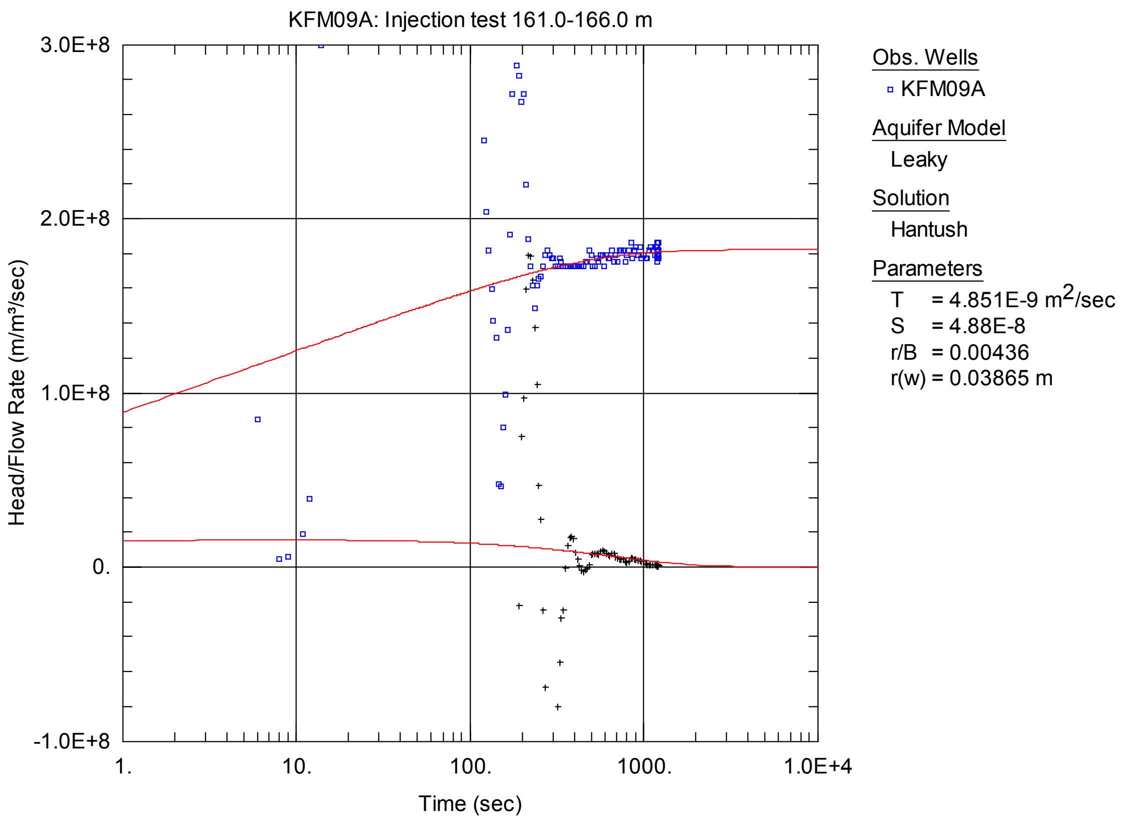


***Figure A3-265.** Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 161.0-166.0 m in KFM09A.*

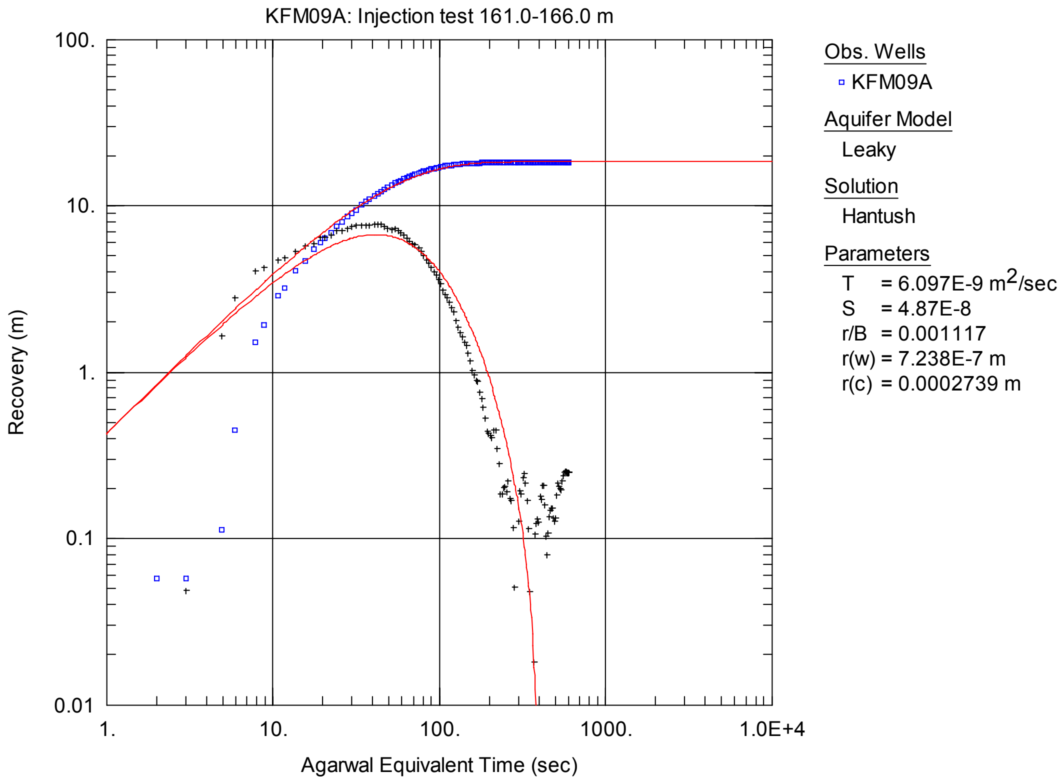


Figure A3-266. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 161.0-166.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.*

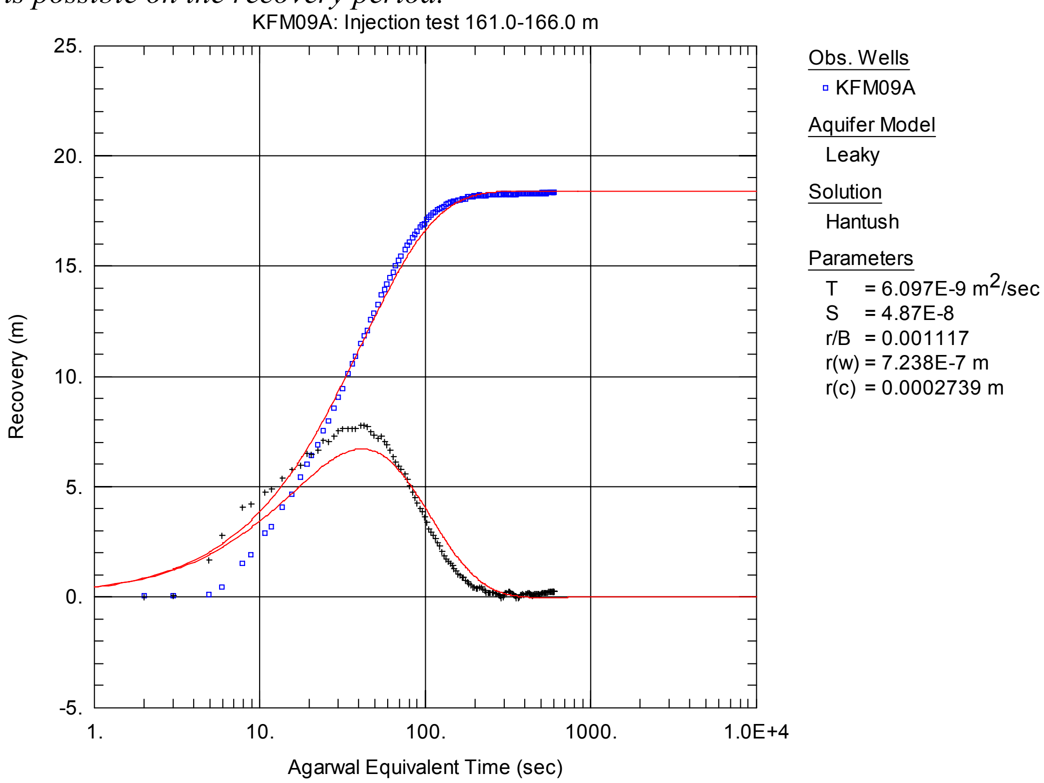


Figure A3-267. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 161.0-166.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.*

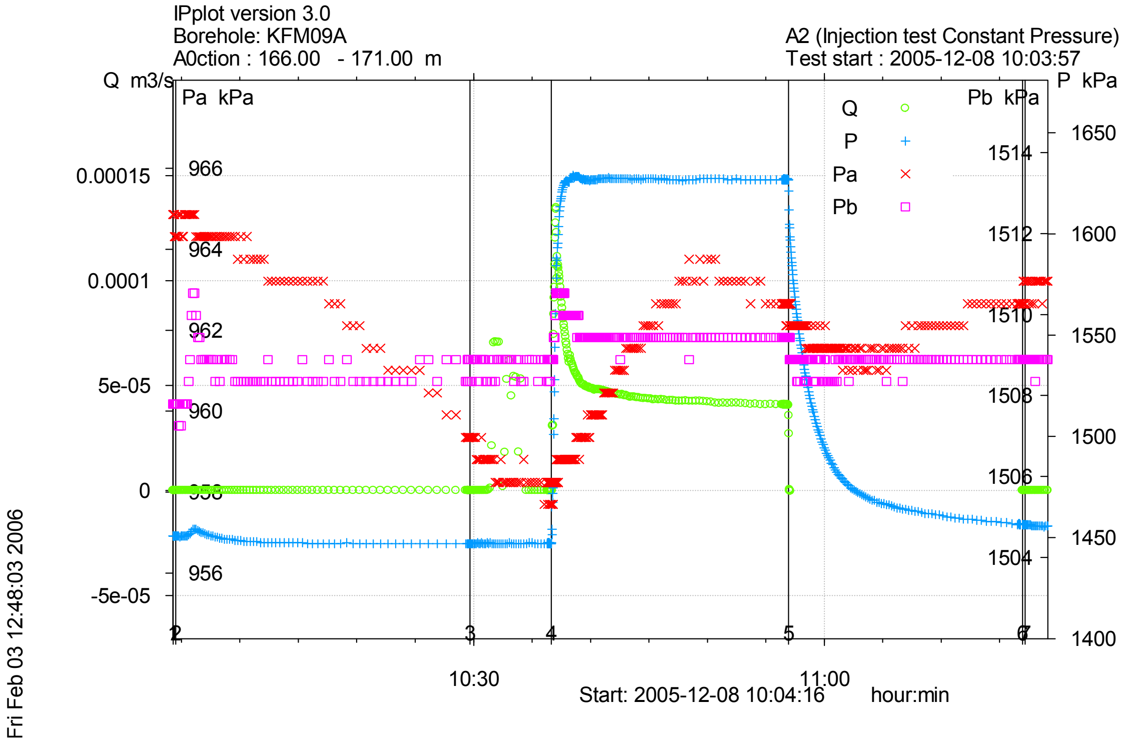


Figure A3-268. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 166.0-171.0 m in borehole KFM09A.*

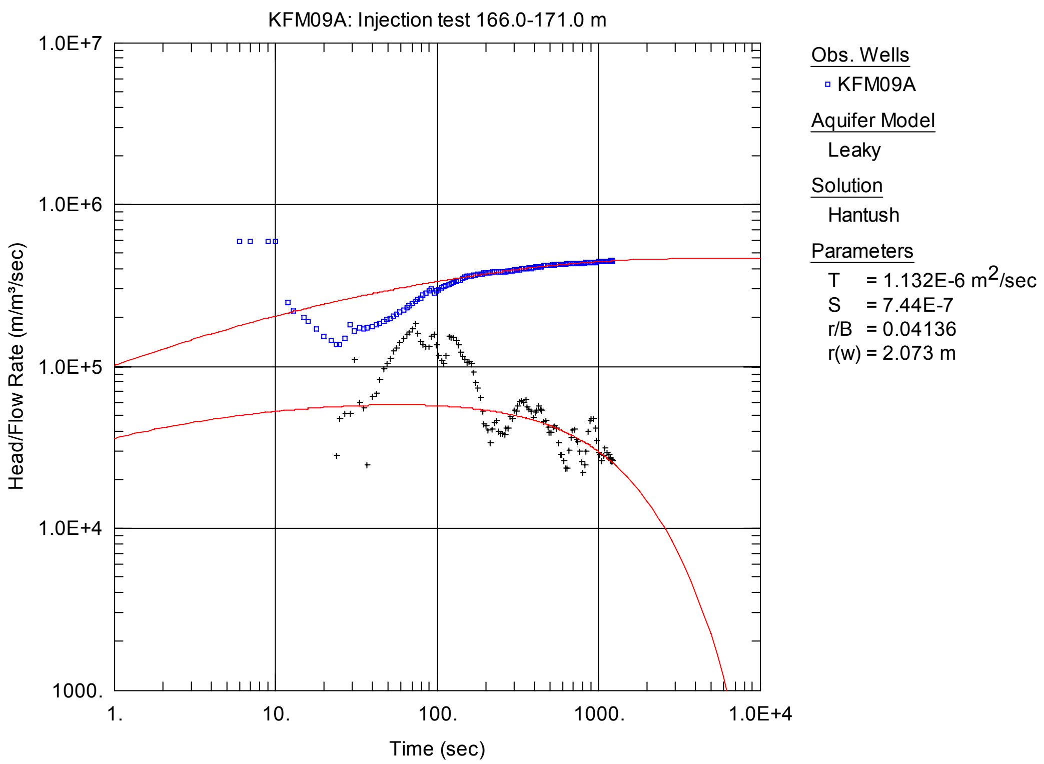


Figure A3-269. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 166.0-171.0 m in KFM09A.*

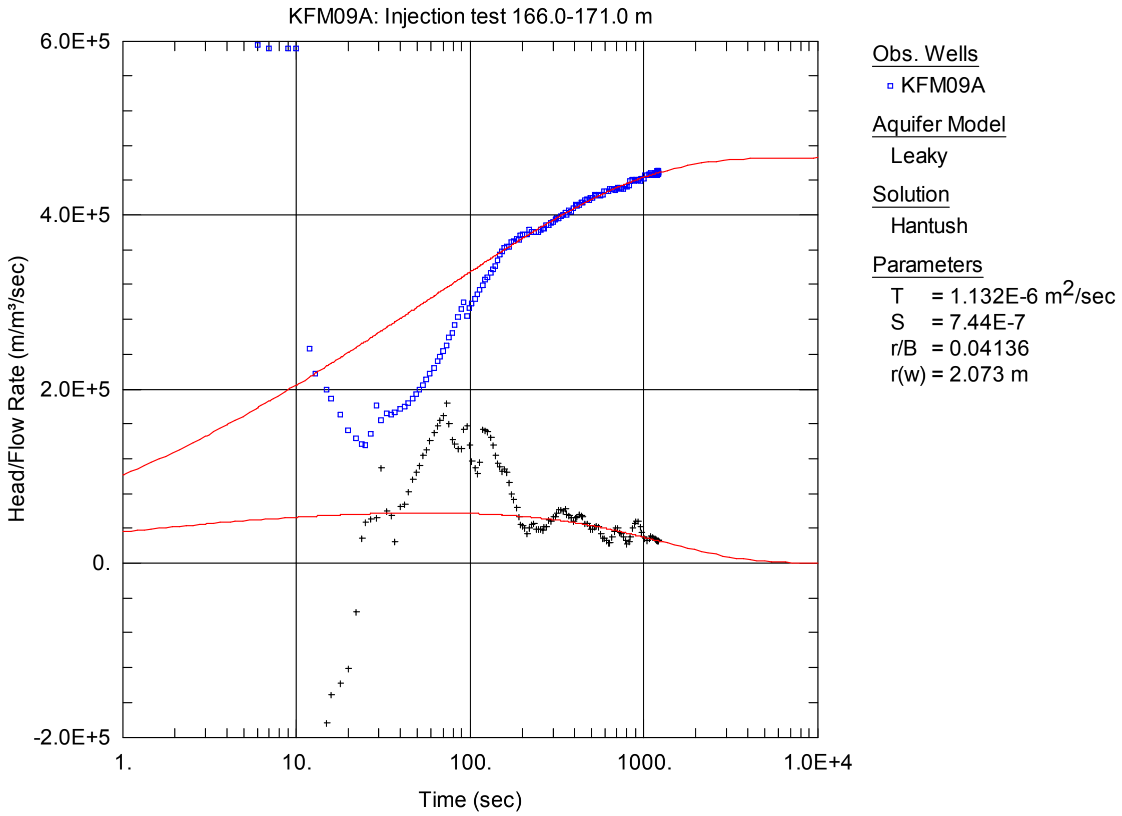


Figure A3-270. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 166.0-171.0 m in KFM09A.*

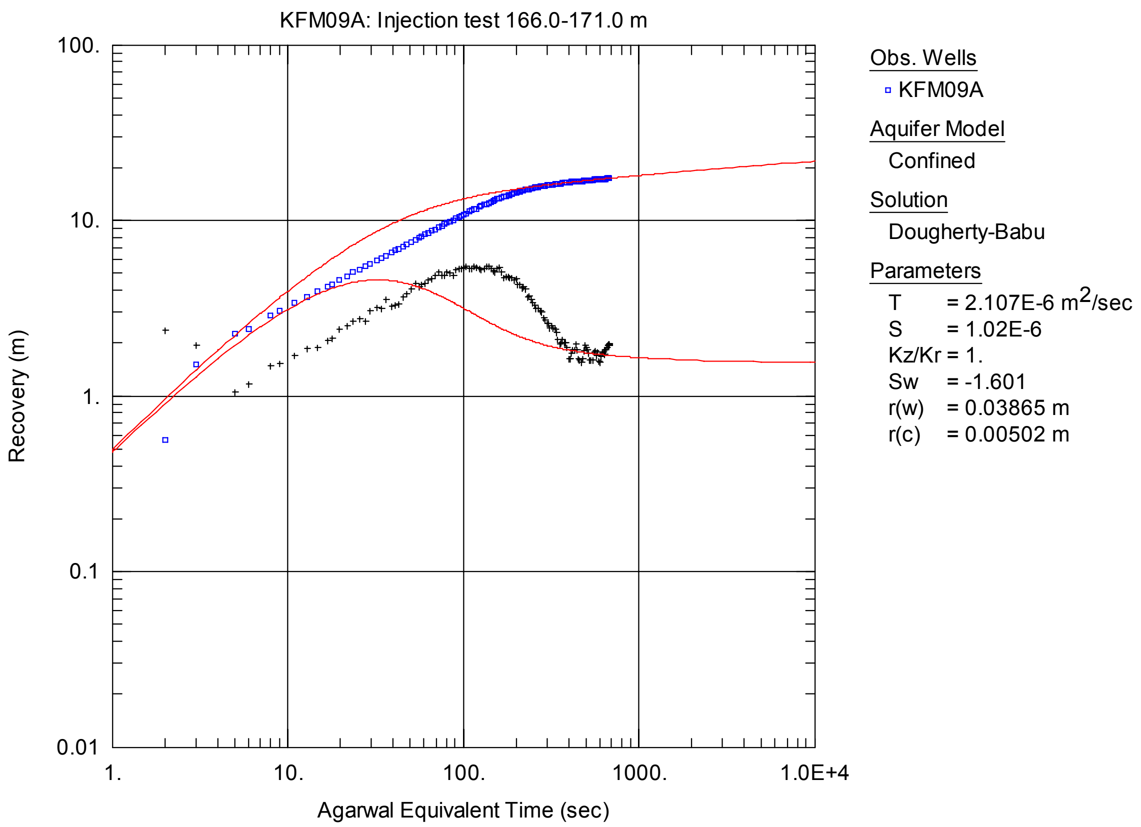


Figure A3-271. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 166.0-171.0 m in KFM09A.*

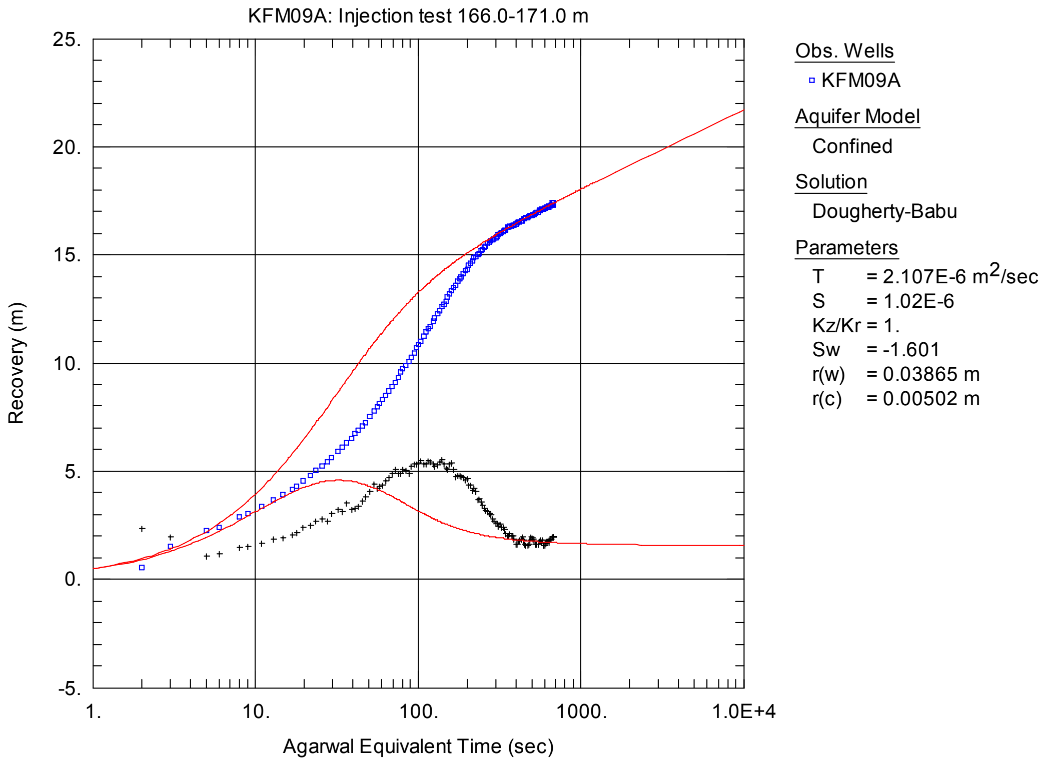


Figure A3-272. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 166.0-171.0 m in KFM09A.*

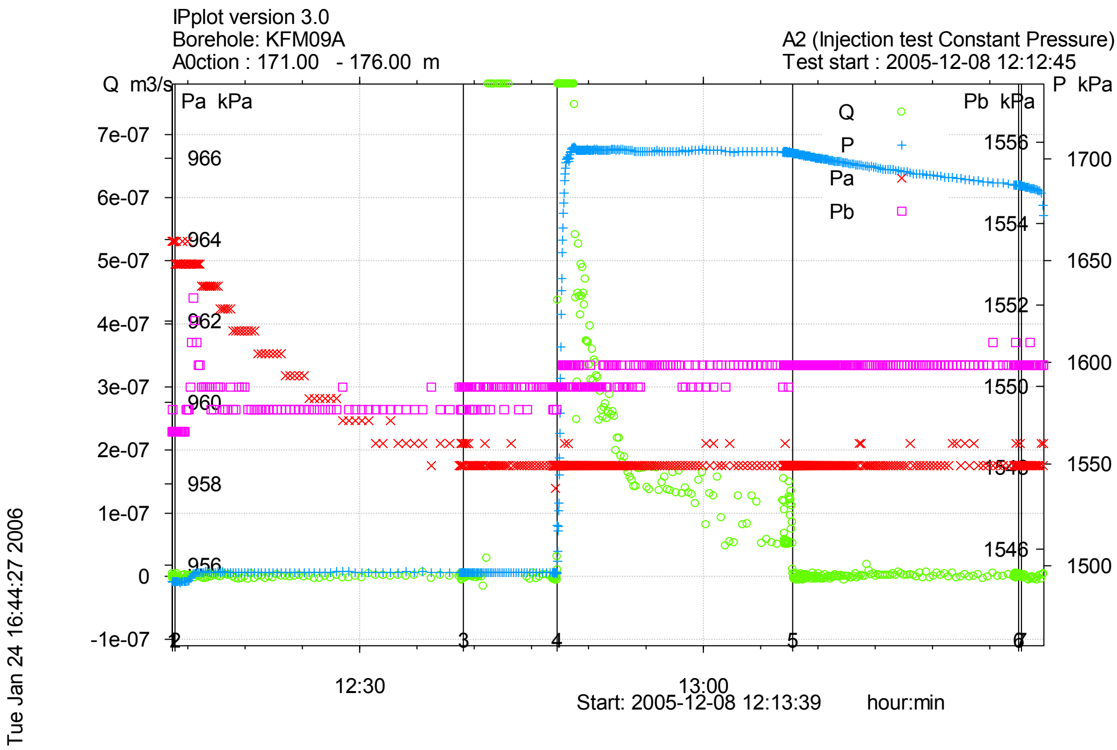


Figure A3-273. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 171.0-176.0 m in borehole KFM09A*

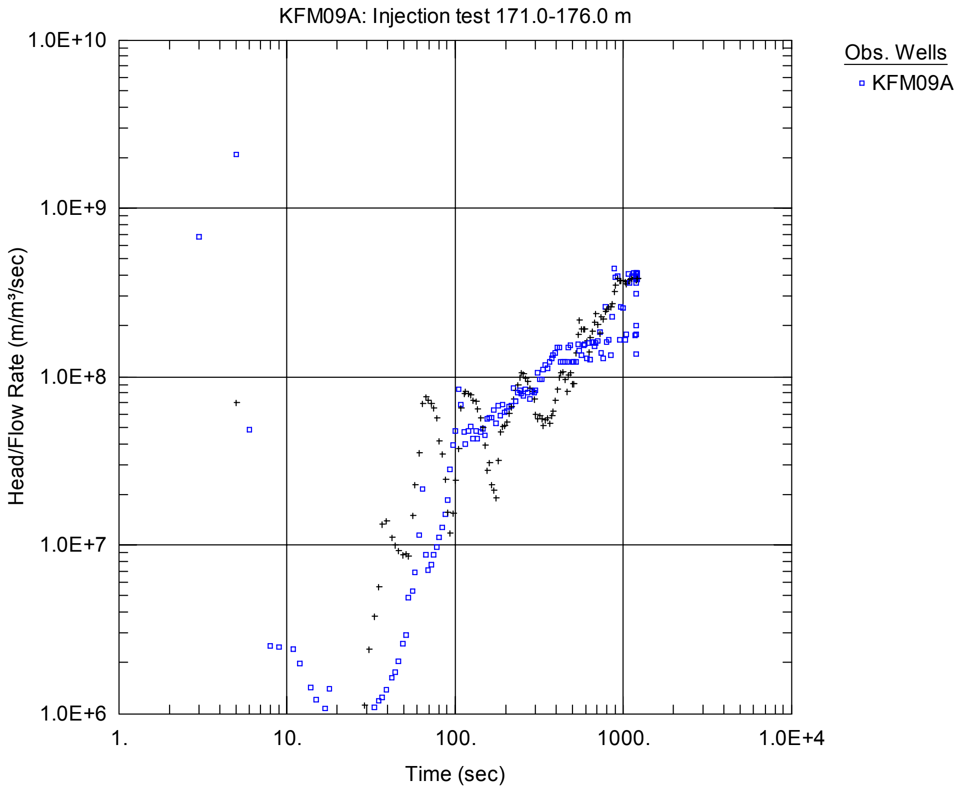


Figure A3-274. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 171.0-176.0 m in KFM09A.

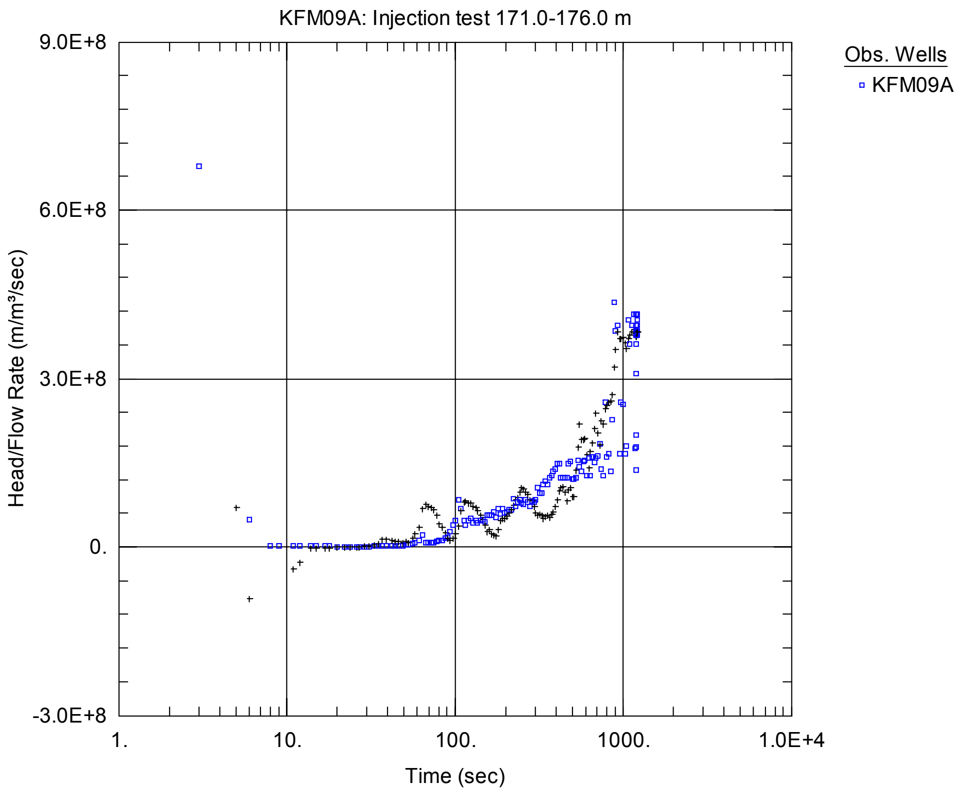


Figure A3-275. Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 171.0-176.0 m in KFM09A.

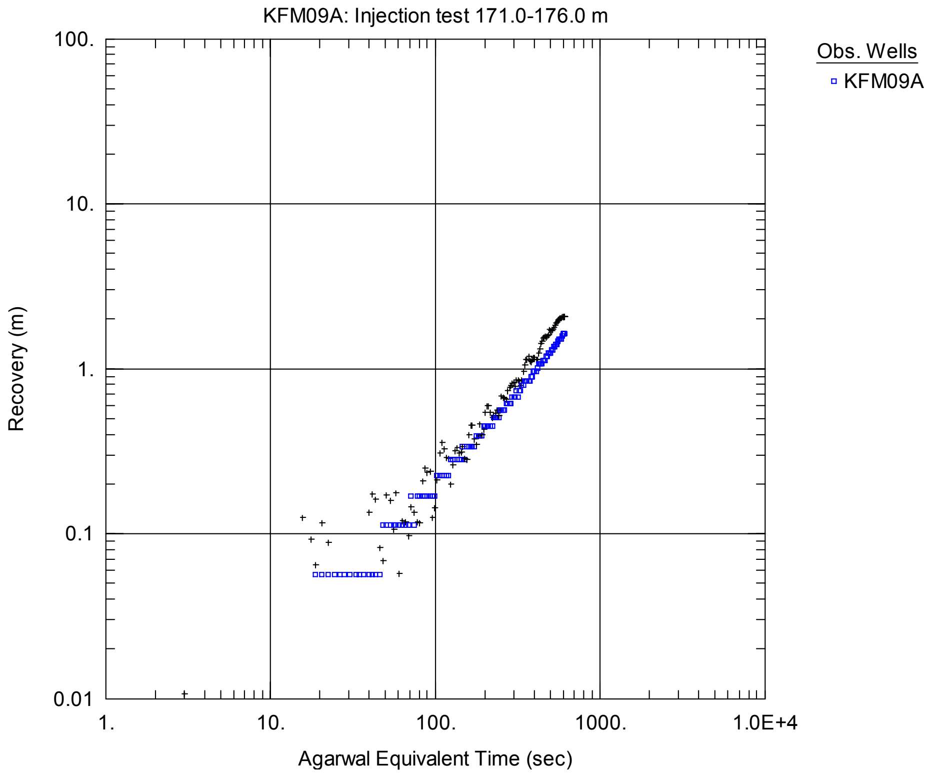


Figure A3-276. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 171.0-176.0 m in KFM09A.*

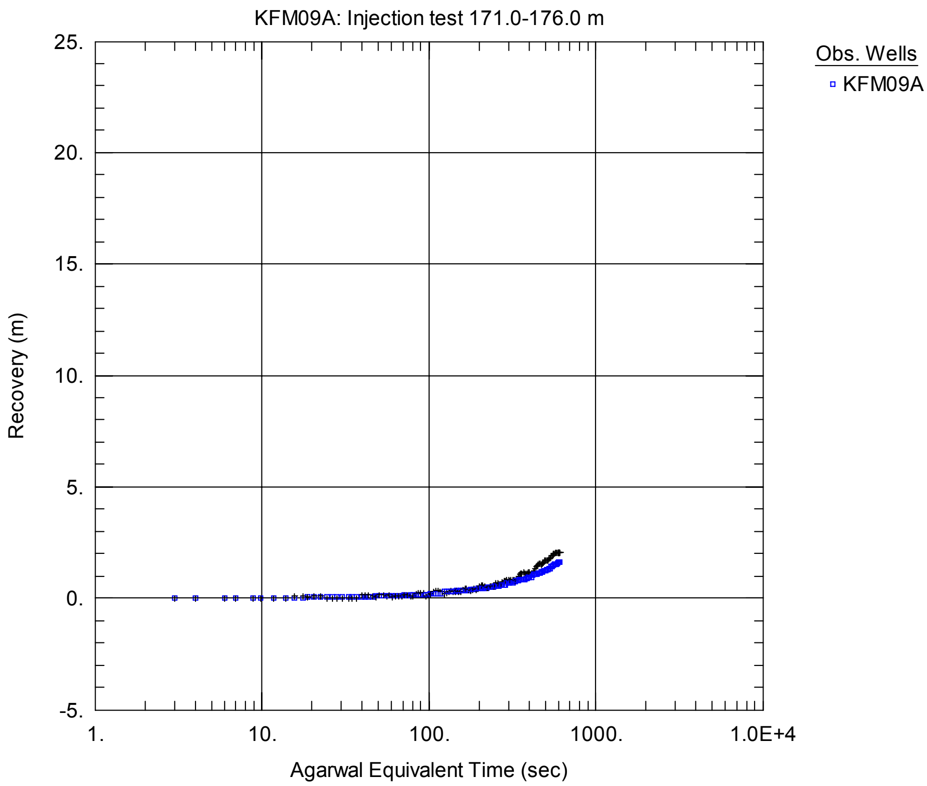


Figure A3-277. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 171.0-176.0 m in KFM09A.*

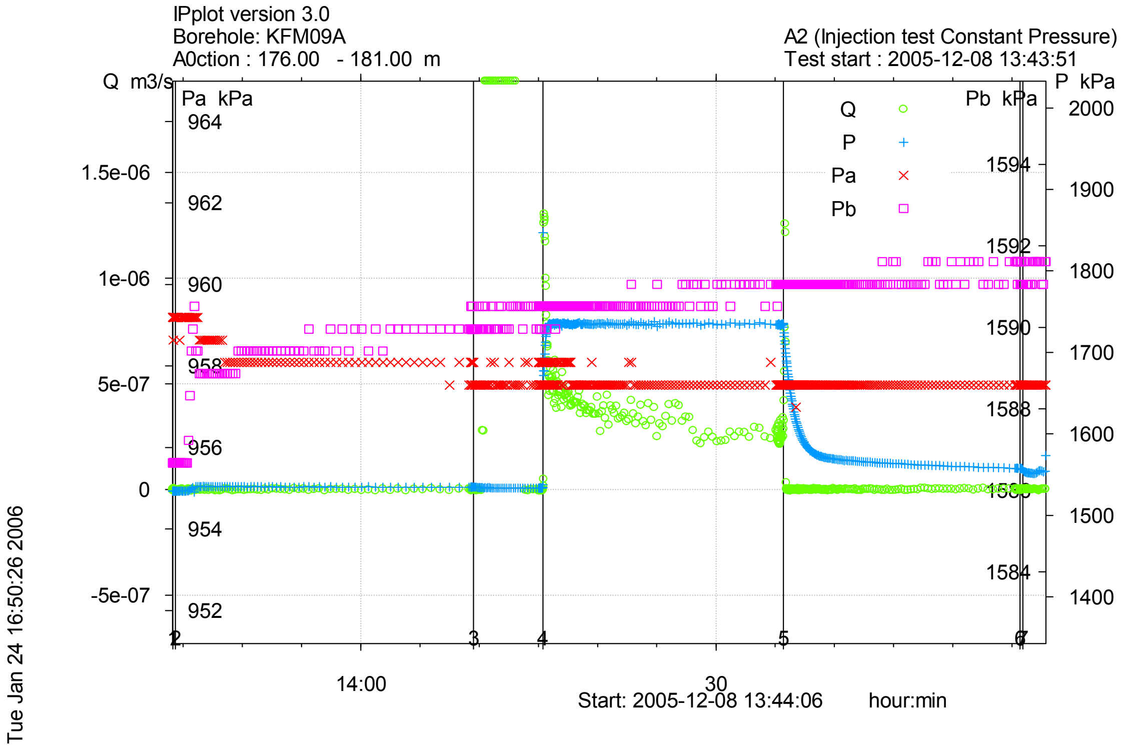


Figure A3-278. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 176.0-181.0 m in borehole KFM09A.*

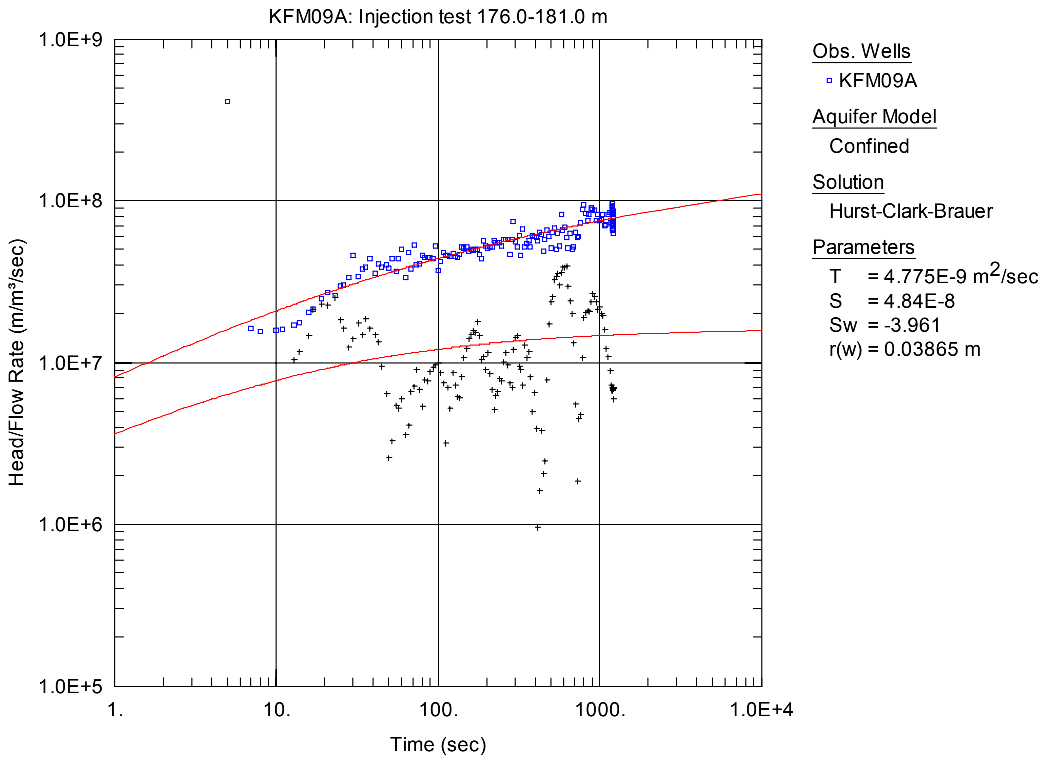


Figure A3-279. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 176.0-181.0 m in KFM09A.*

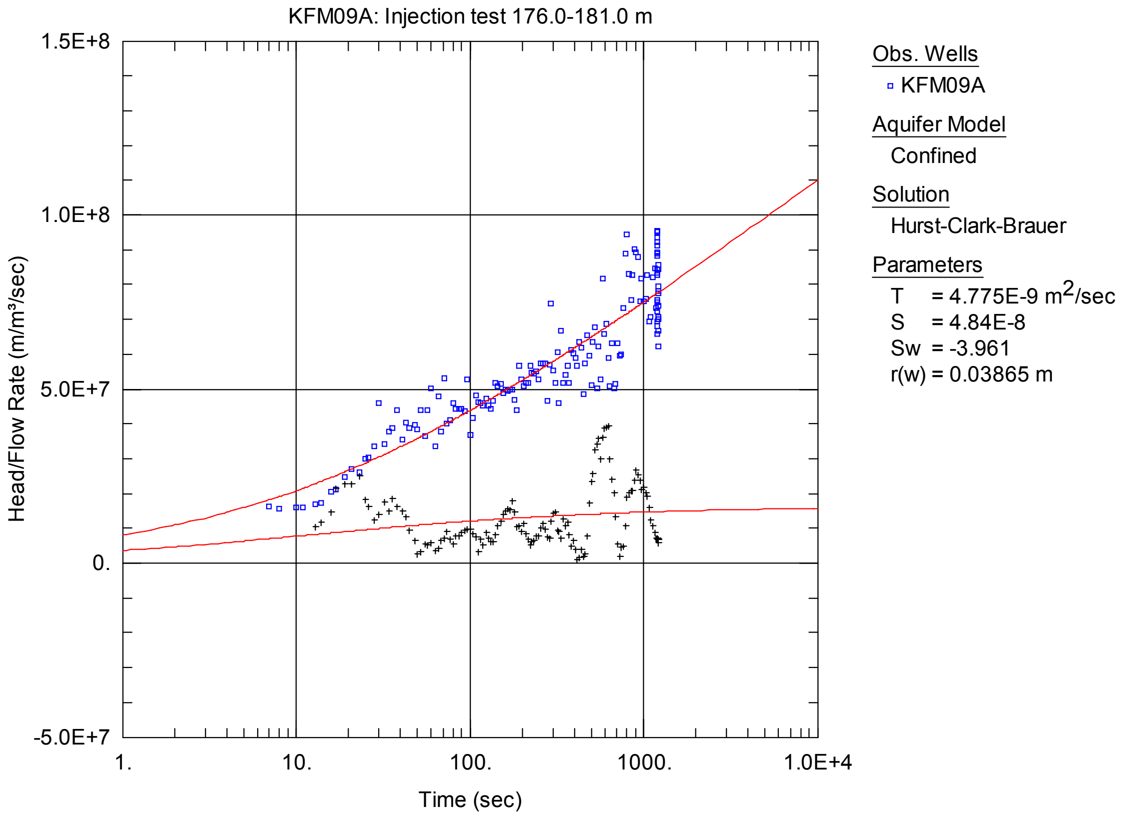


Figure A3-280. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 176.0-181.0 m in KFM09A.*

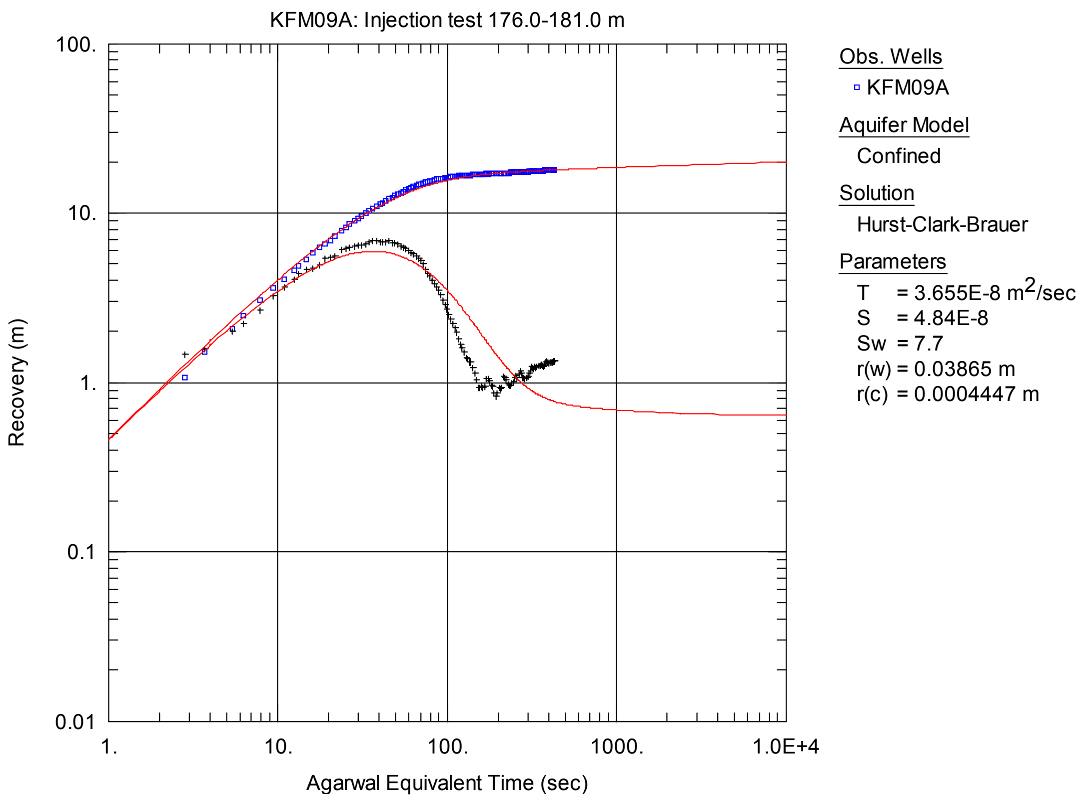


Figure A3-281. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 176.0-181.0 m in KFM09A No unambiguous transient evaluation is possible on the recovery period.*

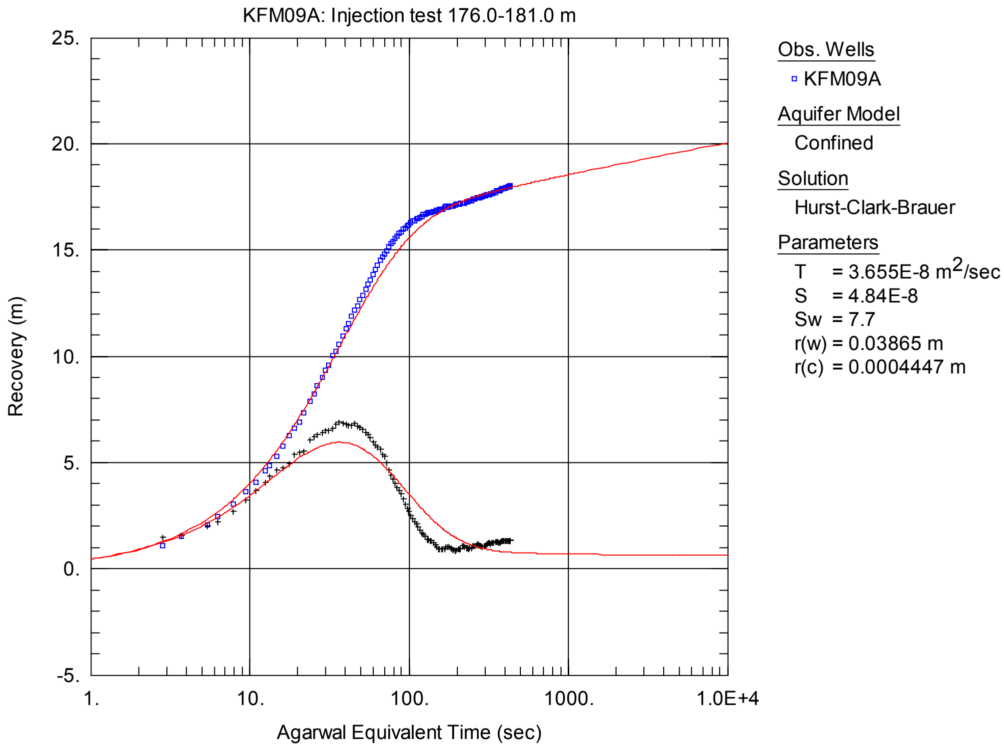


Figure A3-282. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 176.0-181.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.*

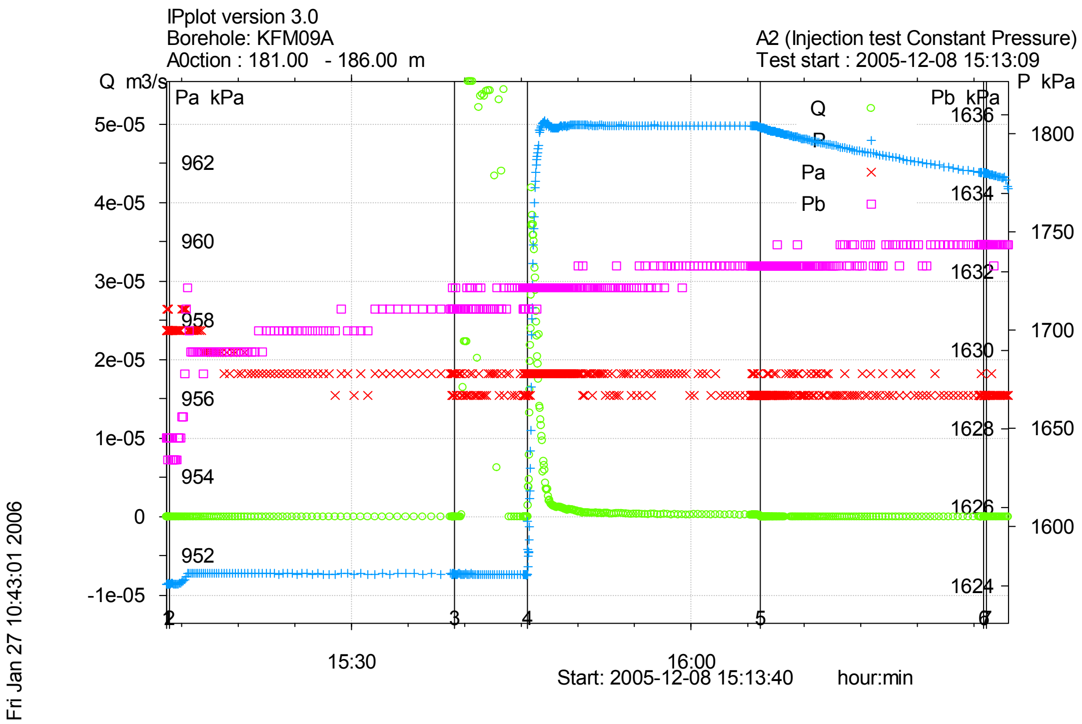


Figure A3-283. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 181.0-186.0 m in borehole KFM09A.*

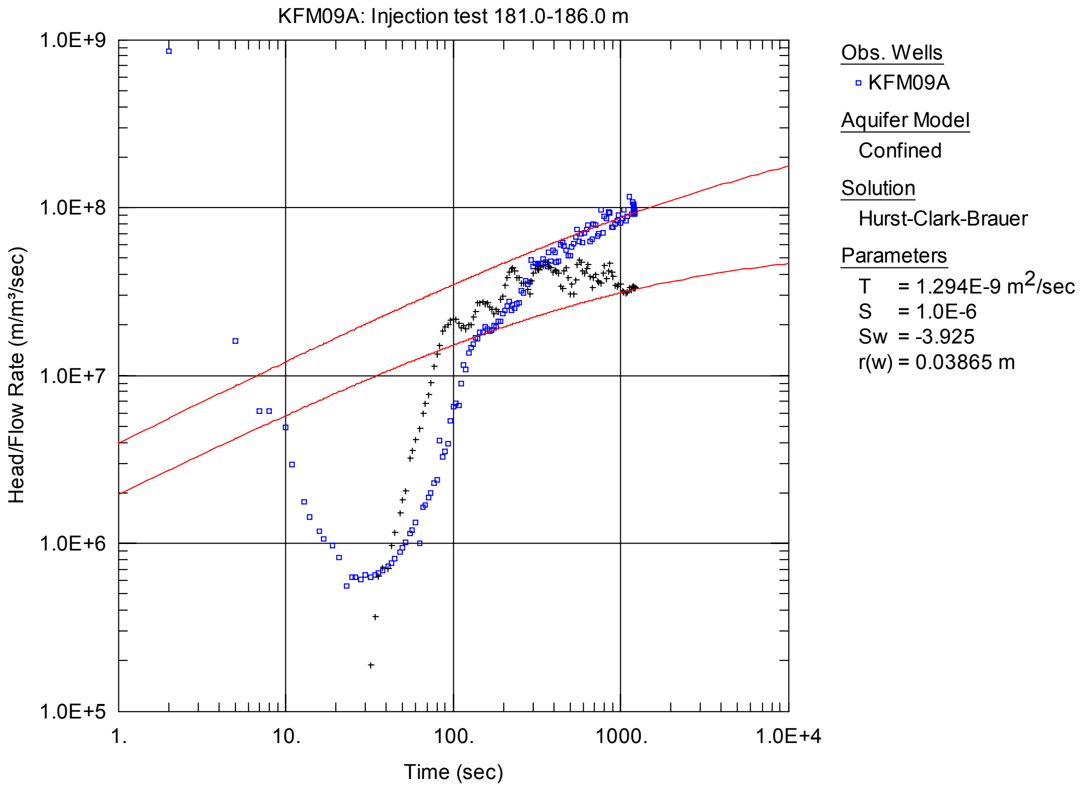


Figure A3-284. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 181.0-186.0 m in KFM09A. A fit with Hurst-Clark-Brauer is not possible and no transient evaluation is possible on the injection.*

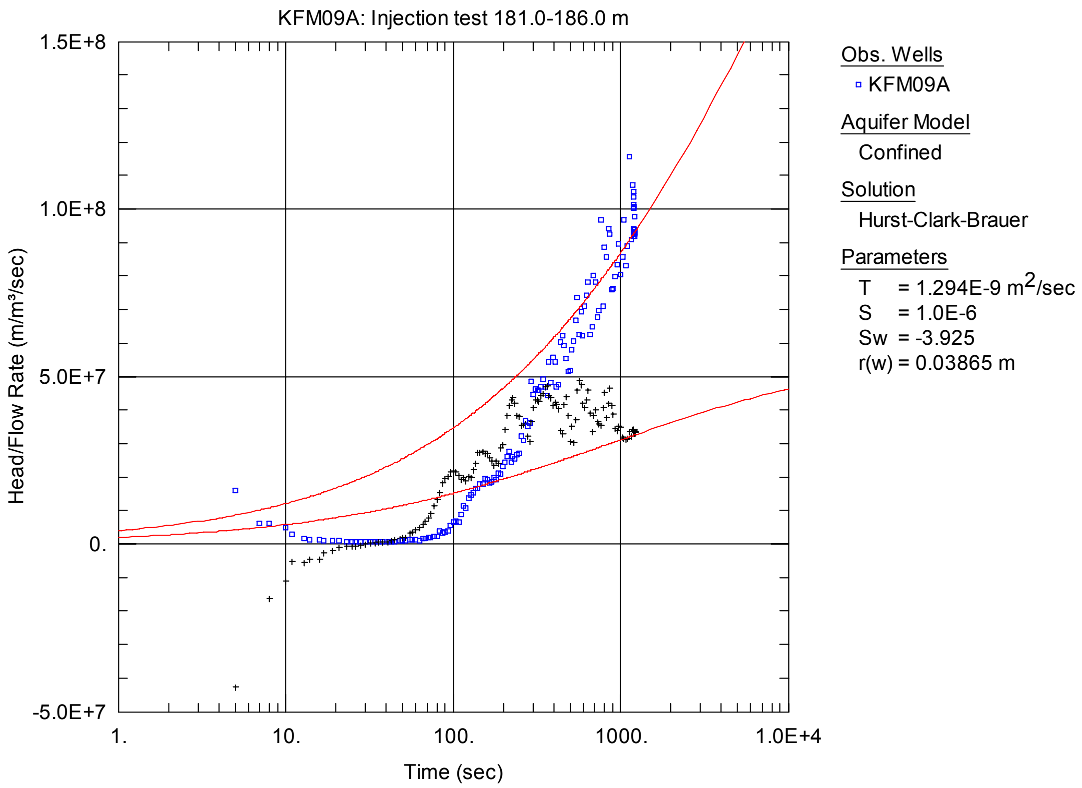


Figure A3-285. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 181.0-186.0 m in KFM09A. A fit with Hurst-Clark-Brauer is not possible and no transient evaluation is possible on the injection.*

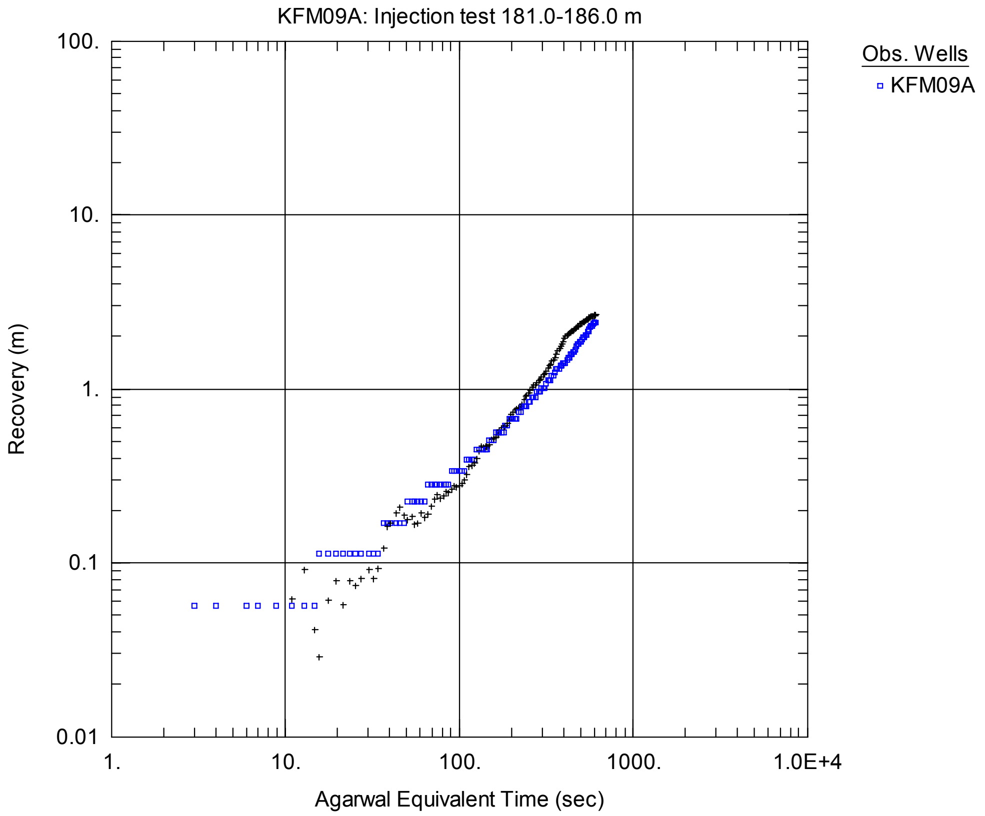


***Figure A3-286.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 181.0-186.0 m in KFM09A.*

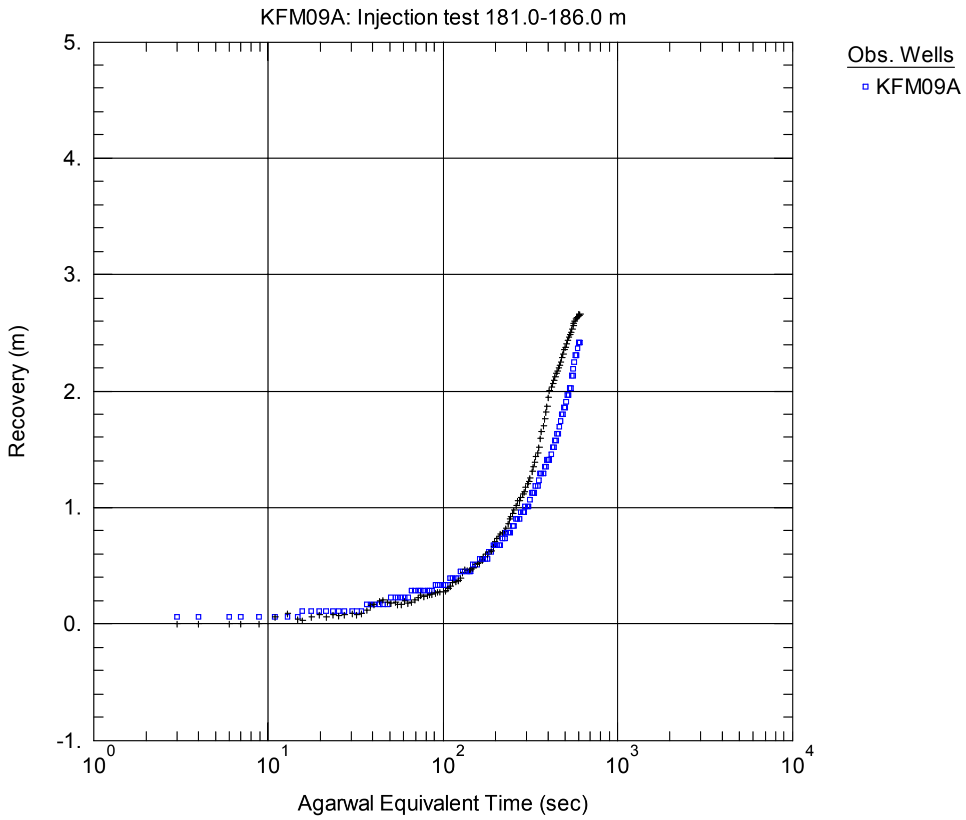


***Figure A3-287.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 181.0-186.0 m in KFM09A.*

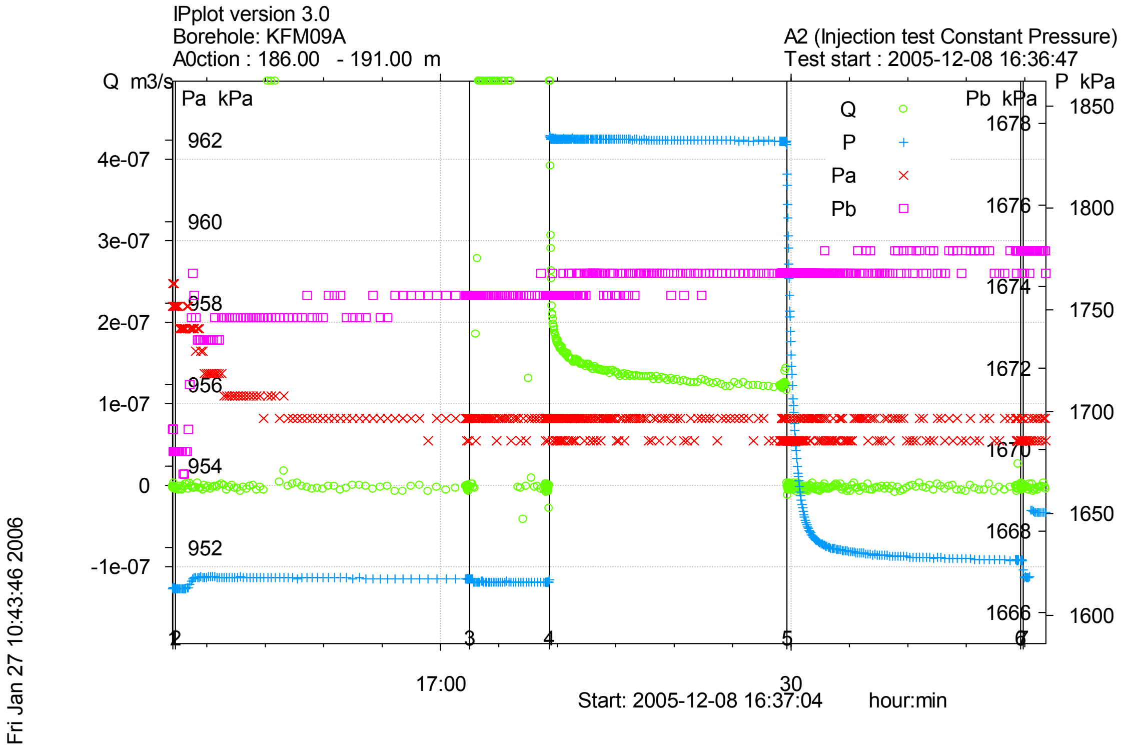


Figure A3-288. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 186.0-191.0 m in borehole KFM09A.

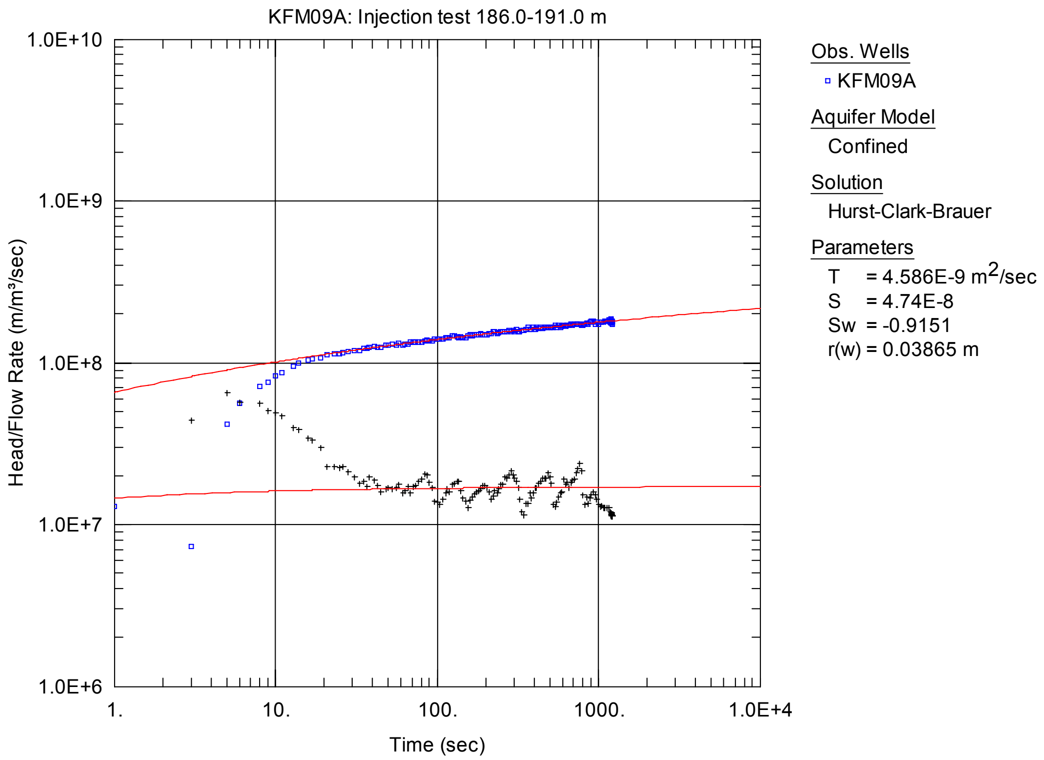


Figure A3-289. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 186.0-191.0 m in KFM09A.

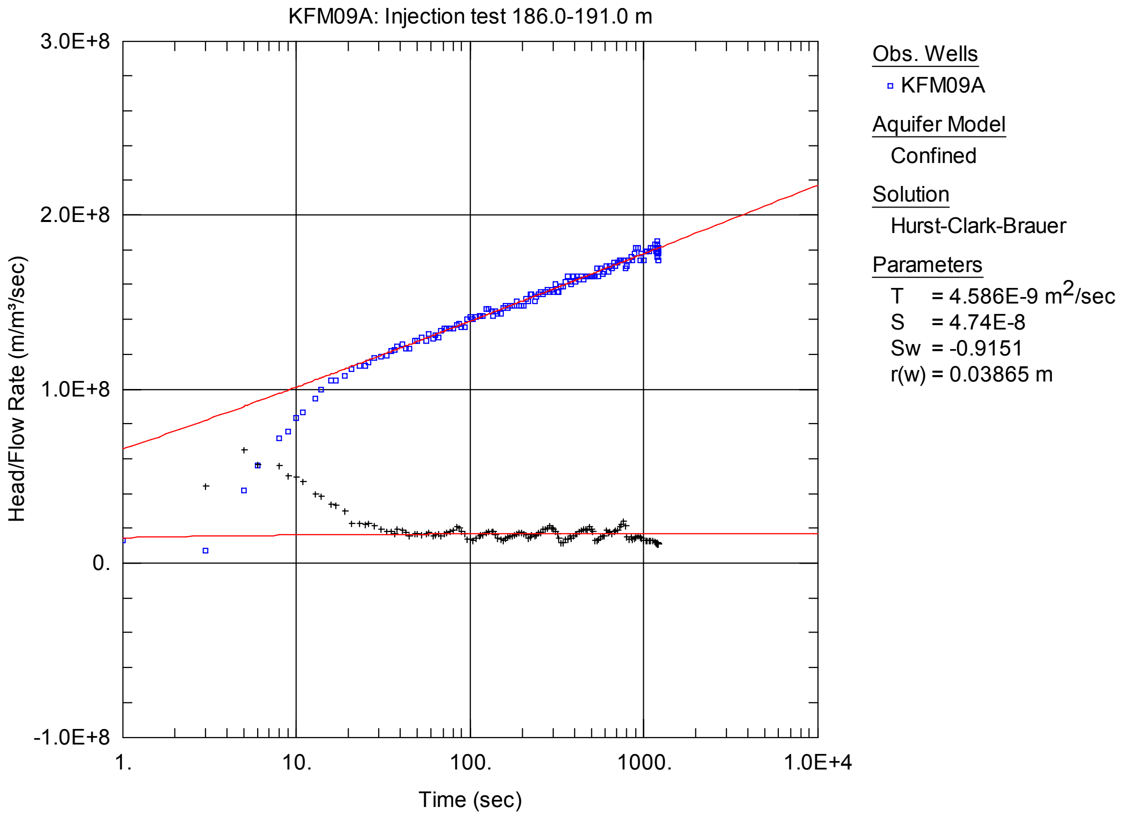


Figure A3-290. Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 186.0-191.0 m in KFM09A.

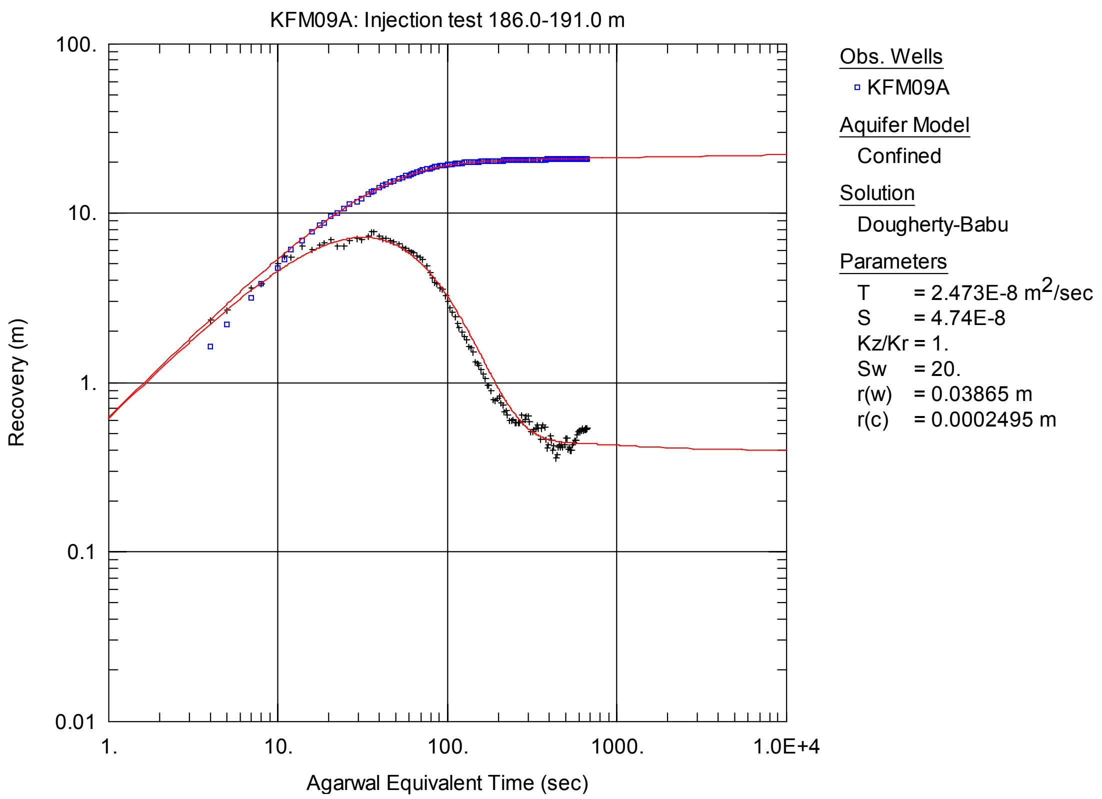


Figure A3-291. Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 186.0-191.0 m in KFM09A. The transient evaluation on the recovery period is not regarded as representative.

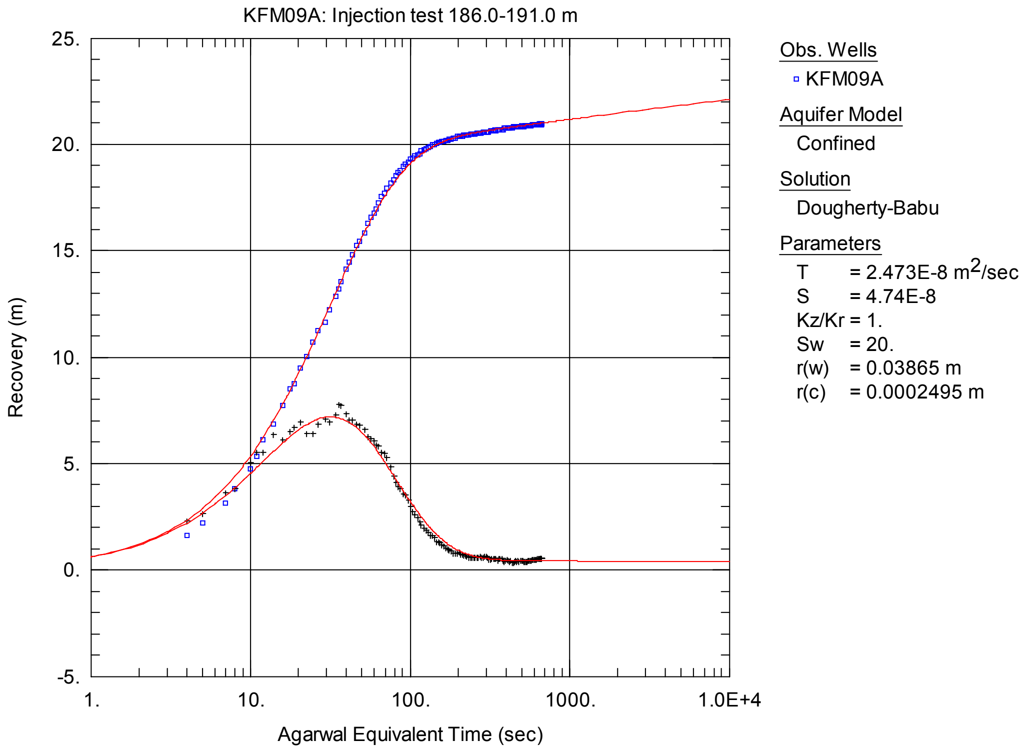


***Figure A3-292.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 186.0-191.0 m in KFM09A. The transient evaluation on the recovery period is not regarded as representative.*

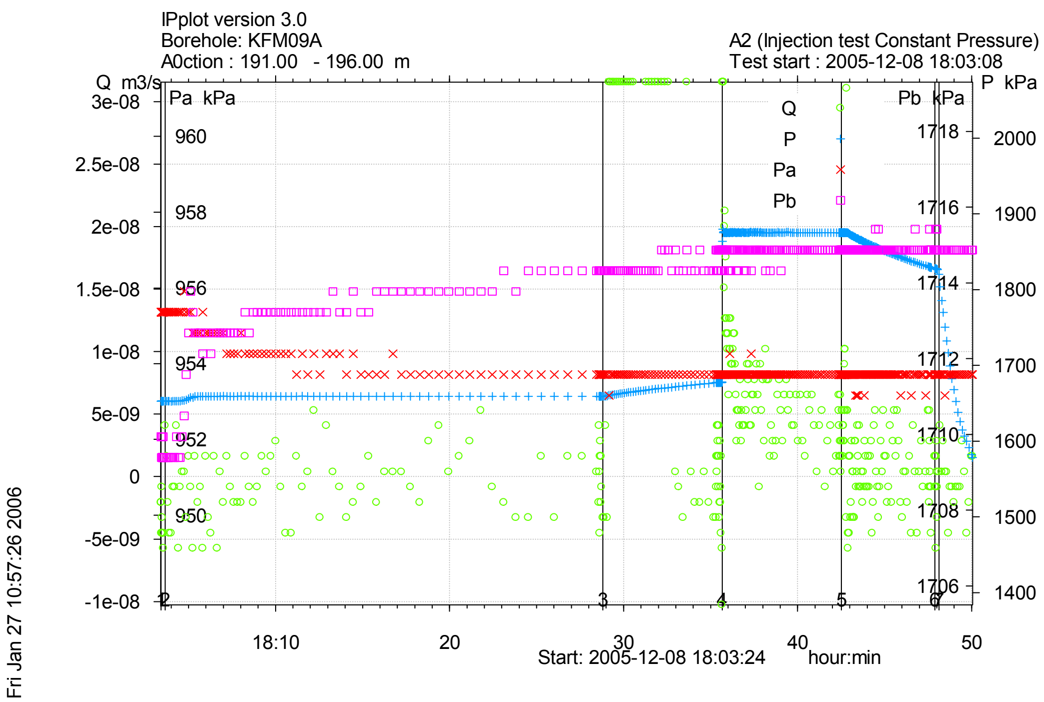


***Figure A3-293.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 191.0-196.0 m in borehole KFM09A.*

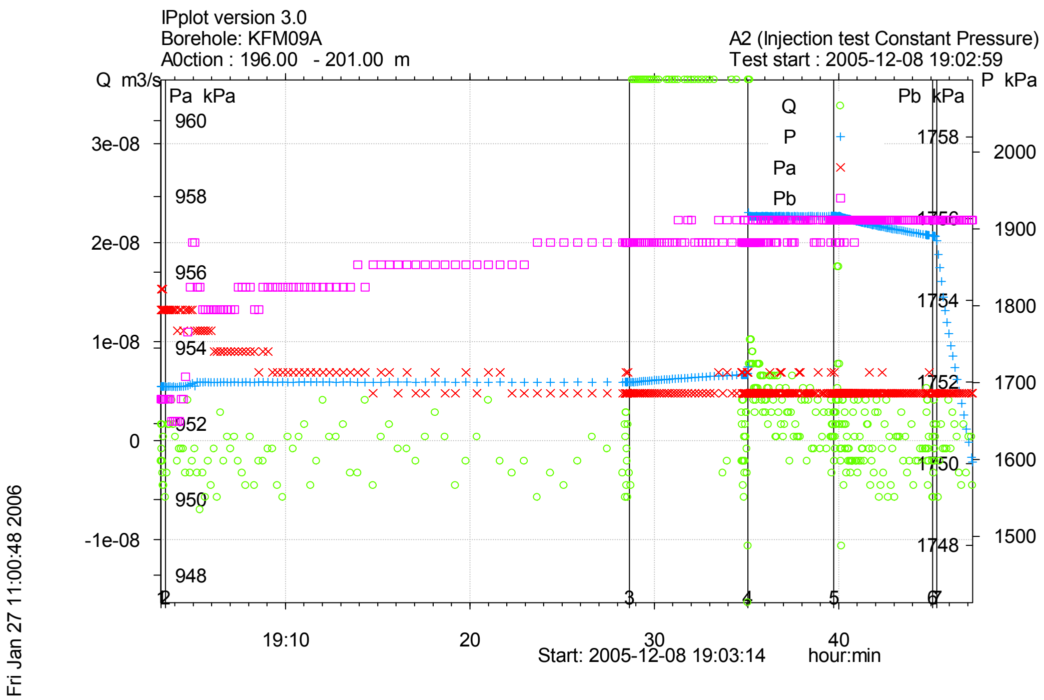


Figure A3-294. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 196.0-201.0 m in borehole KFM09A.*

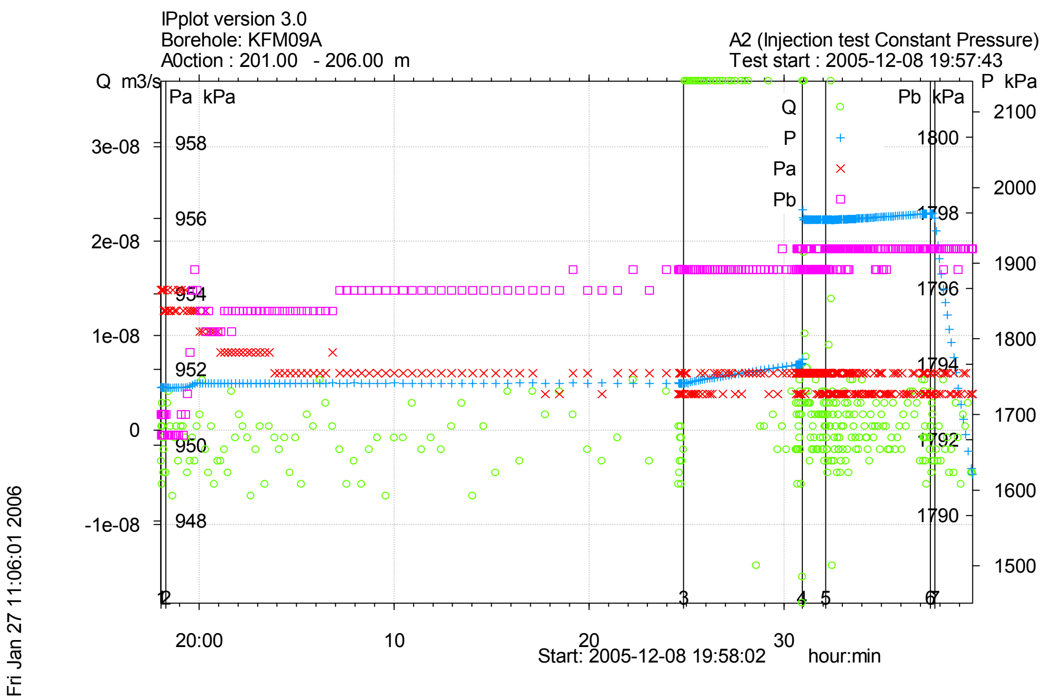


Figure A3-295. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 201.0-206.0 m in borehole KFM09A.*

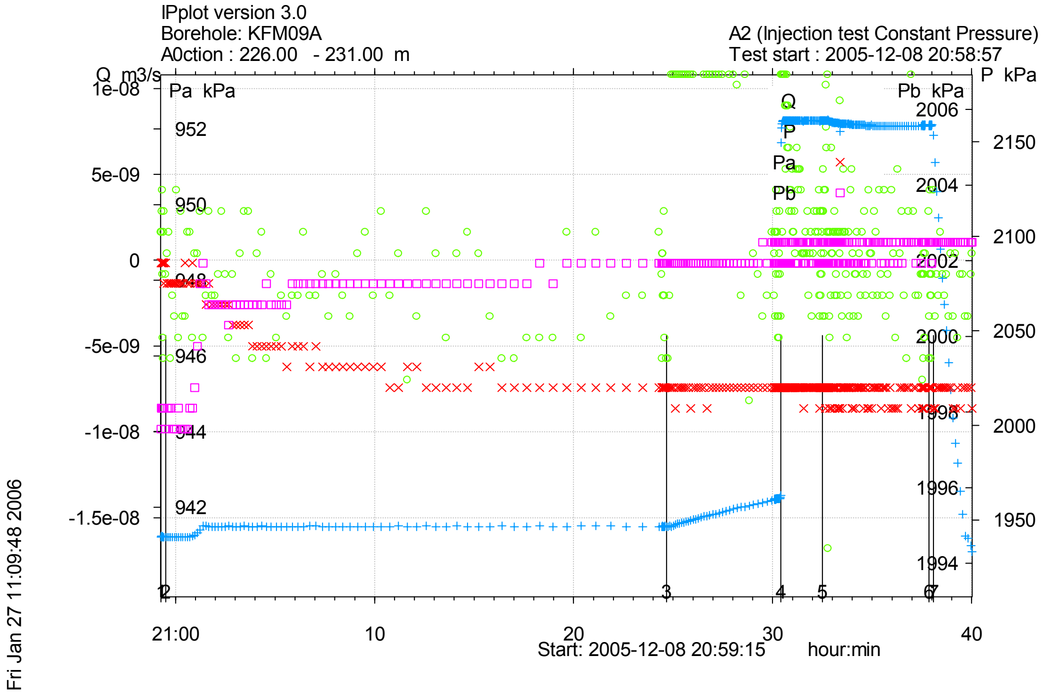


Figure A3-296. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 226.0-231.0 m in borehole KFM09A.*

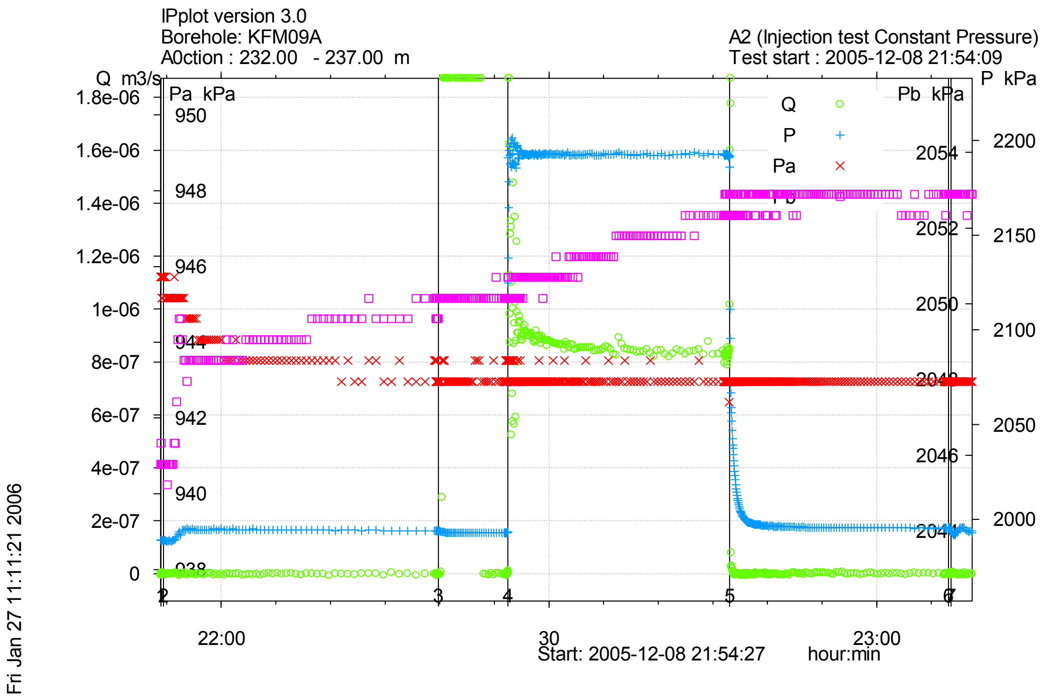


Figure A3-297. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 232.0-237.0 m in borehole KFM09A.*

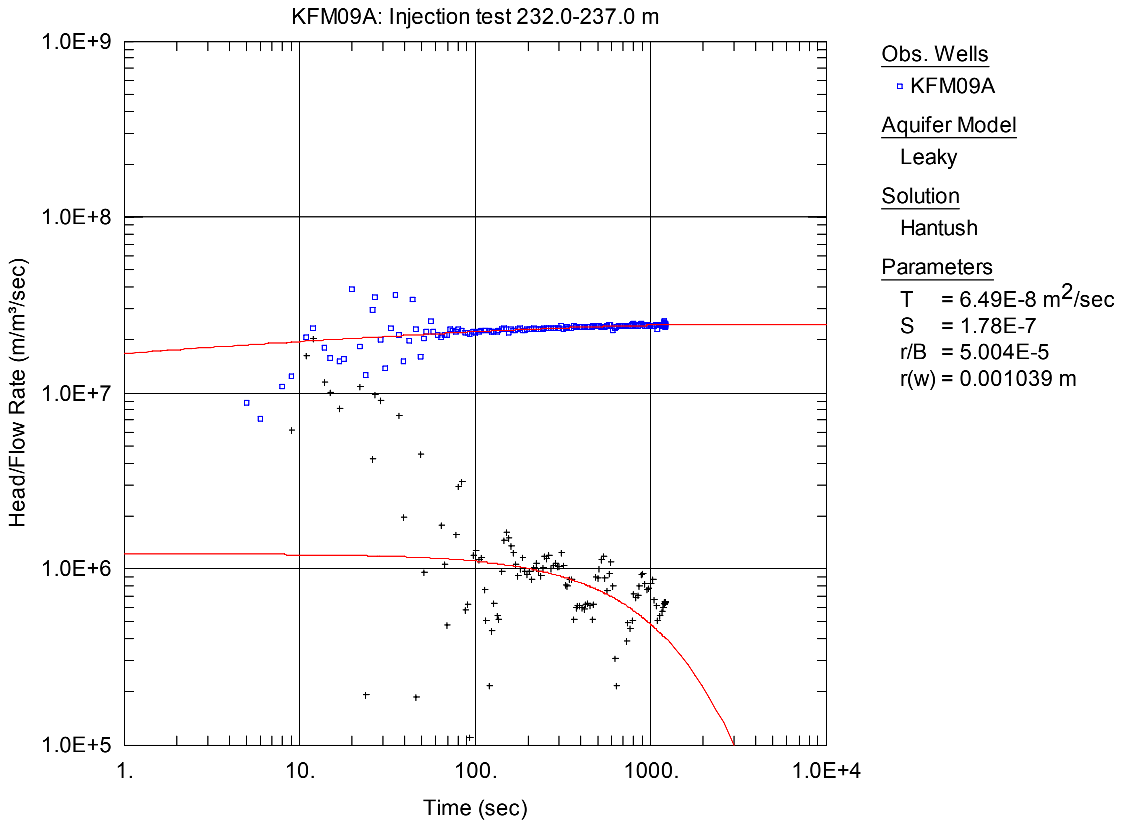


***Figure A3-298.** Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 232.0-237.0 m in KFM09A.*

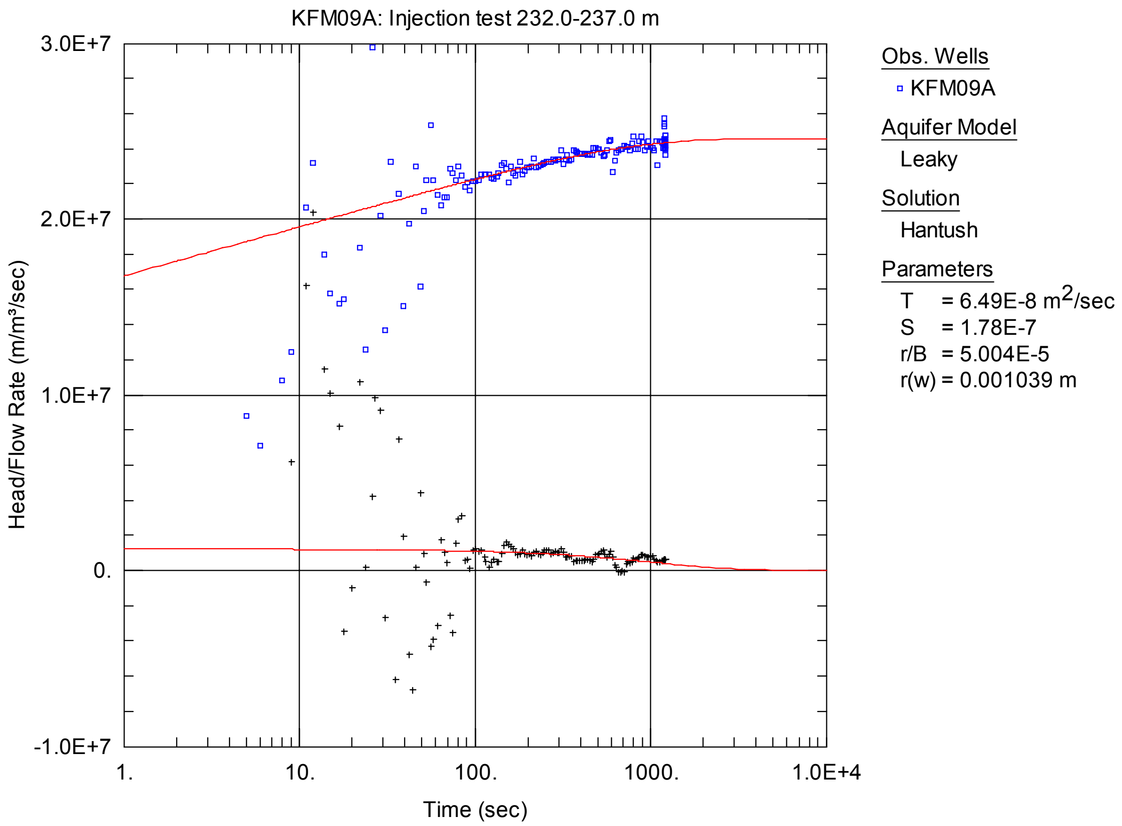


***Figure A3-299.** Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 232.0-237.0 m in KFM09A.*

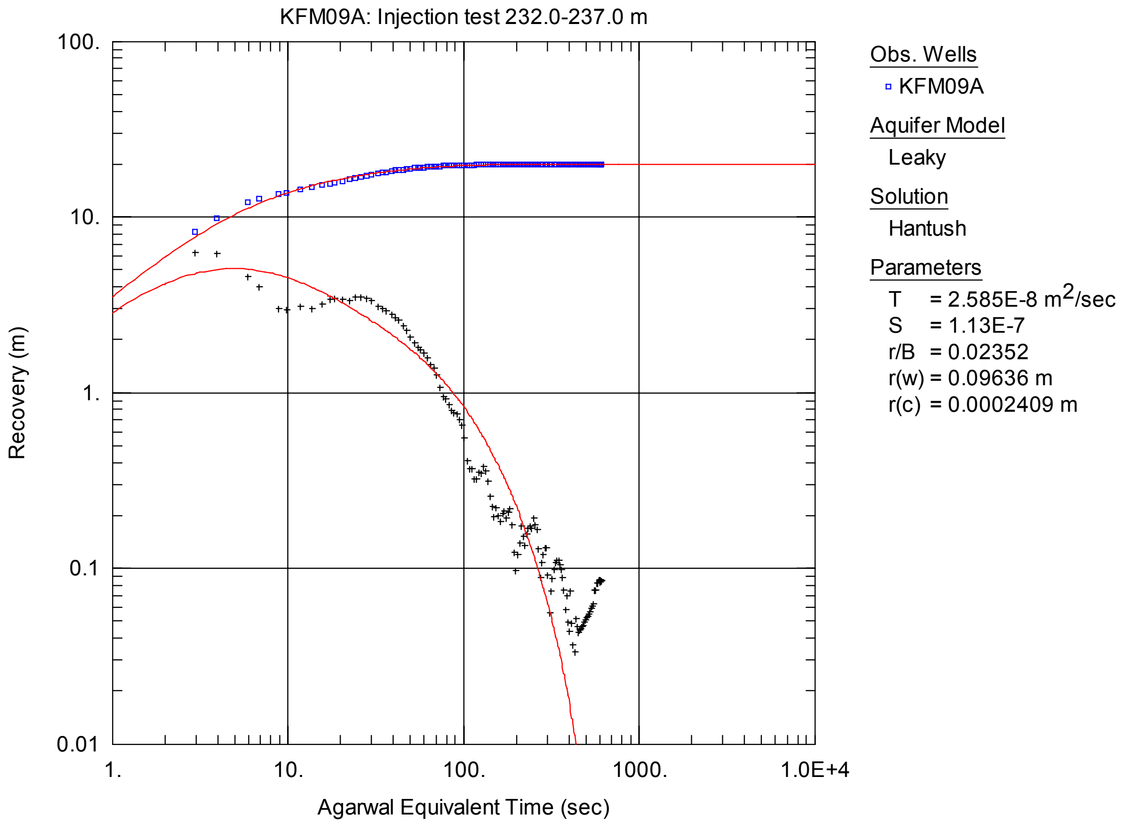


Figure A3-300. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 232.0-237.0 m in KFM09A.*

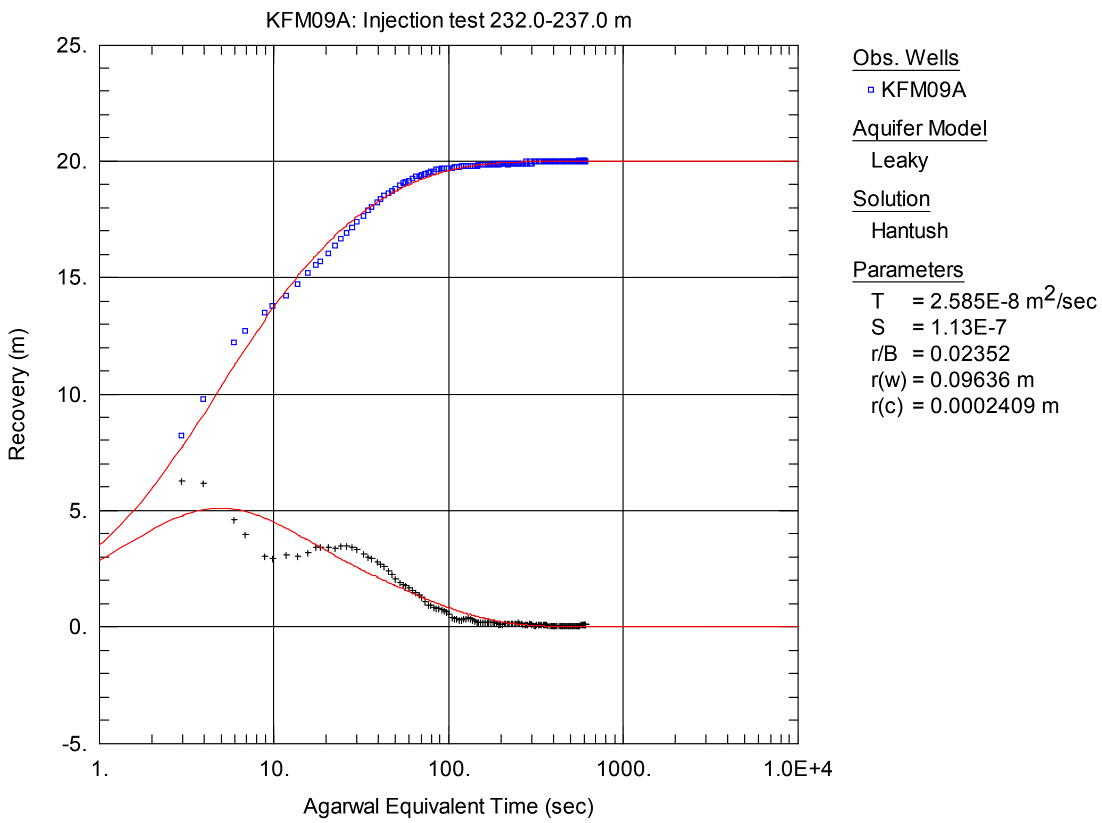


Figure A3-301. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 232.0-237.0 m in KFM09A.*

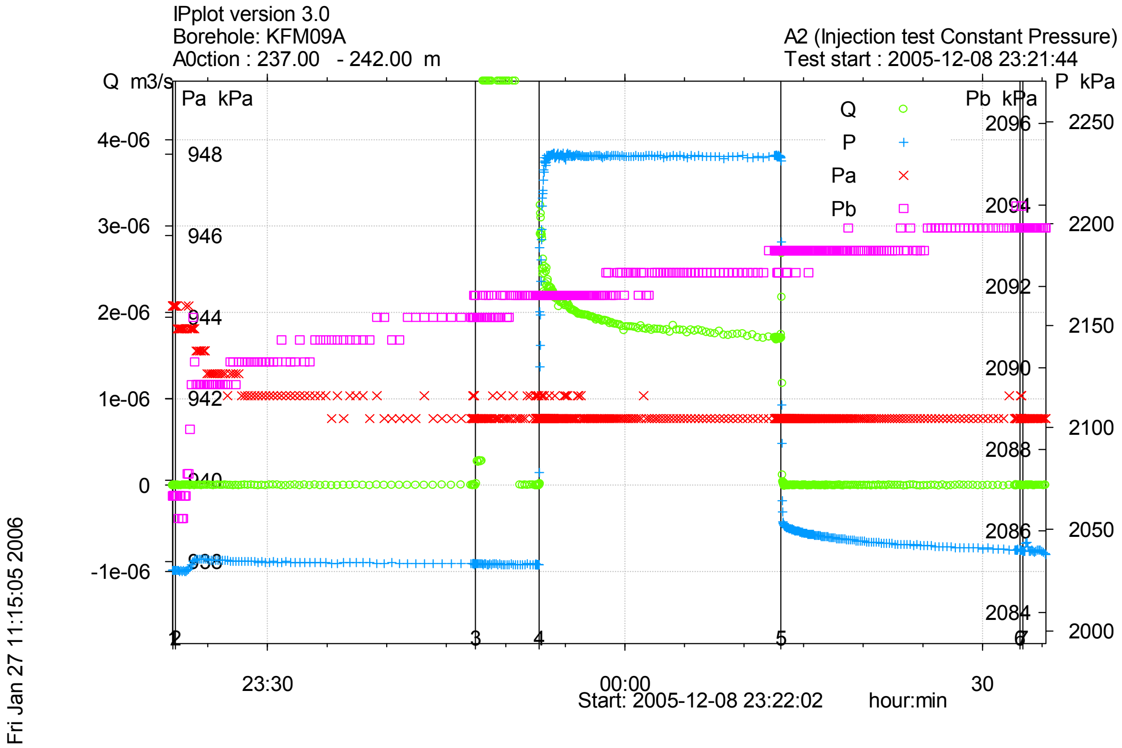


Figure A3-302. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 237.0-242.0 m in borehole KFM09A.

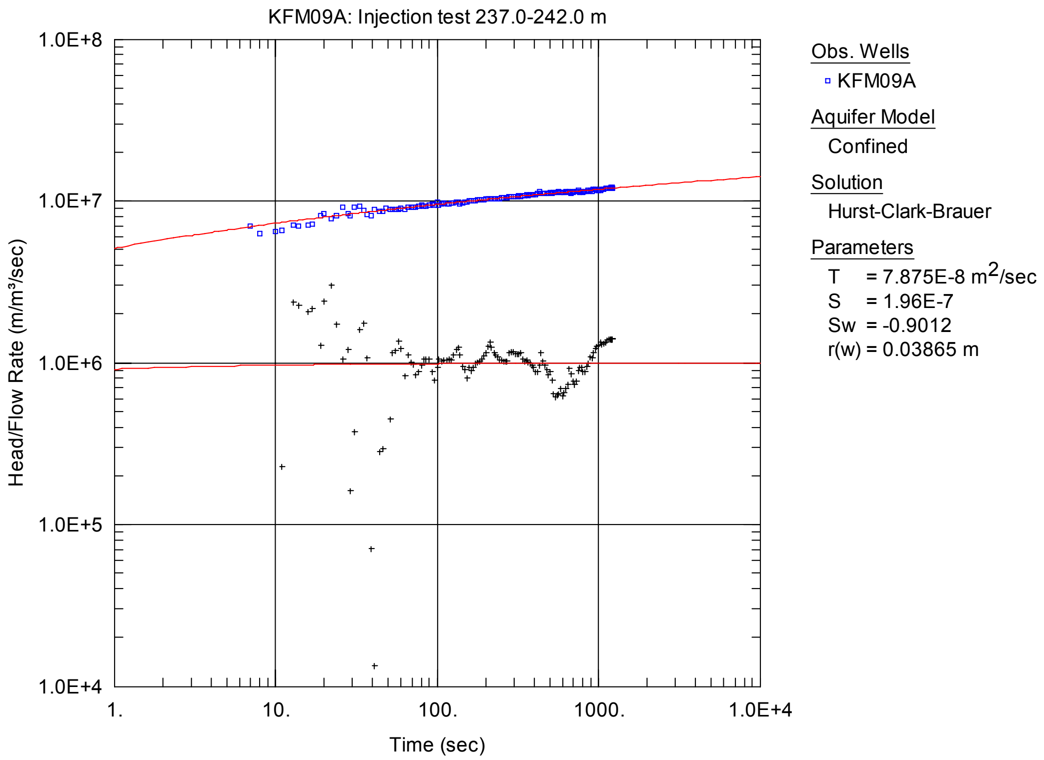


Figure A3-303. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 237.0-242.0 m in KFM09A.

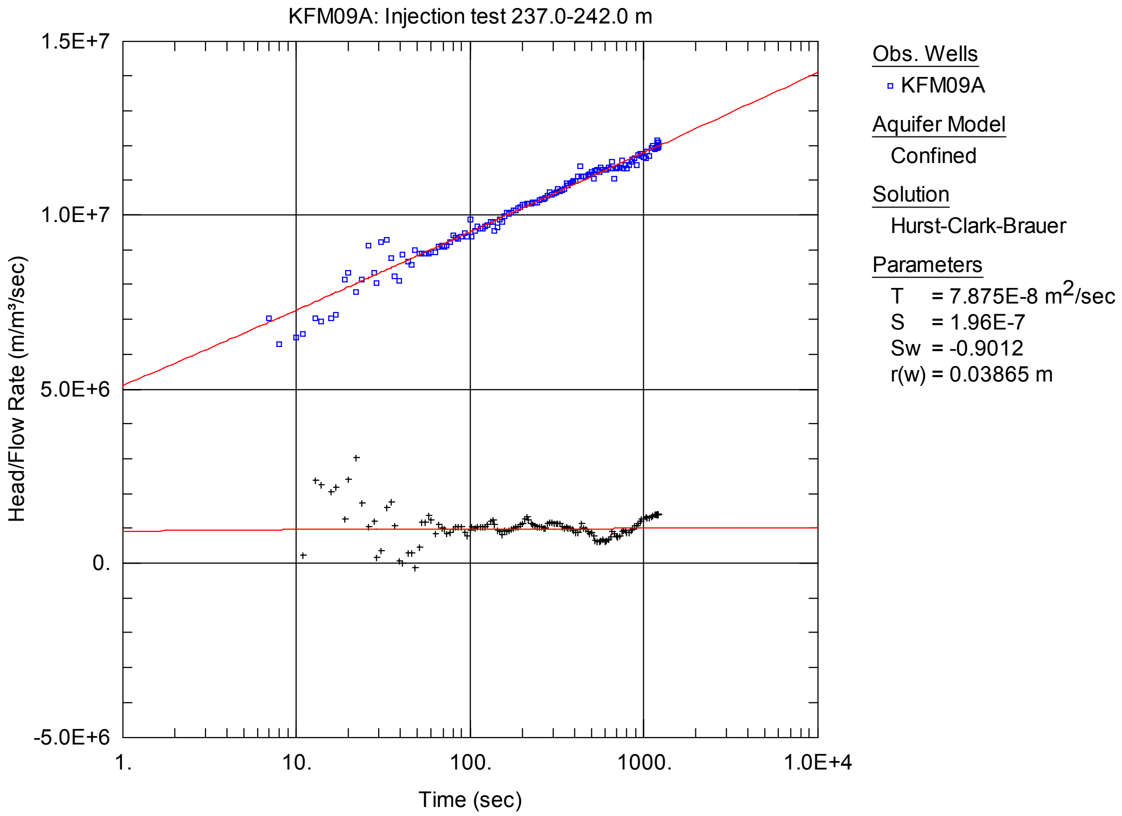


Figure A3-304. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 237.0-242.0 m in KFM09A.*

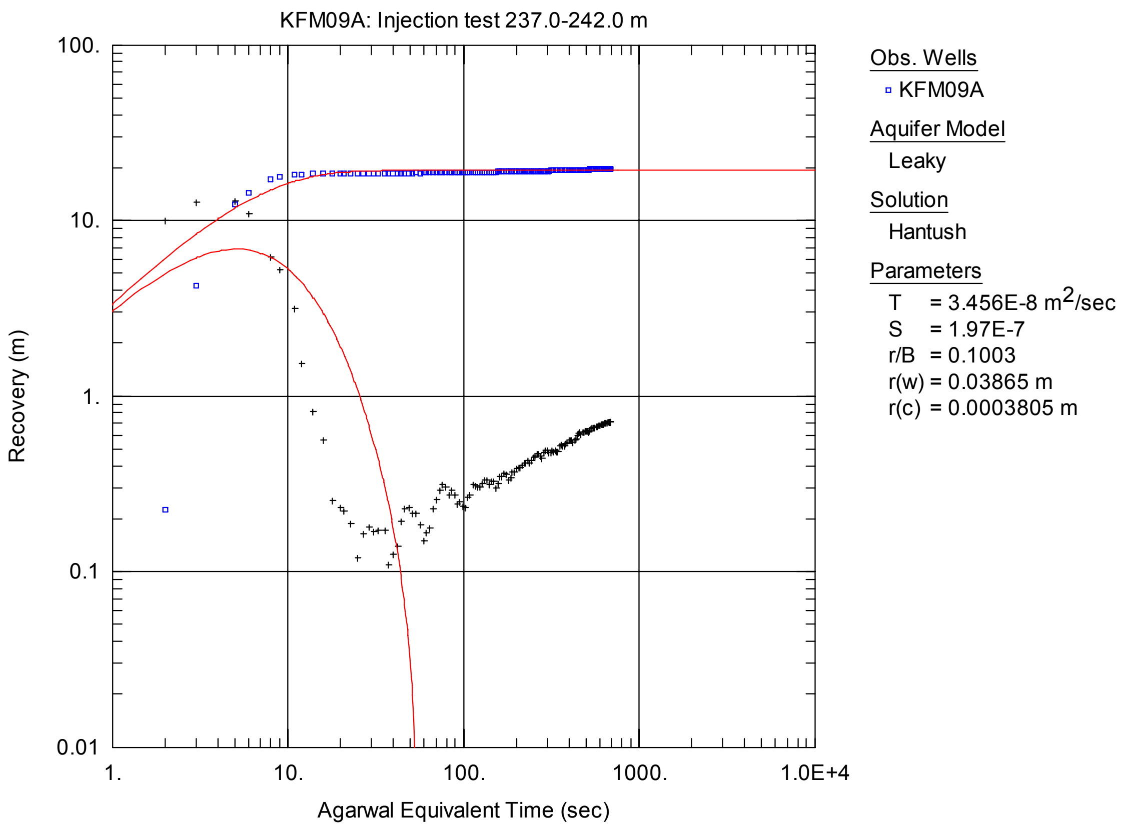


Figure A3-305. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 237.0-242.0 m in KFM09A.*

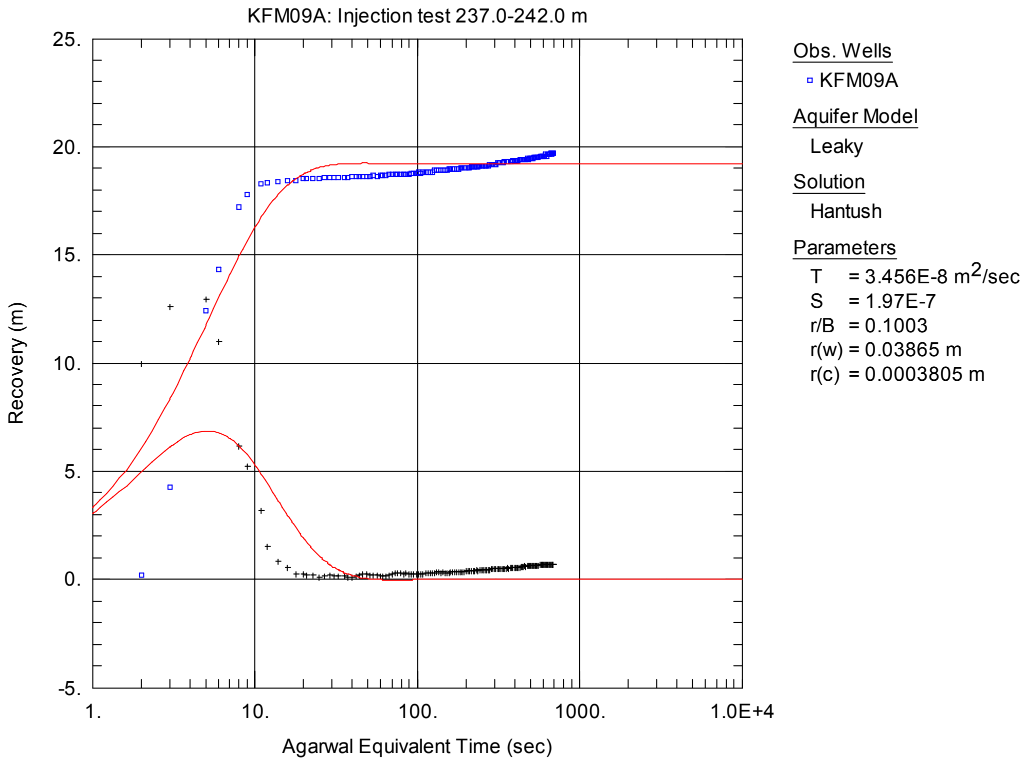


Figure A3-306. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 237.0-242.0 m in KFM09A.*

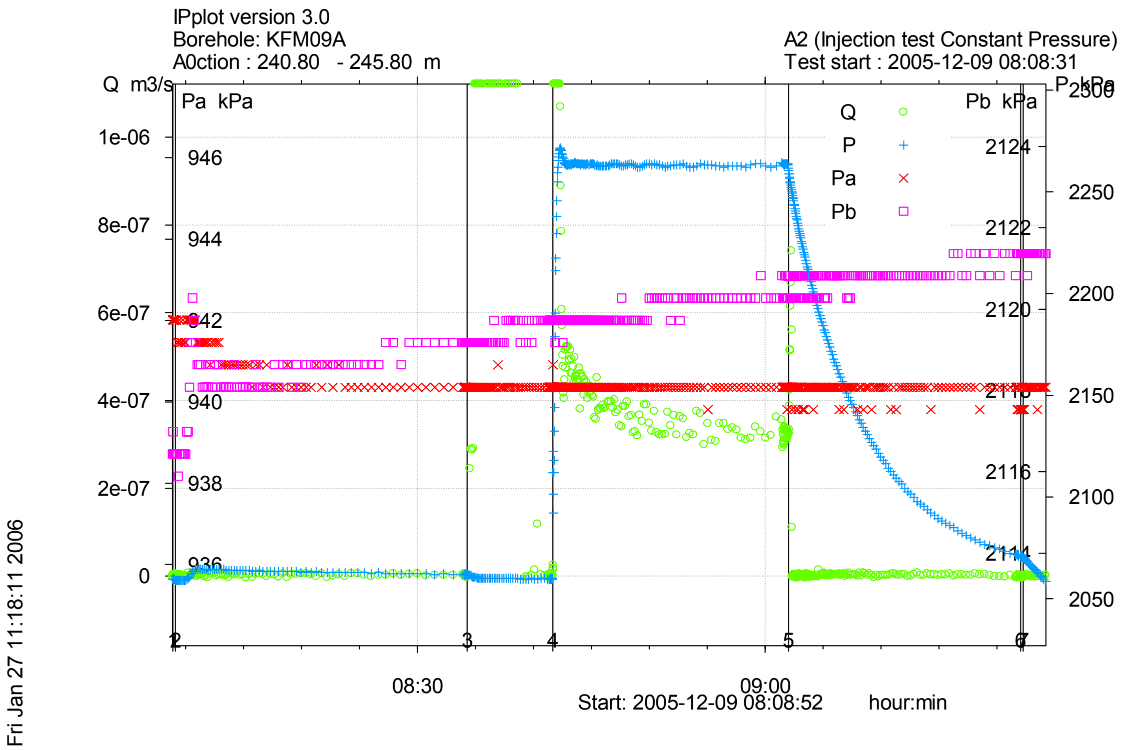


Figure A3-307. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 240.80-245.80 m in borehole KFM09A.*

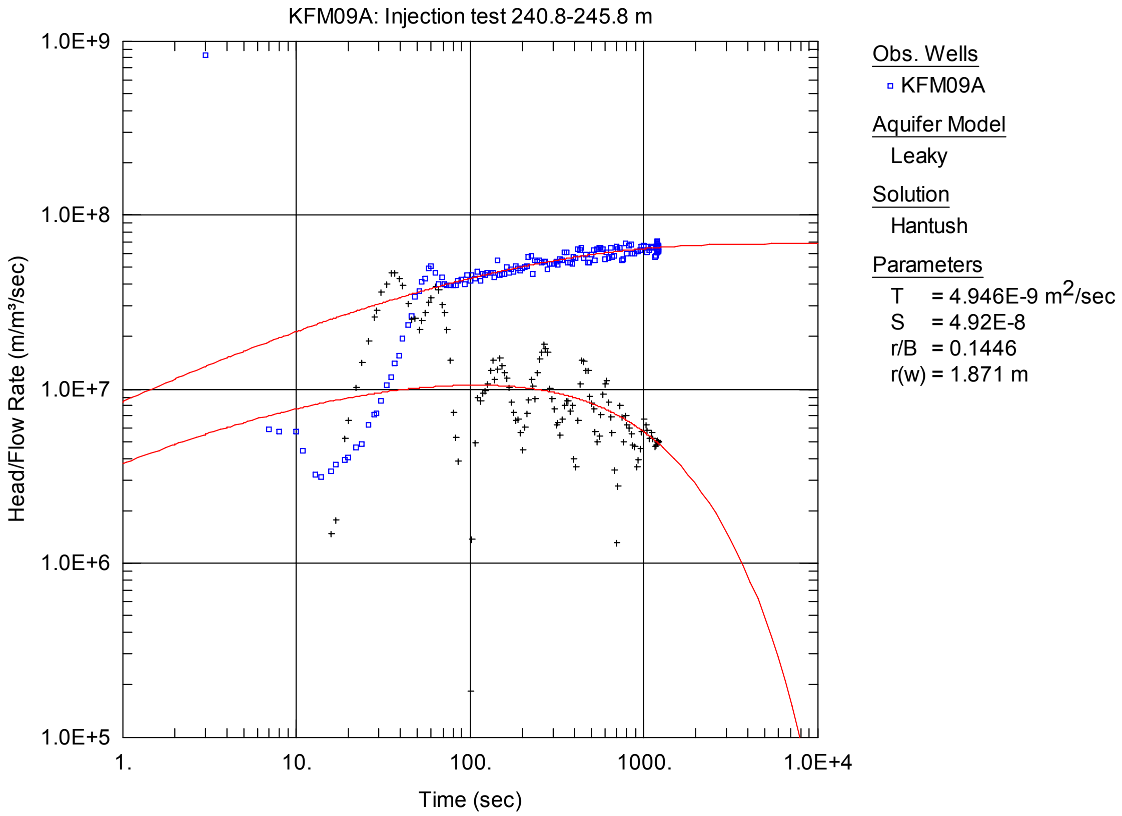


Figure A3-308. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 240.80-245.80 m in KFM09A.*

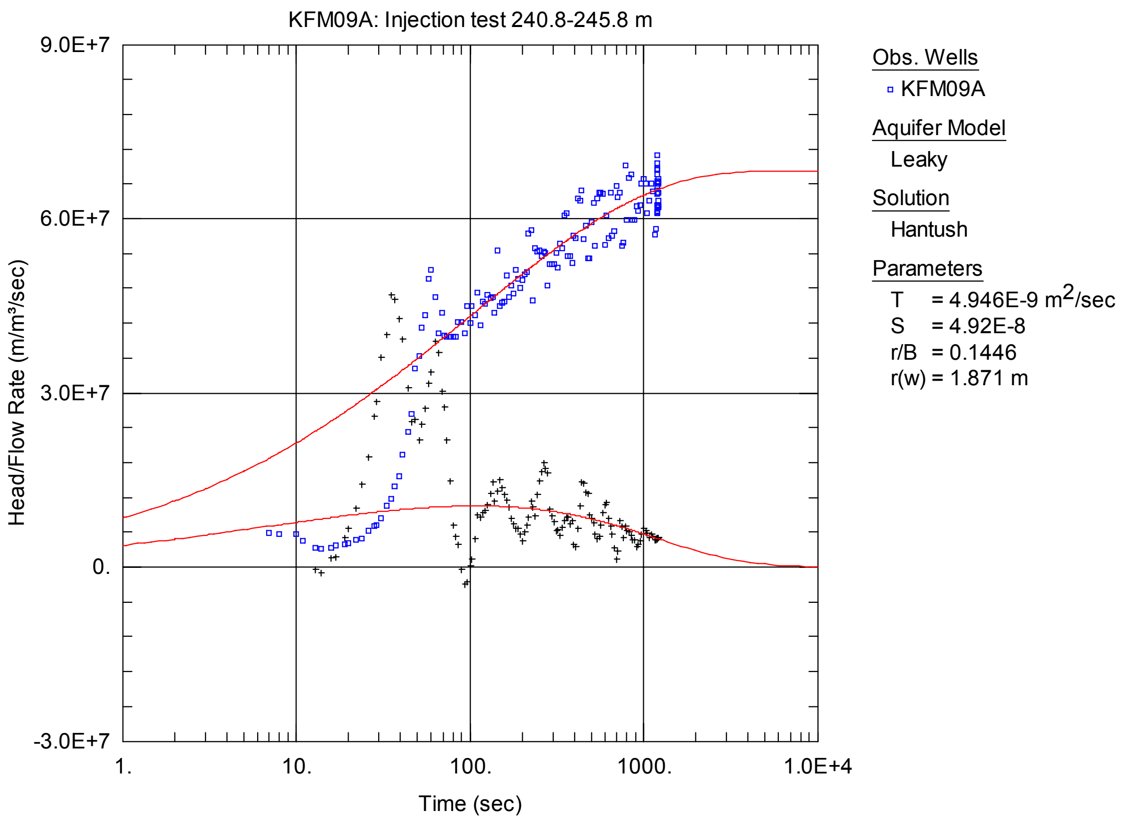


Figure A3-309. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 240.80-245.80 m in KFM09A.*

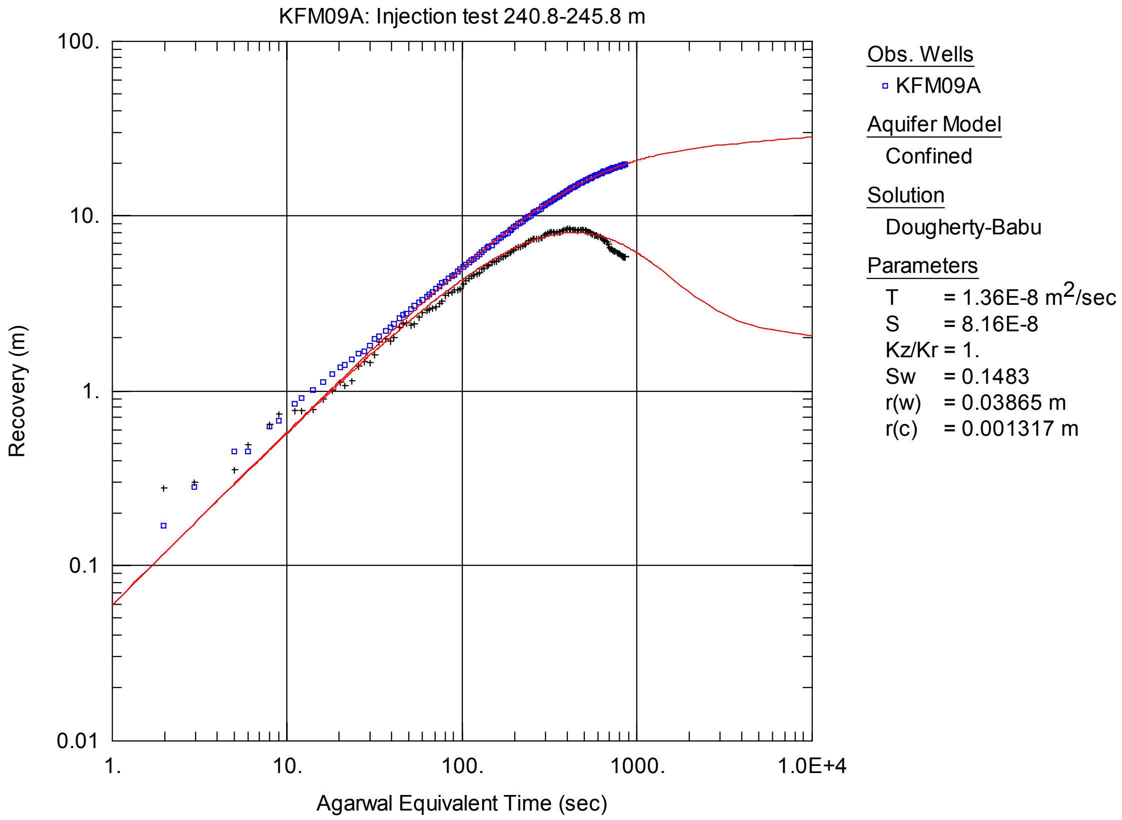


Figure A3-310. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 240.80-245.80 m in KFM09A.*

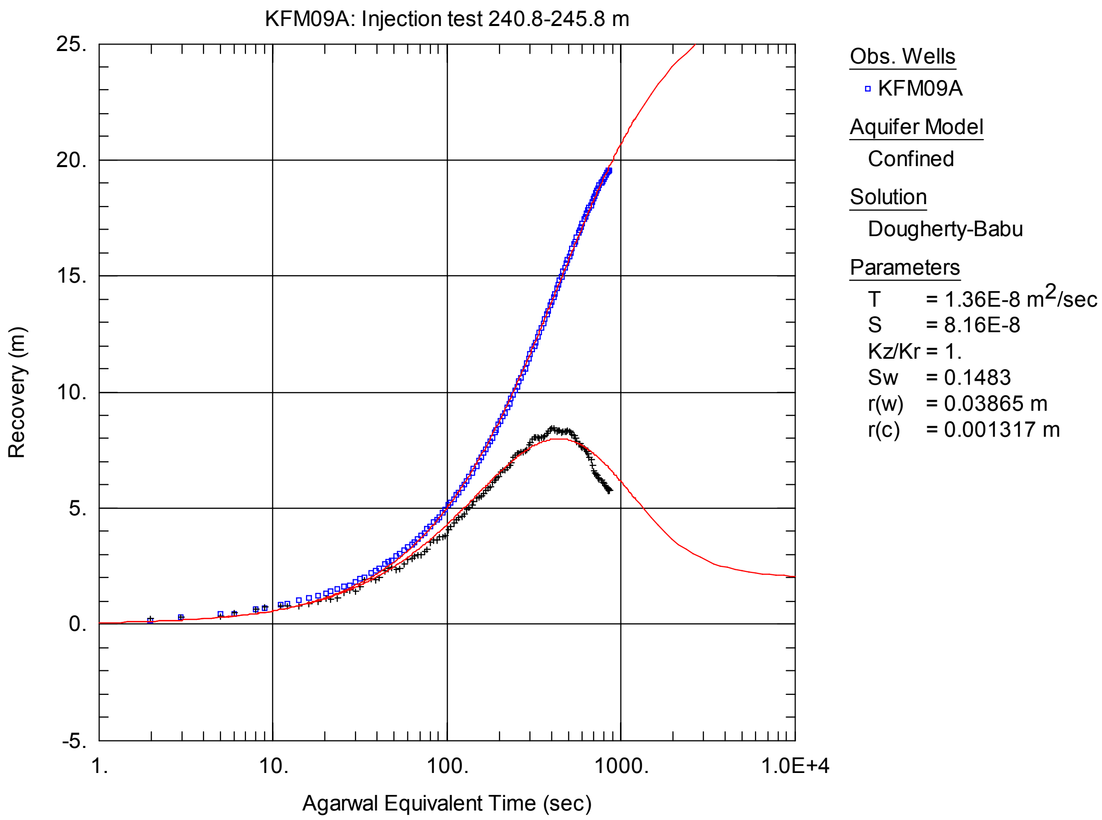


Figure A3-311. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 240.80-245.80 m in KFM09A.*

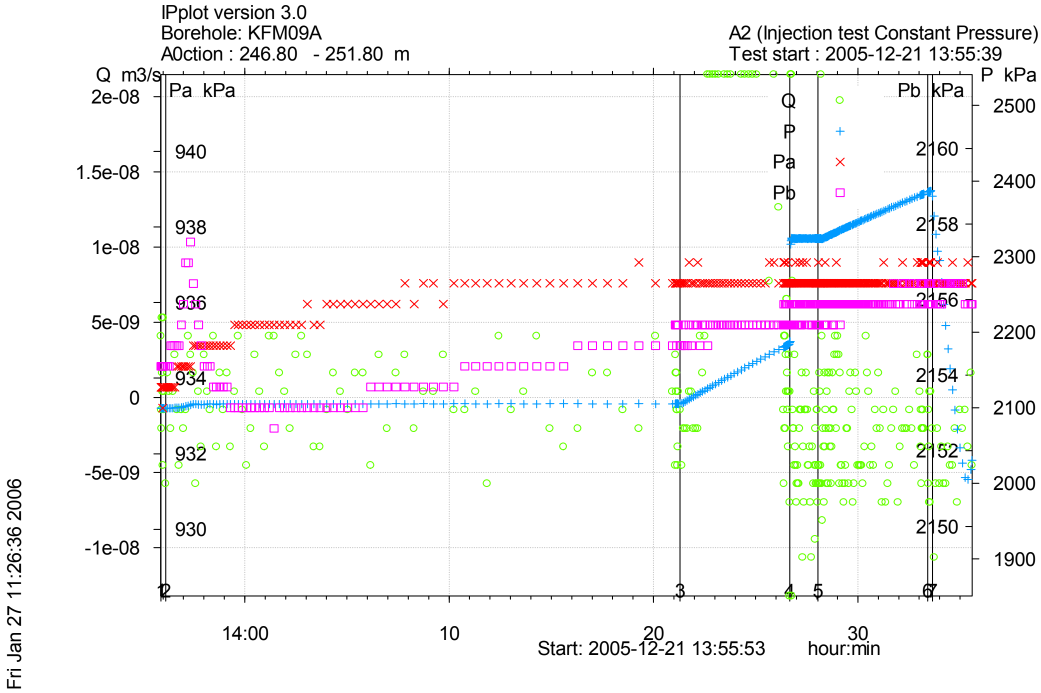


Figure A3-312. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 246.80-251.80 m in borehole KFM09A.*

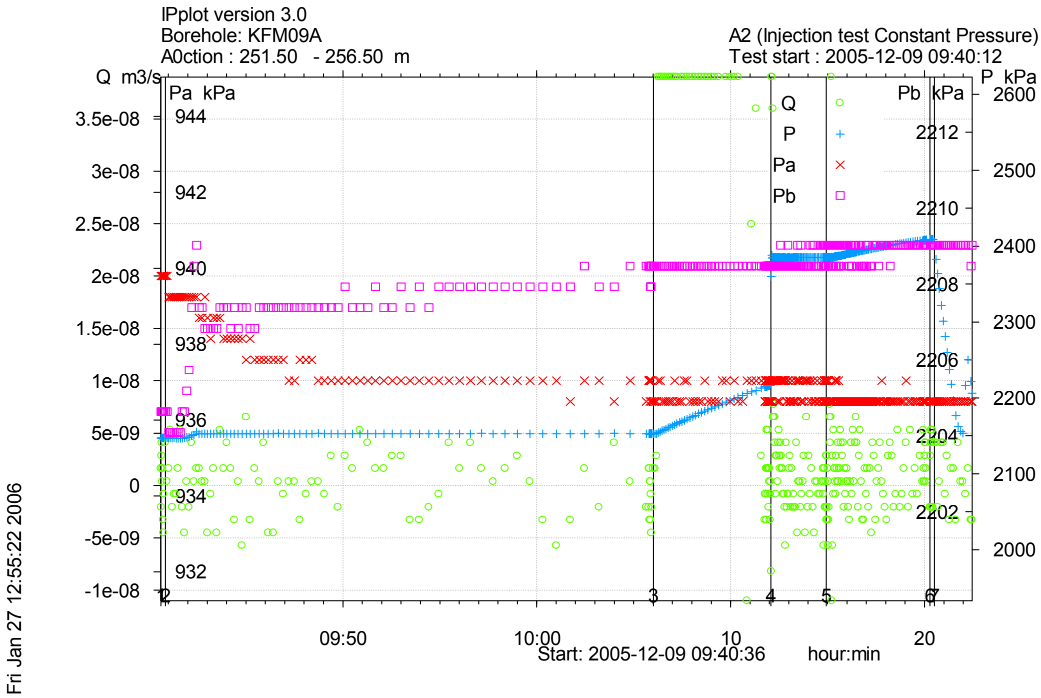


Figure A3-313. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 251.50-256.50 m in borehole KFM09A.*

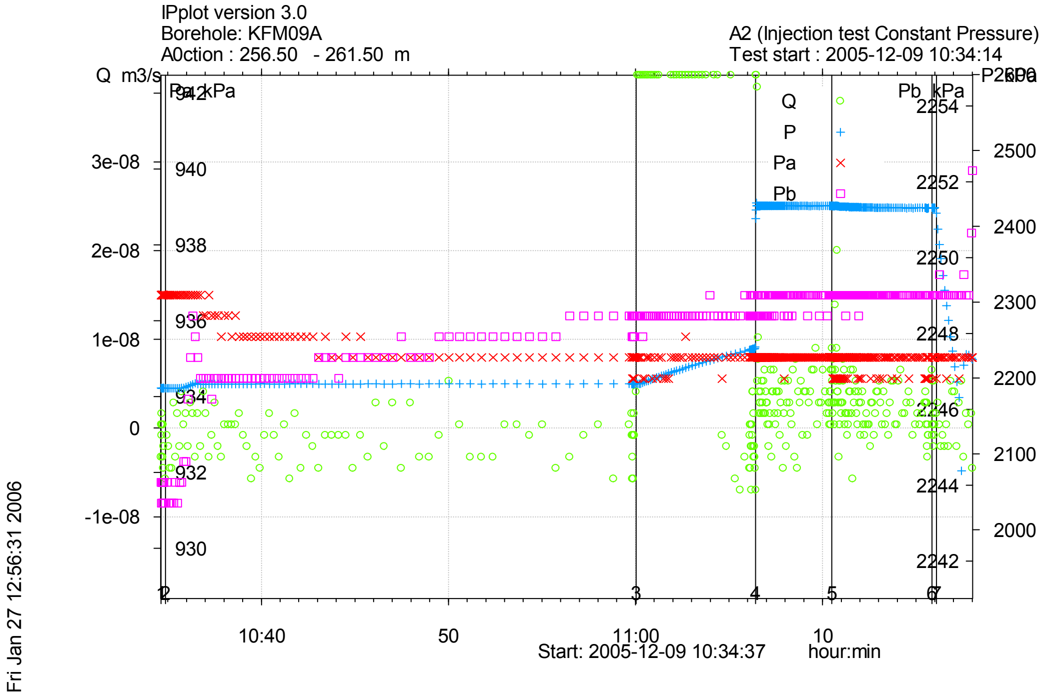


***Figure A3-314.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 256.50-261.50 m in borehole KFM09A.*

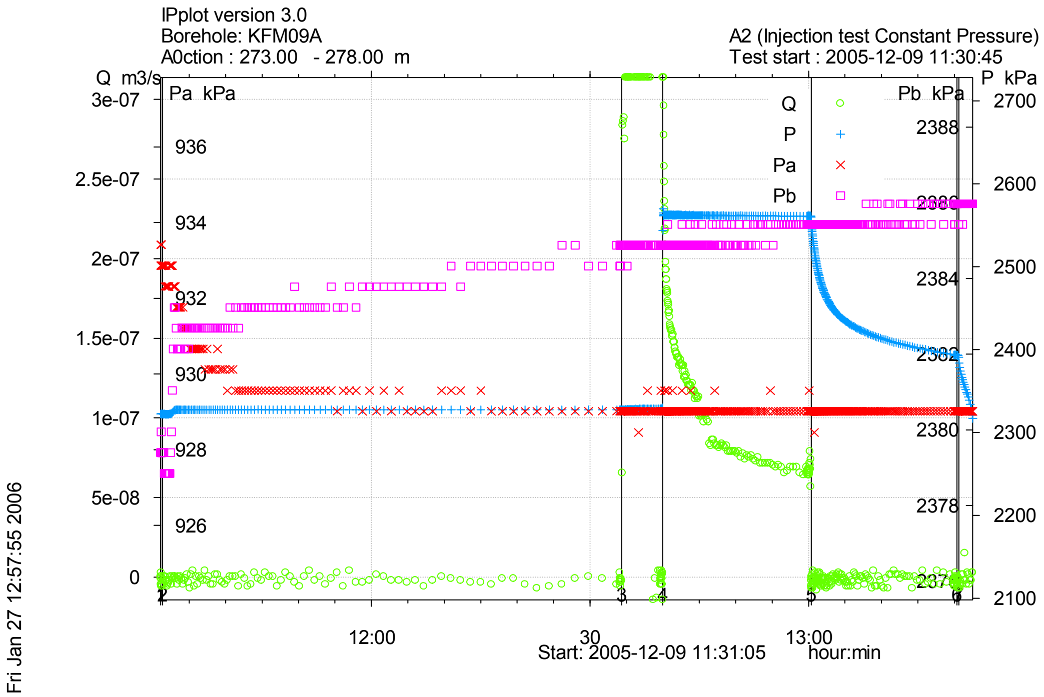


***Figure A3-315.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 273.0-278.0 m in borehole KFM09A.*

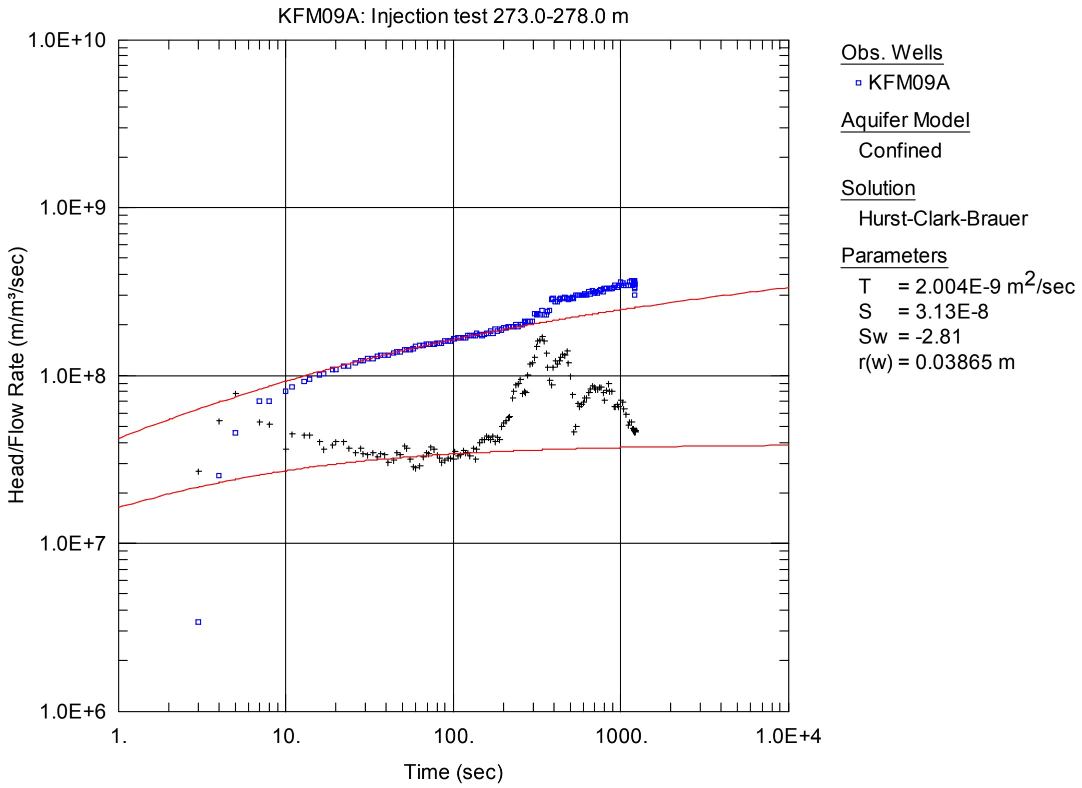


Figure A3-316. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 273.0-278.0 m in KFM09A. This plot shows a fit to the first of two different PRF:s during the injection period in this section.*

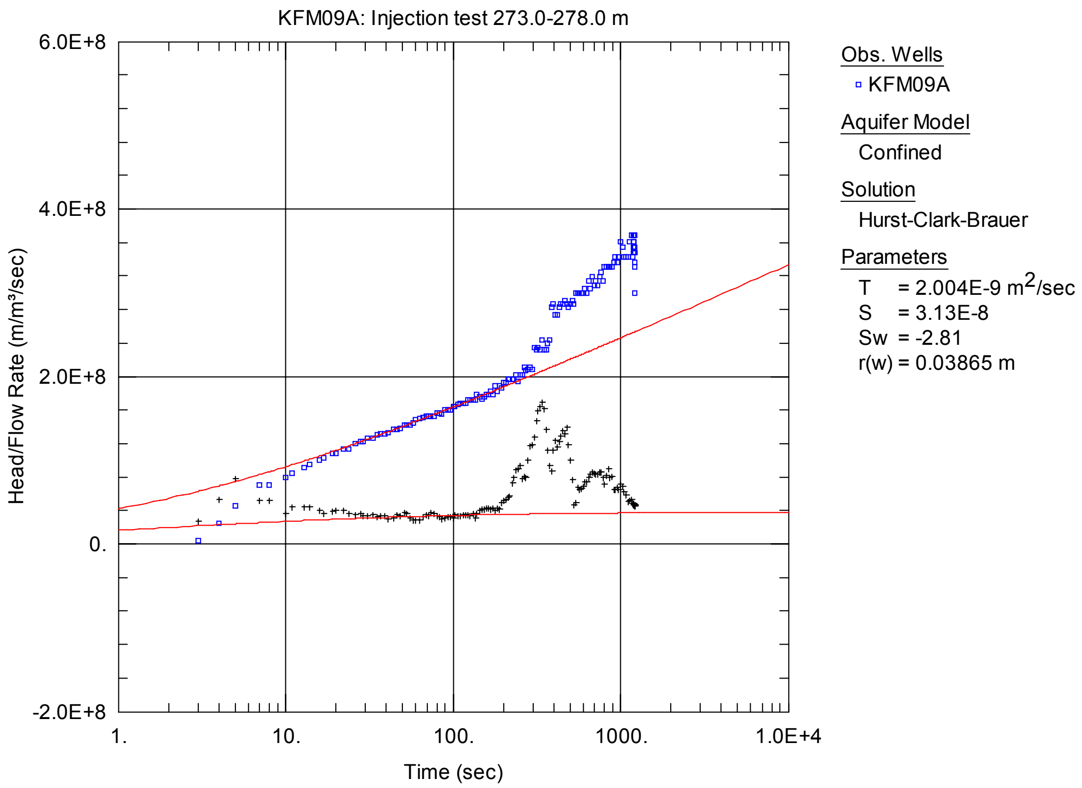


Figure A3-317. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 273.0-278.0 m in KFM09A. This plot shows a fit to the first of two different PRF:s during the injection period in this section.*

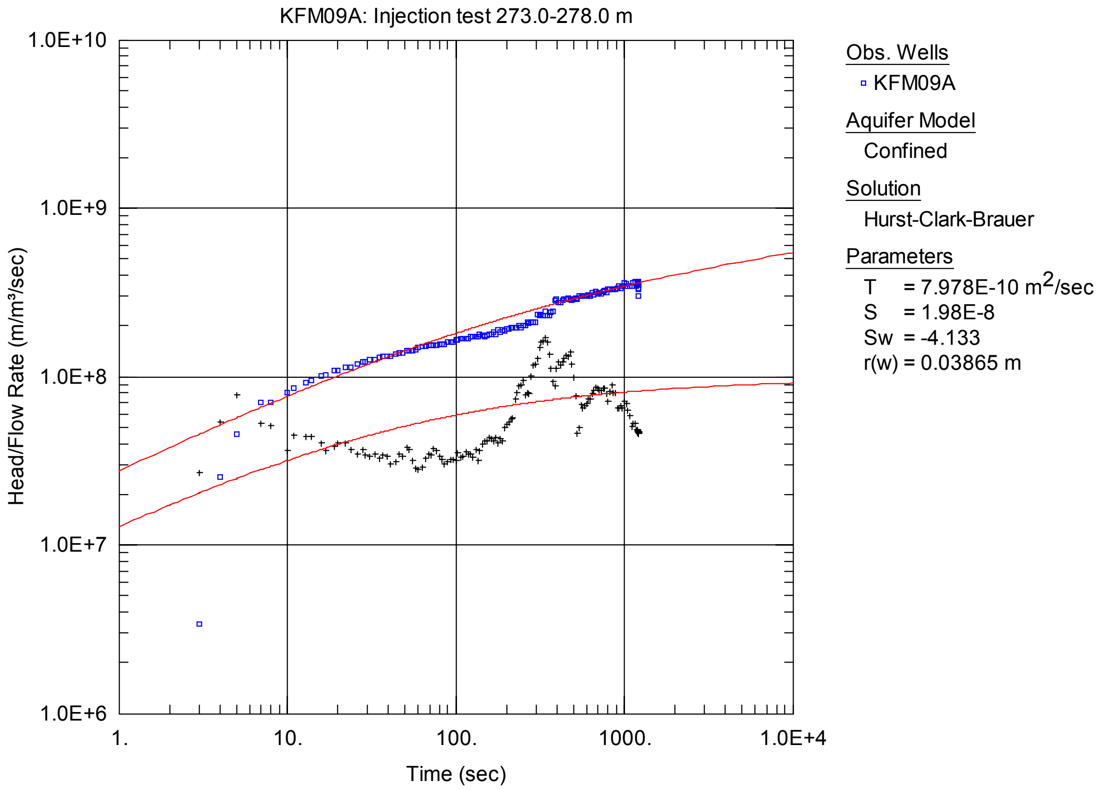


Figure A3-318. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 273.0-278.0 m in KFM09A. This plot shows a fit to the second of two different PRF:s during the injection period in this section.*

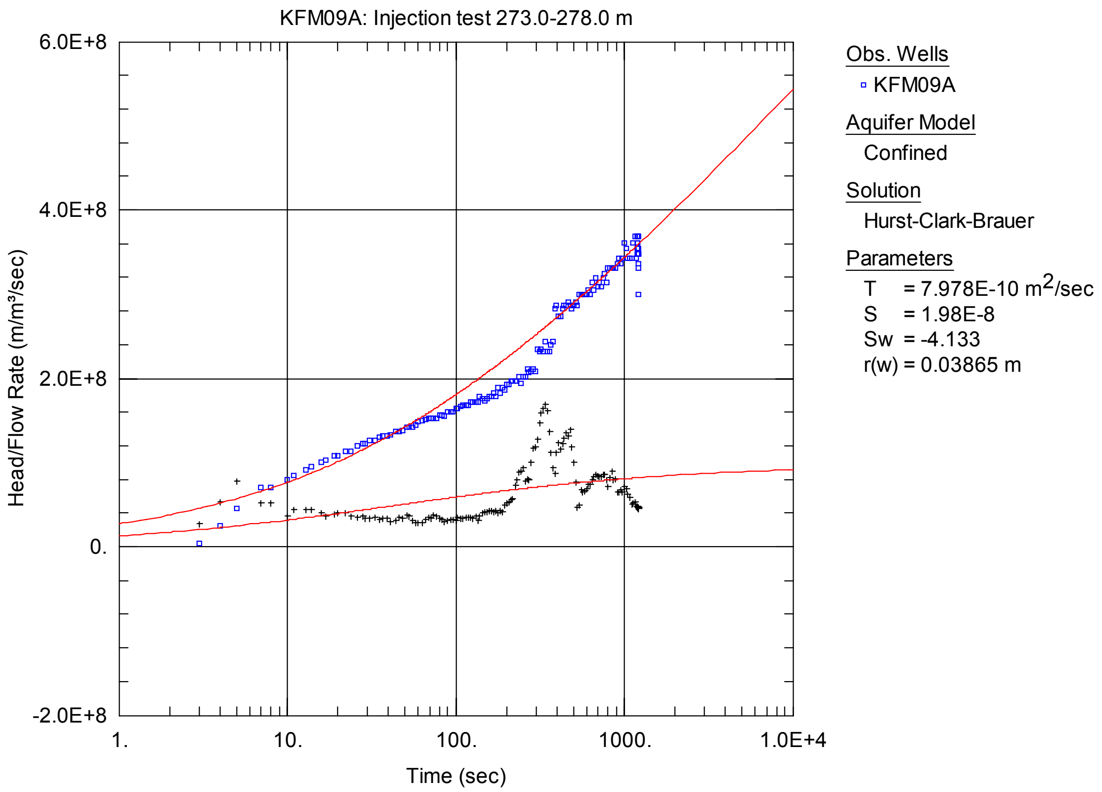


Figure A3-319. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 273.0-278.0 m in KFM09A. This plot shows a fit to the second of two different PRF:s during the injection period in this section.*

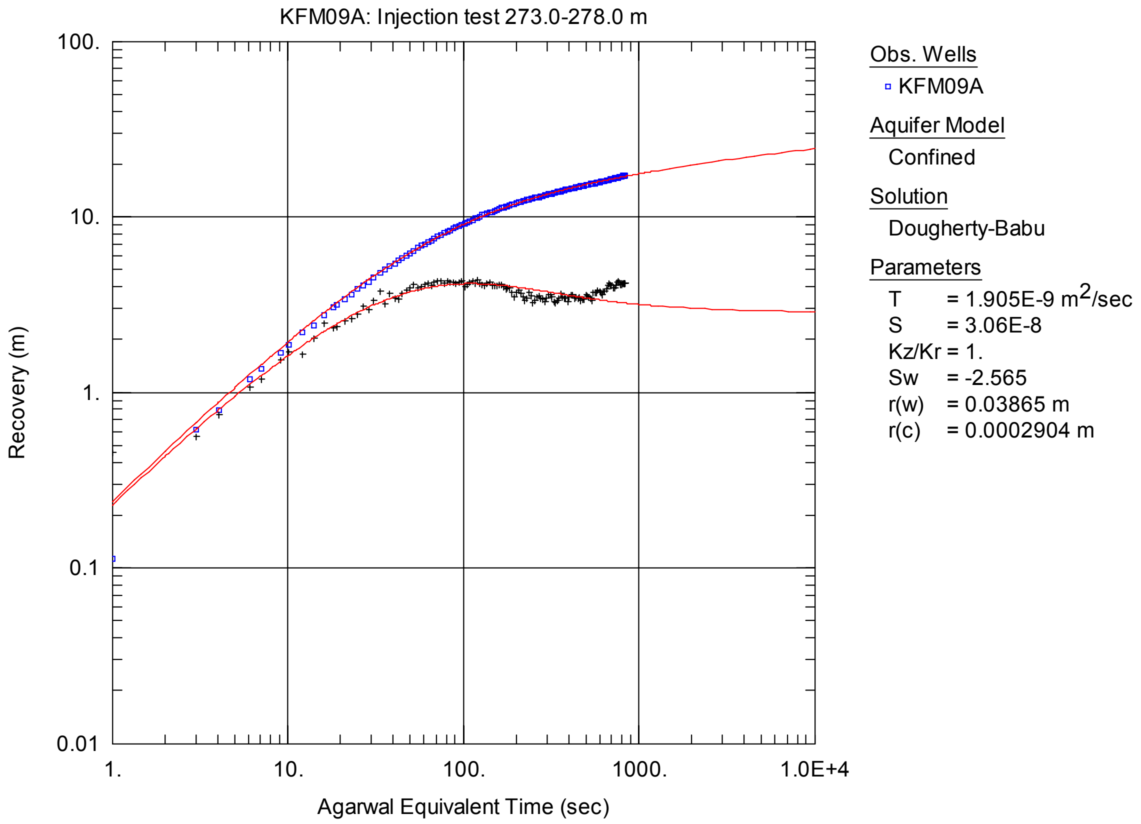


Figure A3-320. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 273.0-278.0 m in KFM09A.*

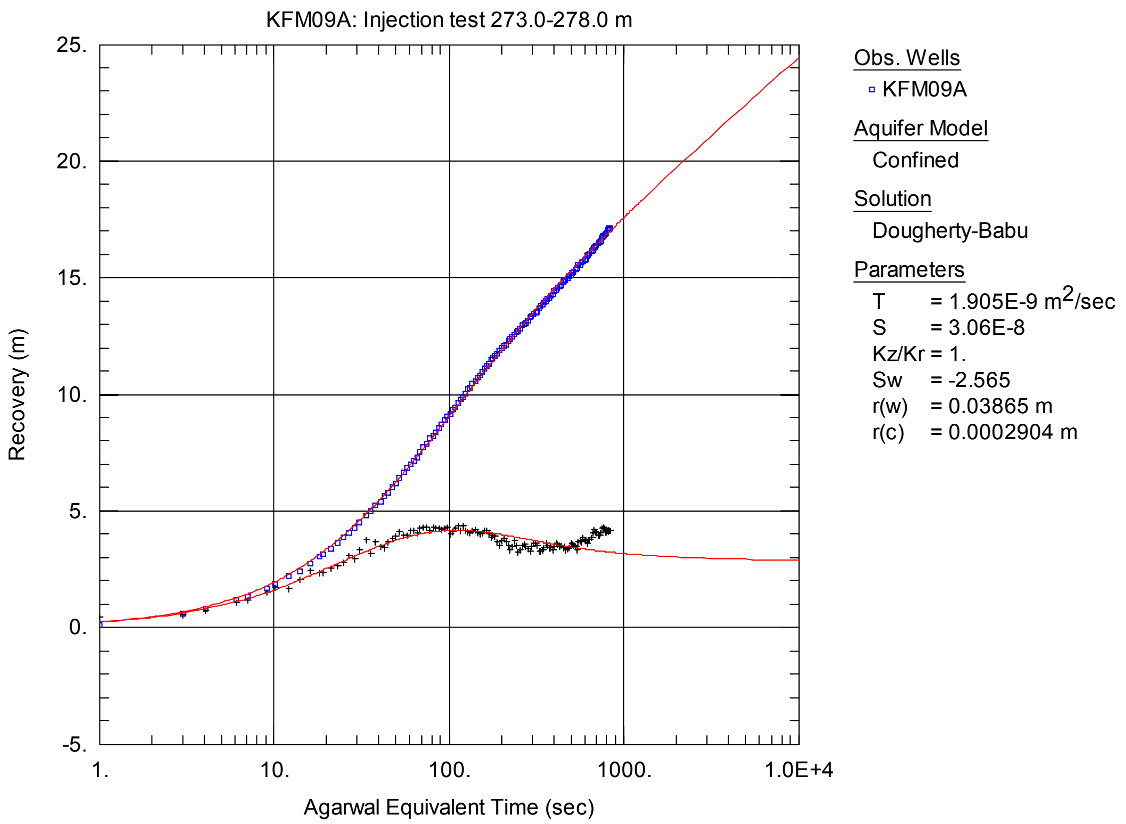


Figure A3-321. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 273.0-278.0 m in KFM09A.*

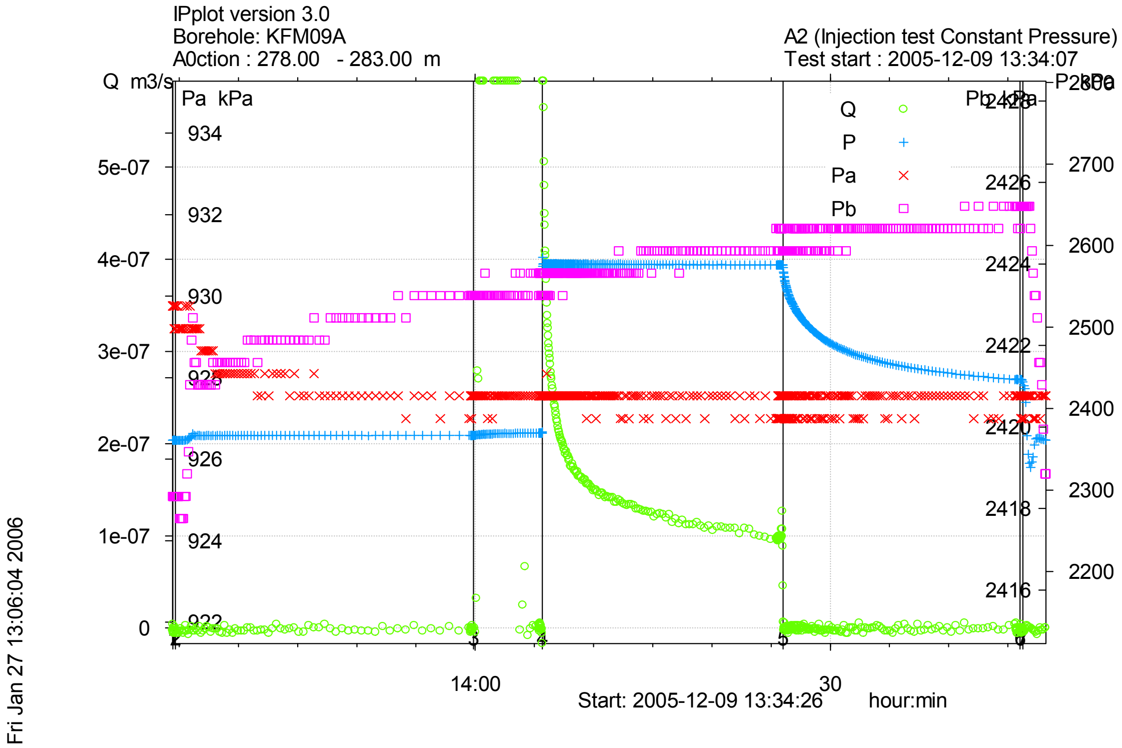


Figure A3-322. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in 278.0-283.0 m in borehole KFM09A.

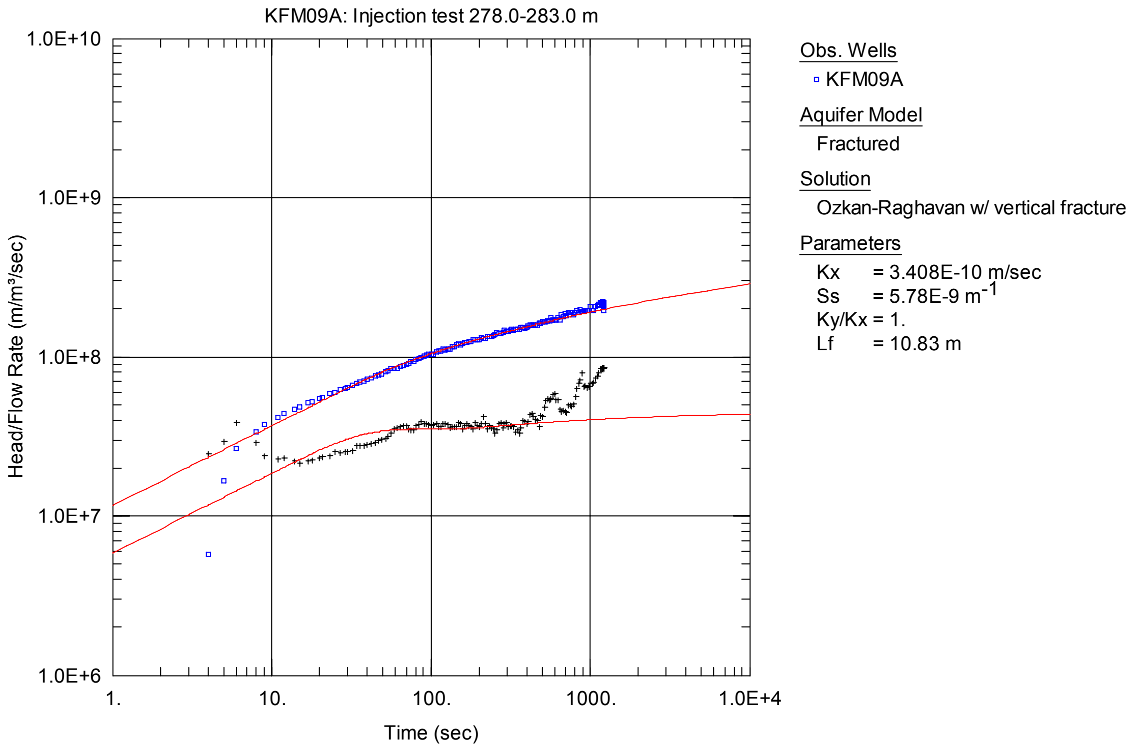


Figure A3-323. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 278.0-283.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.

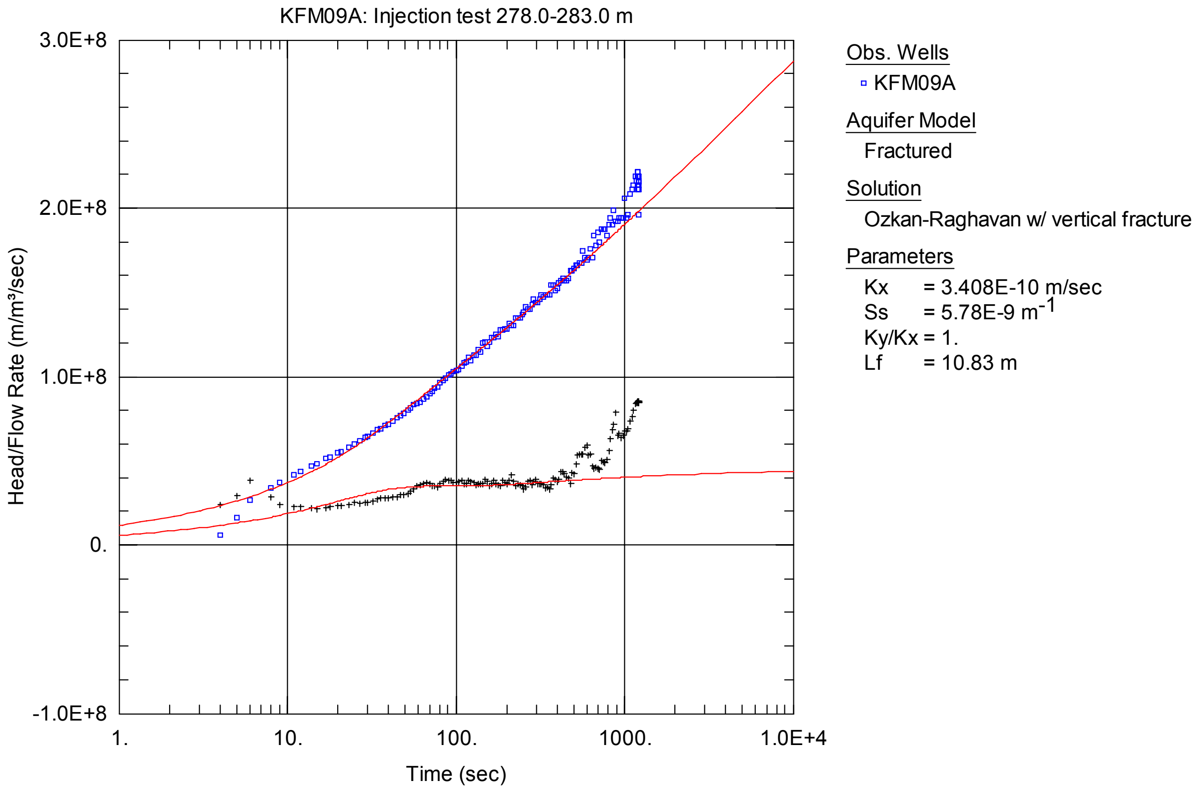


Figure A3-324. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 278.0-283.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

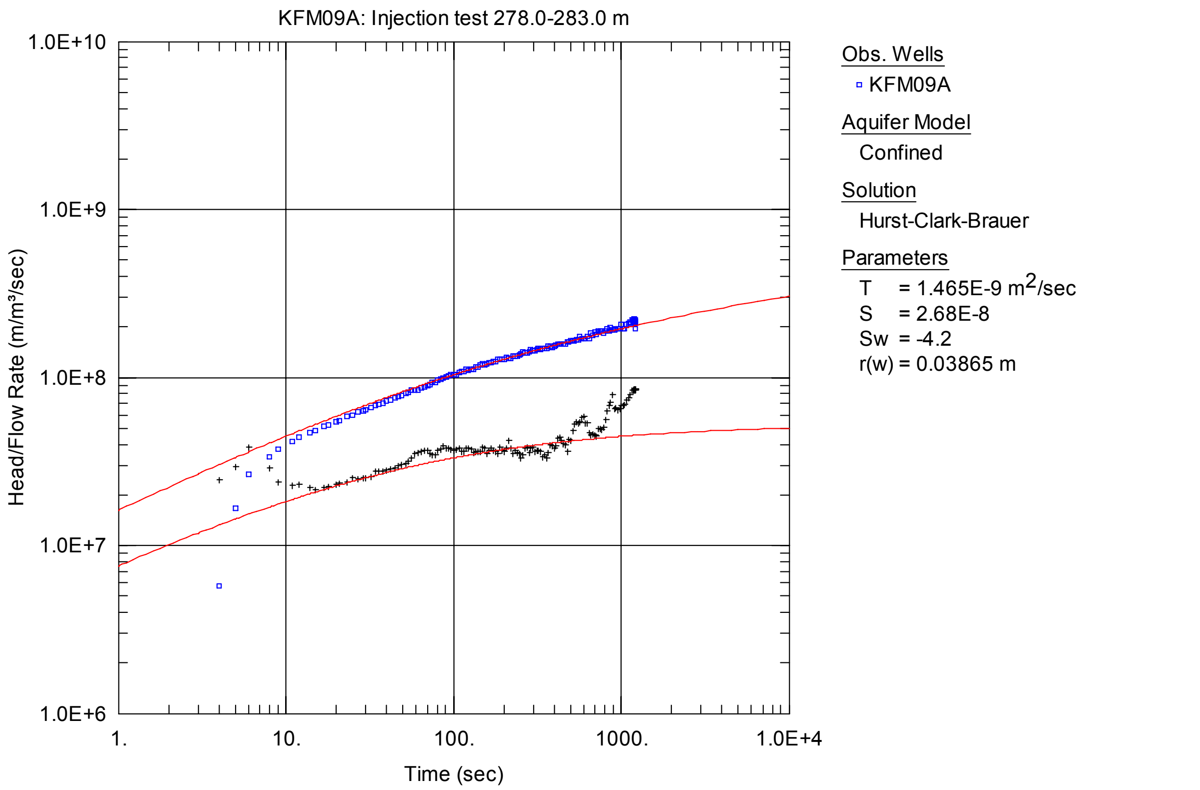


Figure A3-325. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 278.0-283.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for a pseudo-radial response.*

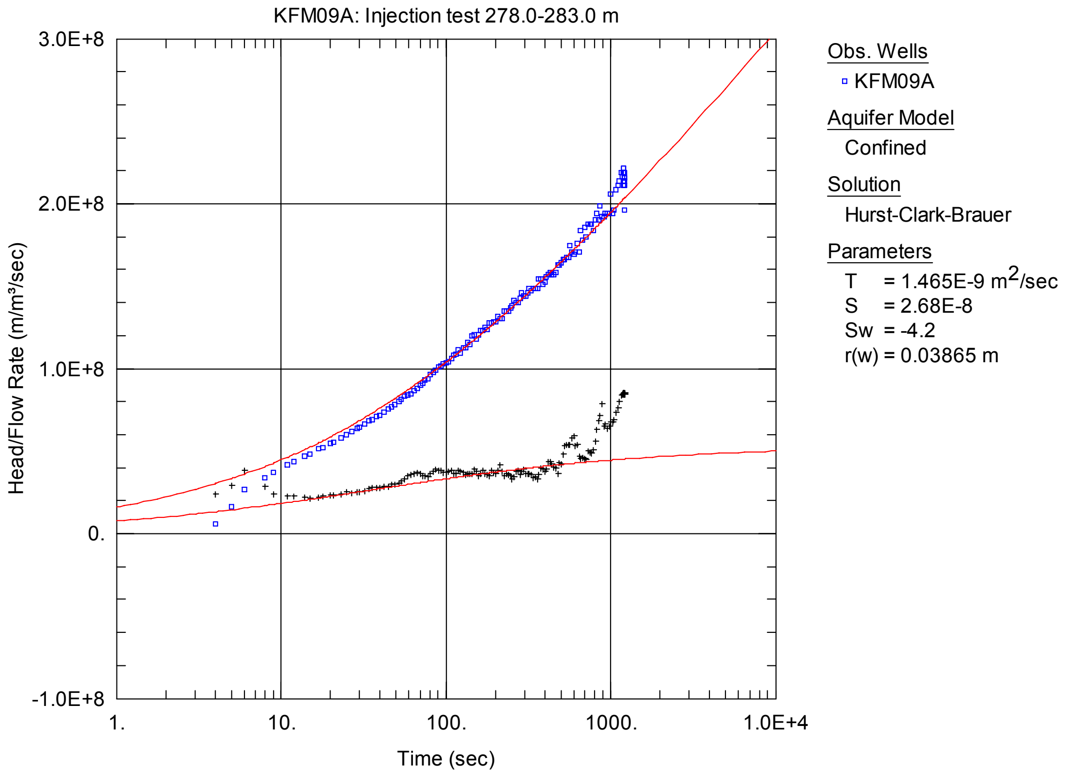


Figure A3-326. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 278.0-283.0 m in KFM09A This evaluation is made with the Hurst-Clark-Brauer model for a pseudo-radial response.*

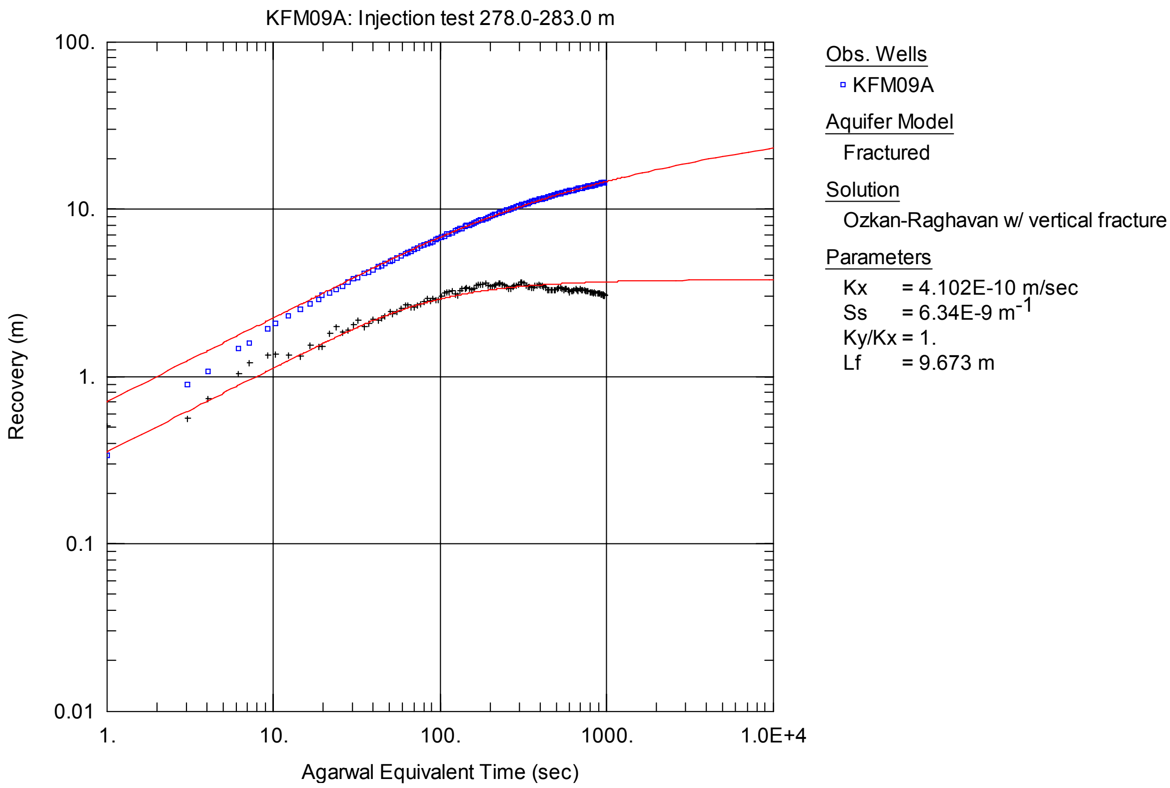


Figure A3-327. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 278.0-283.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

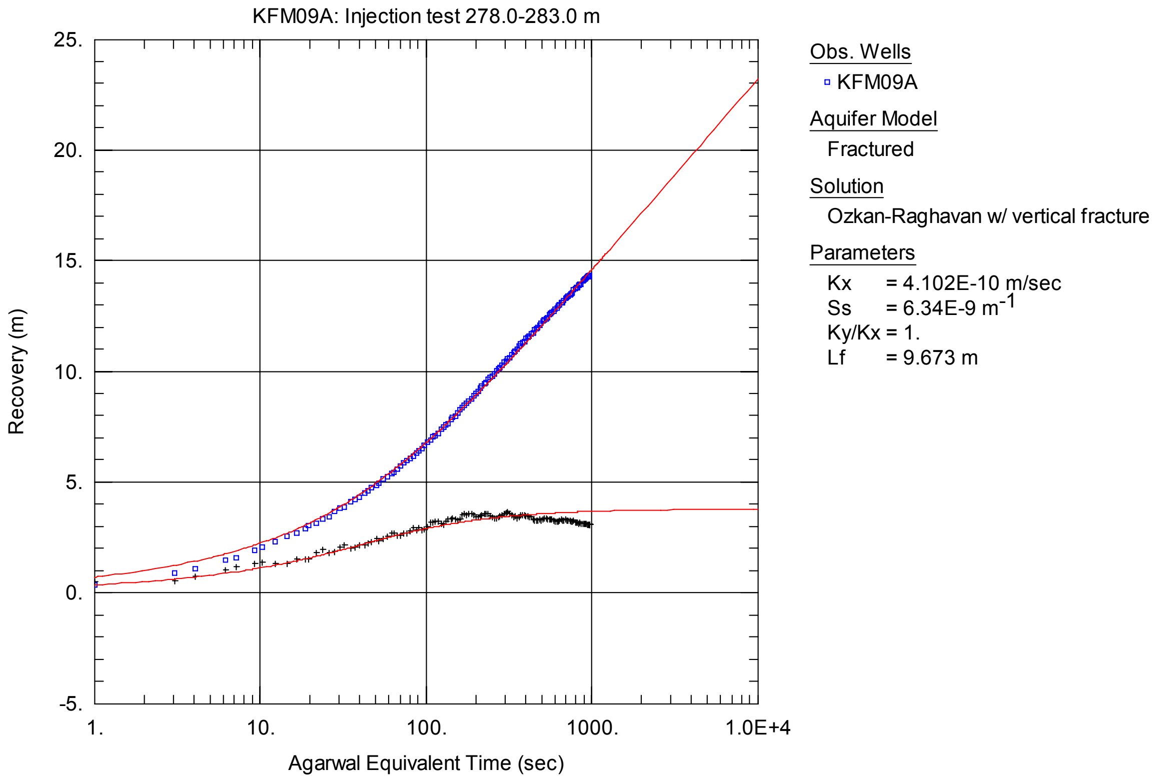


Figure A3-328. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 278.0-283.0 m in KFM09A This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

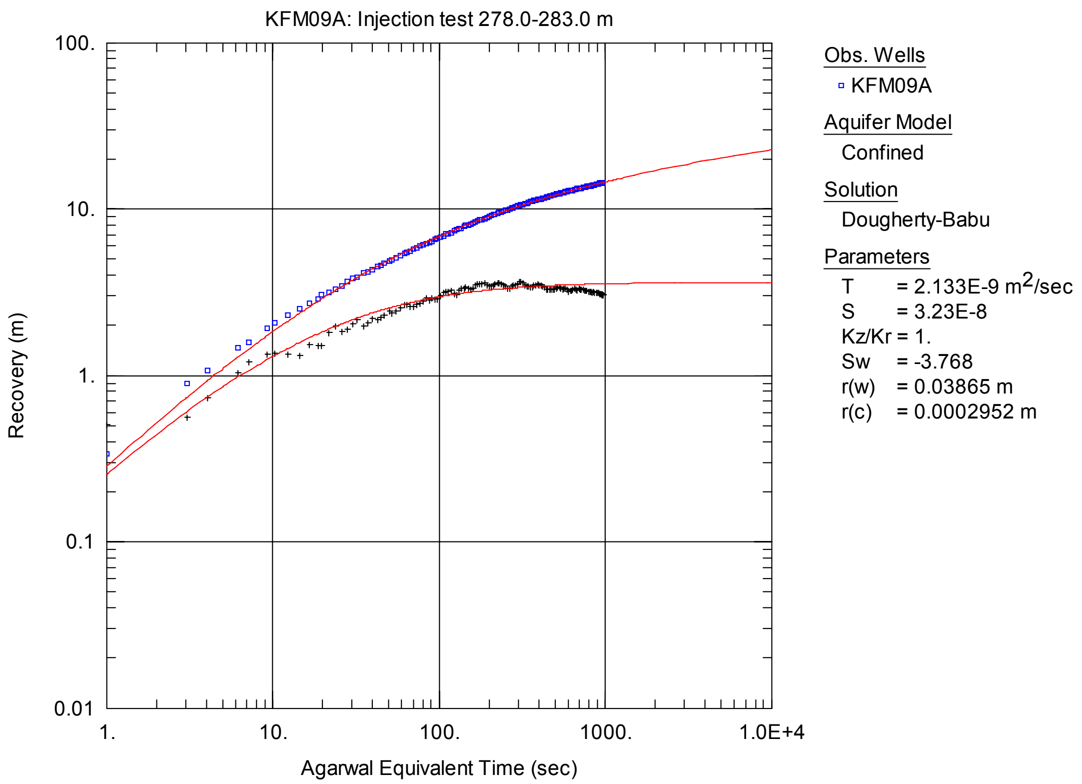


Figure A3-329. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 278.0-283.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for pseudo-radial response during recovery.*

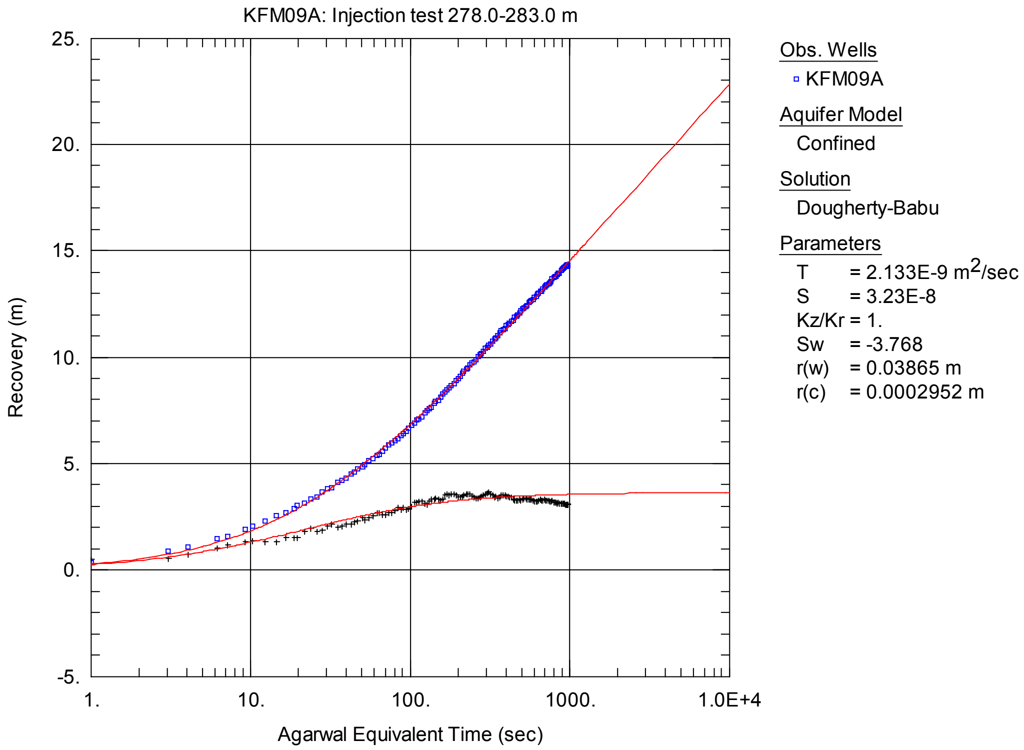


Figure A3-330. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 278.0-283.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for pseudo-radial response during recovery.*

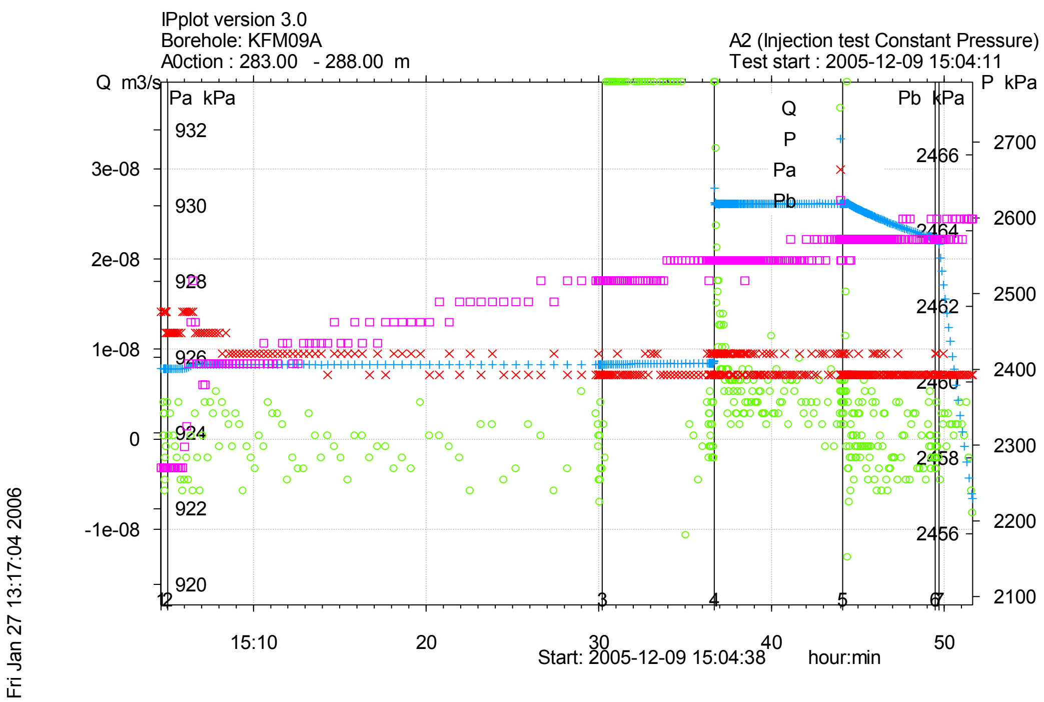


Figure A3-331. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 283.0-288.0 m in borehole KFM09A.*

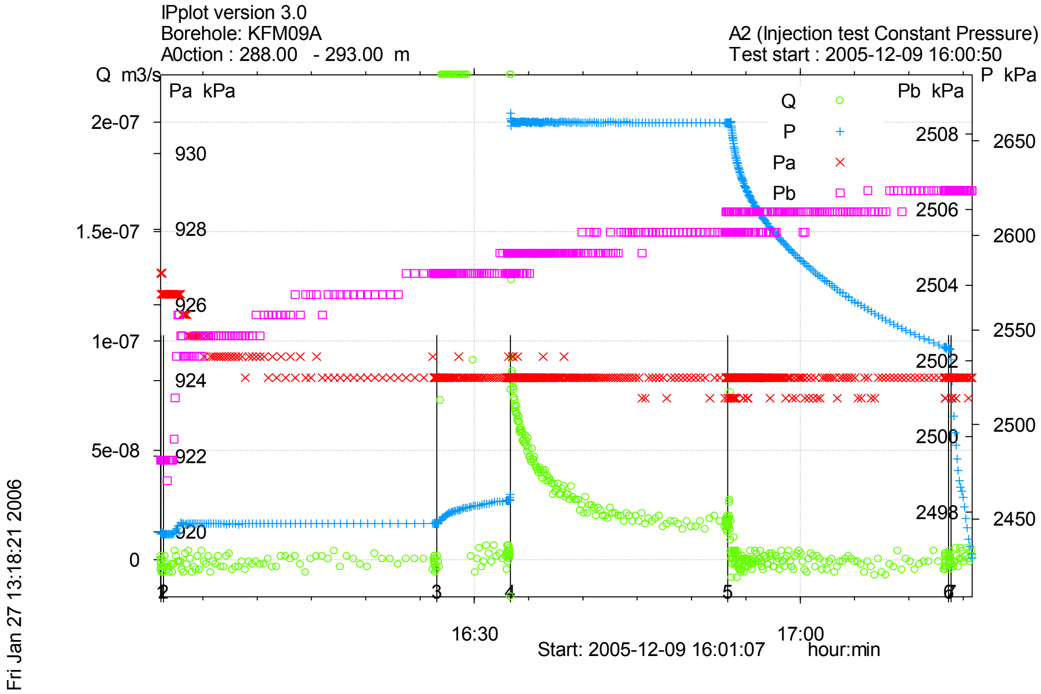


Figure A3-332. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 288.0-293.0 m in borehole KFM09A.

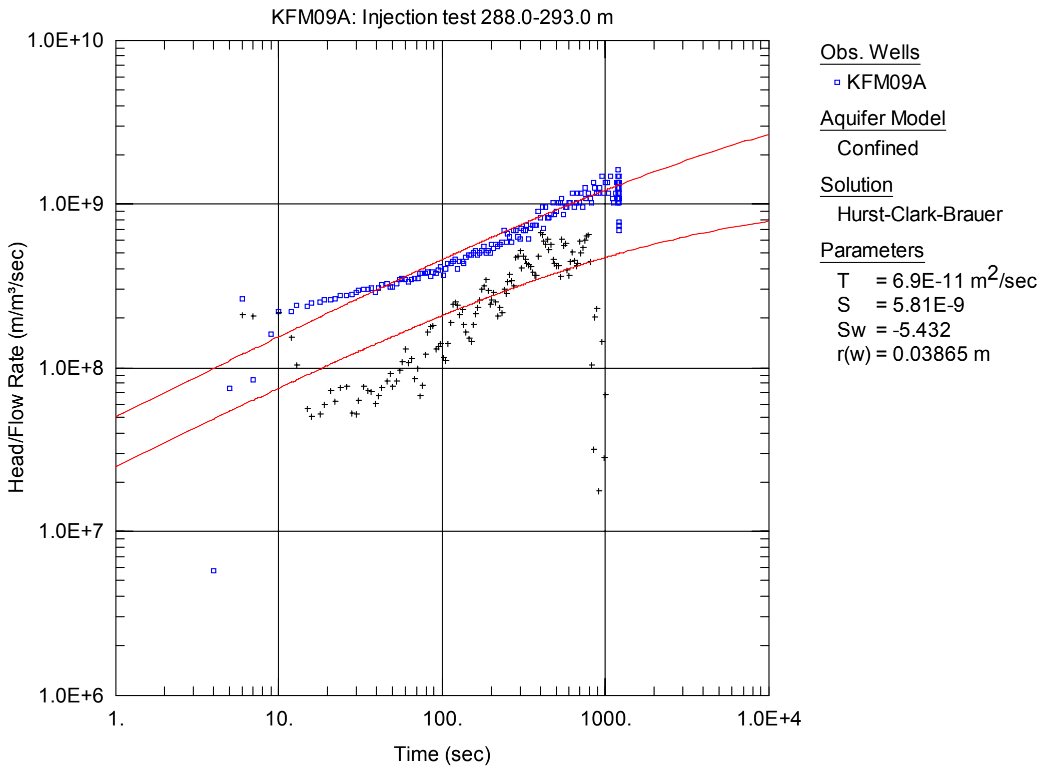


Figure A3-333. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 288.0-293.0 m in KFM09A.

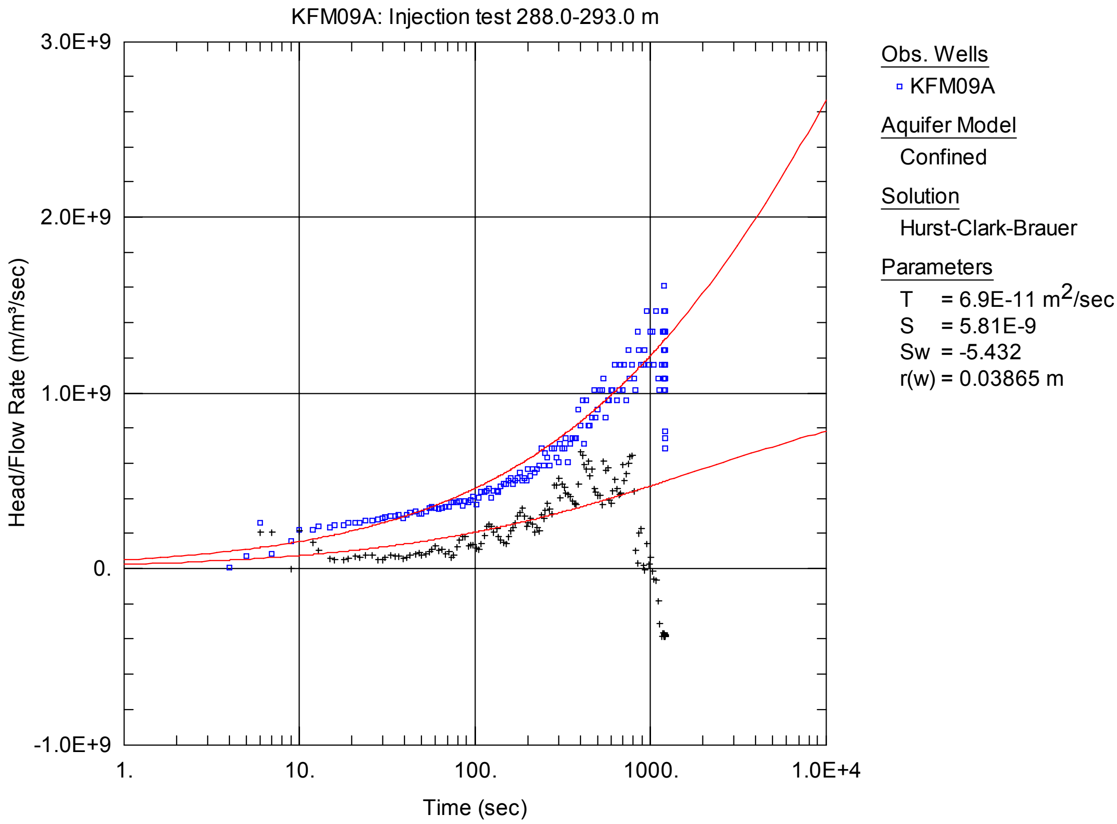


Figure A3-334. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 288.0-293.0 m in KFM09A.*

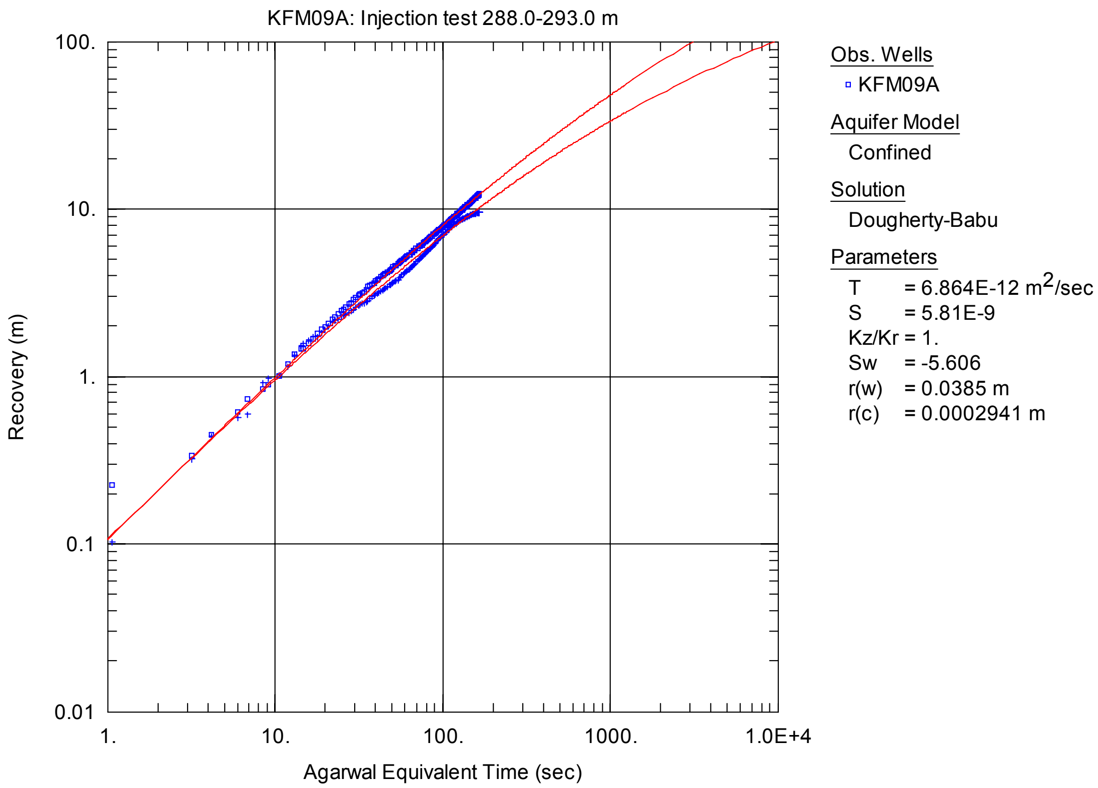


Figure A3-335. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 288.0-293.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.*

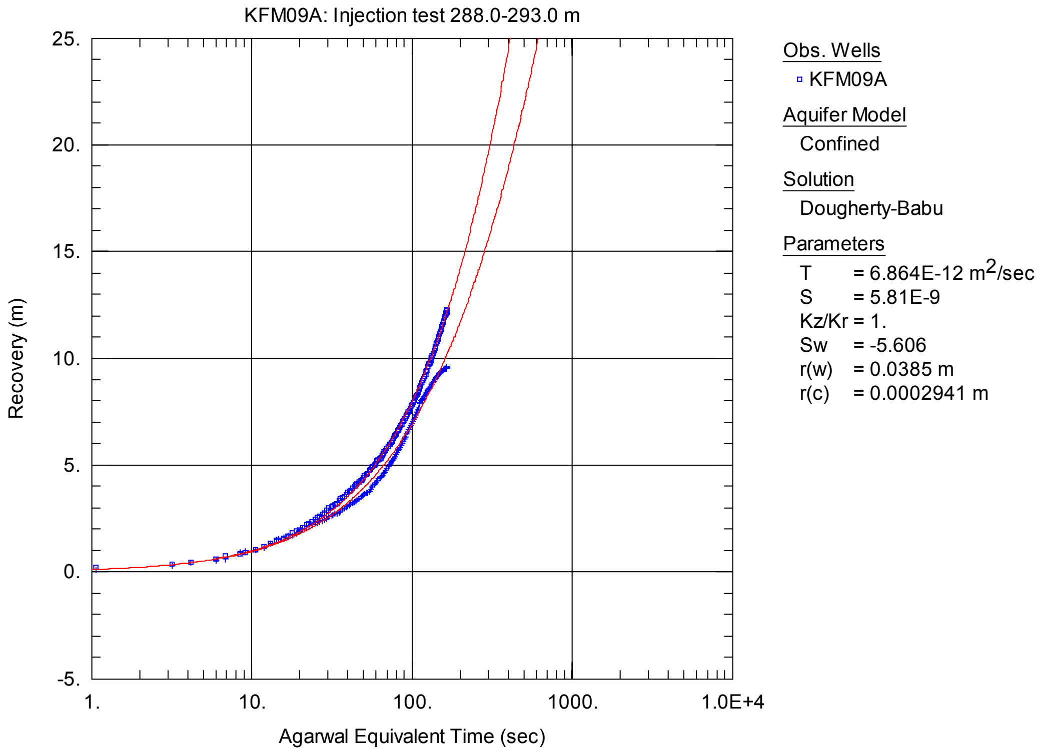


Figure A3-336. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 288.0-293.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.*

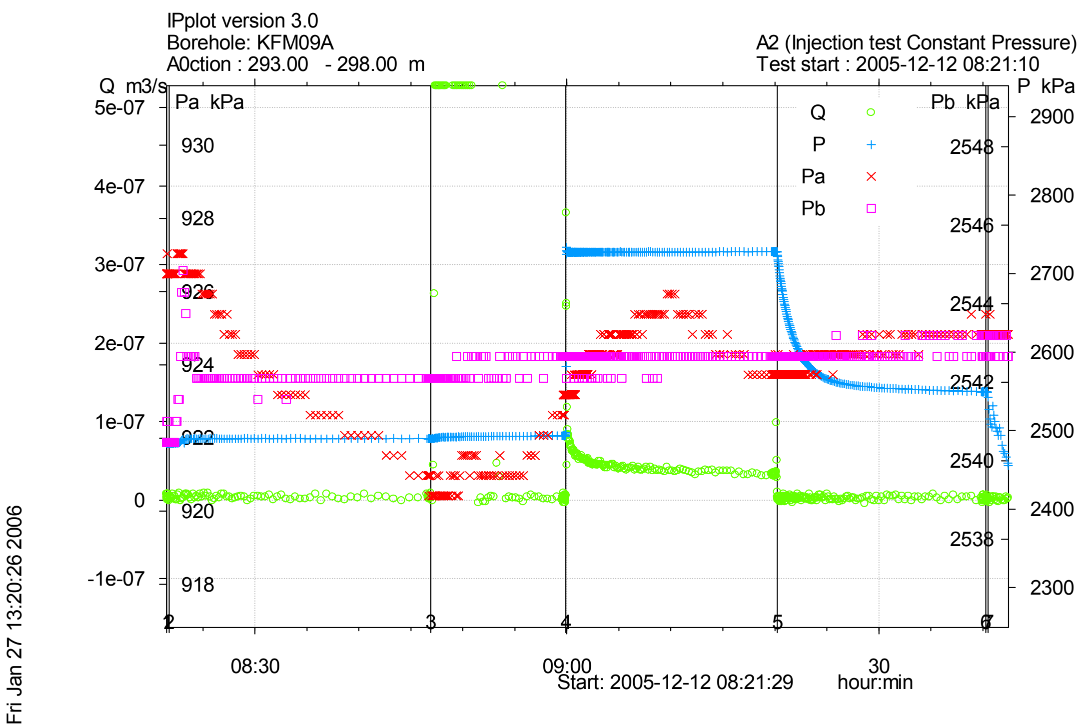


Figure A3-337. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 293.0-298.0 m in borehole KFM09A.*

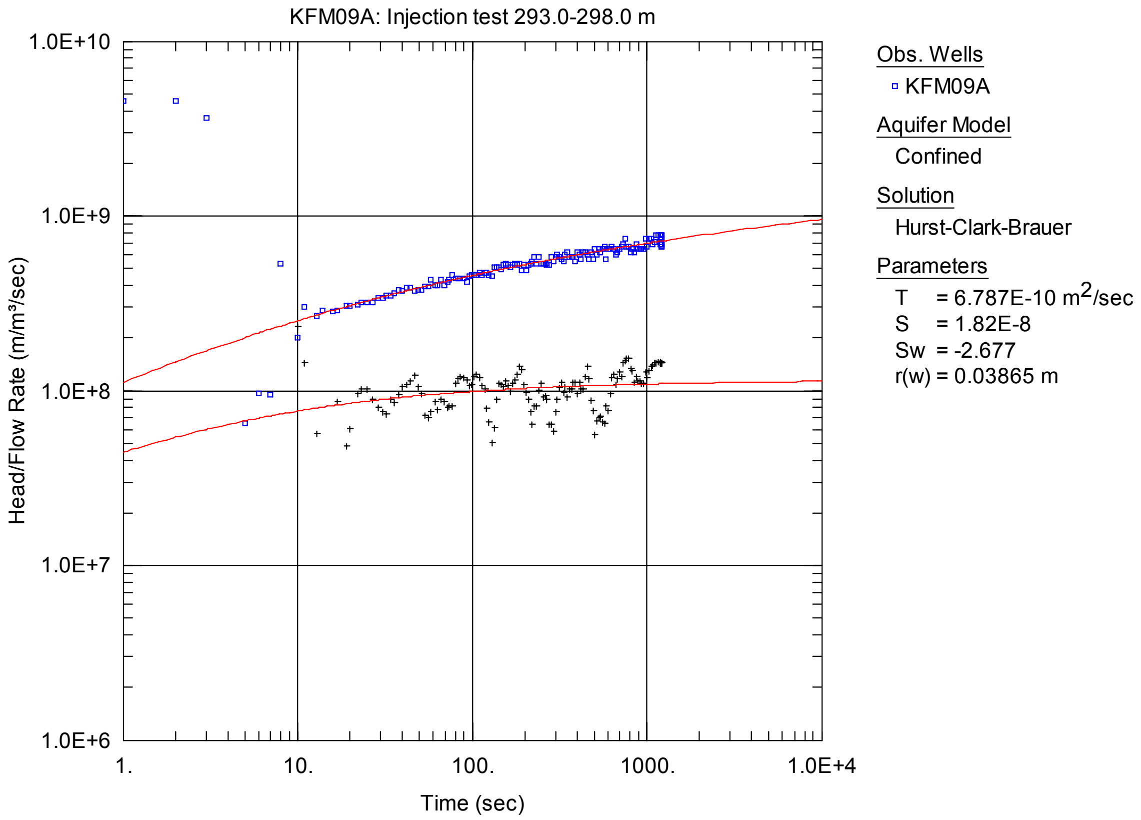


***Figure A3-338.** Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 293.0-298.0 m in KFM09A.*

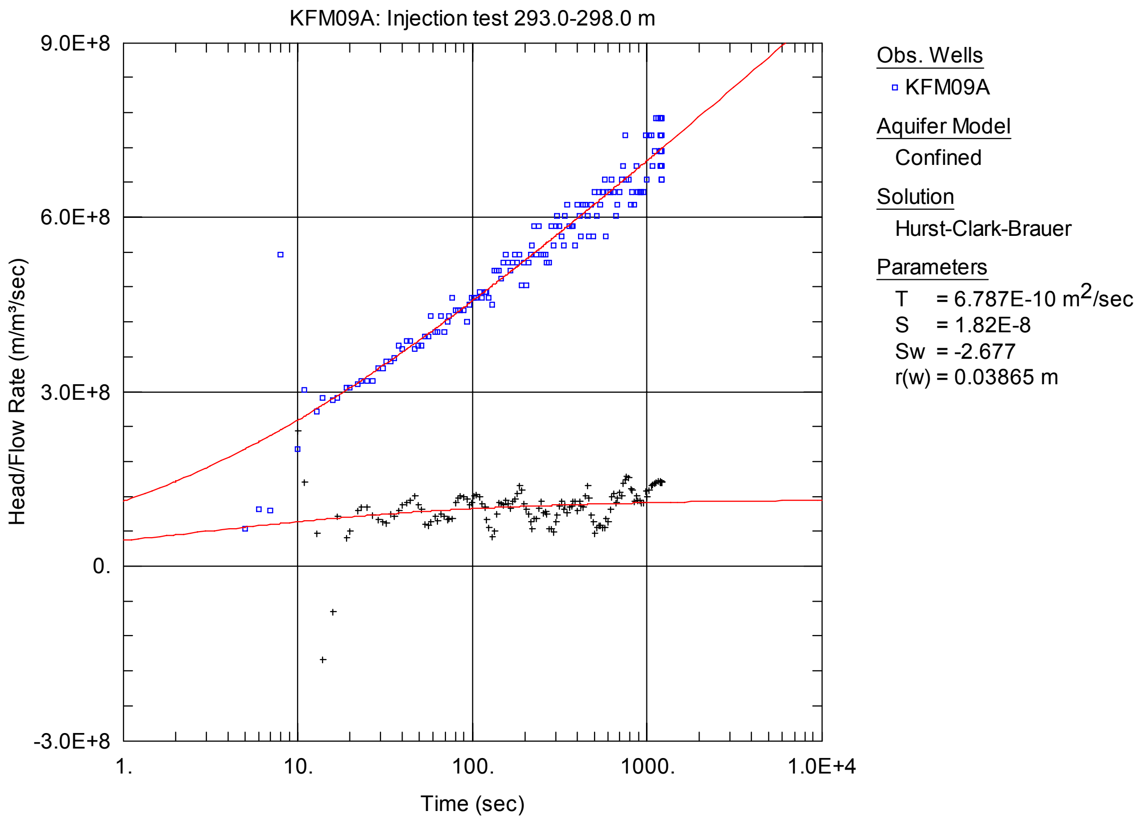


***Figure A3-339.** Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 293.0-298.0 m in KFM09A.*

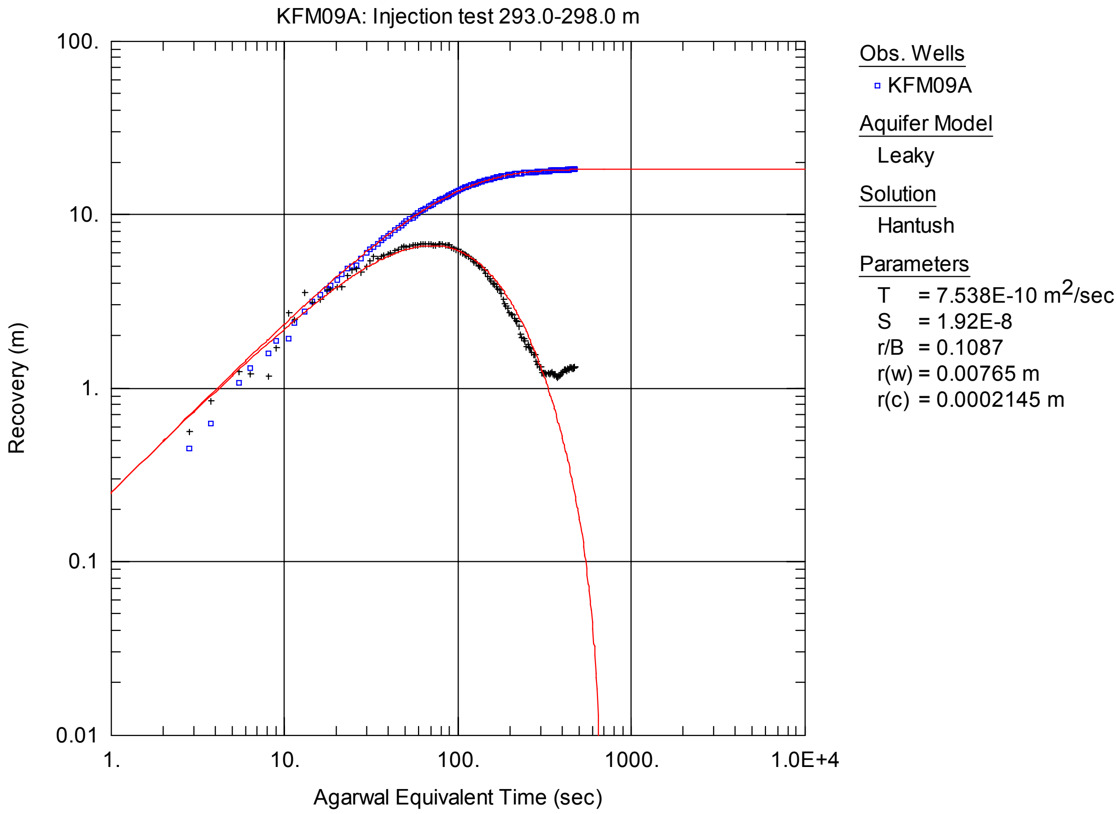


Figure A3-340. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 293.0-298.0 m in KFM09A.*

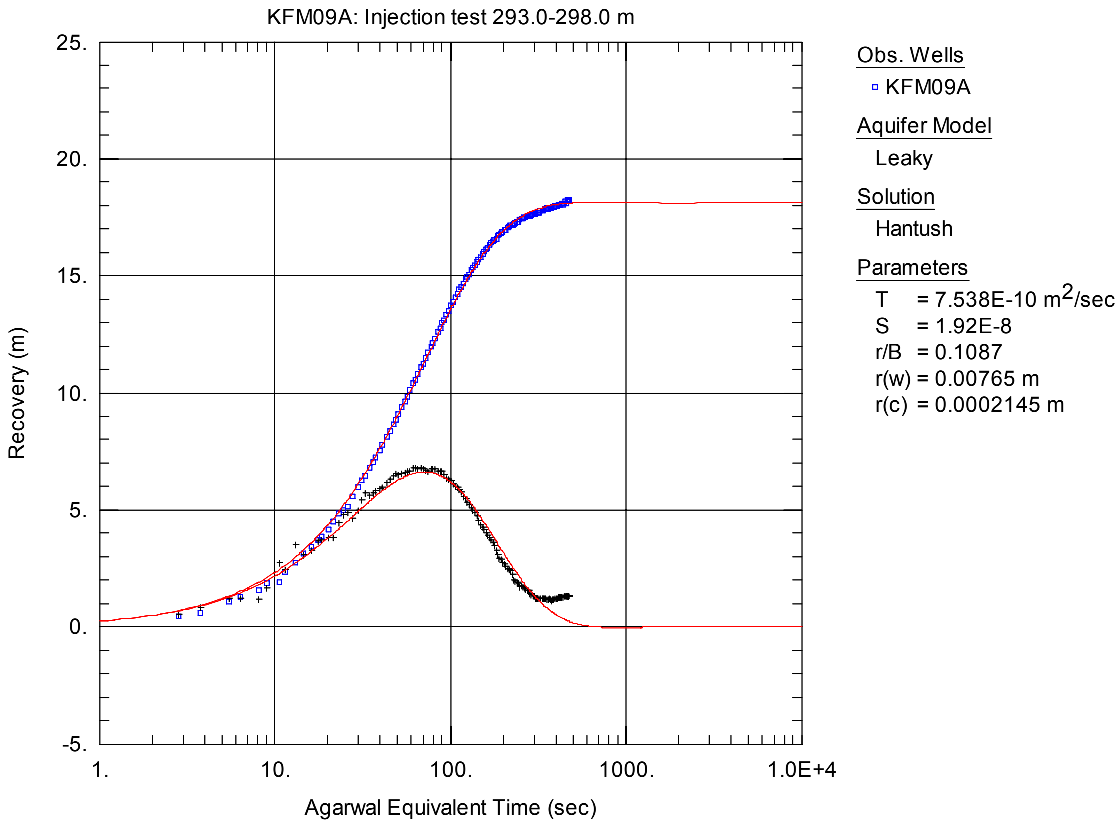


Figure A3-341. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 293.0-298.0 m in KFM09A.*

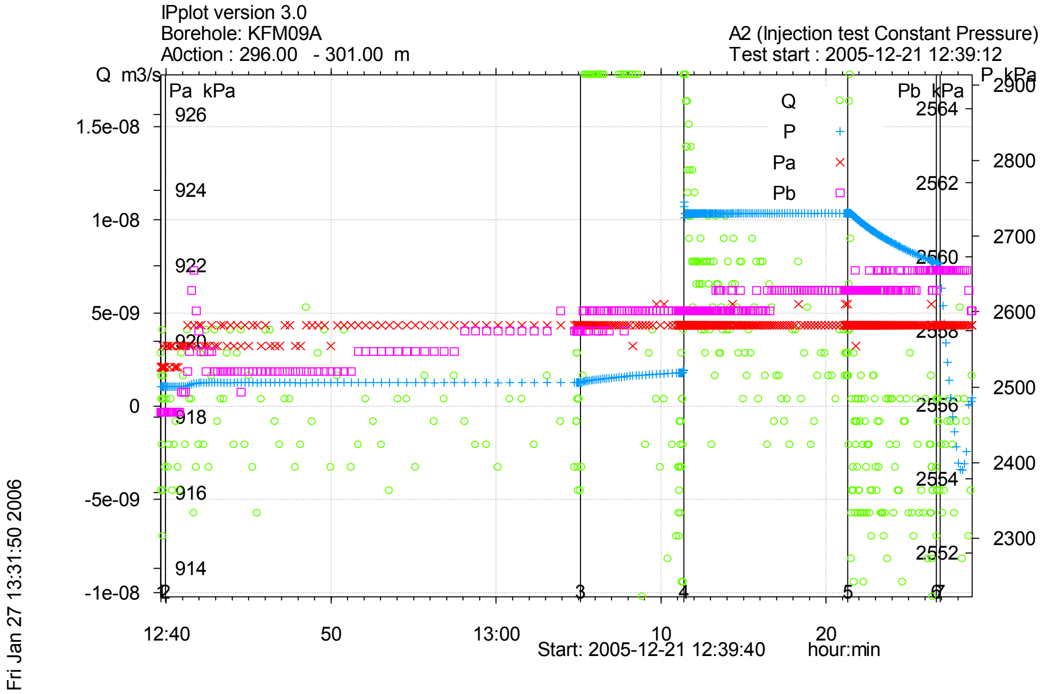


Figure A3-342. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 296.0-301.0 m in borehole KFM09A.*

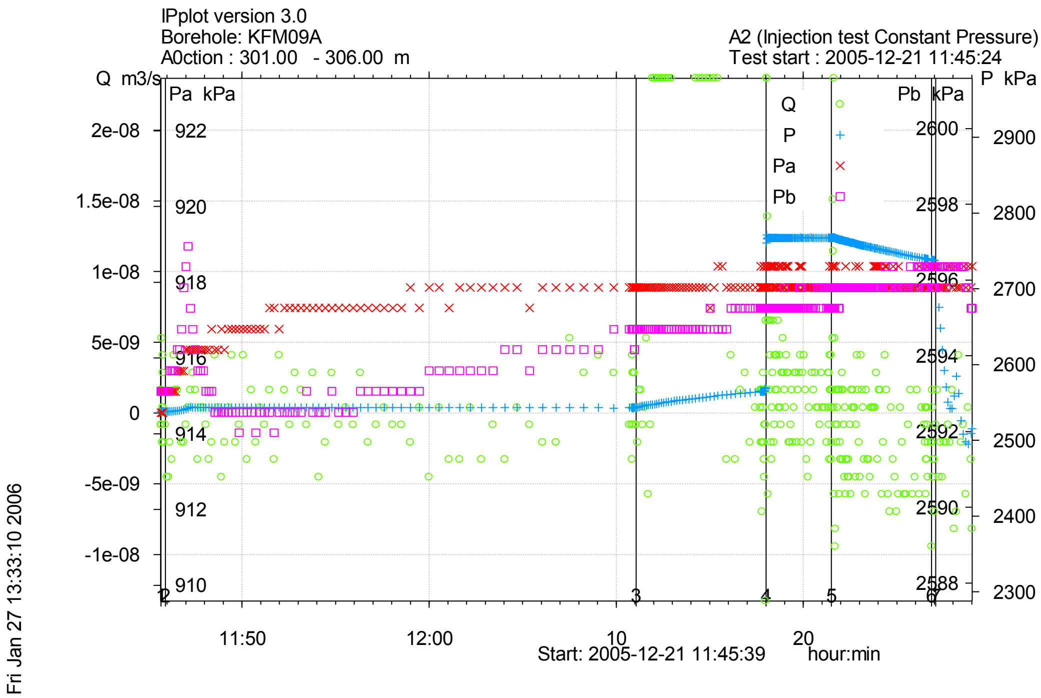


Figure A3-343. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 301.0-306.0 m in borehole KFM09A.*

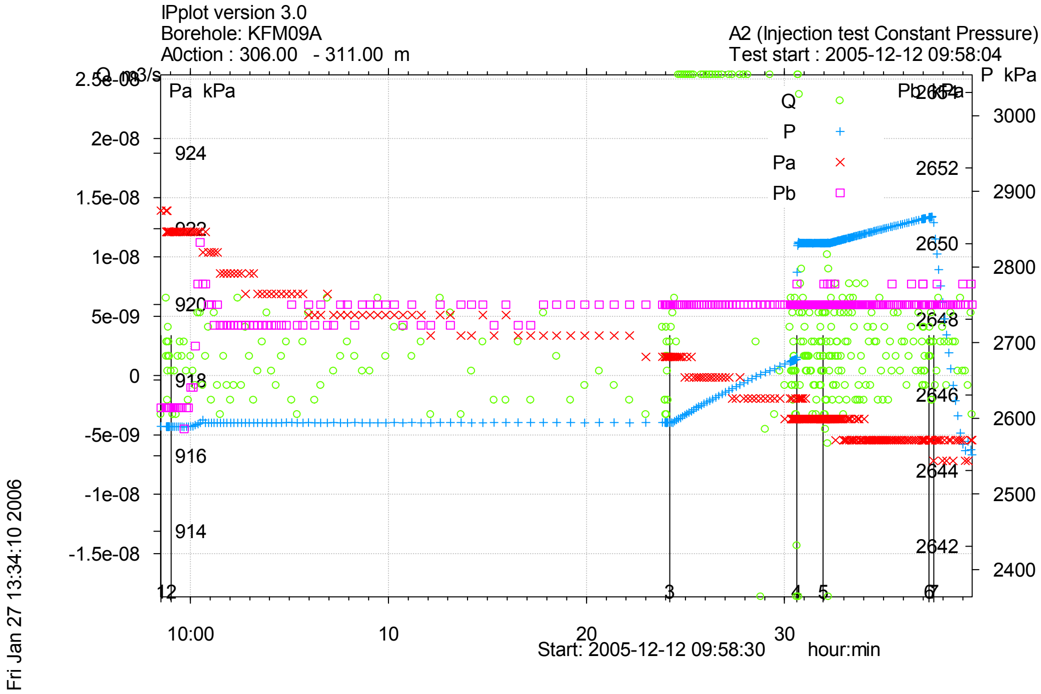


Figure A3-344. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 306.0-311.0 m in borehole KFM09A.*

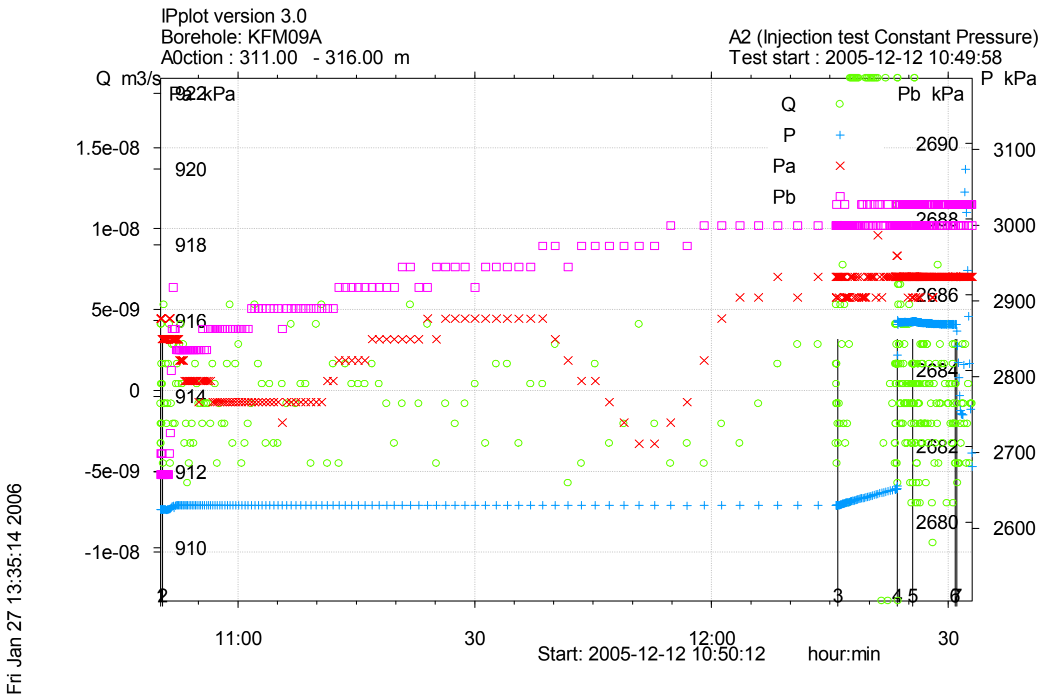


Figure A3-345. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 311.0-316.0 m in borehole KFM09A.*

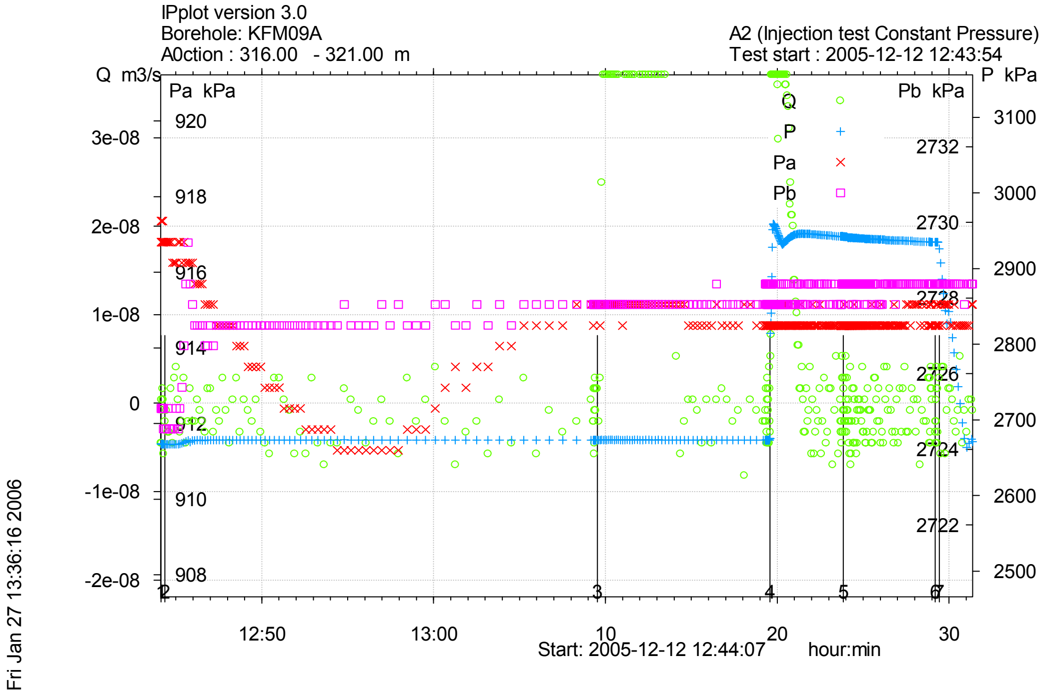


Figure A3-346. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 316.0-321.0 m in borehole KFM09A.

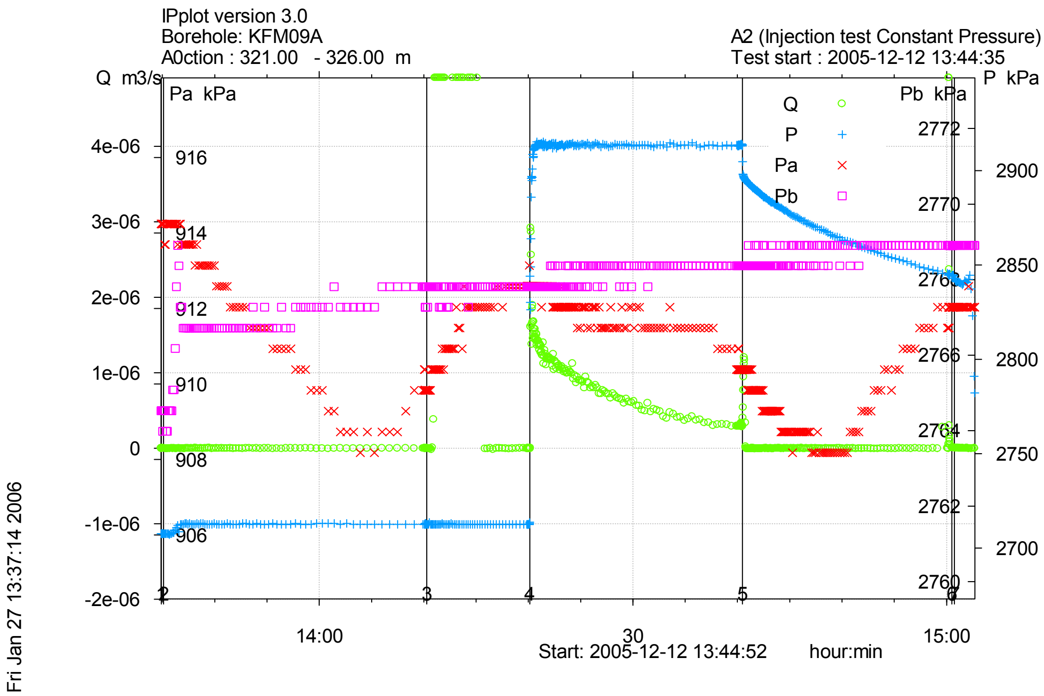


Figure A3-347. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 321.0-326.0 m in borehole KFM09A.

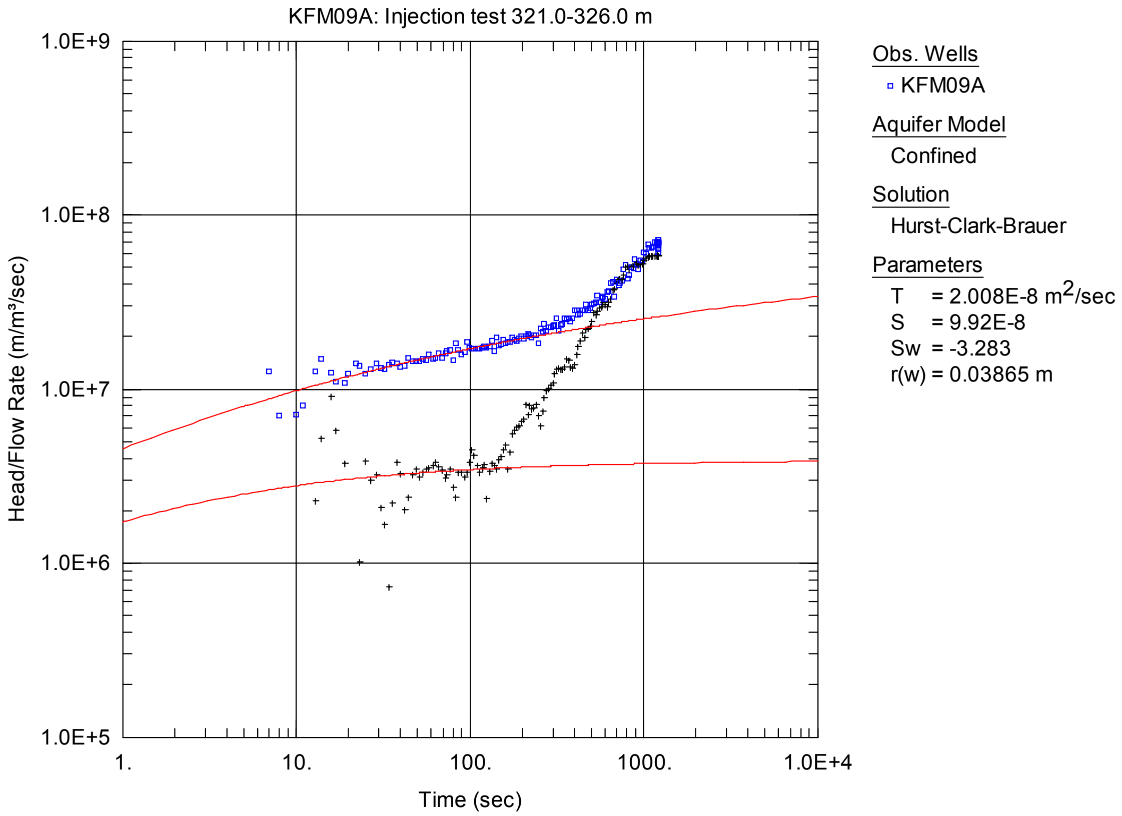


Figure A3-348. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 321.0-326.0 m in KFM09A.*

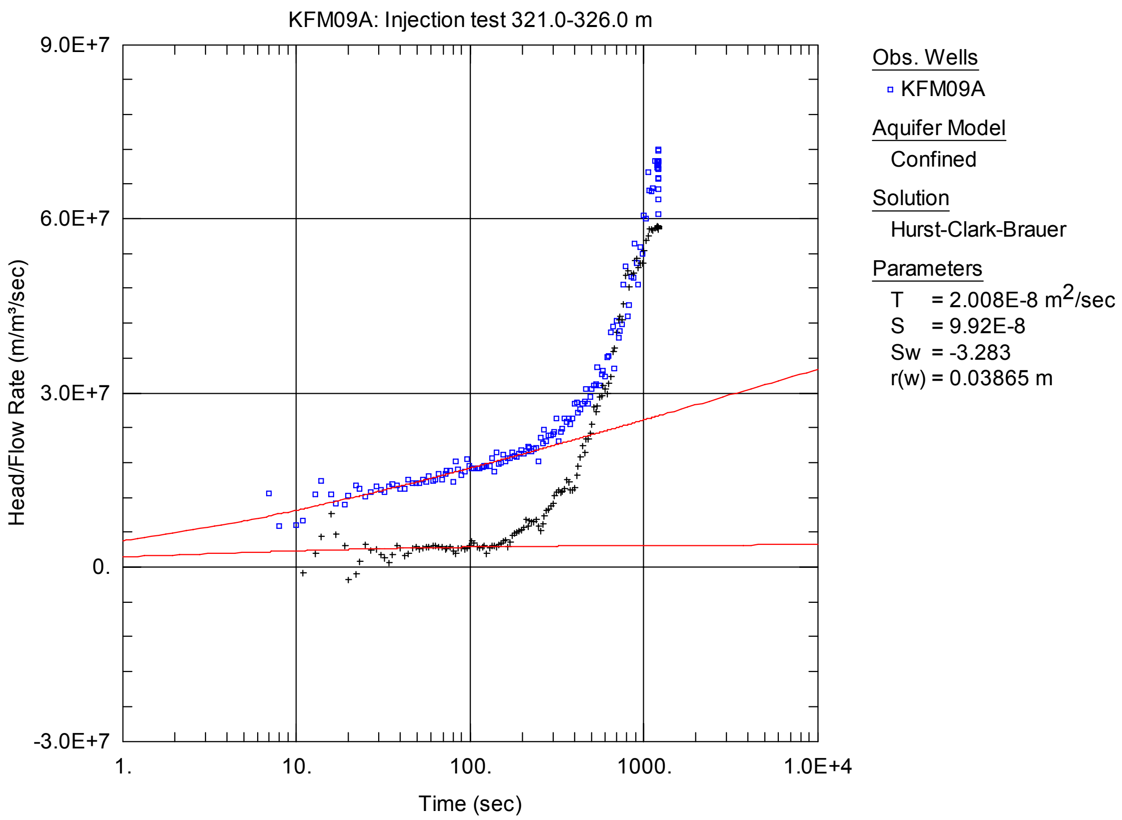


Figure A3-349. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 321.0-326.0 m in KFM09A.*

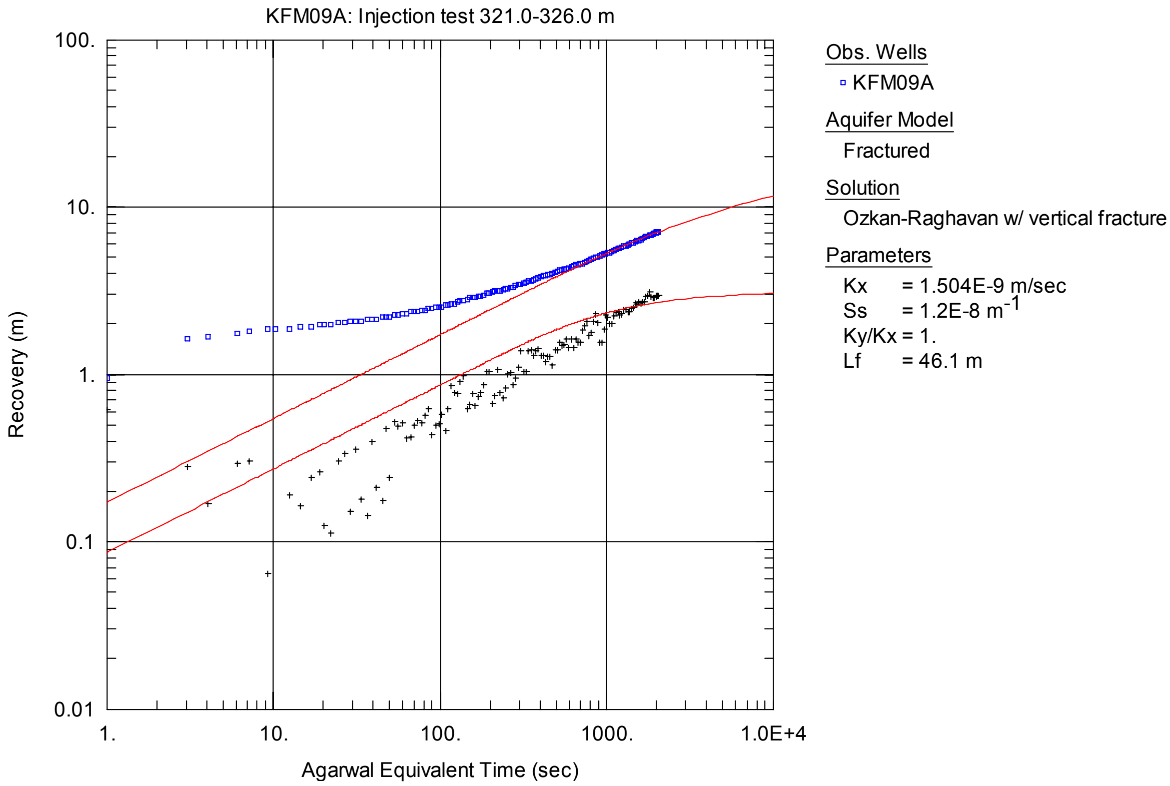


Figure A3-350. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 321.0-326.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.*

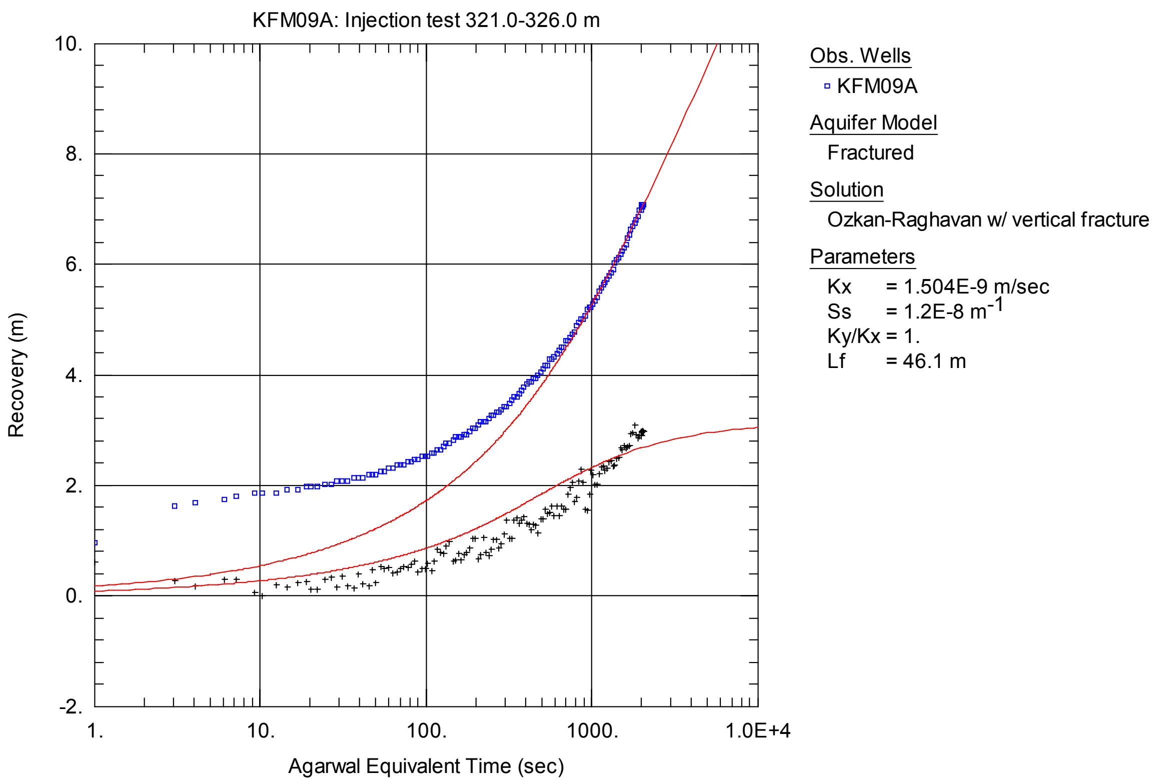


Figure A3-351. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 321.0-326.0 m in KFM09A No unambiguous transient evaluation is possible on the recovery period.*

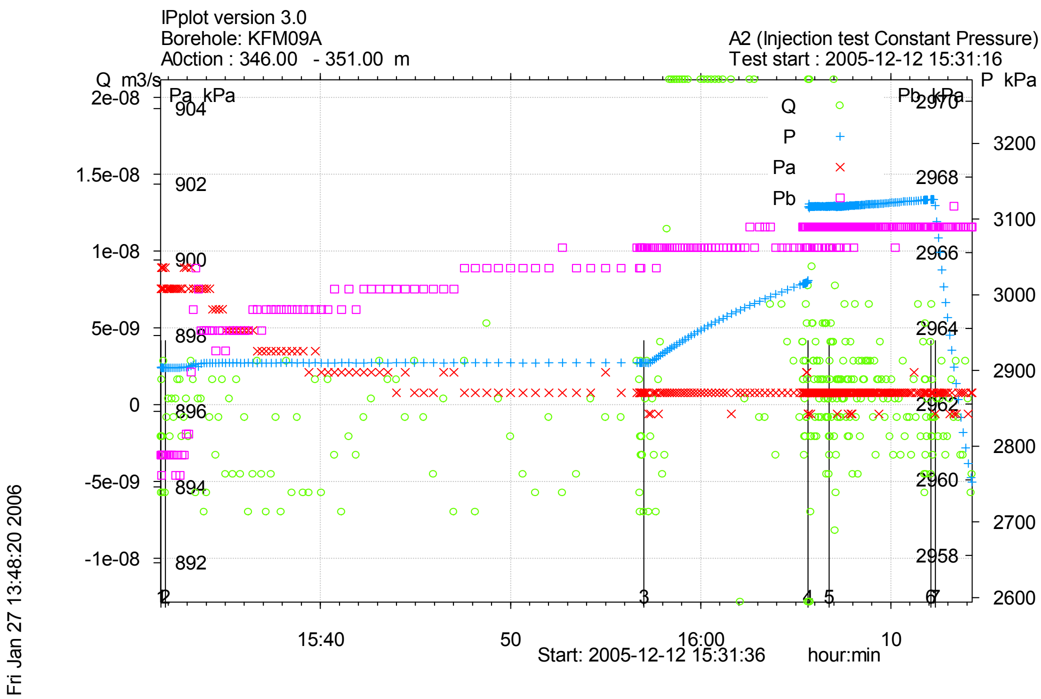


Figure A3-352. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 346.0-351.0 m in borehole KFM09A.

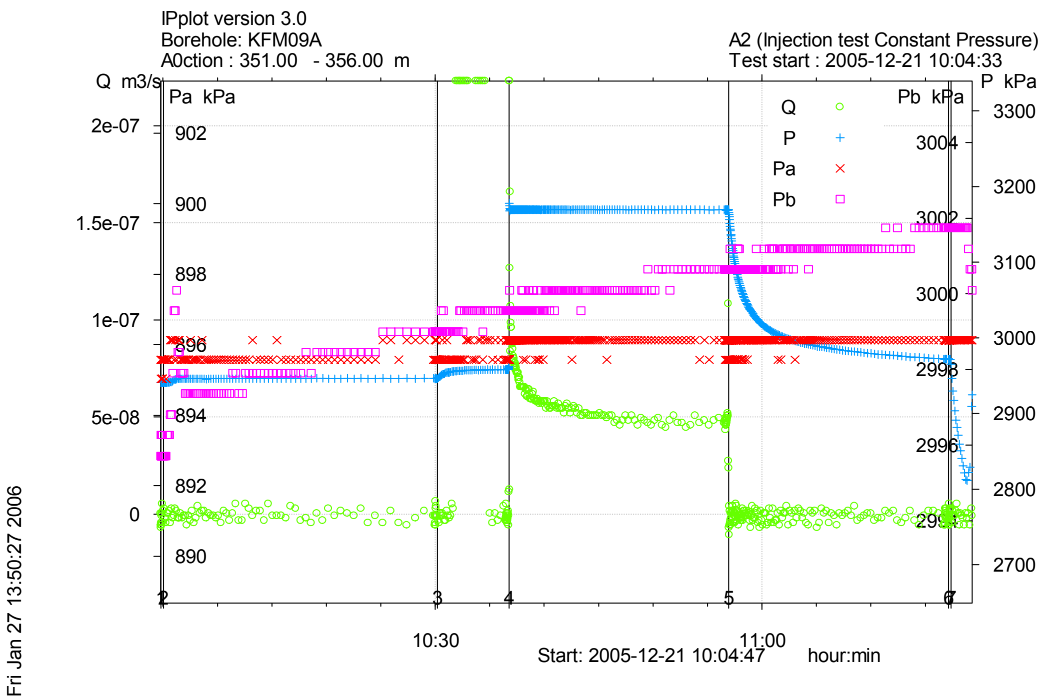


Figure A3-353. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 351.0-356.0 m in borehole KFM09A.*

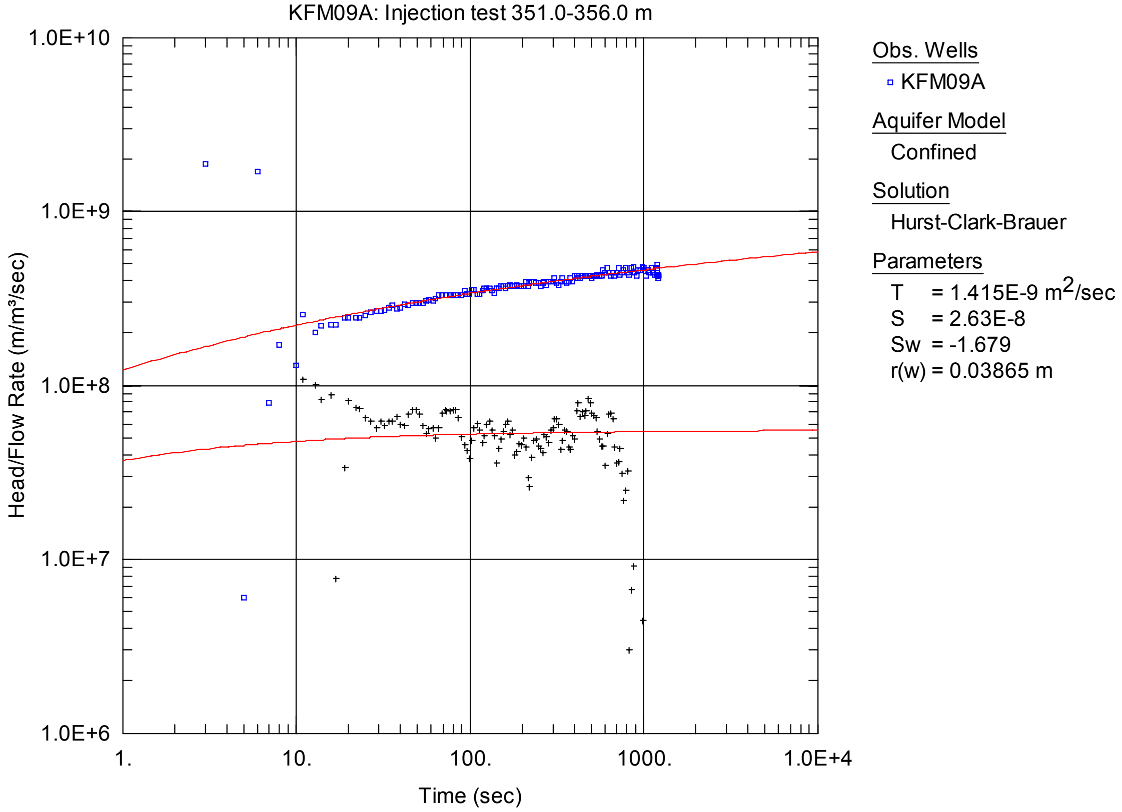


Figure A3-354. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 351.0-356.0 m in KFM09A.*

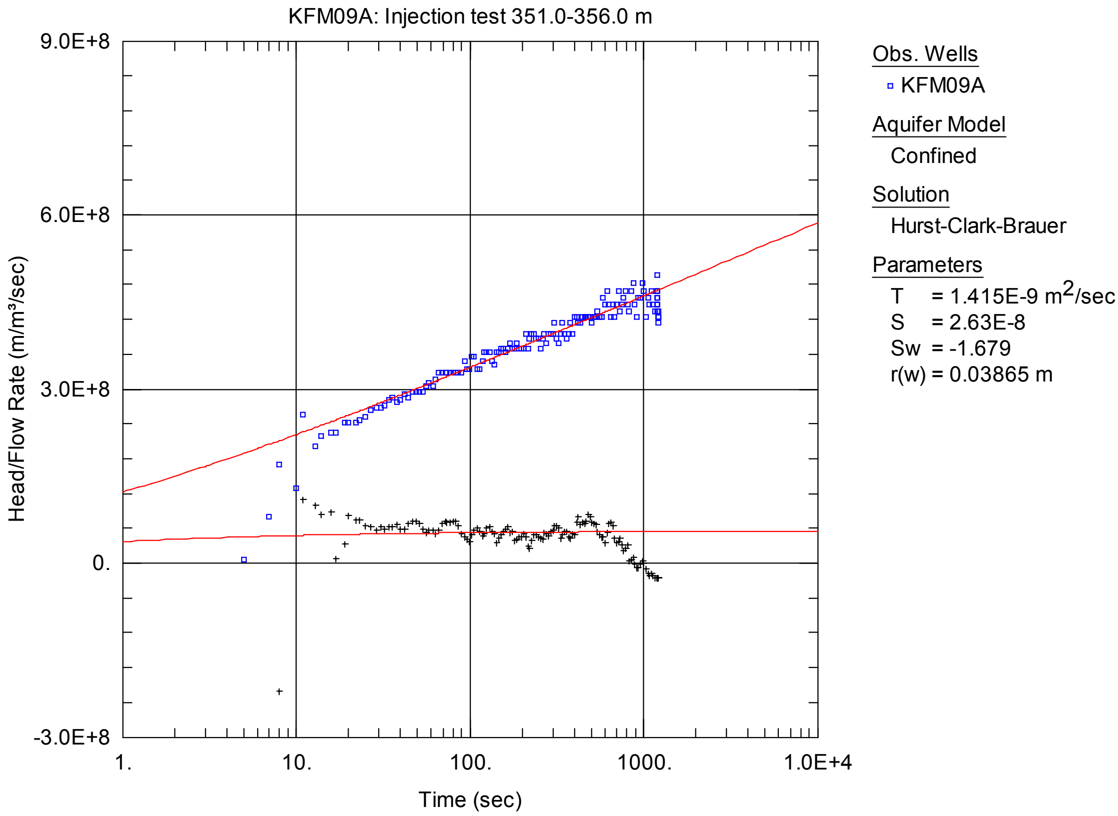


Figure A3-355. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 351.0-356.0 m in KFM09A.*

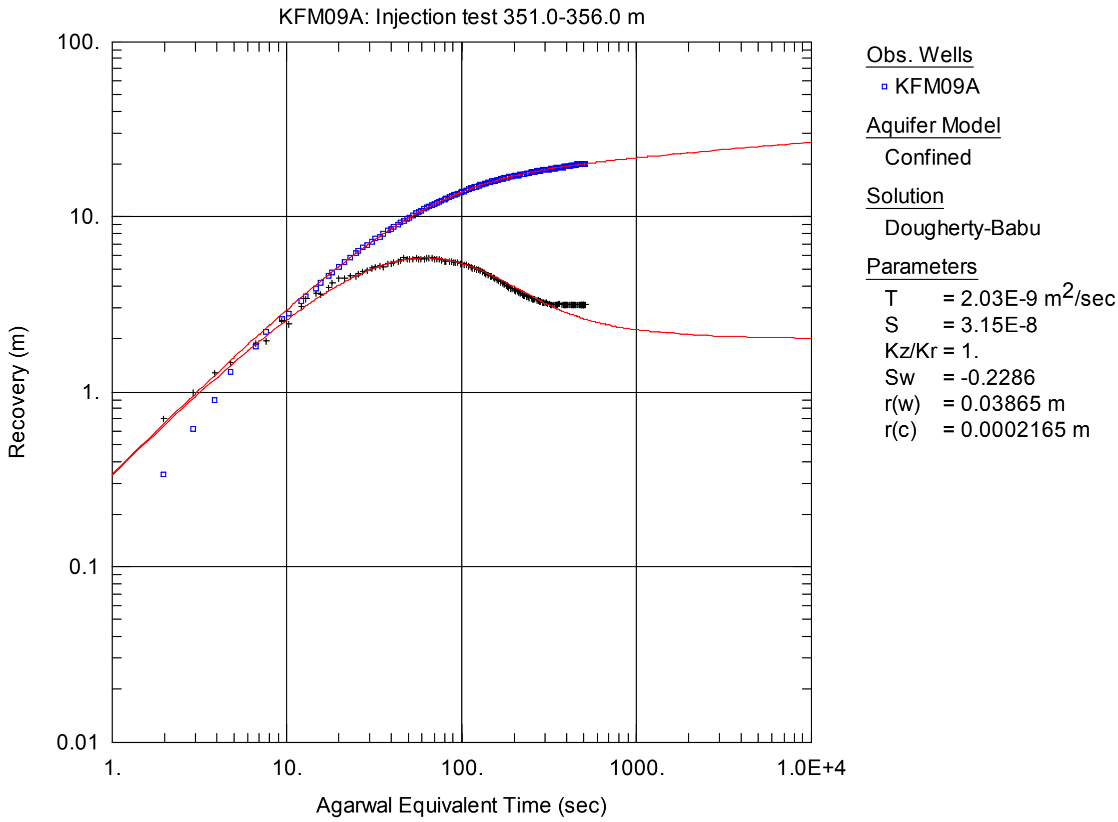


Figure A3-356. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 351.0-356.0 m in KFM09A.*

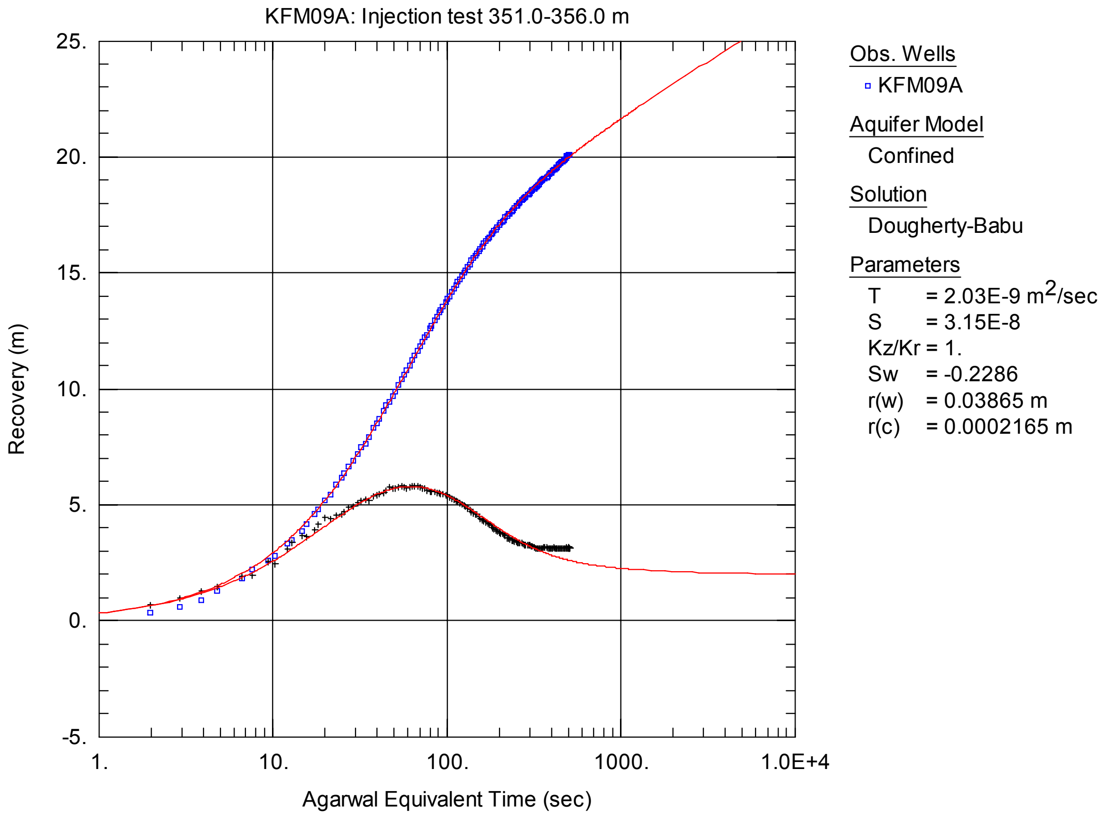


Figure A3-357. Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 351.0-356.0 m in KFM09A.

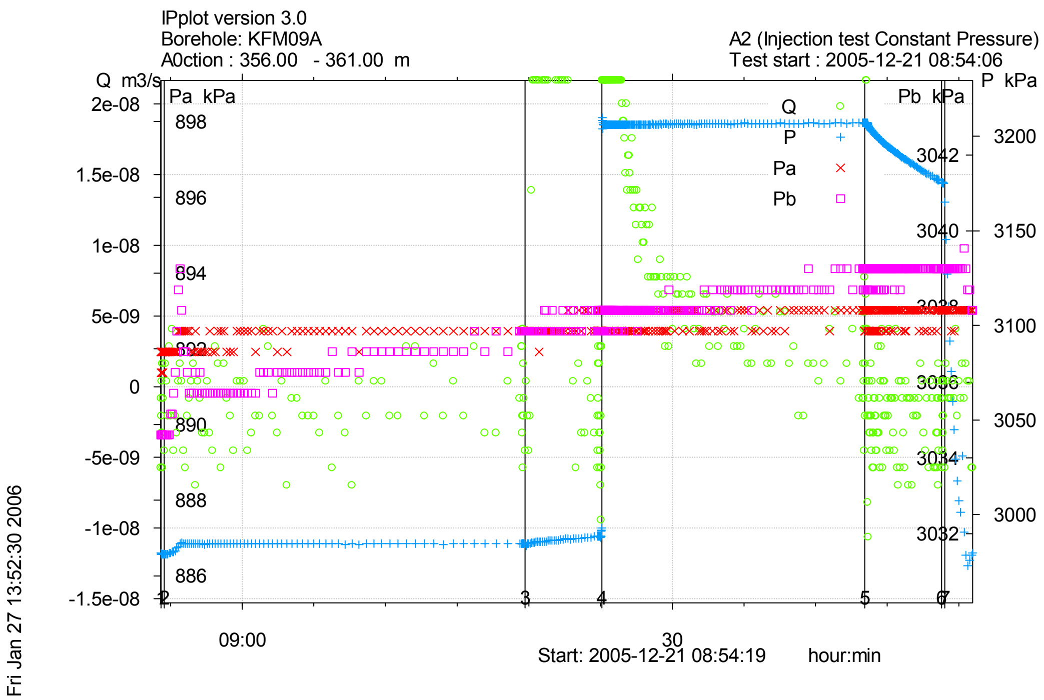


Figure A3-358. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 356.0-361.0 m in borehole KFM09A.

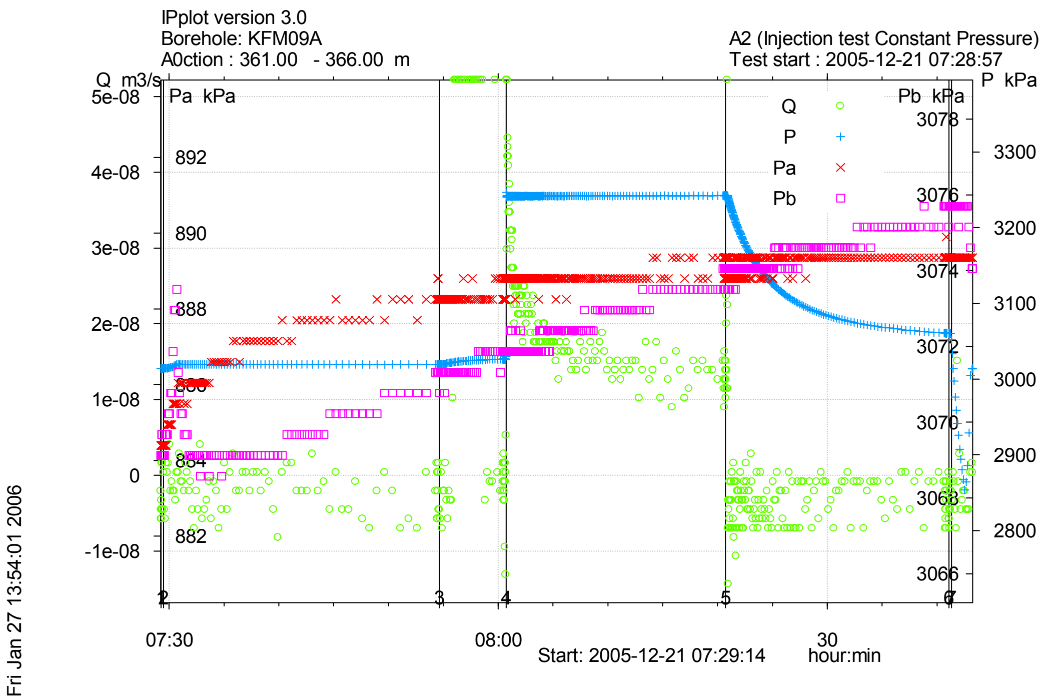


Figure A3-359. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 361.0-366.0 m in borehole KFM09A.*

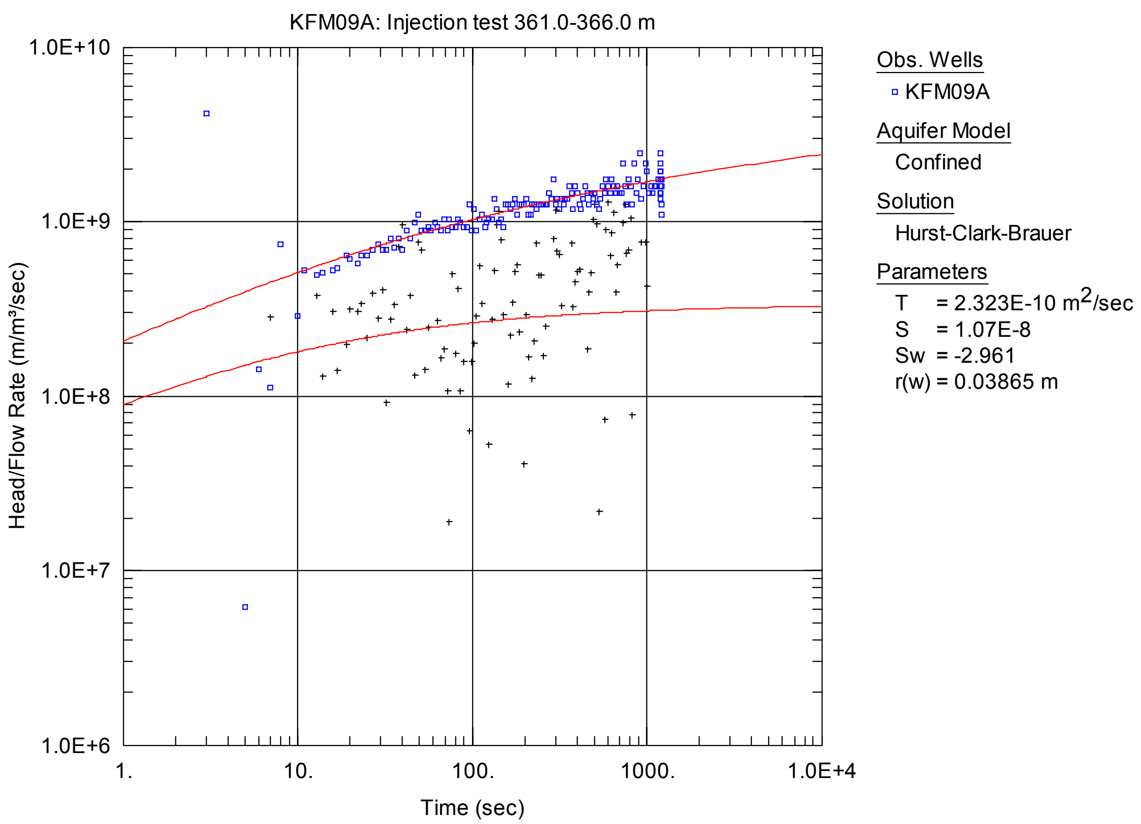


Figure A3-360. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 361.0-366.0 m in KFM09A.*

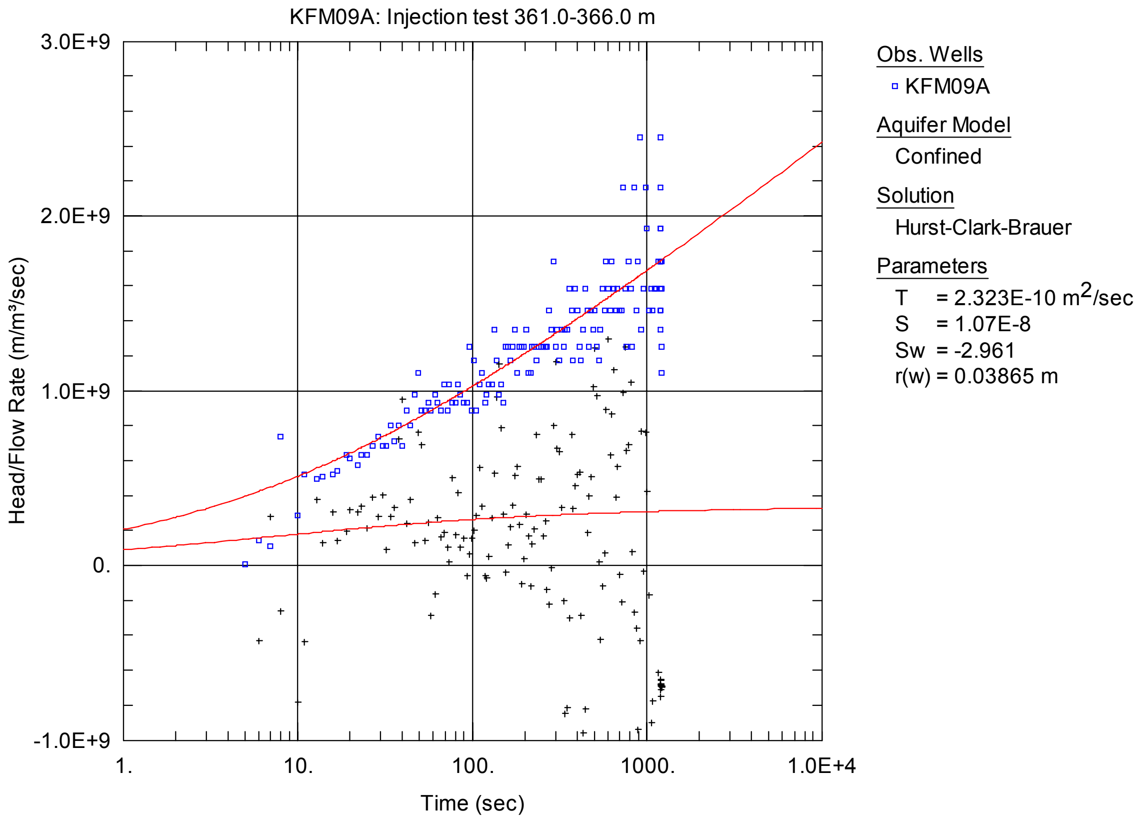


Figure A3-361. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 361.0-366.0 m in KFM09A.*

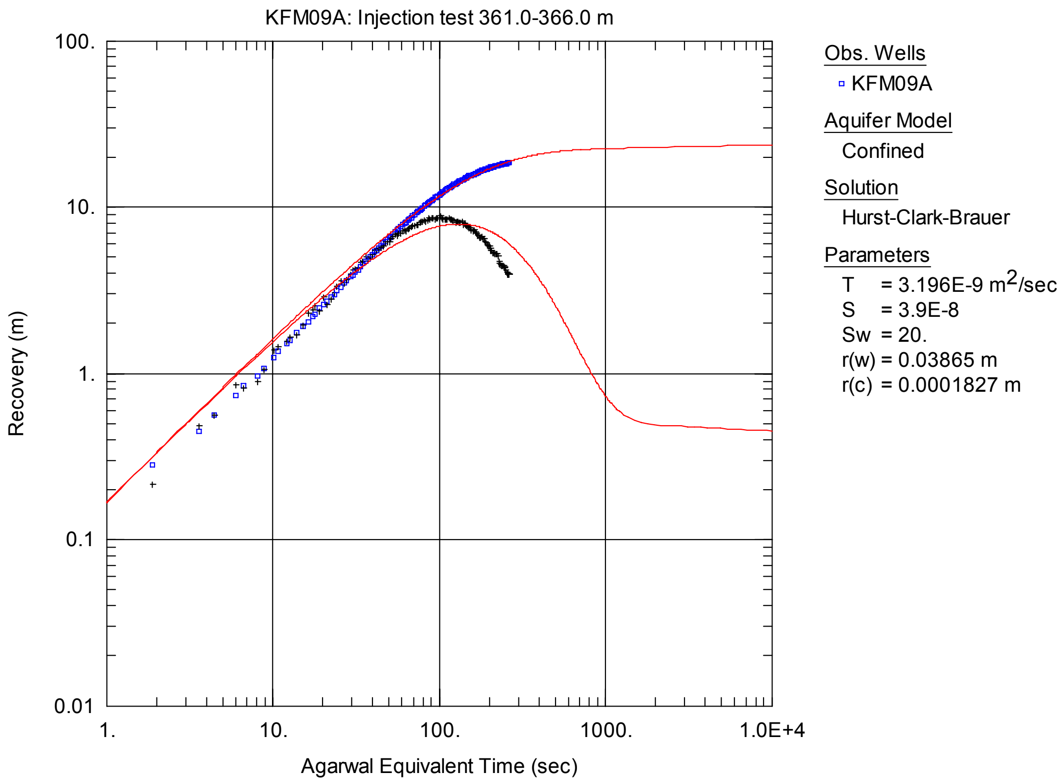


Figure A3-362. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 361.0-366.0 m in KFM09A. No unambiguous transient evaluation could be made from the recovery period.*

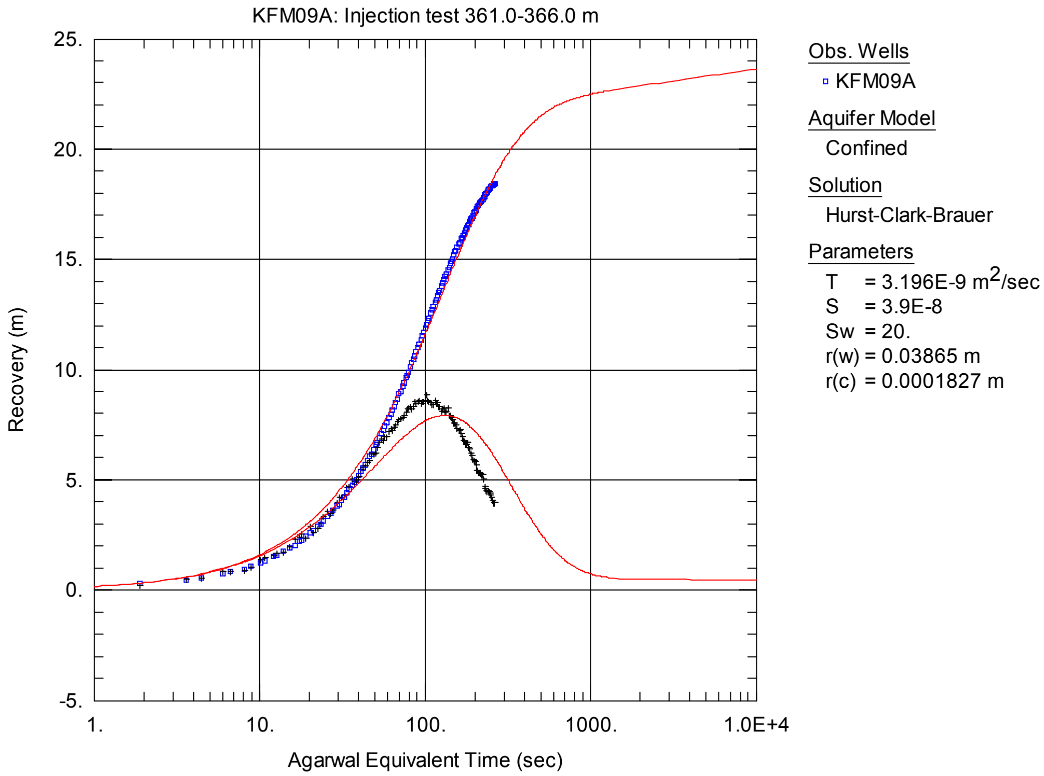


***Figure A3-363.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 361.0-366.0 m in KFM09A. No unambiguous transient evaluation could be made from the recovery period.*

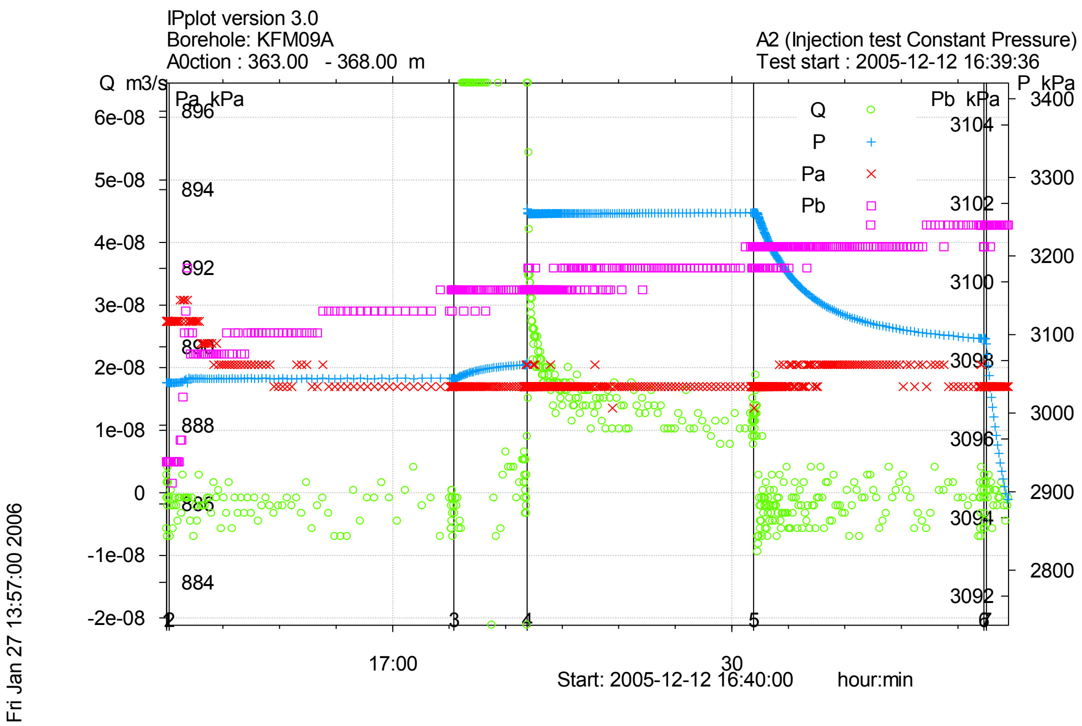


***Figure A3-364.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 363.0-368.0 m in borehole KFM09A.*

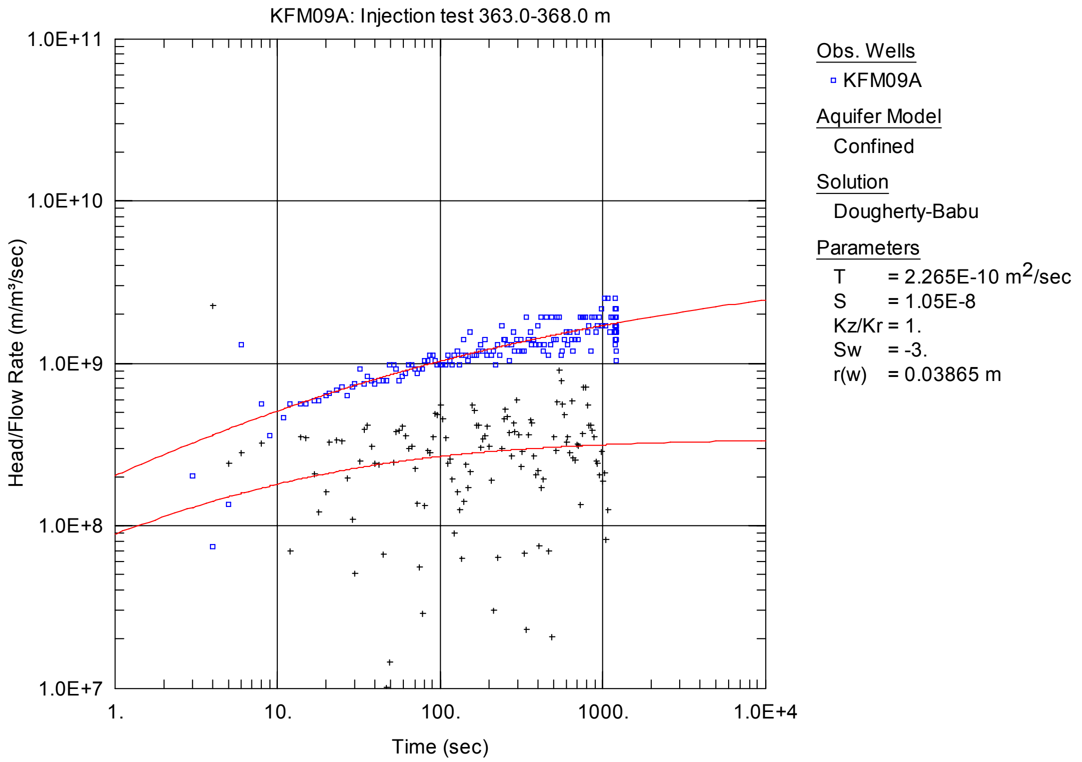


Figure A3-365. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 363.0-368.0 m in KFM09A.*

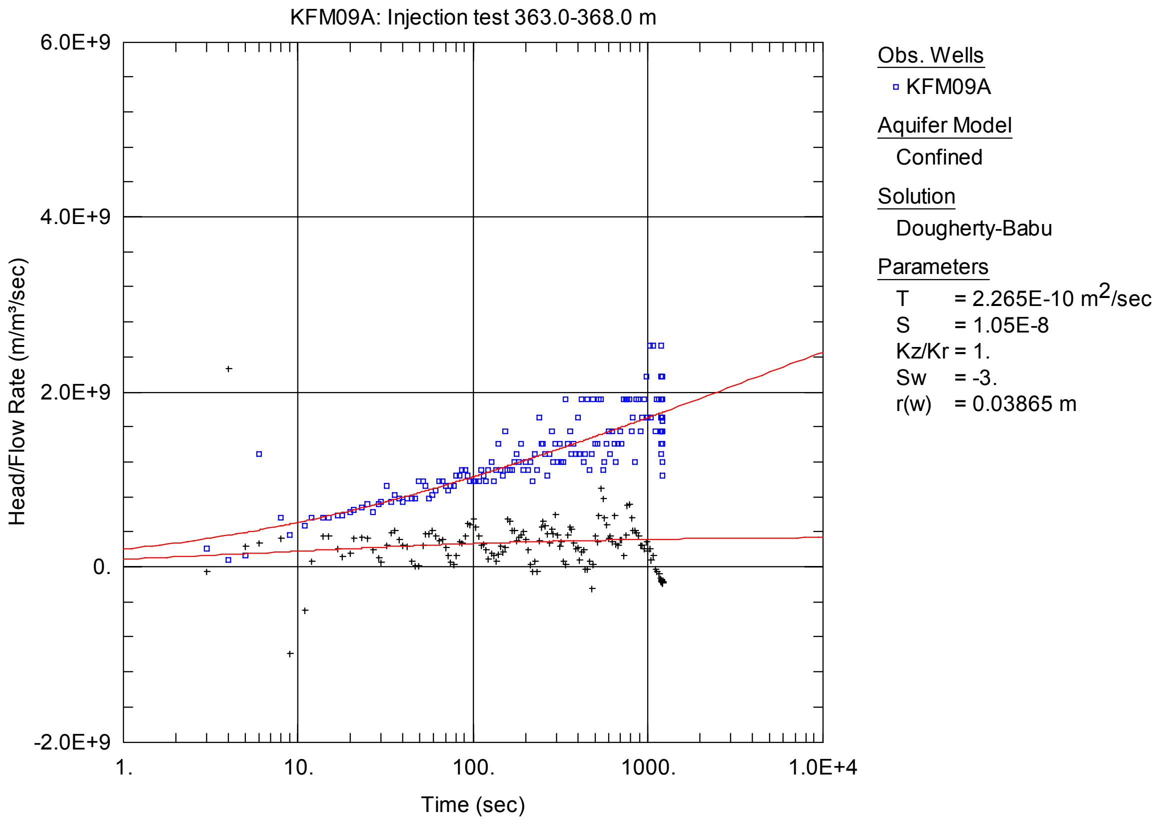


Figure A3-366. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 363.0-368.0 m in KFM09A.*

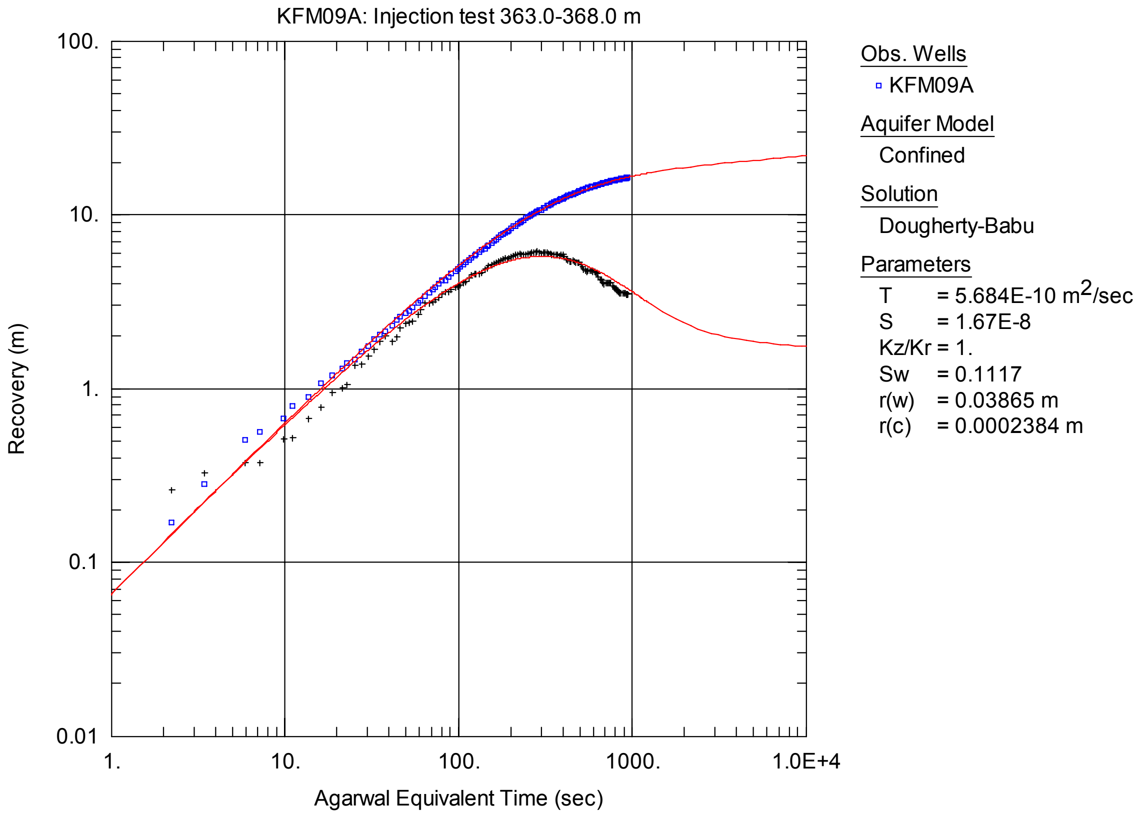


Figure A3-367. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 363.0-368.0 m in KFM09A.*

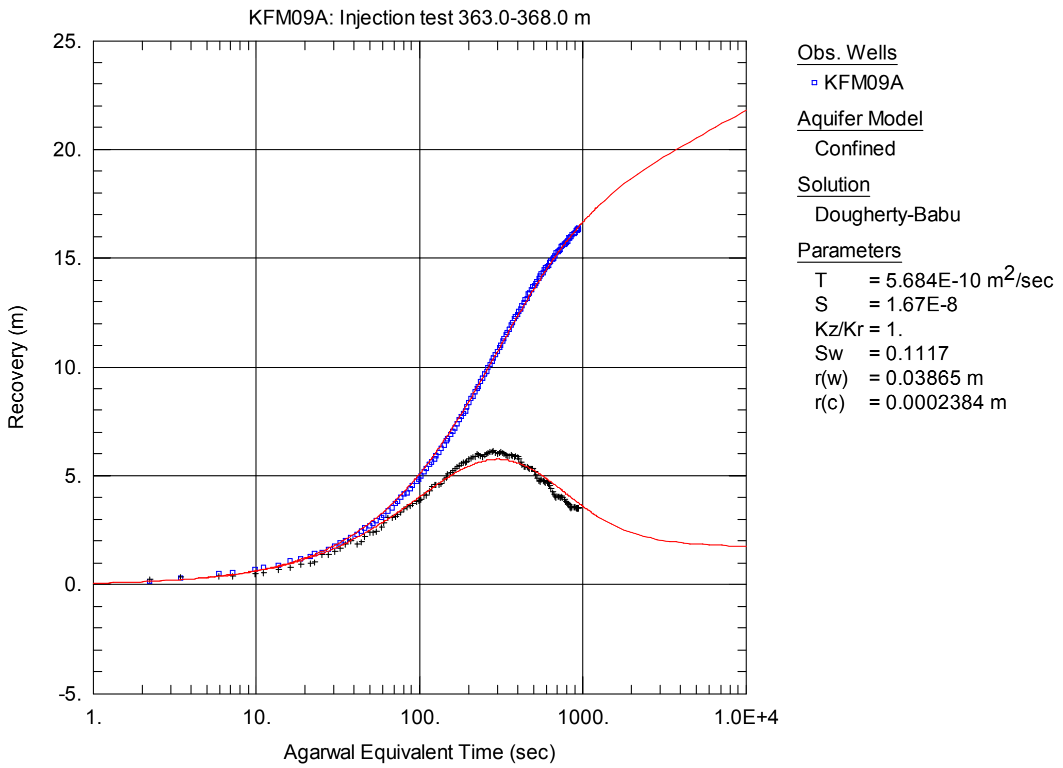


Figure A3-368. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 363.0-368.0 m in KFM09A.*

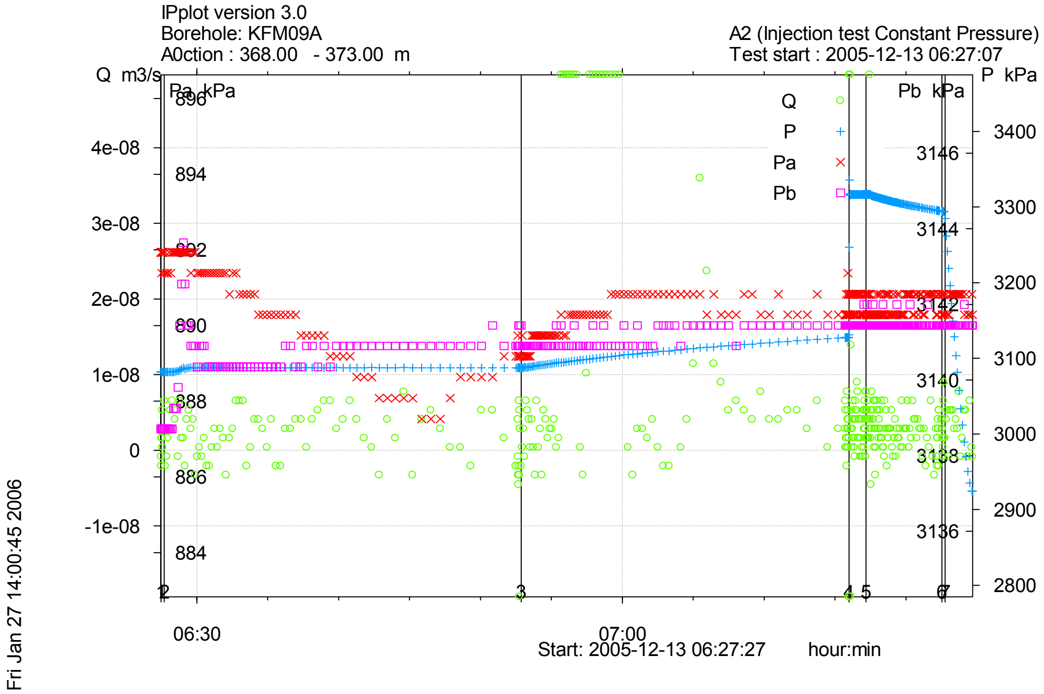


Figure A3-369. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 368.0-373.0 m in borehole KFM09A.*

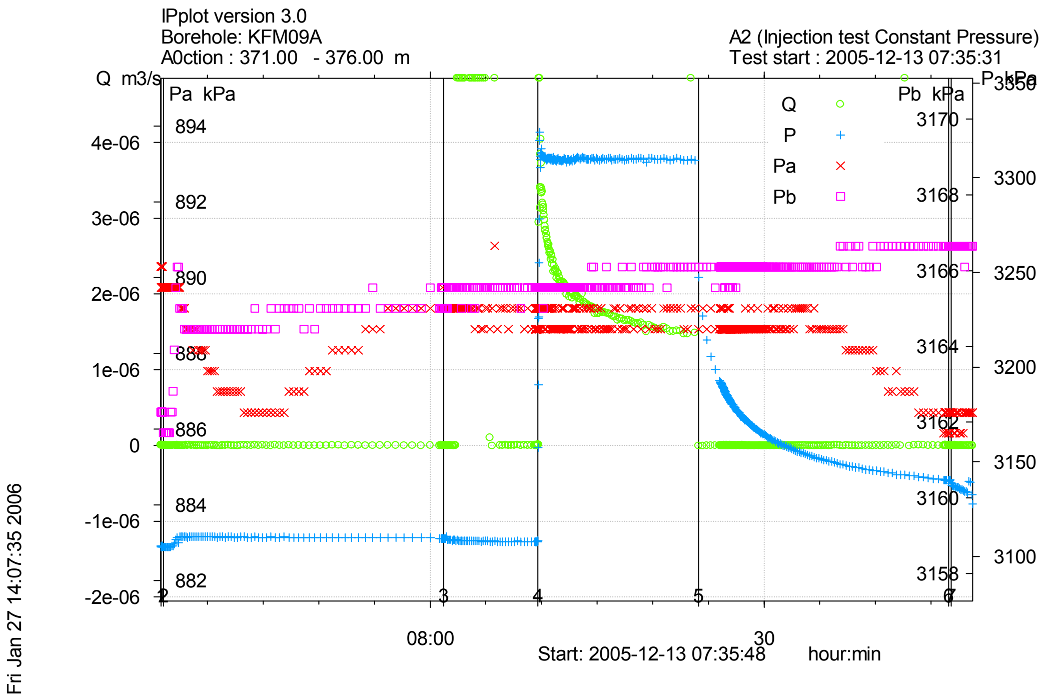


Figure A3-370. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 371.0-376.0 m in borehole KFM09A.*

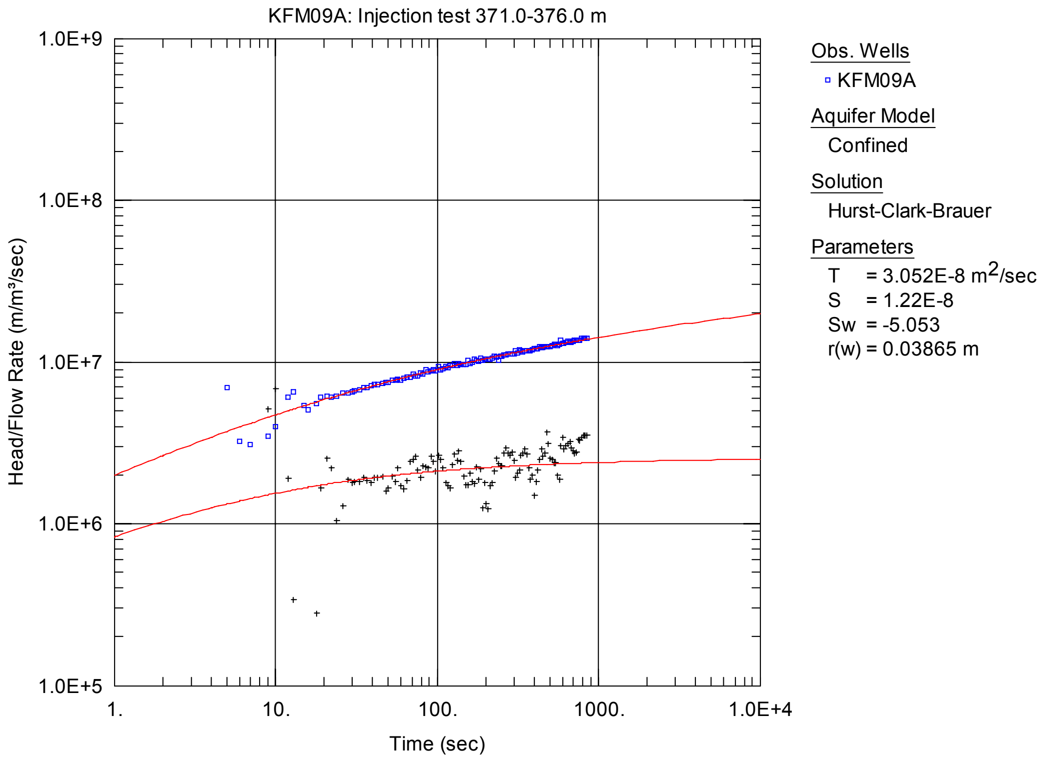


Figure A3-371. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 371.0-376.0 m in KFM09A.*

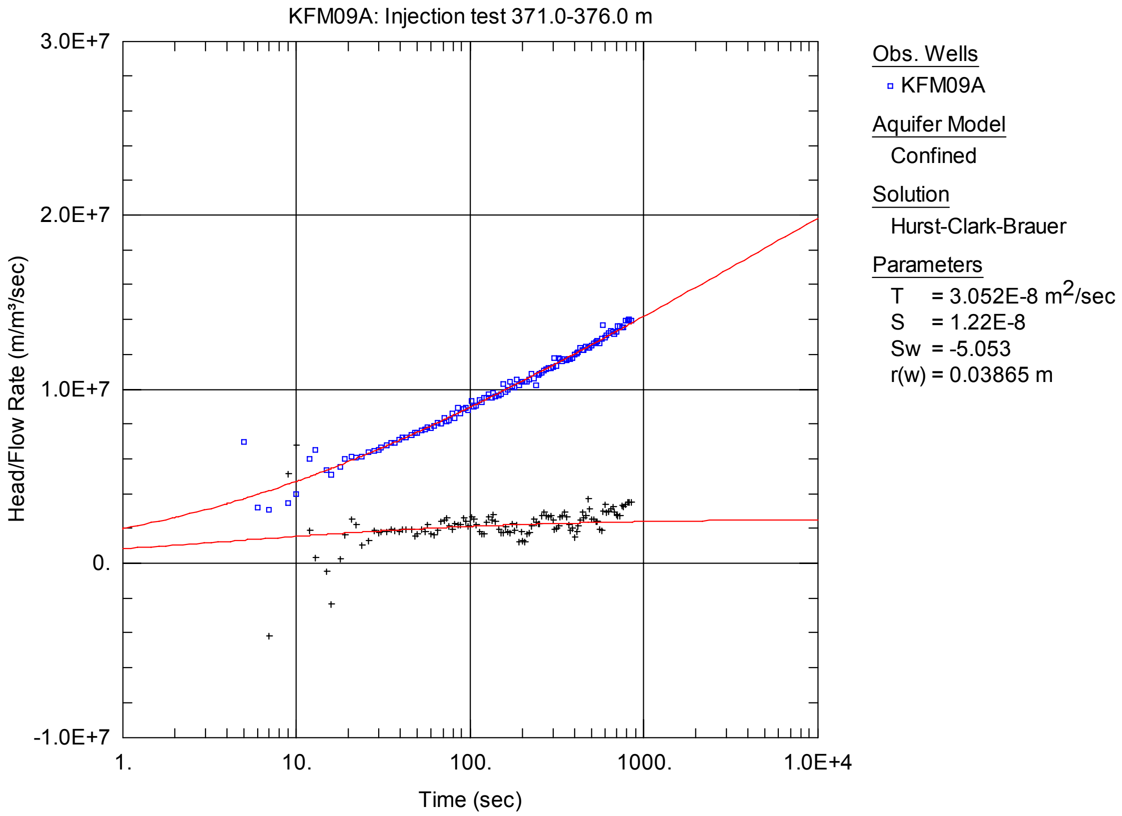


Figure A3-372. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 371.0-376.0 m in KFM09A.*

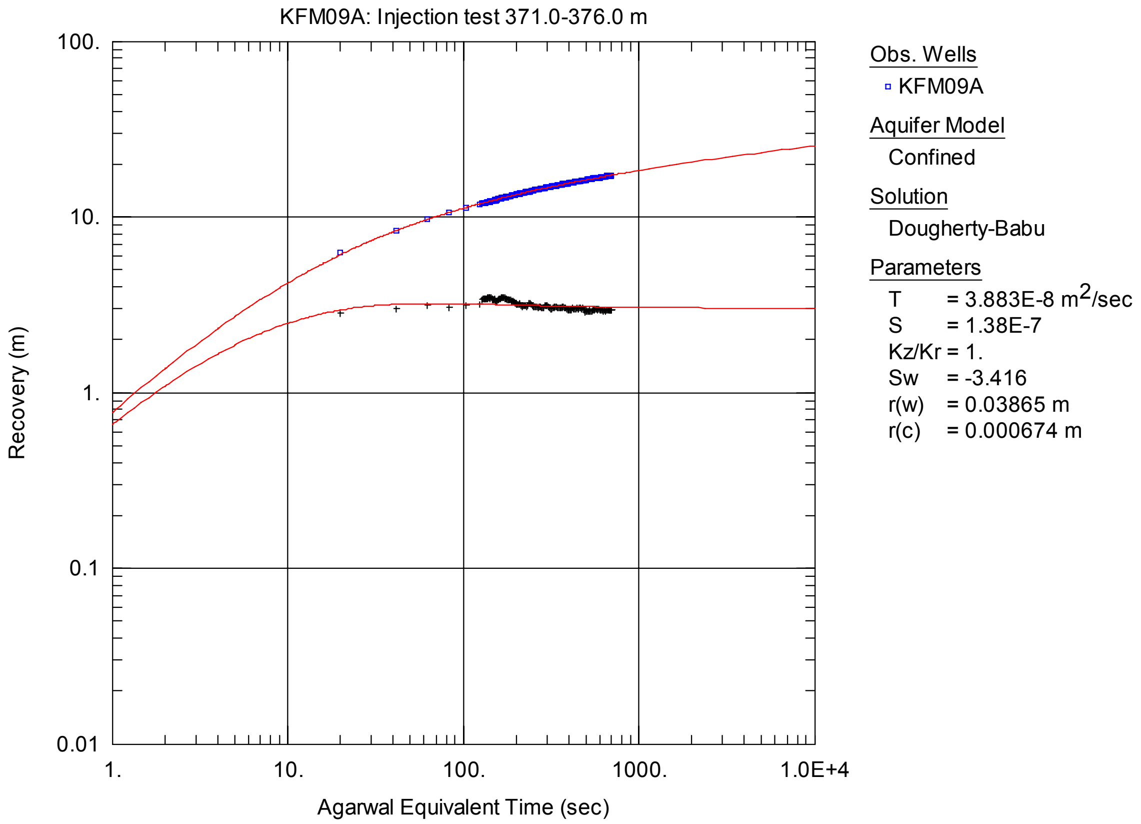


Figure A3-373. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 371.0-376.0 m in KFM09A.*

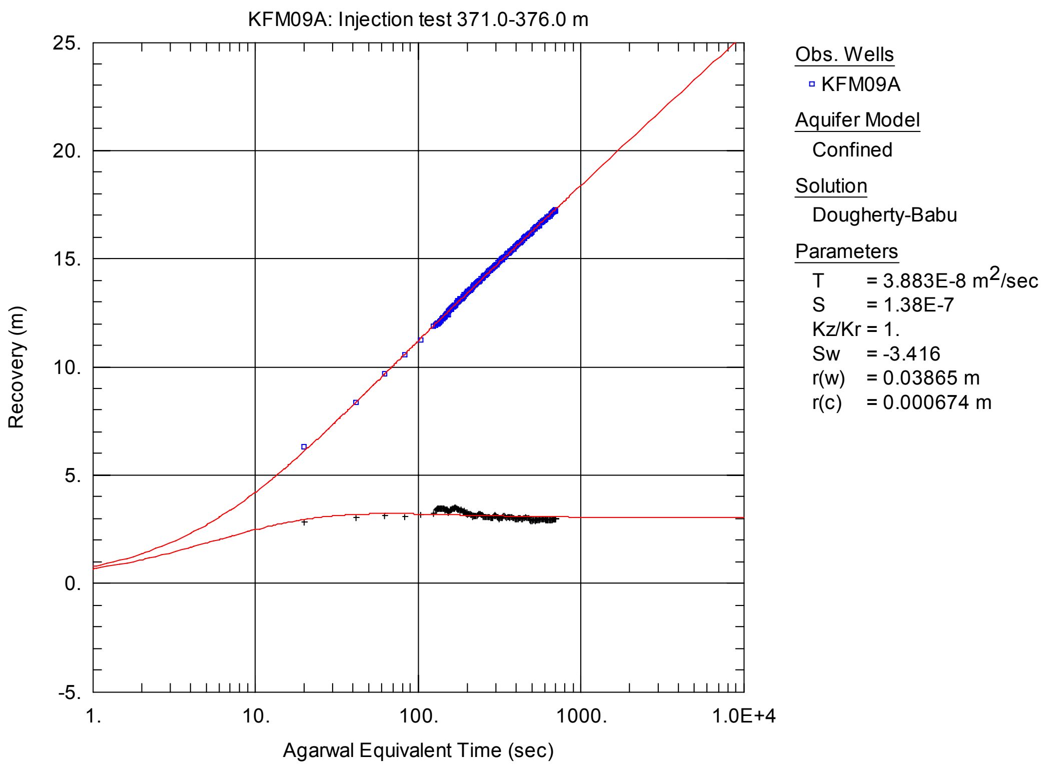


Figure A3-374. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 371.0-376.0 m in KFM09A.*

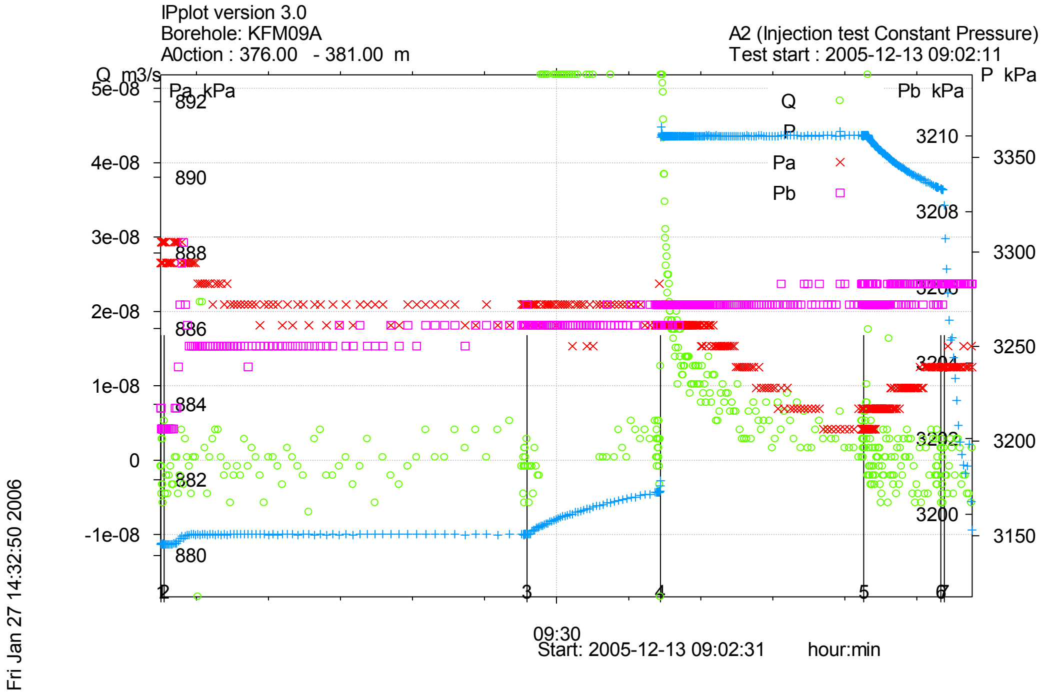


Figure A3-375. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 376.0-381.0 m in borehole KFM09A.

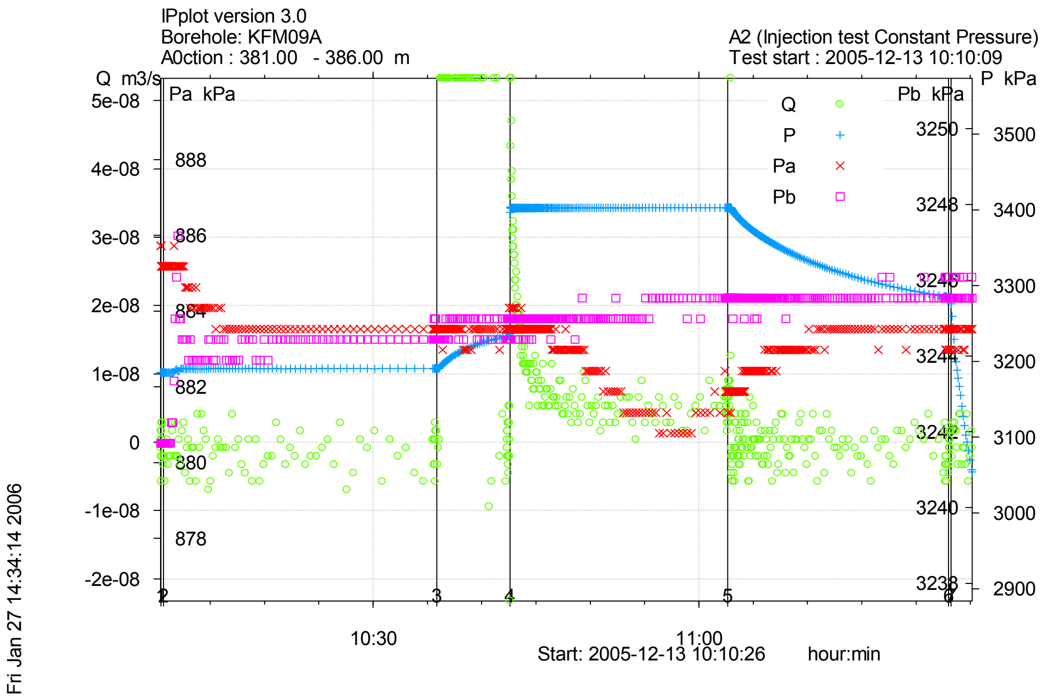


Figure A3-376. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 381.0-386.0 m in borehole KFM09A.

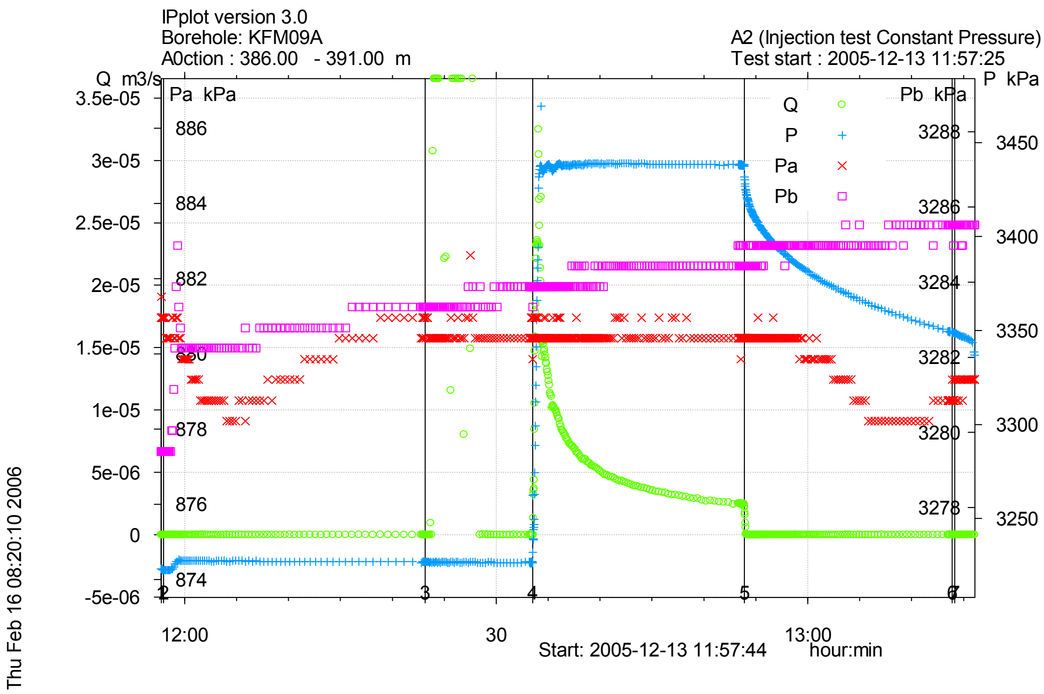


Figure A3-377. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 386.0-391.0 m in borehole KFM09A.

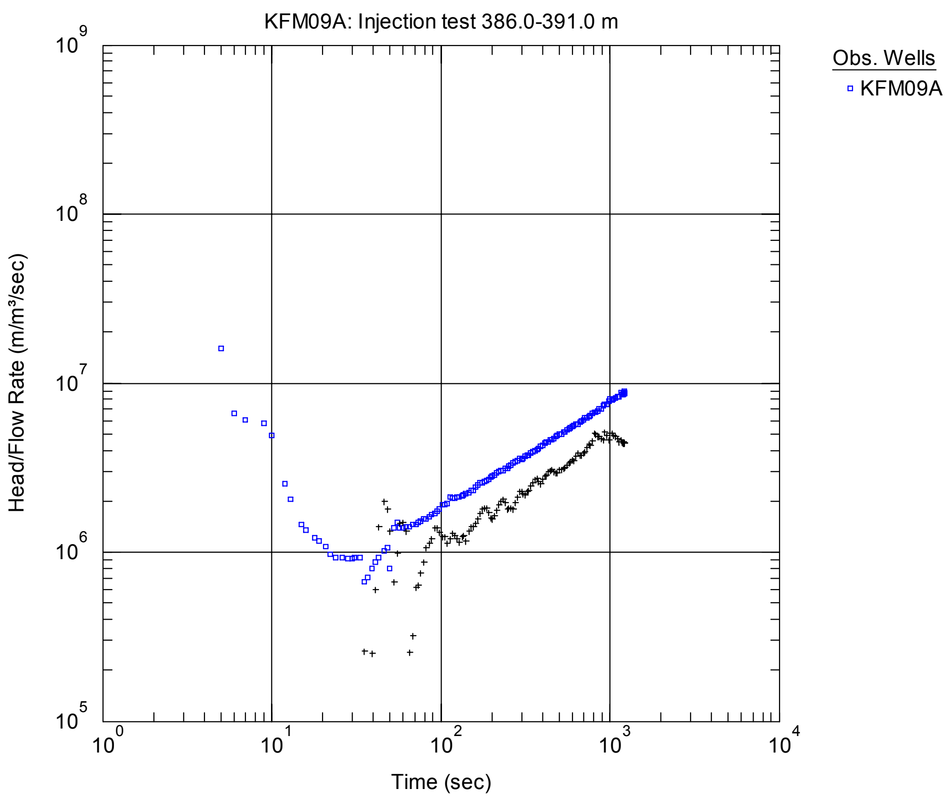


Figure A3-378. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 386.0-391.0 m in KFM09A

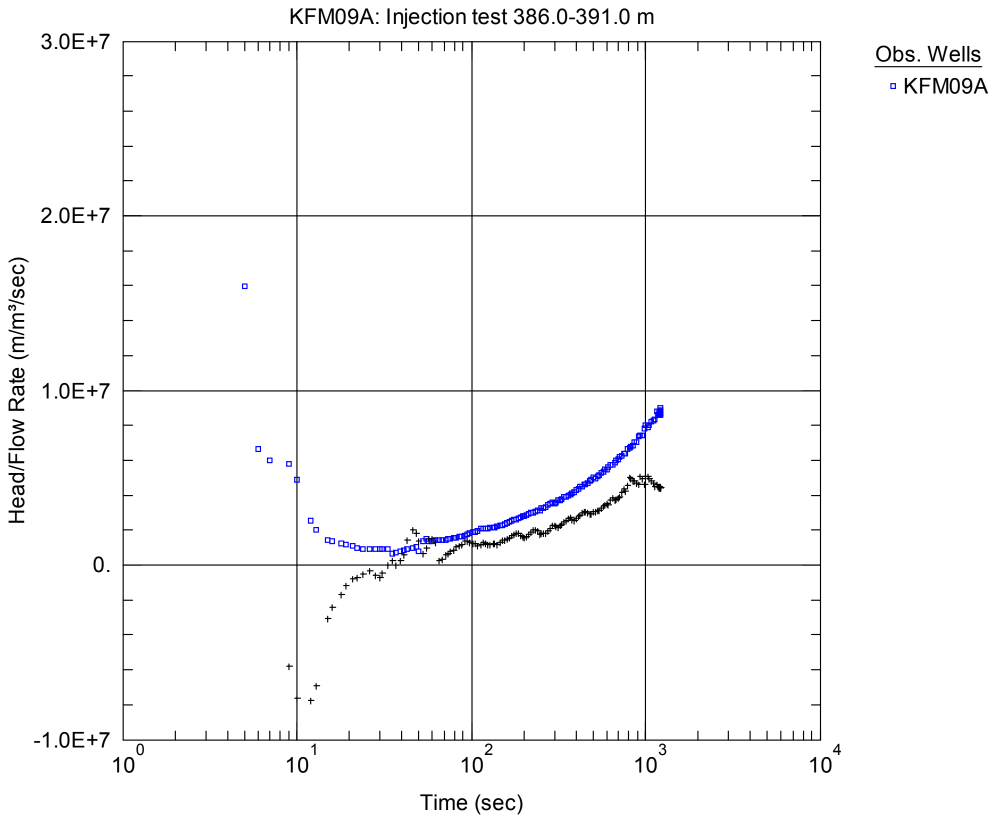


Figure A3-379. Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 386.0-391.0 m in KFM09A.

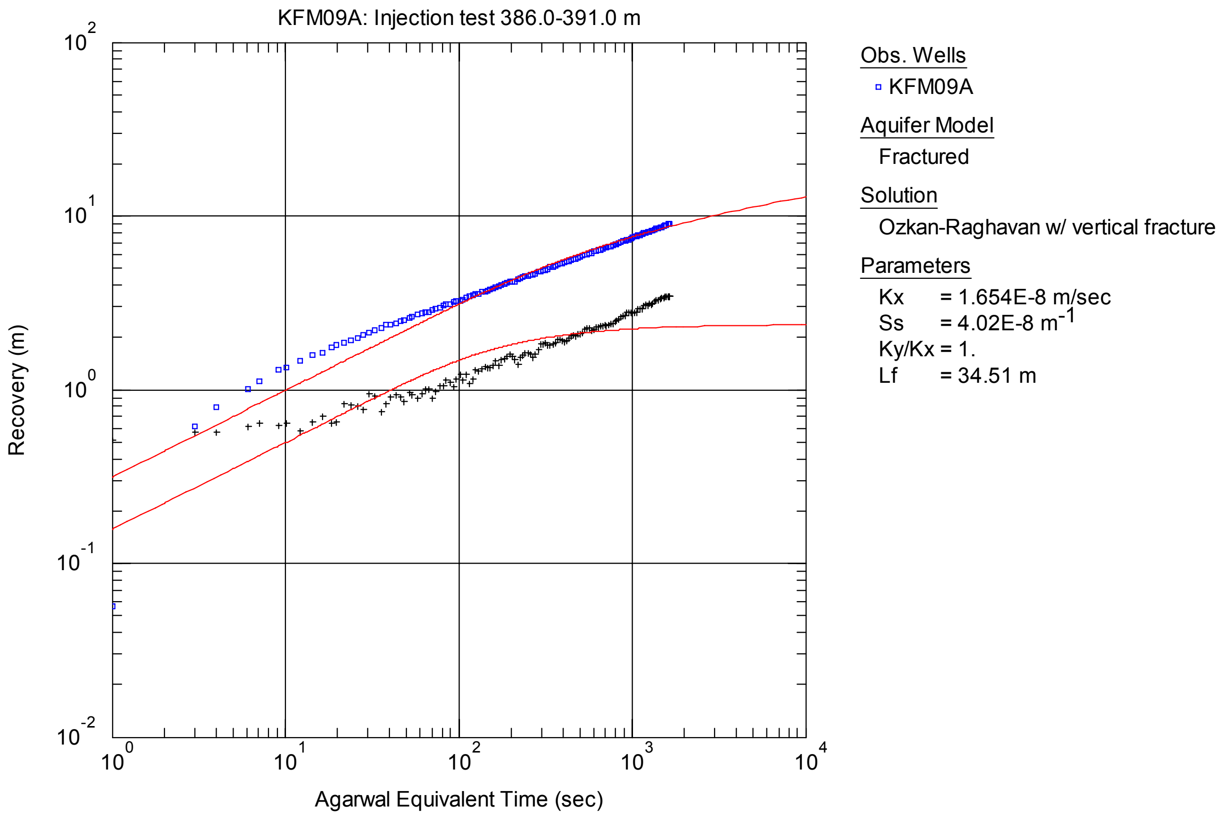


Figure A3-380. Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 386.0-391.0 m in KFM09A.

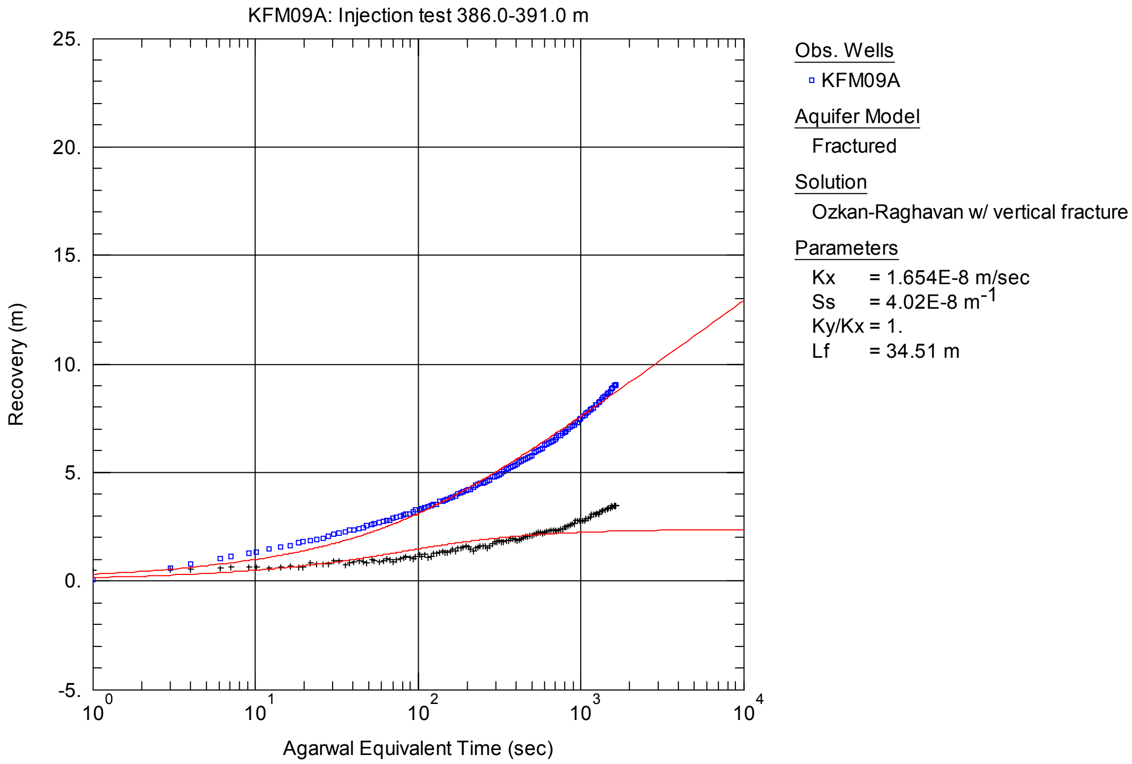


Figure A3-381. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 386.0-391.0 m in KFM09A.*

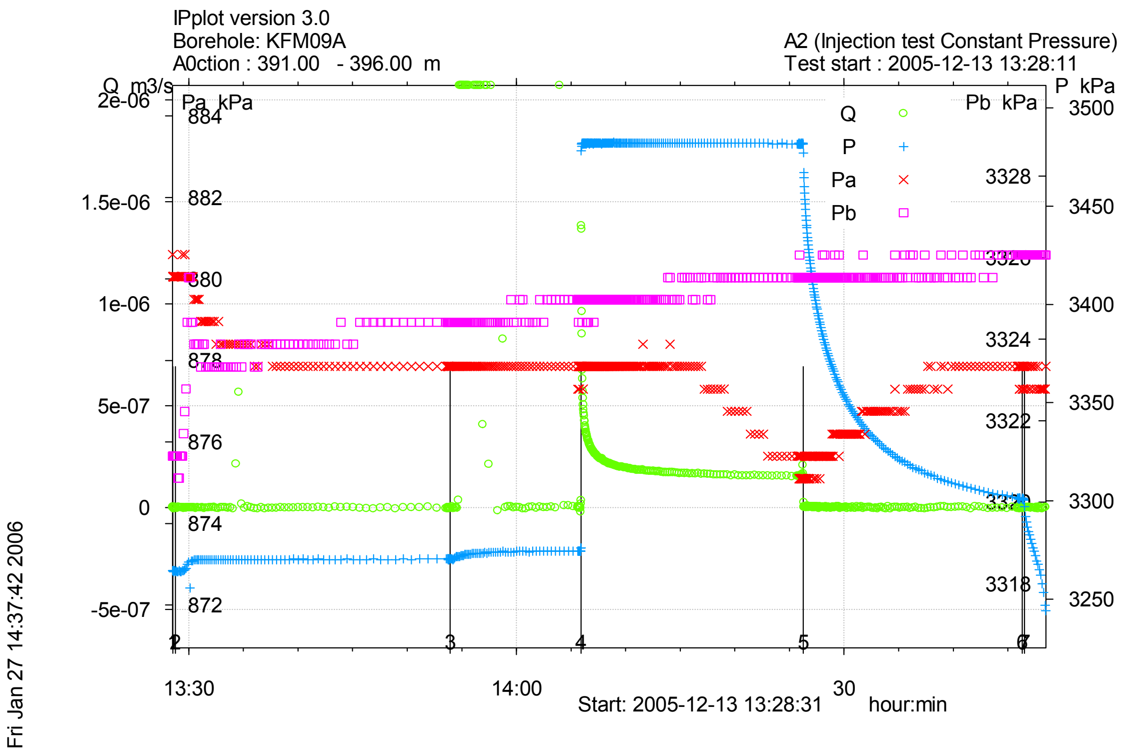


Figure A3-382. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 391.0-396.0 m in borehole KFM09A.*

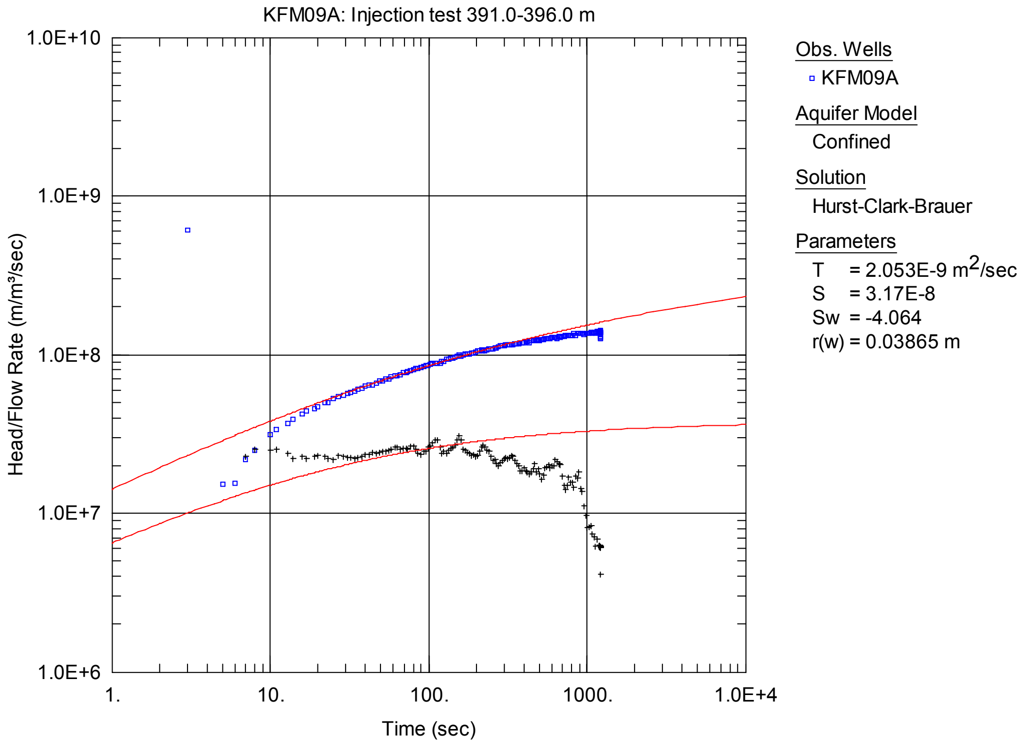


Figure A3-383. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 391.0-396.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for a pseudo-radial response.*

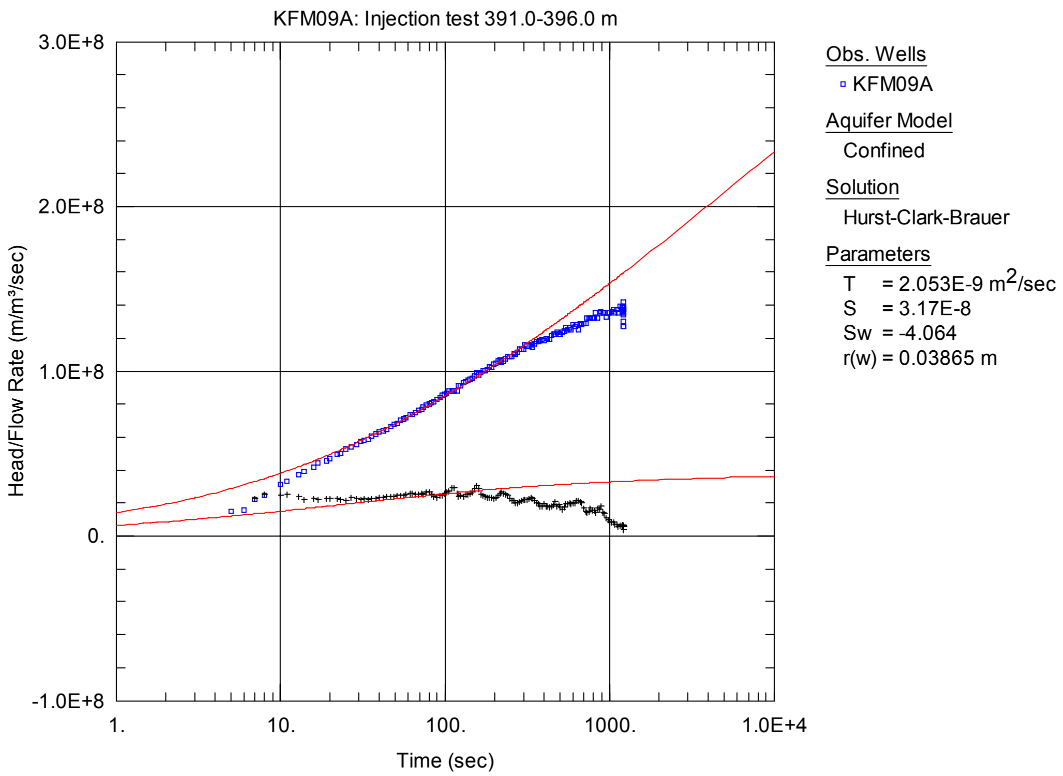


Figure A3-384. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 391.0-396.0 m in KFM09A This evaluation is made with the Hurst-Clark-Brauer model for a pseudo-radial response.*

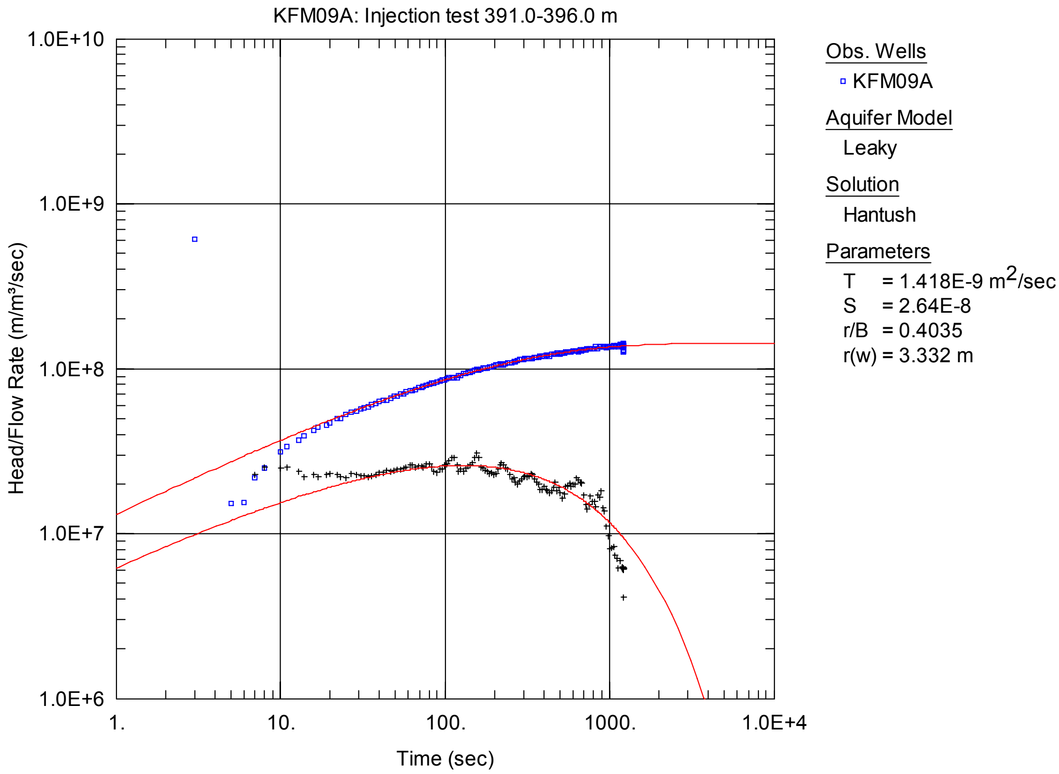


Figure A3-385. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 391.0-396.0 m in KFM09A This evaluation is made with the Hantush model for a pseudo-spherical response.*

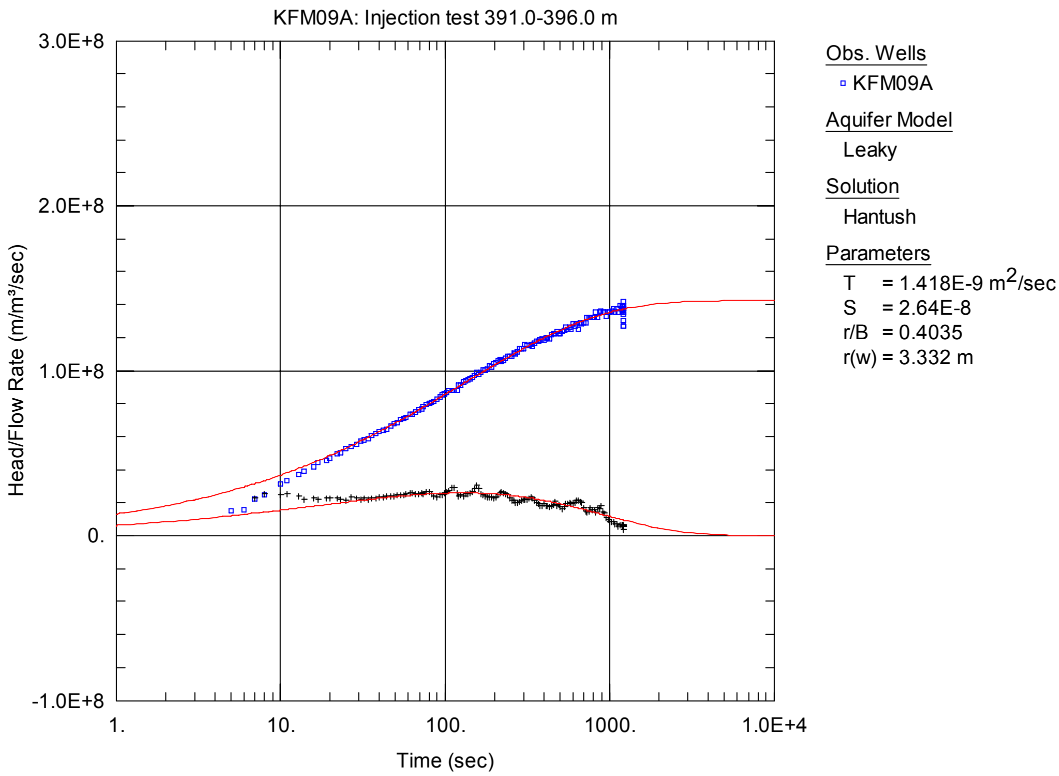


Figure A3-386. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 391.0-396.0 m in KFM09A This evaluation is made with the Hantush model for a pseudo-spherical response.*

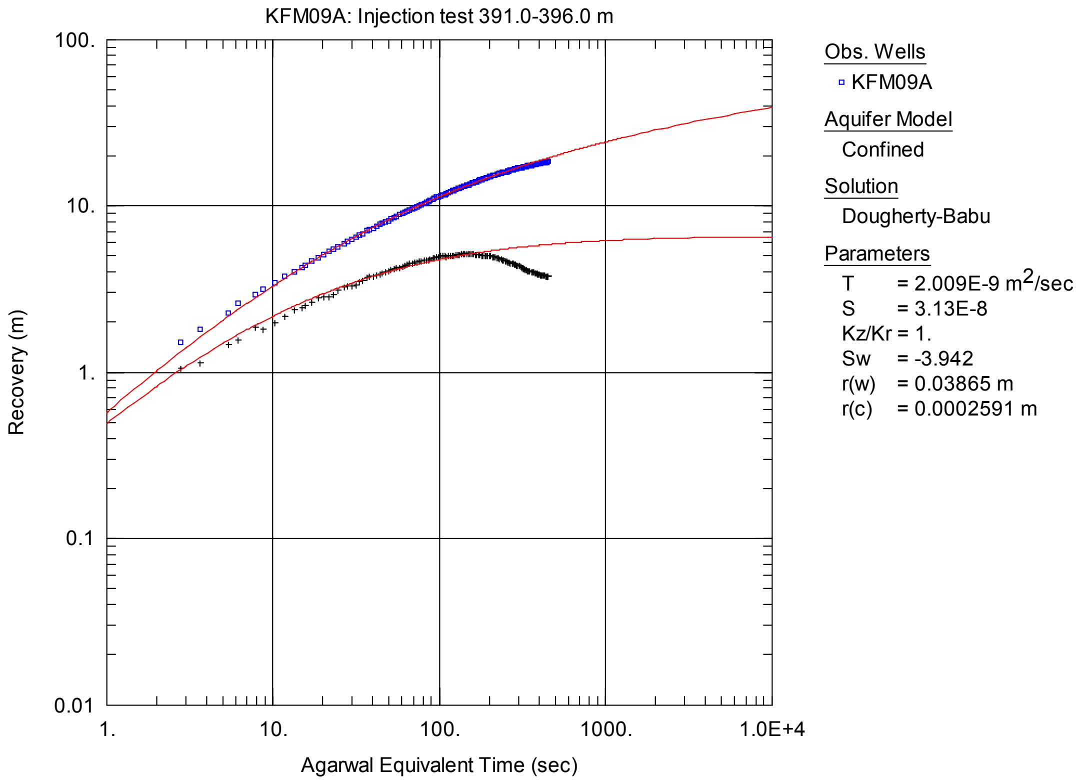


Figure A3-387. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 391.0-396.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

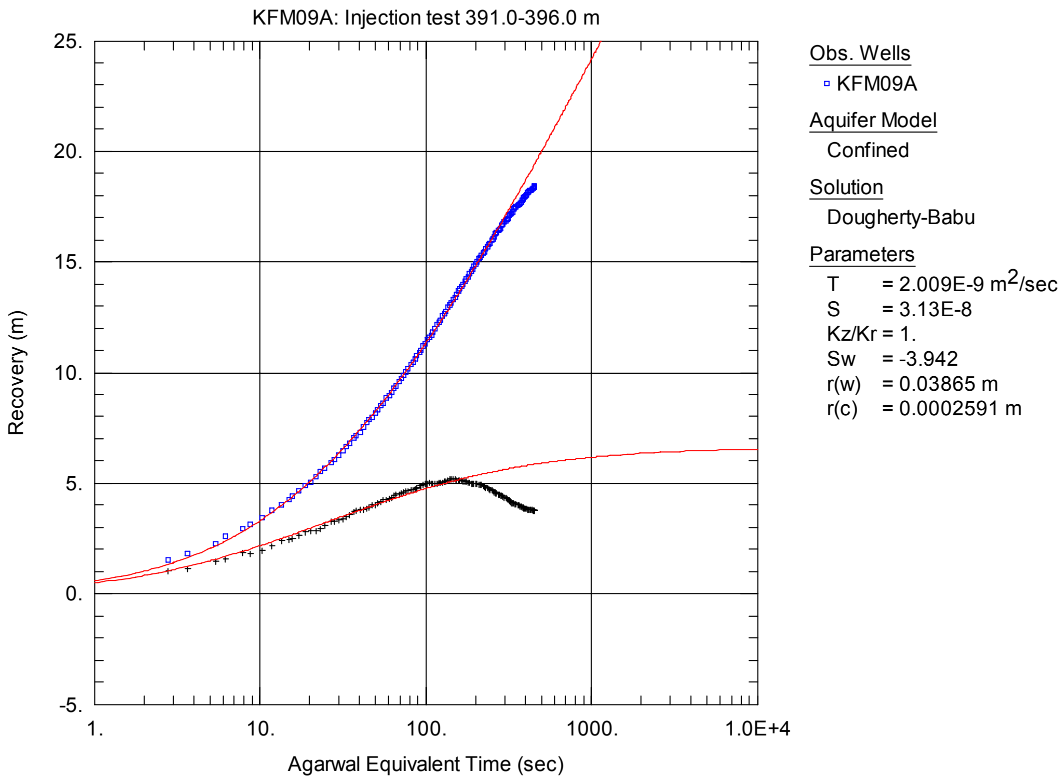


Figure A3-388. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 391.0-396.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

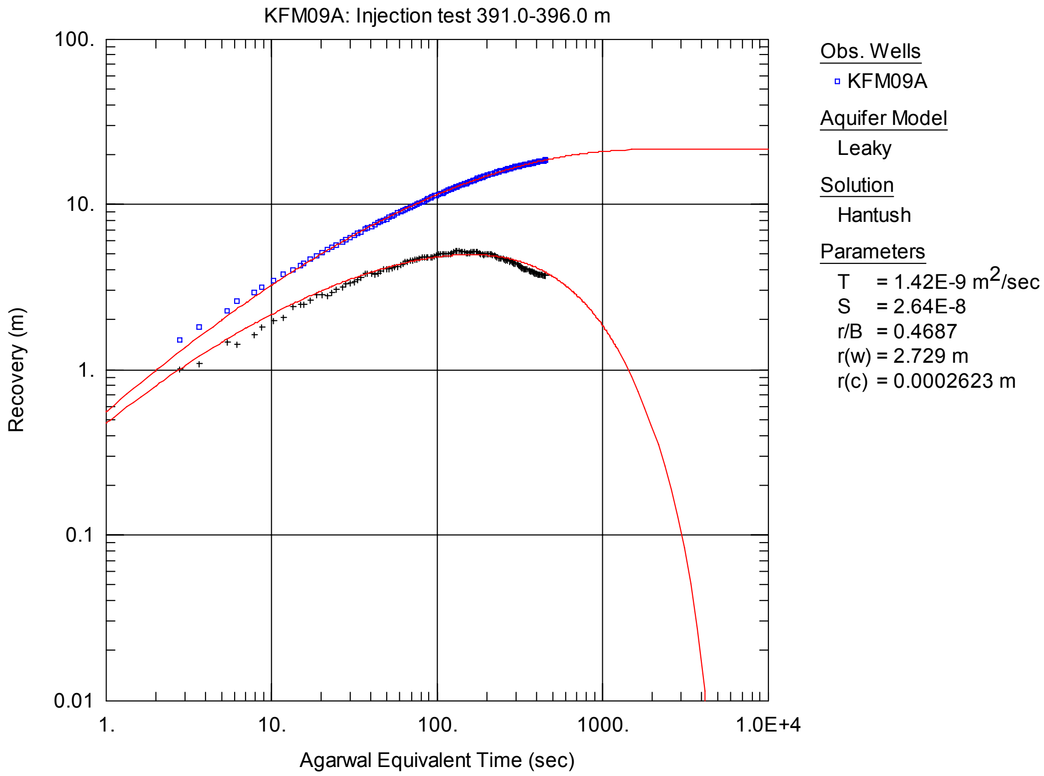


Figure A3-389. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 391.0-396.0 m in KFM09A. This evaluation is made with the Hantush model for a pseudo-spherical response.*

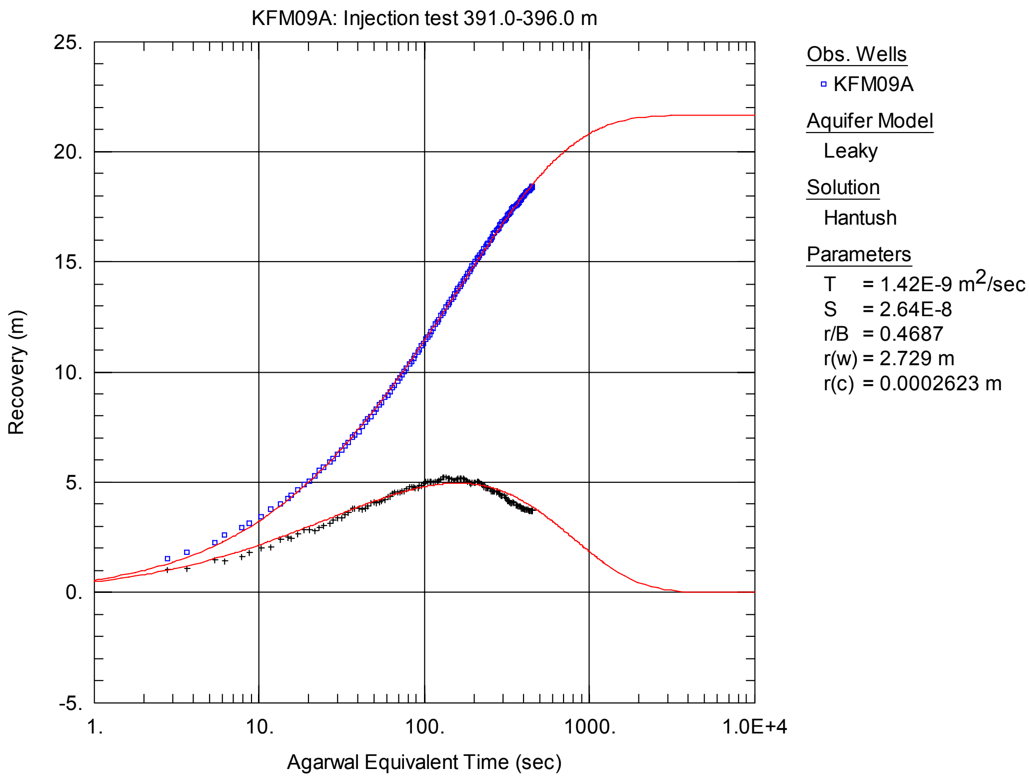


Figure A3-390. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 391.0-396.0 m in KFM09A. This evaluation is made with the Hantush model for a pseudo-spherical response.*

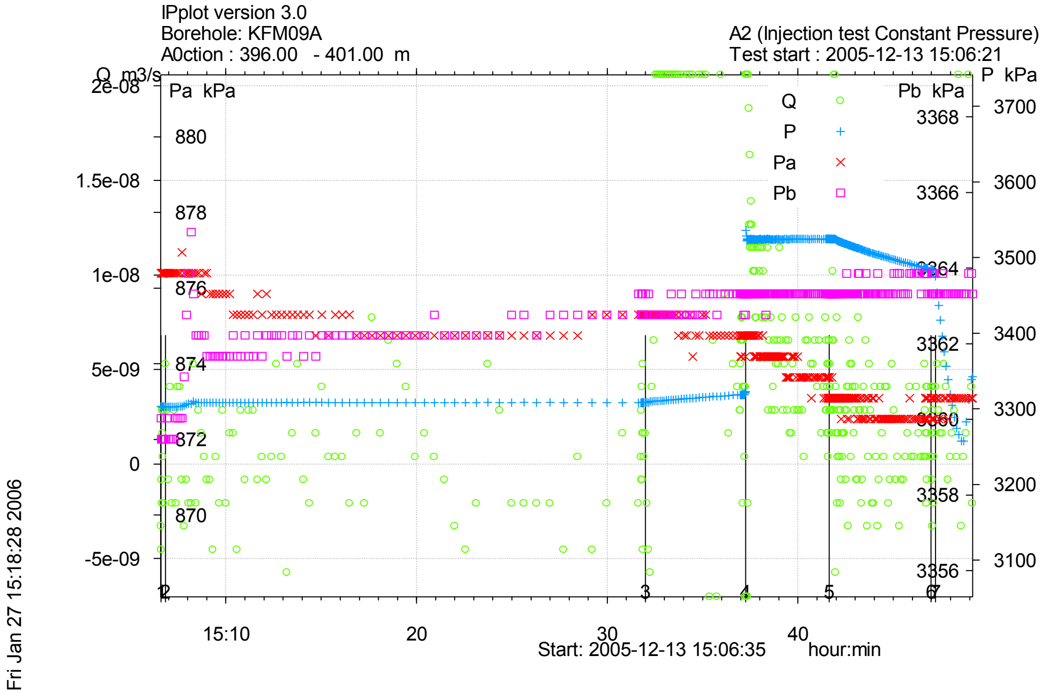


***Figure A3-391.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 396.0-401.0 m in borehole KFM09A.*

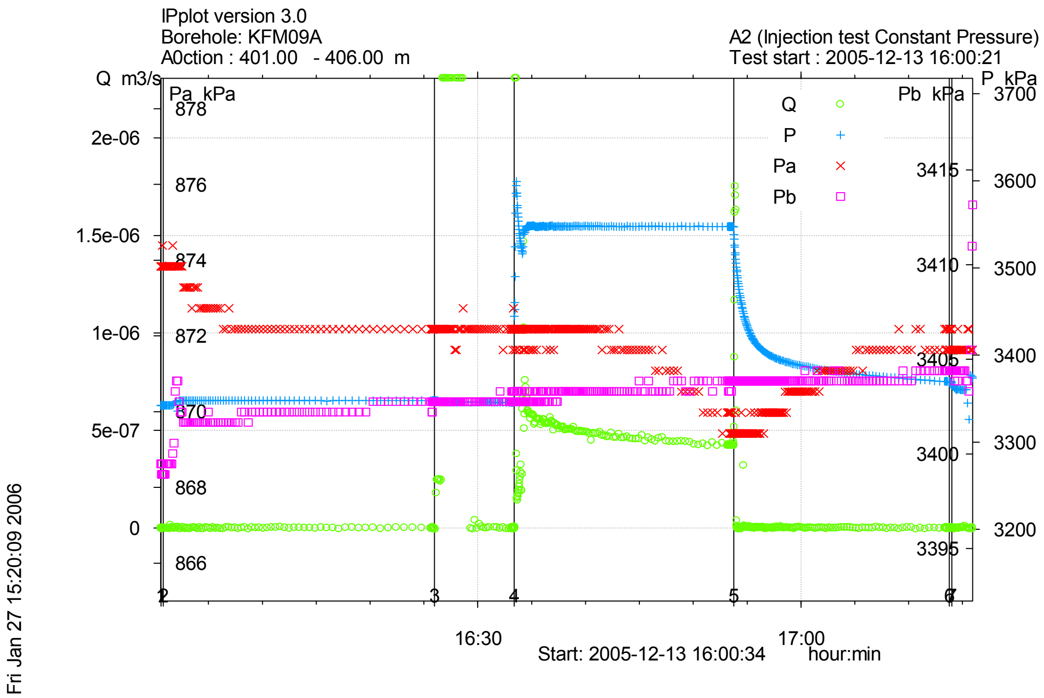


***Figure A3-392.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 401.0-406.0 m in borehole KFM09A.*

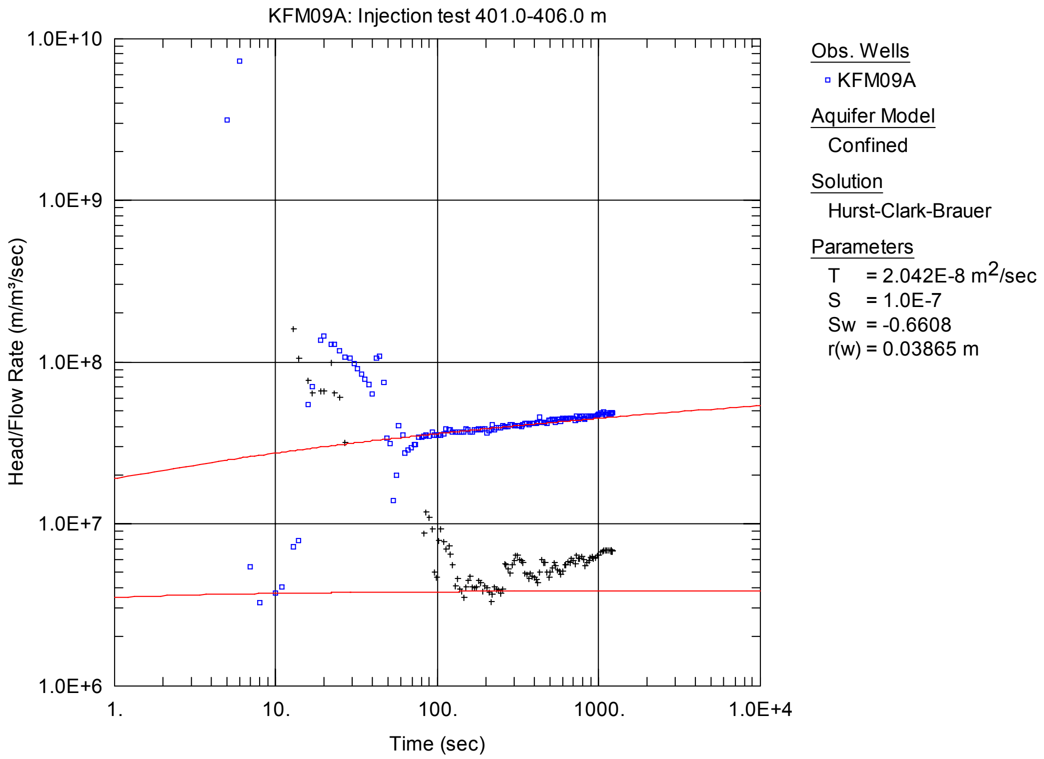


Figure A3-393. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 401.0-406.0 m in KFM09A.*

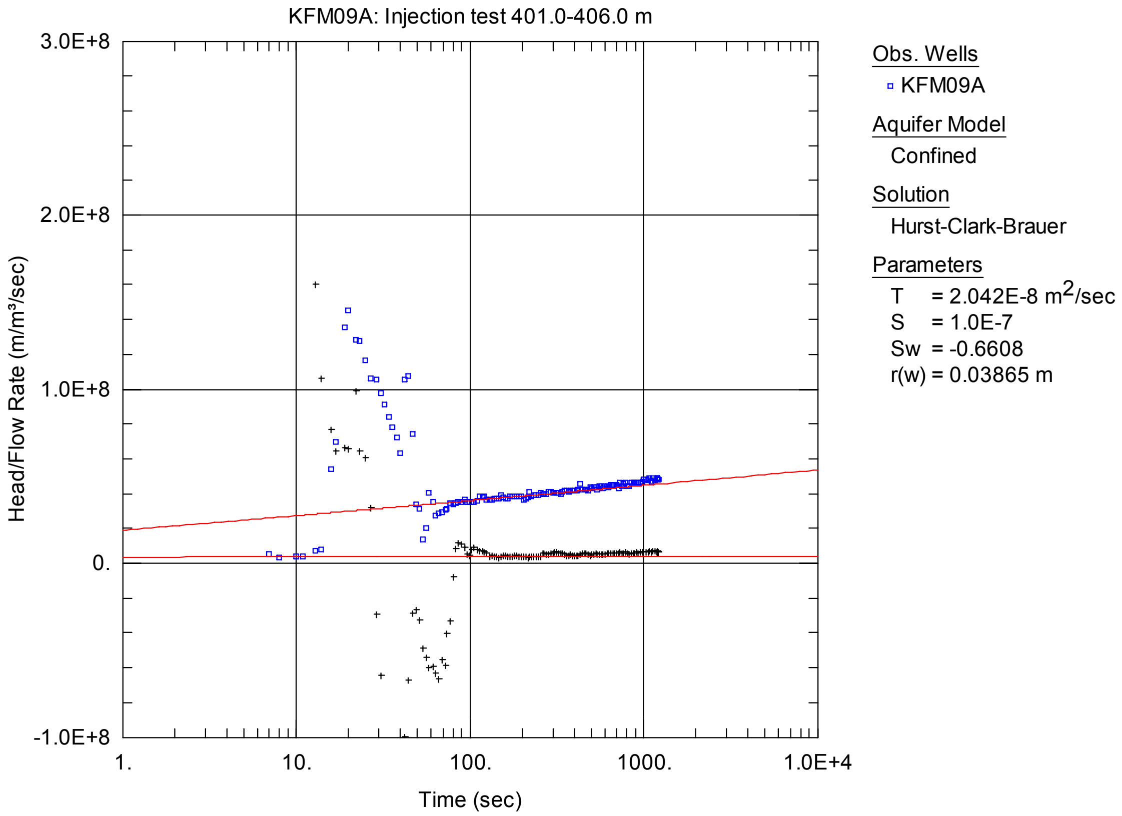


Figure A3-394. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 401.0-406.0 m in KFM09A.*

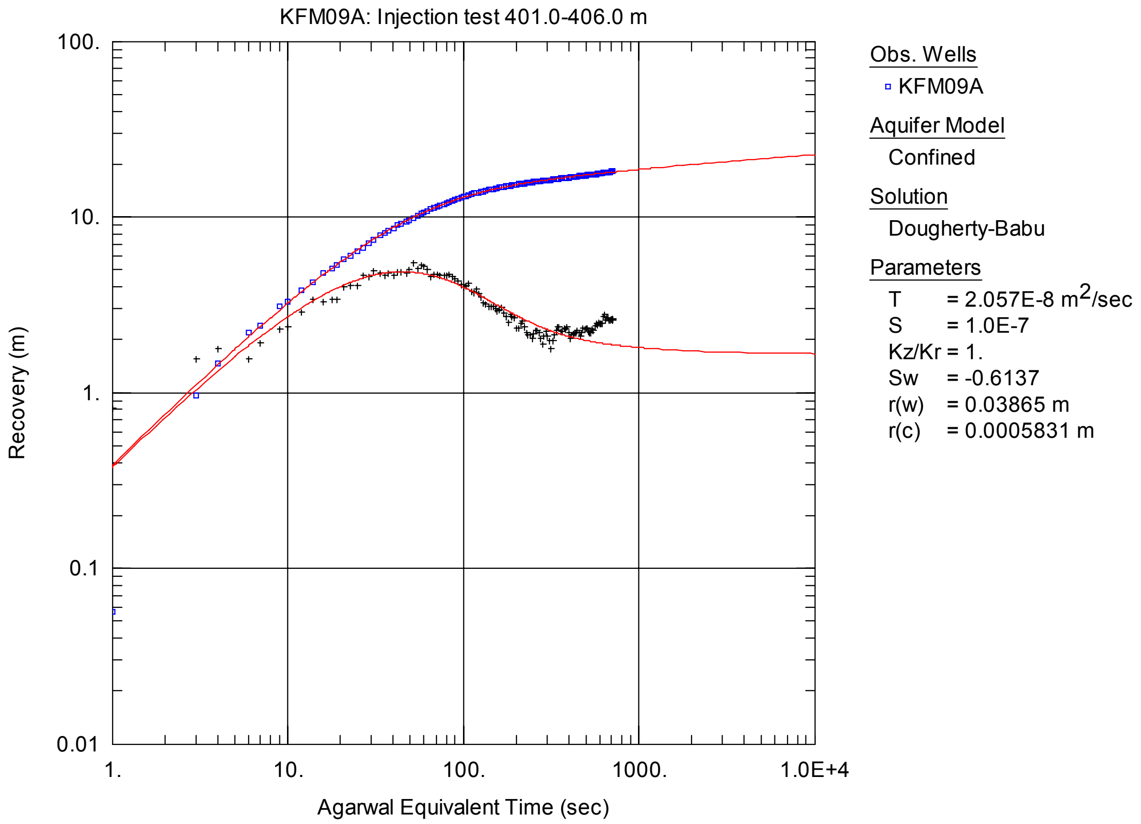


Figure A3-395. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 401.0-406.0 m in KFM09A.*

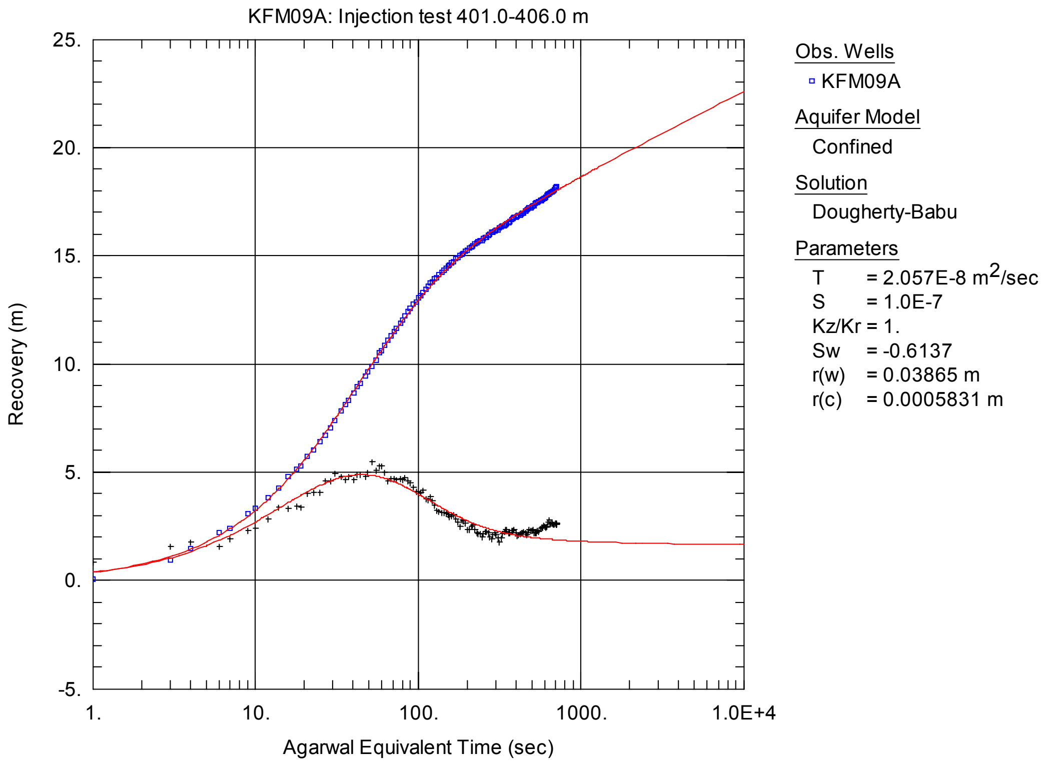


Figure A3-396. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 401.0-406.0 m in KFM09A.*

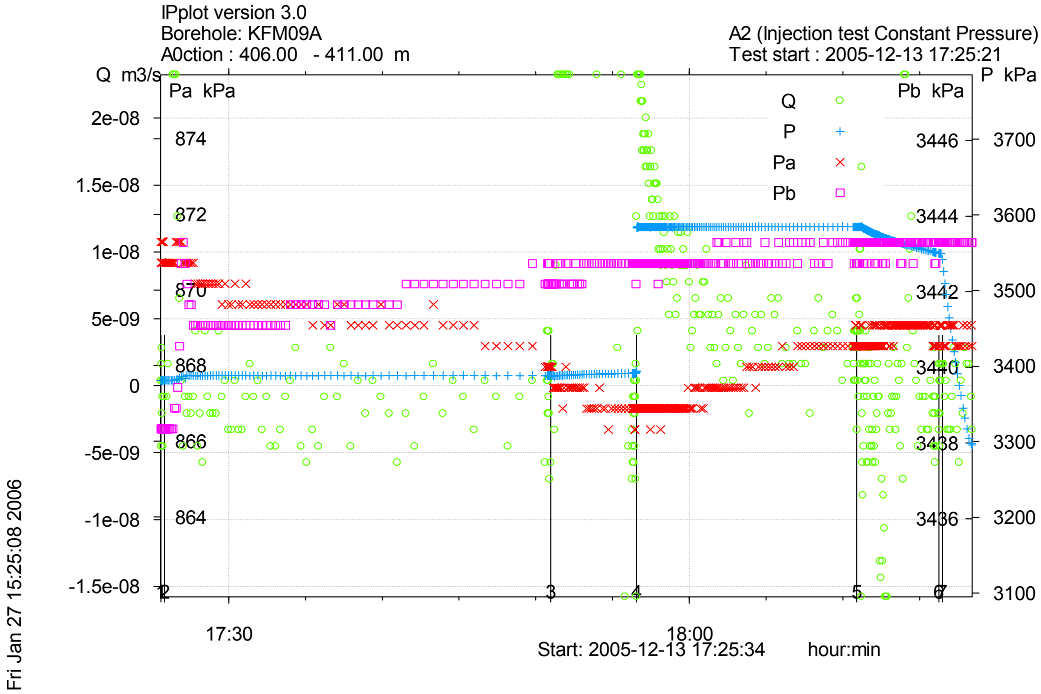


Figure A3-397. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 406.0-411.0 m in borehole KFM09A.*

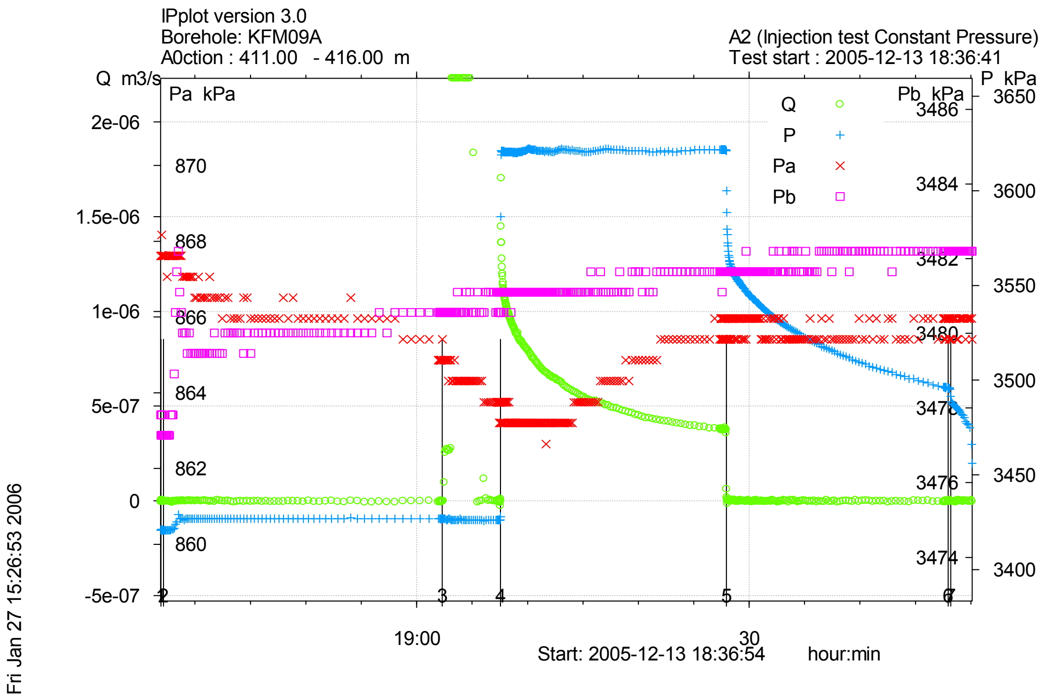


Figure A3-398. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 411.0-416.0 m in borehole KFM09A.*

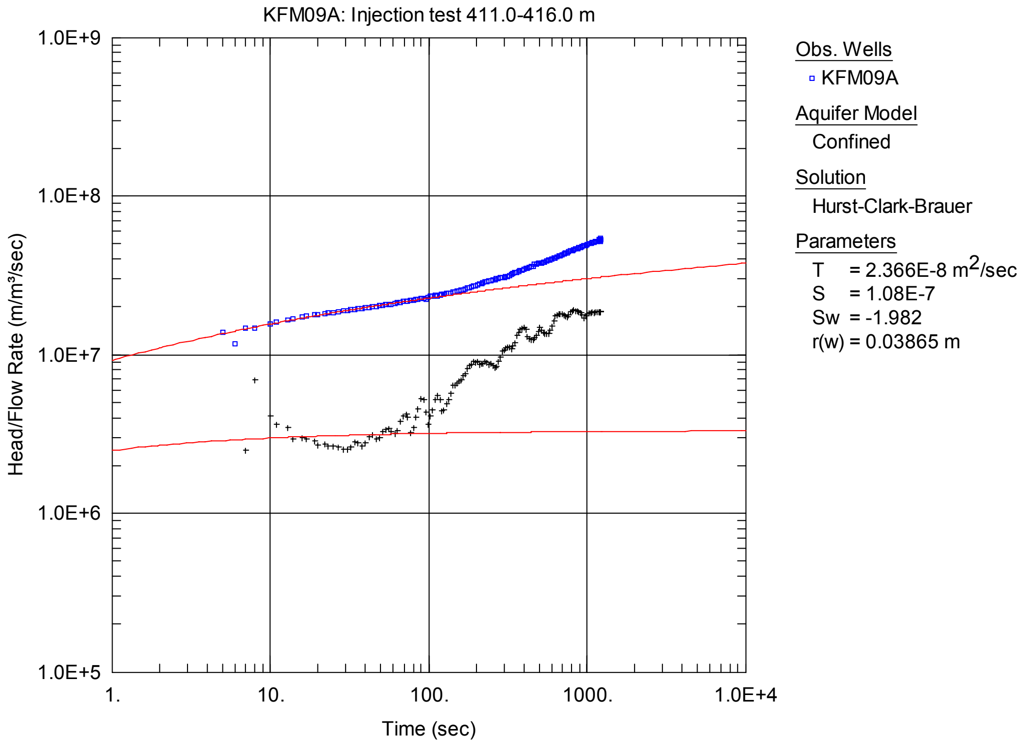


Figure A3-399. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 411.0-416.0 m in KFM09A. This plot shows a fit to the first of two different PRF:s during the injection period in this section.*

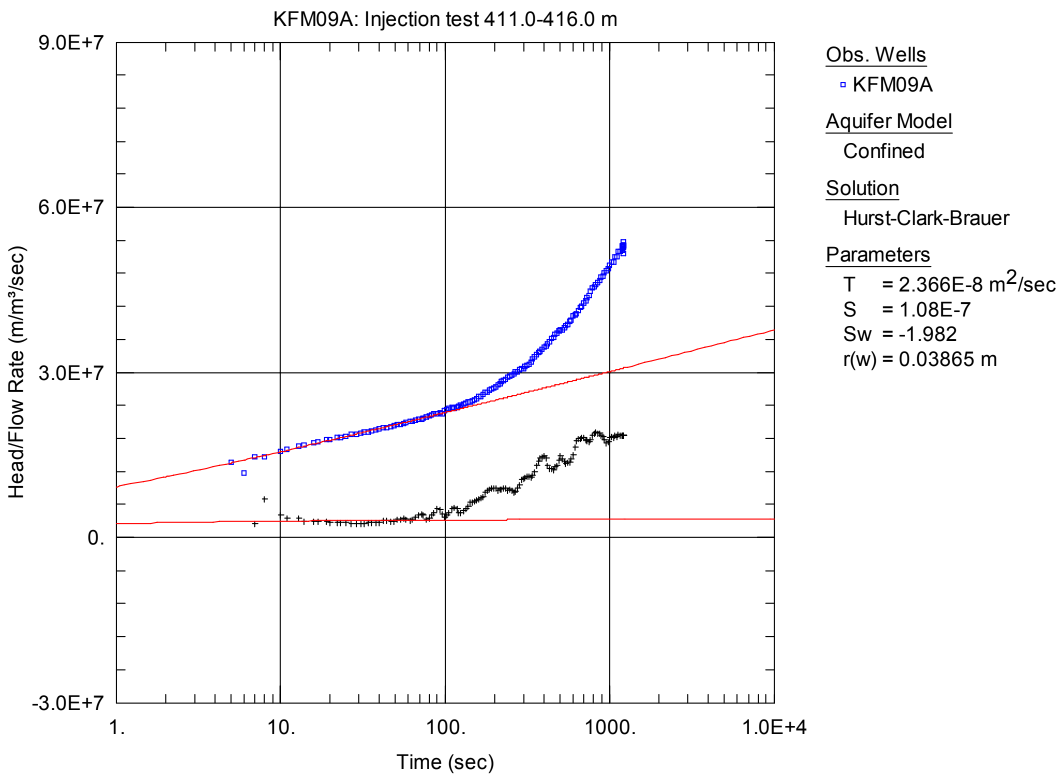


Figure A3-400. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 411.0-416.0 m in KFM09A. This plot shows a fit to the first of two different PRF:s during the injection period in this section.*

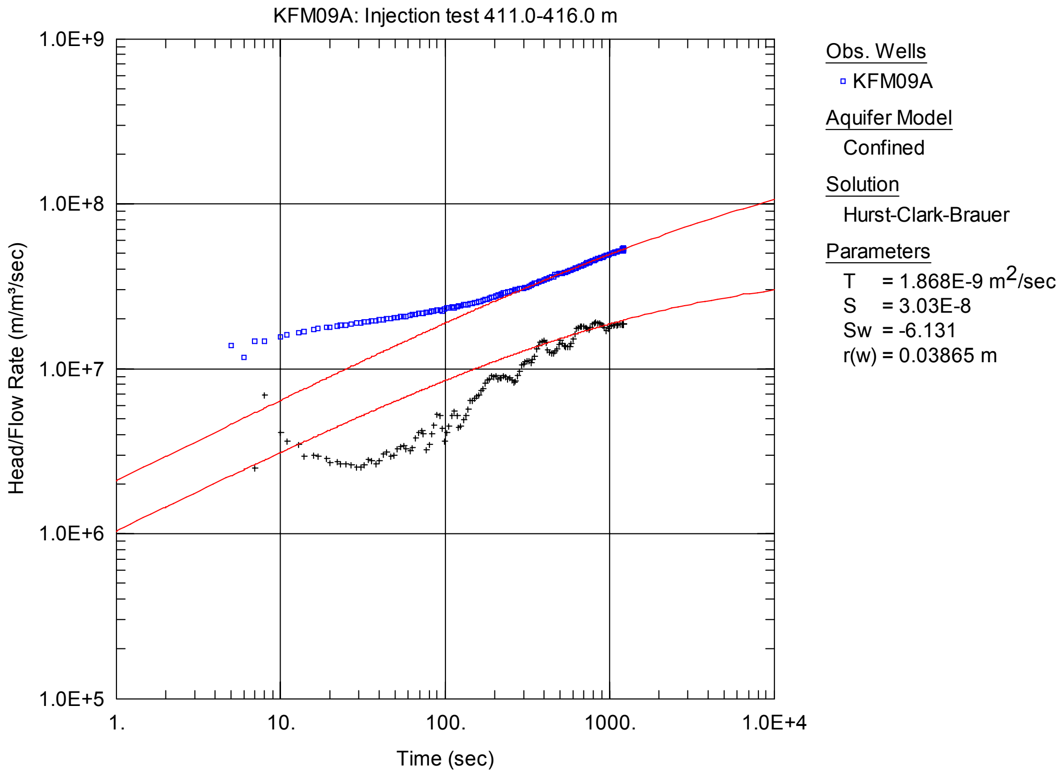


Figure A3-401. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 411.0-416.0 m in KFM09A. This plot shows a fit to the second of two different PRF:s during the injection period in this section.*

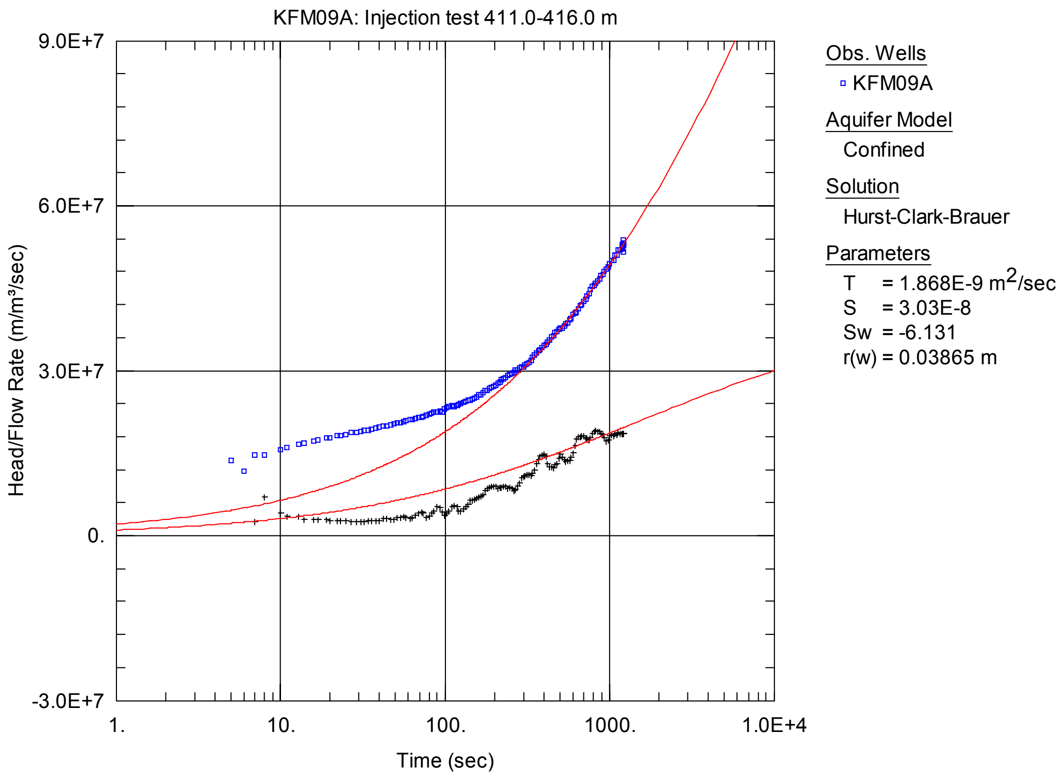


Figure A3-402. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 411.0-416.0 m in KFM09A. This plot shows a fit to the second of two different PRF:s during the injection period in this section.*

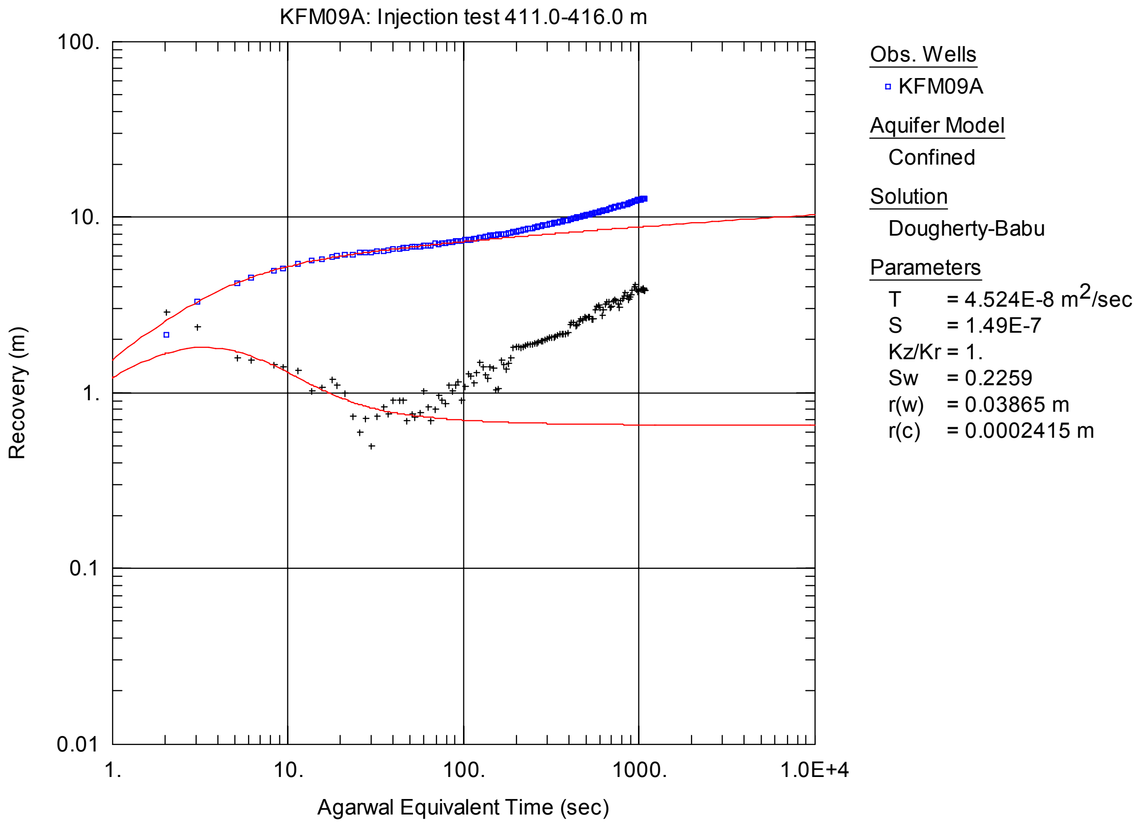


Figure A3-403. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 411.0-416.0 x m in KFM09A.*

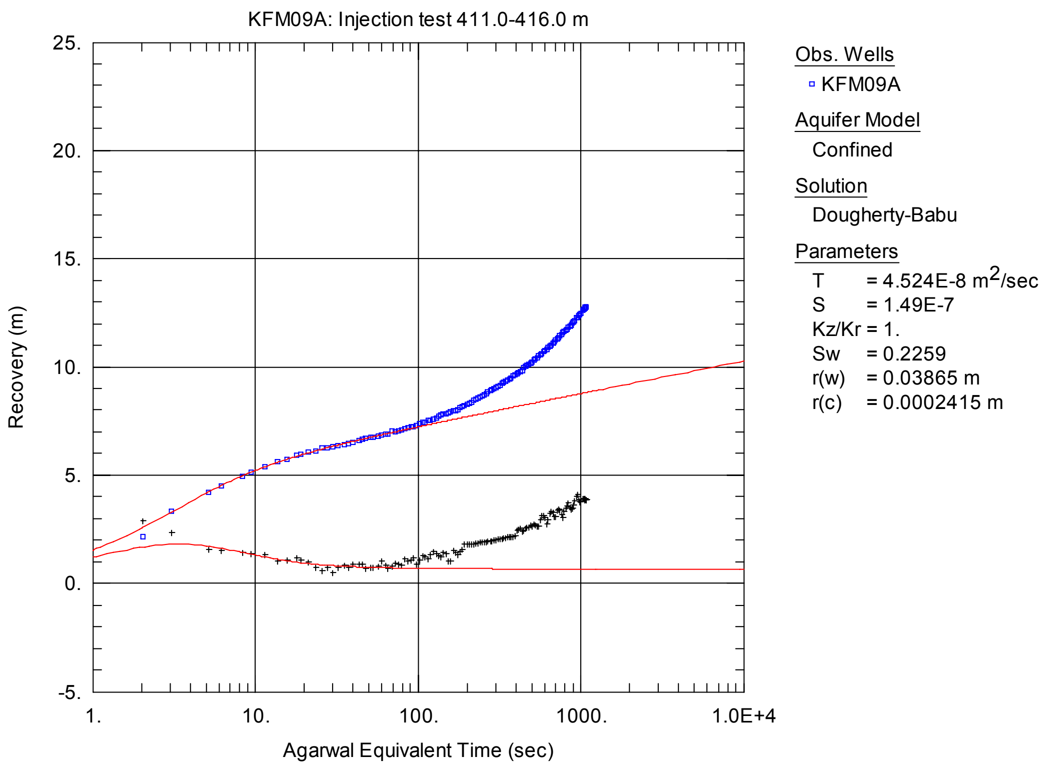


Figure A3-404. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 411.0-416.0 m in KFM09A.*

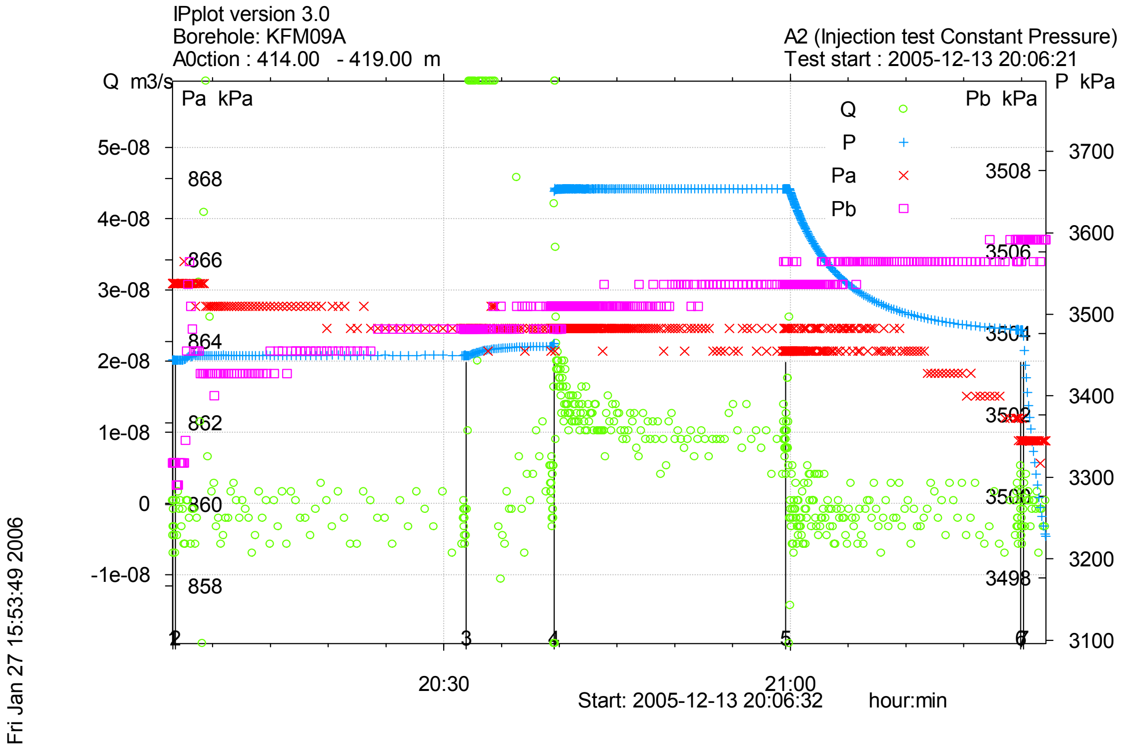


__Figure A3-405.__ Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 414.0-419.0 m in borehole KFM09A.

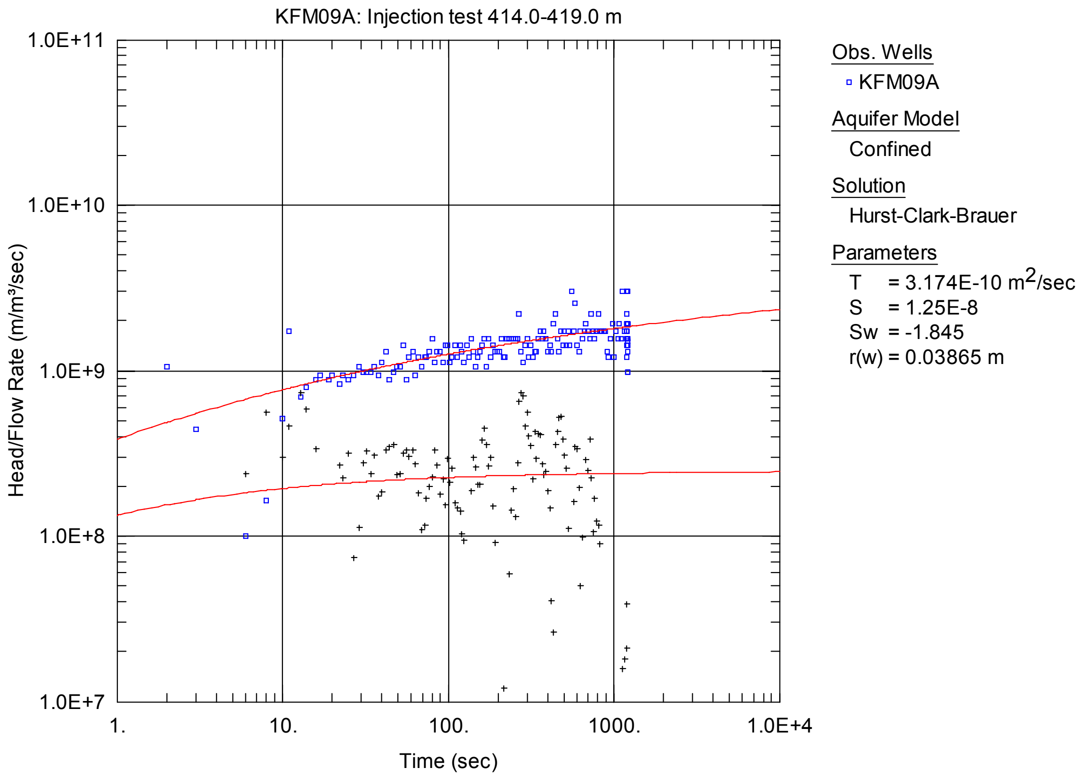


__Figure A3-406.__ Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 414.0-419.0 m in KFM09A.

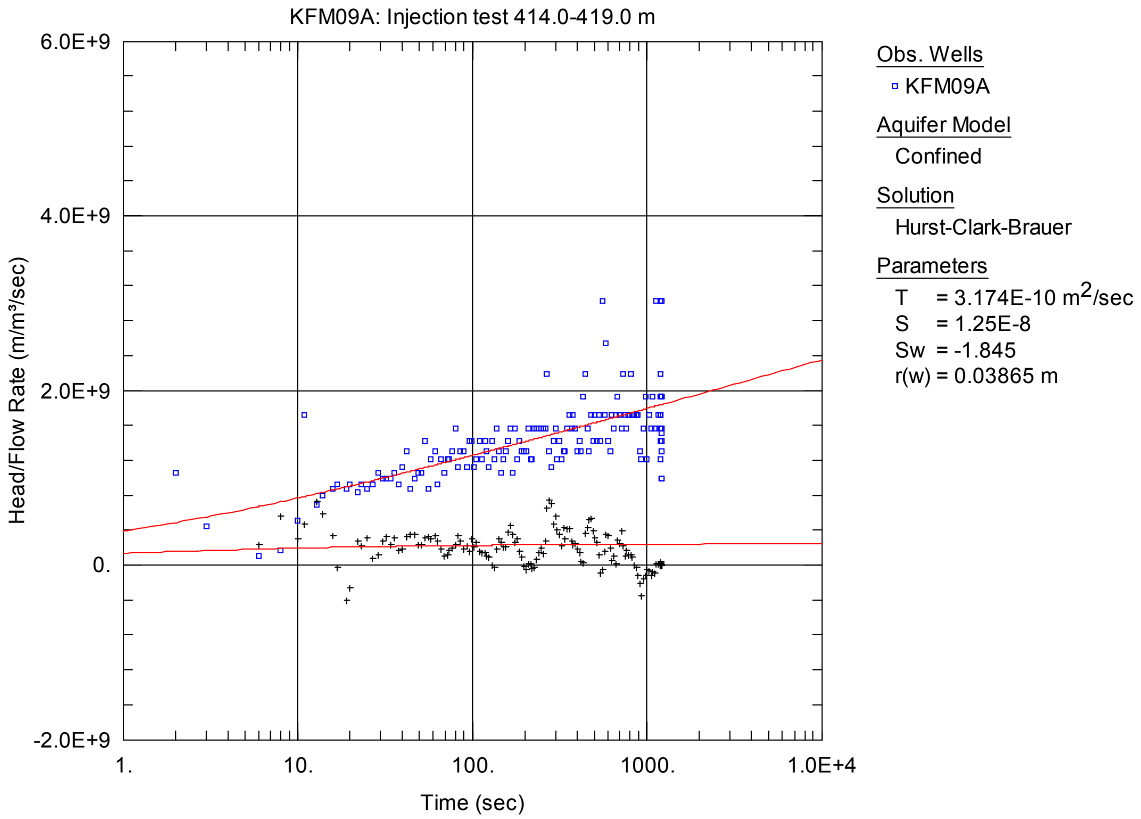


Figure A3-407. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 414.0-419.0 m in KFM09A.*

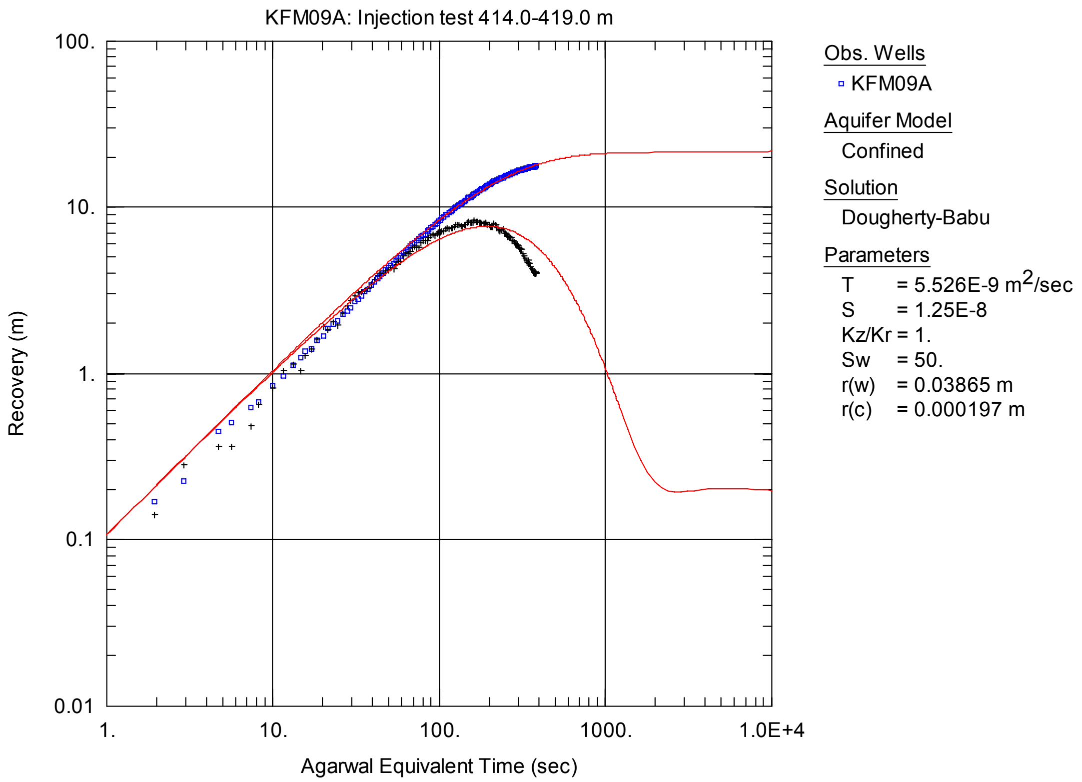


Figure A3-408. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 414.0-419.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.*

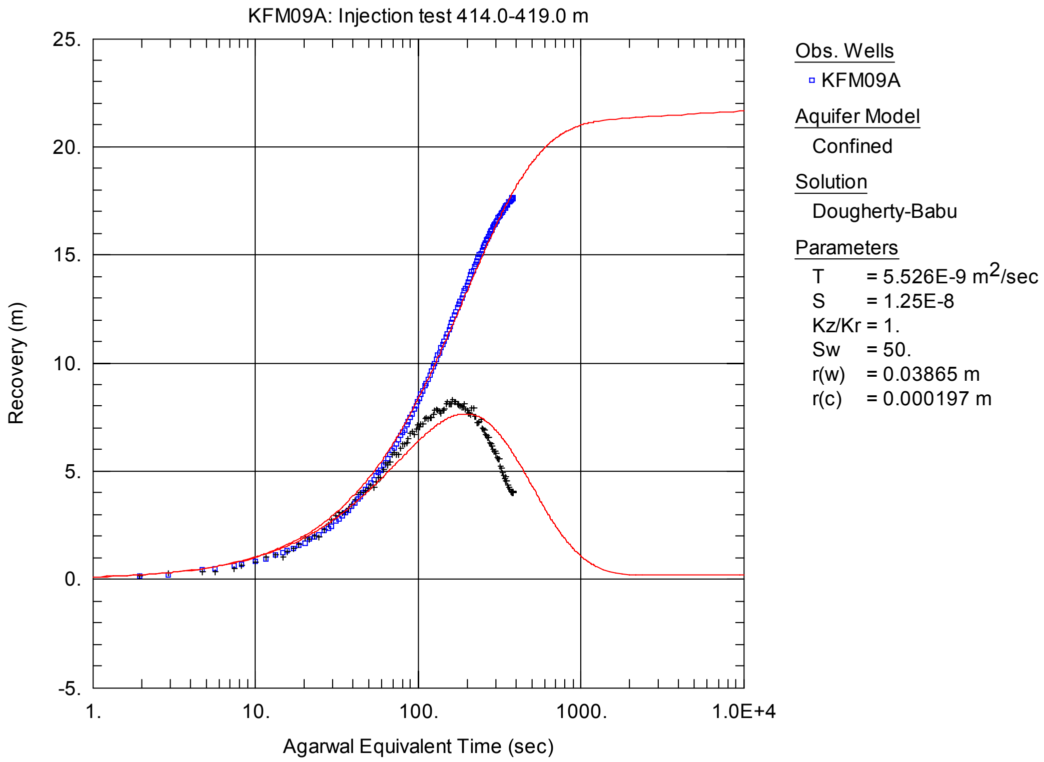


Figure A3-409. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 414.0-419.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.*

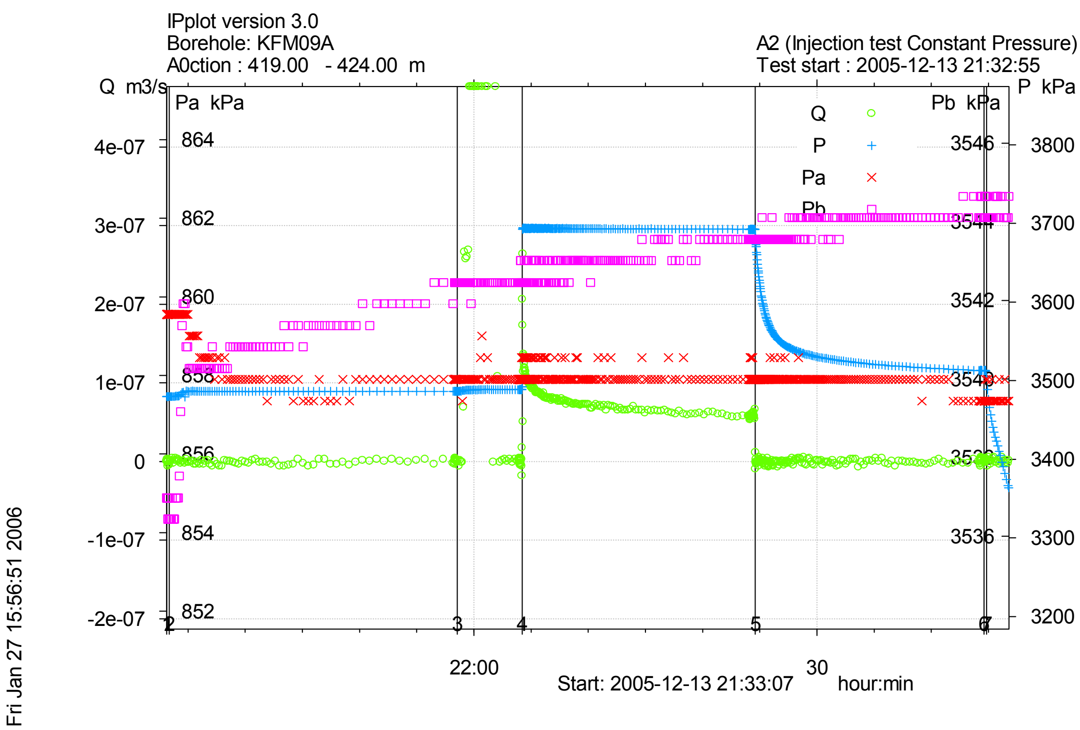


Figure A3-410. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 419.0-424.0 m in borehole KFM09A.*

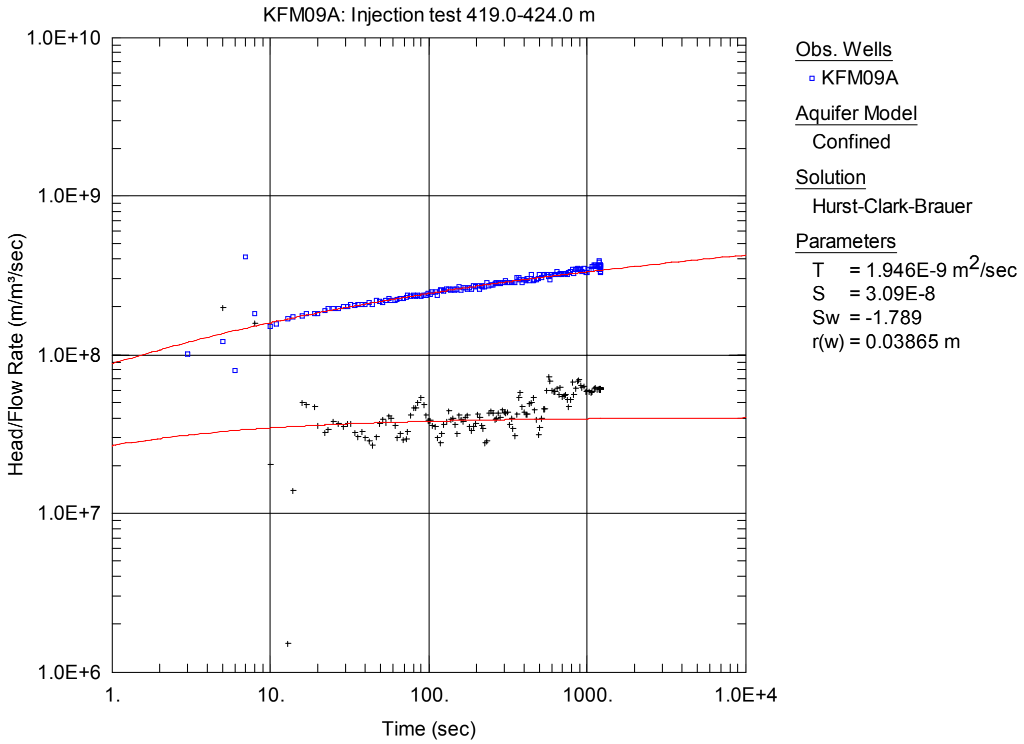


Figure A3-411. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 419.0-424.0 m in KFM09A. This plot shows a fit to the first of two different PRF:s during the injection period in this section.*

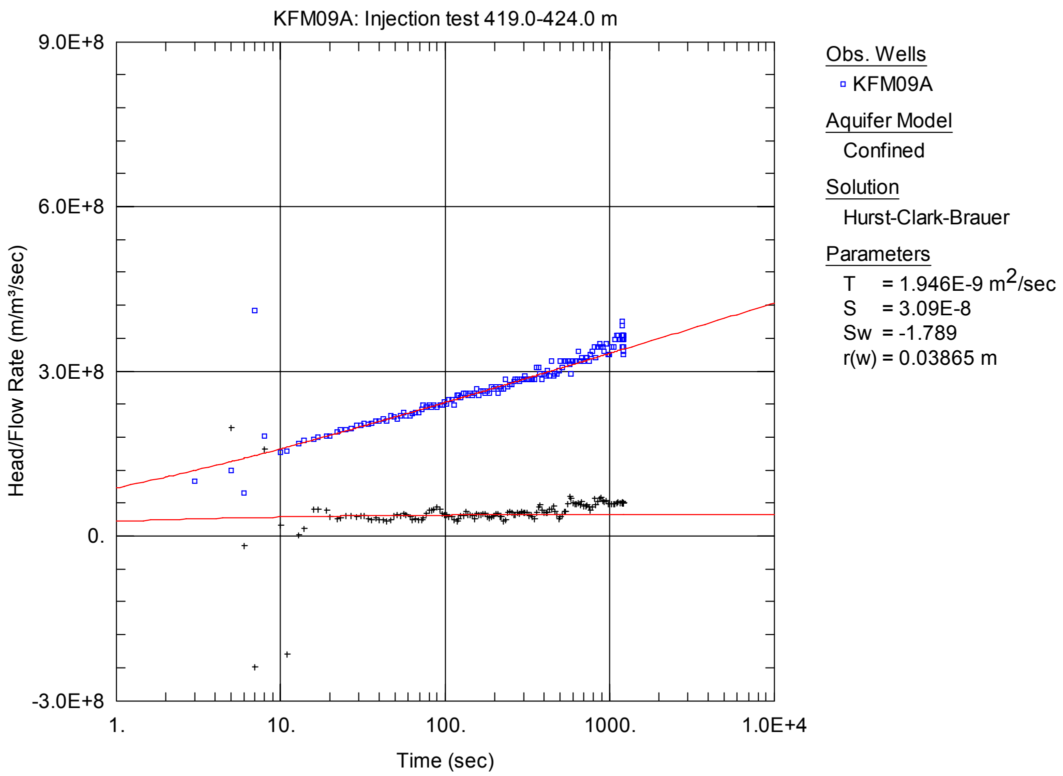


Figure A3-412. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 419.0-424.0 m in KFM09A. This plot shows a fit to the first of two different PRF:s during the injection period in this section.*

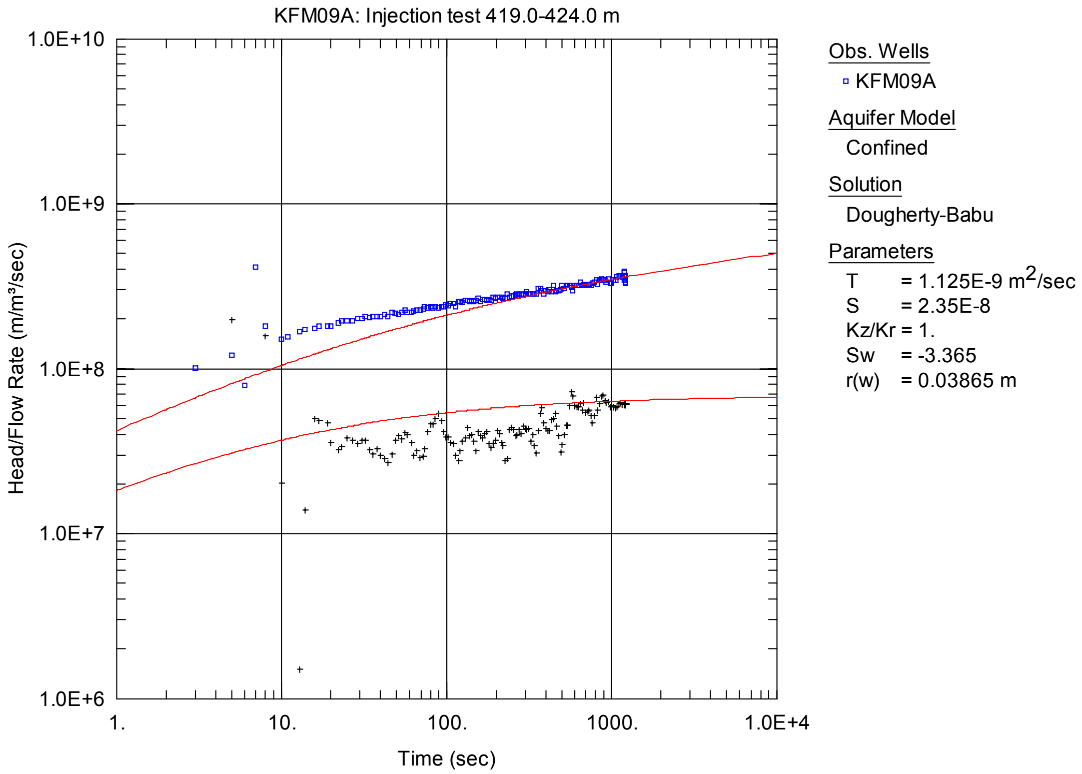


Figure A3-413. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 419.0-424.0 m in KFM09A. This plot shows a fit to the second of two different PRF:s during the injection period in this section.*

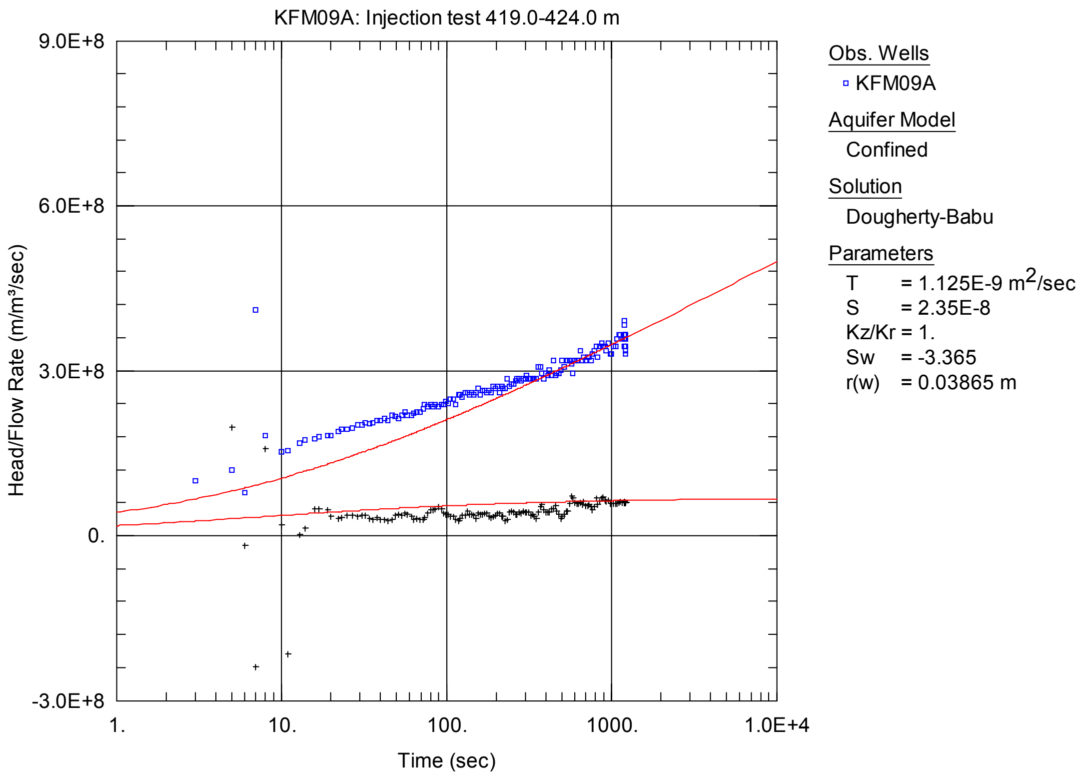


Figure A3-414. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 419.0-424.0 m in KFM09A. This plot shows a fit to the second of two different PRF:s during the injection period in this section.*

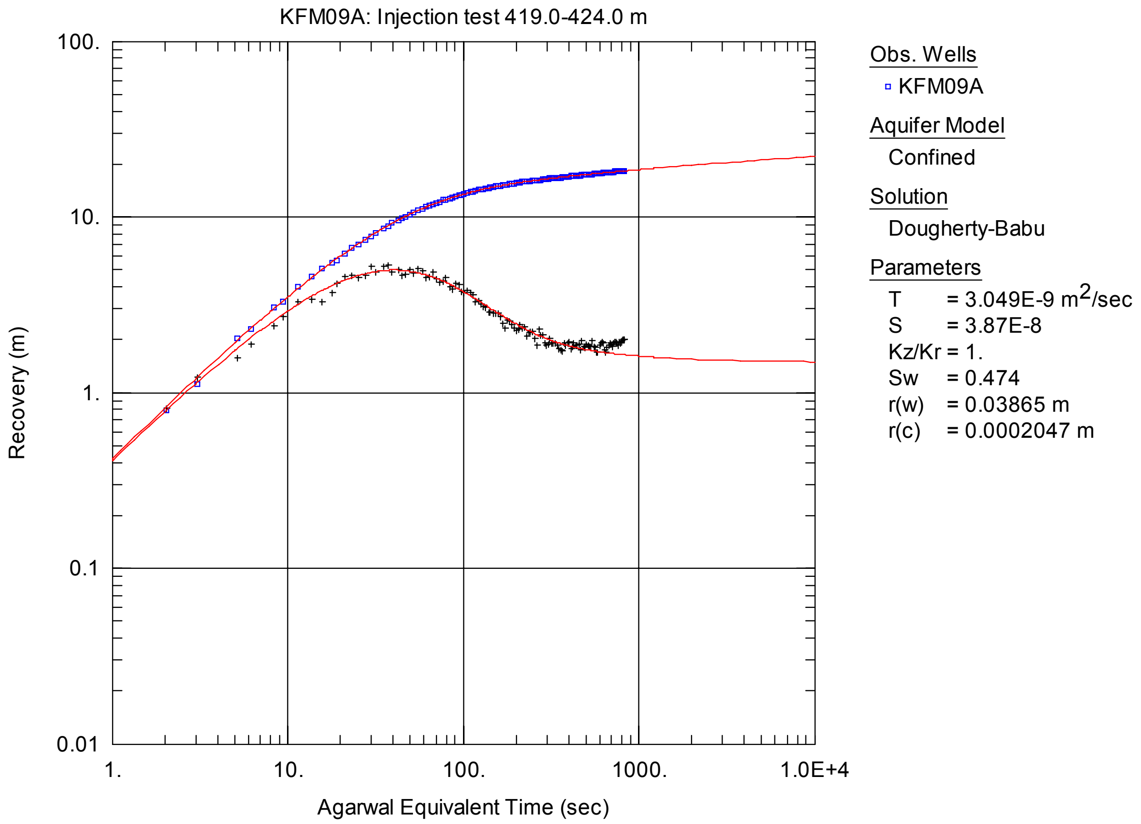


***Figure A3-415.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 419.0-424.0 m in KFM09A.*

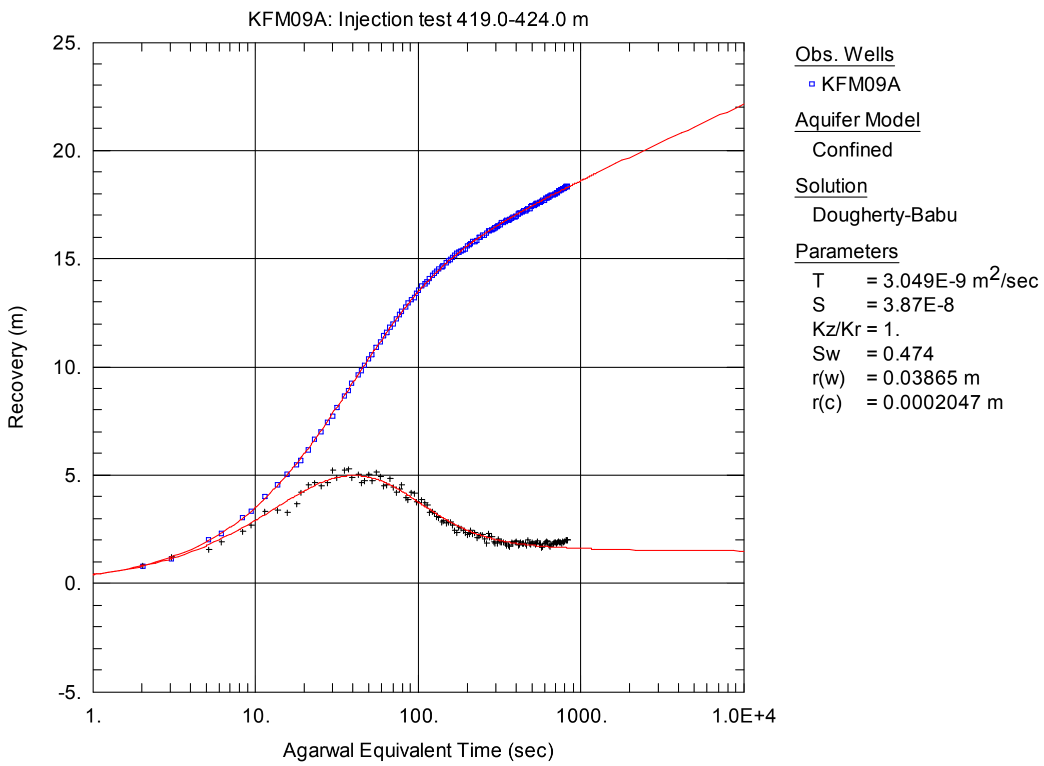


***Figure A3-416.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 419.0-424.0 m in KFM09A.*

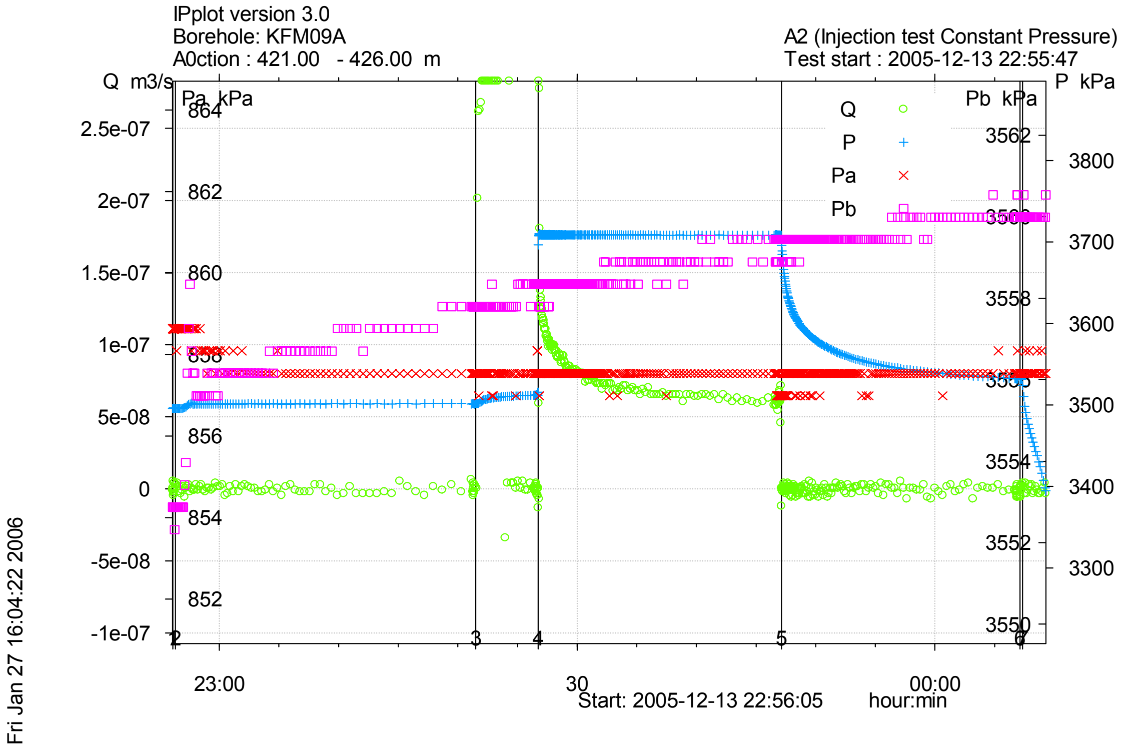


Figure A3-417. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 421.0-426.0 m in borehole KFM09A.

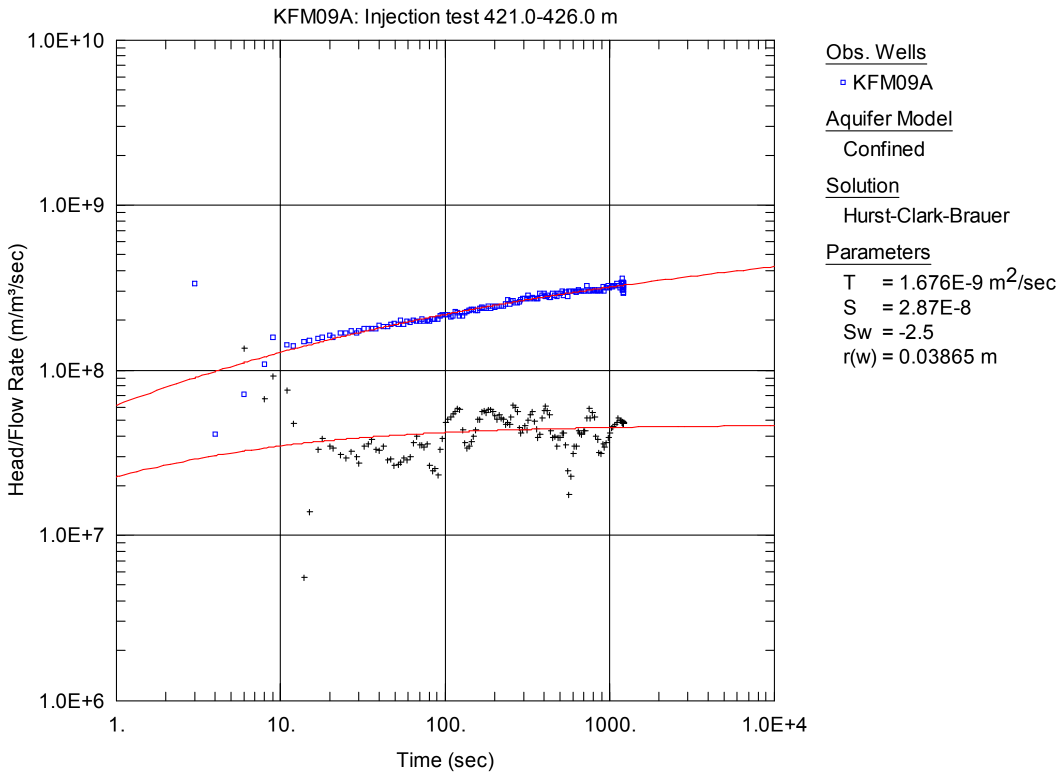


Figure A3-418. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 421.0-426.0 m in KFM09A.

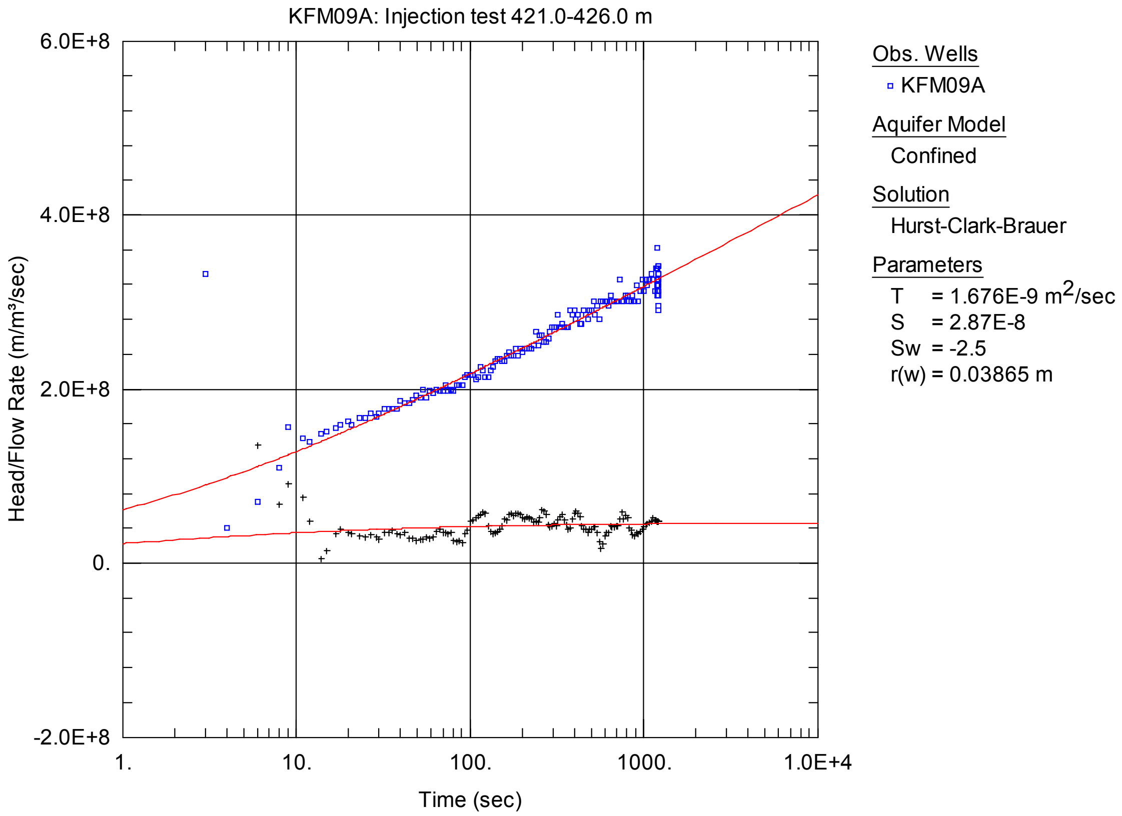


__Figure A3-419.__ Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 421.0-426.0 m in KFM09A.

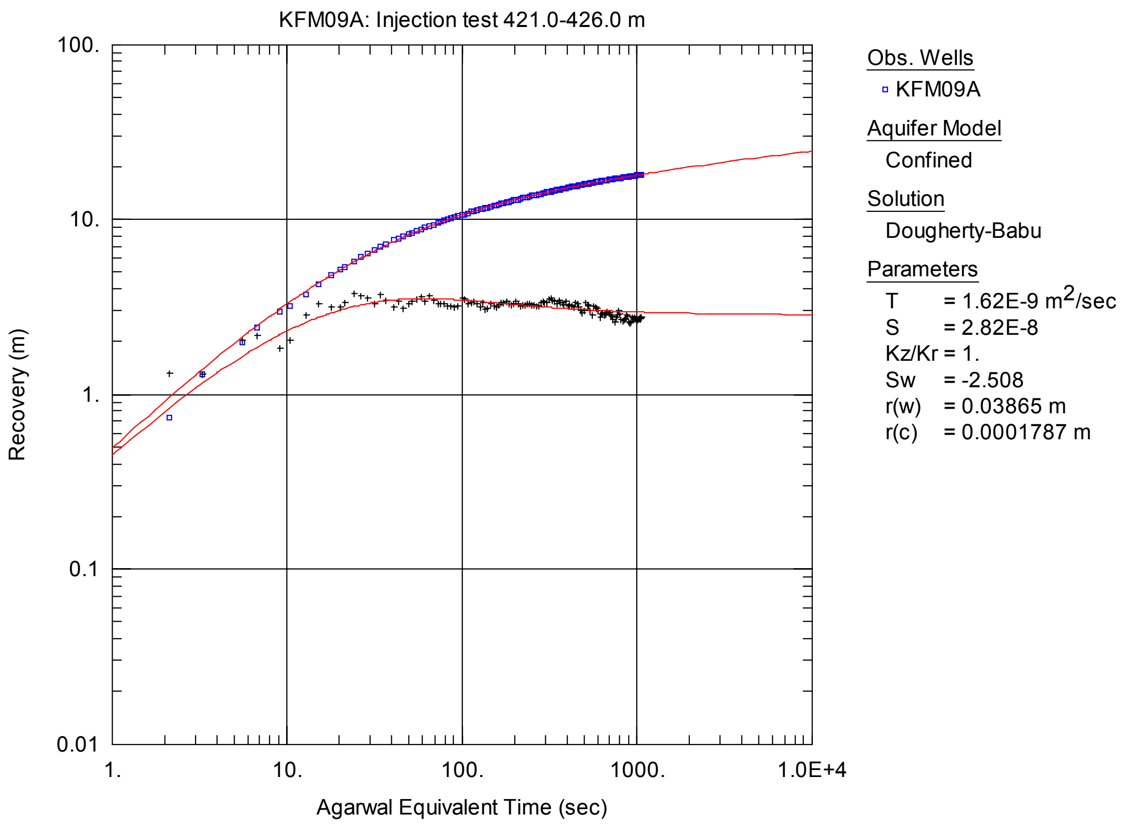


__Figure A3-420.__ Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 421.0-426.0 m in KFM09A.

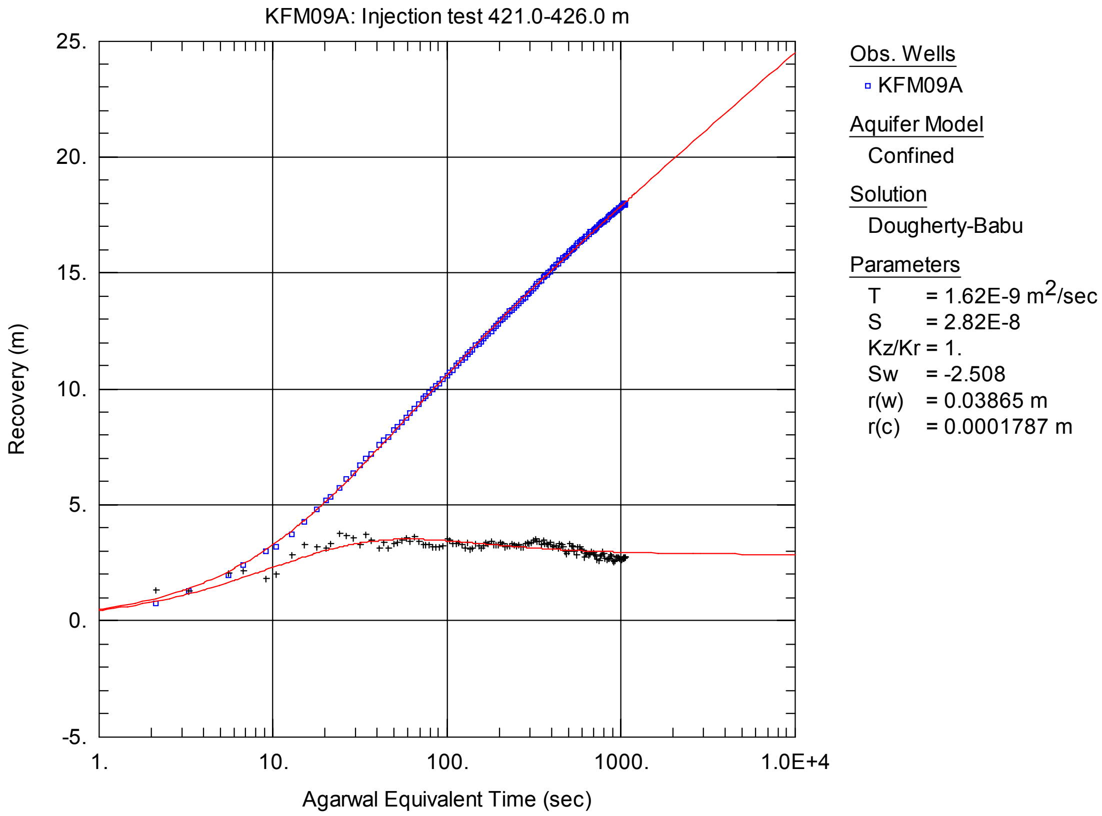


Figure A3-421. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 421.0-426.0 m in KFM09A.*

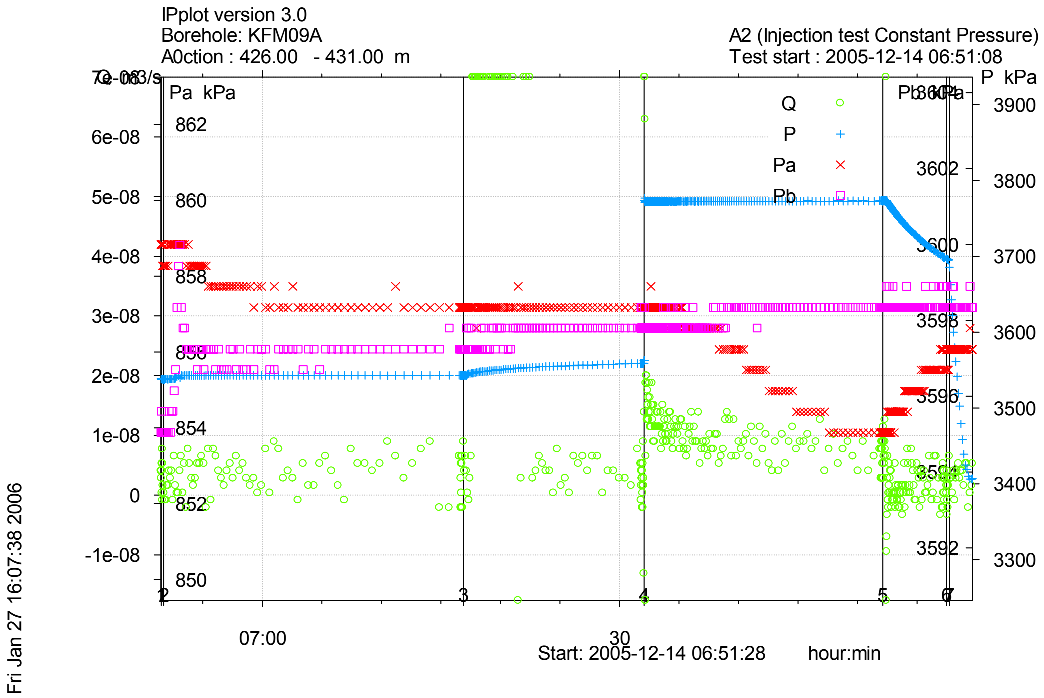


Figure A3-422. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 426.0-431.0 m in borehole KFM09A.*

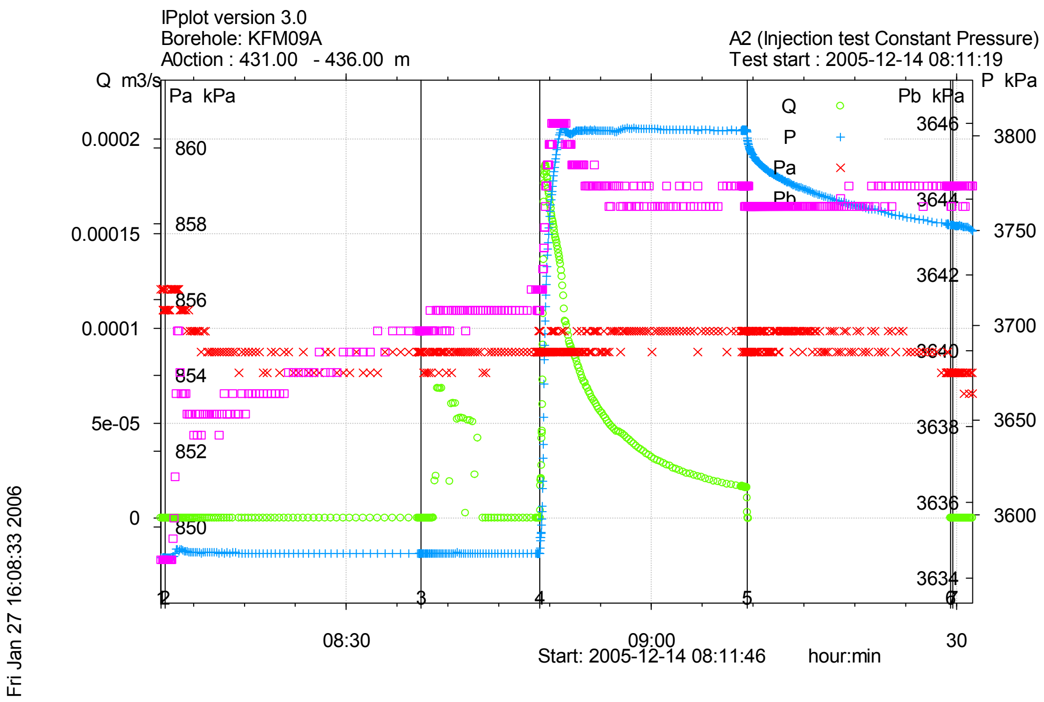


***Figure A3-423.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 431.0-436.0 m in borehole KFM09A.*

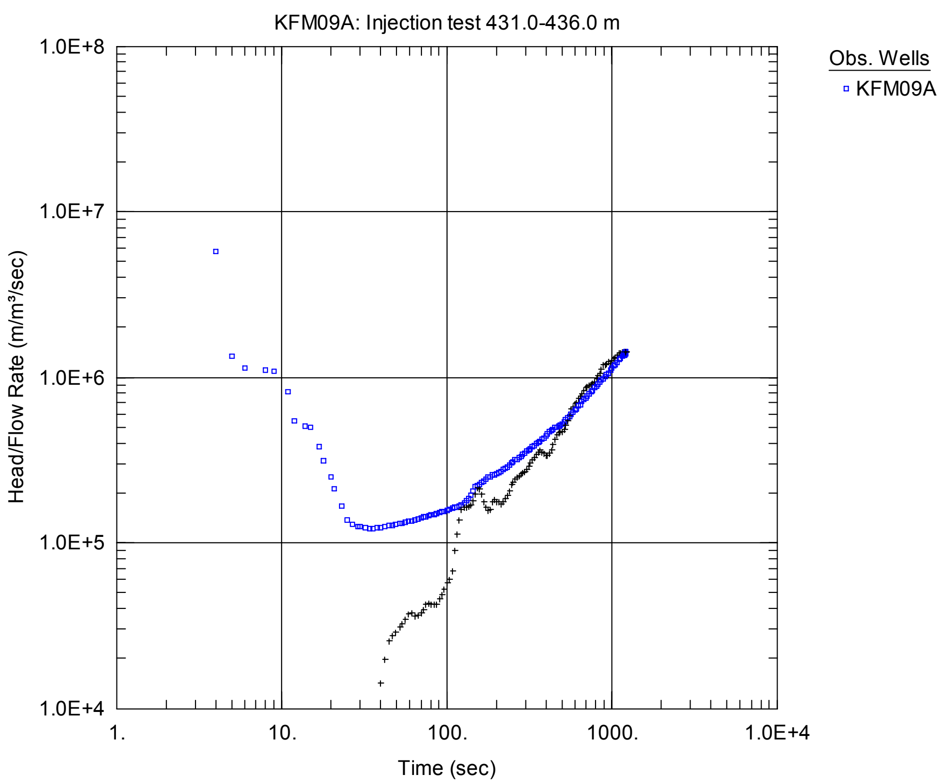


***Figure A3-424.** Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 431.0-436.0 m in KFM09A.*

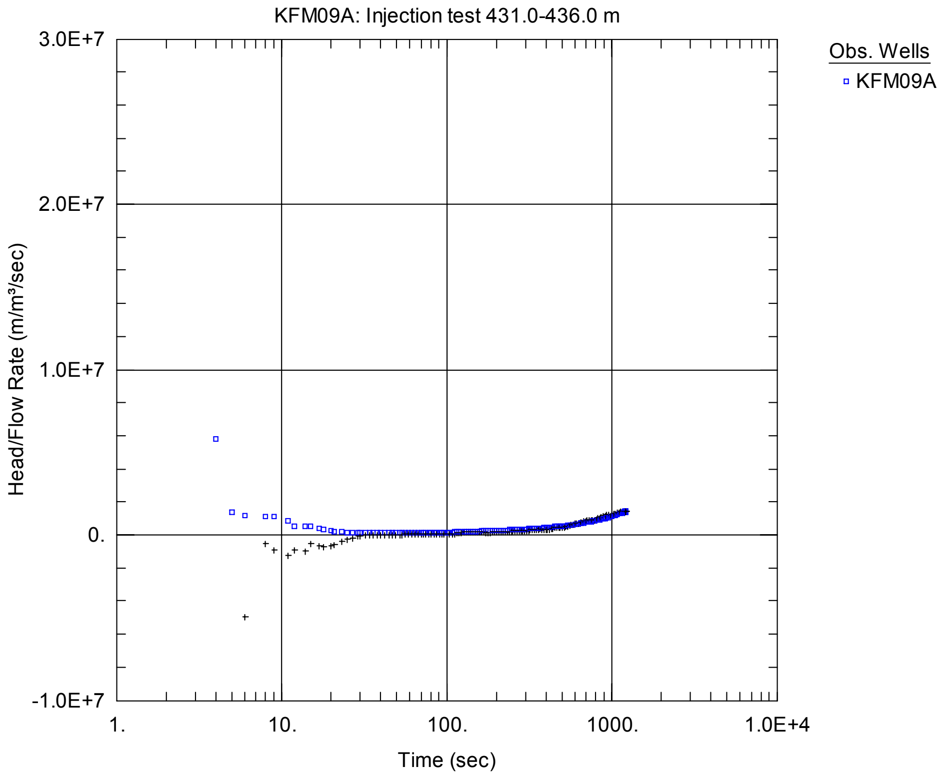


***Figure A3-425.** Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 431.0-436.0 m in KFM09A.*

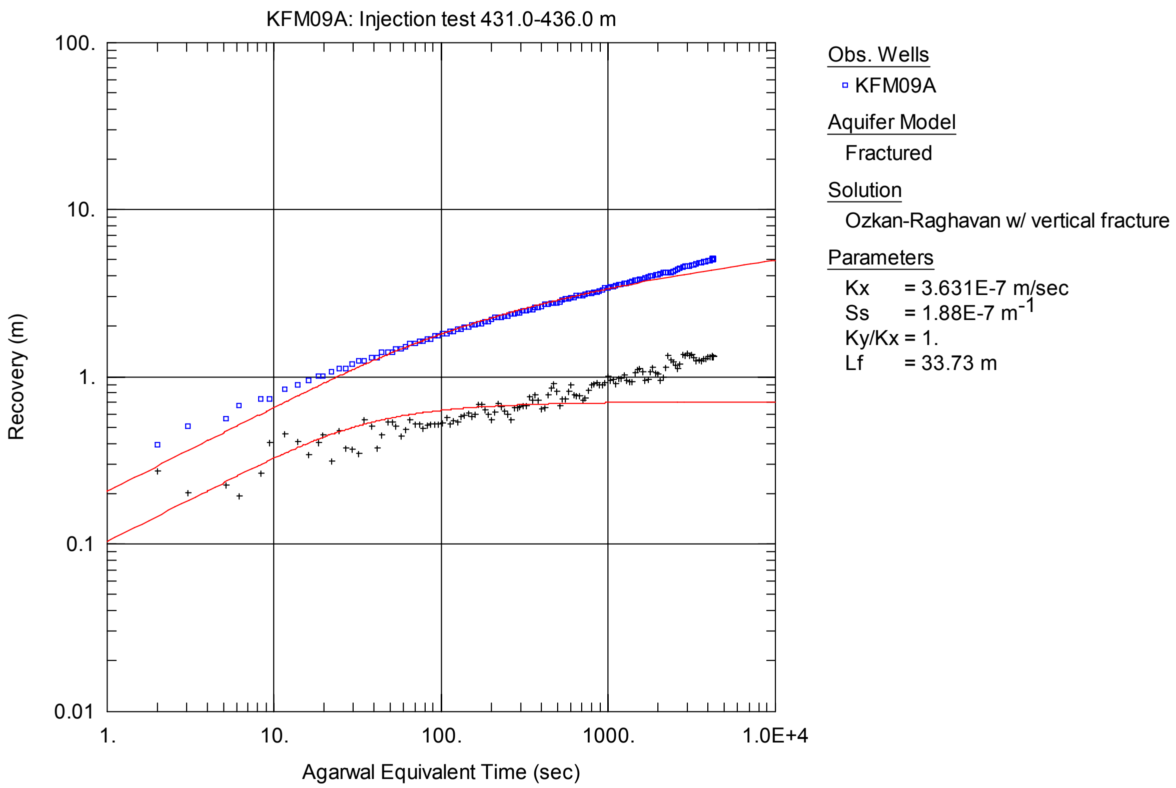


***Figure A3-426.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 431.0-436.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

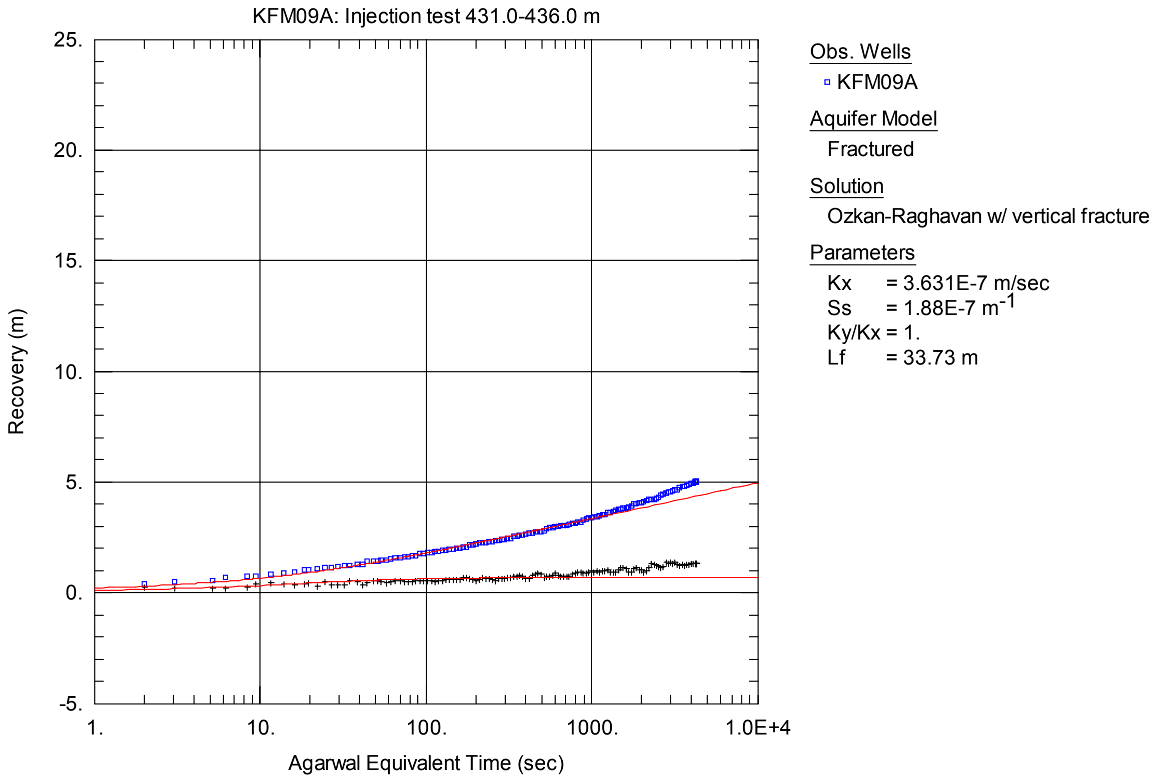


Figure A3-427. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 431.0-436.0 m in KFM09A.This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

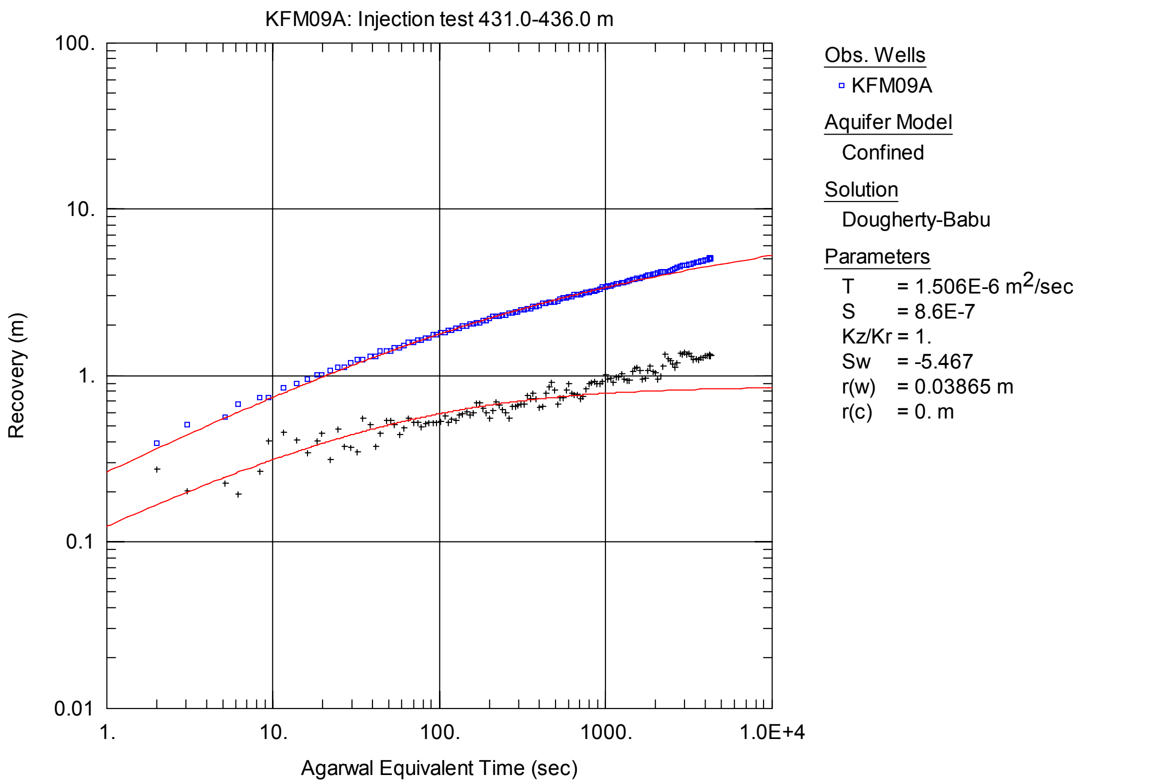


Figure A3-428. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 431.0-436.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

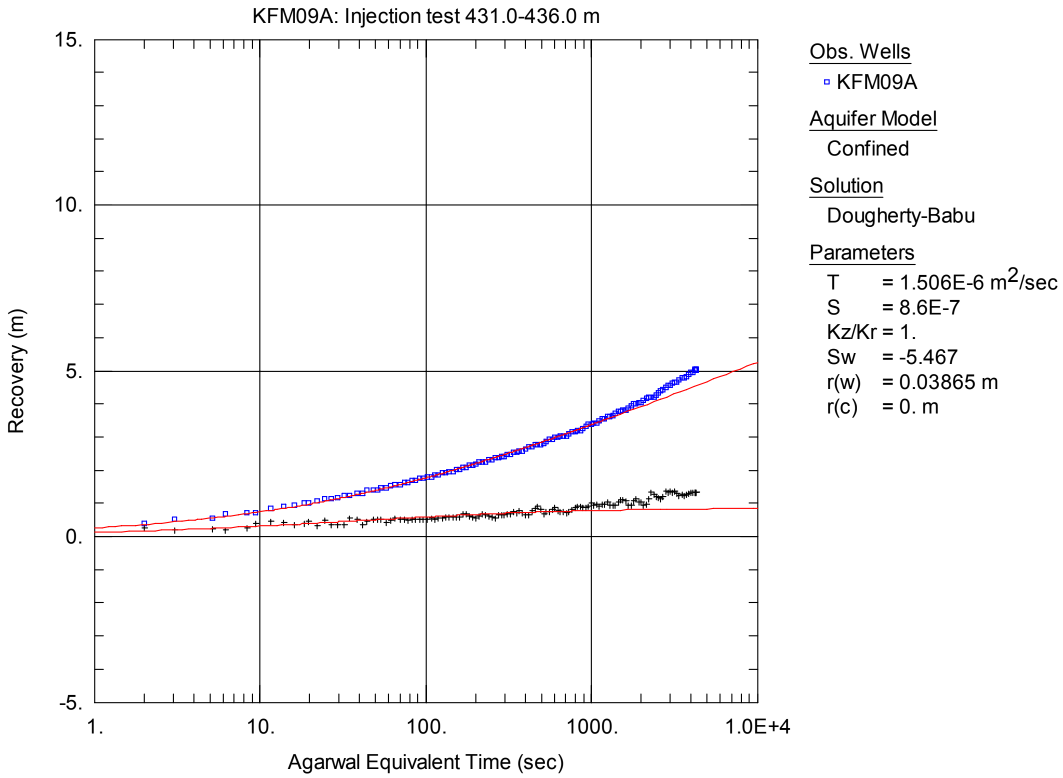


Figure A3-429. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 431.0-436.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

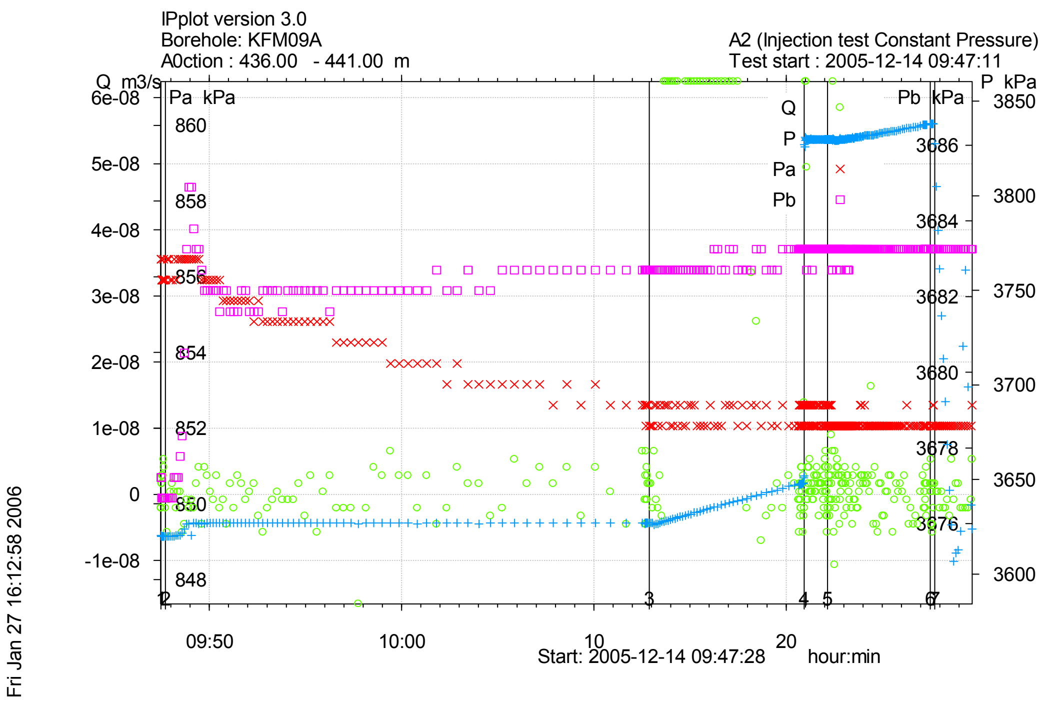


Figure A3-430. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 436.0-441.0 m in borehole KFM09A.*

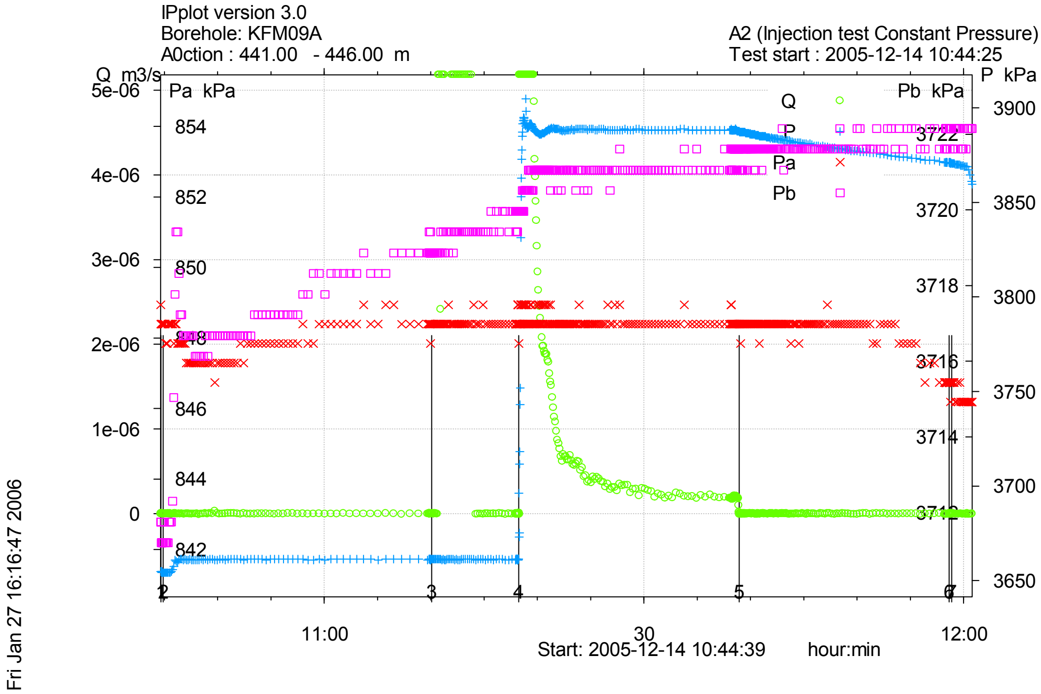


Figure A3-431. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in 441.0-446.0 m in borehole KFM09A.*

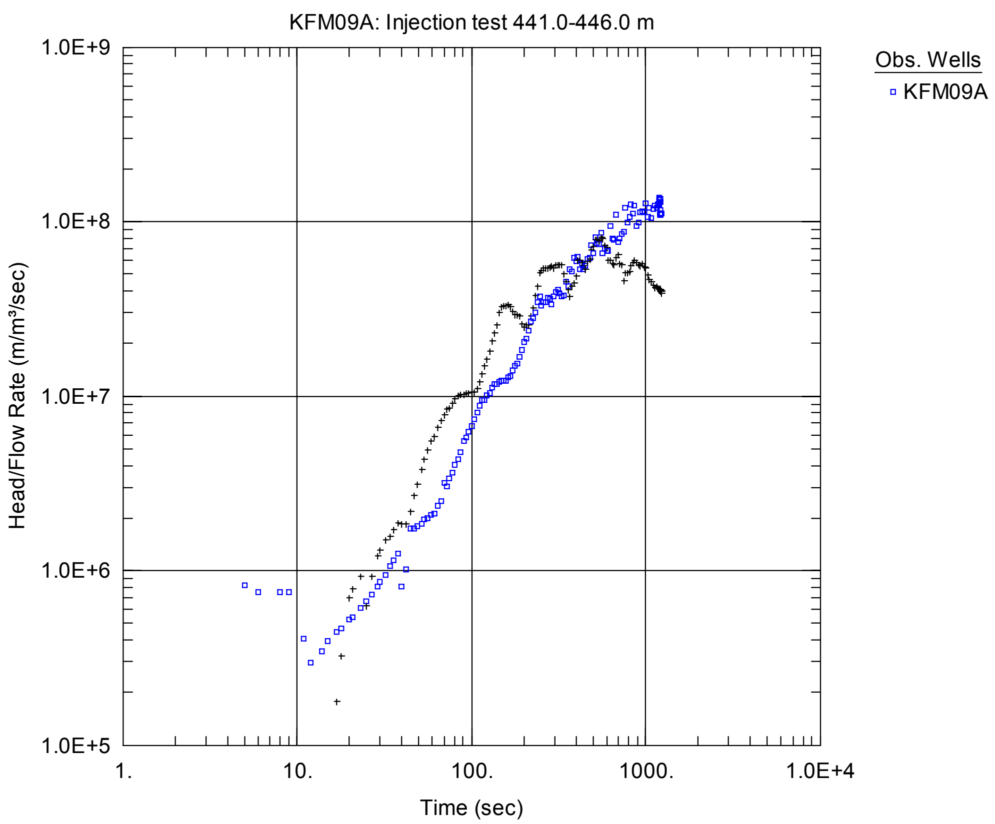


Figure A3-432. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 441.0-446.0 m in KFM09A.*

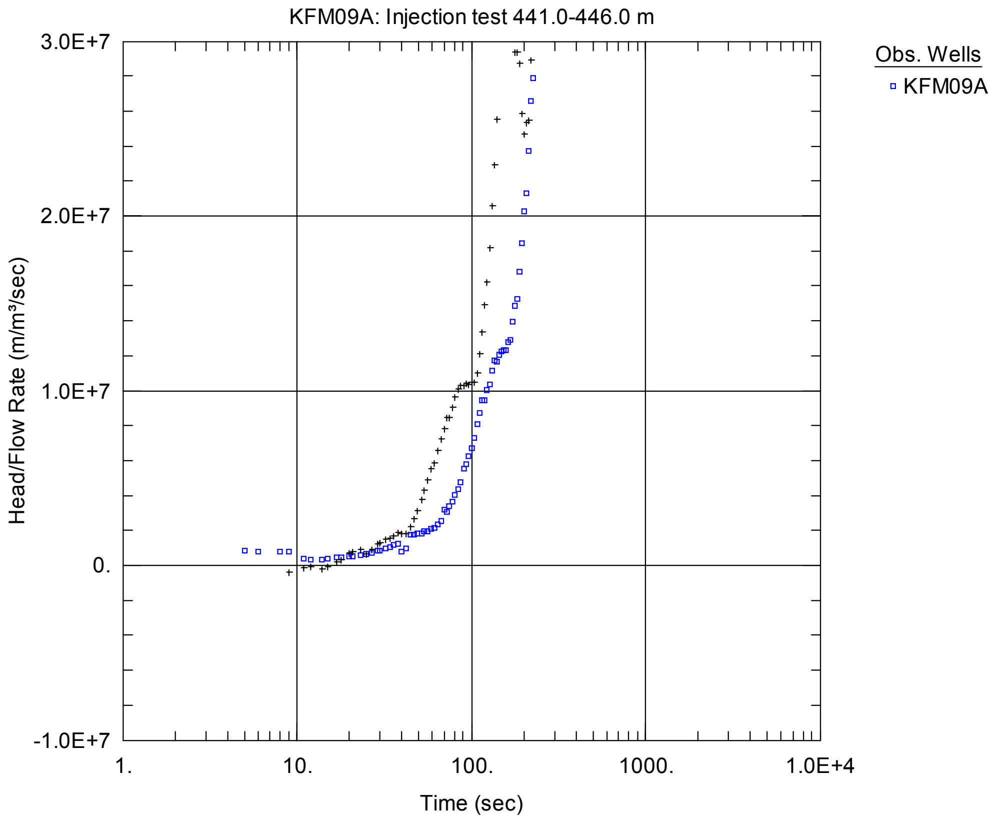


Figure A3-433. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 441.0-446.0 m in KFM09A.*

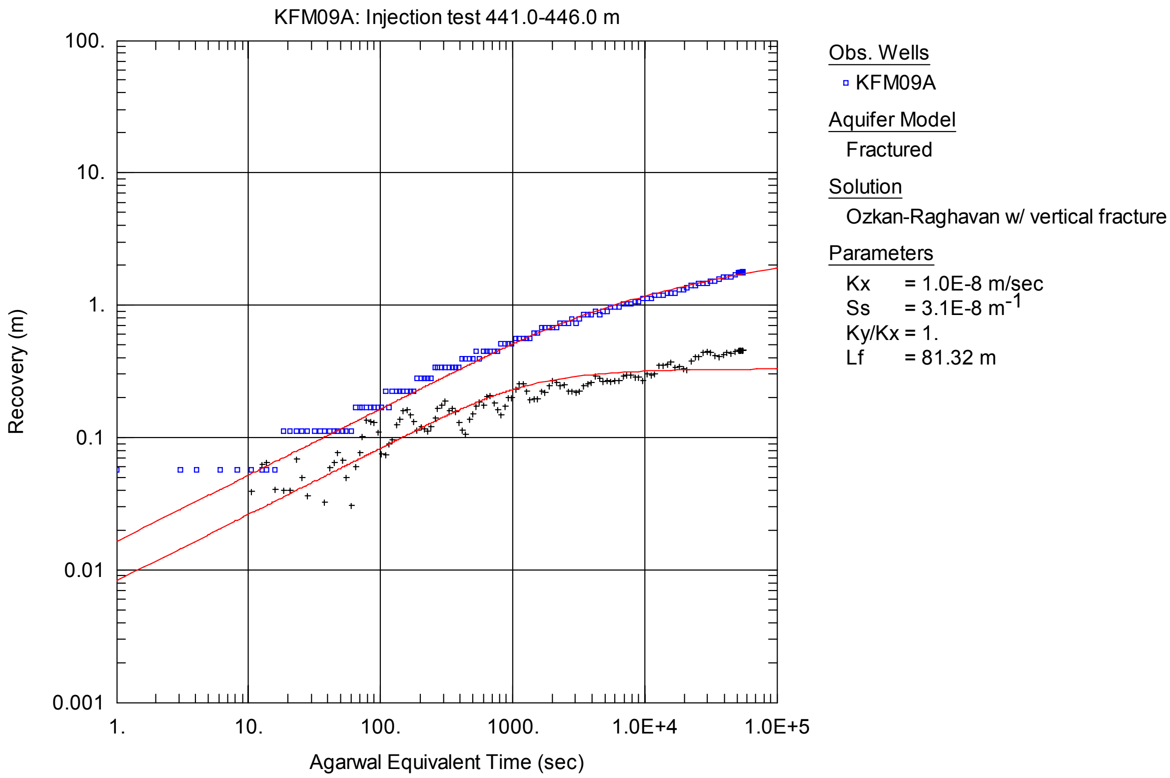


Figure A3-434. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 441.0-446.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

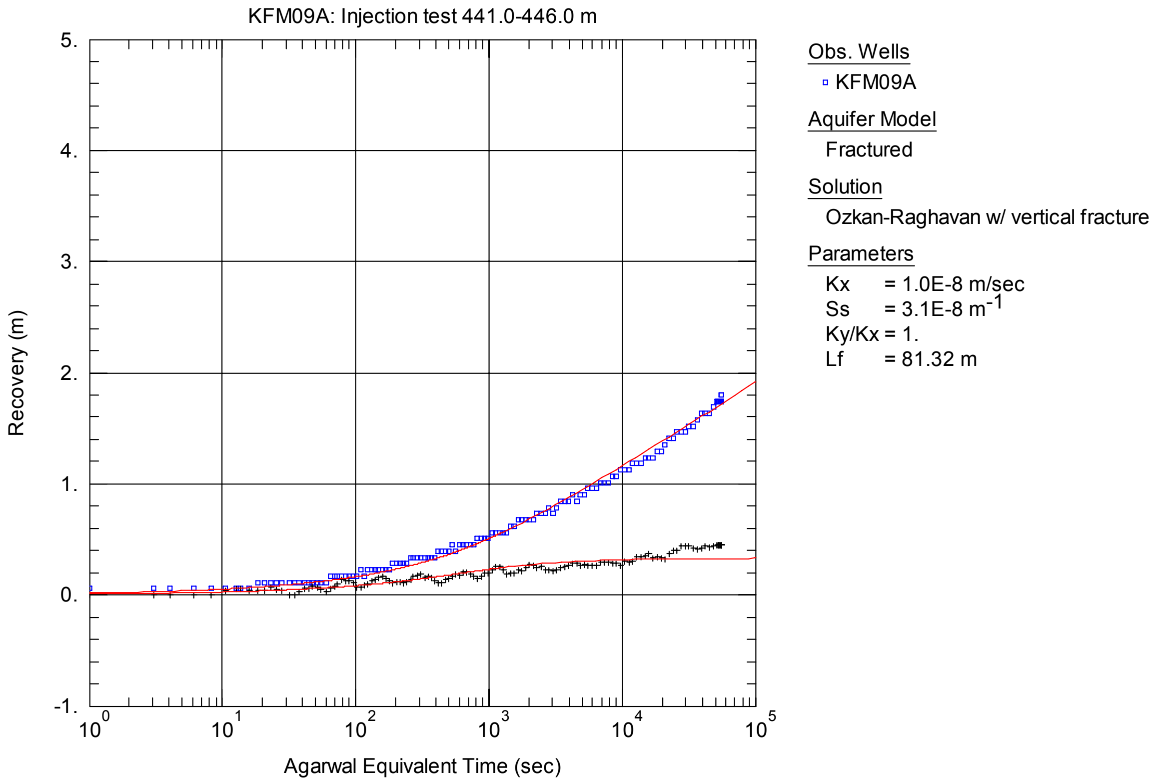


Figure A3-435. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 441.0-446.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

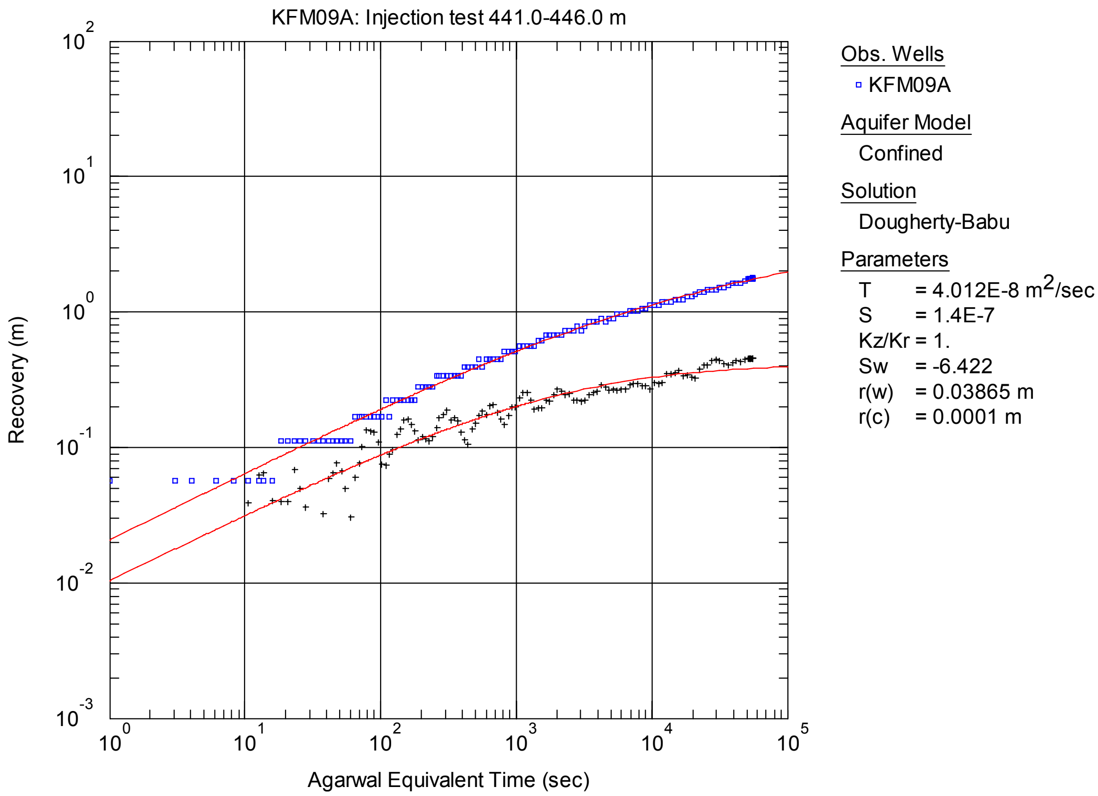


Figure A3-436. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 441.0-446.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

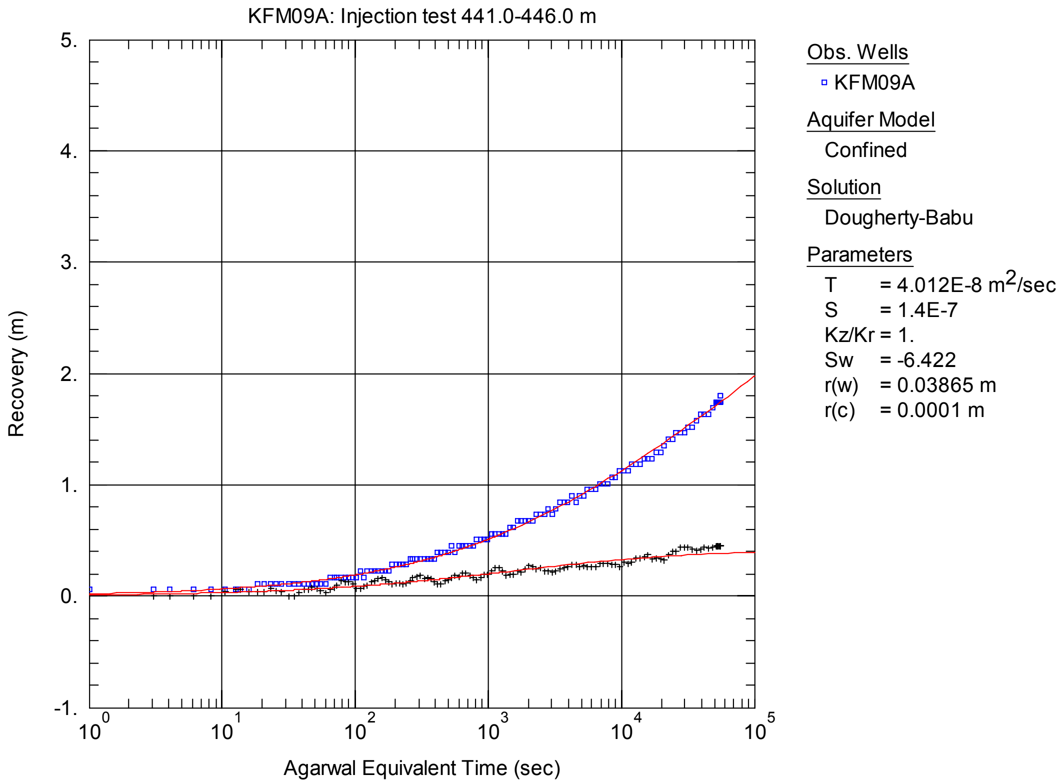


Figure A3-437. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 441.0-446.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

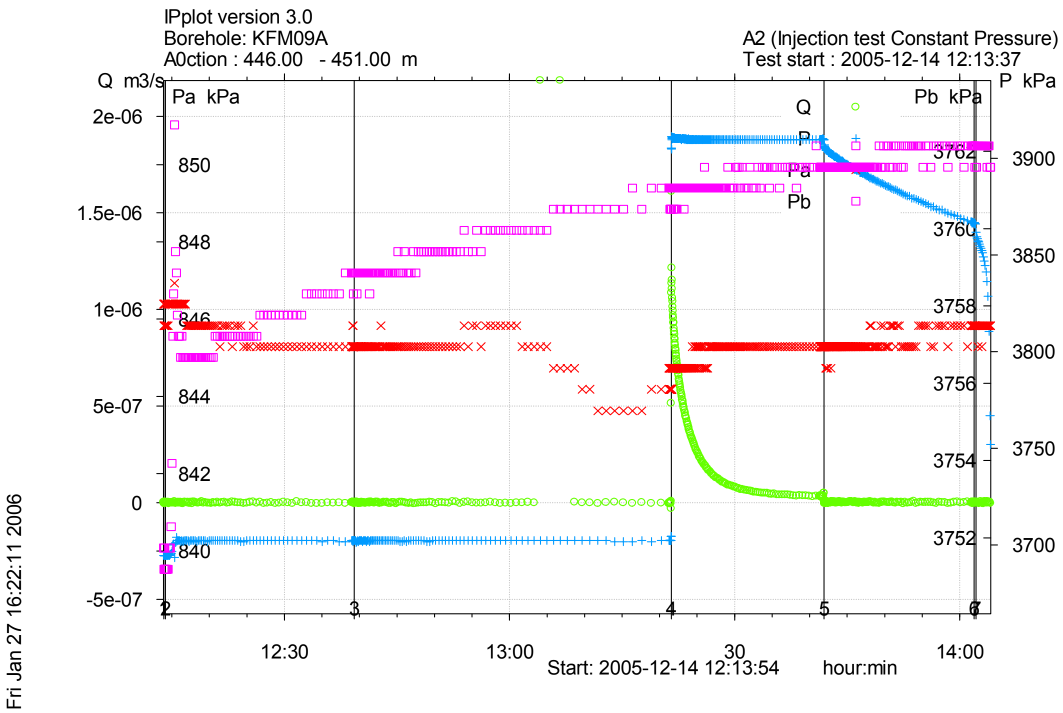


Figure A3-438. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 446.0-451.0 m in borehole KFM09A.*

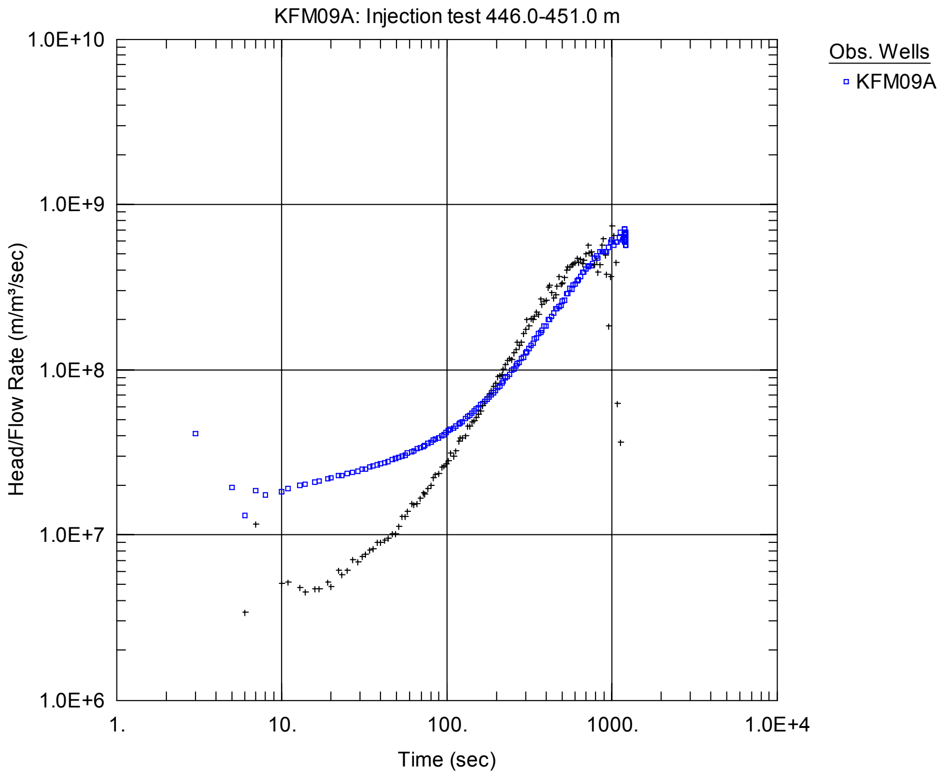


Figure A3-439. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 446.0-451.0 m in KFM09A.*

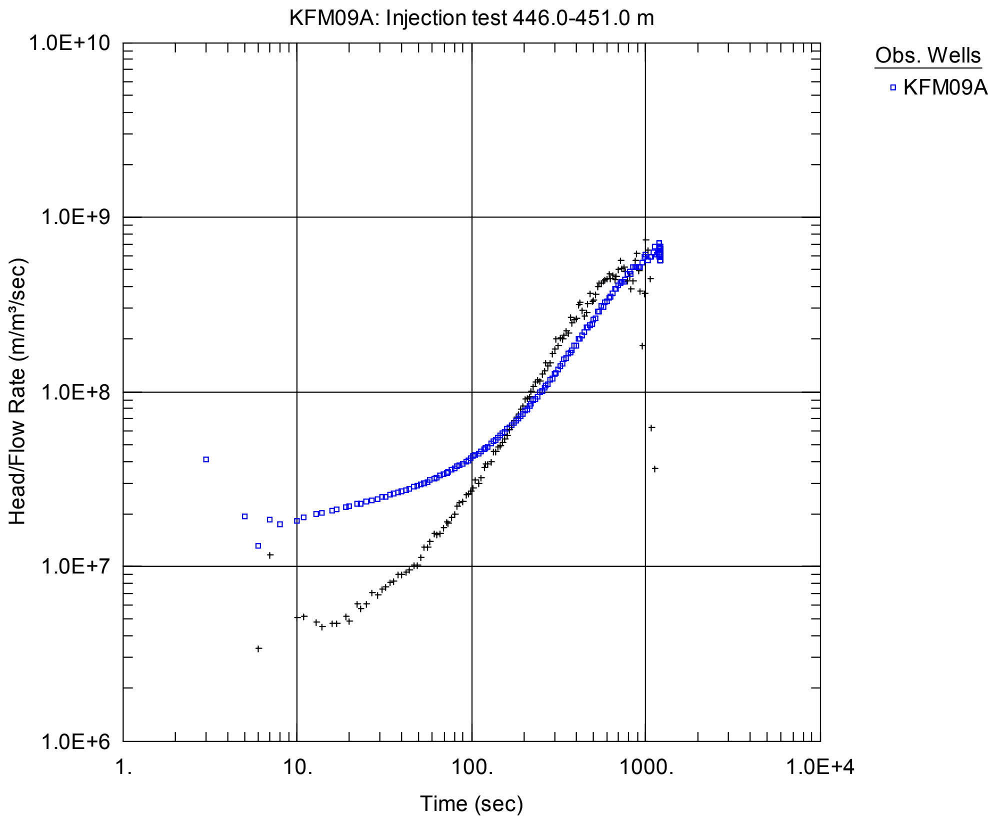


Figure A3-440. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 446.0-451.0 m in KFM09A.*

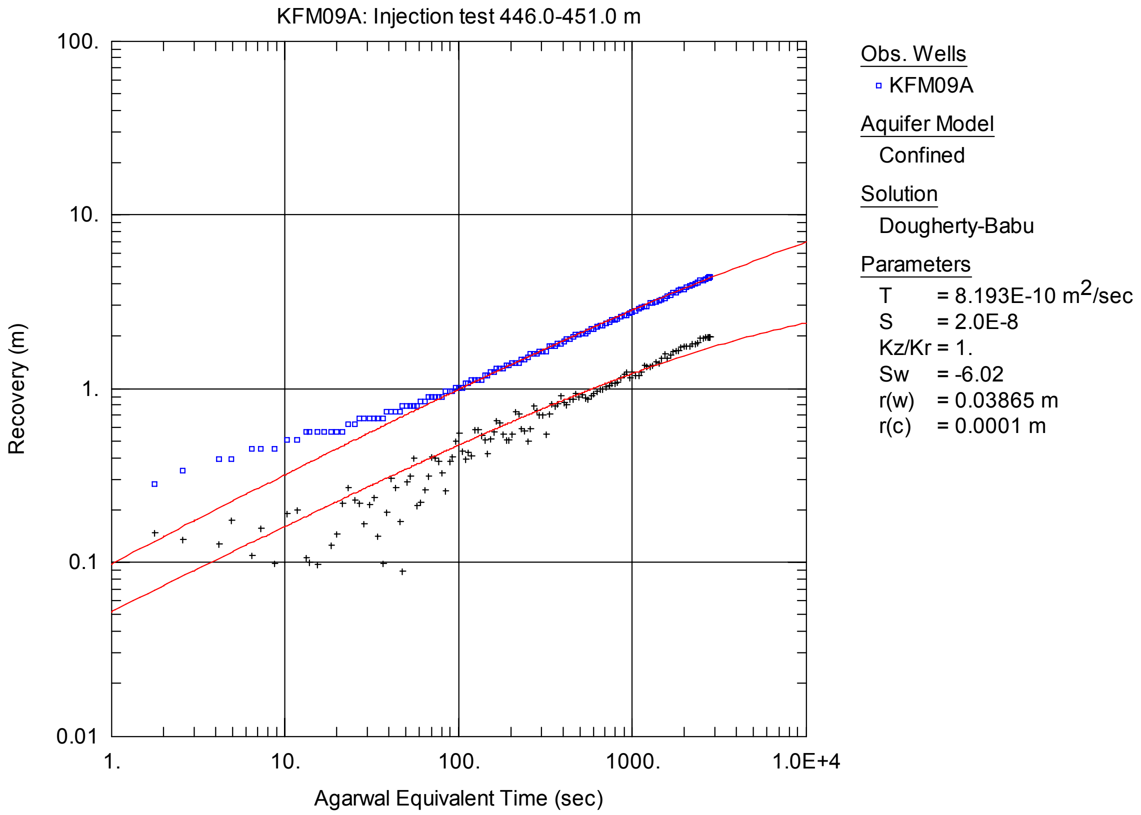


Figure A3-441. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 446.0-451.0 m in KFM09A.*

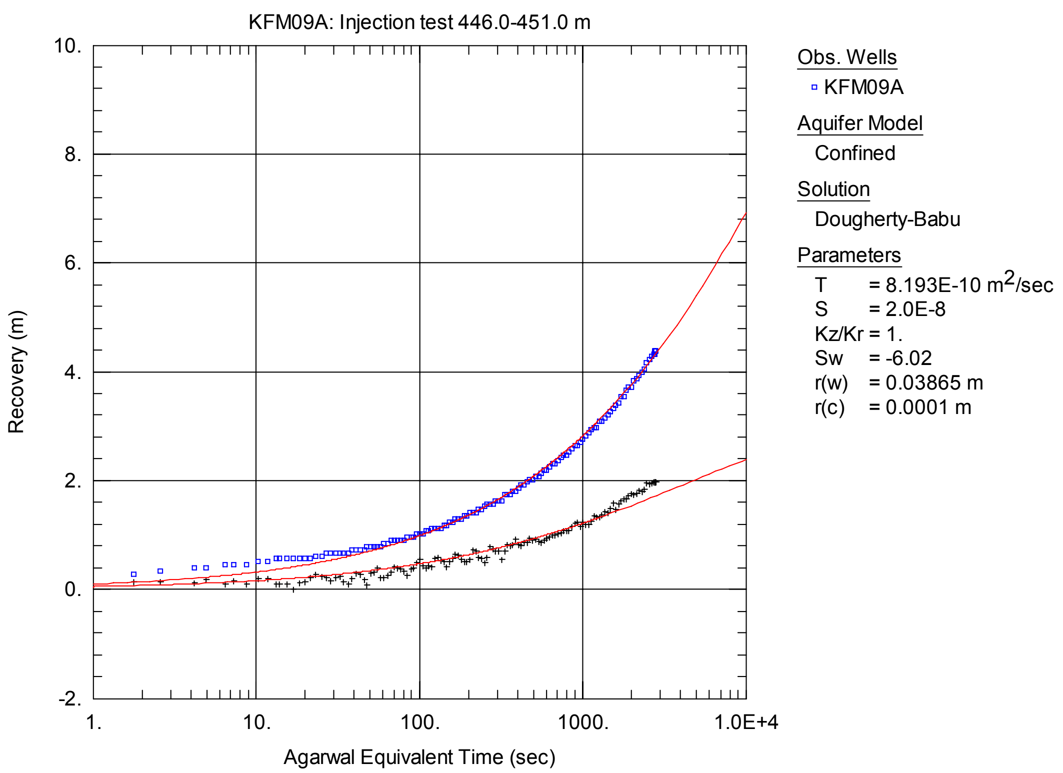


Figure A3-442. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 446.0-451.0 m in KFM09A.*

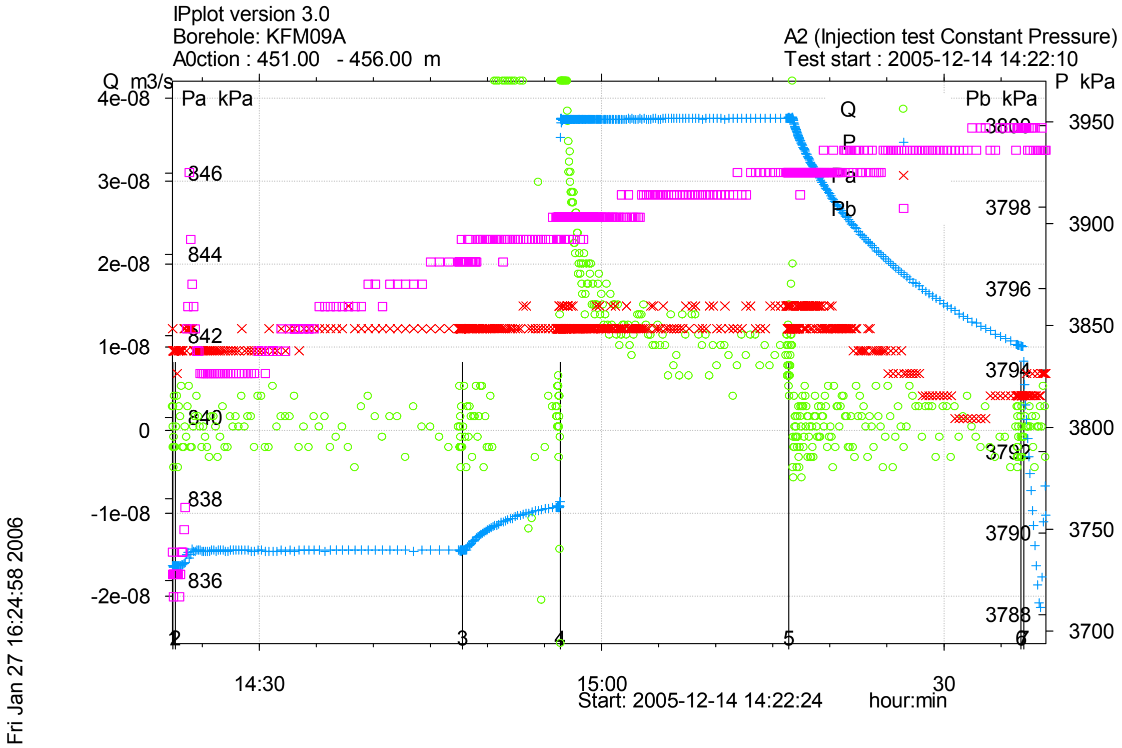


Figure A3-443. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 451.0-456.0 m in borehole KFM09A.*

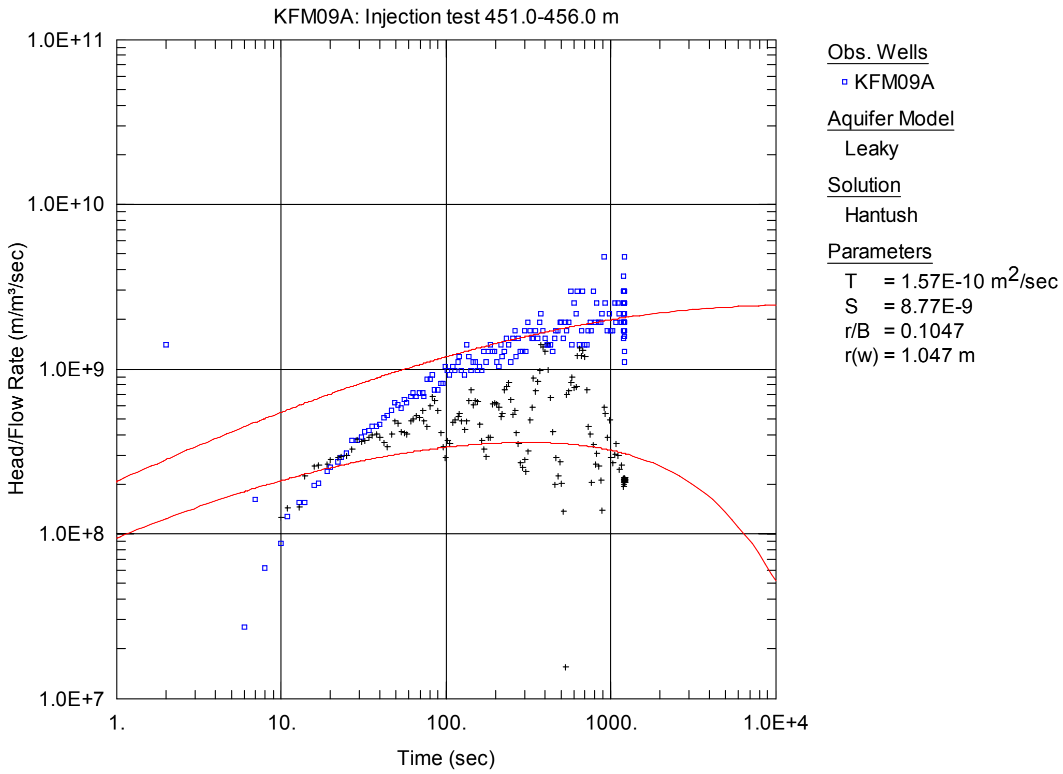


Figure A3-444. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 451.0-456.0 m in KFM09A.*

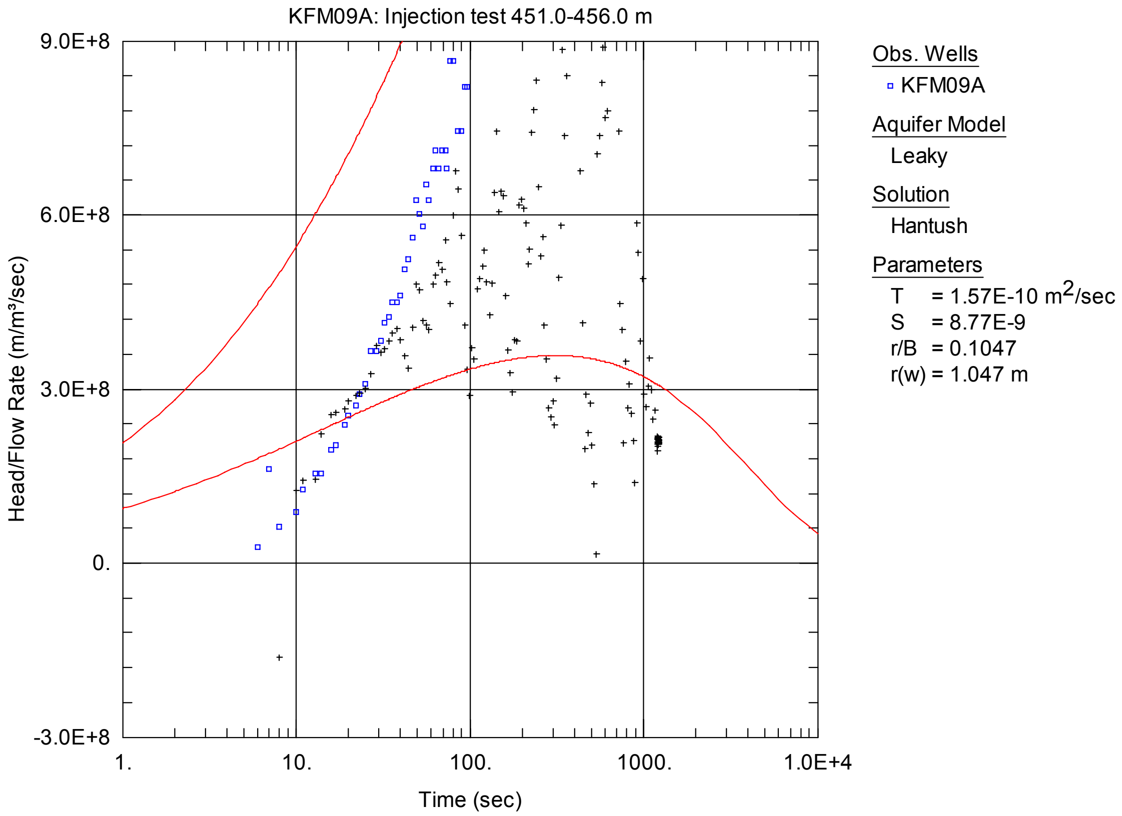


Figure A3-445. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 451.0-456.0 m in KFM09A.*

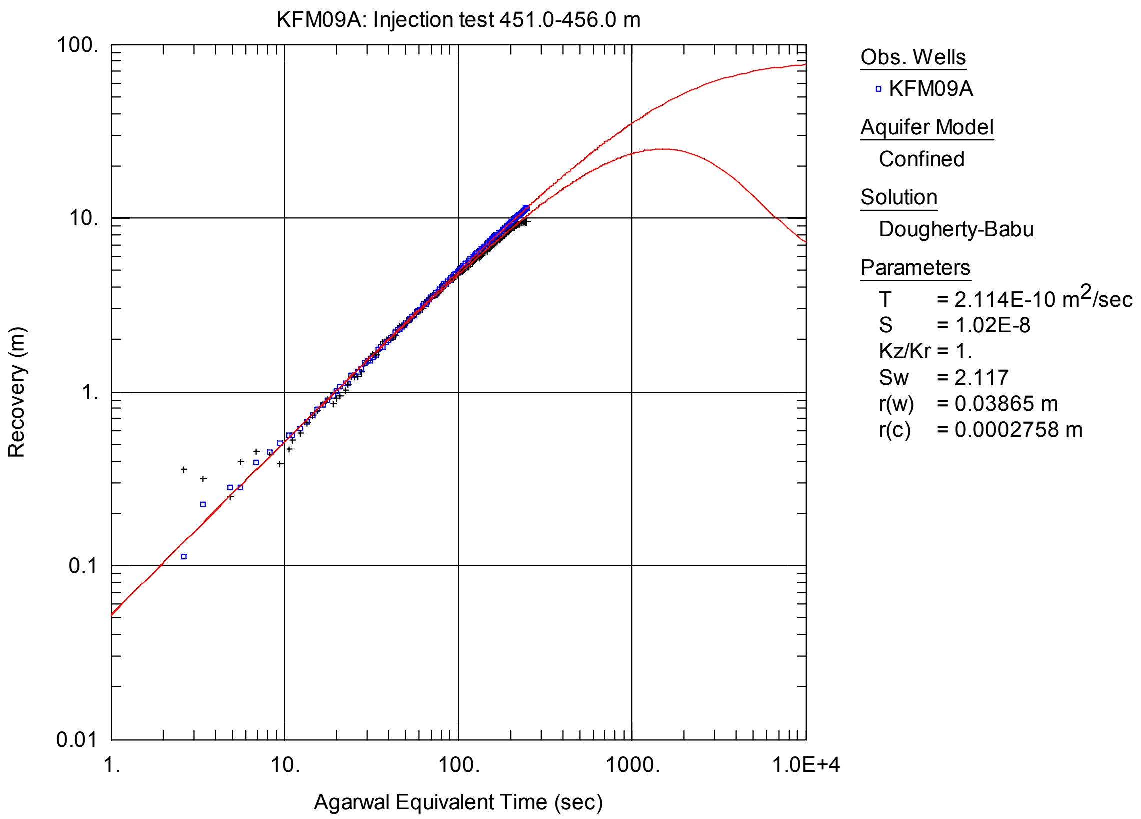


Figure A3-446. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 451.0-456.0 m in KFM09A.*

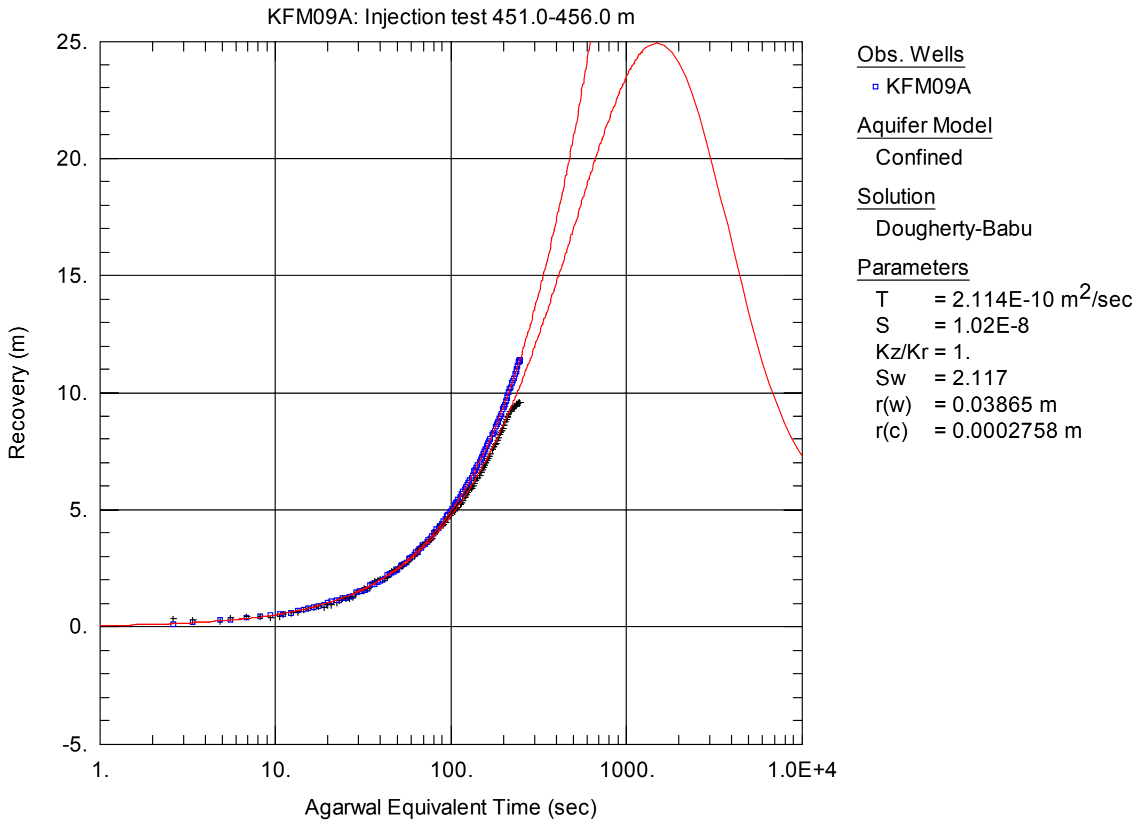


__Figure A3-447.__ Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 451.0-456.0 m in KFM09A.

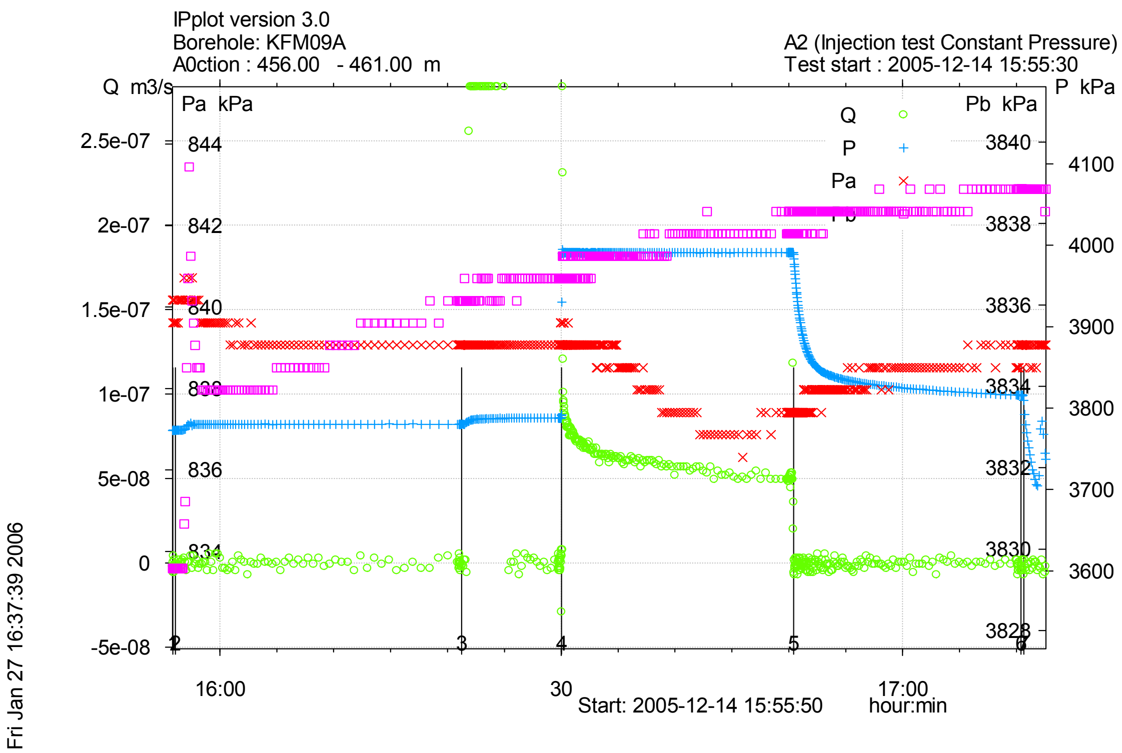


Figure A3-448. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 456.0-461.0 m in borehole KFM09A.

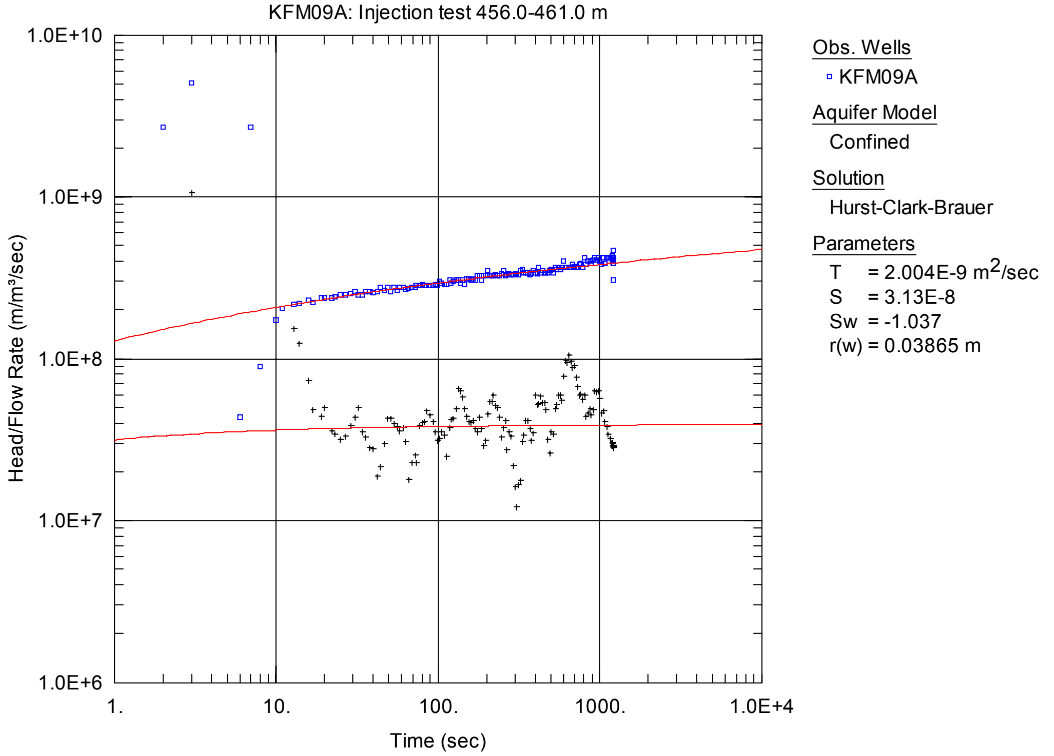


Figure A3-449. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 456.0-461.0 m in KFM09A.

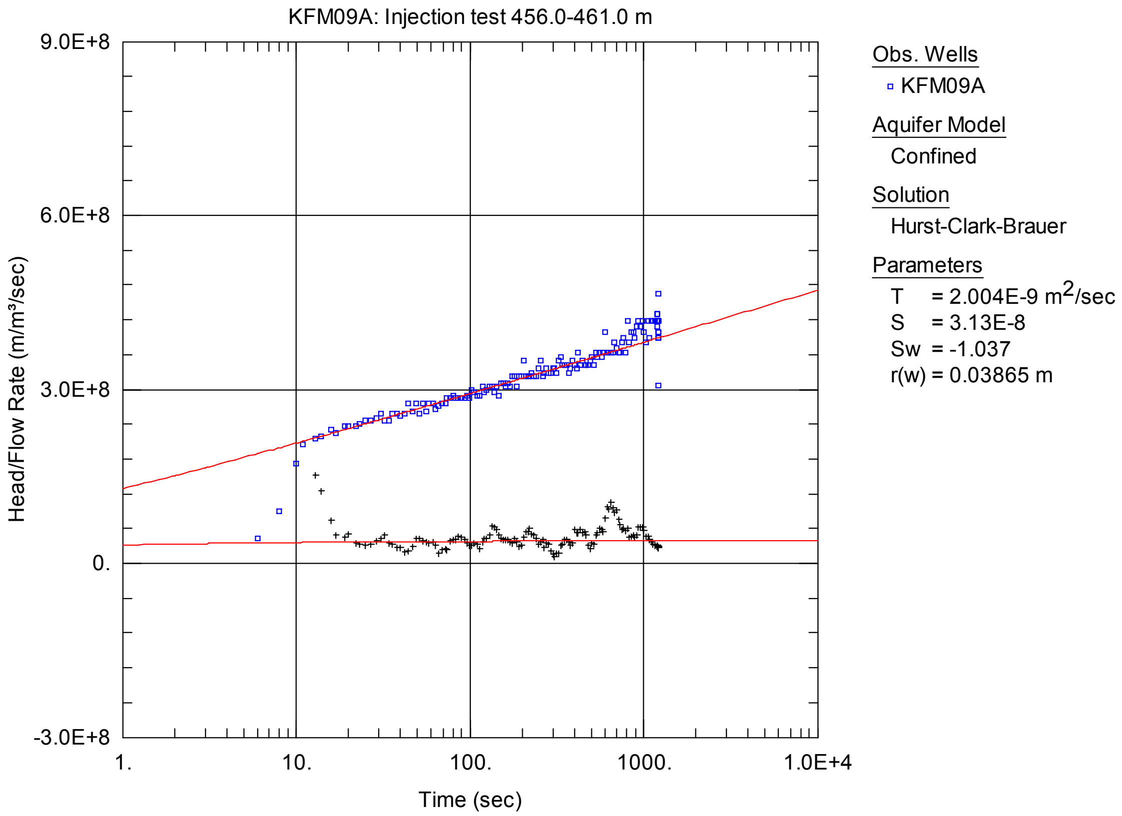


Figure A3-450. Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 456.0-461.0 m in KFM09A.

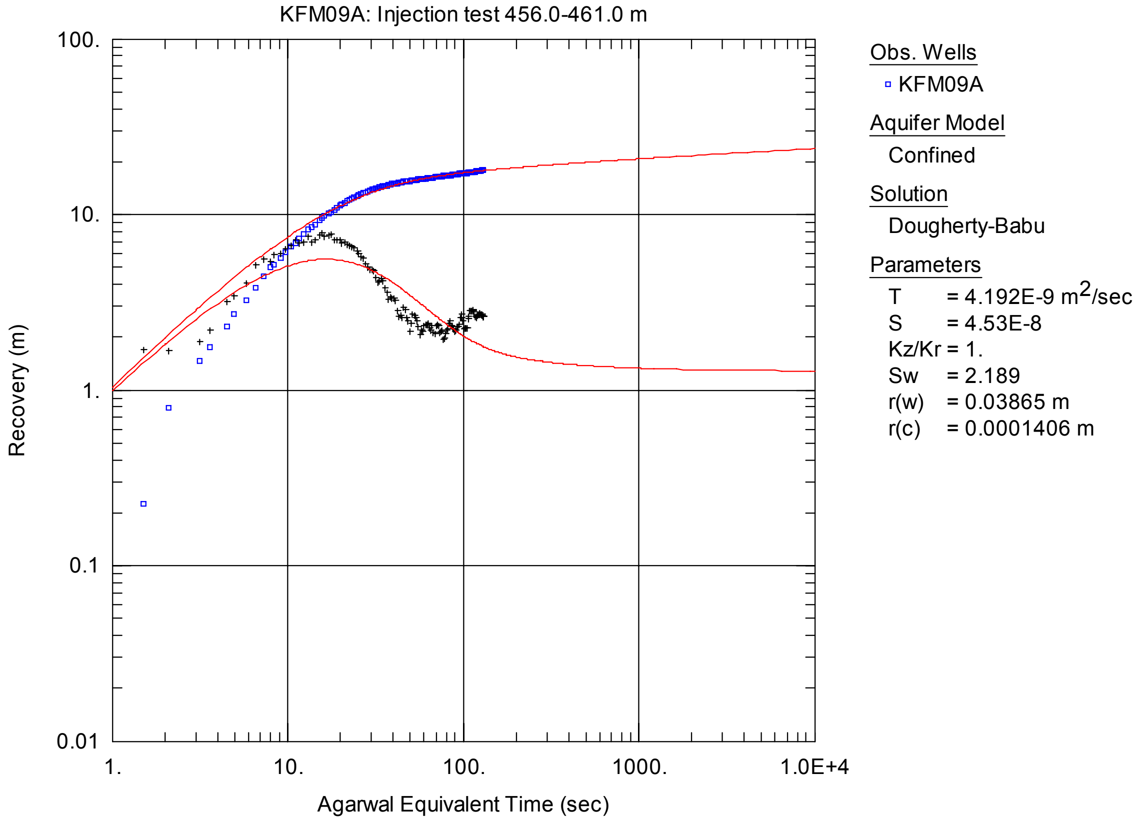


Figure A3-451. Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 456.0-461.0 m in KFM09A.

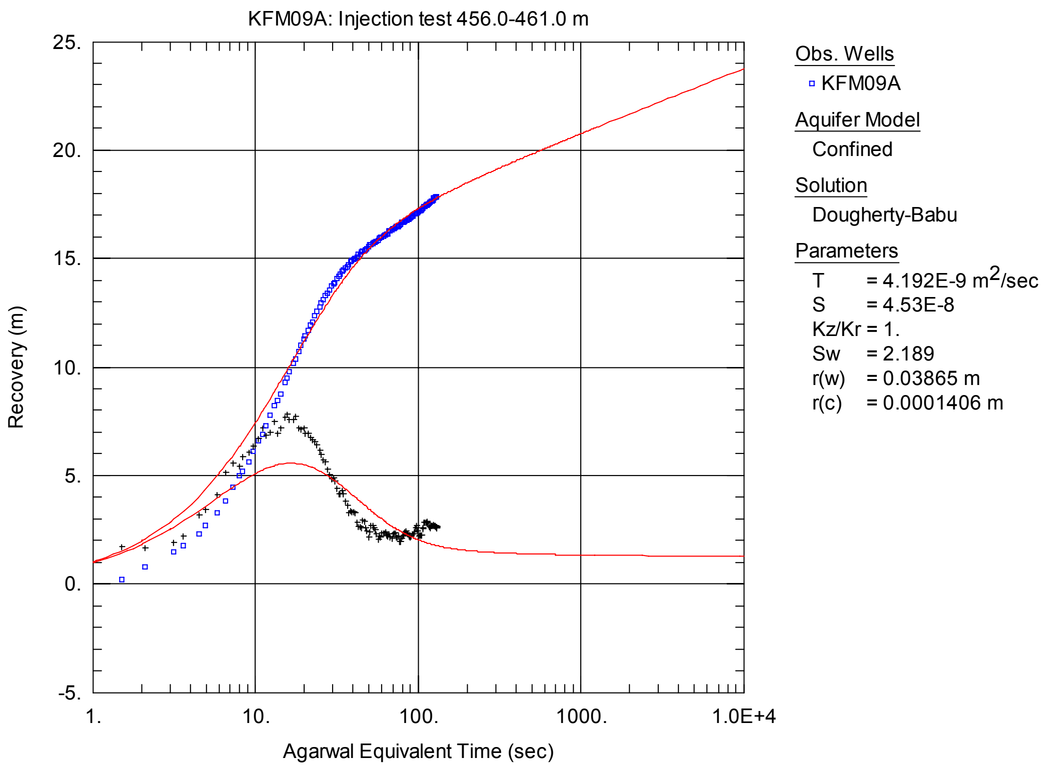


Figure A3-452. Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 456.0-461.0 m in KFM09A.

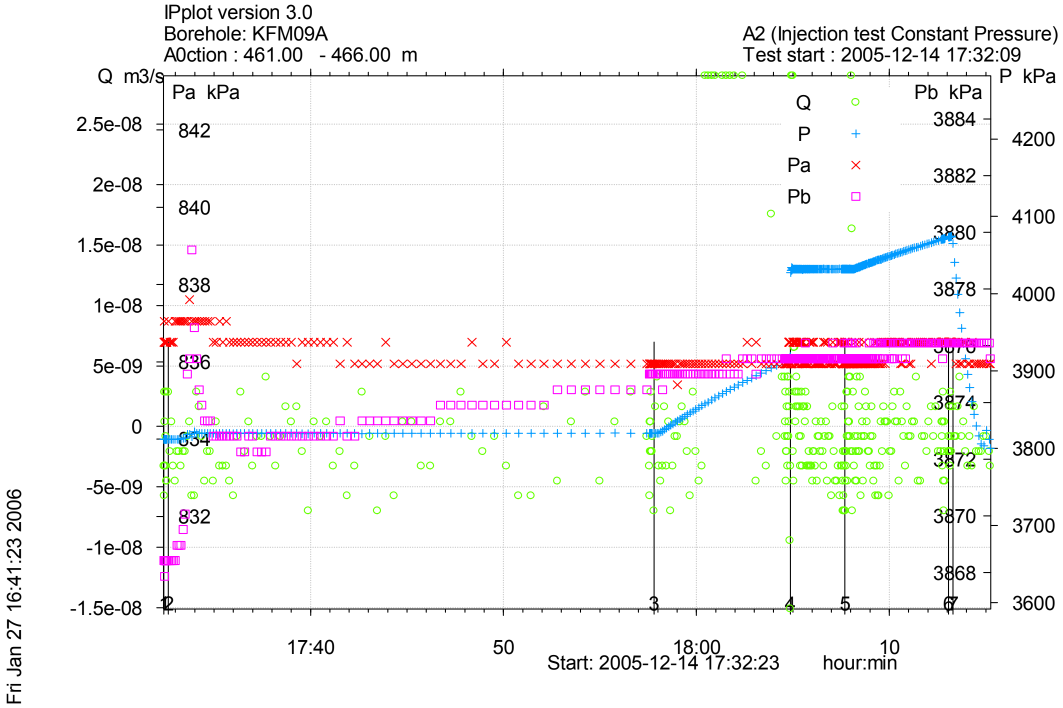


Figure A3-453. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 461.0-466.0 m in borehole KFM09A.

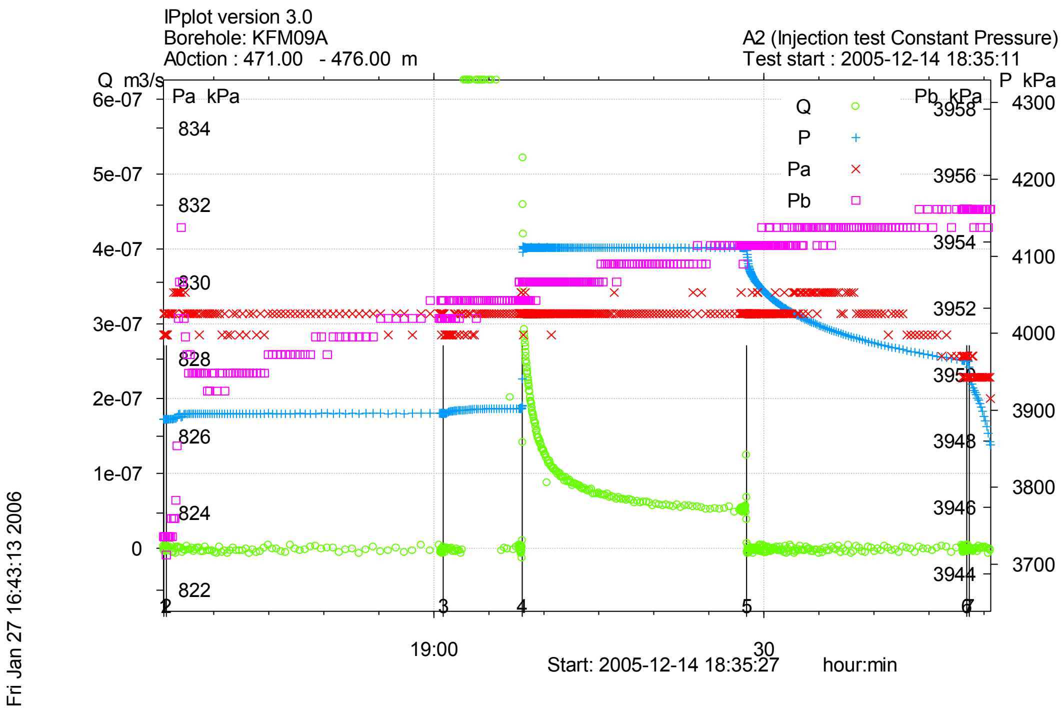


Figure A3-454. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 471.0-476.0 m in borehole KFM09A.*

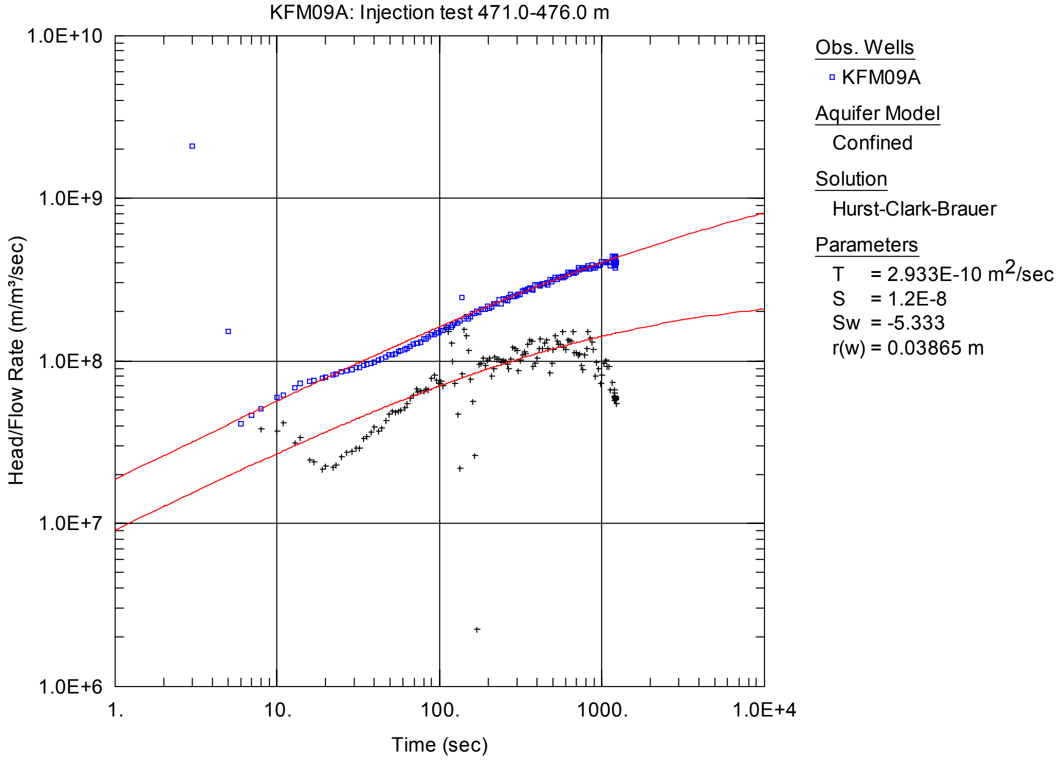


Figure A3-455. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 471.0-476.0 m in KFM09A.*

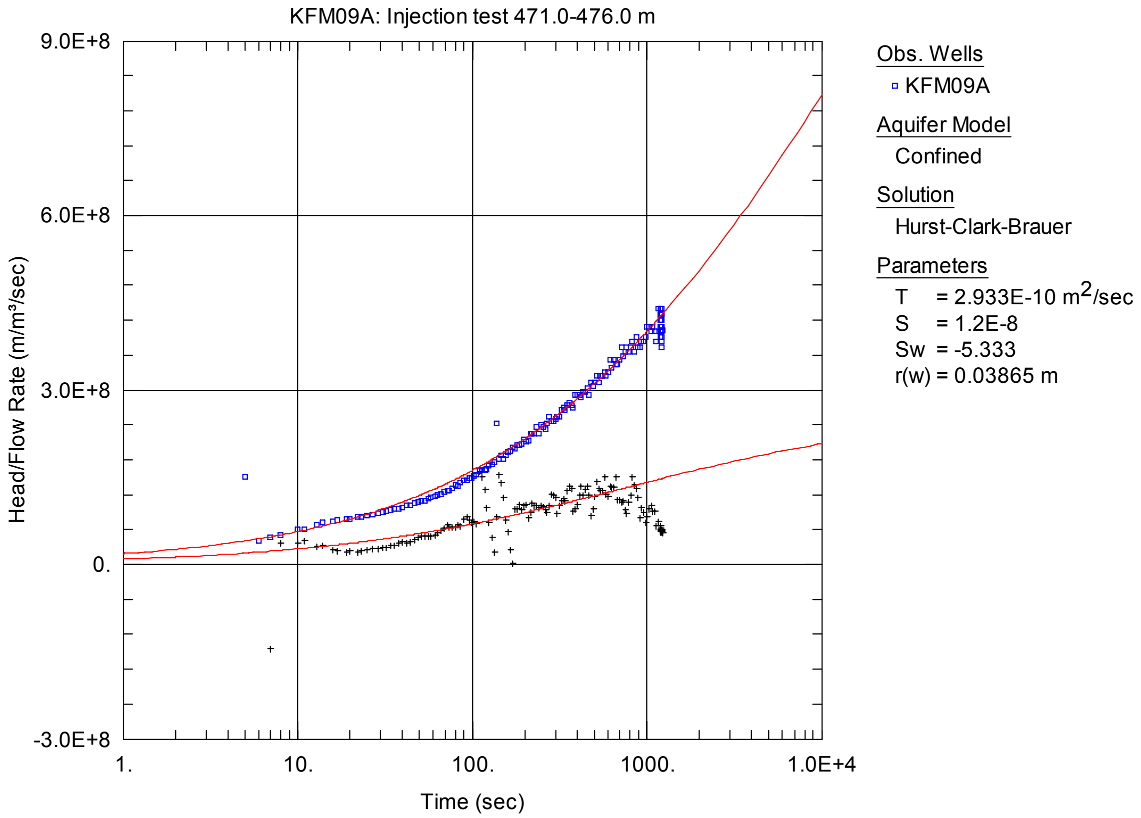


Figure A3-456. Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 471.0-476.0 m in KFM09A.

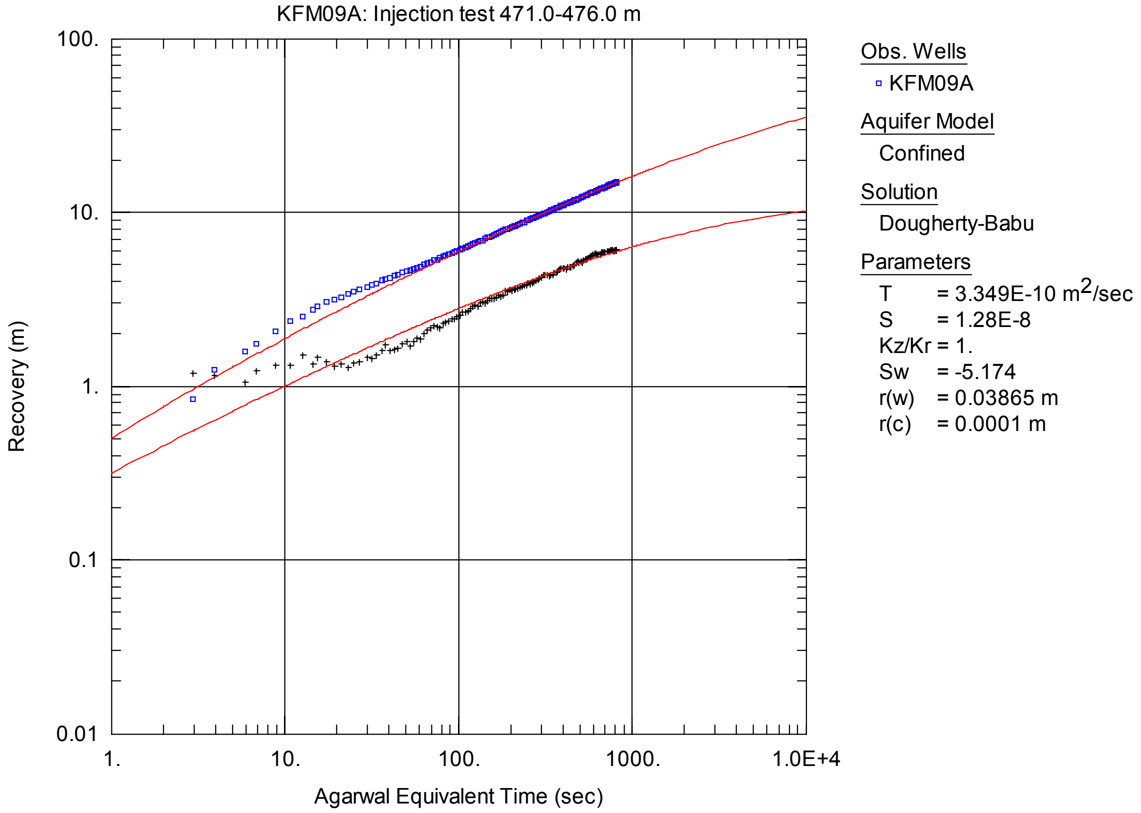


Figure A3-457. Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 471.0-476.0 m in KFM09A.

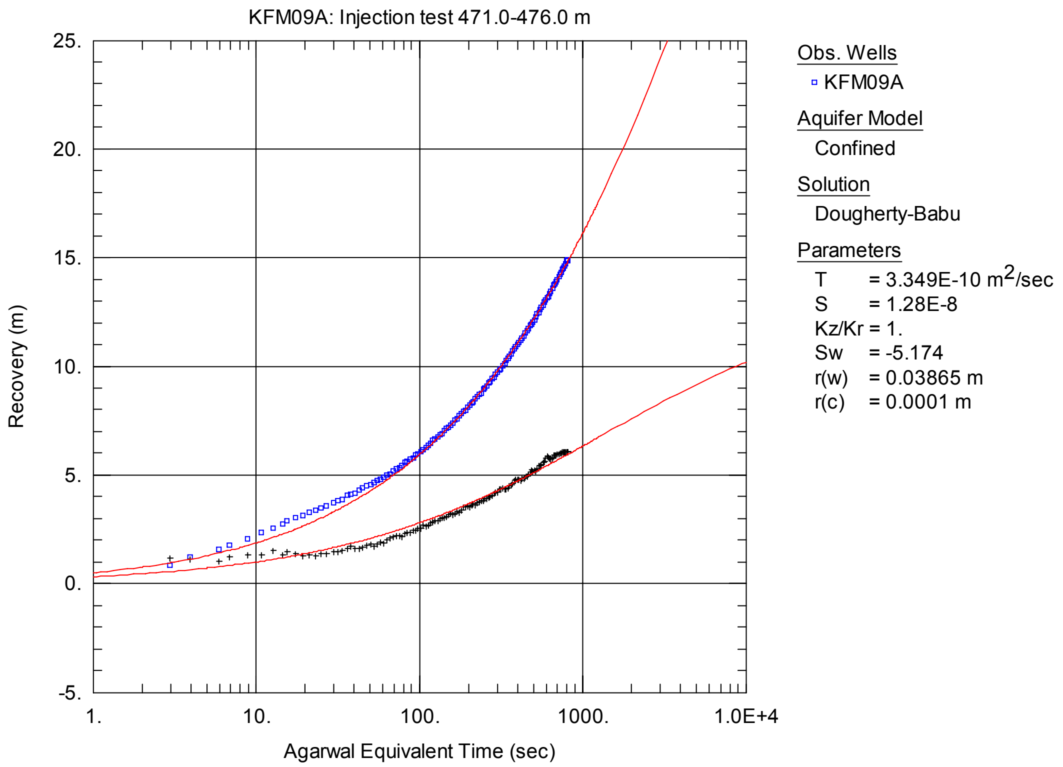


***Figure A3-458.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 471.0-476.0 m in KFM09A.*

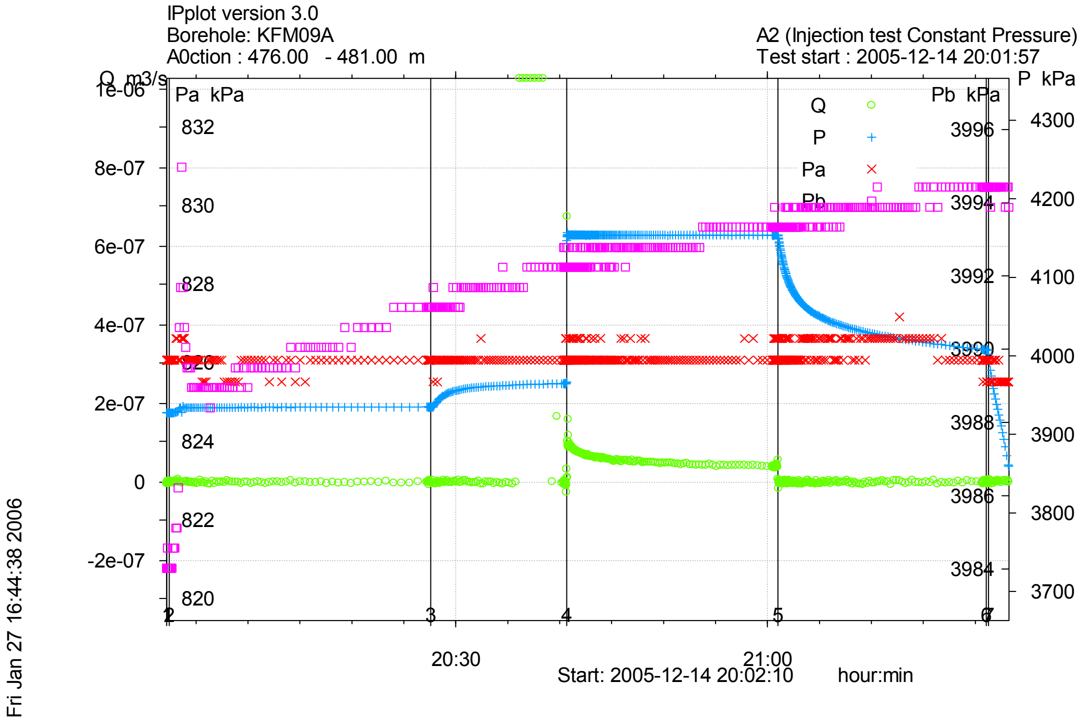


***Figure A3-459.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 476.0-481.0 m in borehole KFM09A.*

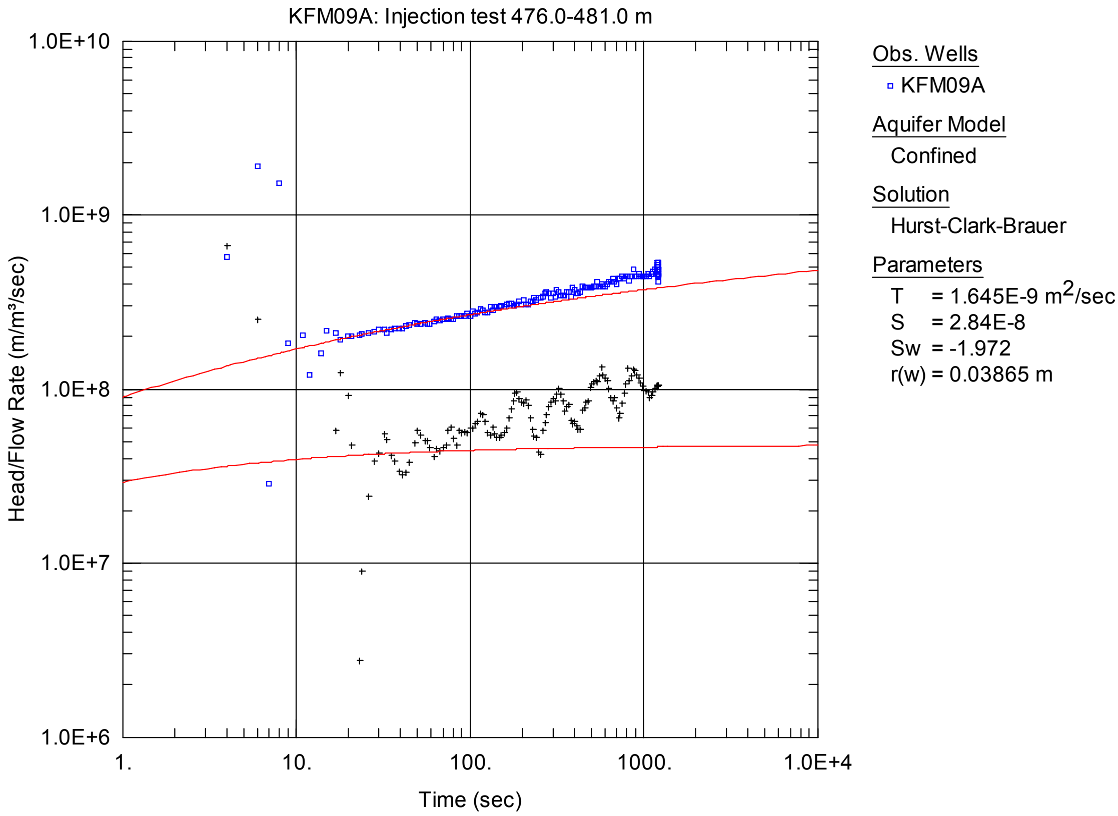


Figure A3-460. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 476.0-481.0 m in KFM09A.*

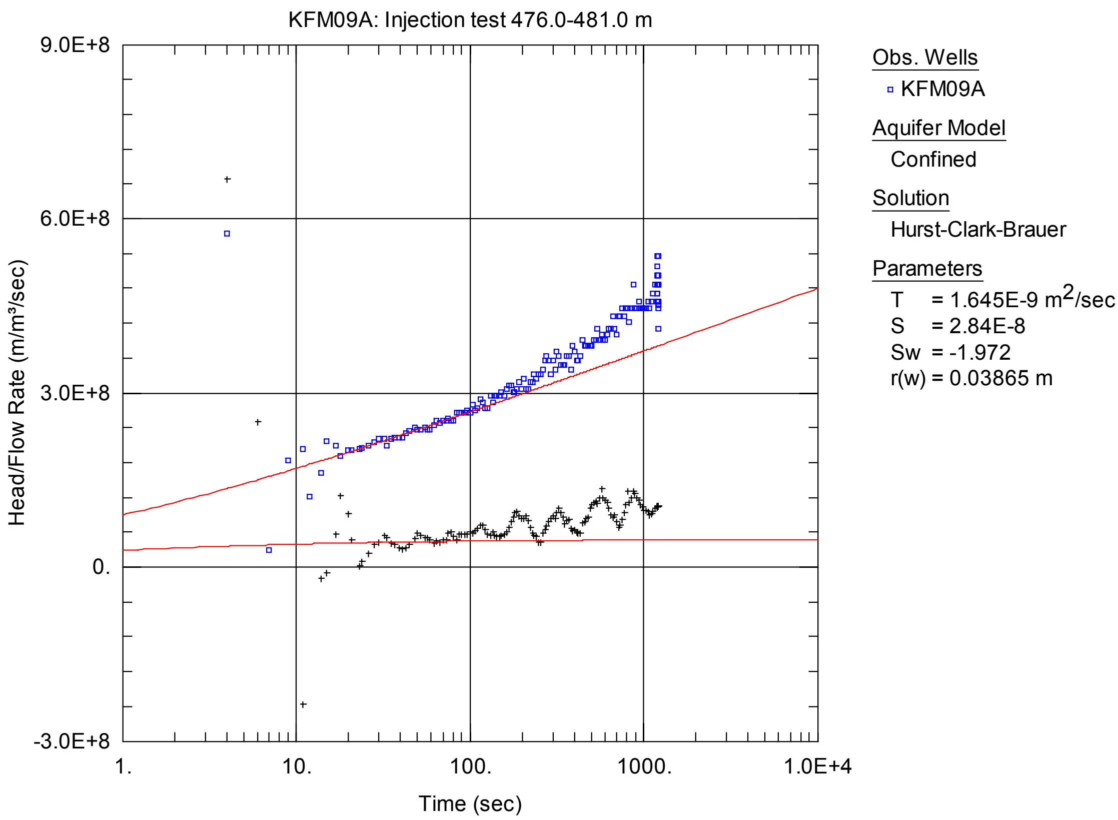


Figure A3-461. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 476.0-481.0 m in KFM09A.*

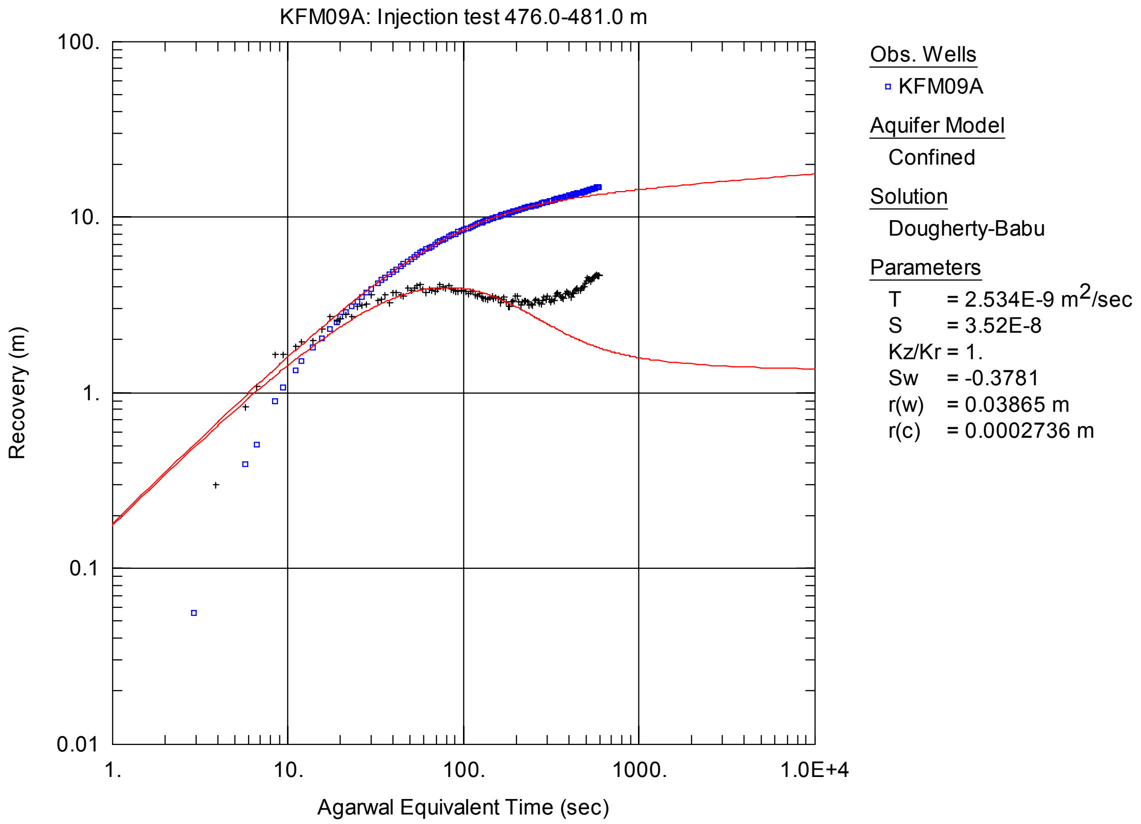


***Figure A3-462.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 476.0-481.0 m in KFM09A.*

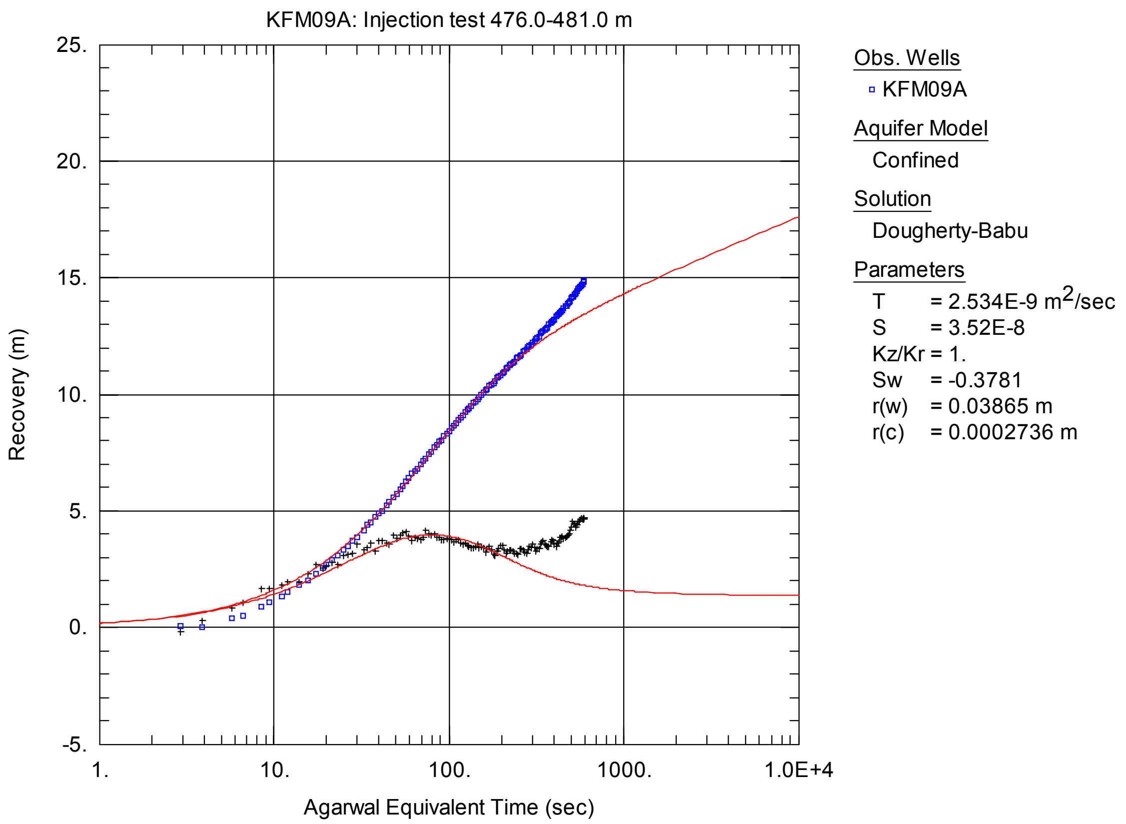


***Figure A3-463.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 476.0-481.0 m in KFM09A.*

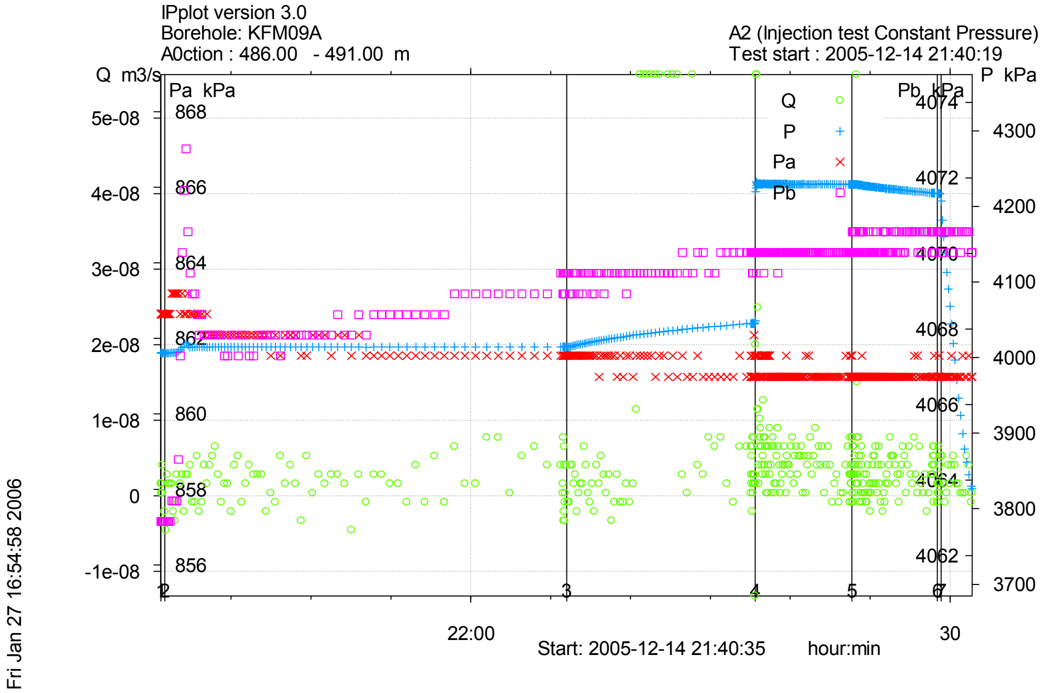


__Figure A3-464.__ Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 486.0-491.0 m in borehole KFM09A.

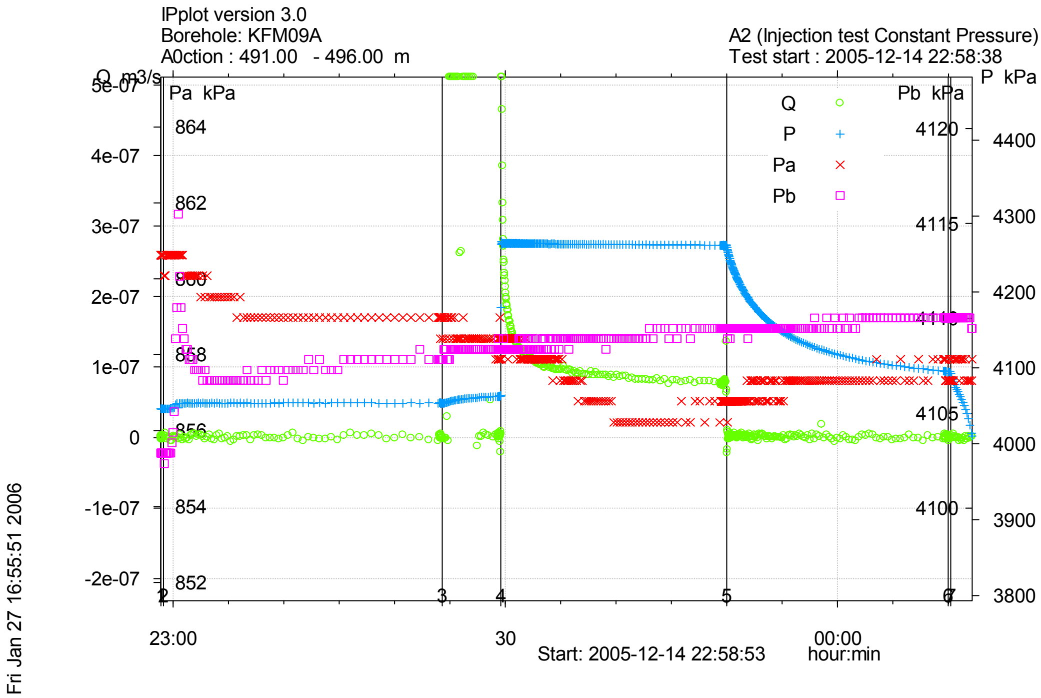


__Figure A3-465.__ Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 491.0-496.0 m in borehole KFM09A.

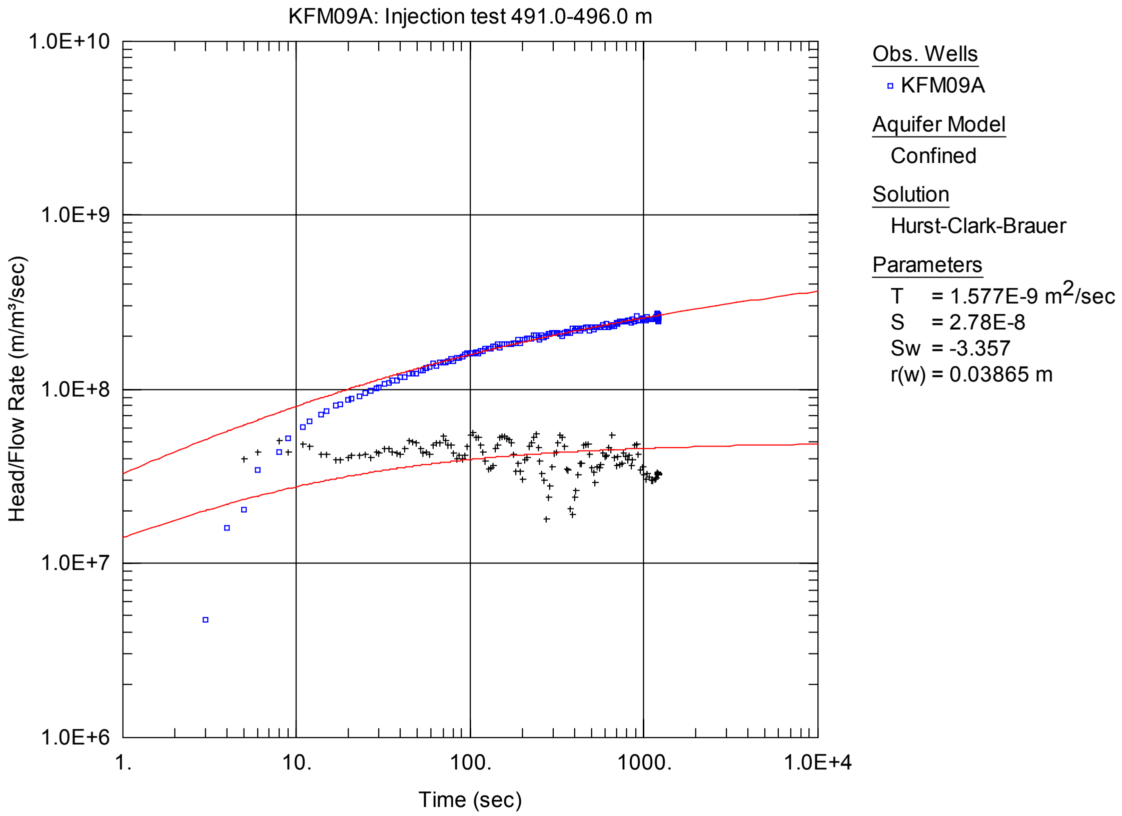


Figure A3-466. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 491.0-496.0 m in KFM09A.*

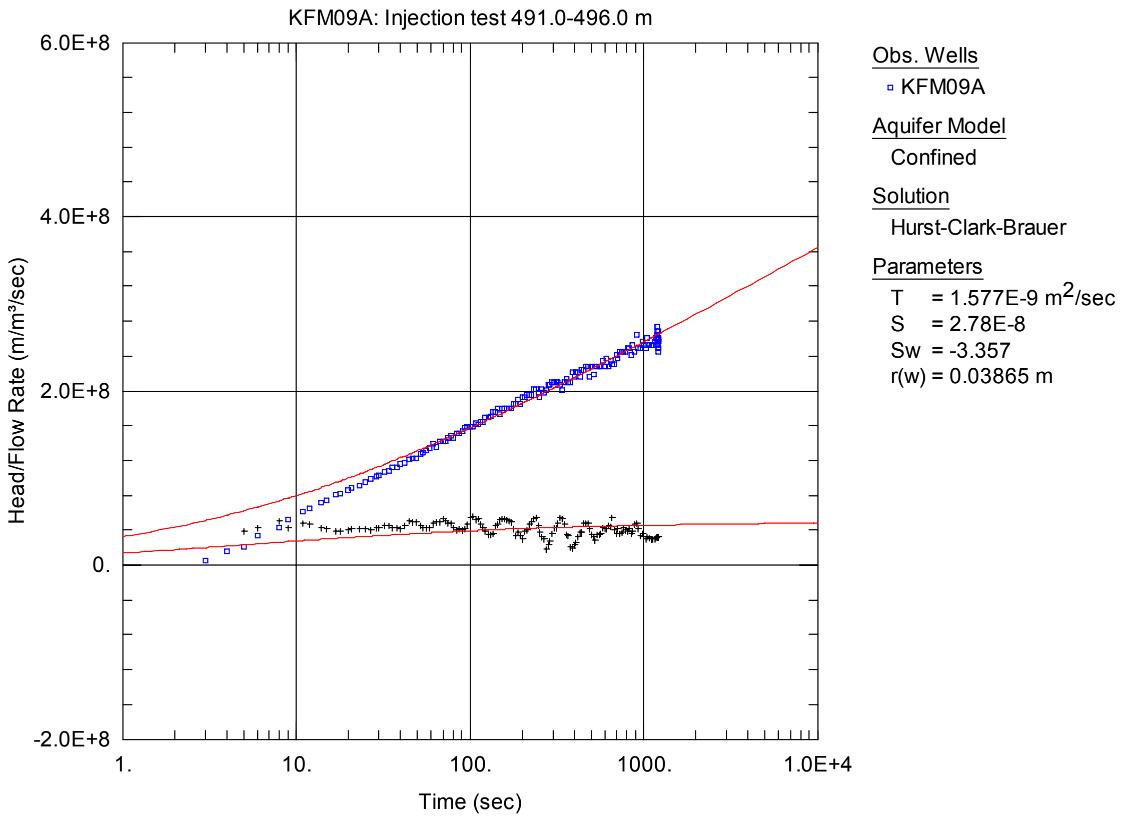


Figure A3-467. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 491.0-496.0 m in KFM09A.*

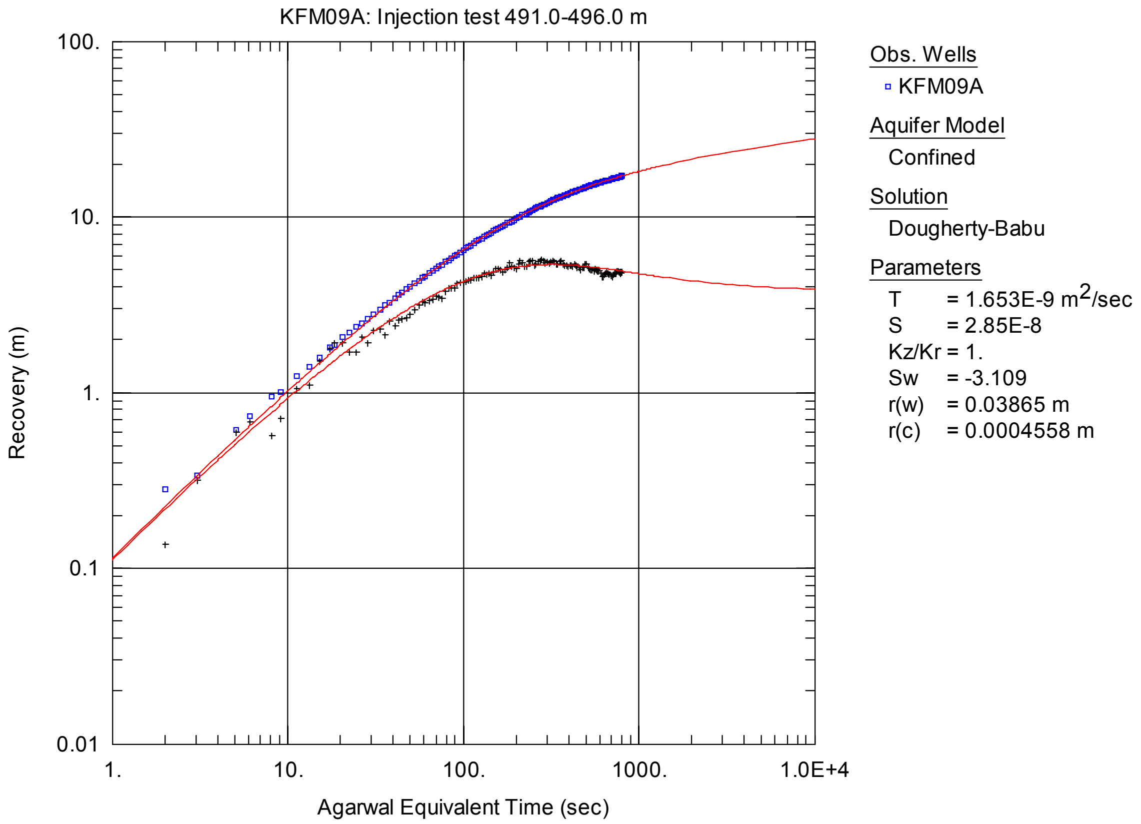


***Figure A3-468.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 491.0-496.0 m in KFM09A.*

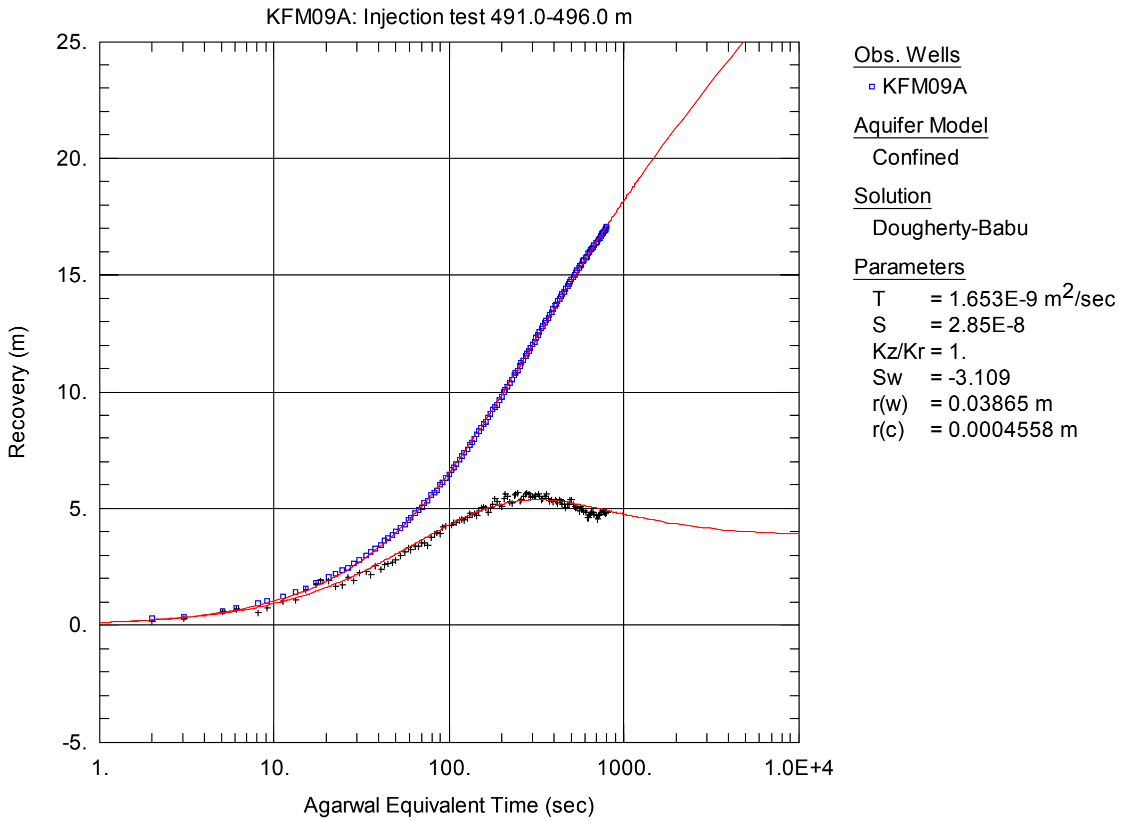


***Figure A3-469.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 491.0-496.0 m in KFM09A.*

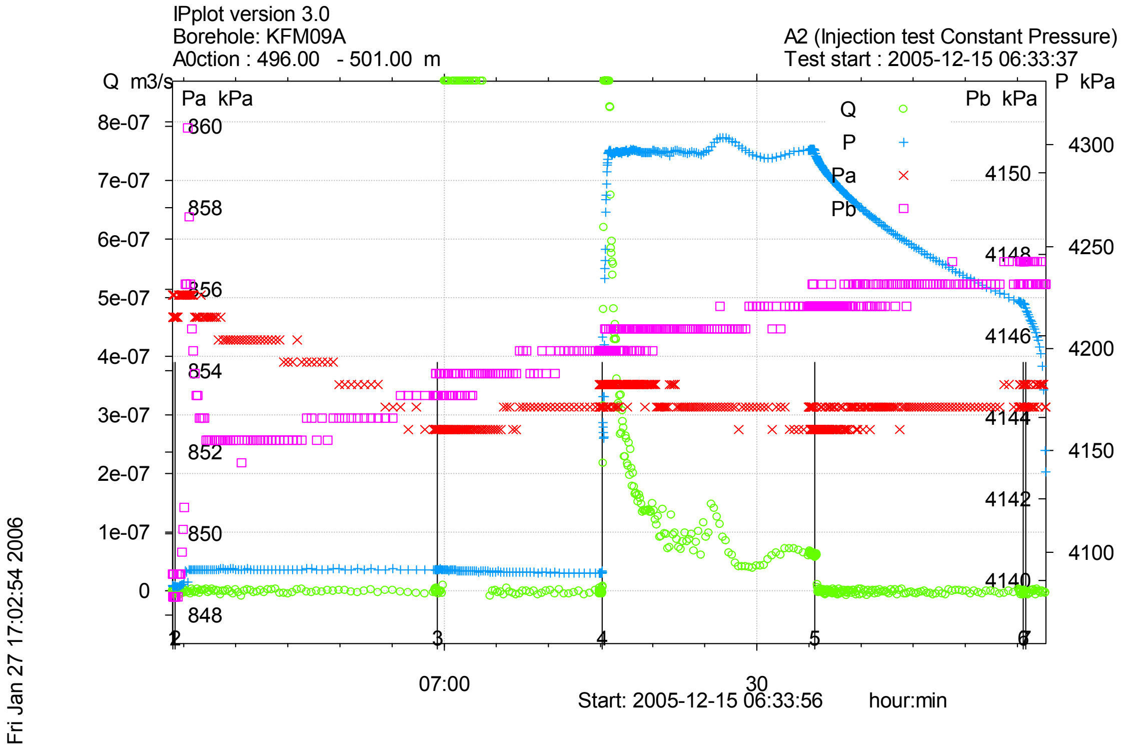


Figure A3-470. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 496.0-501.0 m in borehole KFM09A.*

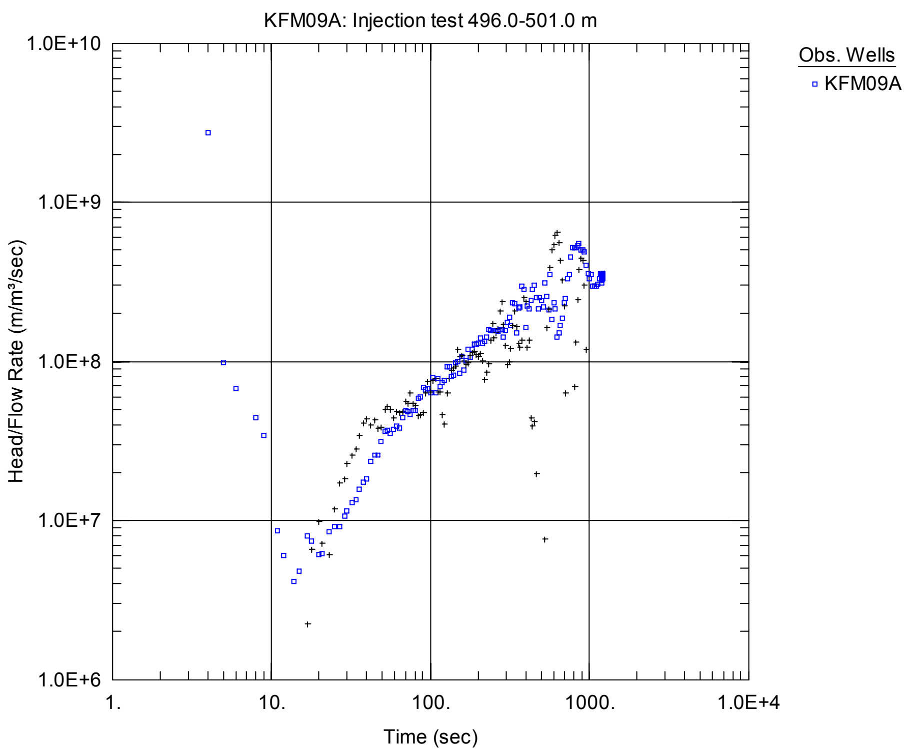


Figure A3-471. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 496.0-501.0 m in KFM09A.*

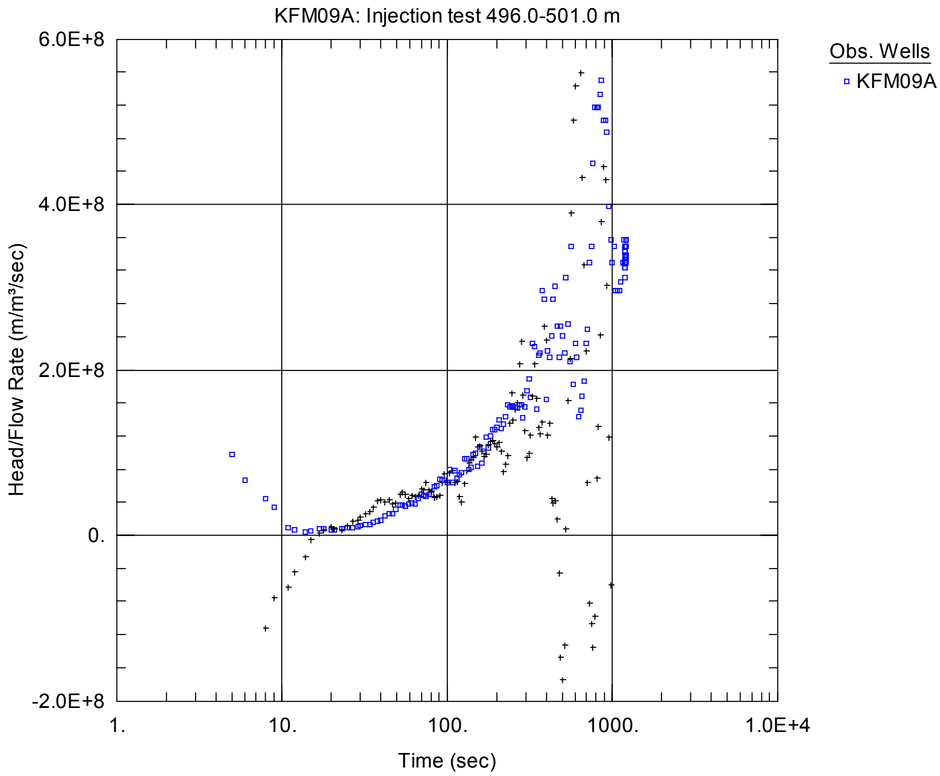


***Figure A3-472.** Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 496.0-501.0 m in KFM09A.*

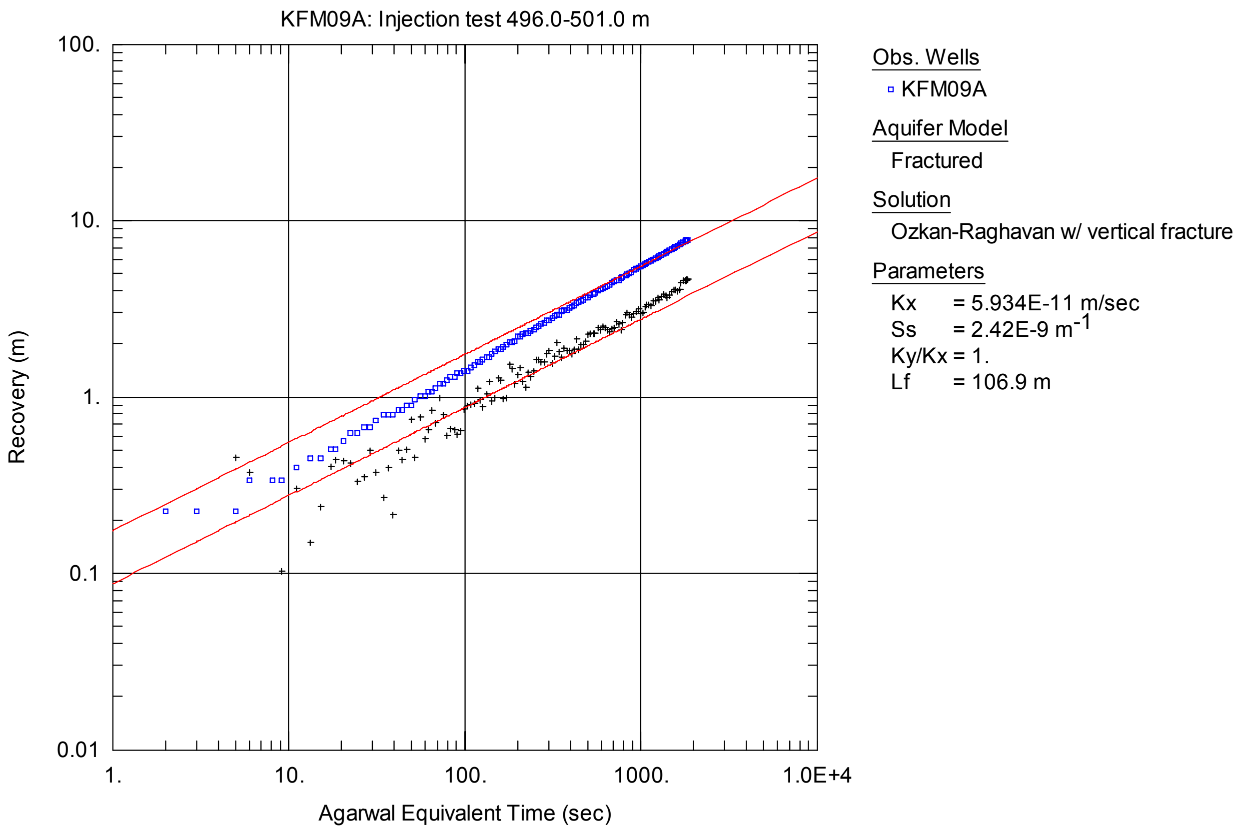


***Figure A3-473.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 496.0-501.0 m in KFM09A.*

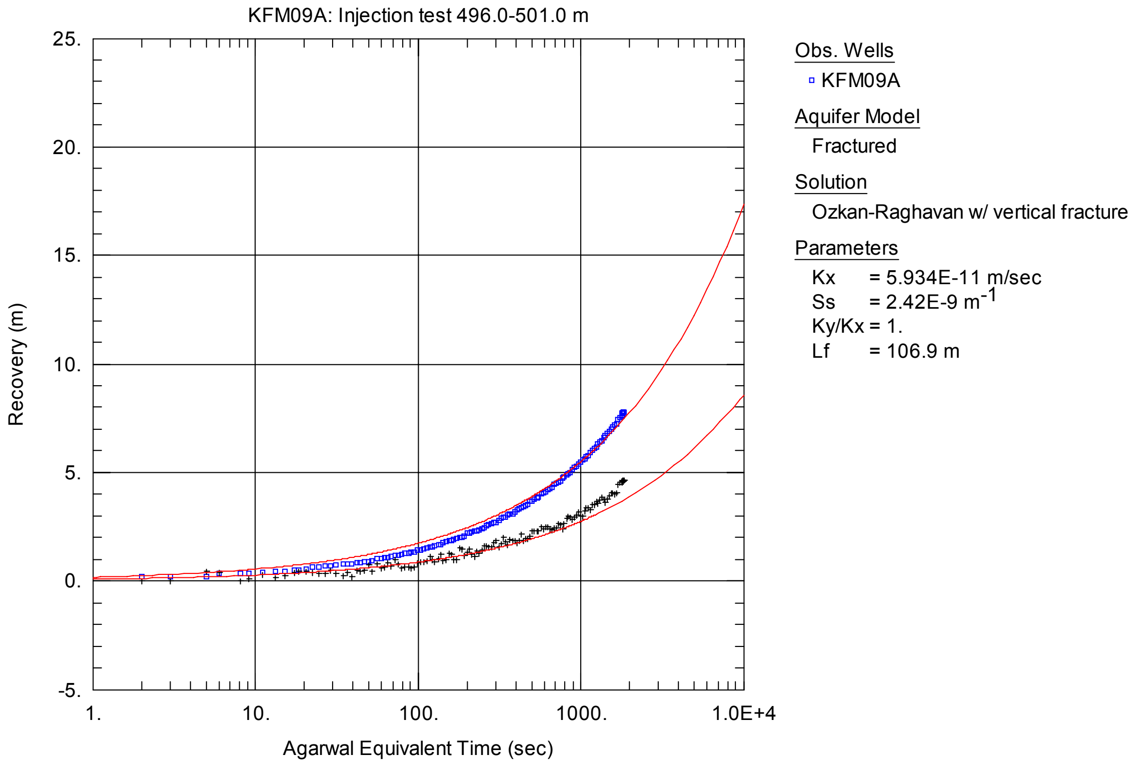


Figure A3-474. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 496.0-501.0 m in KFM09A.*

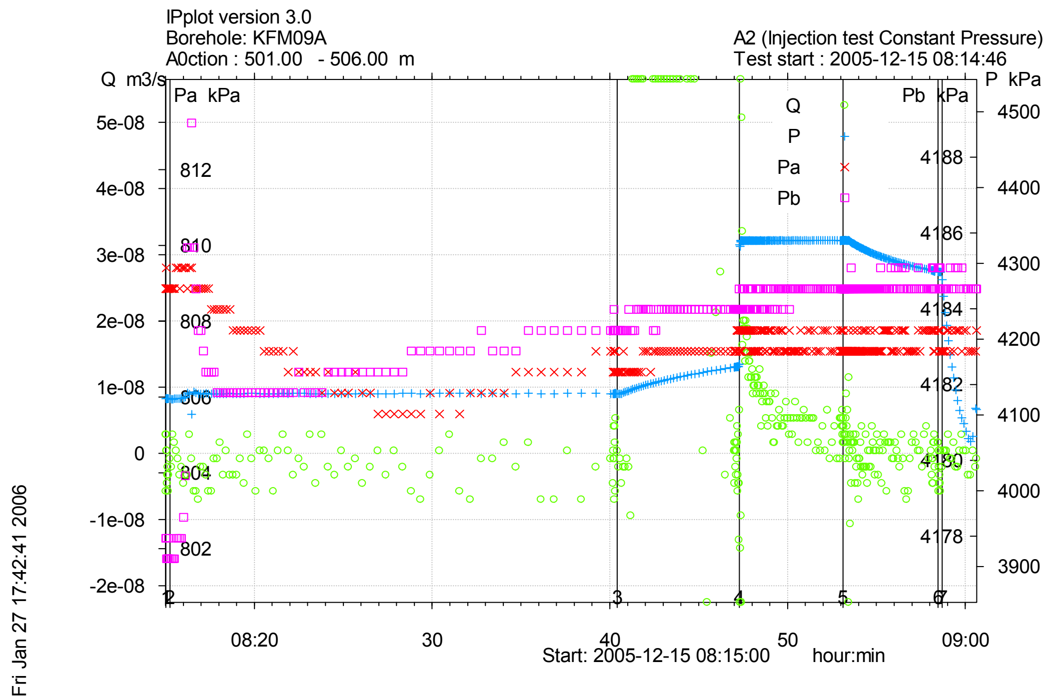


Figure A3-475. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 501.0-506.0 m in borehole KFM09A.*

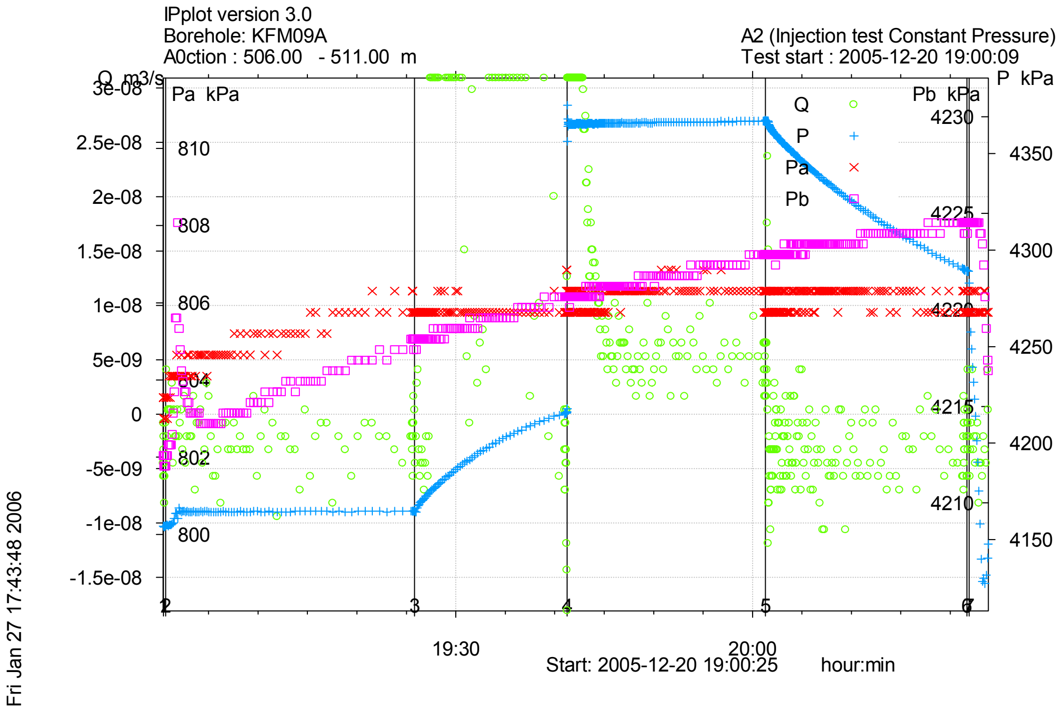


Figure A3-476. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 506.0-511.0 m in borehole KFM09A.

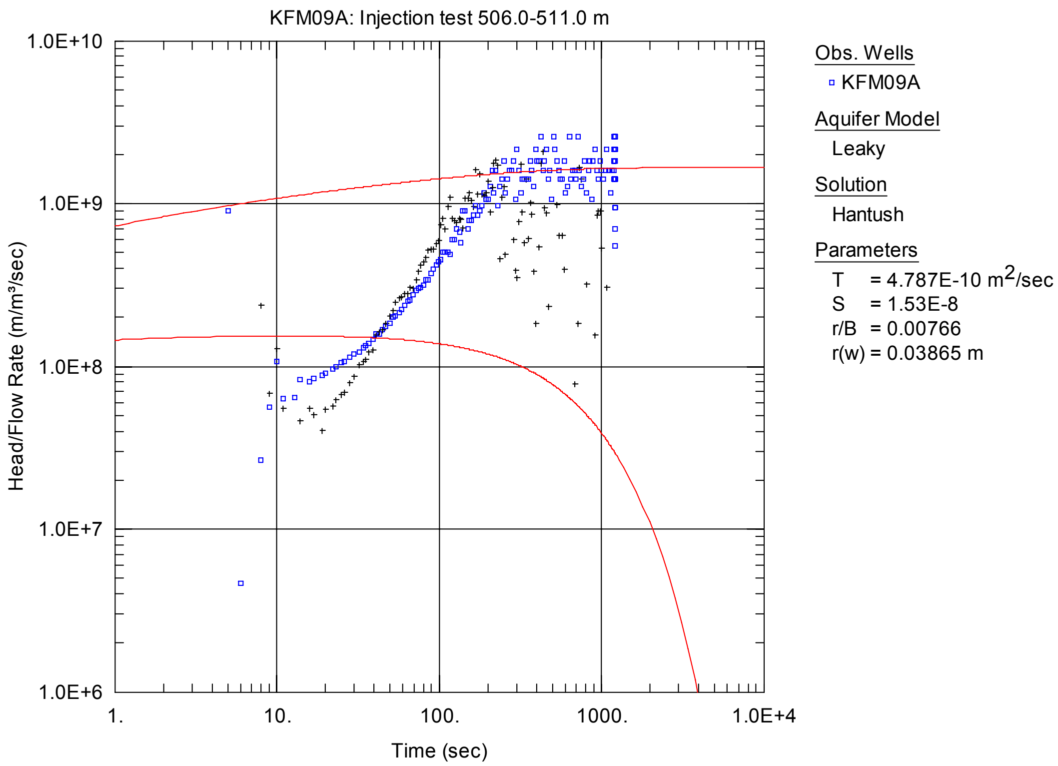


Figure A3-477. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 506.0-511.0 m in KFM09A.

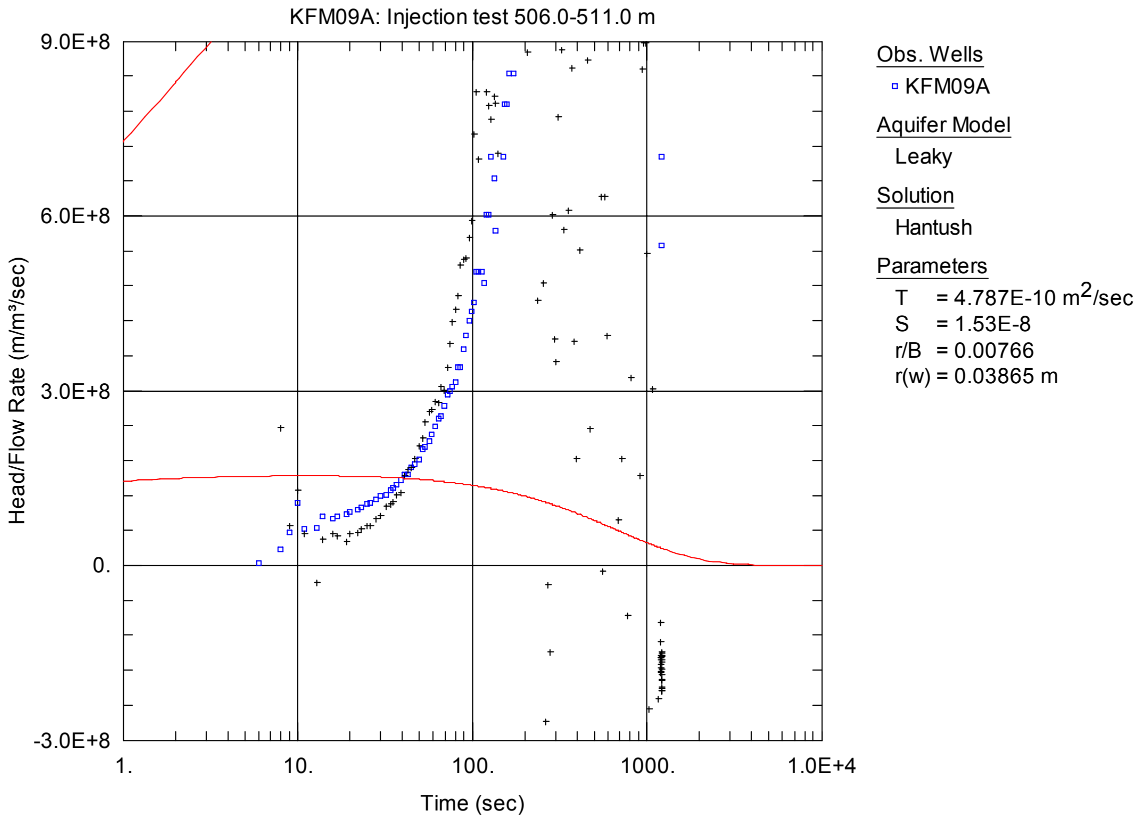


***Figure A3-478.** Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 506.0-511.0 m in KFM09A.*

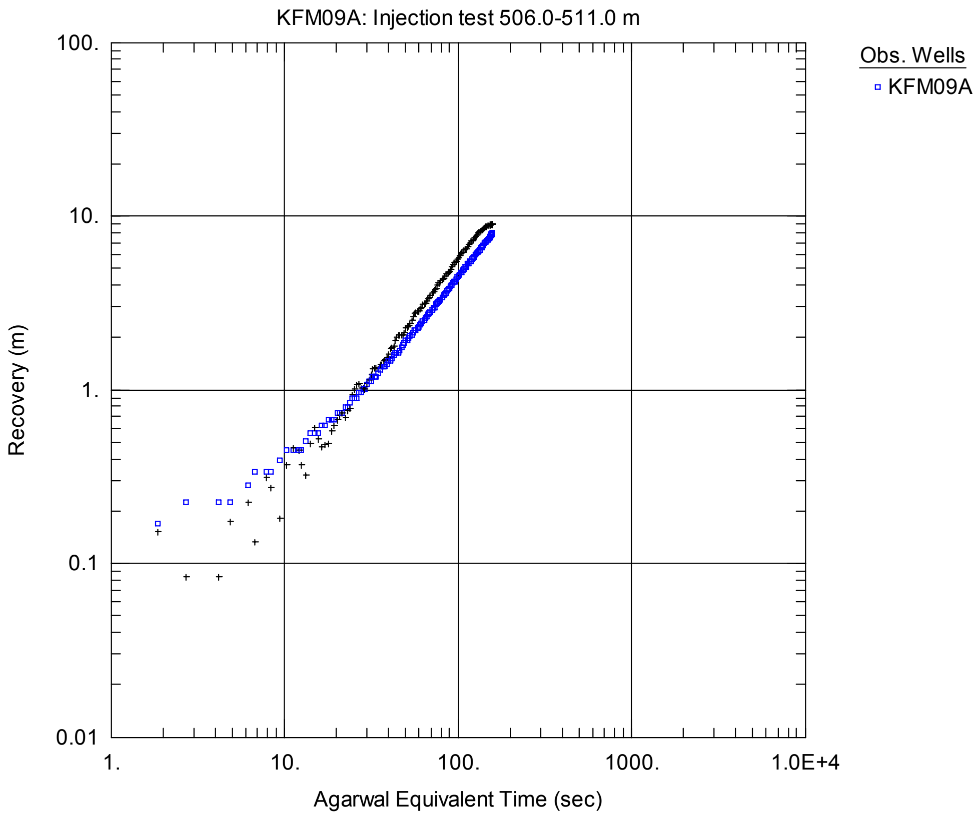


***Figure A3-479.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 506.0-511.0 m in KFM09A.*

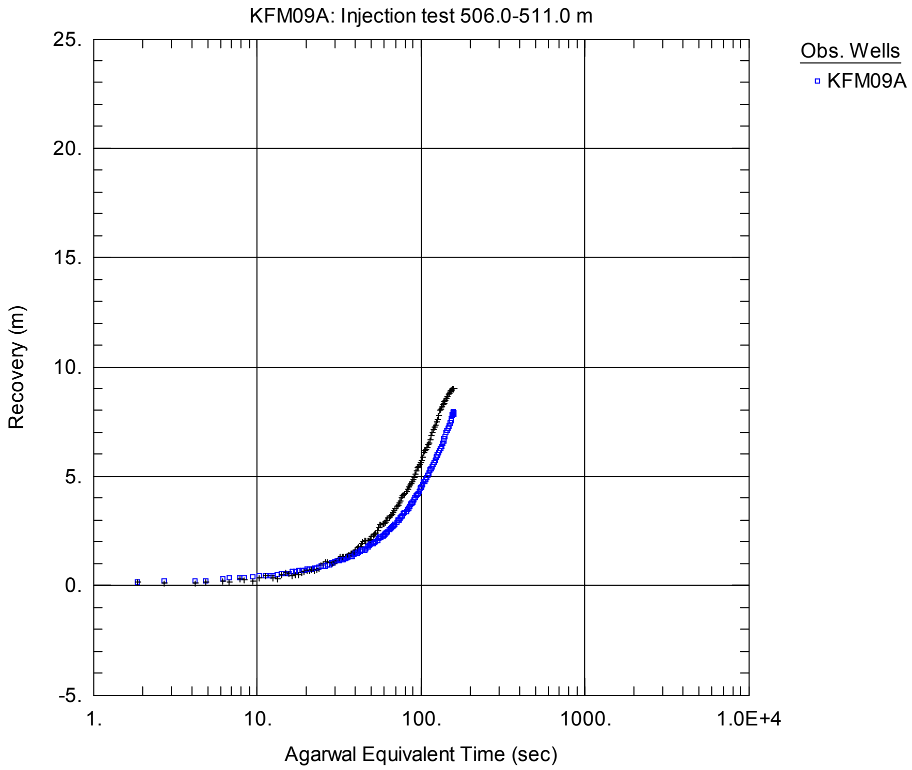


Figure A3-480. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 506.0-511.0 m in KFM09A.*

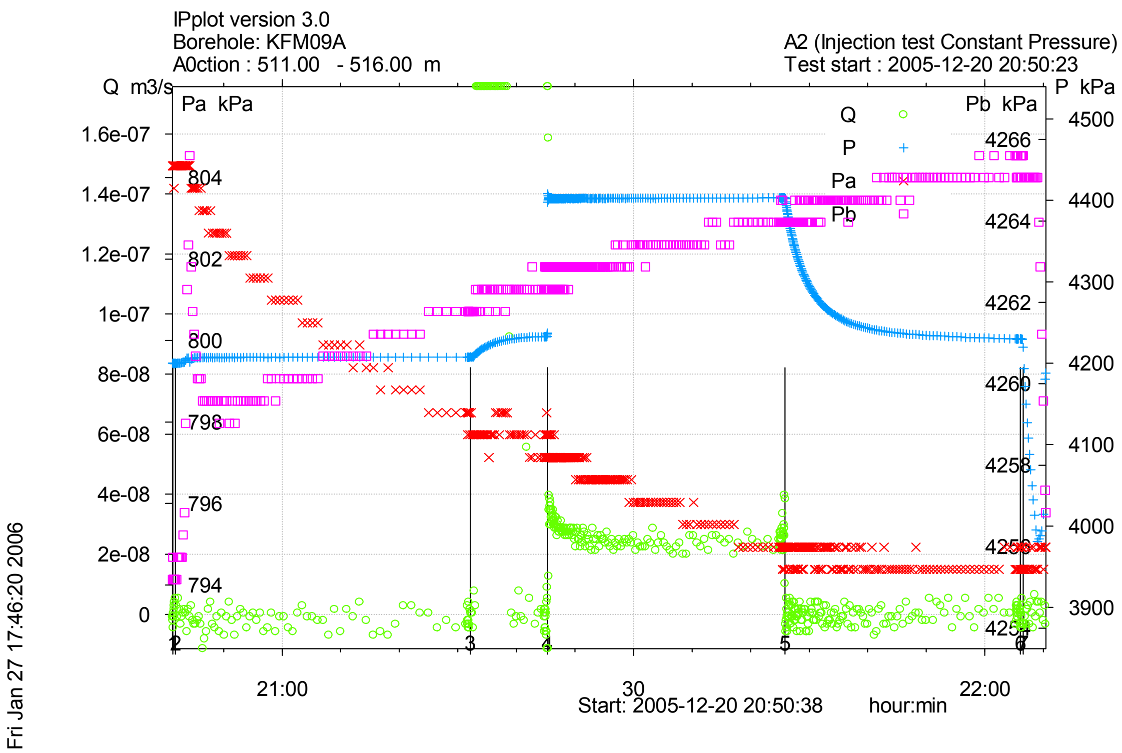


Figure A3-481. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 511.0-516.0 m in borehole KFM09A.*

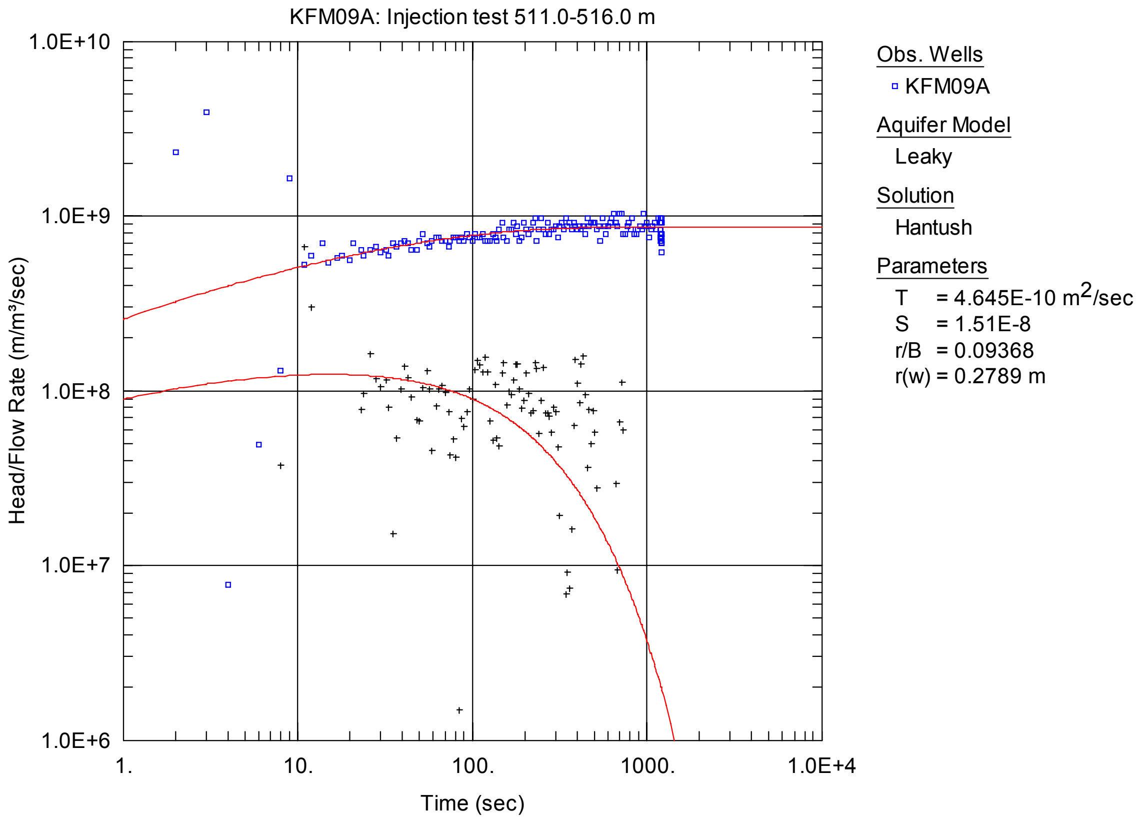


Figure A3-482. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 511.0-516.0 m in KFM09A.*

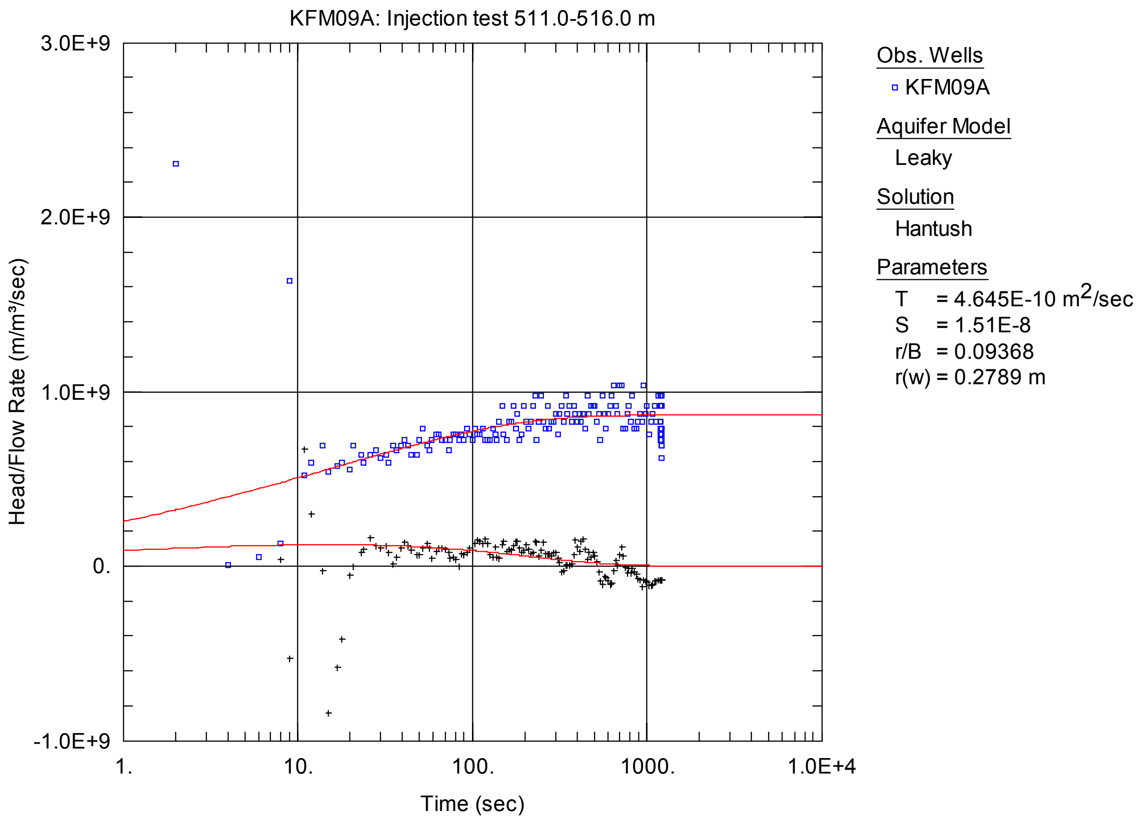


Figure A3-483. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 511.0-516.0 m in KFM09A.*

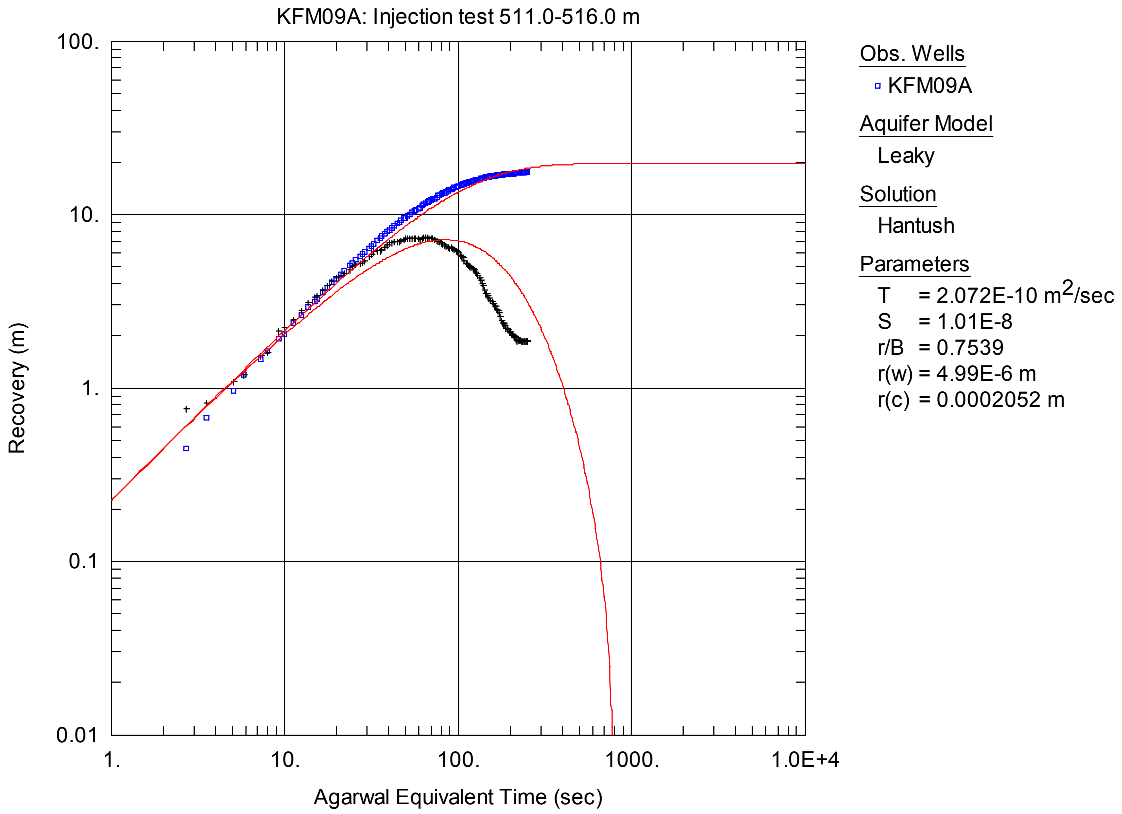


Figure A3-484. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 511.0-516.0 m in KFM09A.*

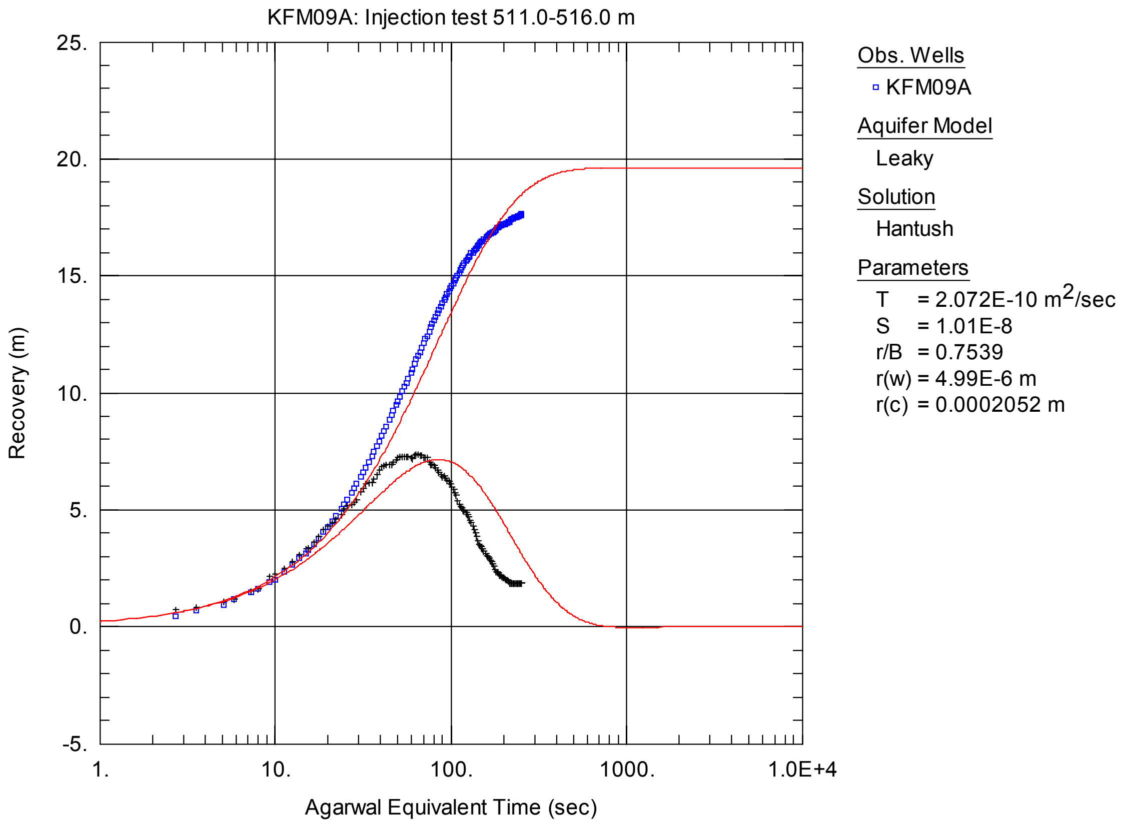


Figure A3-485. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 511.0-516.0 m in KFM09A.*

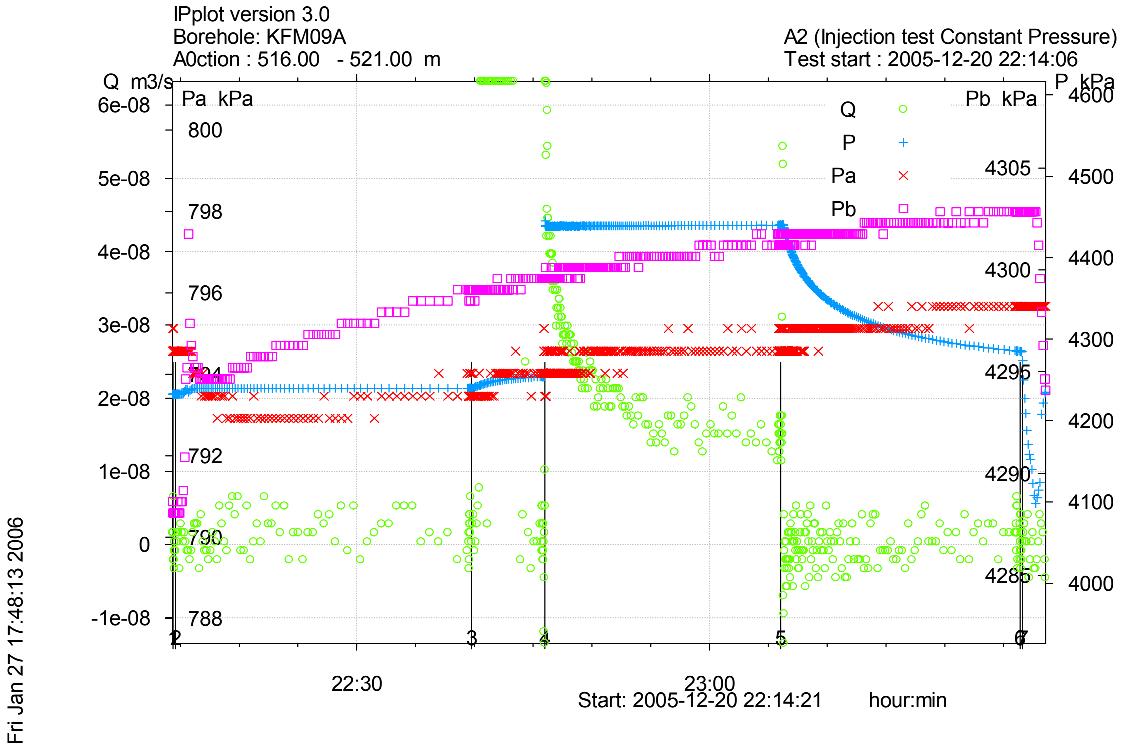


Figure A3-486. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 516.0-521.0 m in borehole KFM09A.*

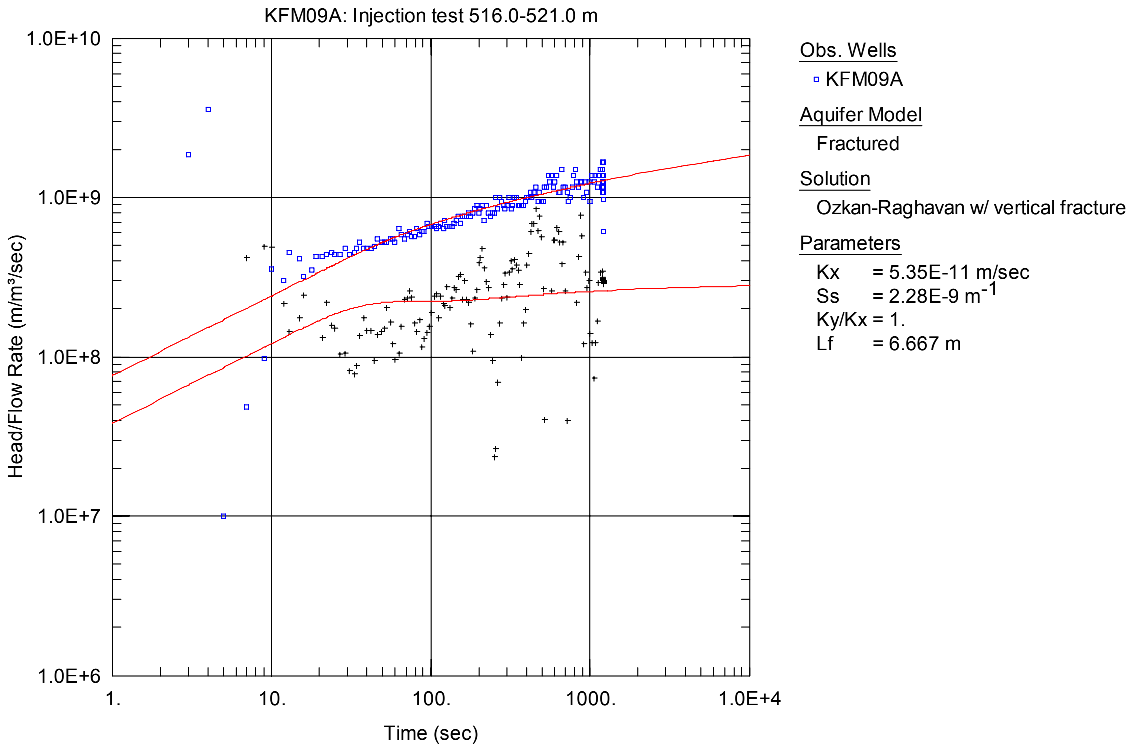


Figure A3-487. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 516.0-521.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

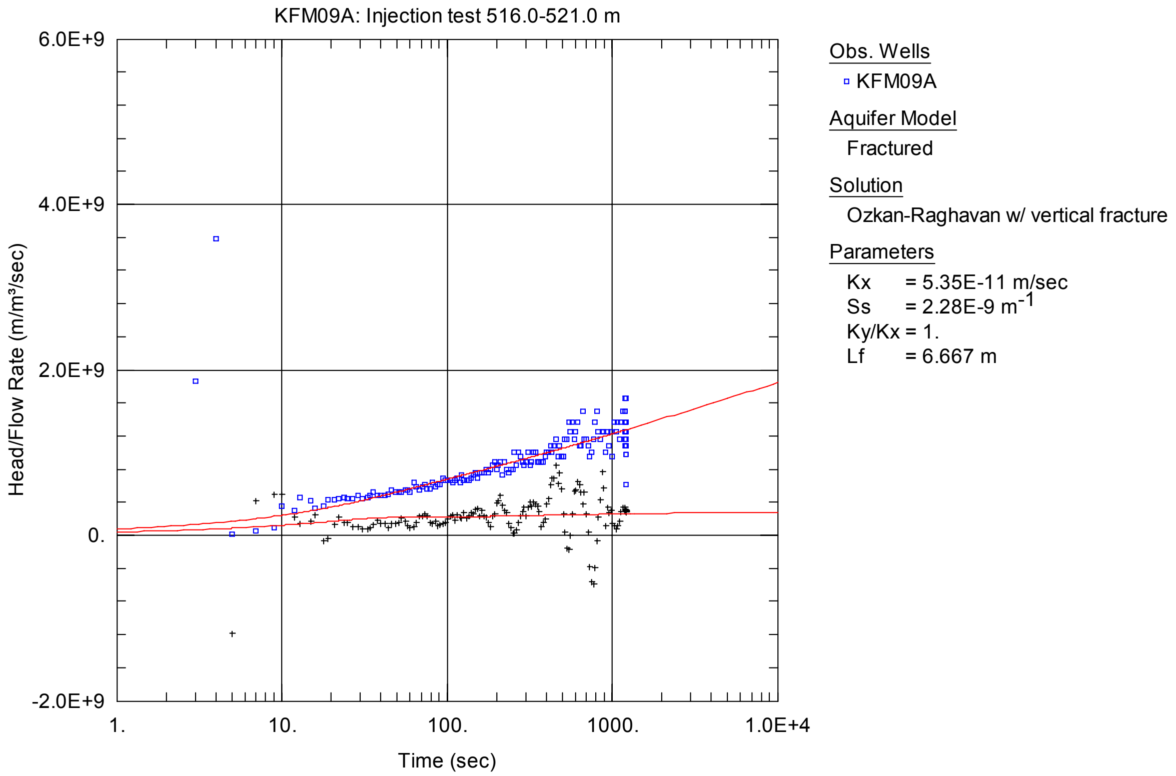


Figure A3-488. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 516.0-521.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

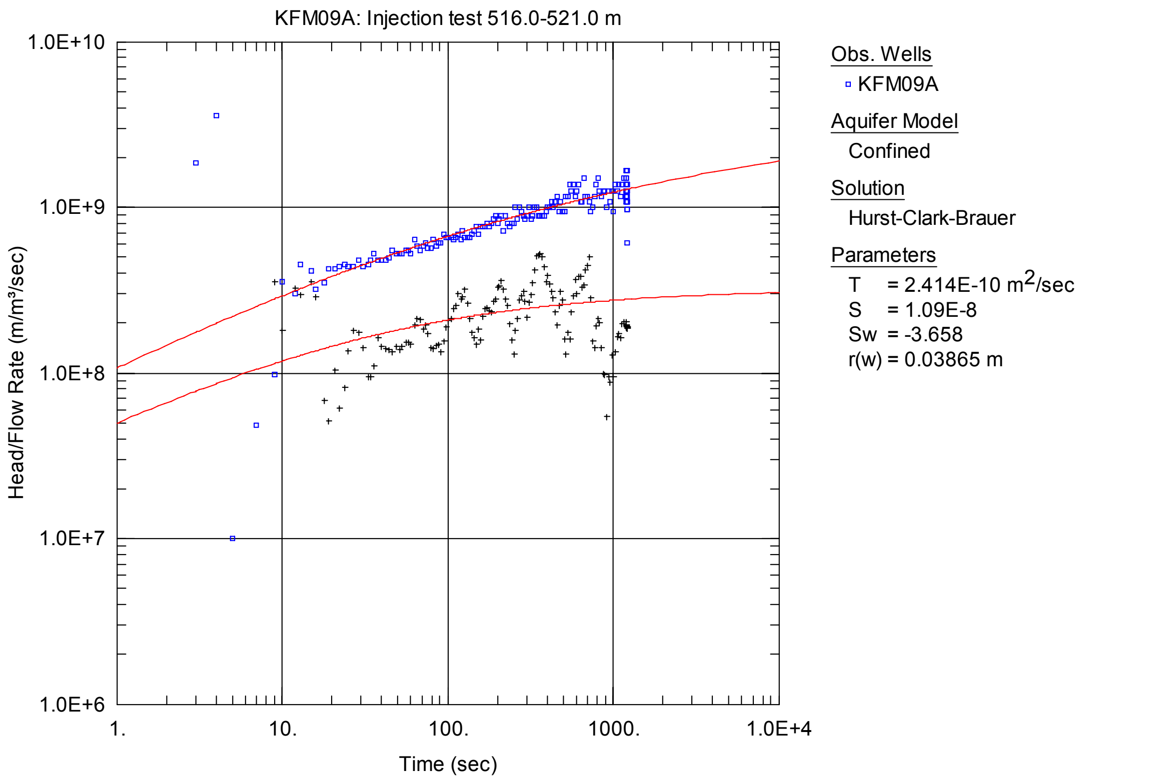


Figure A3-489. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 516.0-521.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for a pseudo-radial response.*

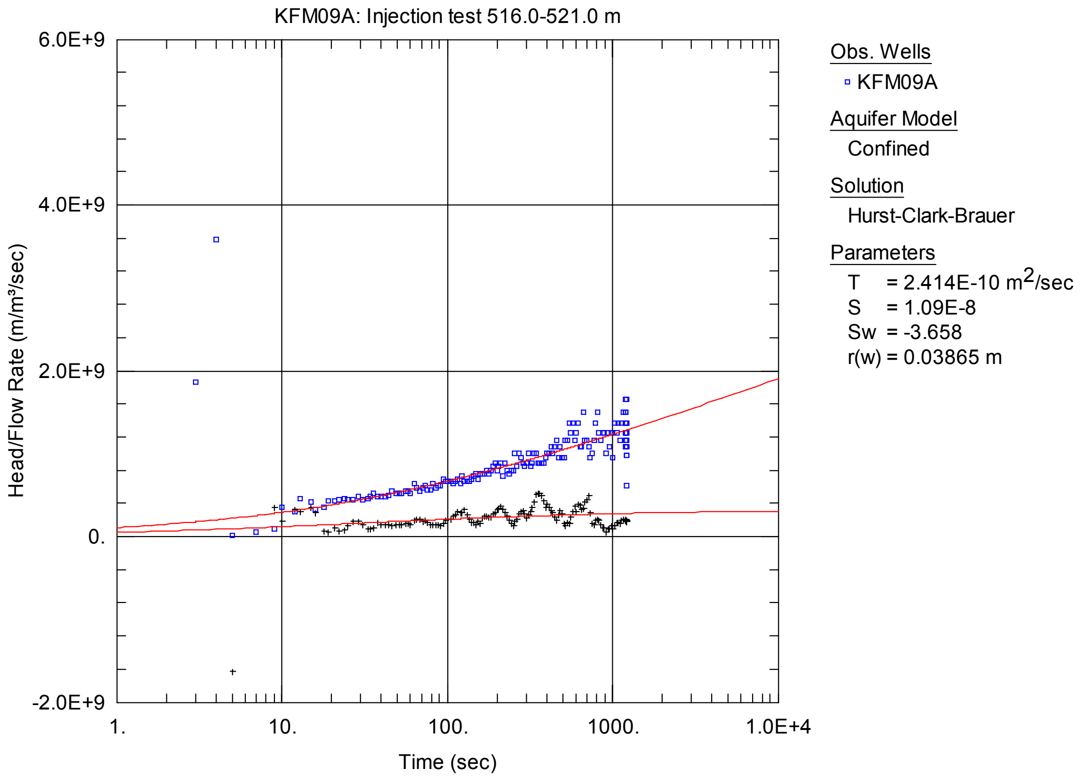


Figure A3-490. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 516.0-521.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for a pseudo-radial response.*

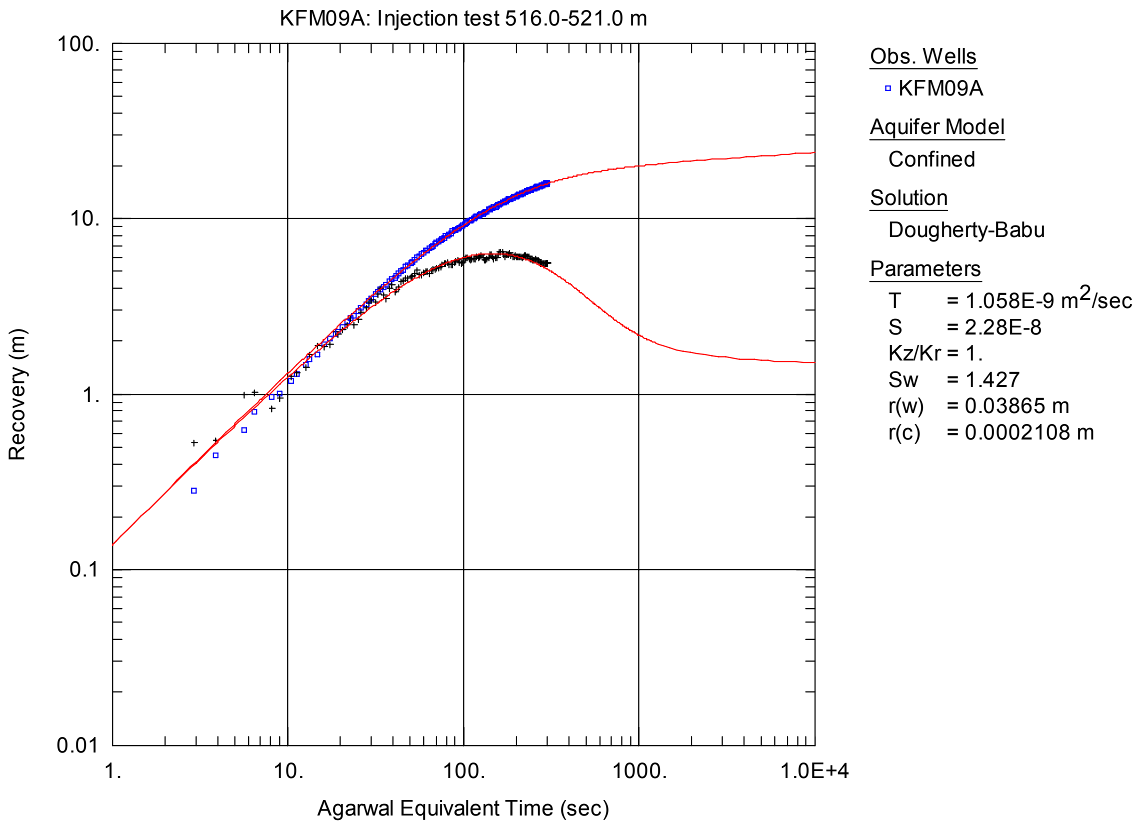


Figure A3-491. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 516.0-521.0 m in KFM09A.*

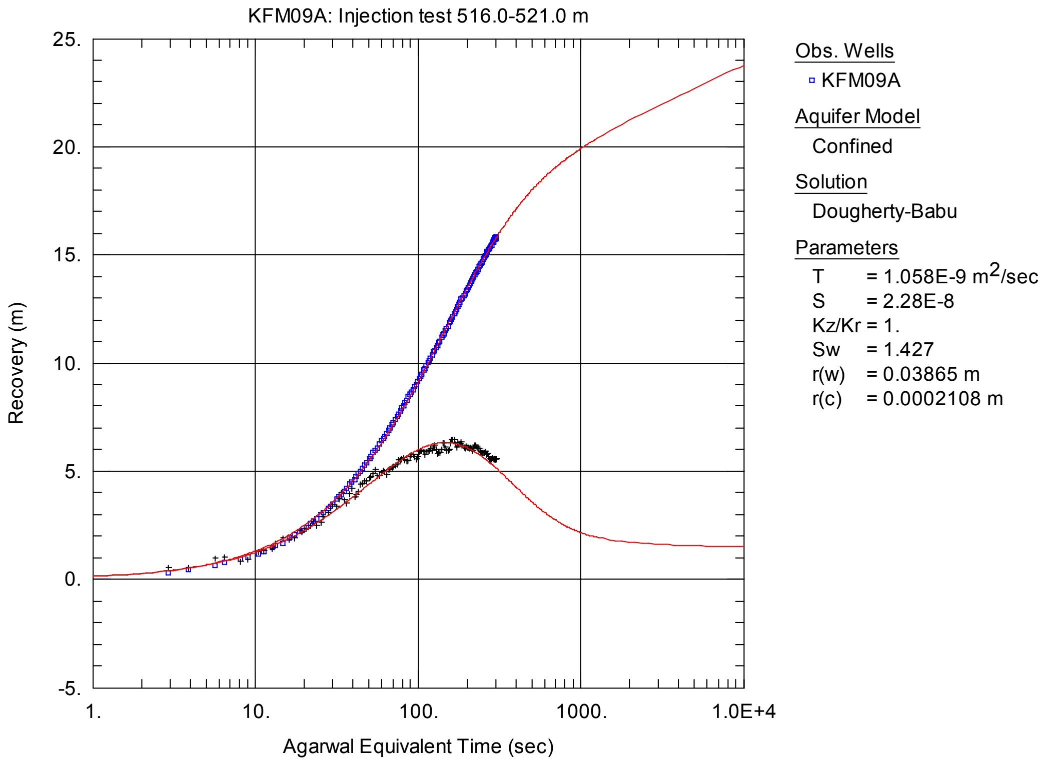


Figure A3-492. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 516.0-521.0 m in KFM09A.*

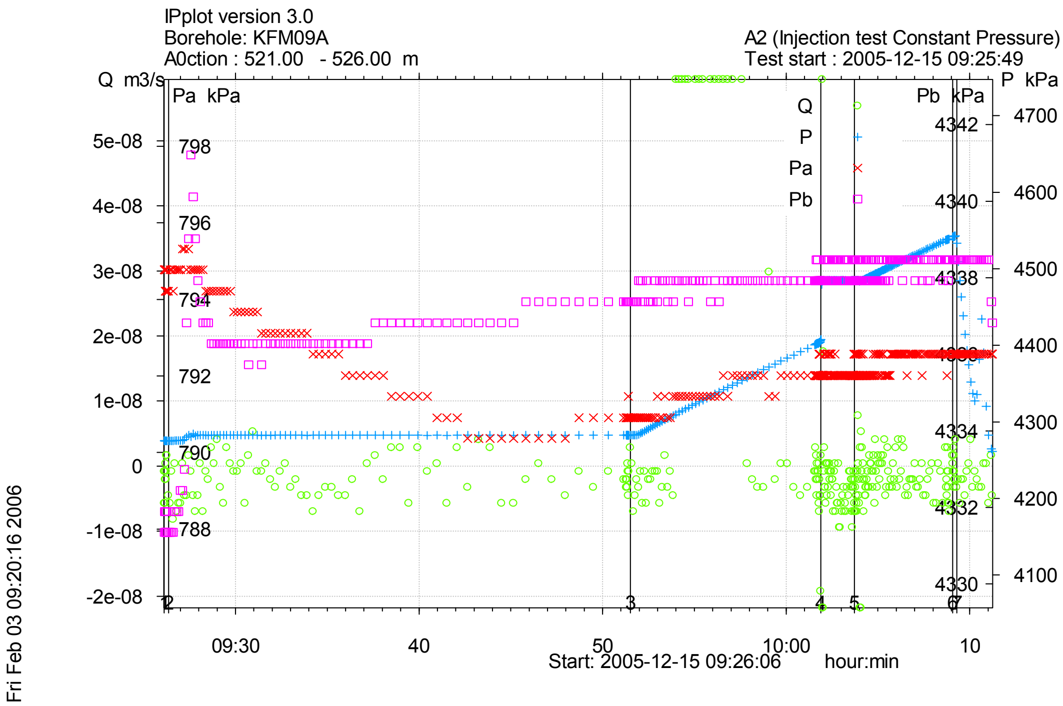


Figure A3-493. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 521.0-526.0 m in borehole KFM09A.*

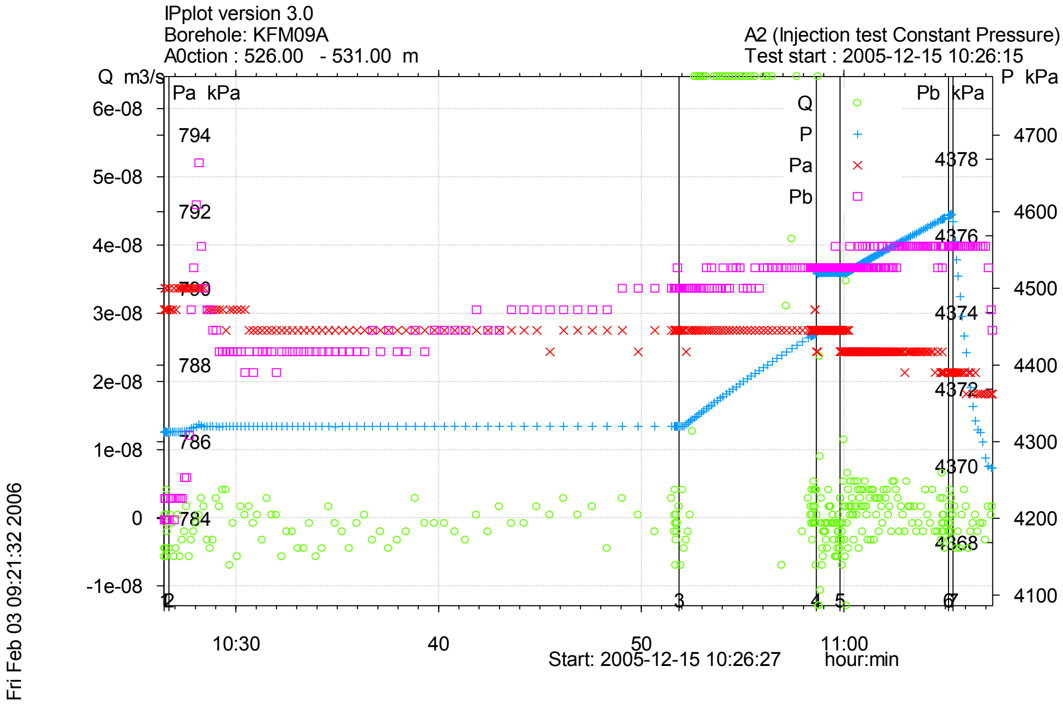


__Figure A3-494.__ Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 526.0-531.0 m in borehole KFM09A.

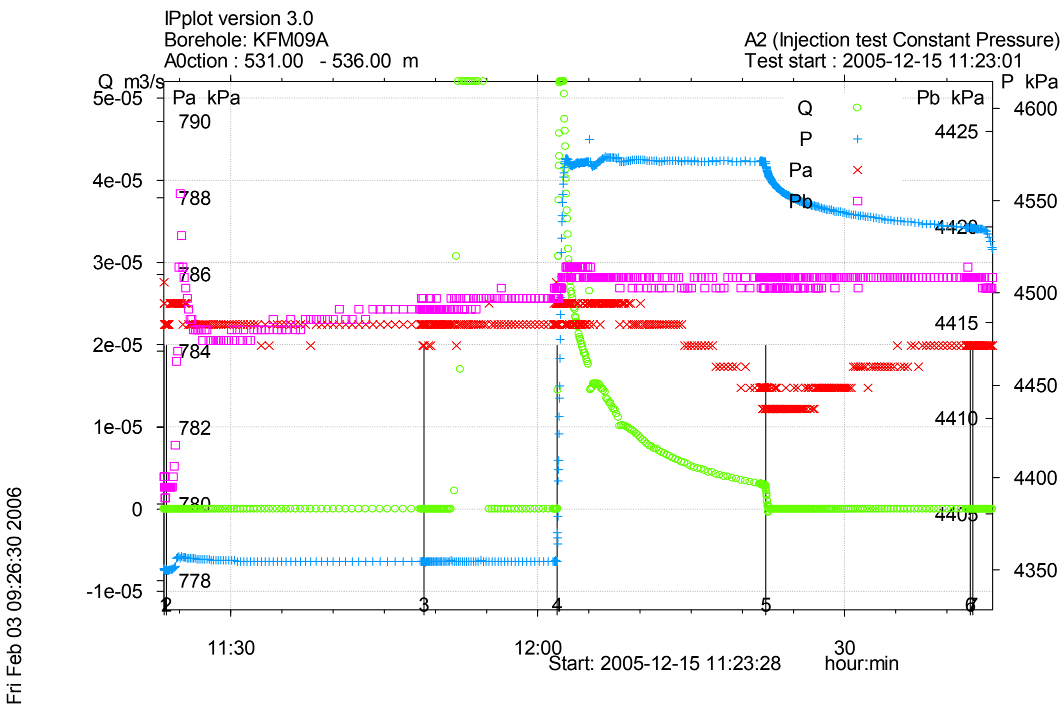


__Figure A3-495.__ Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 531.0-536.0 m in borehole KFM09A.

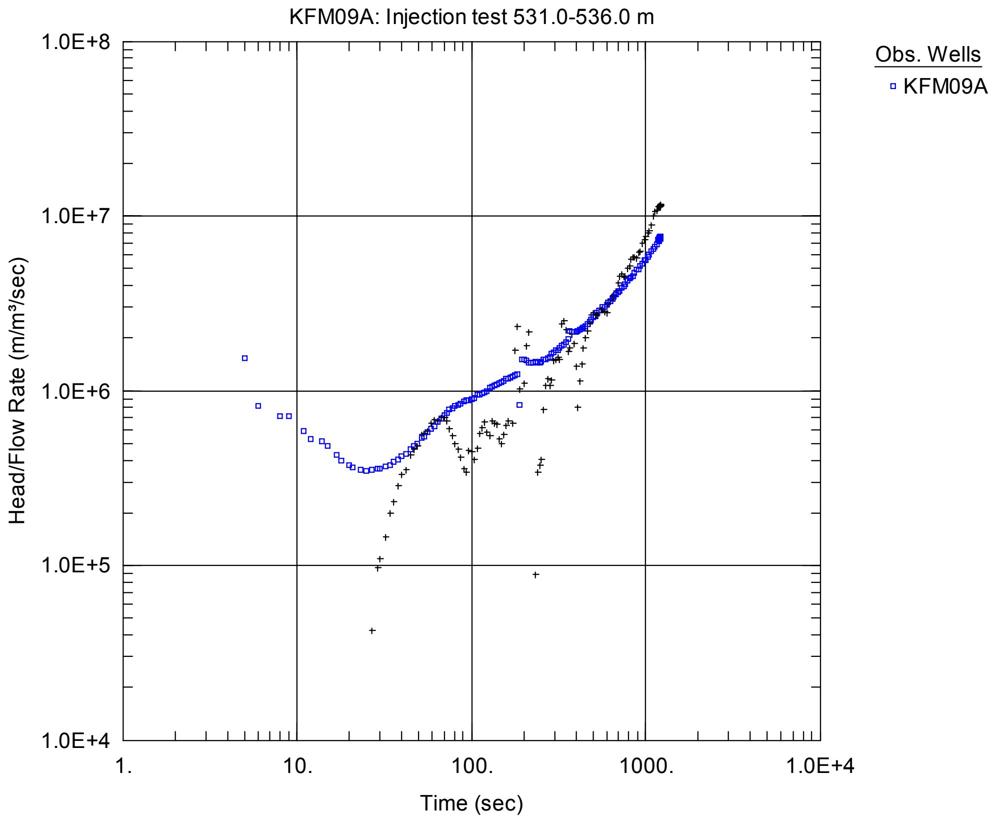


Figure A3-496. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 531.0-536.0 m in KFM09A.*

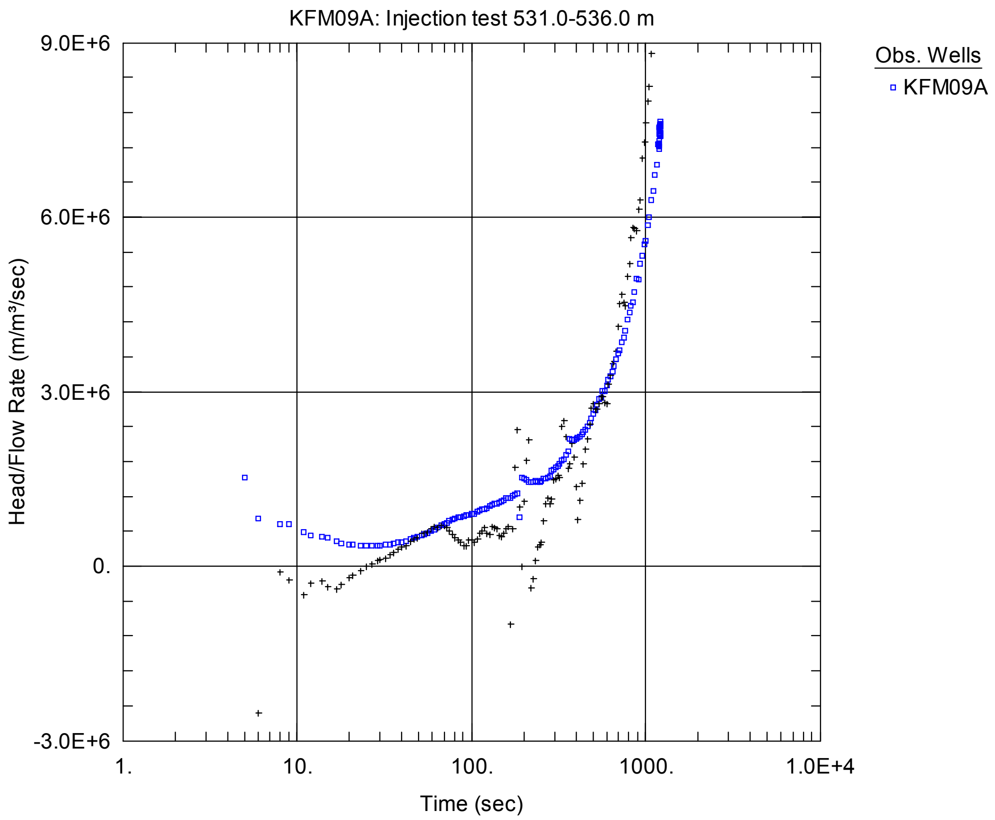


Figure A3-497. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 531.0-536.0 m in KFM09A.*

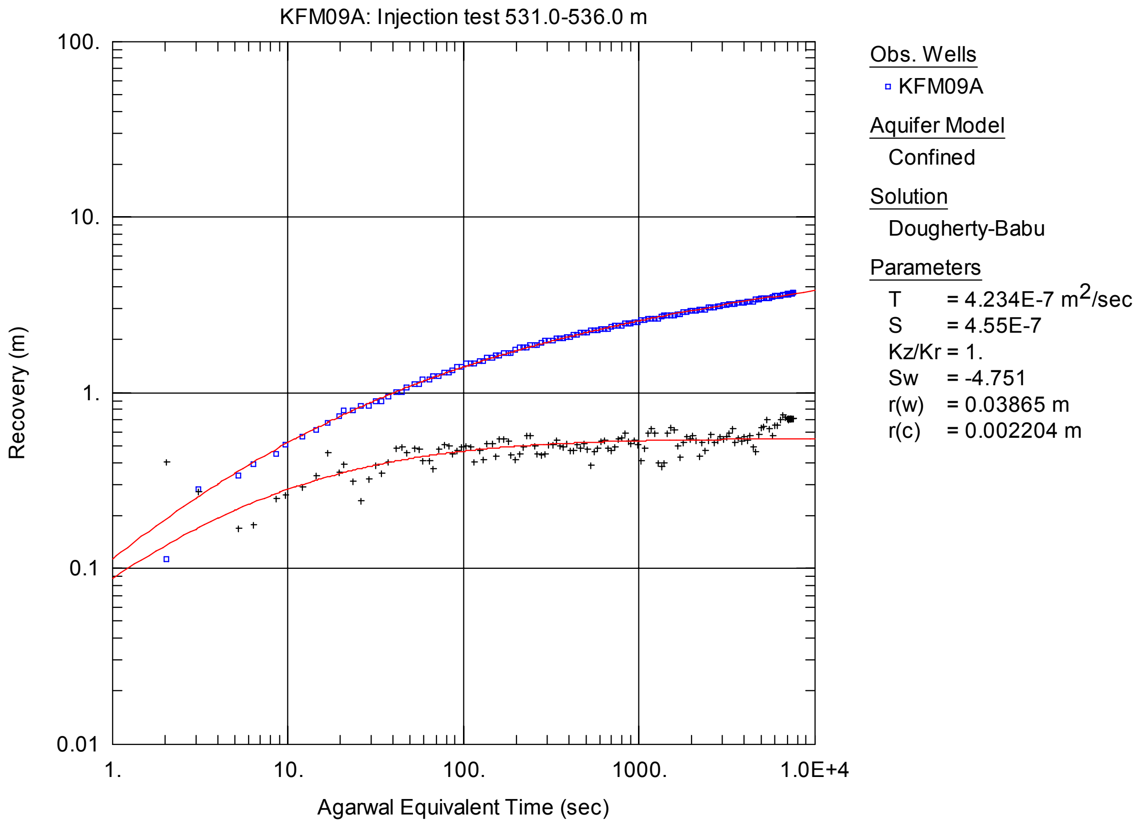


Figure A3-498. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 531.0-536.0 m in KFM09A.*

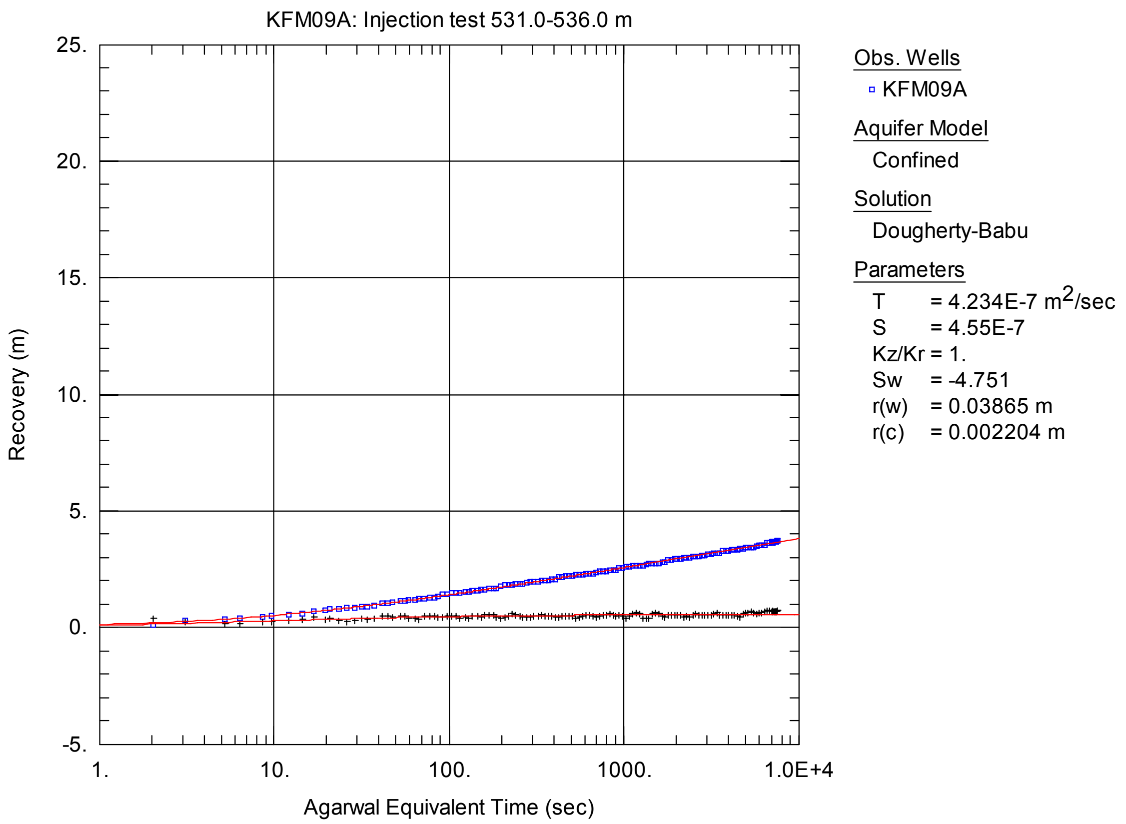


Figure A3-499. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 531.0-536.0 m in KFM09A.*

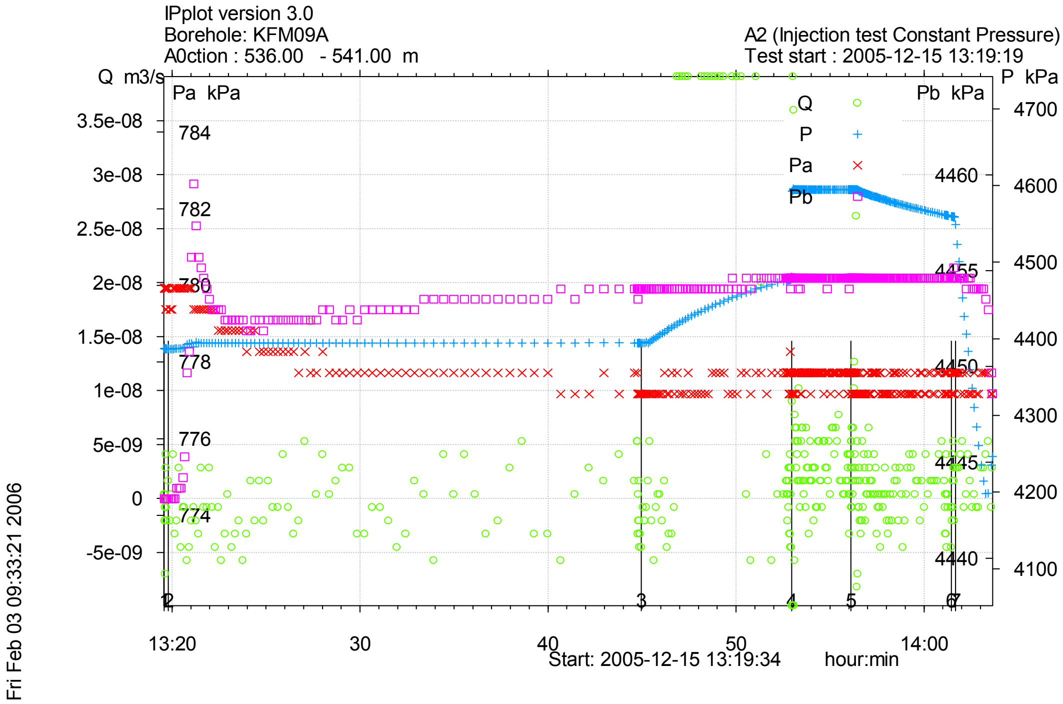


Figure A3-500. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 536.0-541.0 m in borehole KFM09A.*

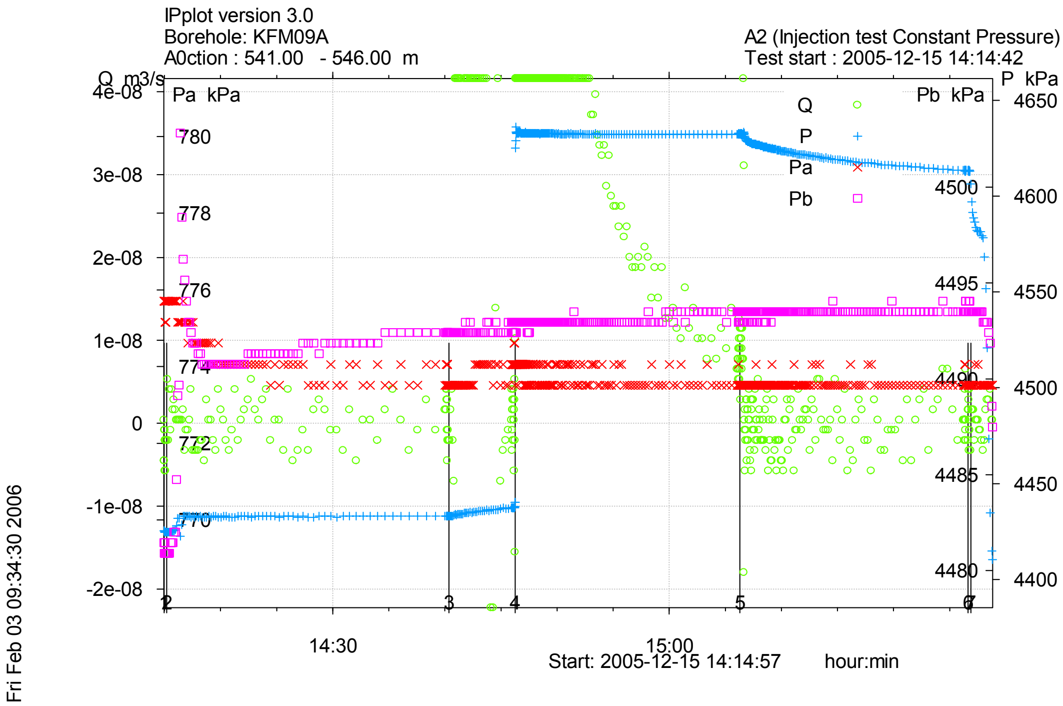


Figure A3-501. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 541.0-546.0 m in borehole KFM09A.*

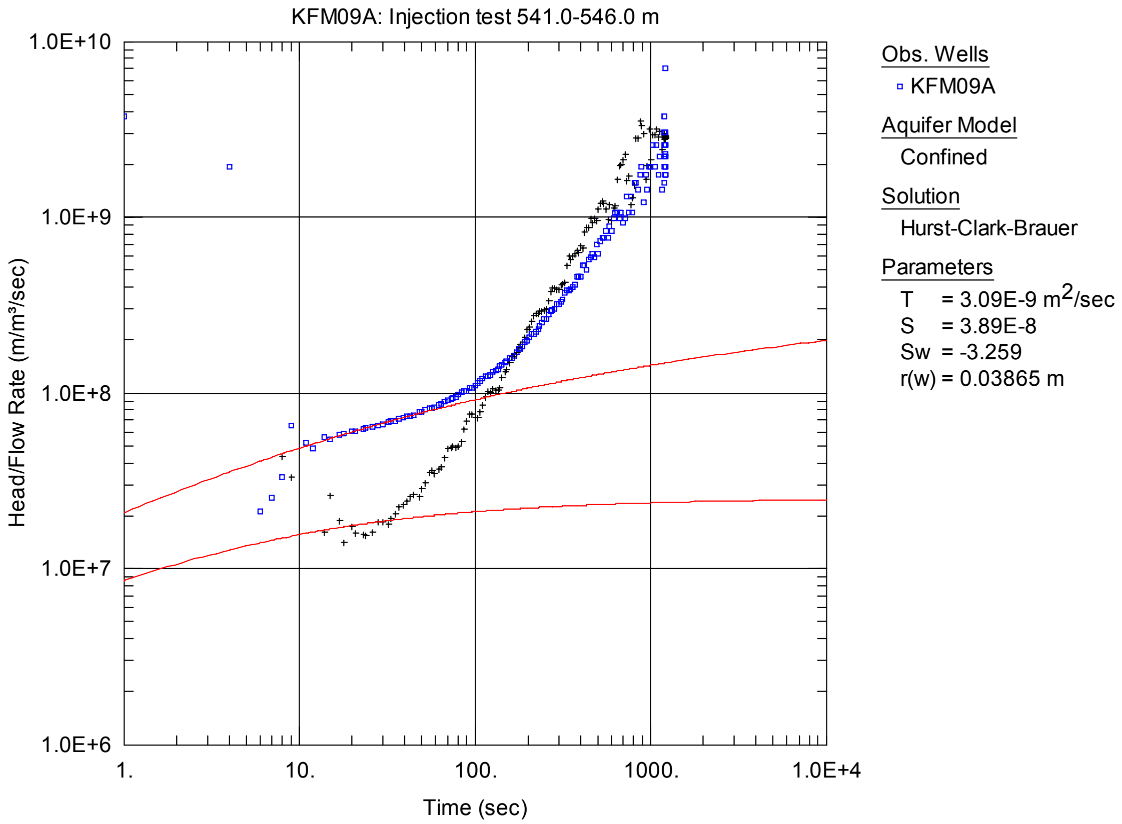


Figure A3-502. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 541.0-546.0 m in KFM09A.*

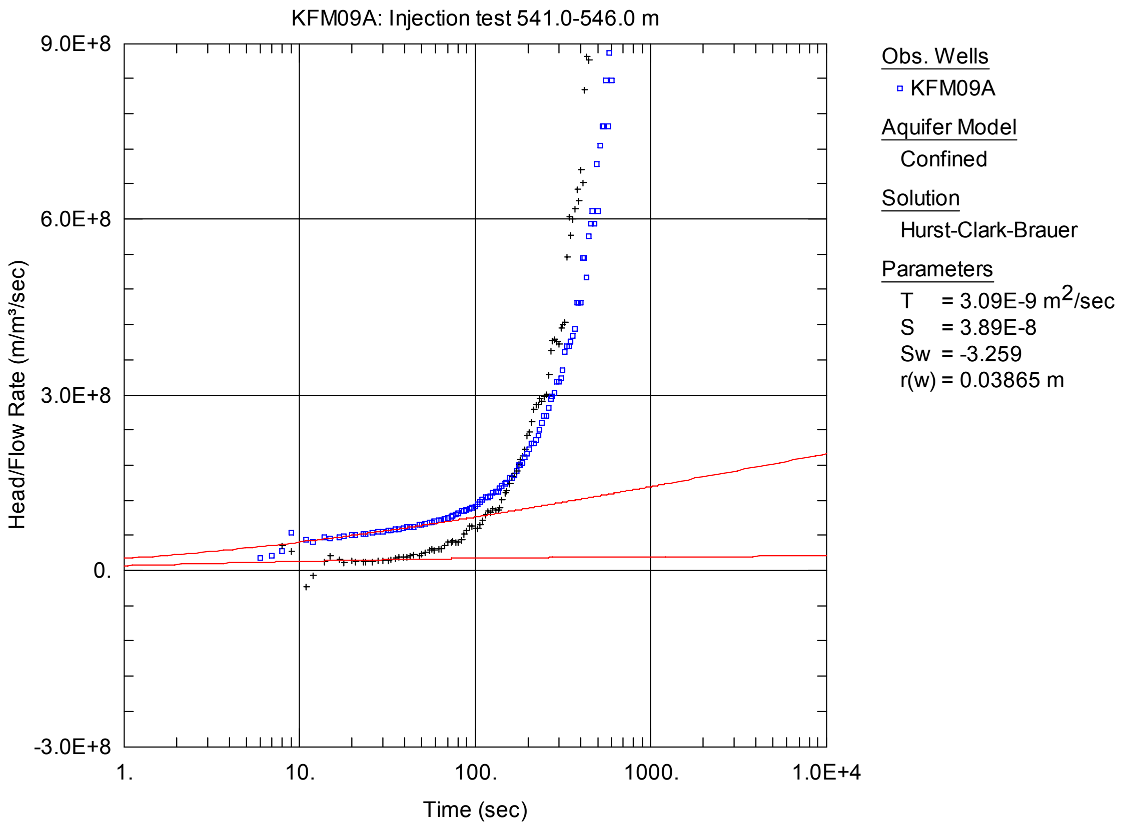


Figure A3-503. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 541.0-546.0 m in KFM09A.*

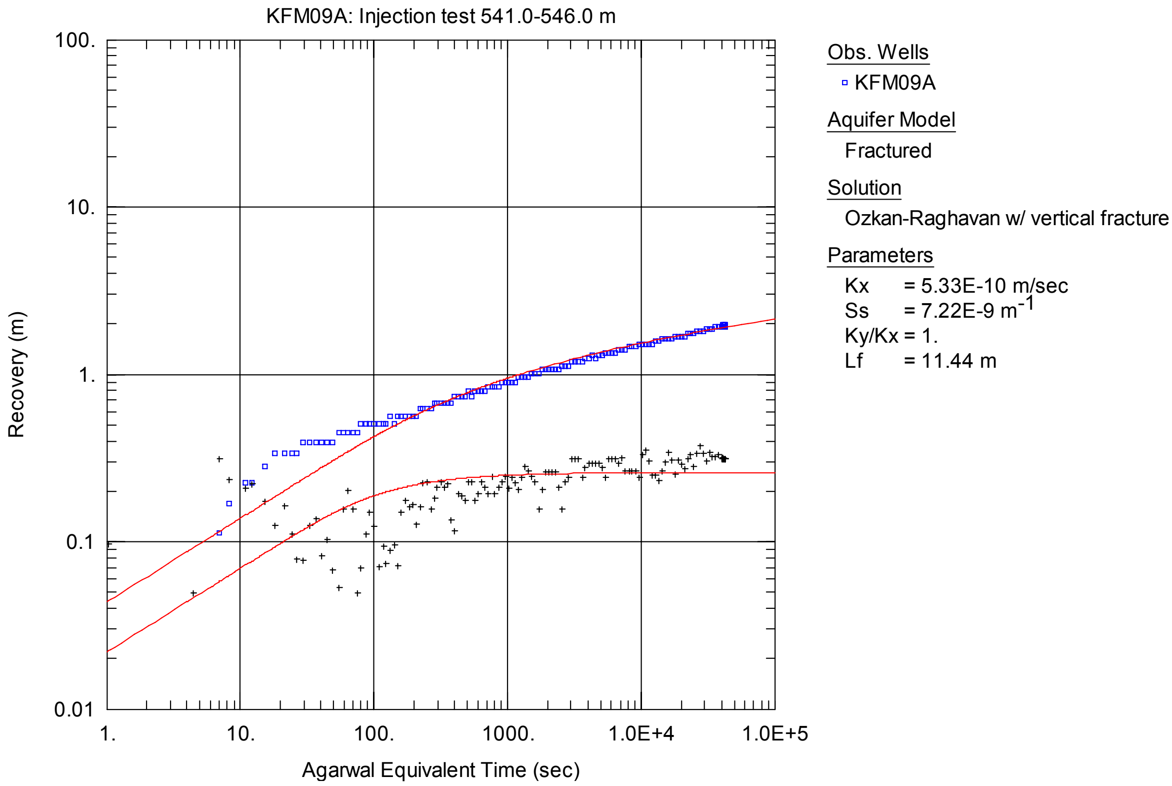


Figure A3-504. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 541.0-546.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

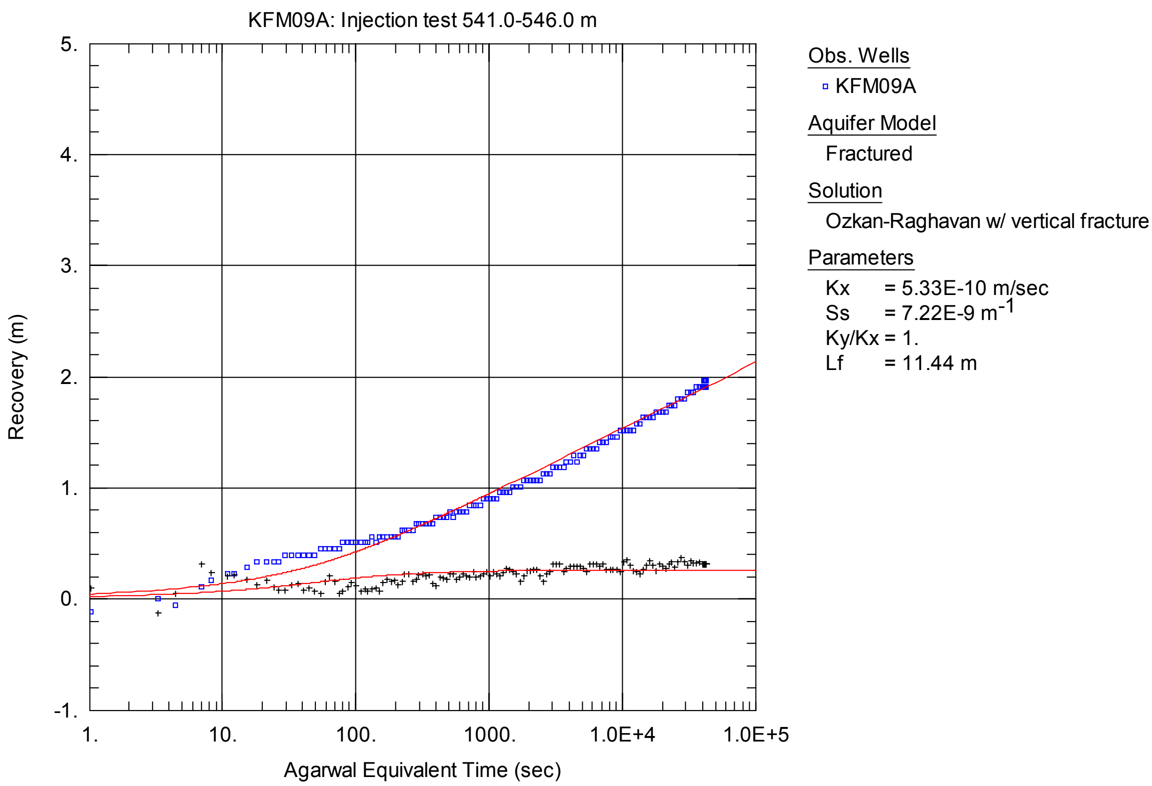


Figure A3-505. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 541.0-546.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

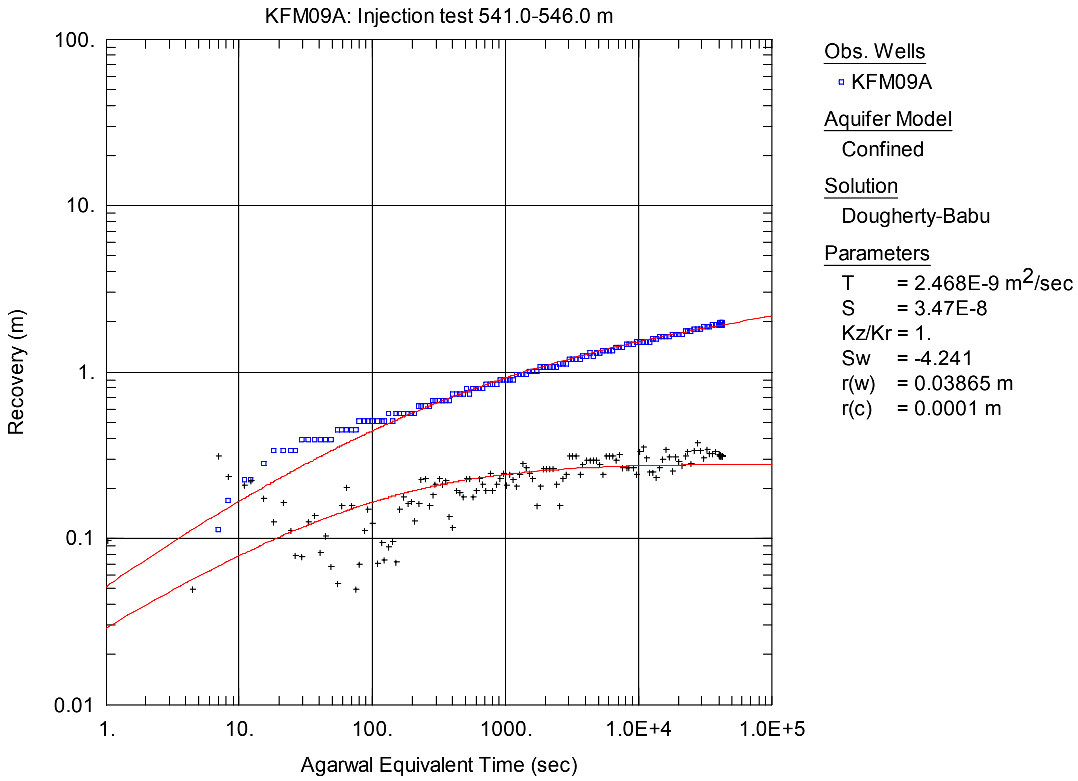


Figure A3-506. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 541.0-546.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

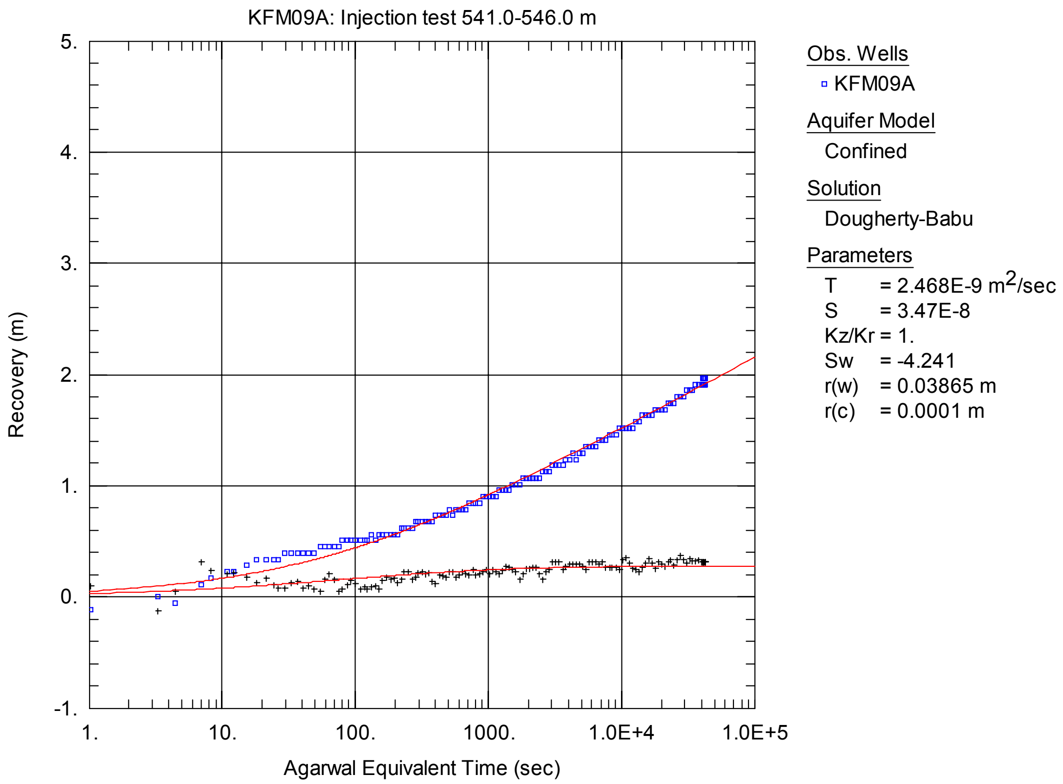


Figure A3-507. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 541.0-546.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

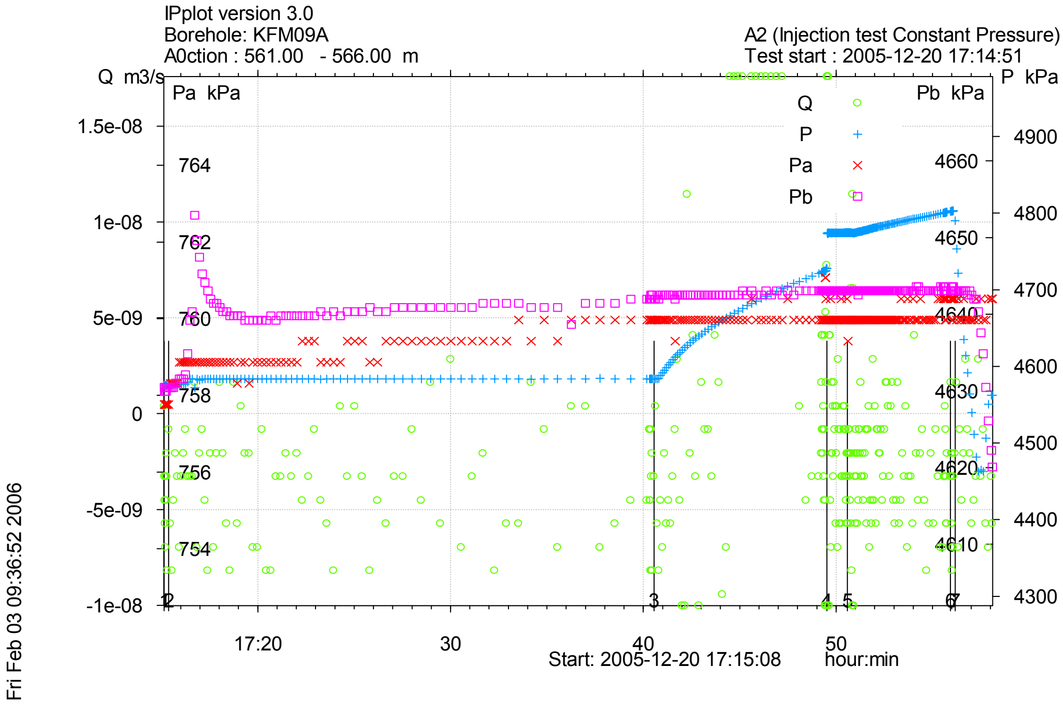


Figure A3-508. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 561.0-566.0 m in borehole KFM09A.*

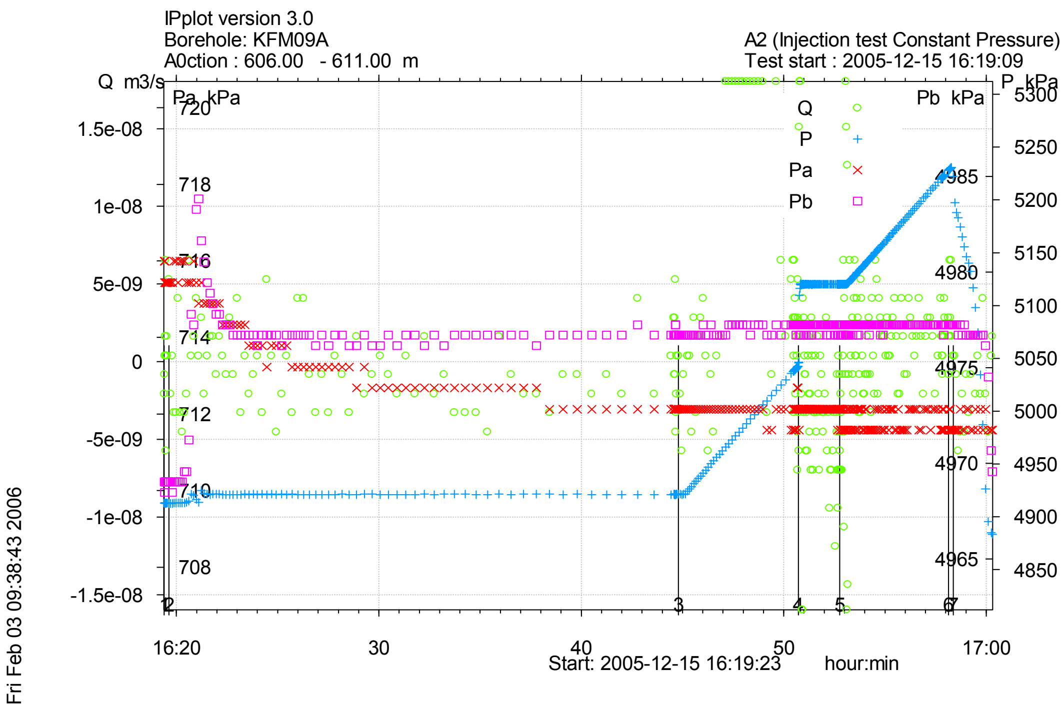


Figure A3-509. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 606.0-611.0 m in borehole KFM09A.*

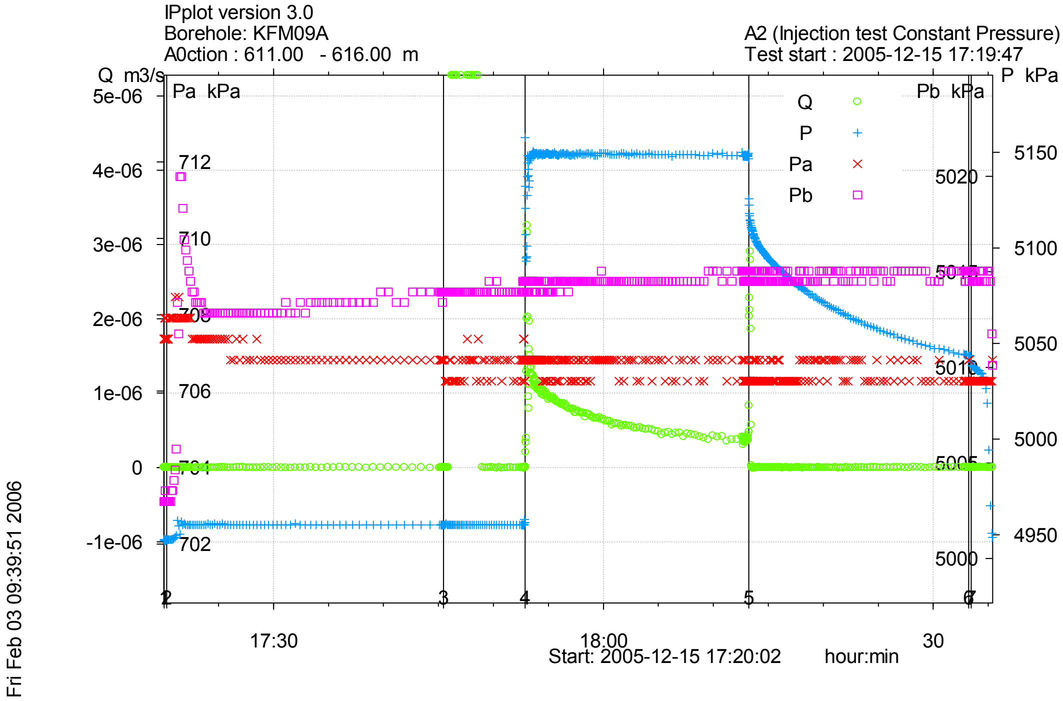


Figure A3-510. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 611.0-616.0 m in borehole KFM09A.

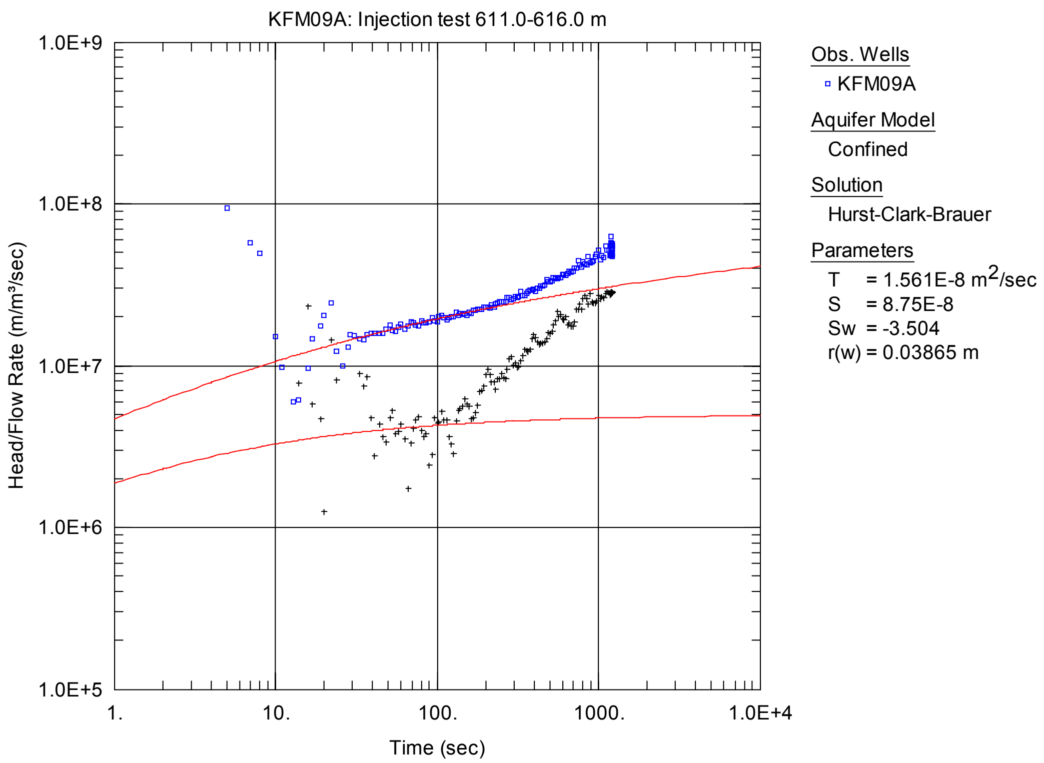


Figure A3-511. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 611.0-616.0 m in KFM09A.

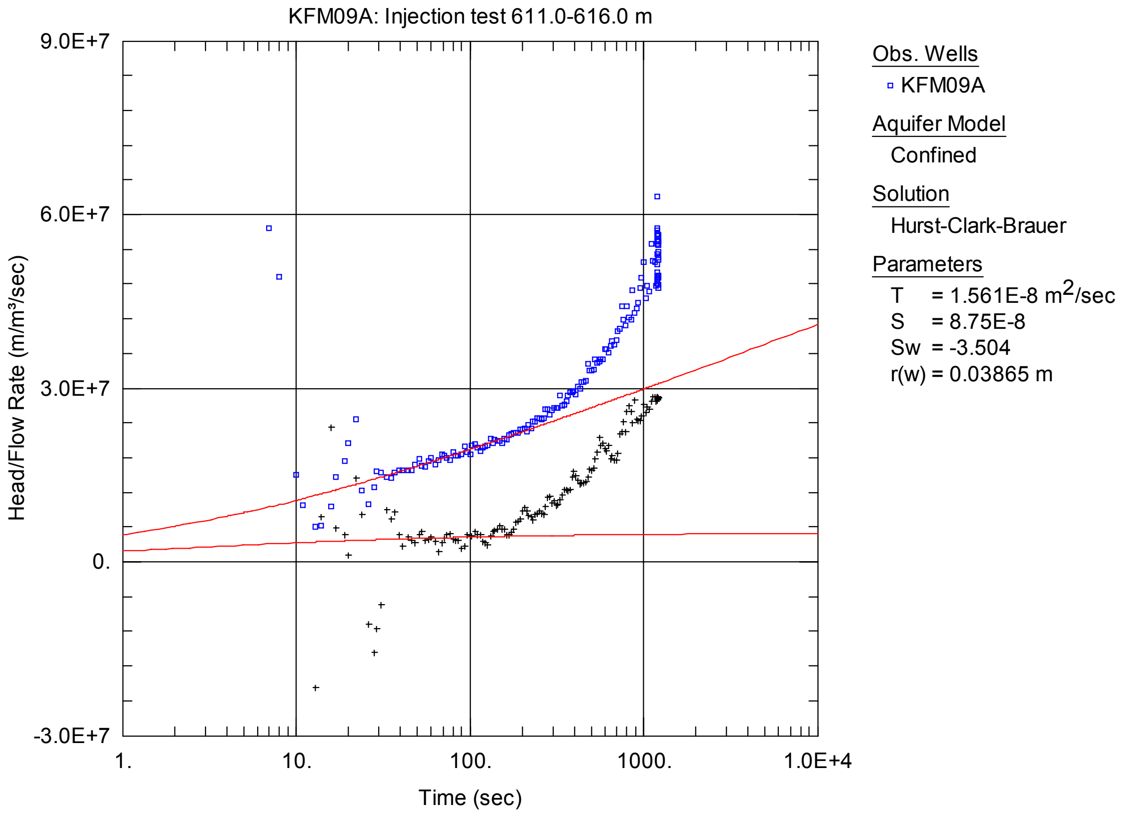


Figure A3-512. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 611.0-616.0 m in KFM09A.*

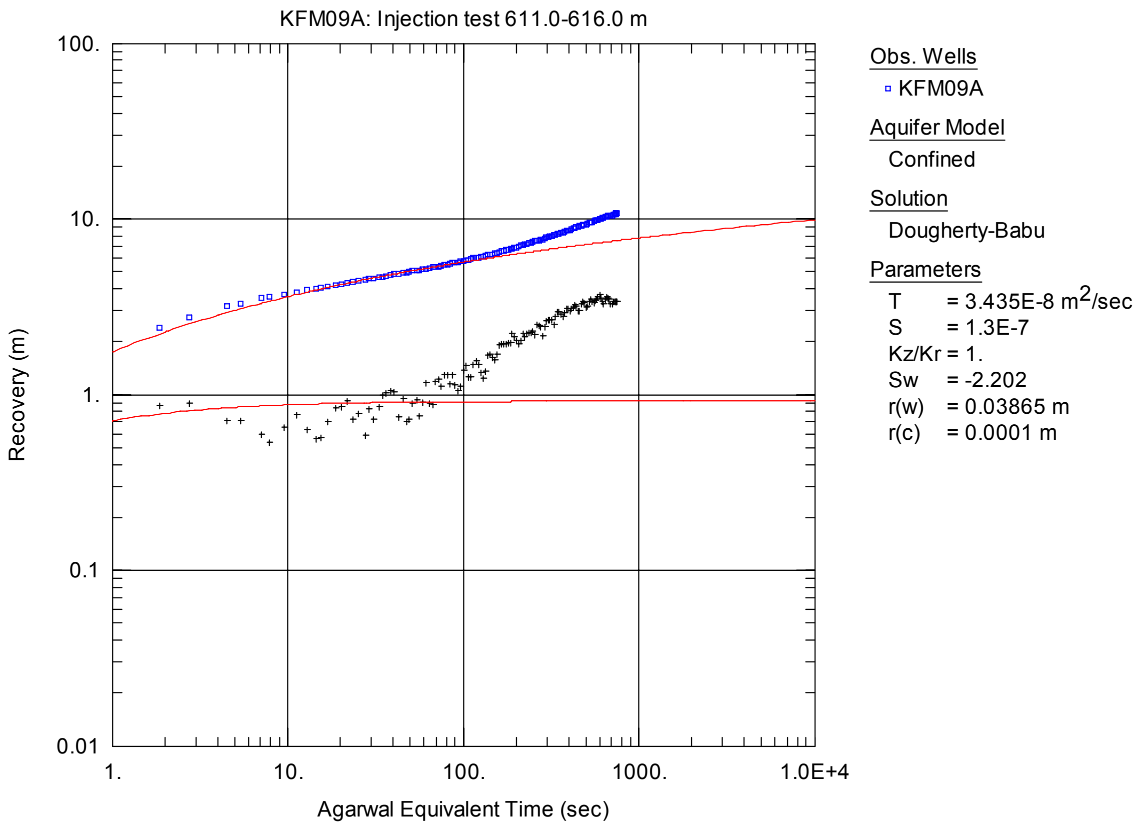


Figure A3-513. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 611.0-616.0 m in KFM09A.*

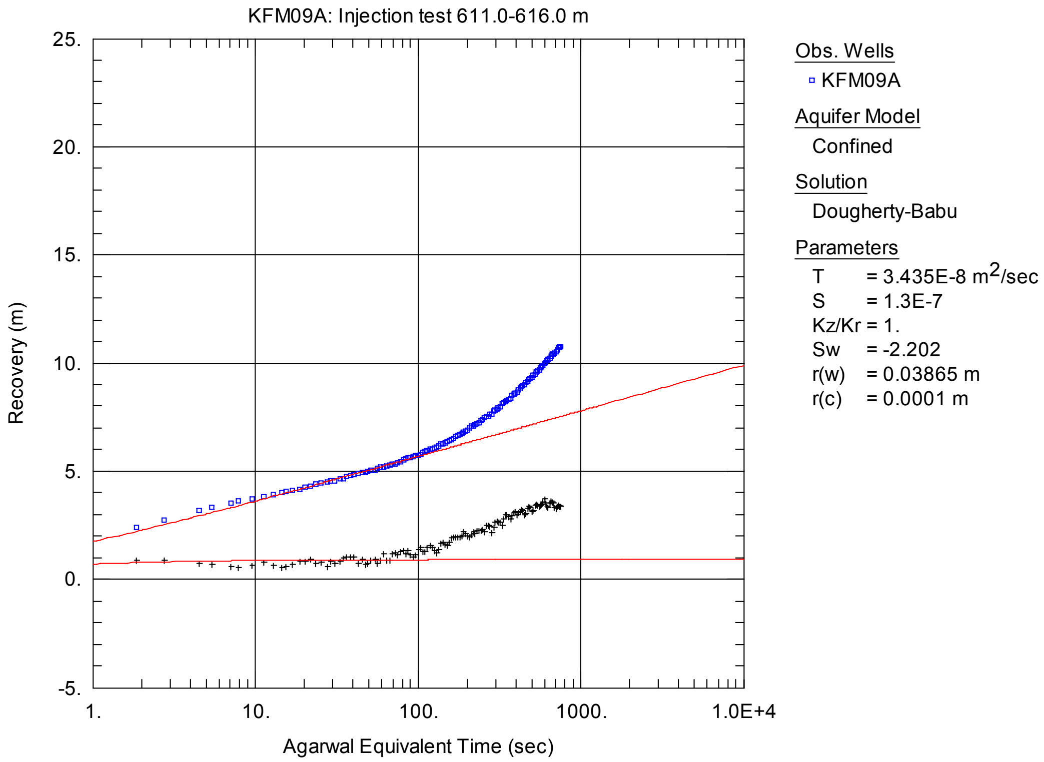


Figure A3-514. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 611.0-616.0 m in KFM09A.*

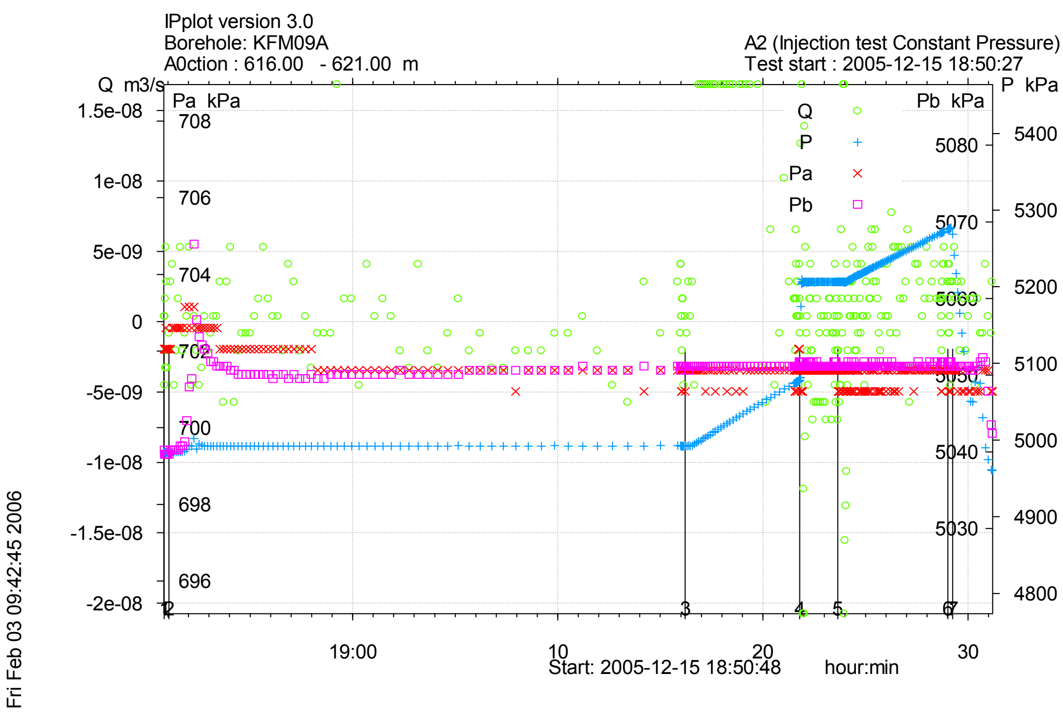


Figure A3-515. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 616.0-621.0 m in borehole KFM09A.*

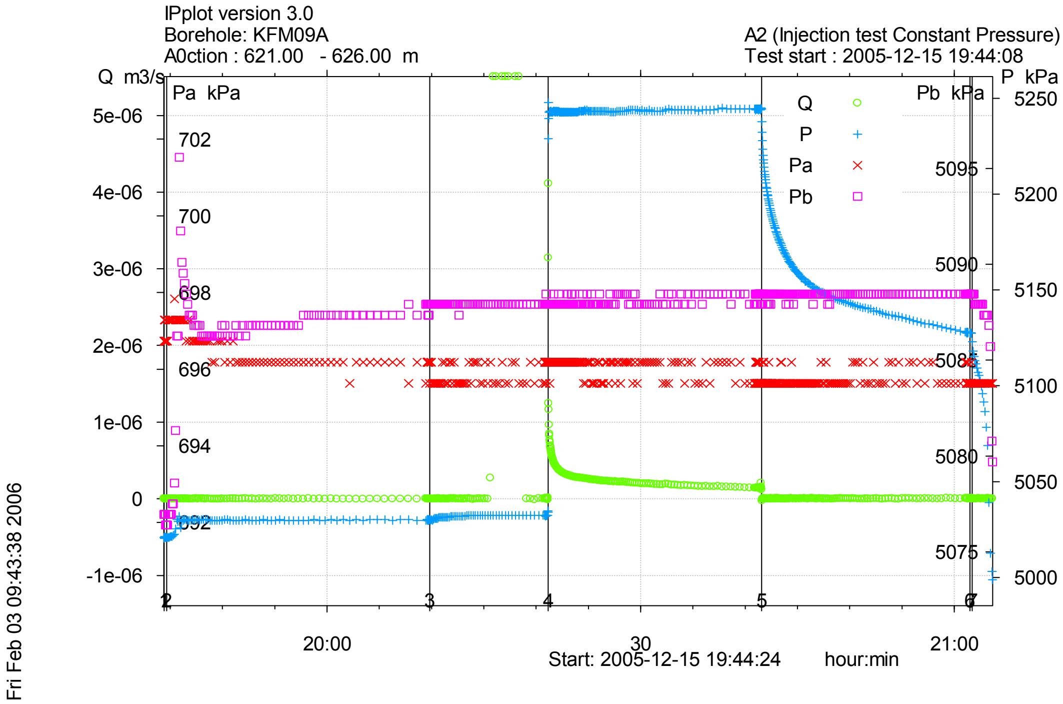


__Figure A3-516.__ Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 621.0-626.0 m in borehole KFM09A.

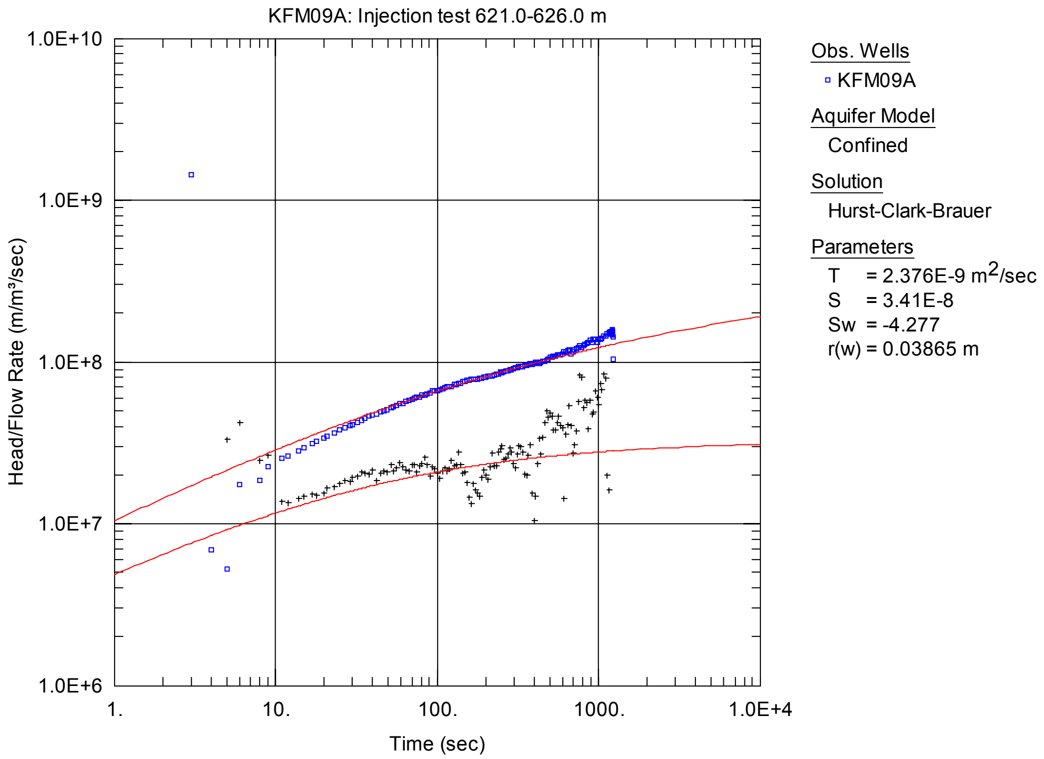


__Figure A3-517.__ Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 621.0-626.0 m in KFM09A.

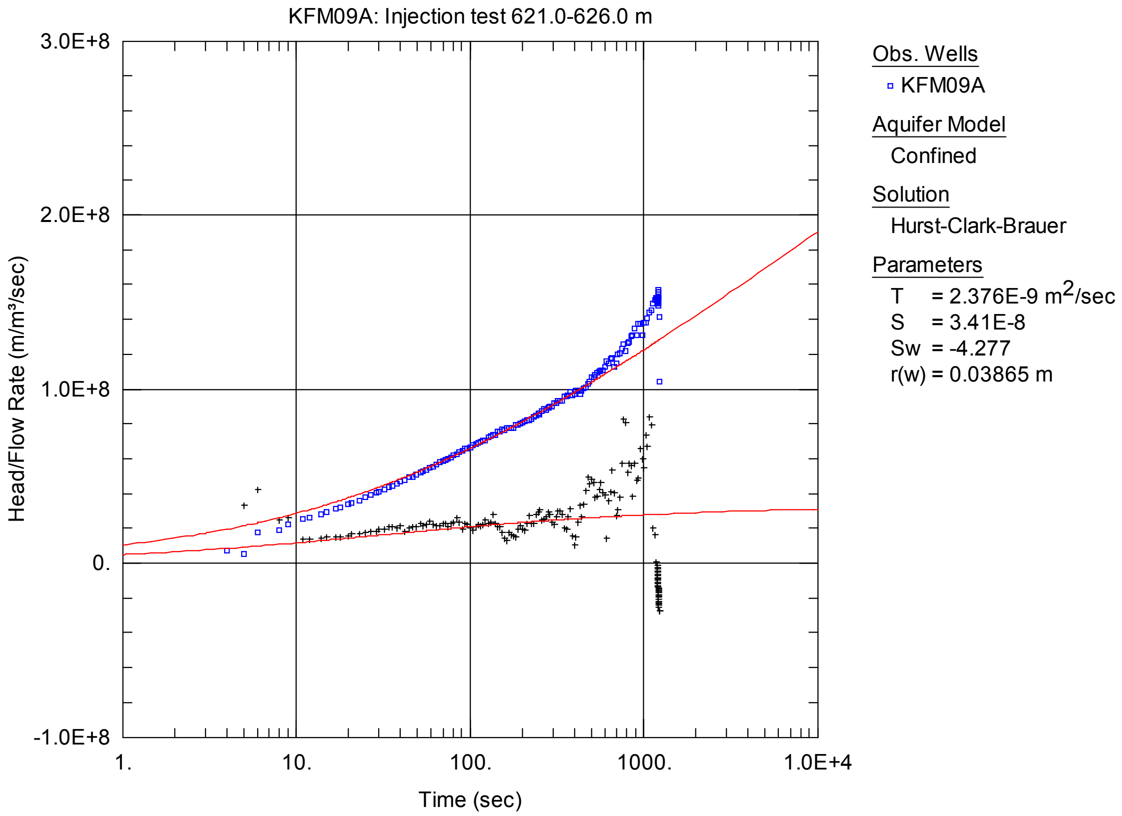


Figure A3-518. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 621.0-626.0 m in KFM09A.*

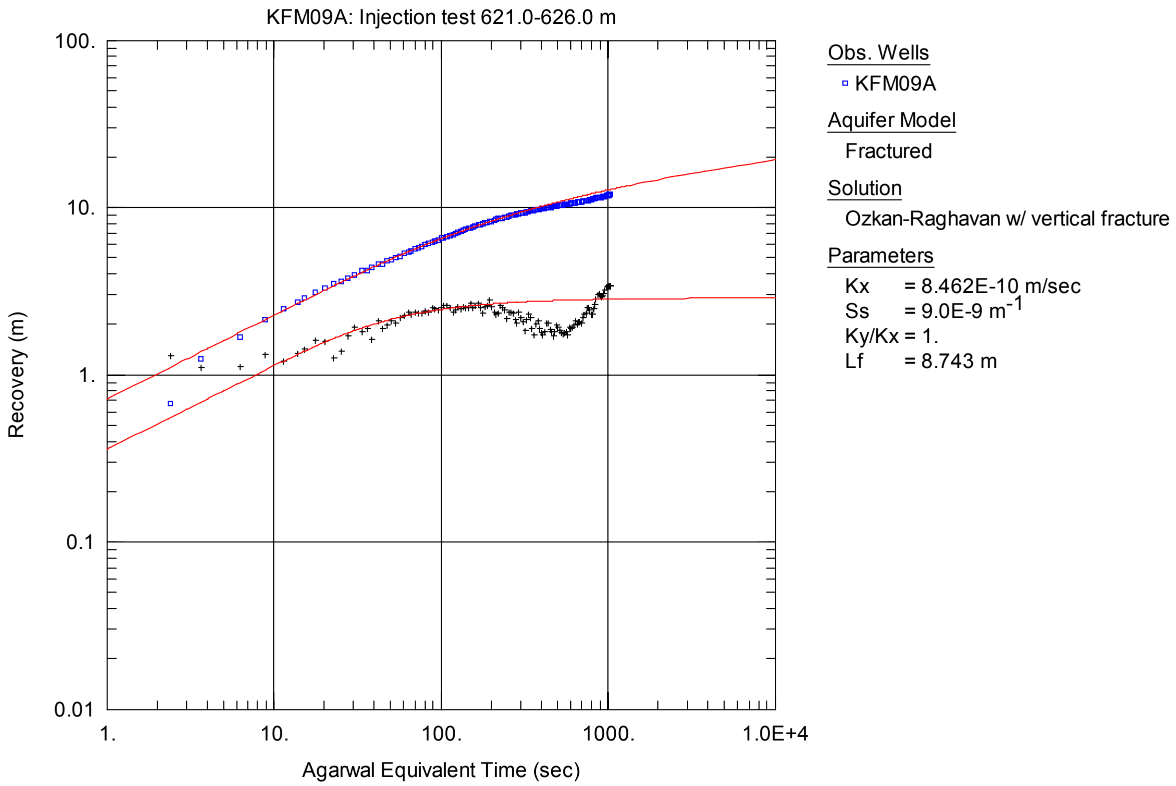


Figure A3-519. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 621.0-626.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

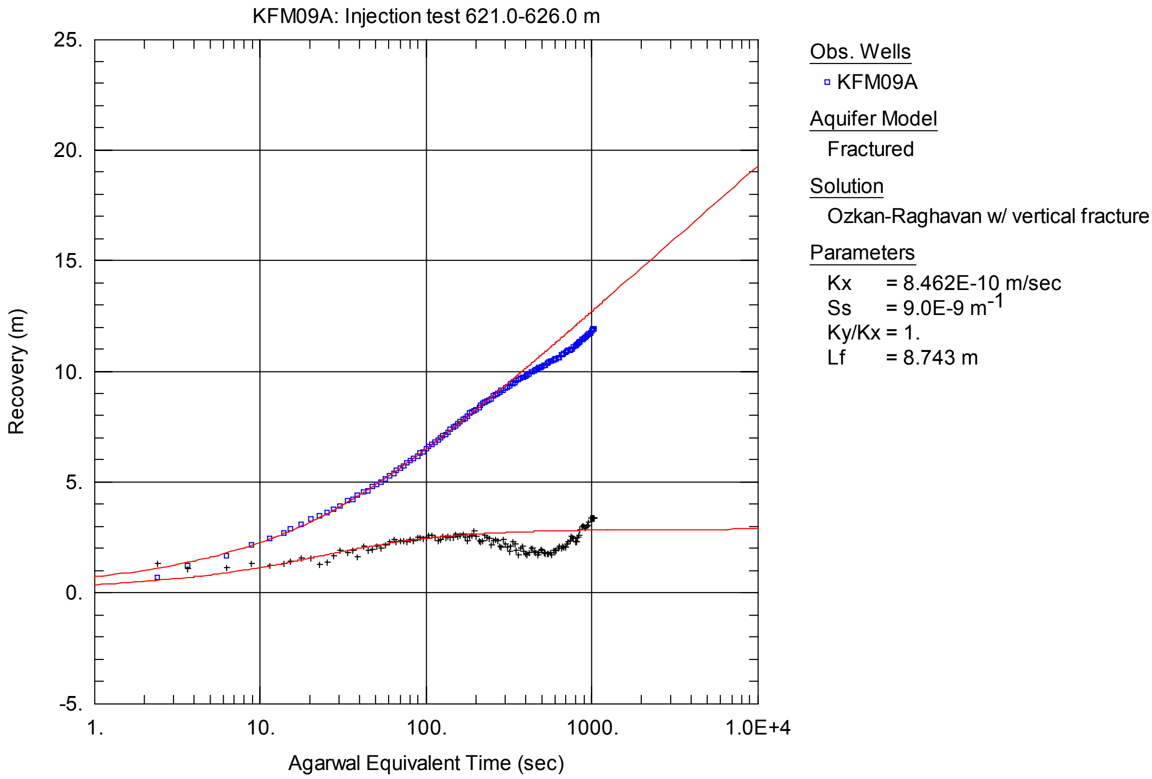


Figure A3-520. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 621.0-626.0 m in KFM09A.This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

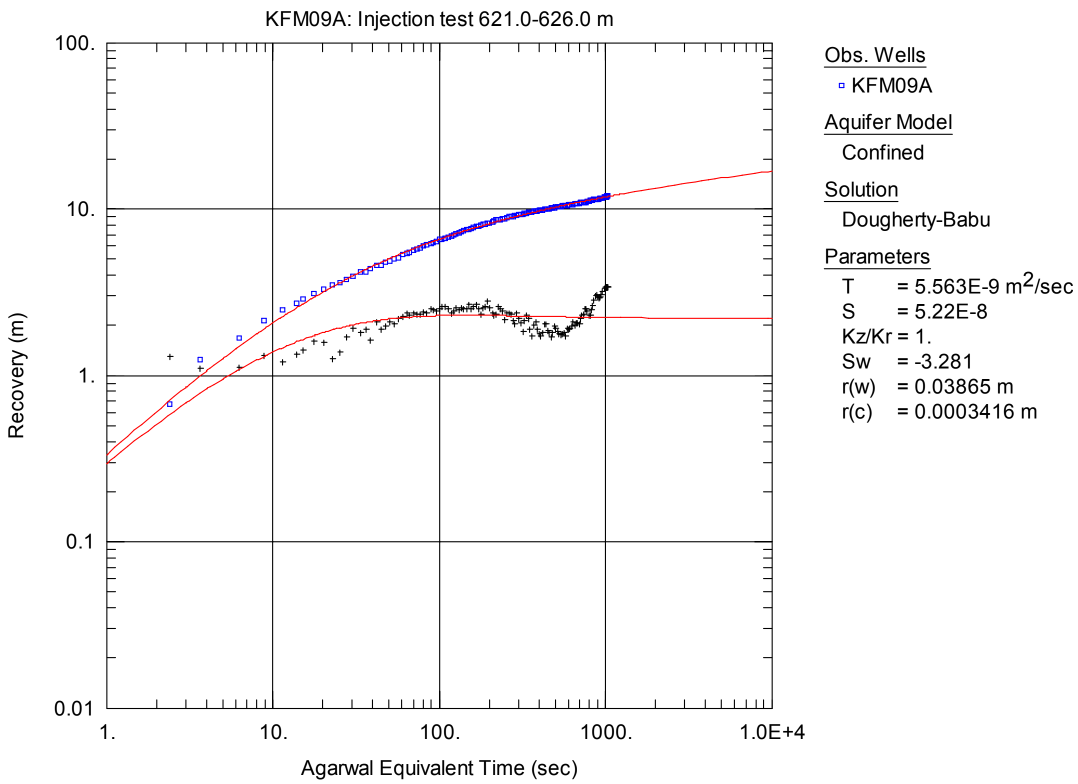


Figure A3-521. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 621.0-626.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

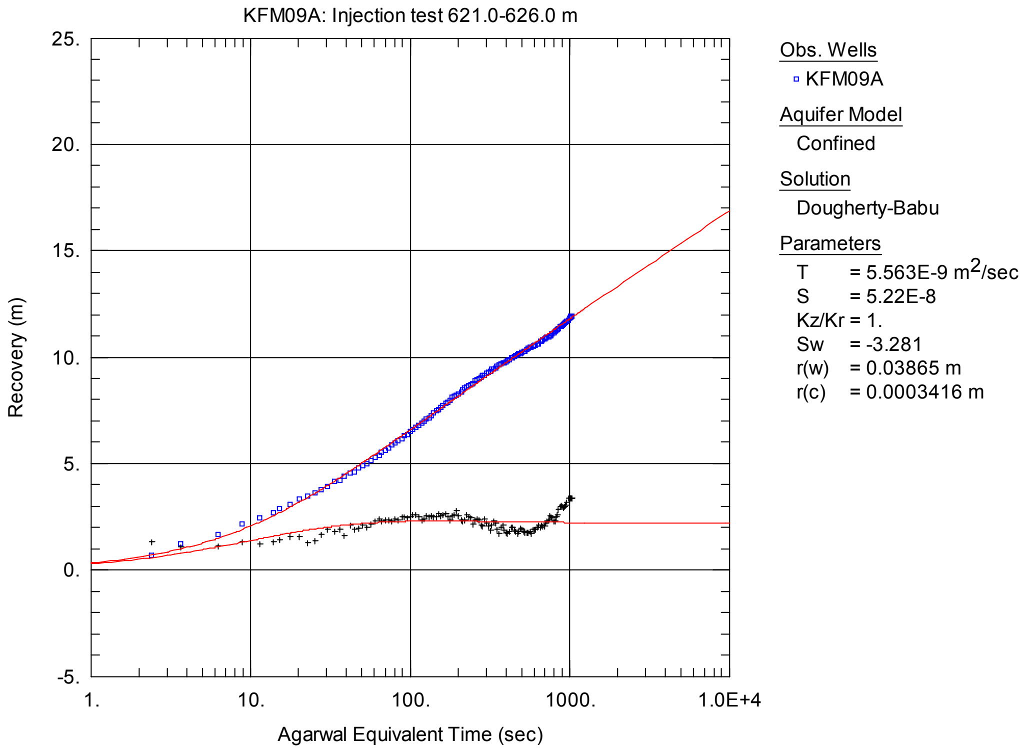


Figure A3-522. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 621.0-626.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

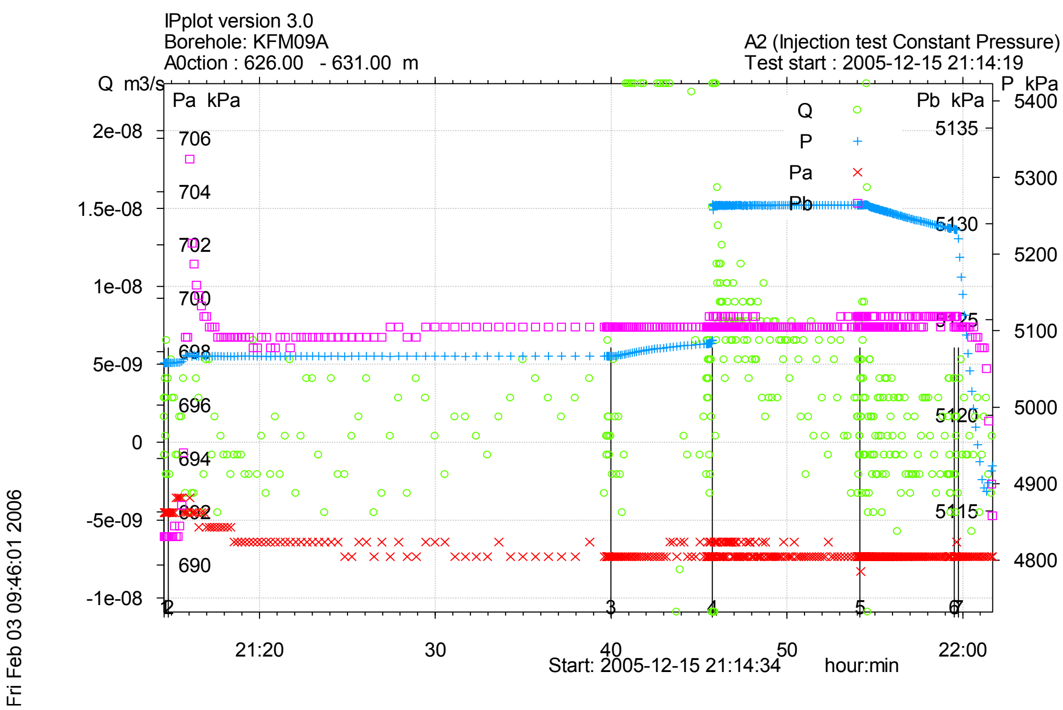


Figure A3-523. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 626.0-631.0 m in borehole KFM09A.*

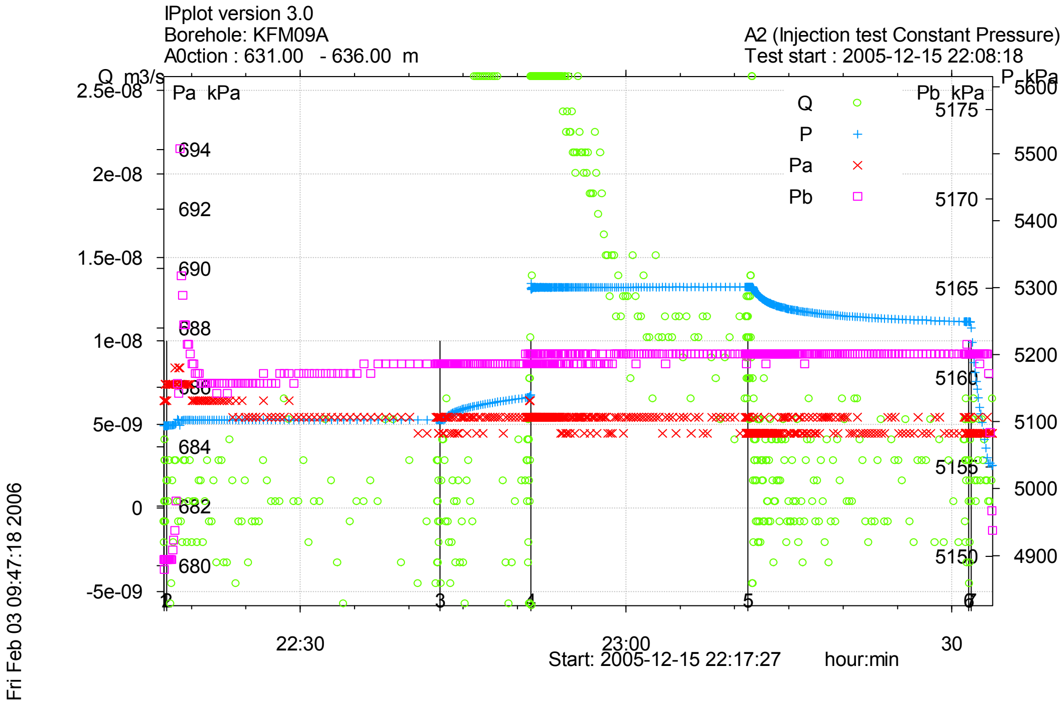


Figure A3-524. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 631.0-636.0 m in borehole KFM09A.*

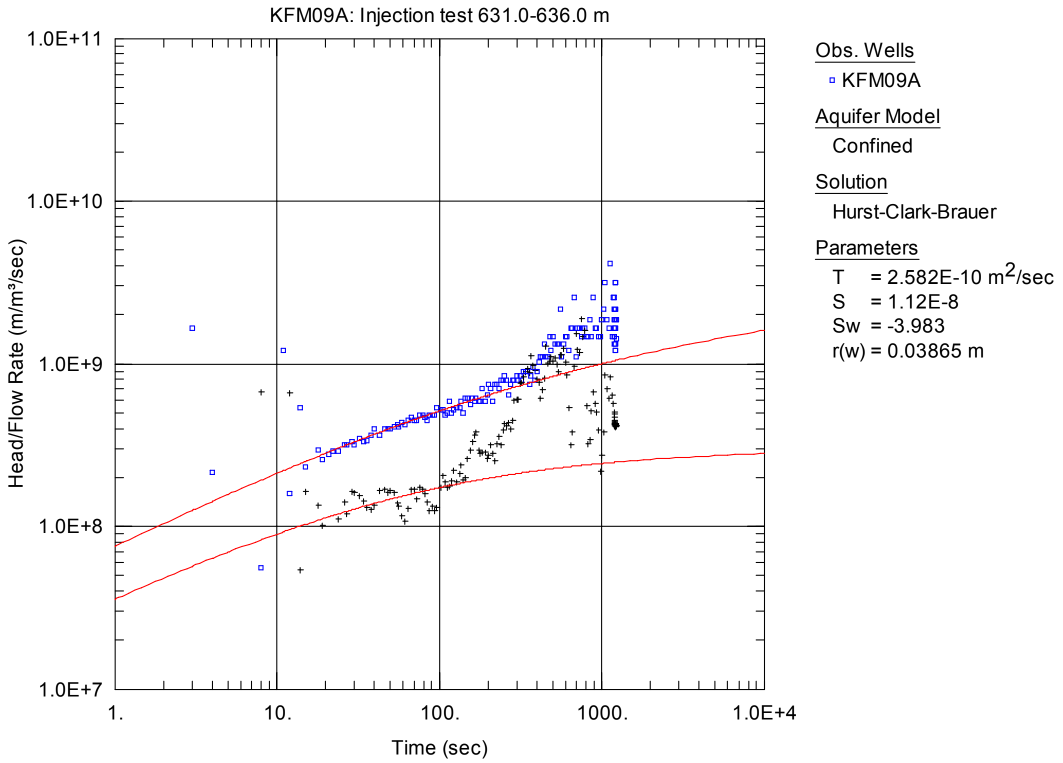


Figure A3-525. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 631.0-636.0 m in KFM09A.*

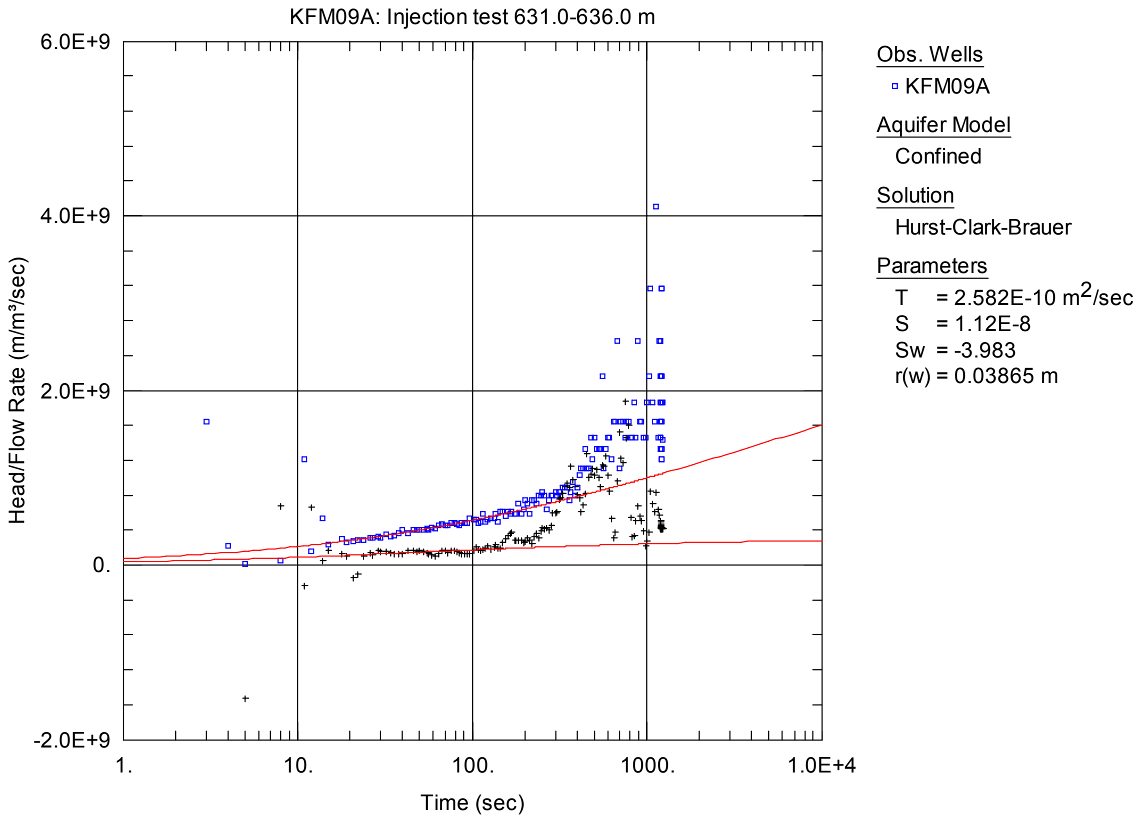


Figure A3-526. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 631.0-636.0 m in KFM09A.*

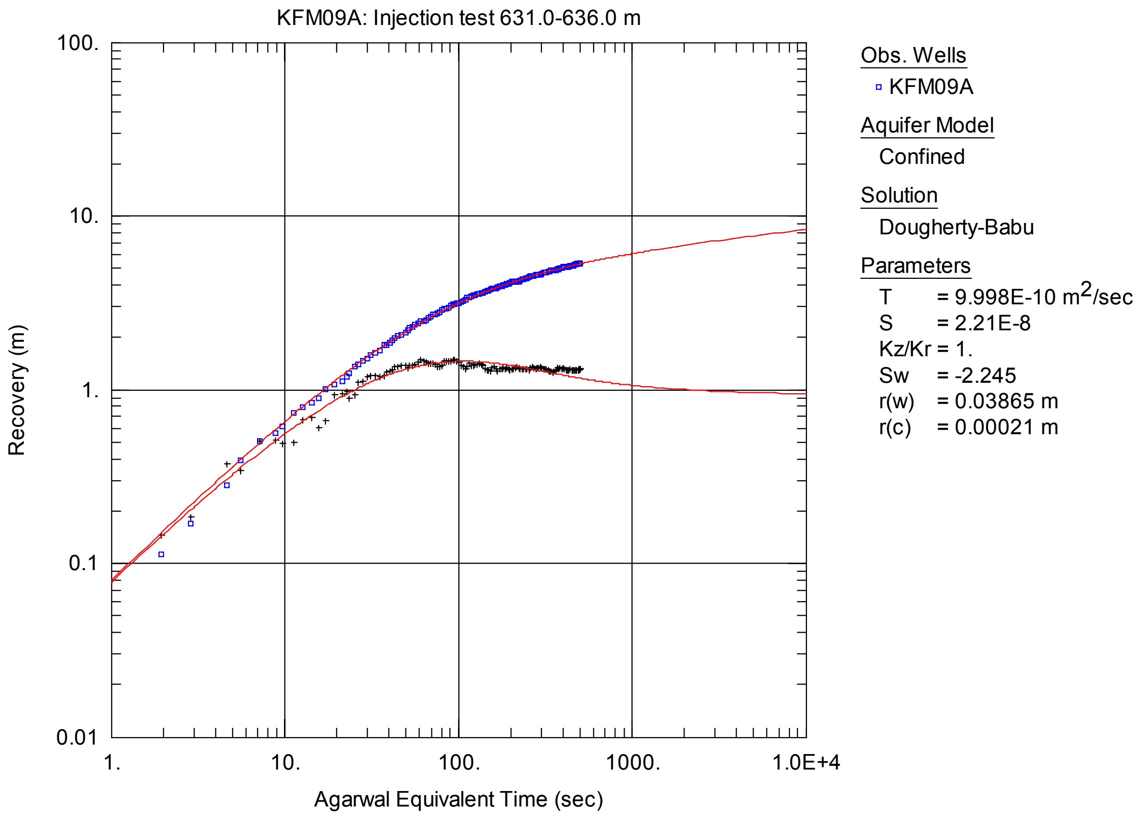


Figure A3-527. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 631.0-636.0 m in KFM09A.*

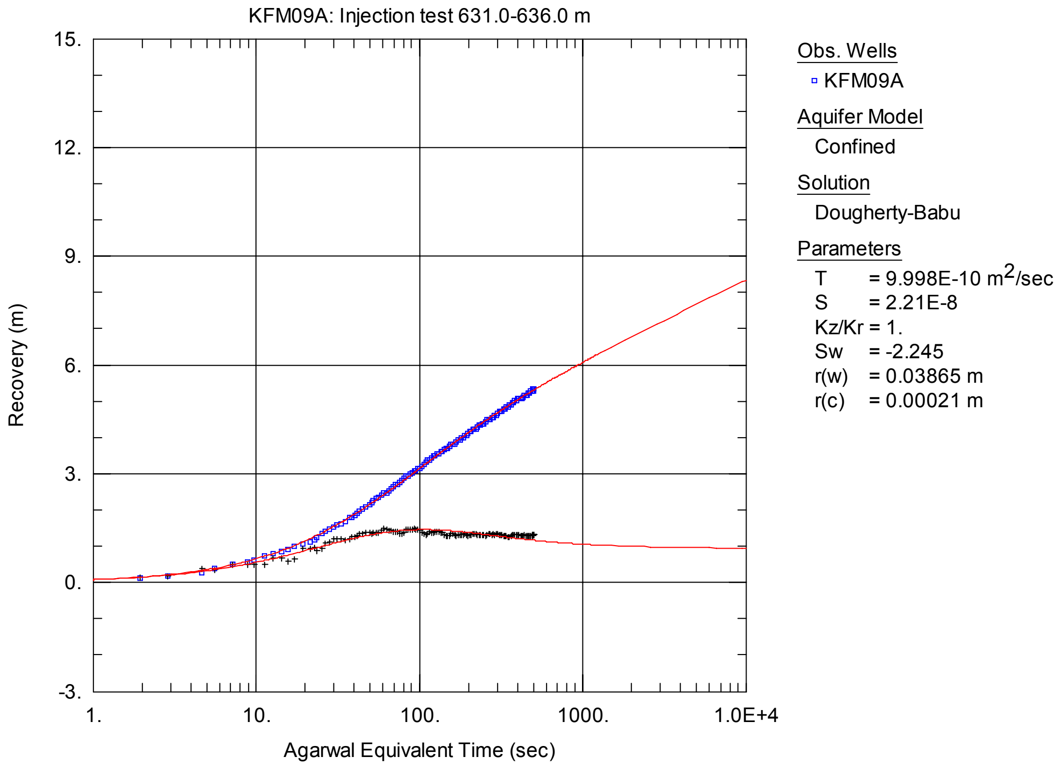


Figure A3-528. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 631.0-636.0 m in KFM09A.*

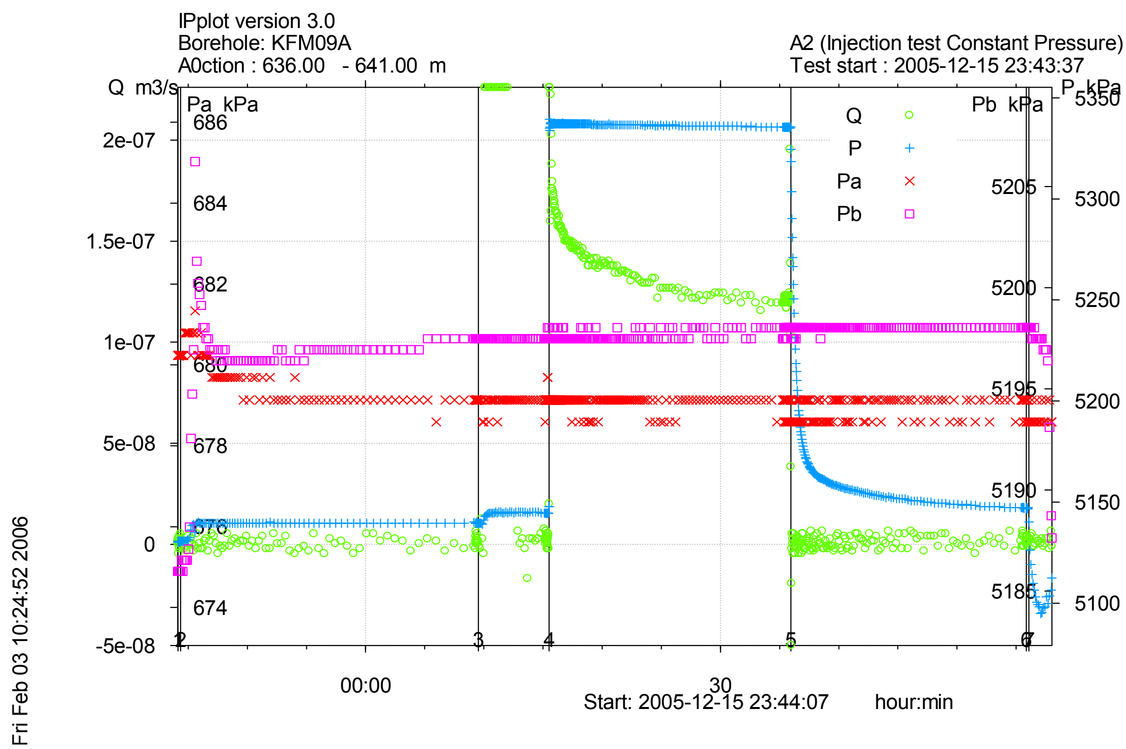


Figure A3-529. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 636.0-641.0 m in borehole KFM09A.*

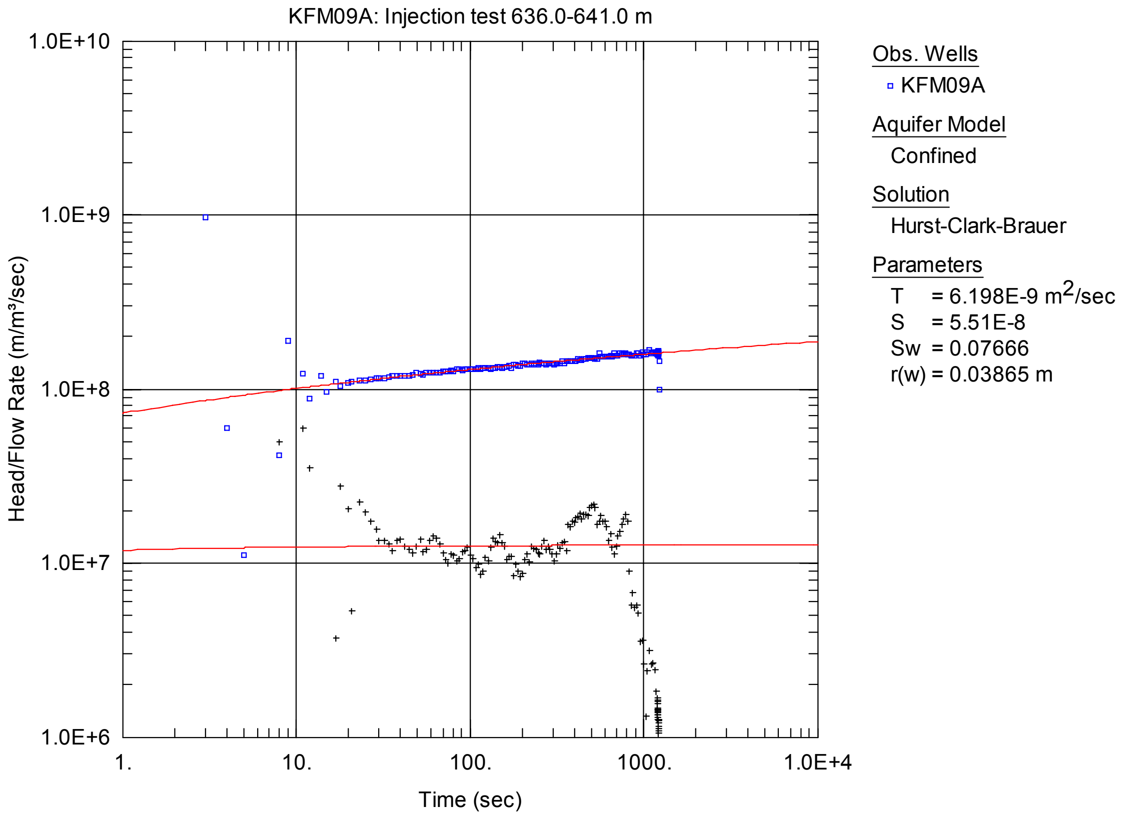


Figure A3-530. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 636.0-641.0 m in KFM09A.*

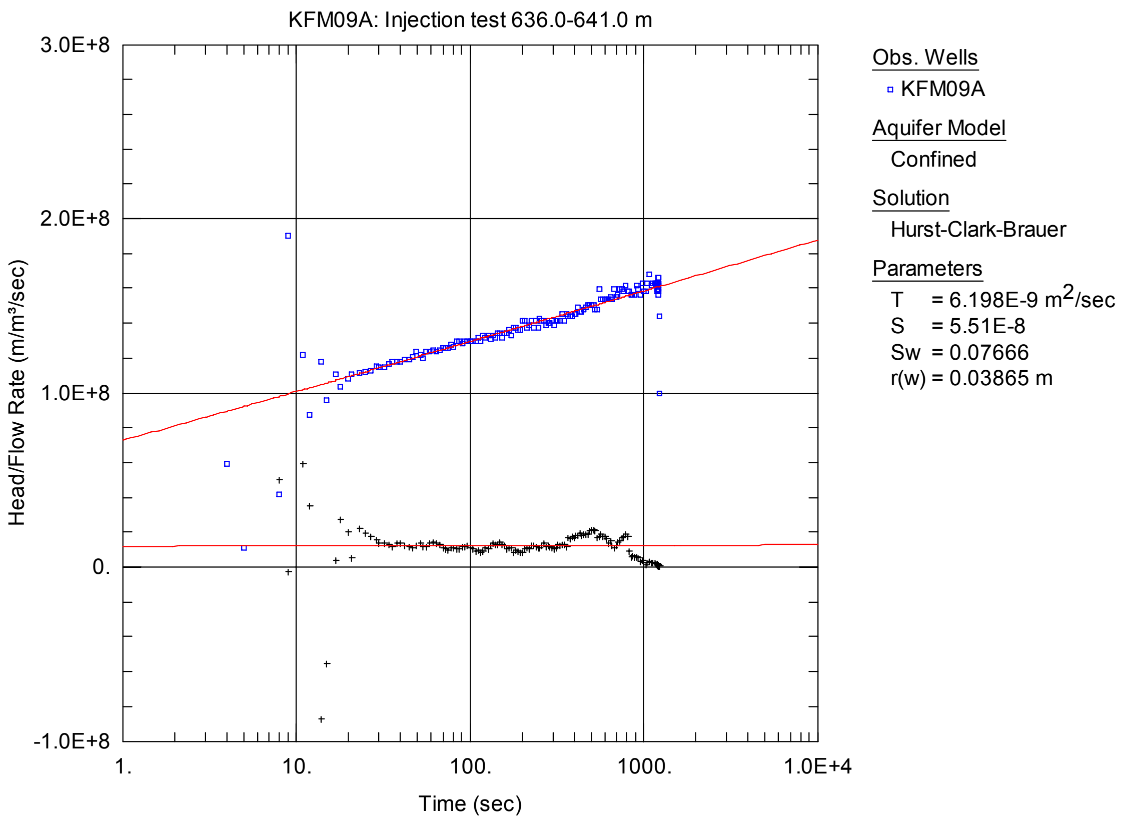


Figure A3-531. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 636.0-641.0 m in KFM09A.*

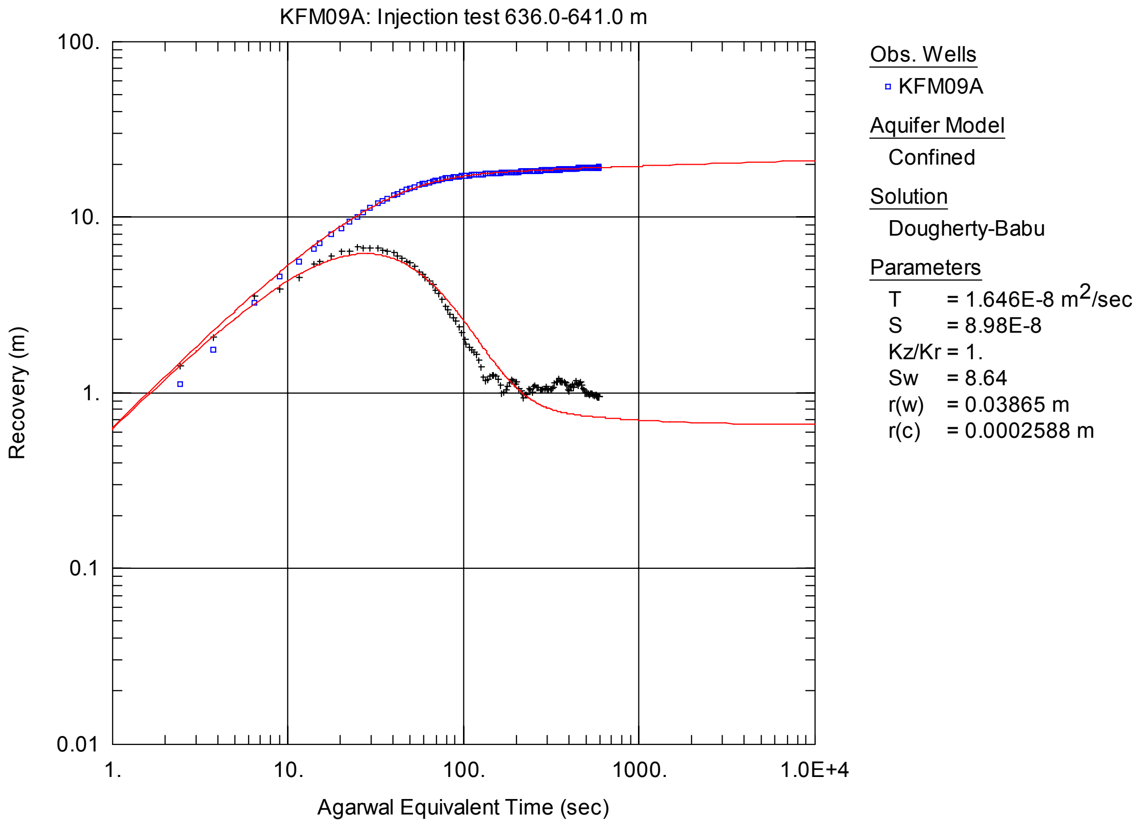


***Figure A3-532.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 636.0-641.0 m in KFM09A.*

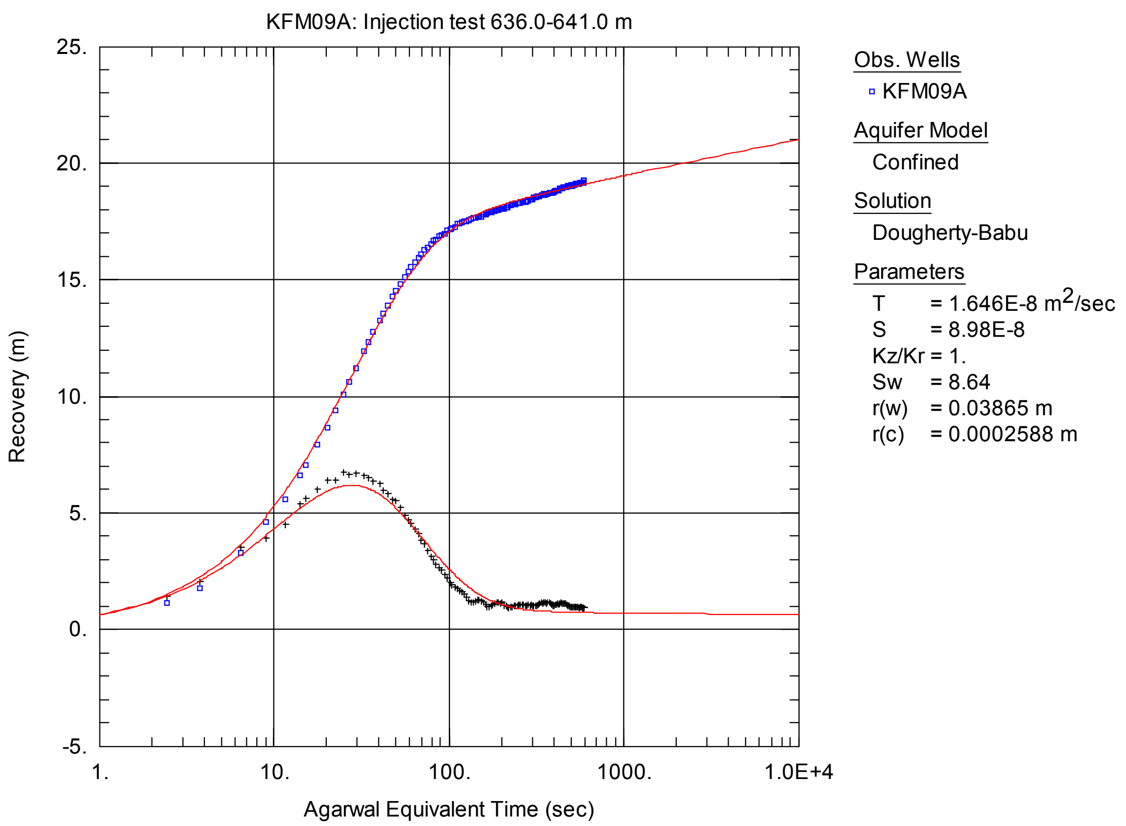


***Figure A3-533.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 636.0-641.0 m in KFM09A.*

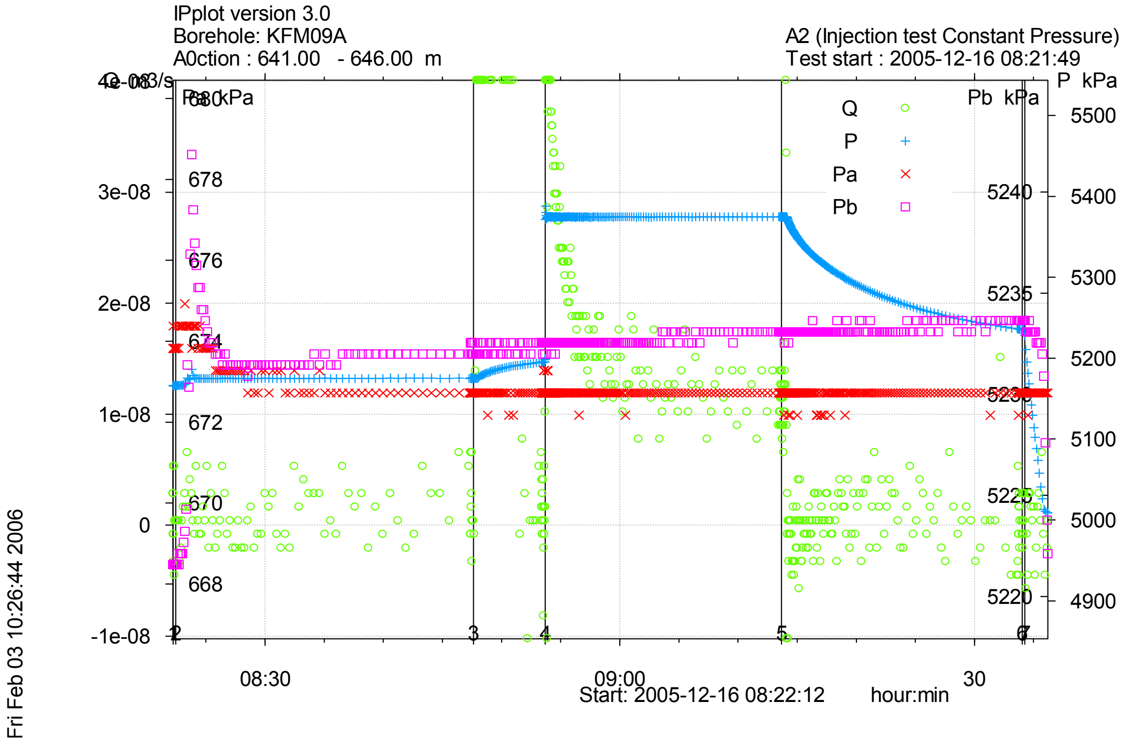


Figure A3-534. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 641.0-646.0 m in borehole KFM09A.*

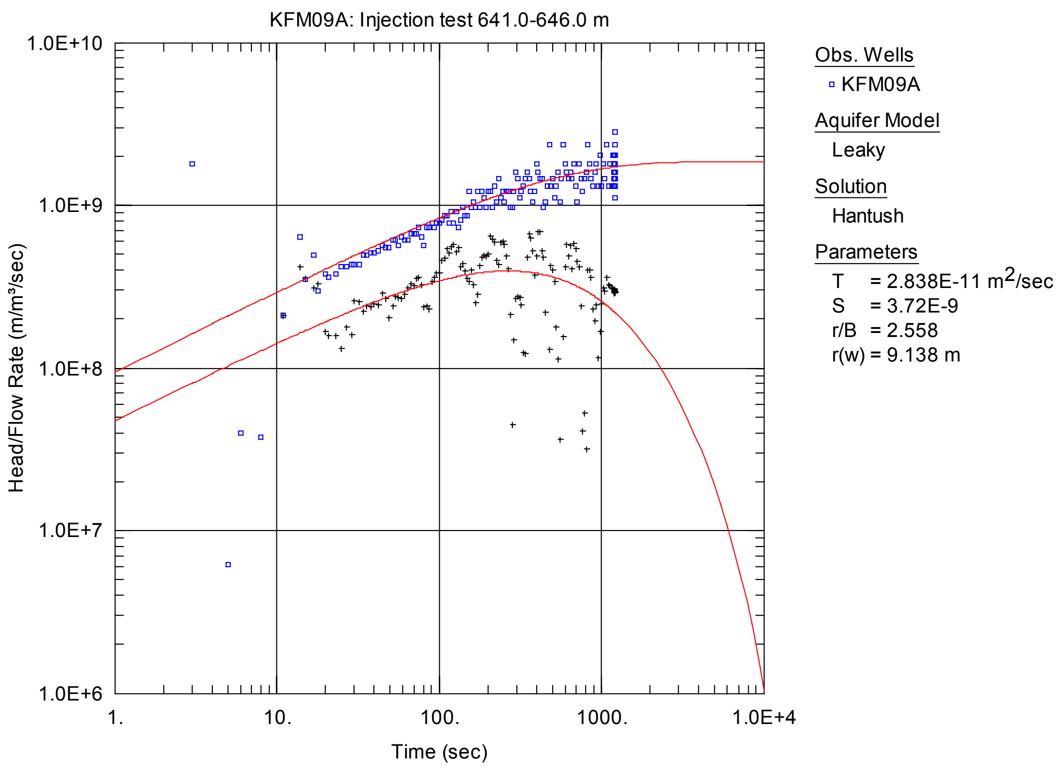


Figure A3-535. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 641.0-646.0 m in KFM09A.*

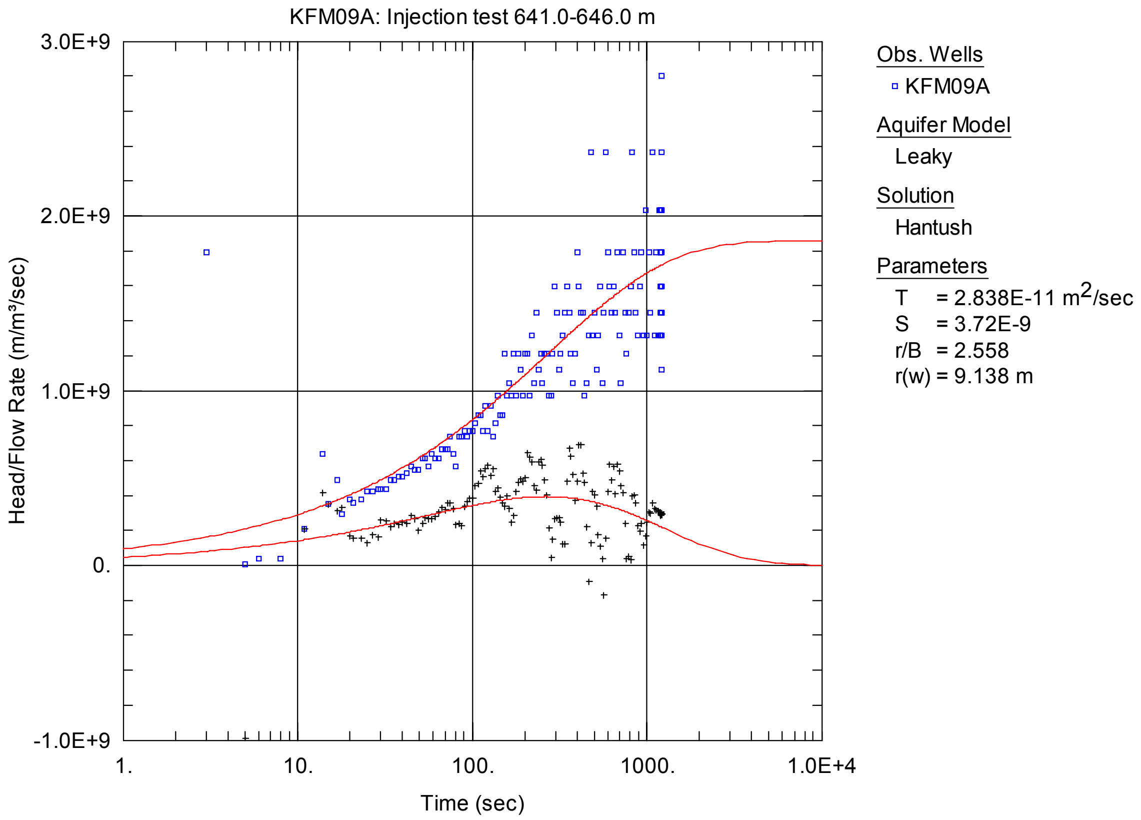


Figure A3-536. Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 641.0-646.0 m in KFM09A.

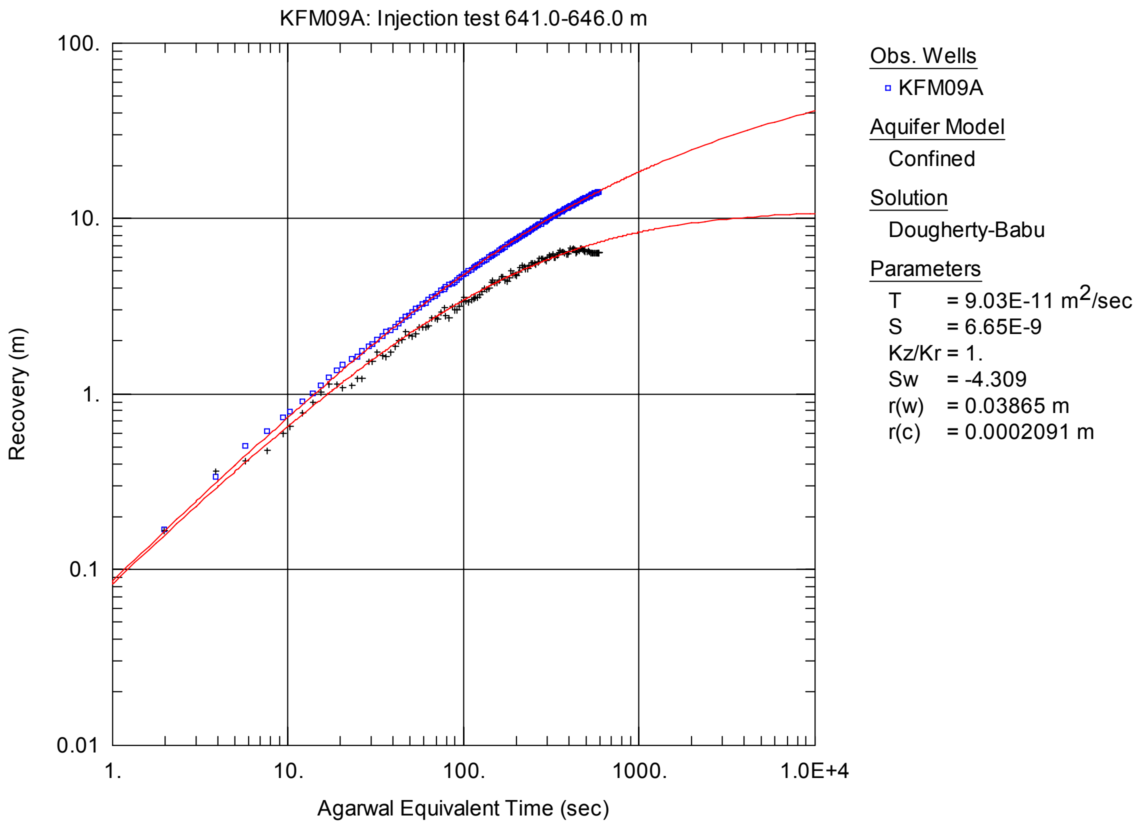


Figure A3-537. Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 641.0-646.0 m in KFM09A.

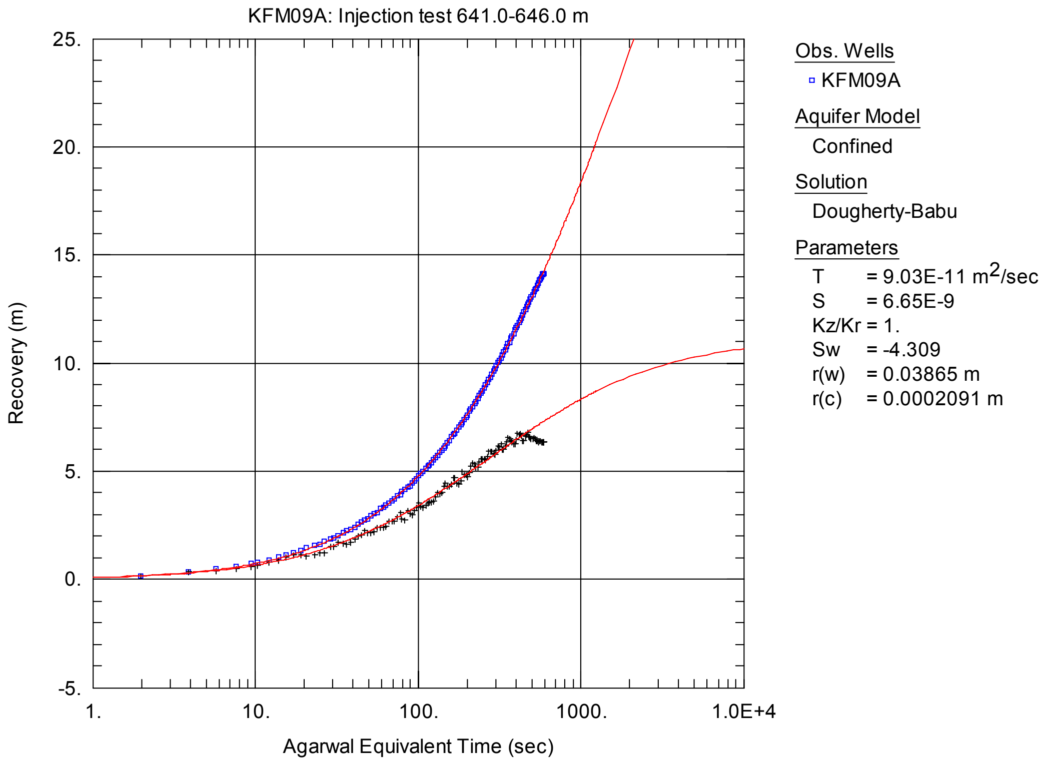


Figure A3-538. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 641.0-646.0 m in KFM09A.*

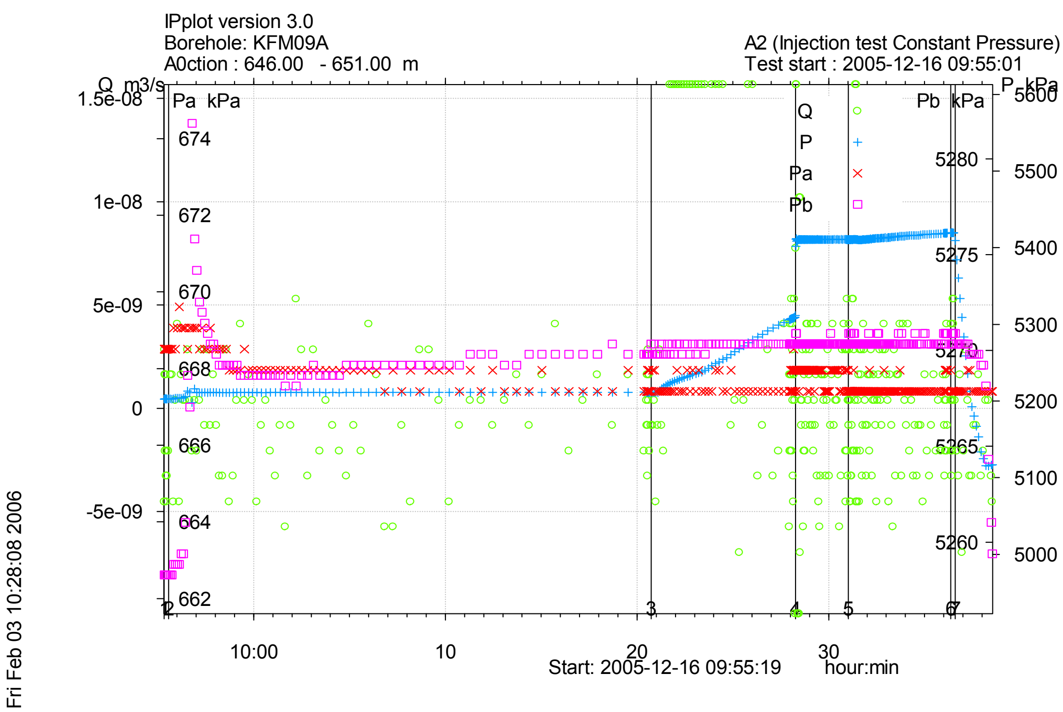


Figure A3-539. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 646.0-651.0 m in borehole KFM09A.*

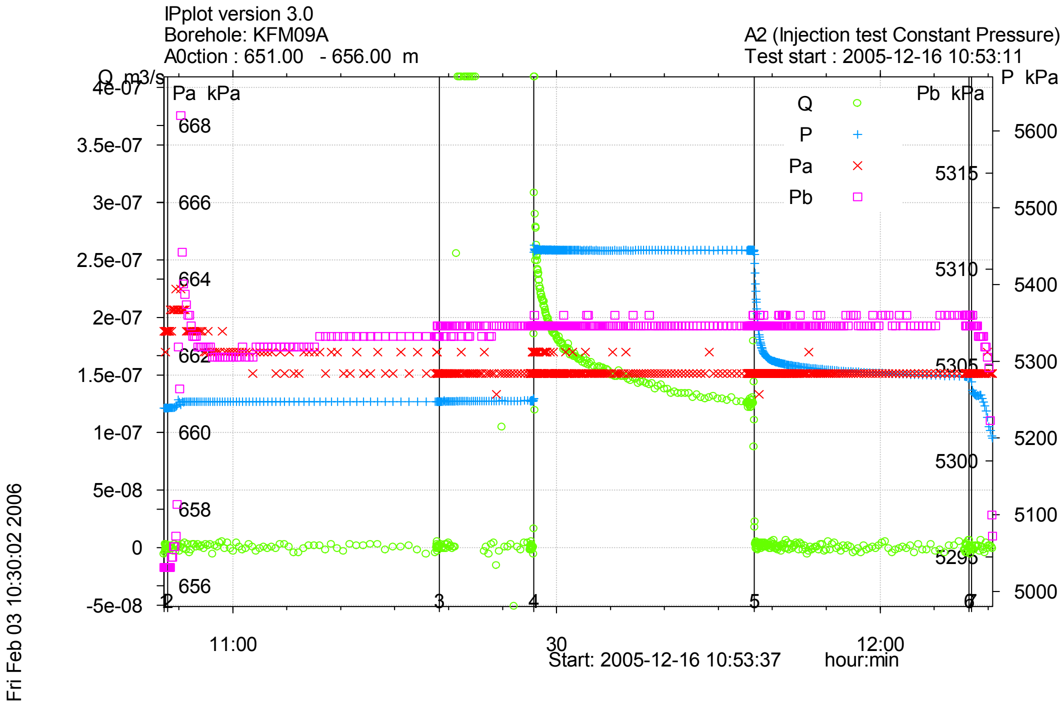


Figure A3-540. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 651.0-656.0 m in borehole KFM09A.*

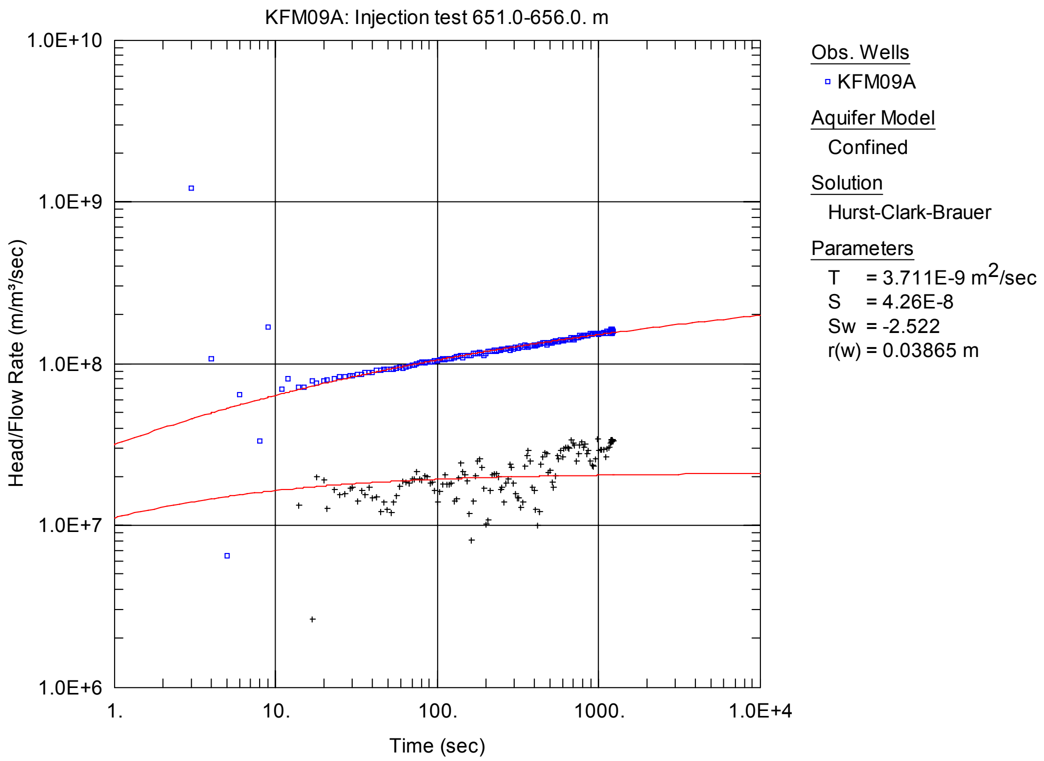


Figure A3-541. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 651.0-656.0 m in KFM09A.*

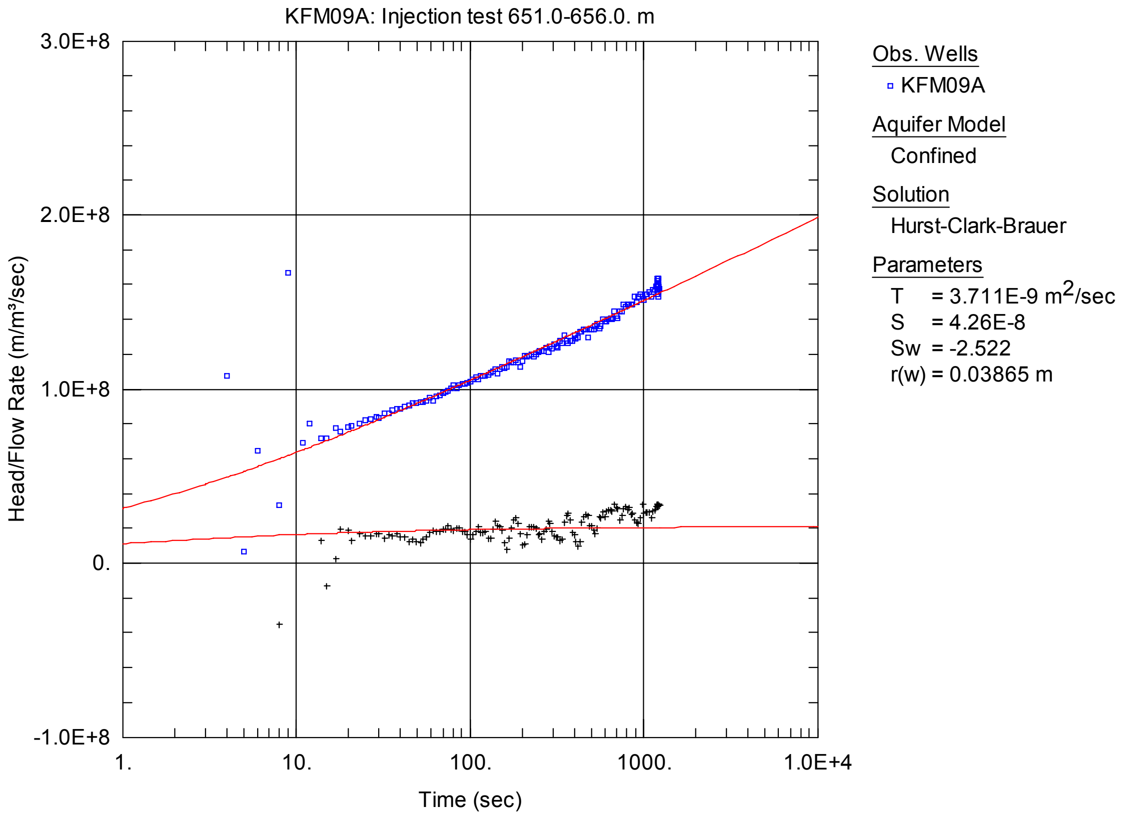


Figure A3-542. Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 651.0-656.0 m in KFM09A.

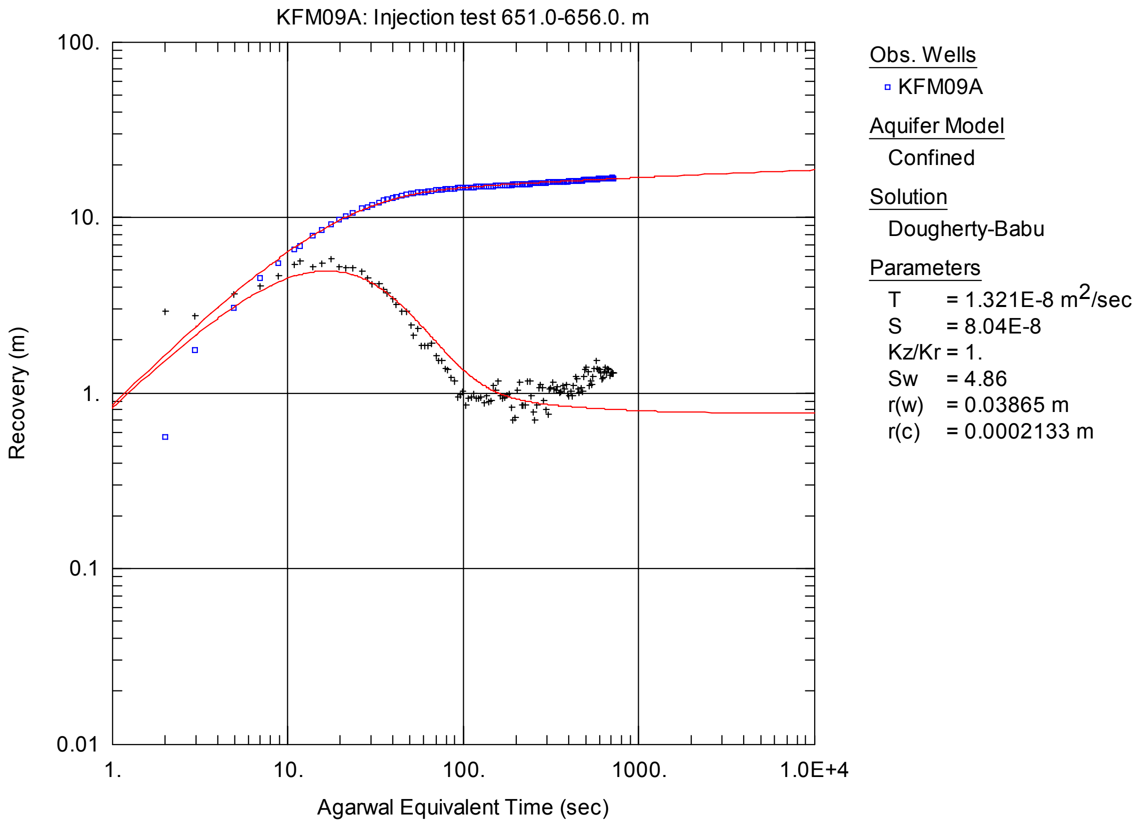


Figure A3-543. Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 651.0-656.0 m in KFM09A.

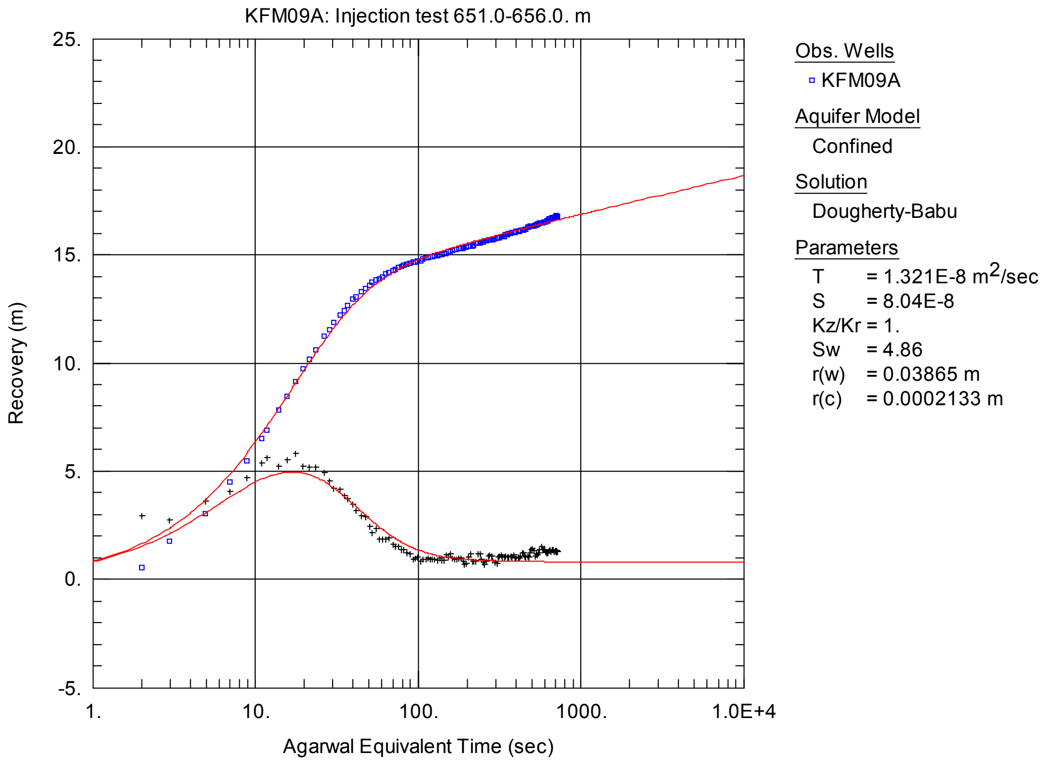


Figure A3-544. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 651.0-656.0 m in KFM09A.*

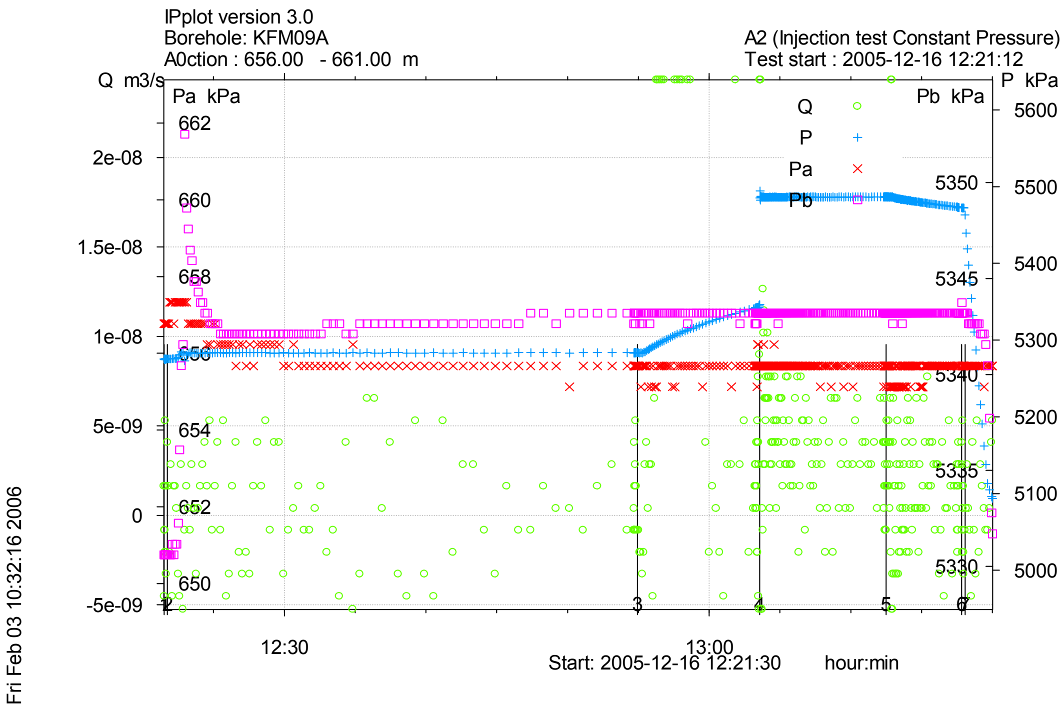


Figure A3-545. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 656.0-661.0 m in borehole KFM09A.*

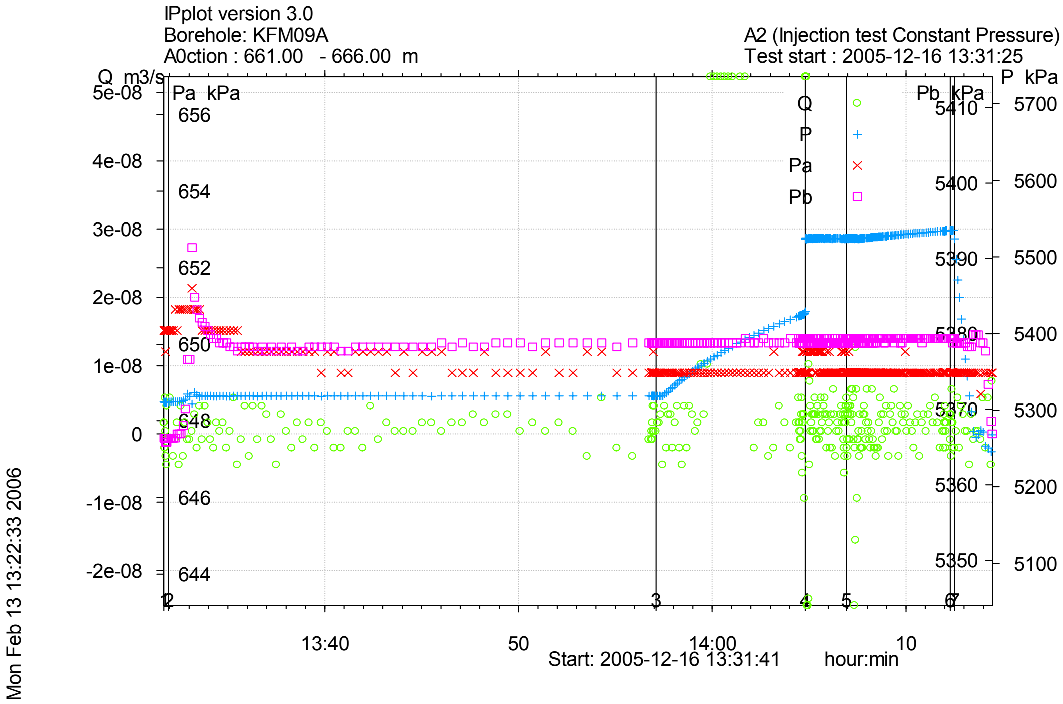


Figure A3-546. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 661.0-666.0 m in borehole KFM09A.*

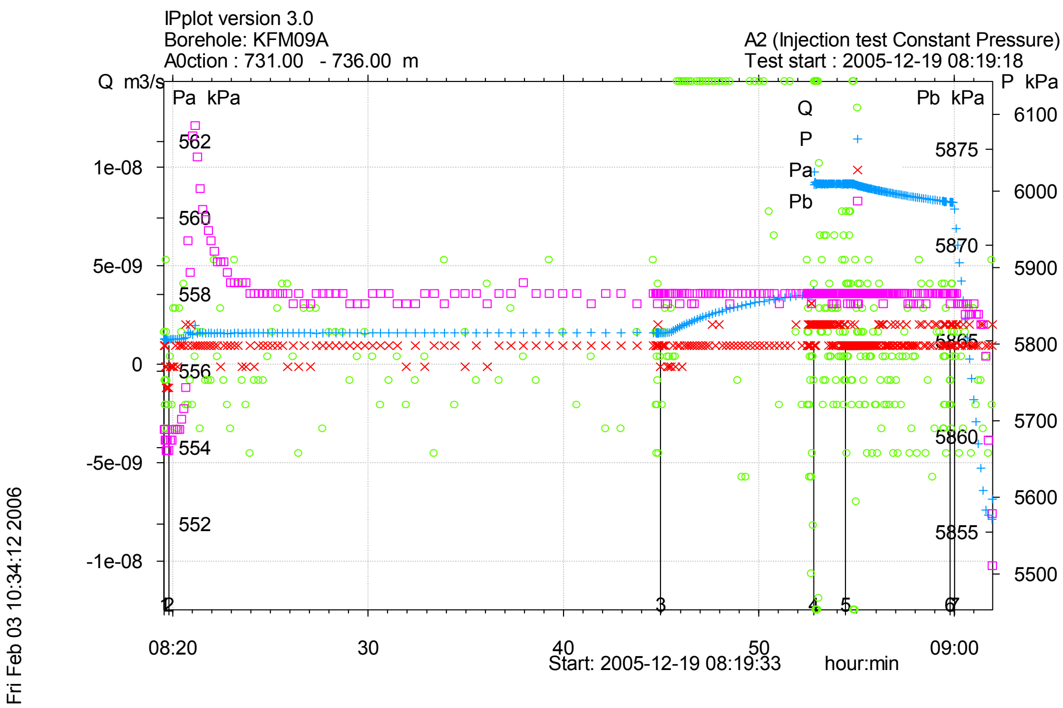


Figure A3-547. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 731.0-736.0 m in borehole KFM09A.*

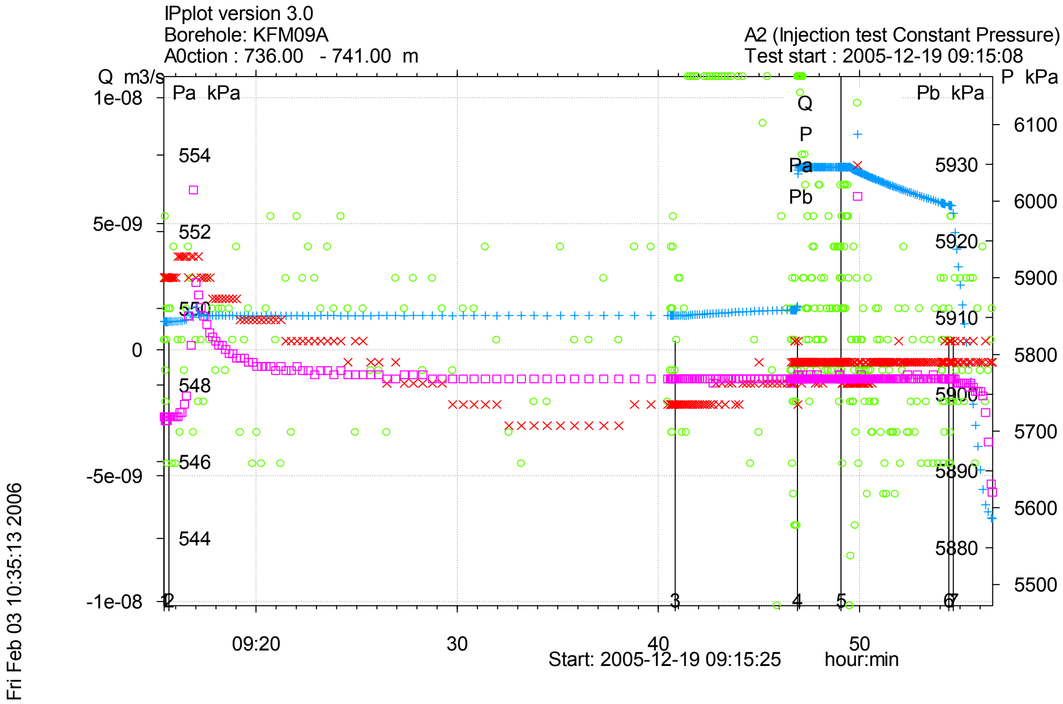


Figure A3-548. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 736.0-741.0 m in borehole KFM09A.*

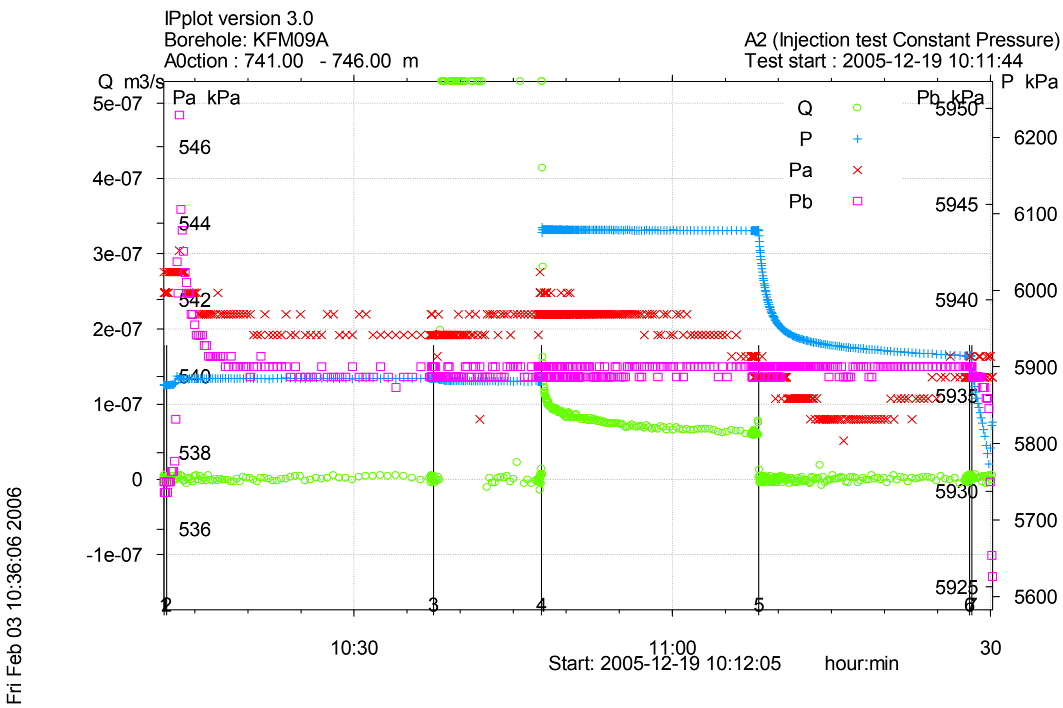


Figure A3-549. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 741.0-746.0 m in borehole KFM09A.*

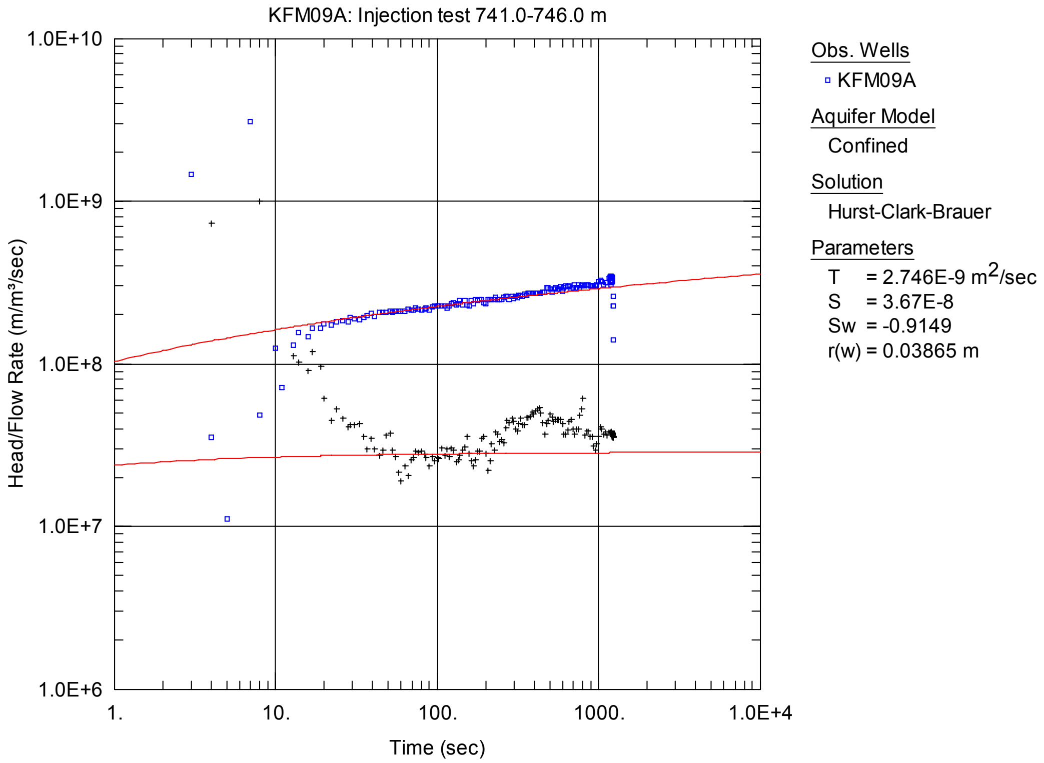


Figure A3-550. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 741.0-746.0 m in KFM09A. This plot shows a fit to the first of two different PRF:s during the injection period in this section.*

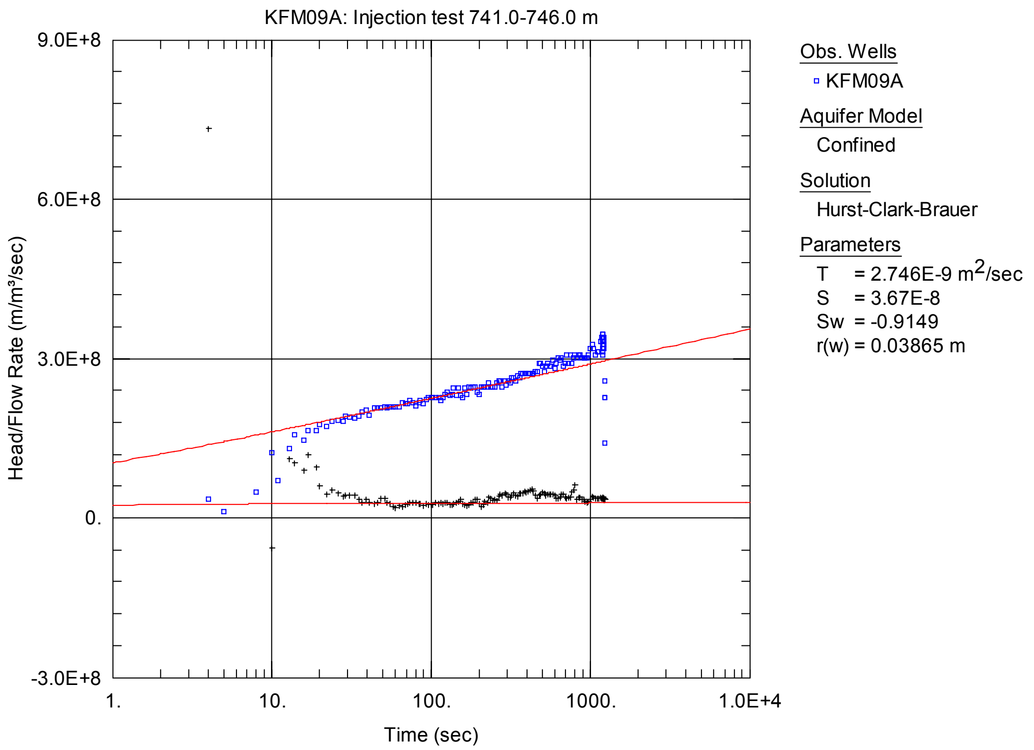


Figure A3-551. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 741.0-746.0 m in KFM09A. This plot shows a fit to the first of two different PRF:s during the injection period in this section.*

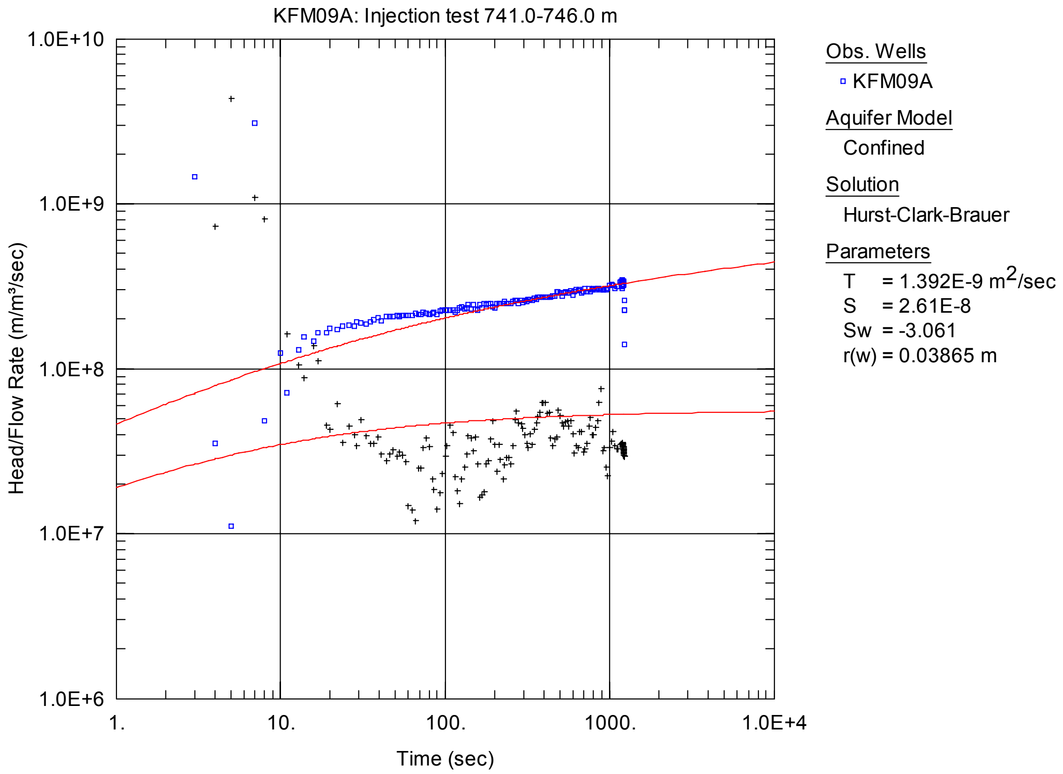


Figure A3-552. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 741.0-746.0 m in KFM09A. This plot shows a fit to the second of two different PRF:s during the injection period in this section.*

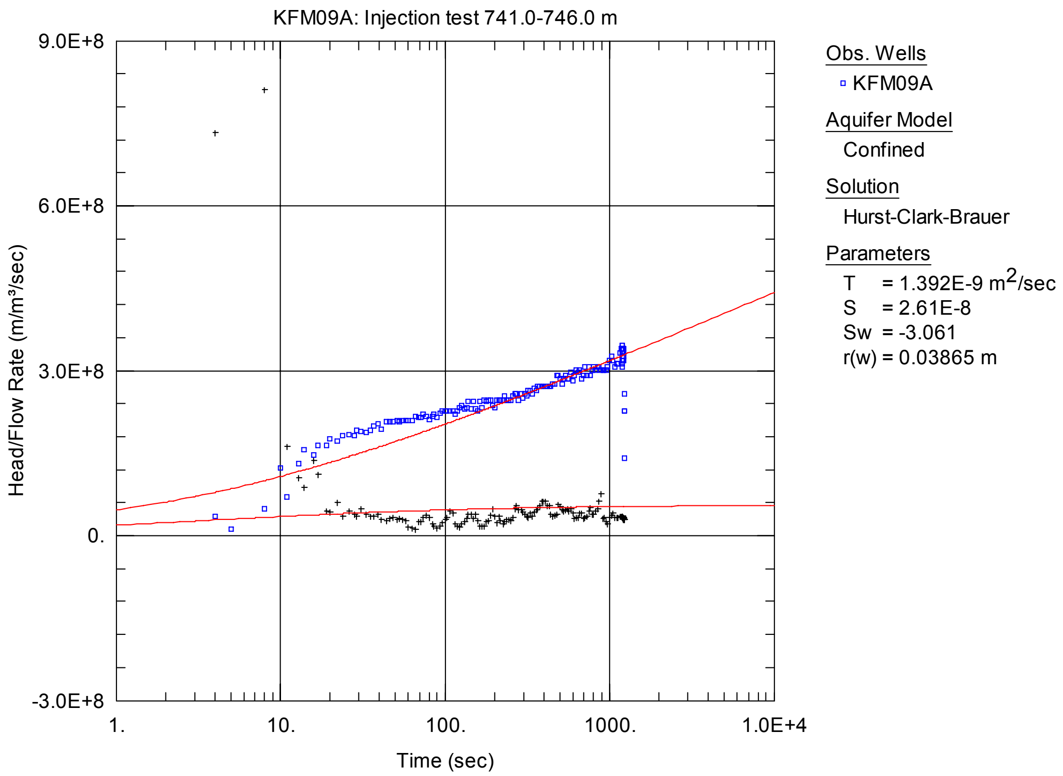


Figure A3-553. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 741.0-746.0 m in KFM09A. This plot shows a fit to the second of two different PRF:s during the injection period in this section.*

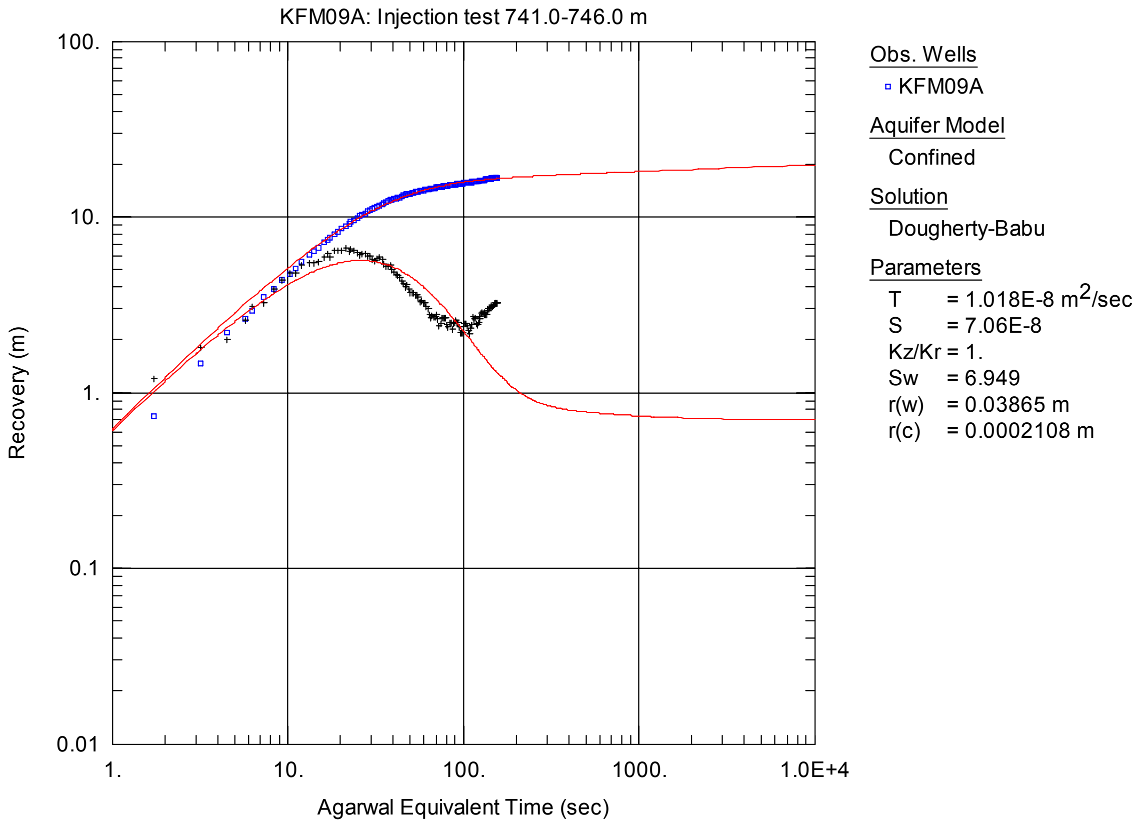


Figure A3-554. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 741.0-746.0 m in KFM09A.*

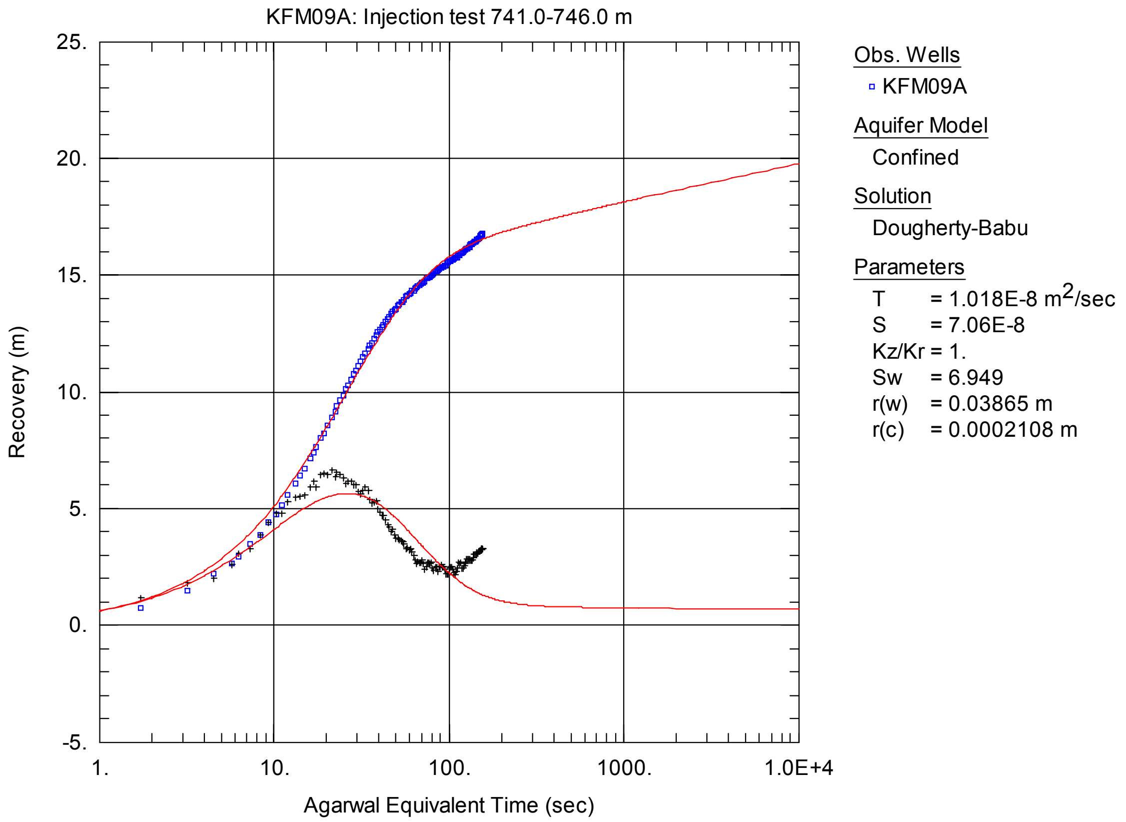


Figure A3-555. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 741.0-746.0 m in KFM09A.*

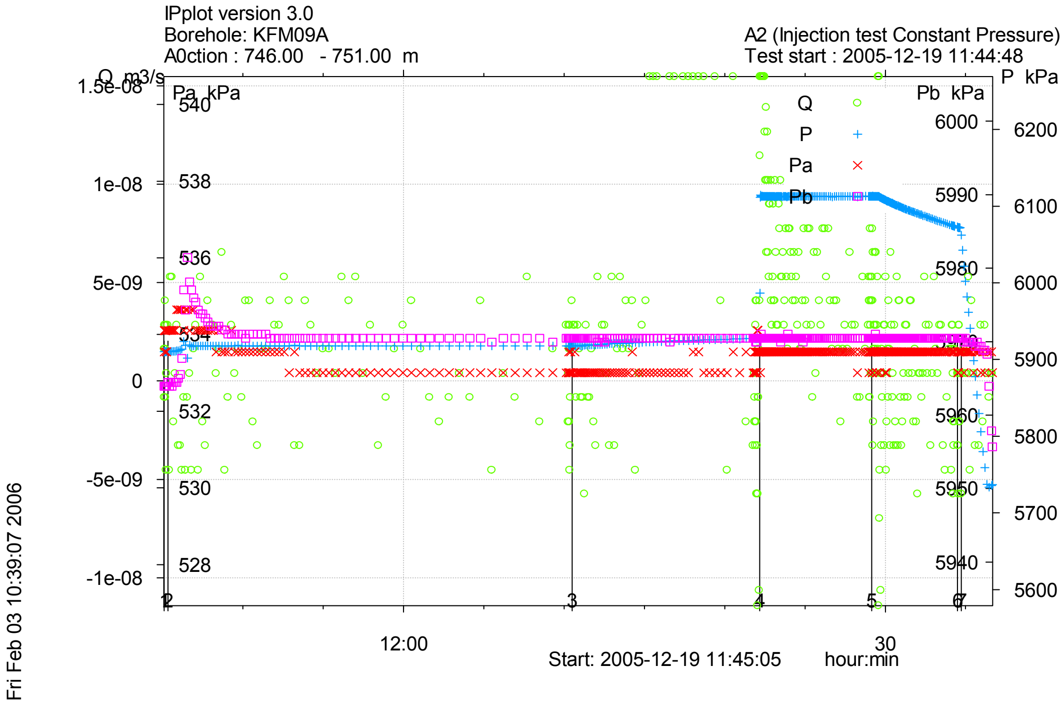


Figure A3-556. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 746.0-751.0 m in borehole KFM09A.*

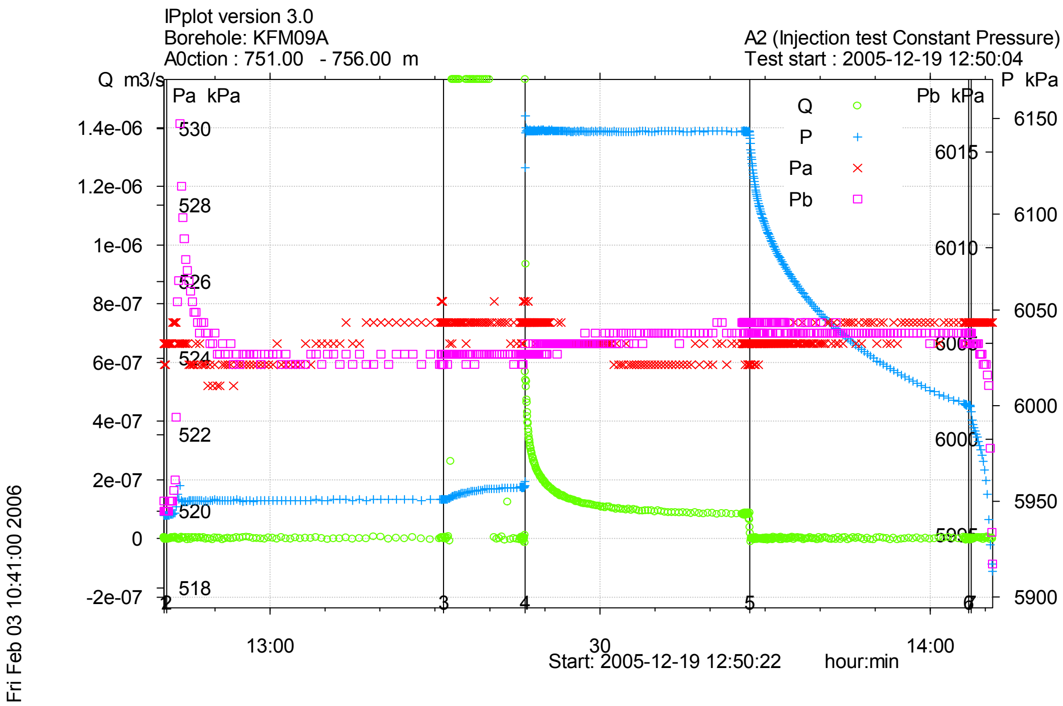


Figure A3-557. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 751.0-756.0 m in borehole KFM09A.*

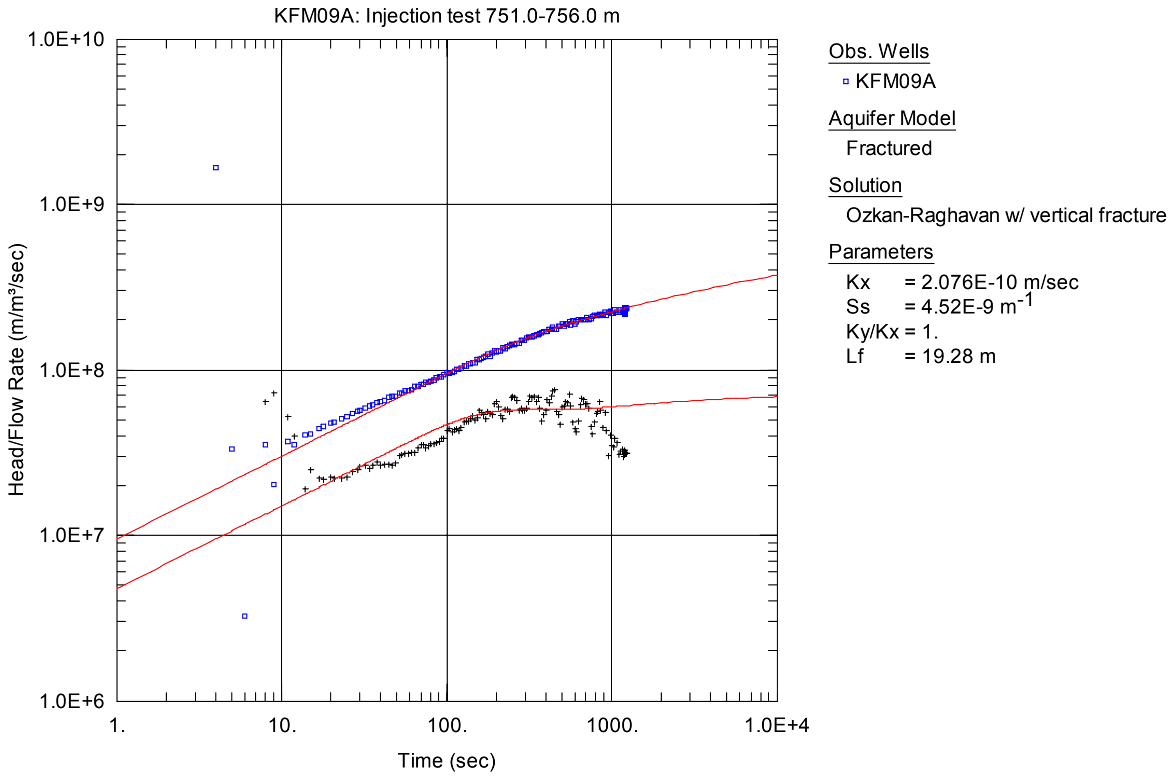


Figure A3-558. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 751.0-756.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

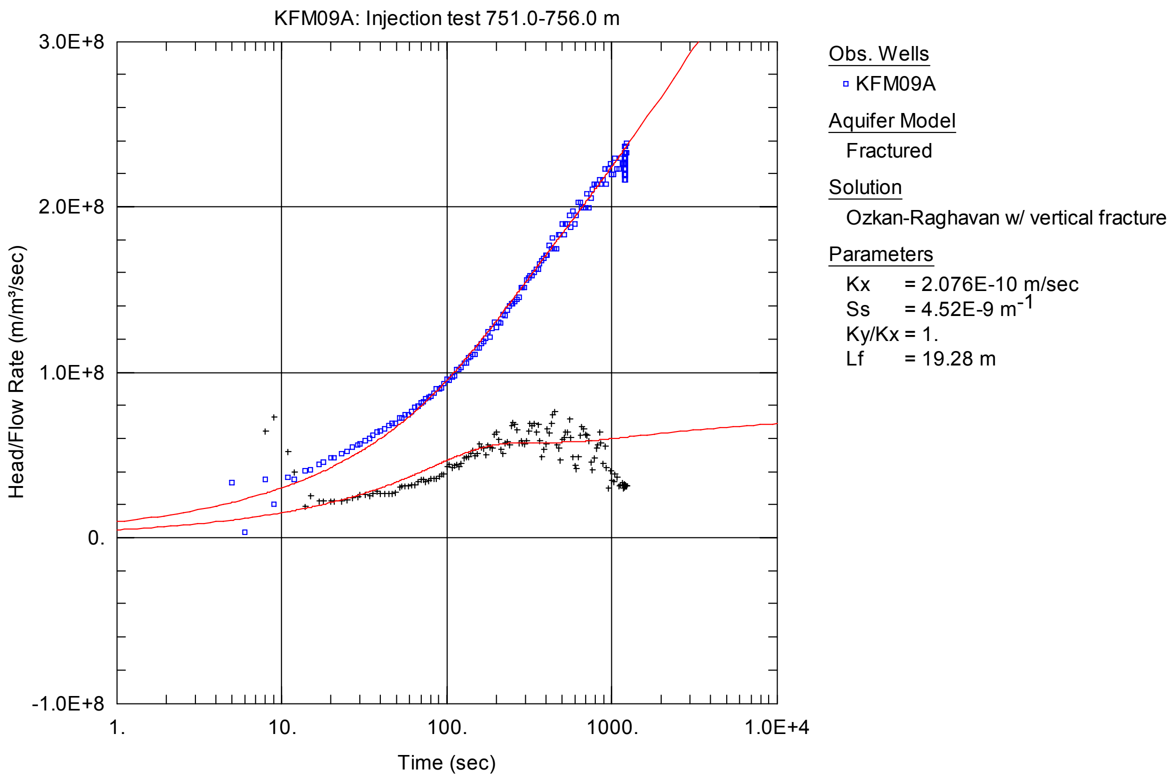


Figure A3-559. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 751.0-756.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

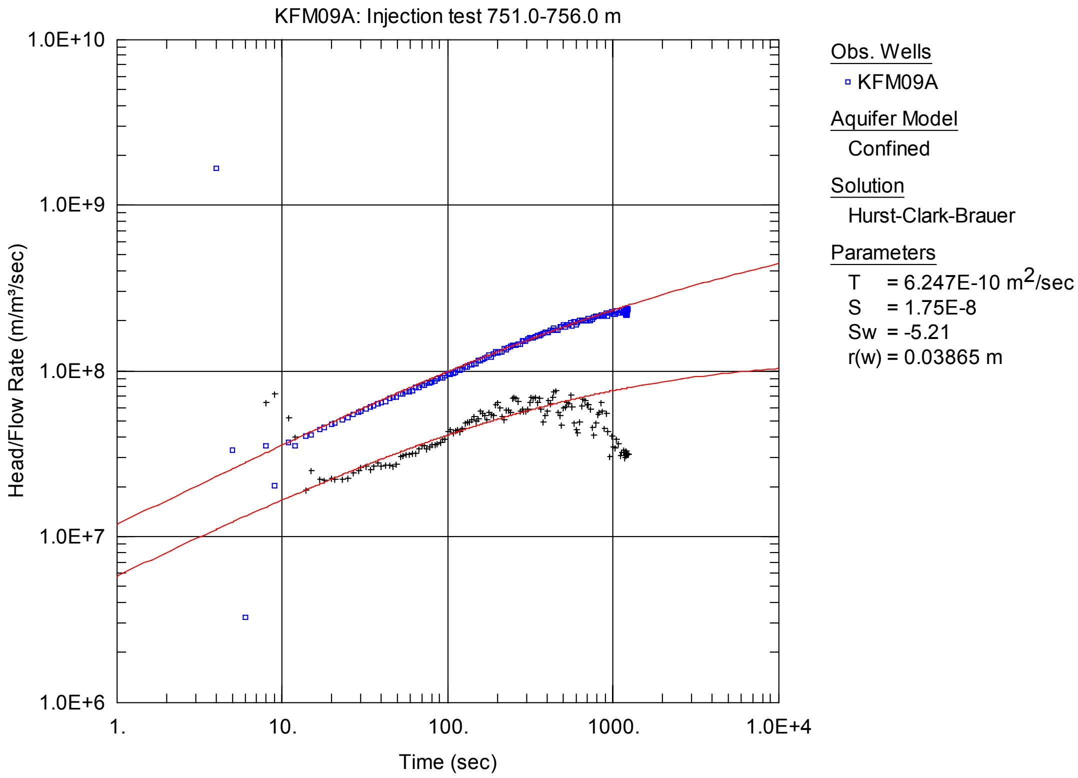


Figure A3-560. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 751.0-756.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for a pseudo-radial response.*

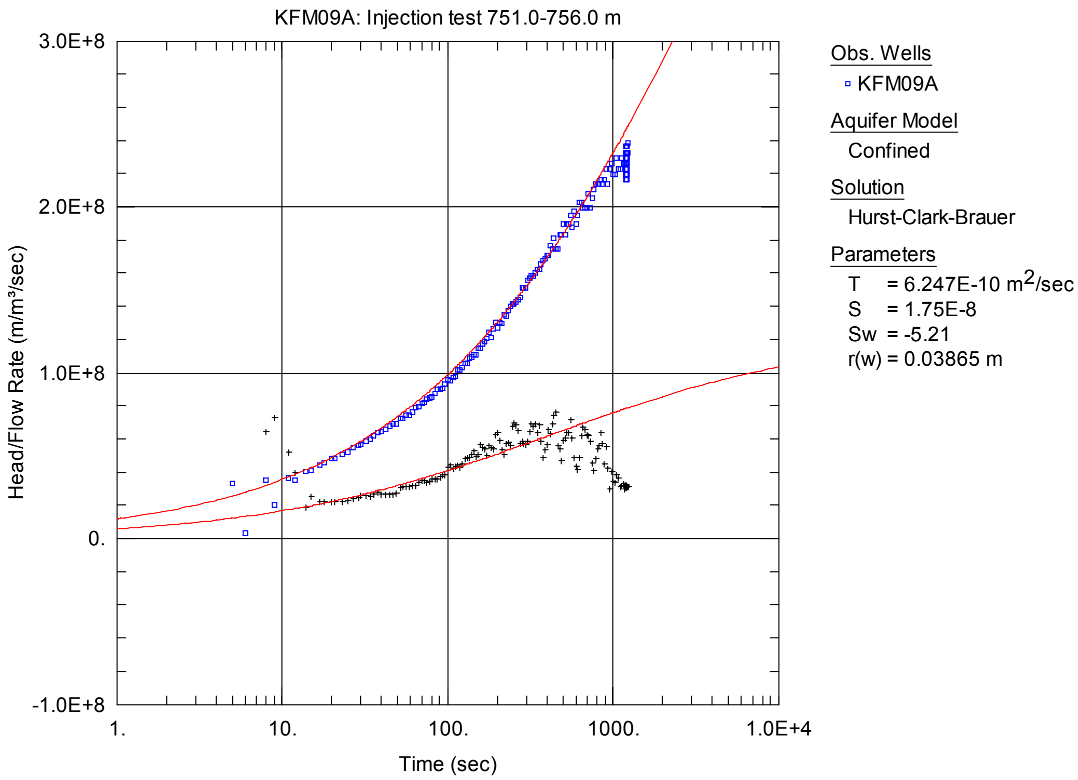


Figure A3-561. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 751.0-756.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for a pseudo-radial response.*

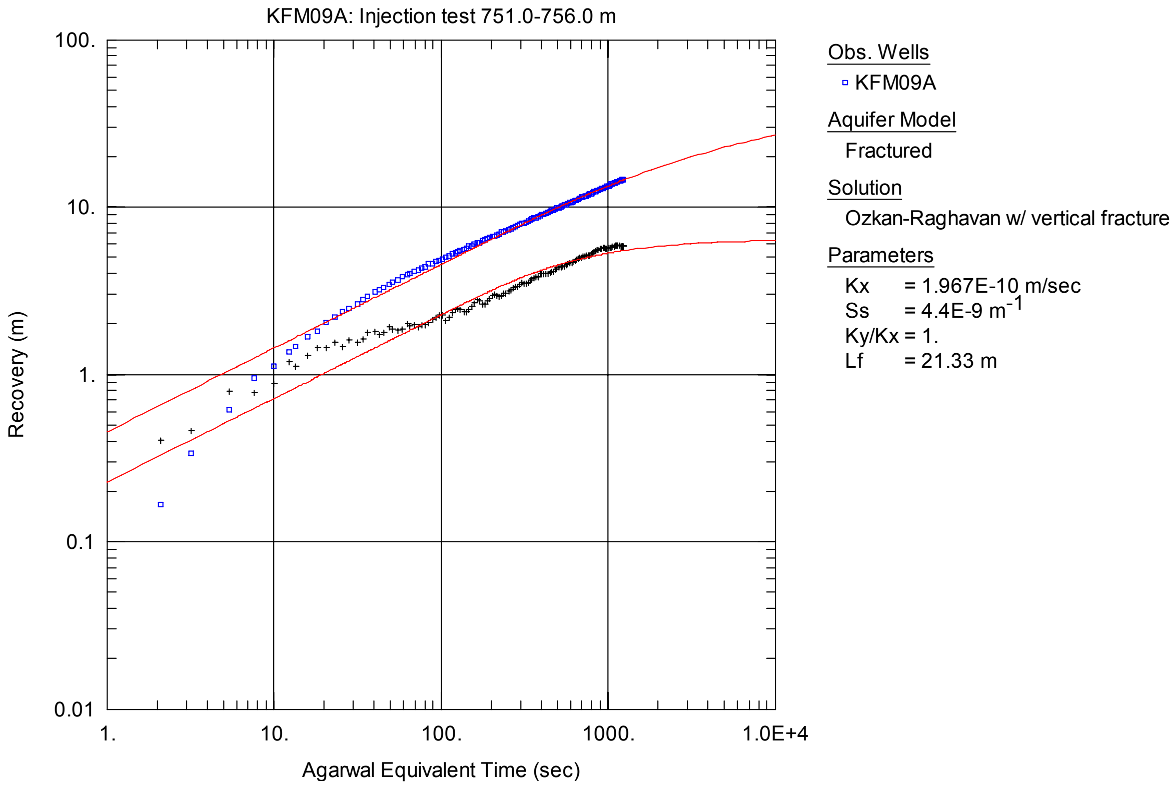


Figure A3-562. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 751.0-756.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

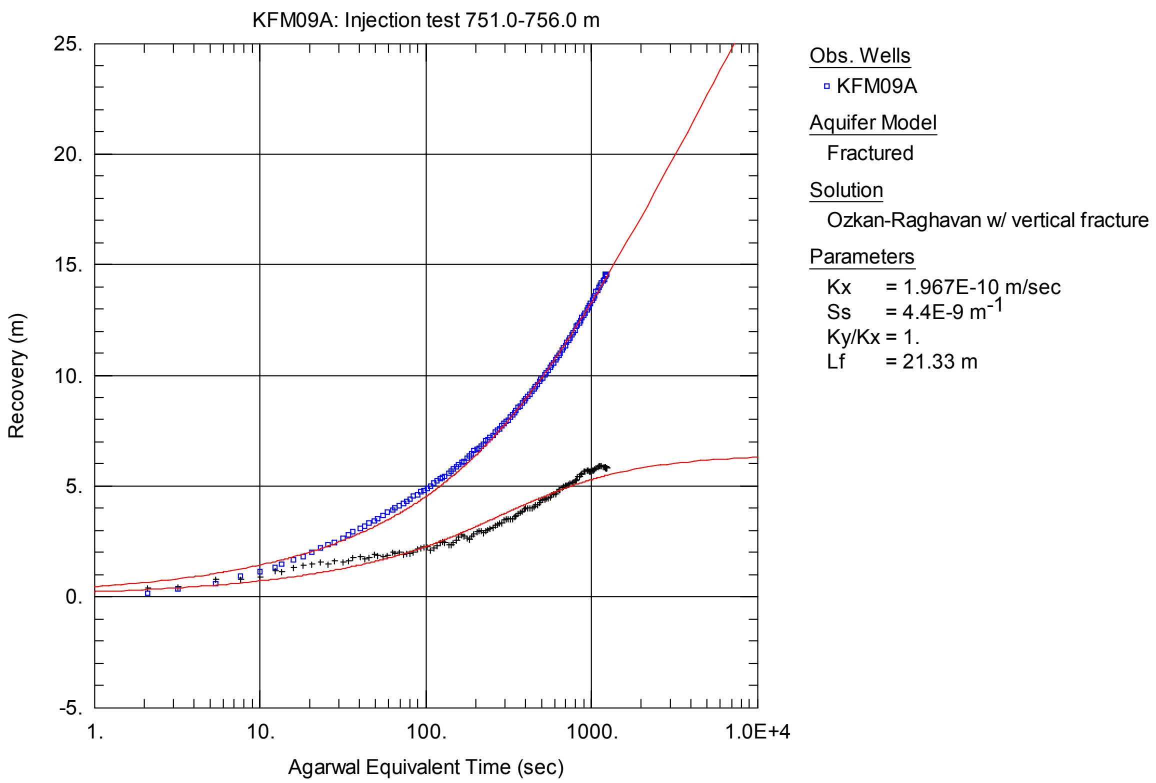


Figure A3-563. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 751.0-756.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

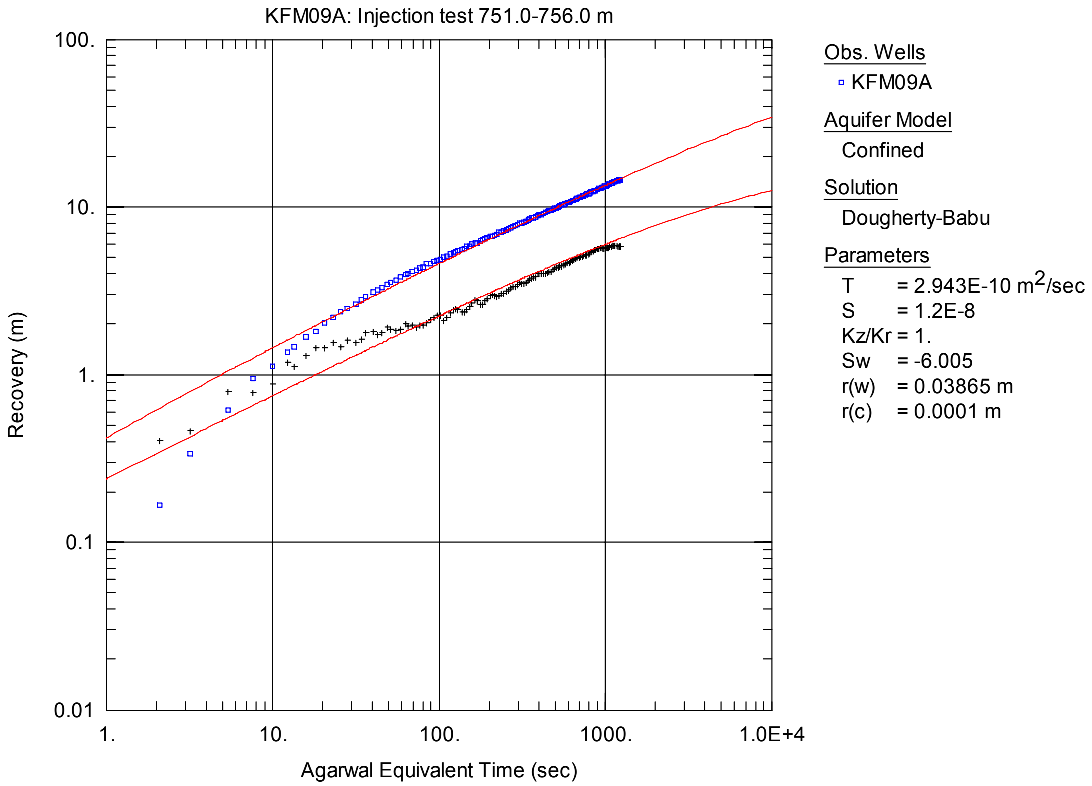


Figure A3-564. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 751.0-756.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

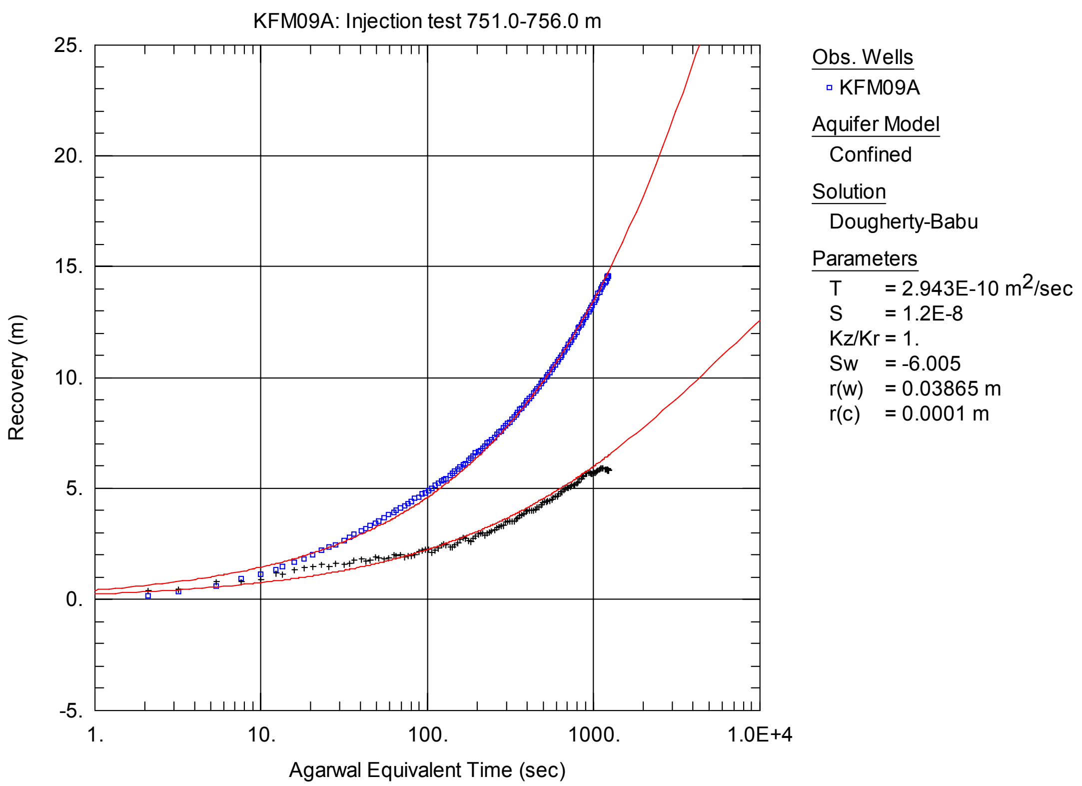


Figure A3-565. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 751.0-756.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

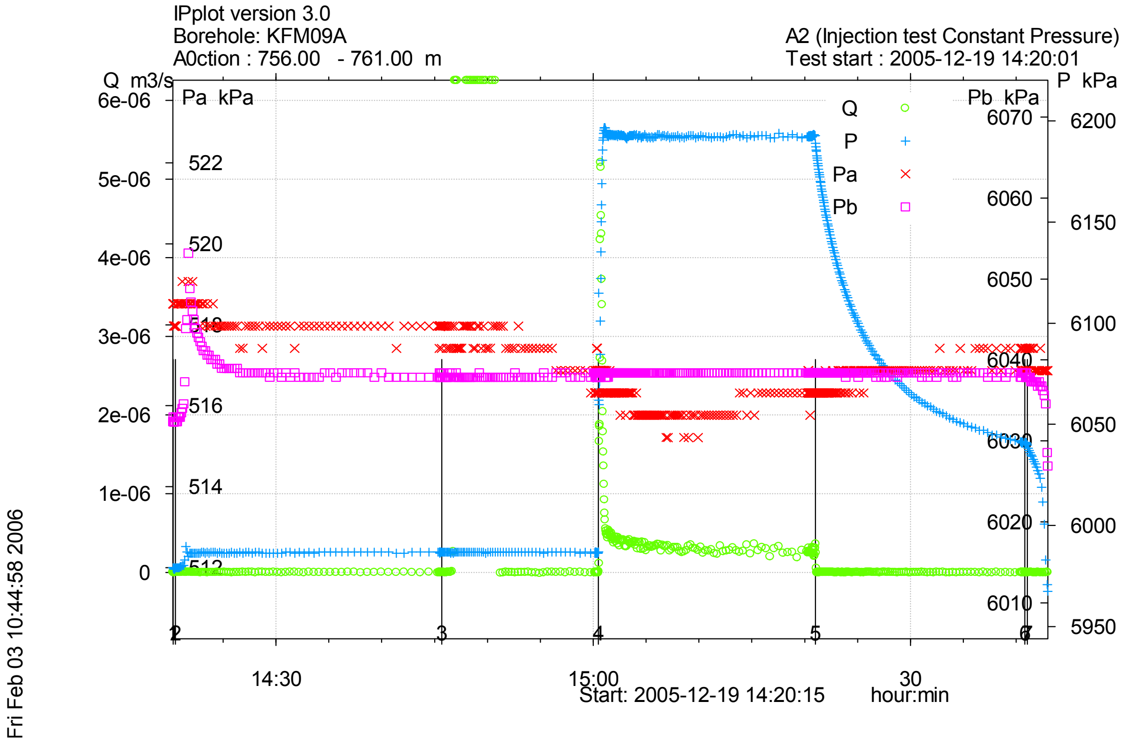


Figure A3-566. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 756.0-761.0 m in borehole KFM09A.*

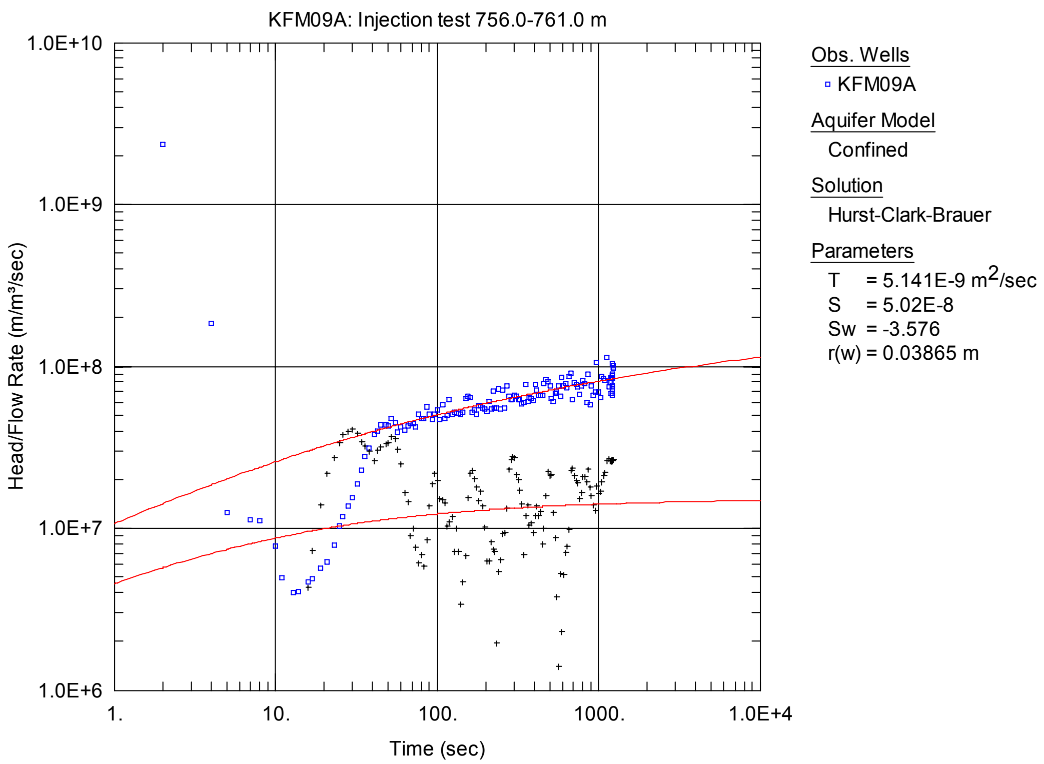


Figure A3-567. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 756.0-761.0 m in KFM09A.*

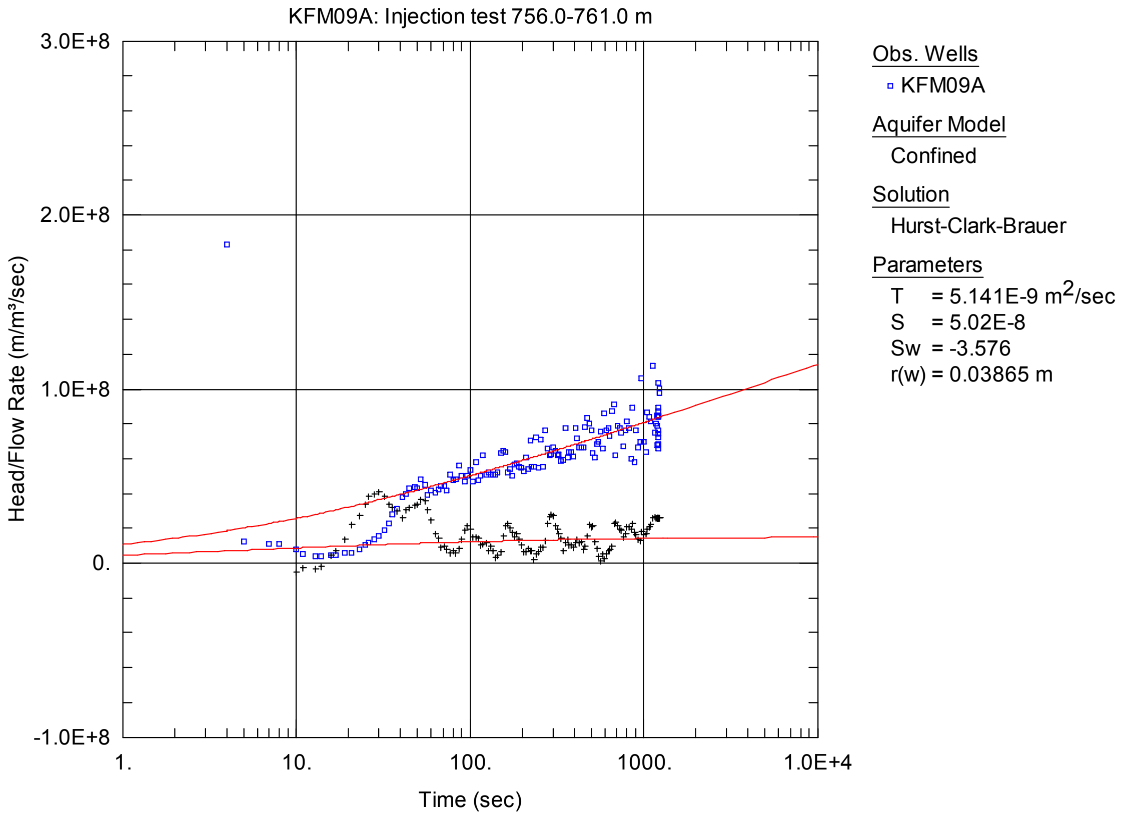


Figure A3-568. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 756.0-761.0 m in KFM09A.*

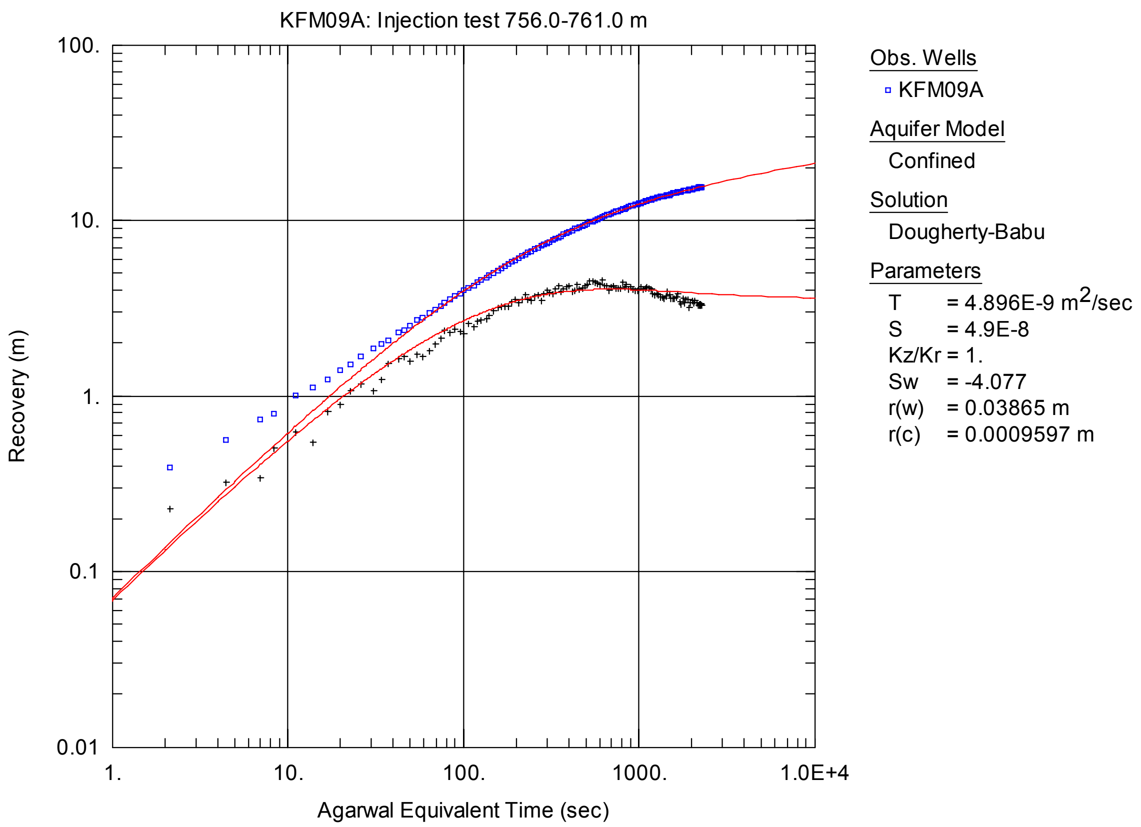


Figure A3-569. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 756.0-761.0 m in KFM09A.*

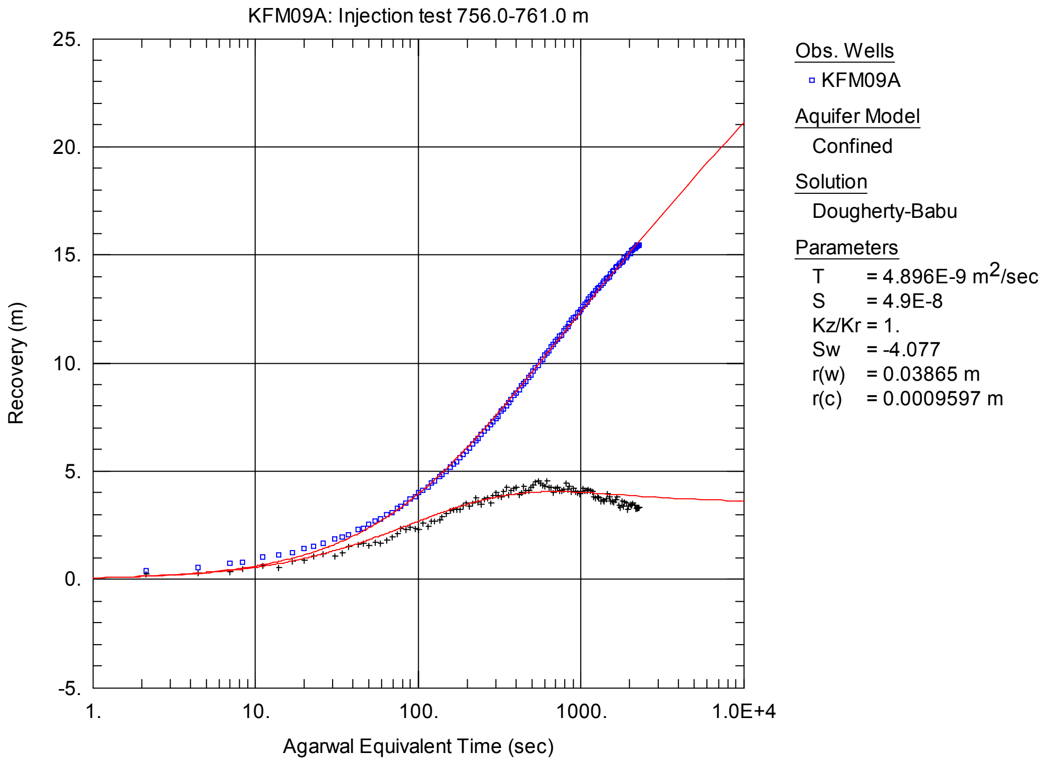


Figure A3-570. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 756.0-761.0 m in KFM09A.*

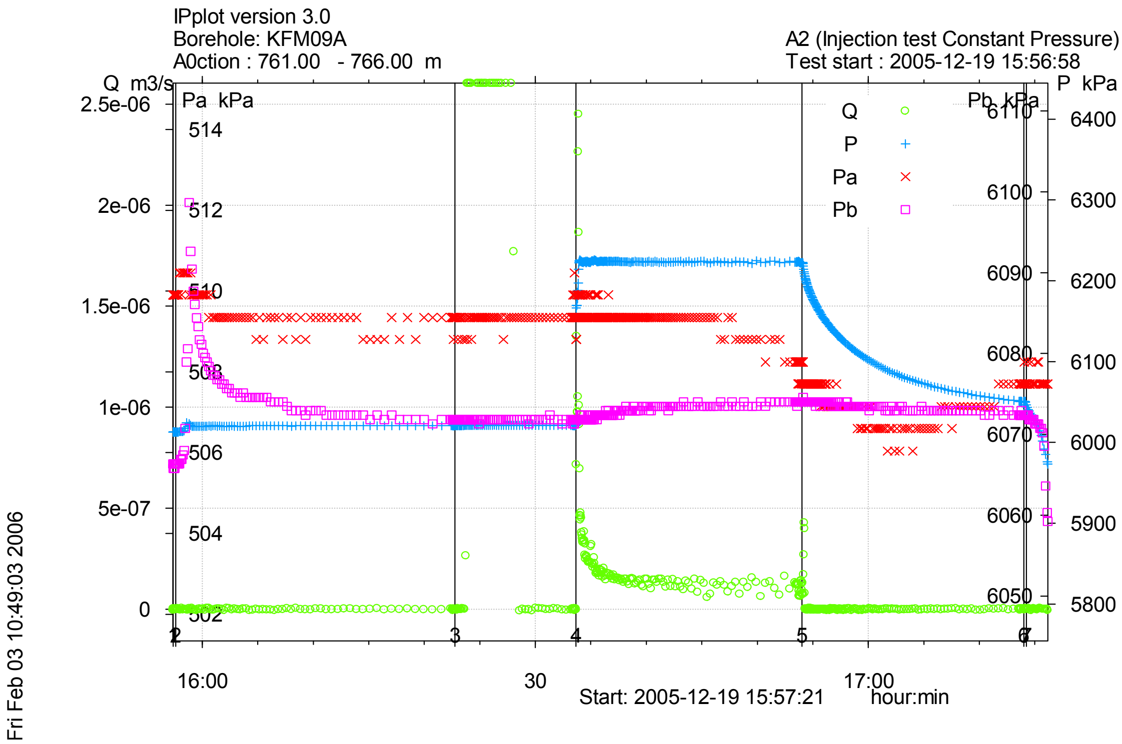


Figure A3-571. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 761.0-766.0 m in borehole KFM09A.*

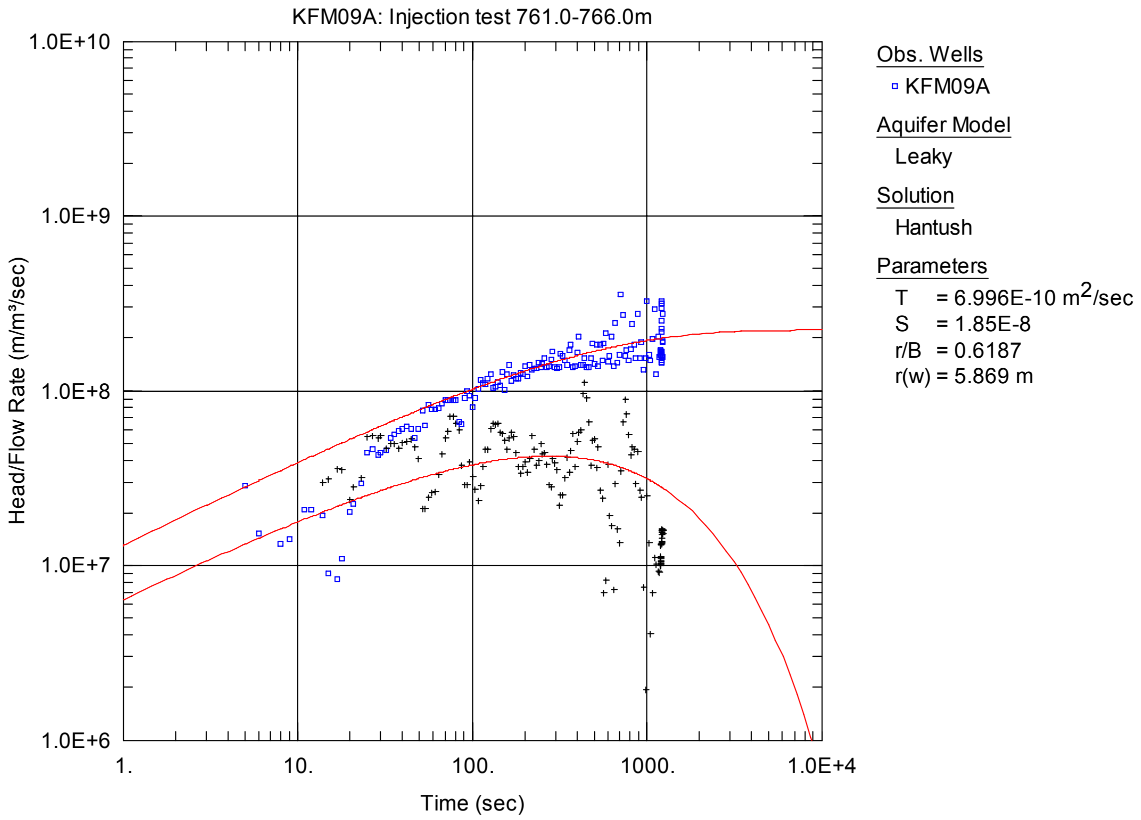


Figure A3-572. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 761.0-766.0 m in KFM09A.*

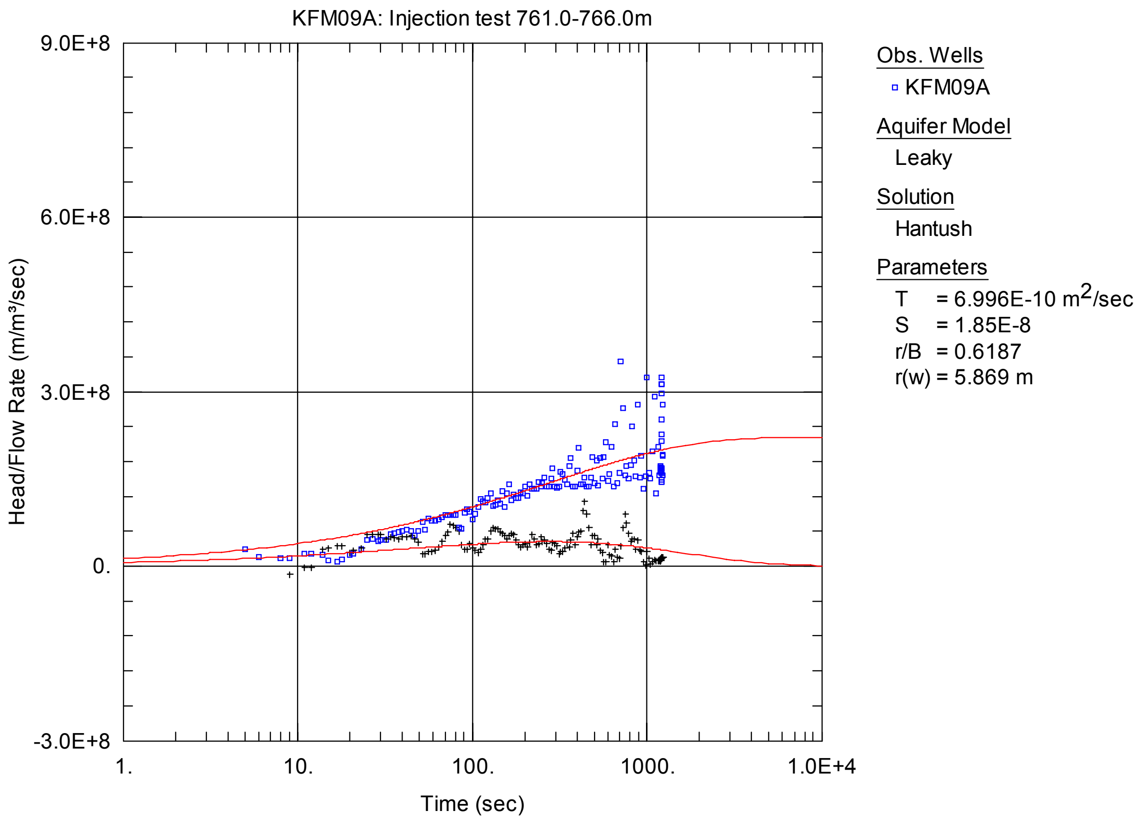


Figure A3-573. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 761.0-766.0 m in KFM09A.*

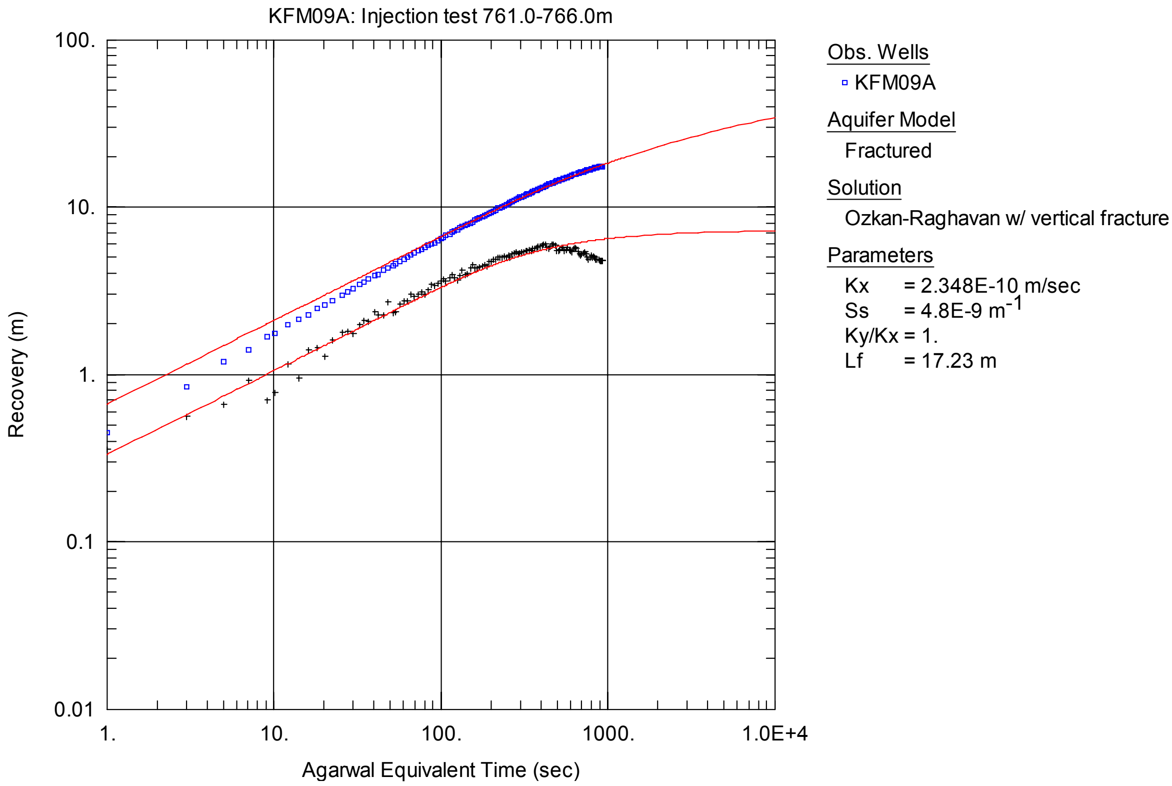


***Figure A3-574.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 761.0-766.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

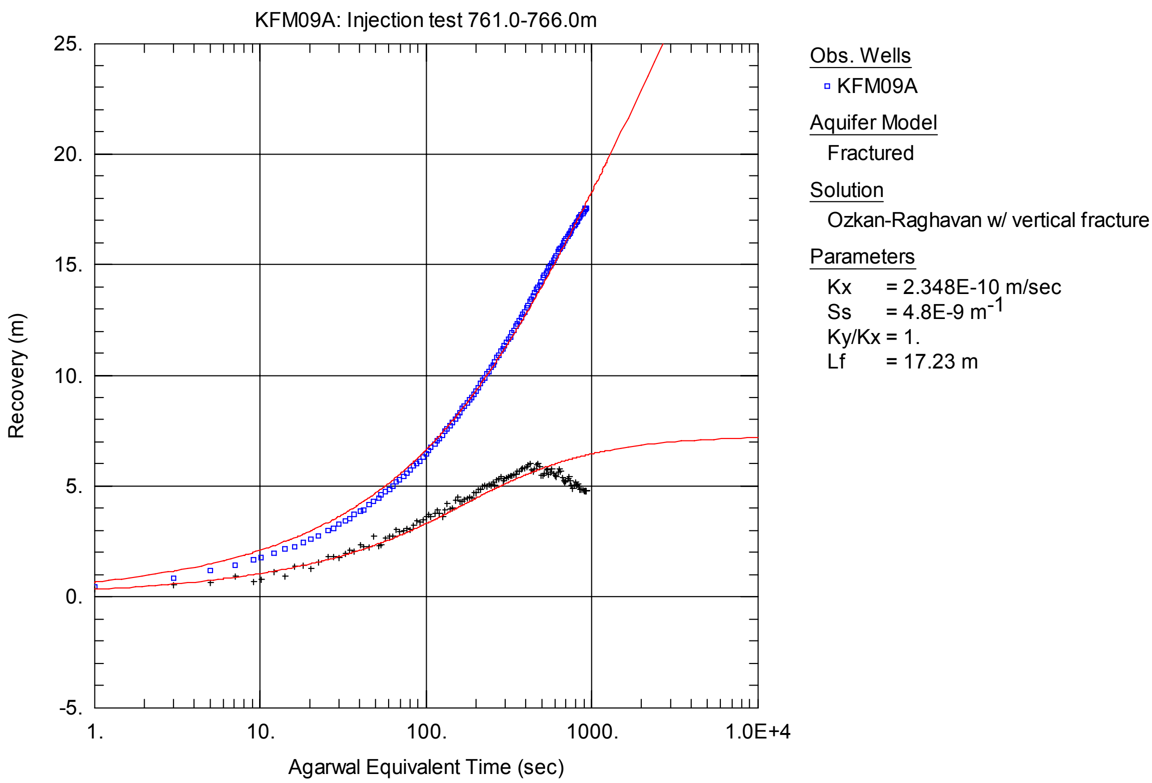


***Figure A3-575.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 761.0-766.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

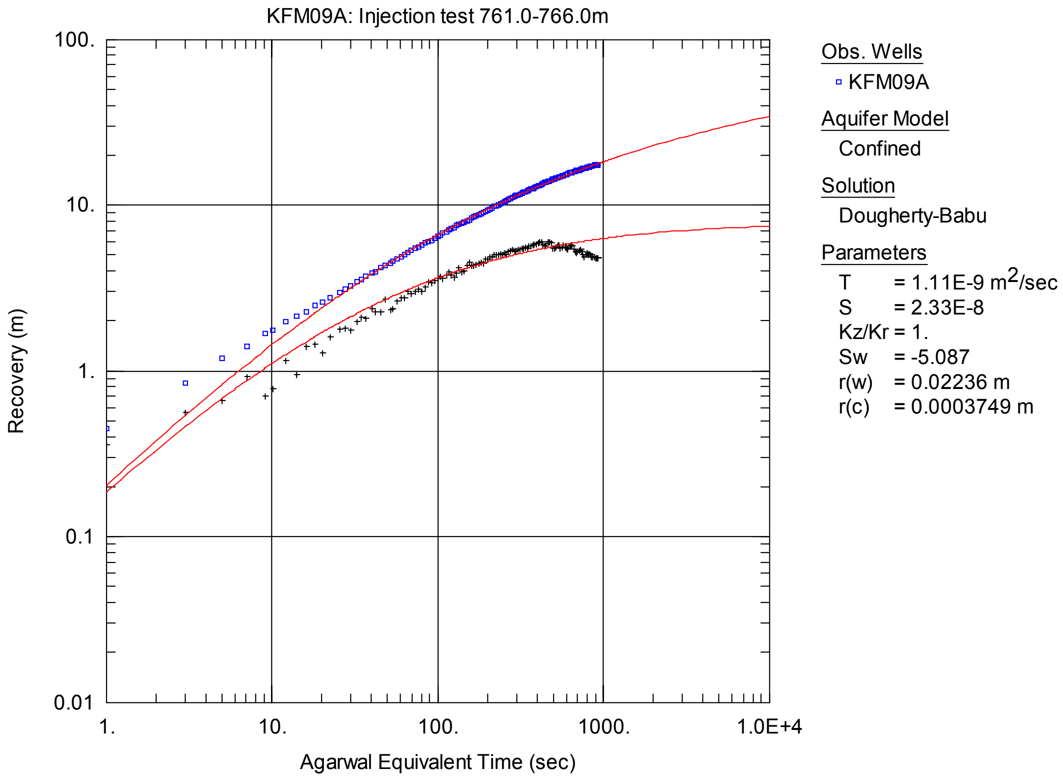


Figure A3-576. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 761.0-766.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

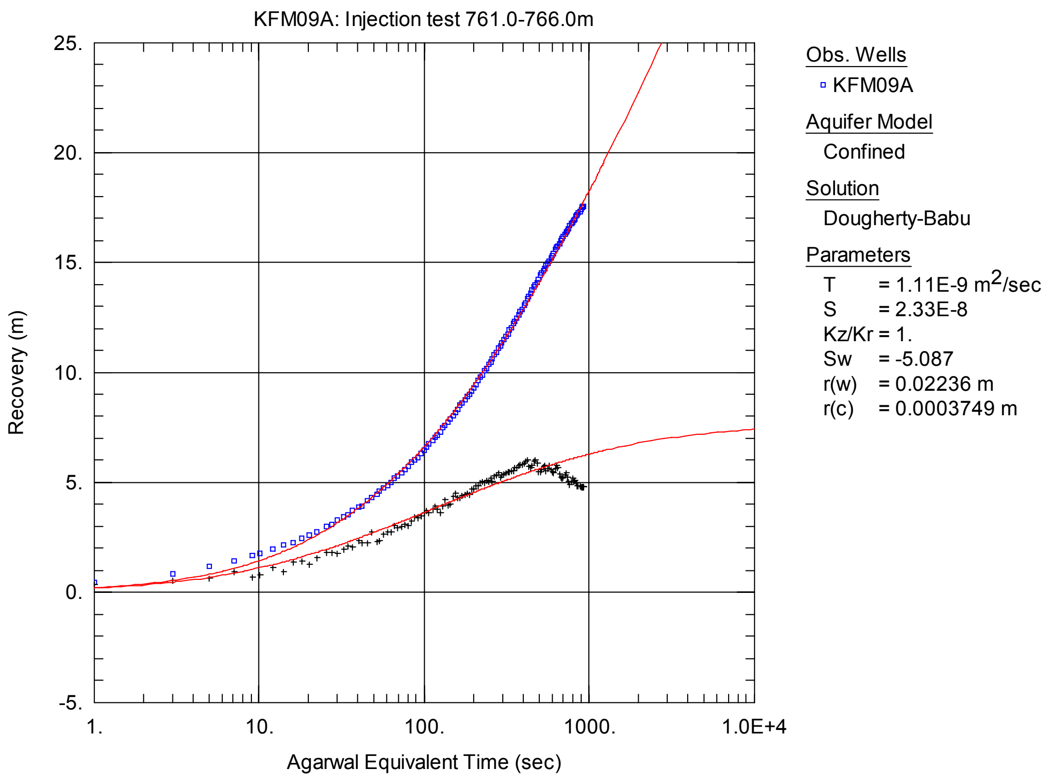


Figure A3-577. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 761.0-766.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

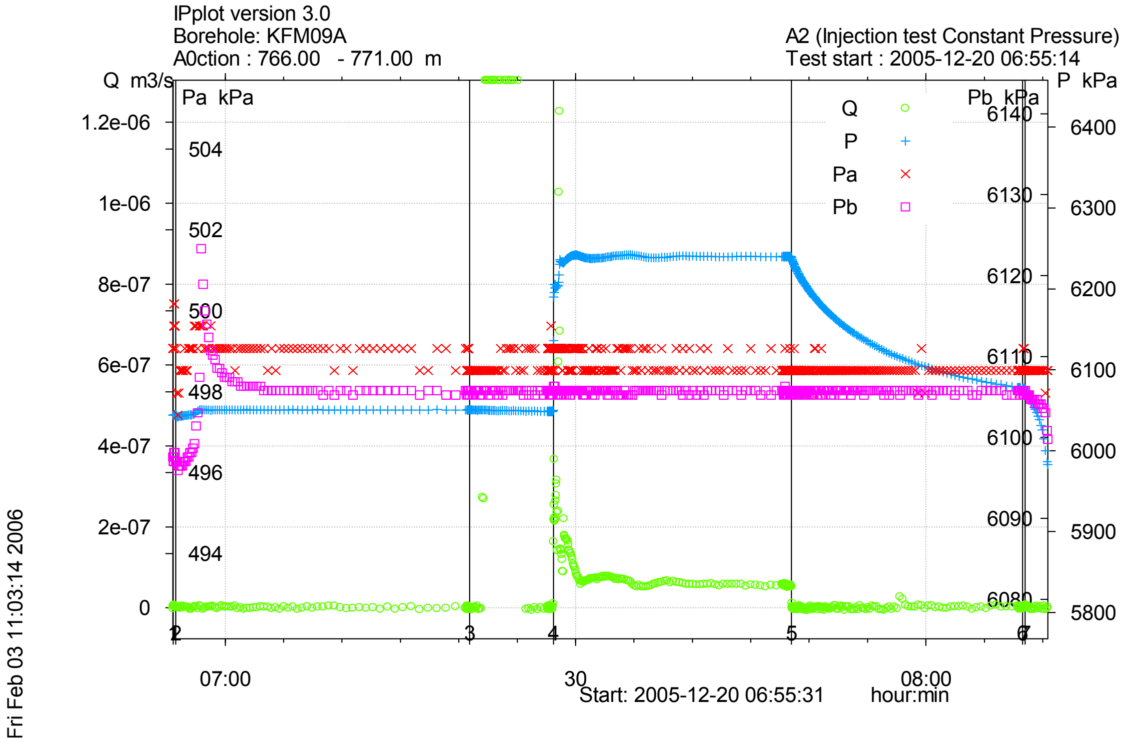


Figure A3-578. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 766.0-771.0 m in borehole KFM09A.*

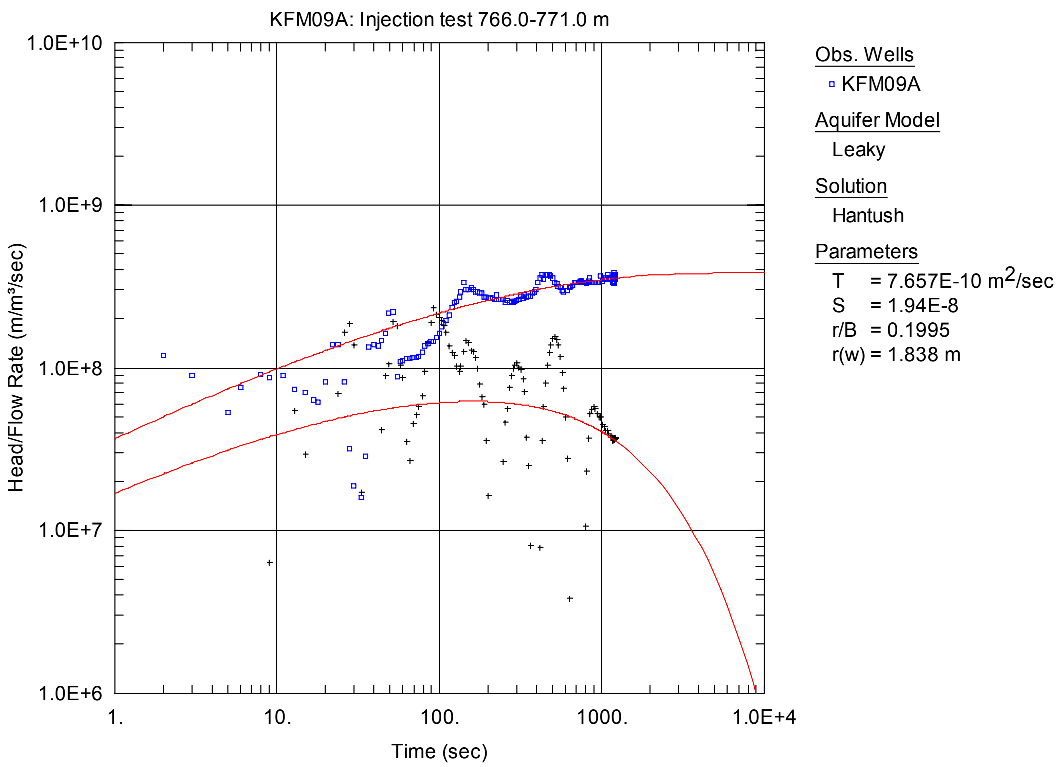


Figure A3-579. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 766.0-771.0 m in KFM09A.*

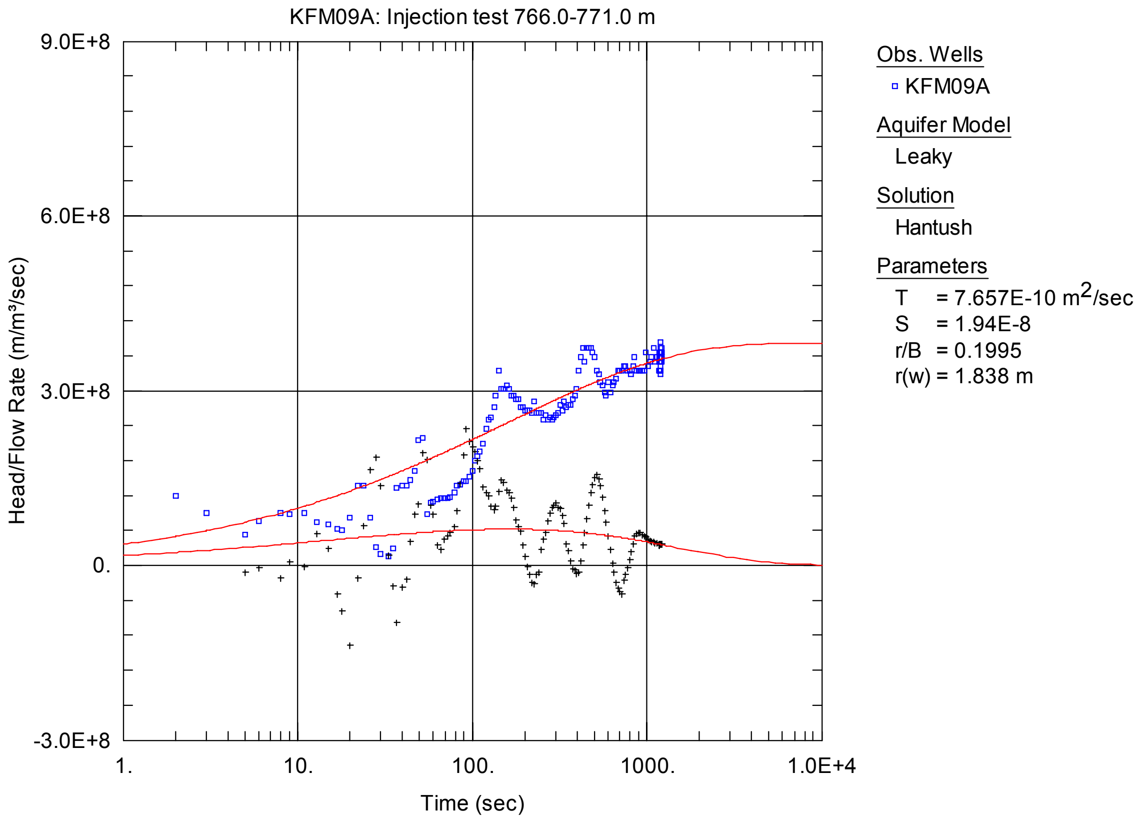


Figure A3-580. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 766.0-771.0 m in KFM09A.*

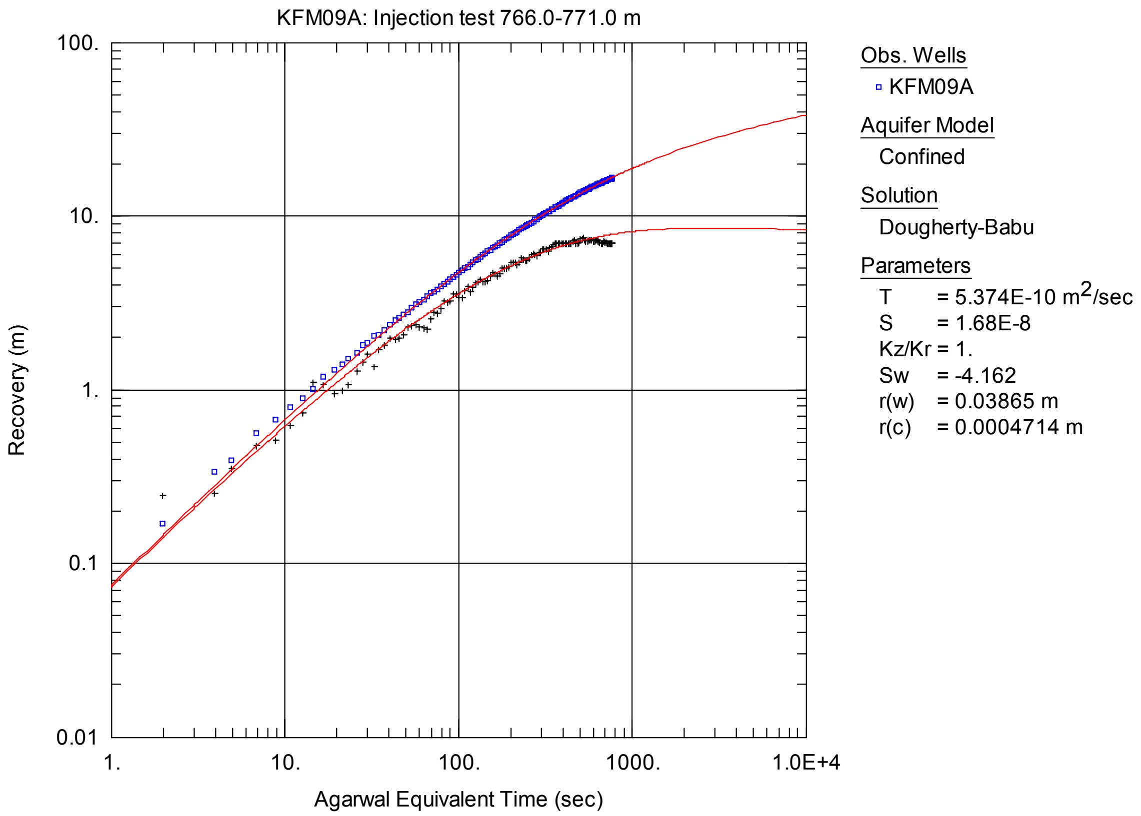


Figure A3-581. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 766.0-771.0 m in KFM09A.*

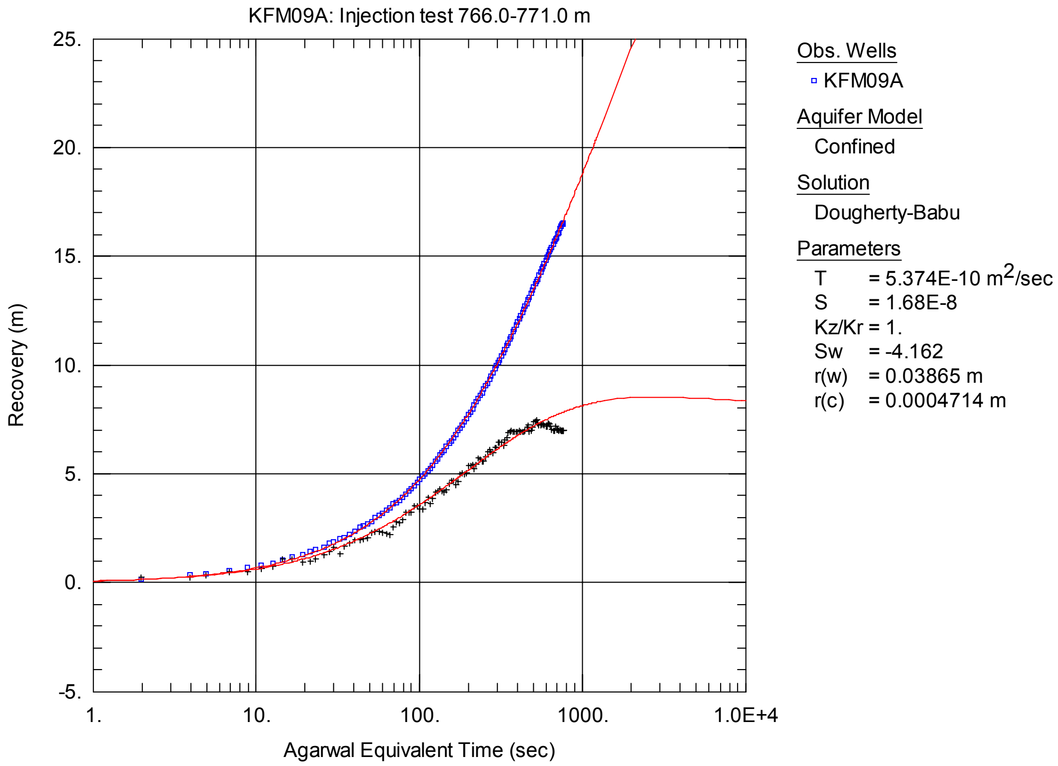


Figure A3-582. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 766.0-771.0 m in KFM09A.*

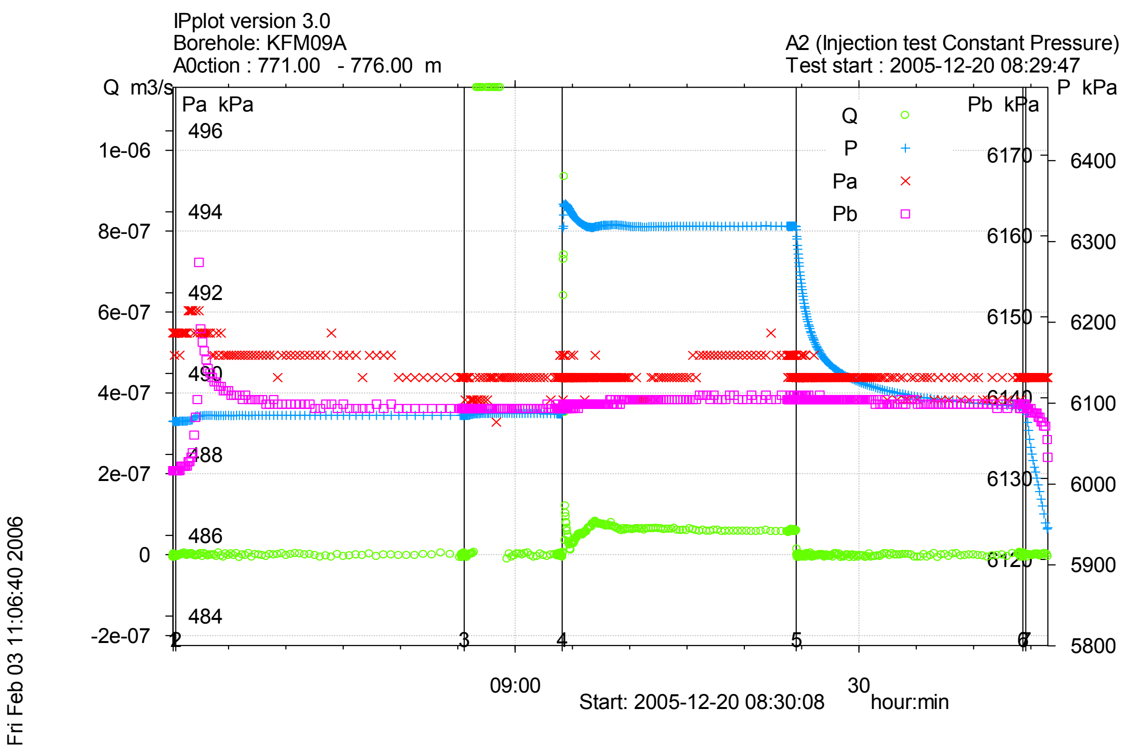


Figure A3-583. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 771.0-776.0 m in borehole KFM09A.*

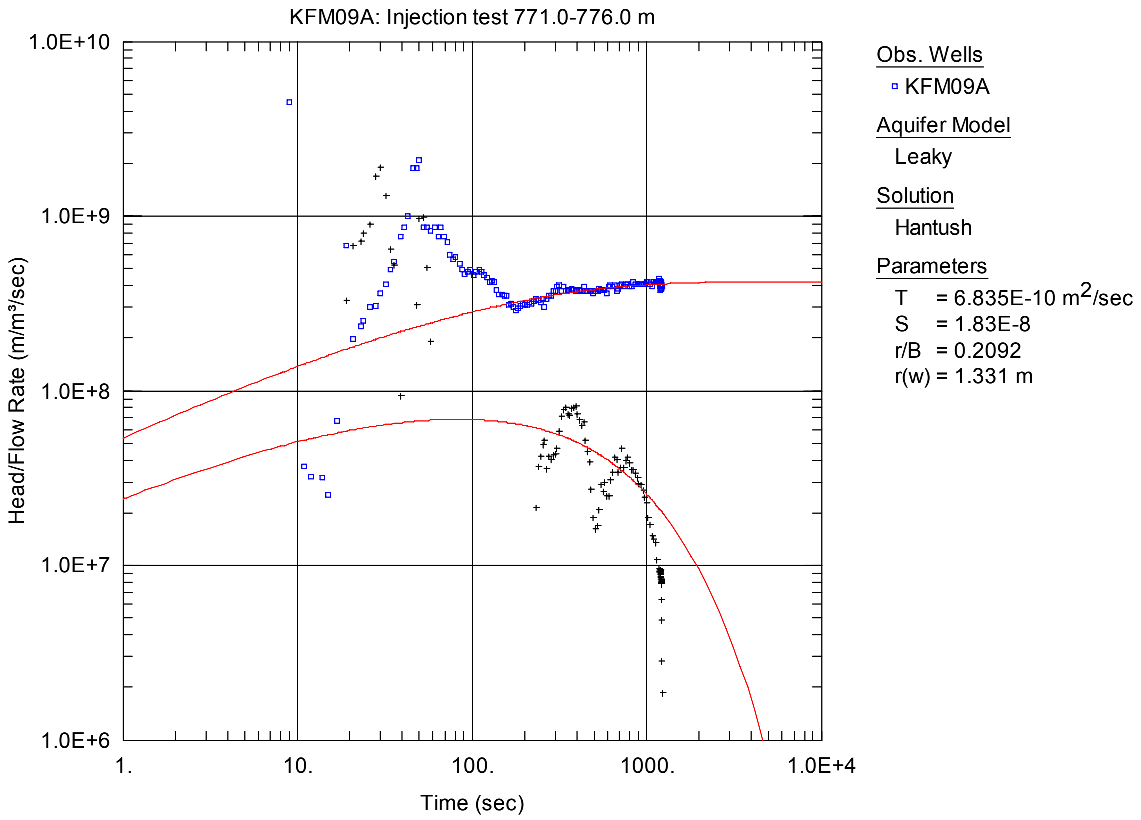


Figure A3-584. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 771.0-776.0 m in KFM09A.*

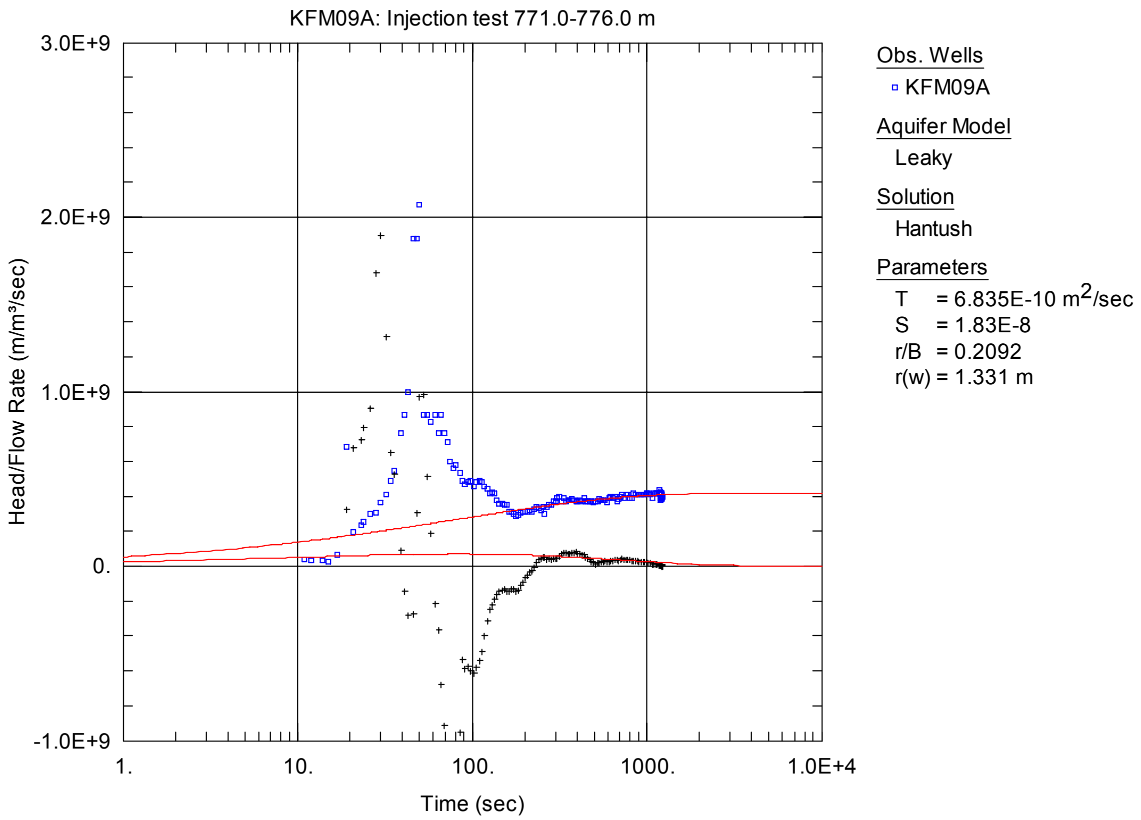


Figure A3-585. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 771.0-776.0 m in KFM09A.*

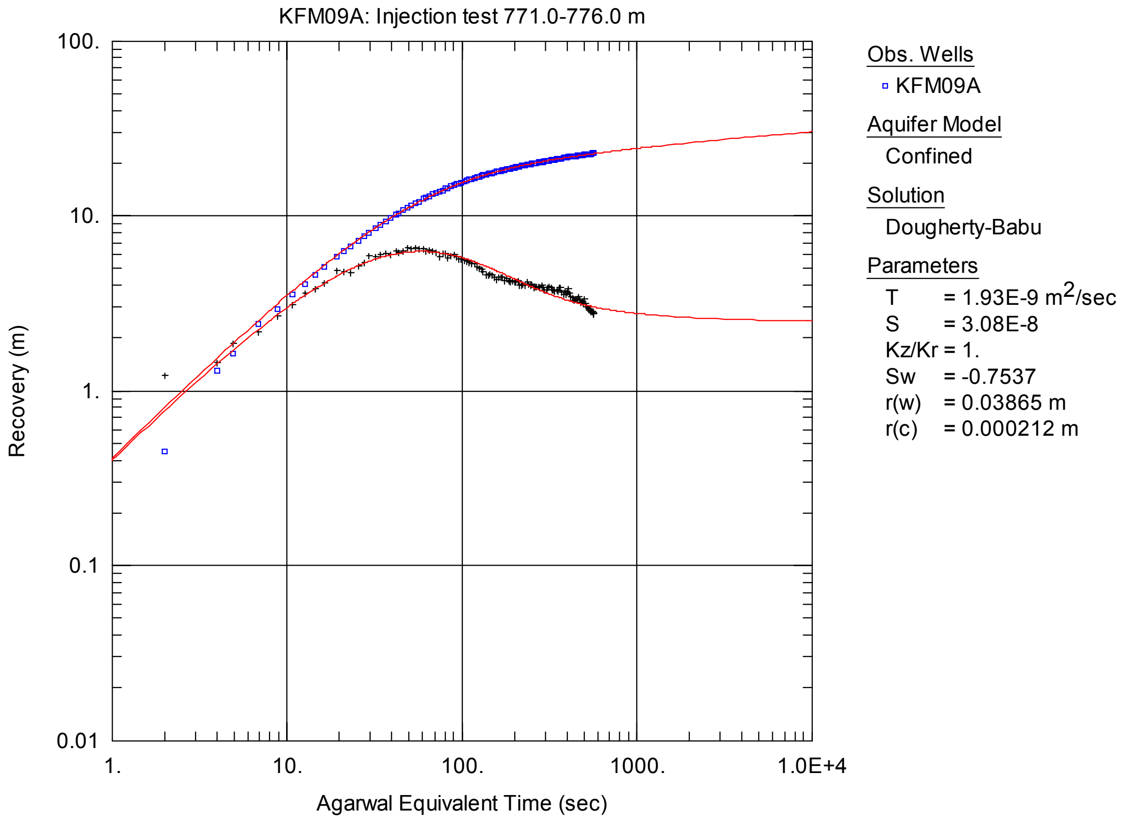


Figure A3-586. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 771.0-776.0 m in KFM09A.*

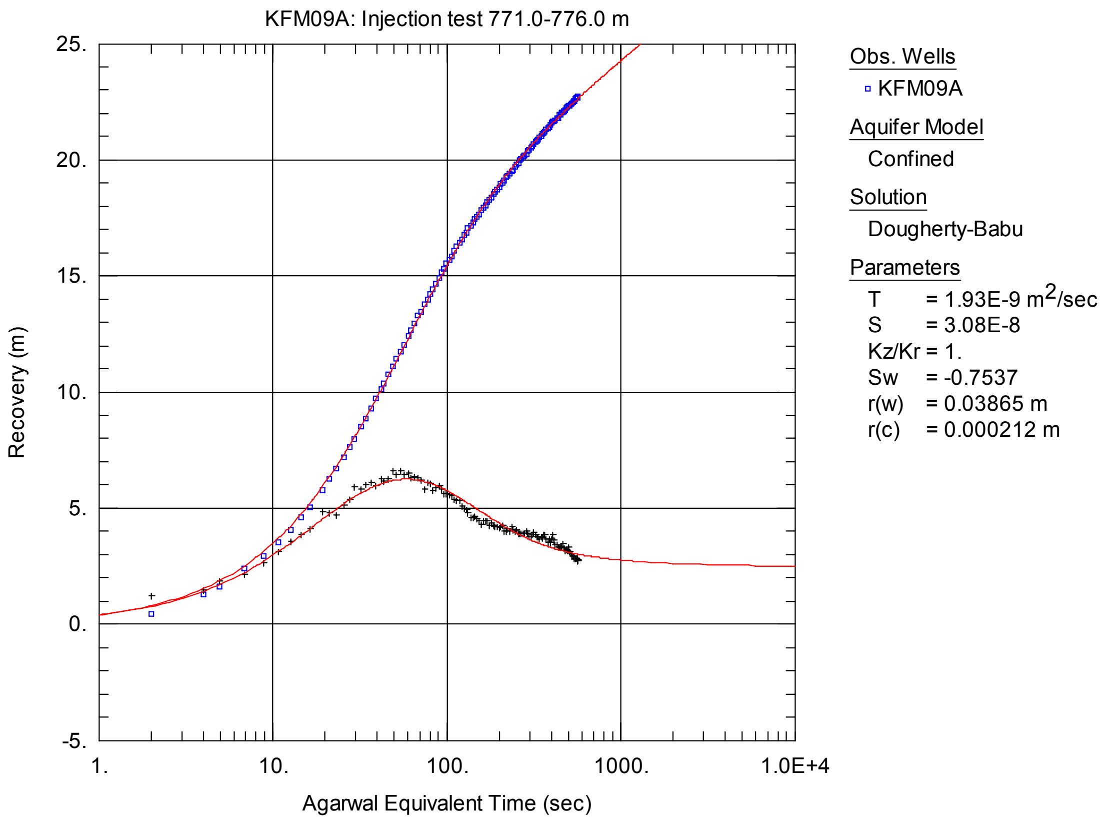


Figure A3-587. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 771.0-776.0 m in KFM09A.*

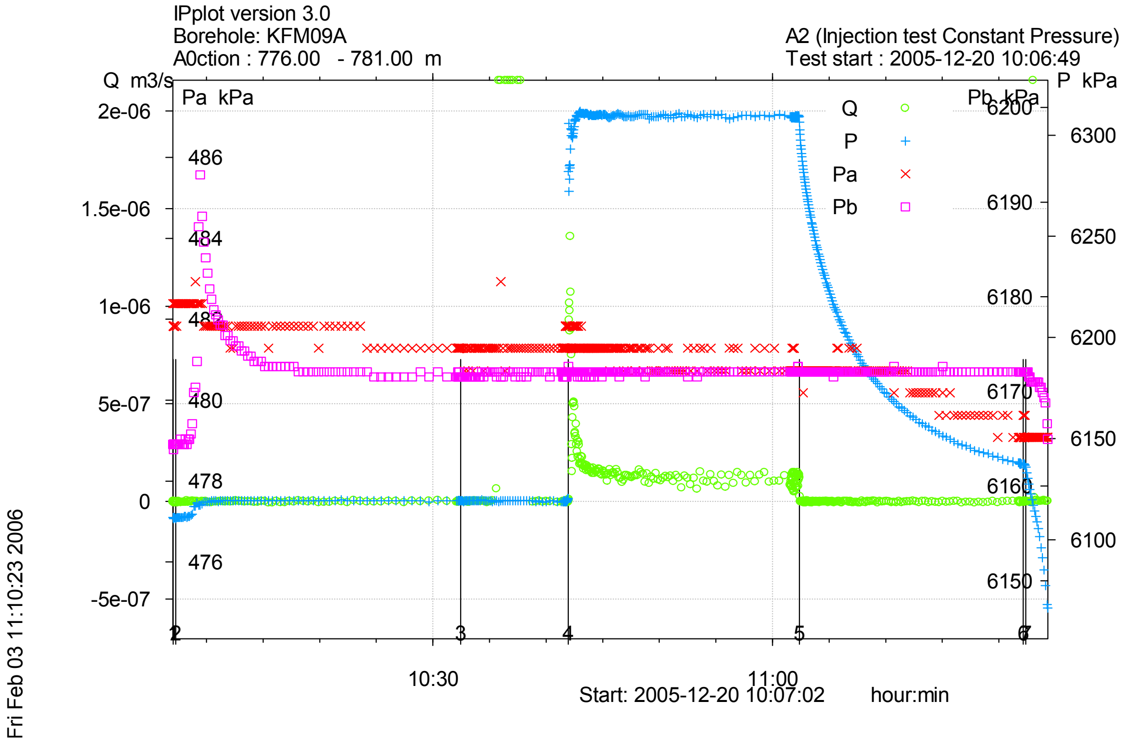


Figure A3-588. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 776.0-781.0 m in borehole KFM09A.*

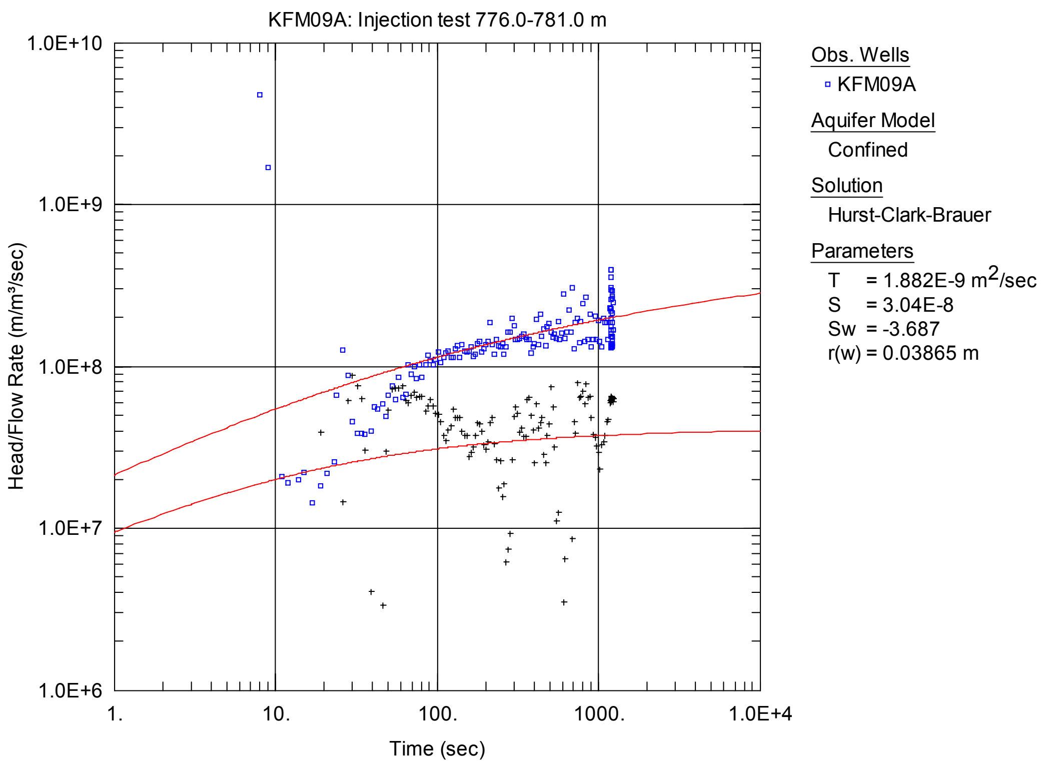


Figure A3-589. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 776.0-781.0 m in KFM09A.*

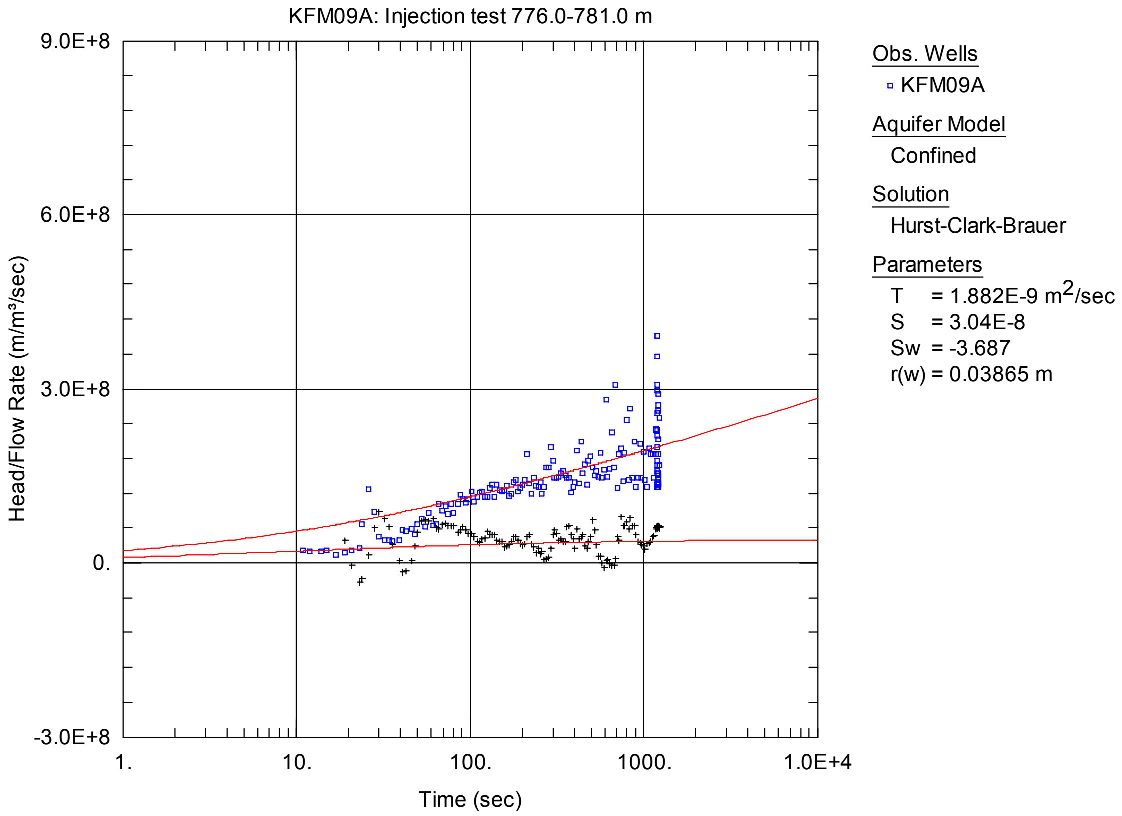


Figure A3-590. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 776.0-781.0 m in KFM09A.*

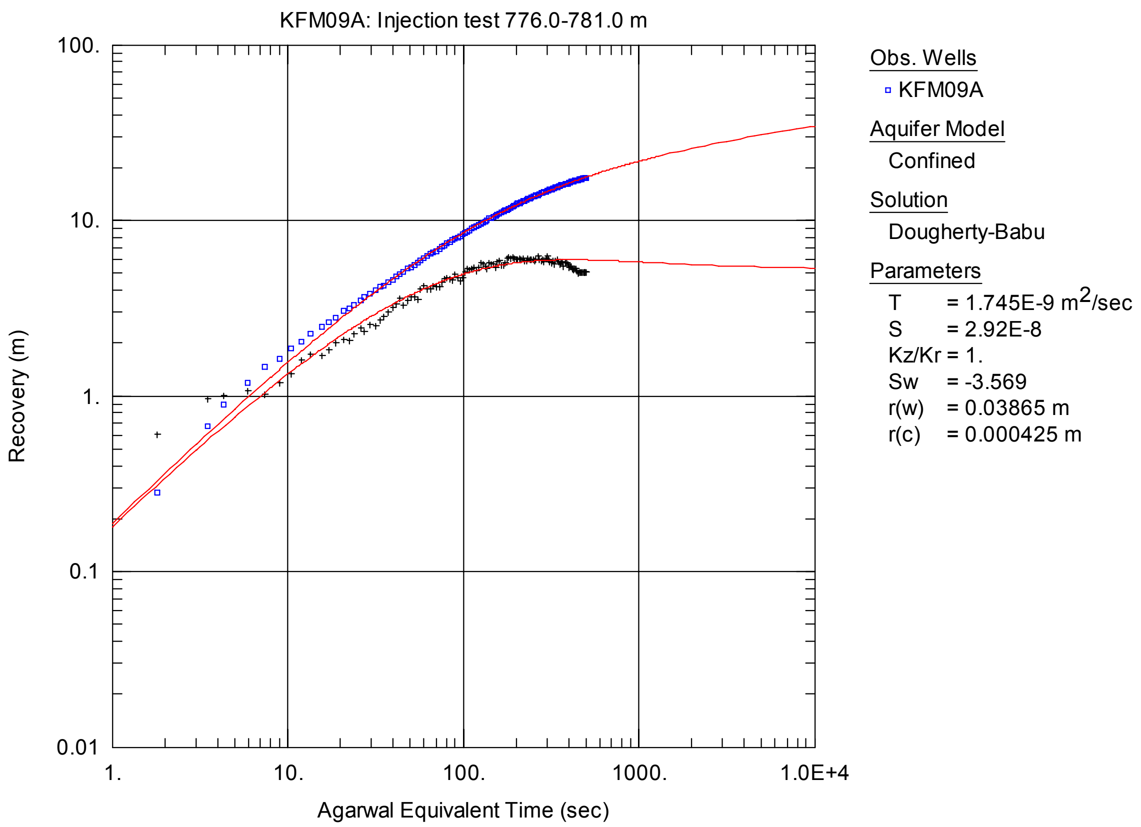


Figure A3-591. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 776.0-781.0 m in KFM09A.*

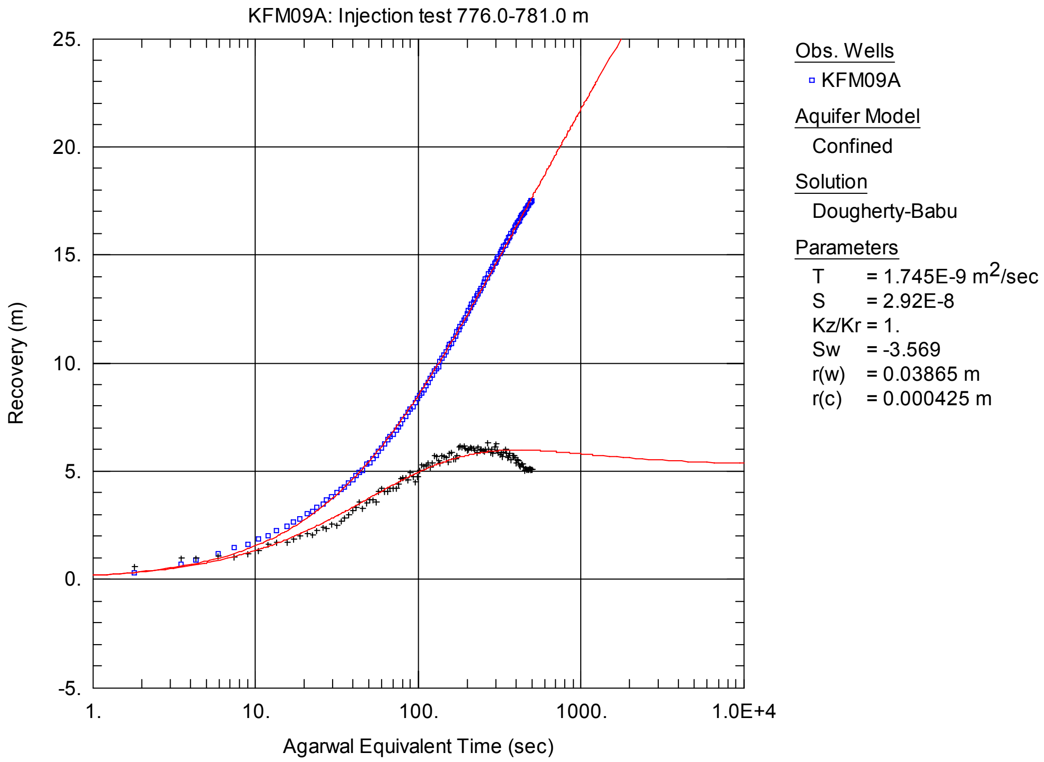


Figure A3-592. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 776.0-781.0 m in KFM09A.*

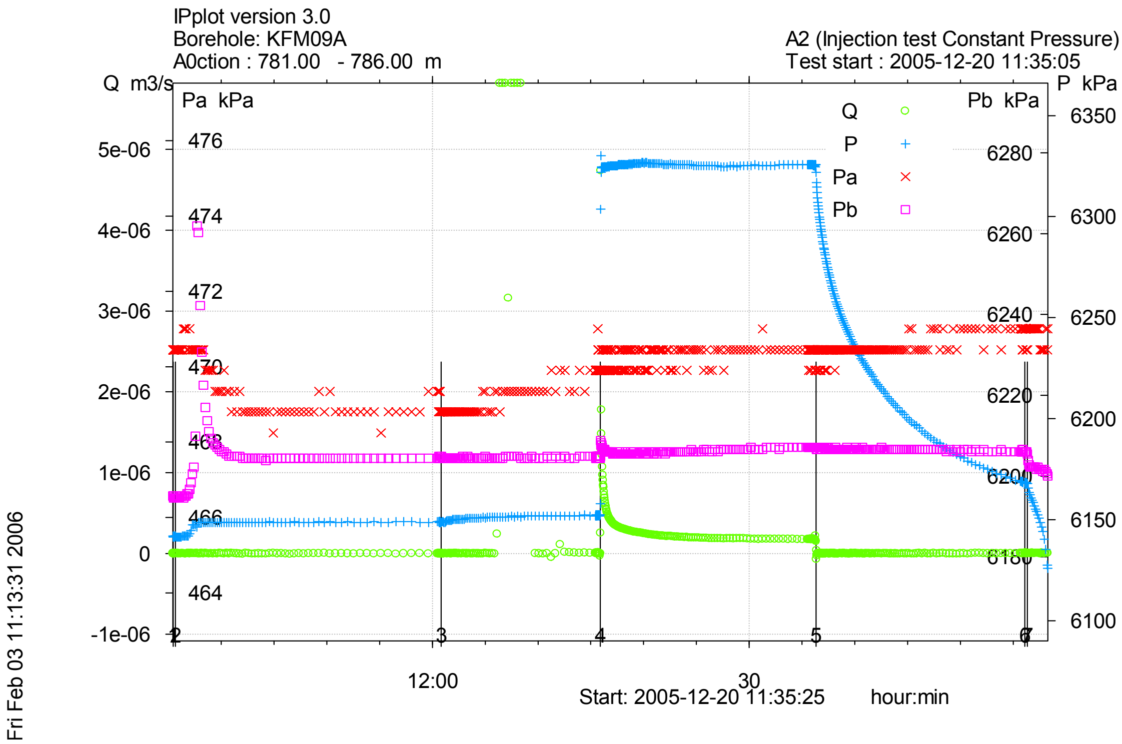


Figure A3-593. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 781.0-786.0 m in borehole KFM09A.*

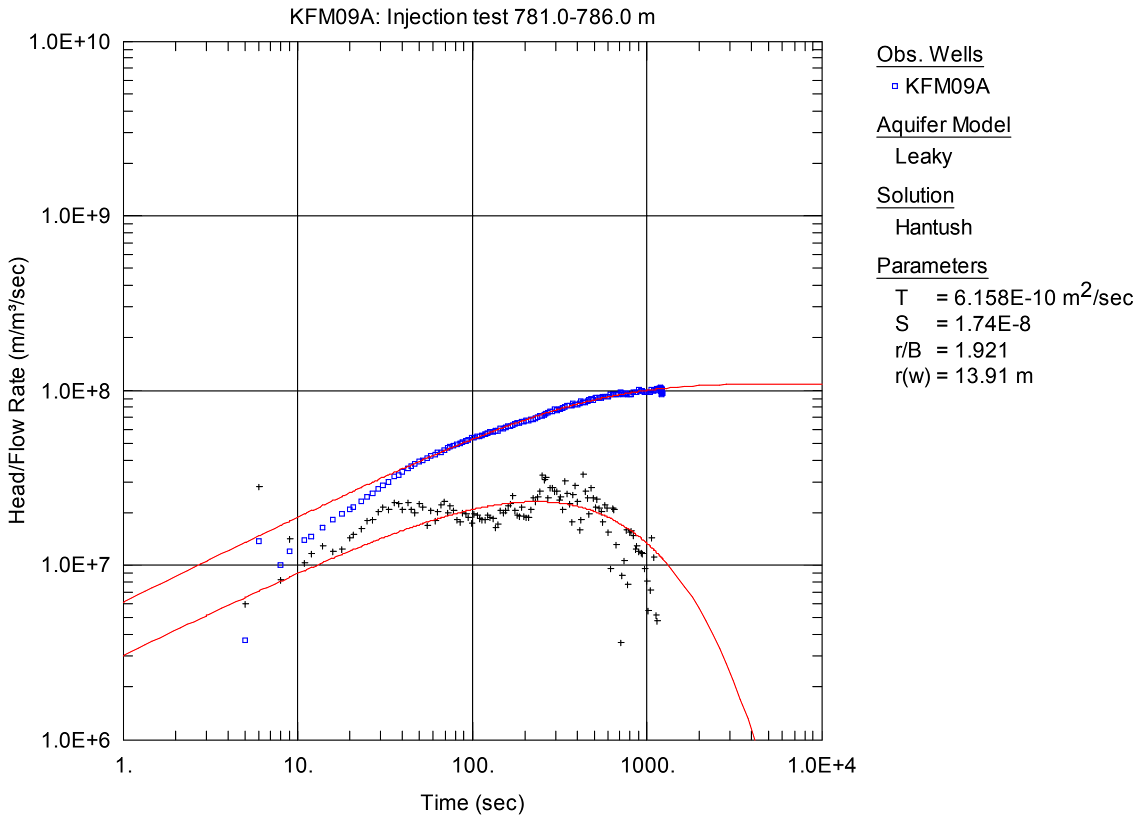


Figure A3-594. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 781.0-786.0 m in KFM09A.*

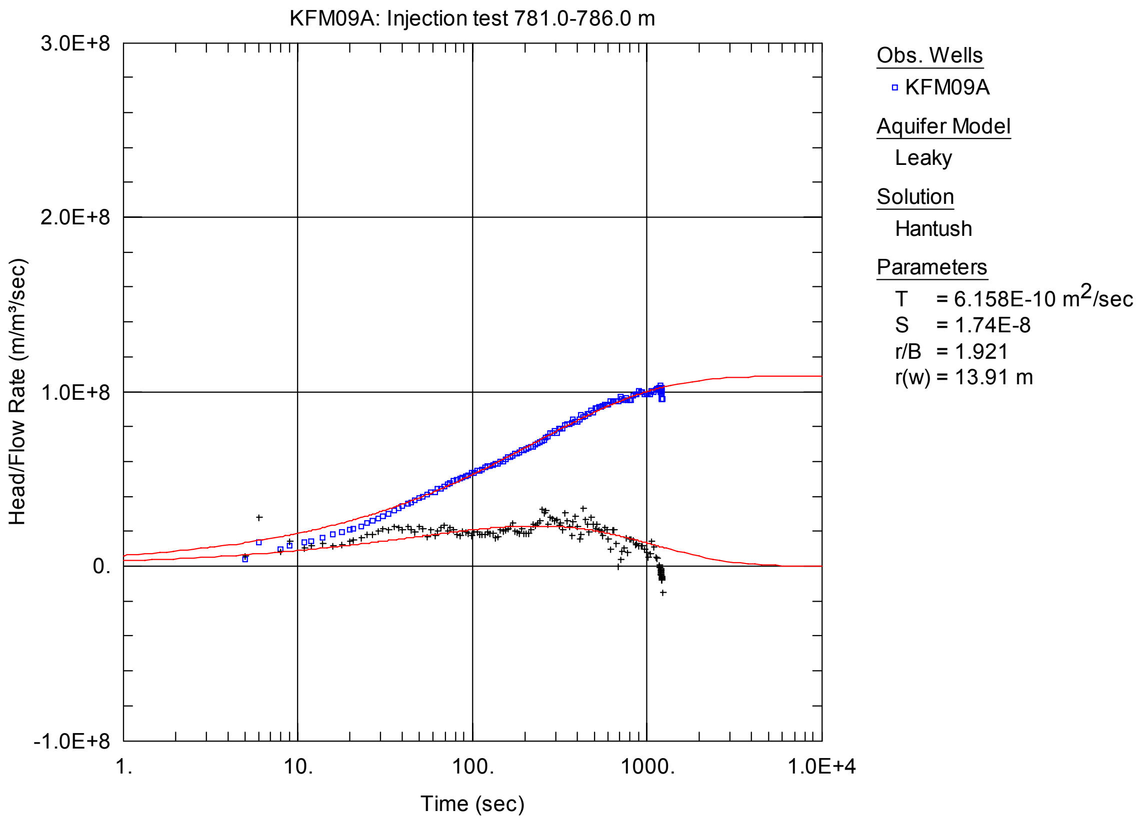


Figure A3-595. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 781.0-786.0 m in KFM09A.*

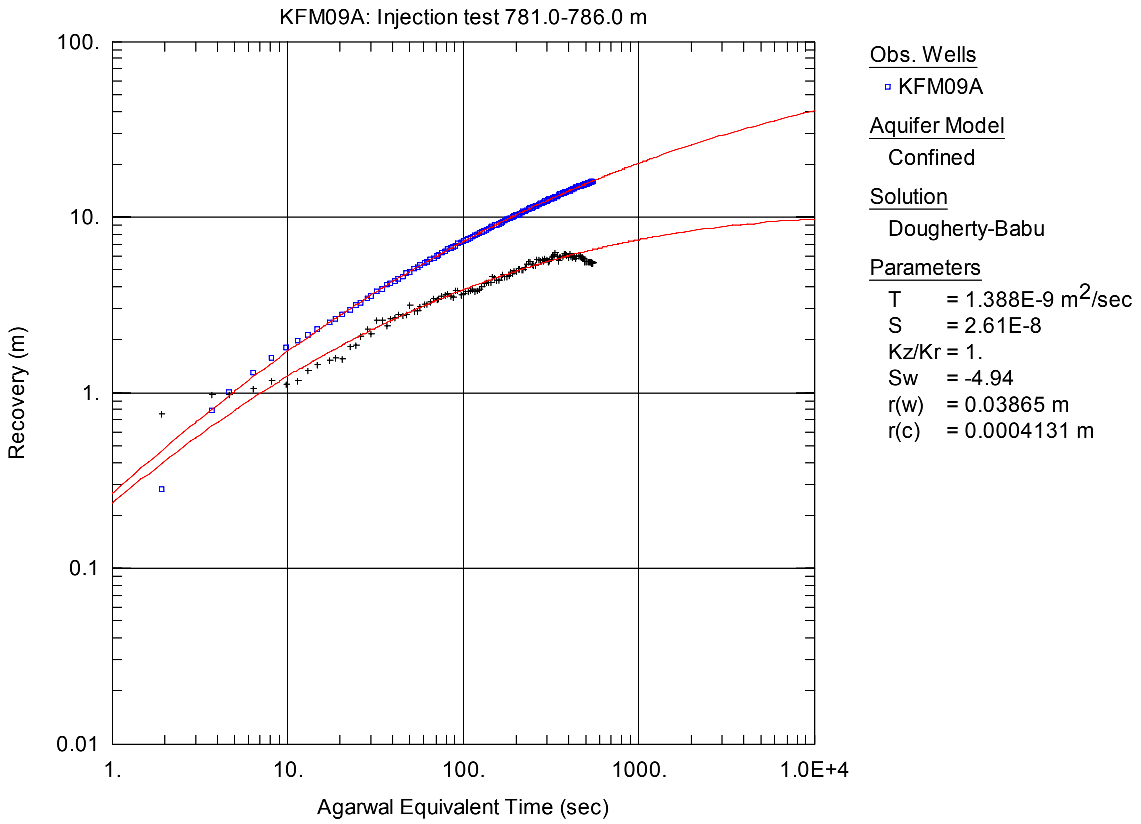


Figure A3-596. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 781.0-786.0 m in KFM09A.*

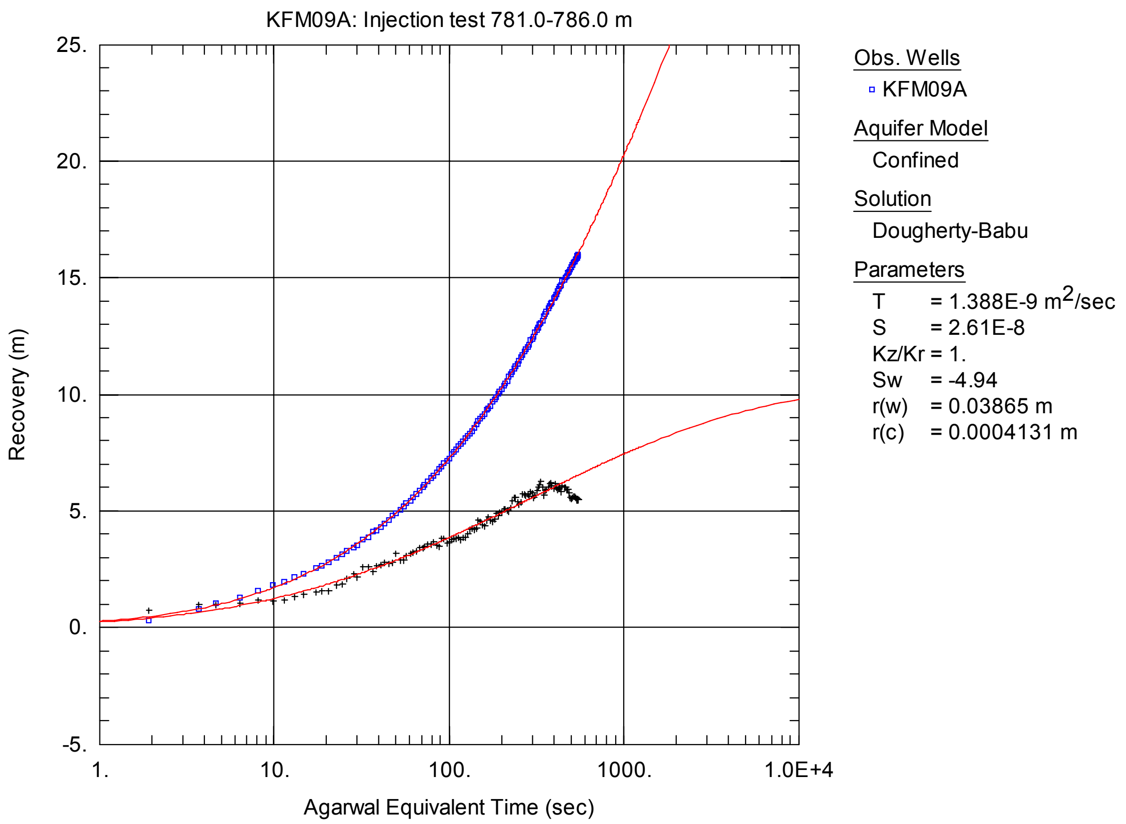


Figure A3-597. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 781.0-786.0 m in KFM09A.*

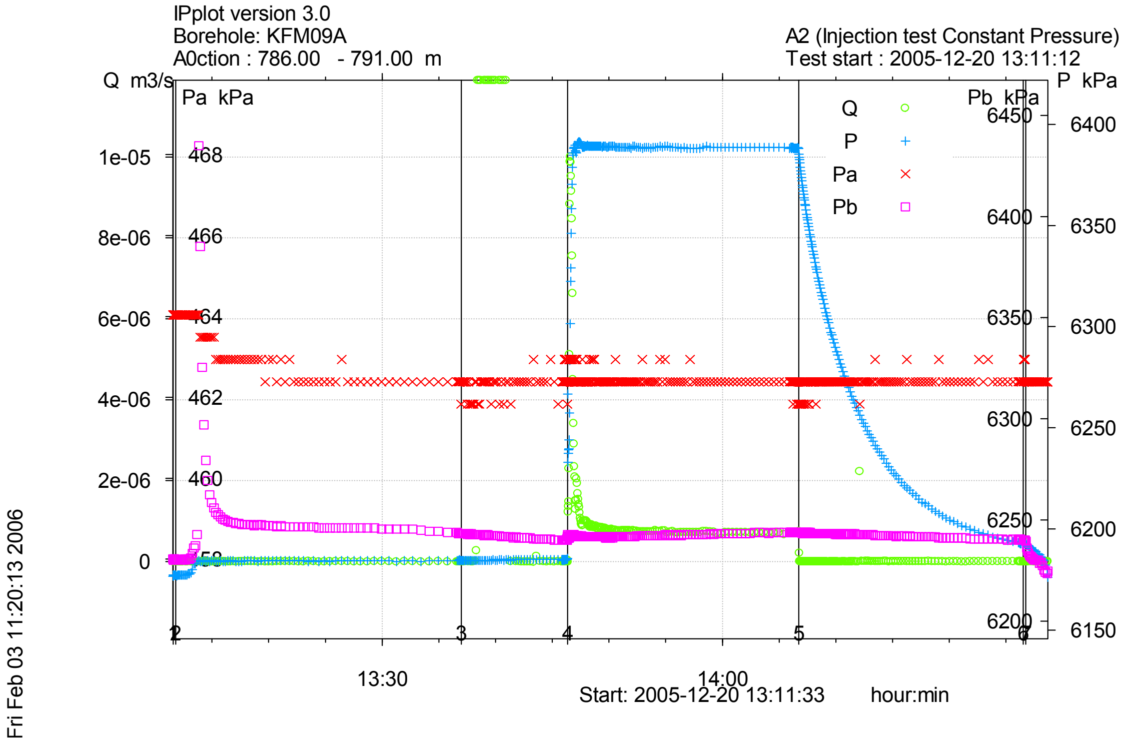


Figure A3-598. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 786.0-791.0 m in borehole KFM09A.

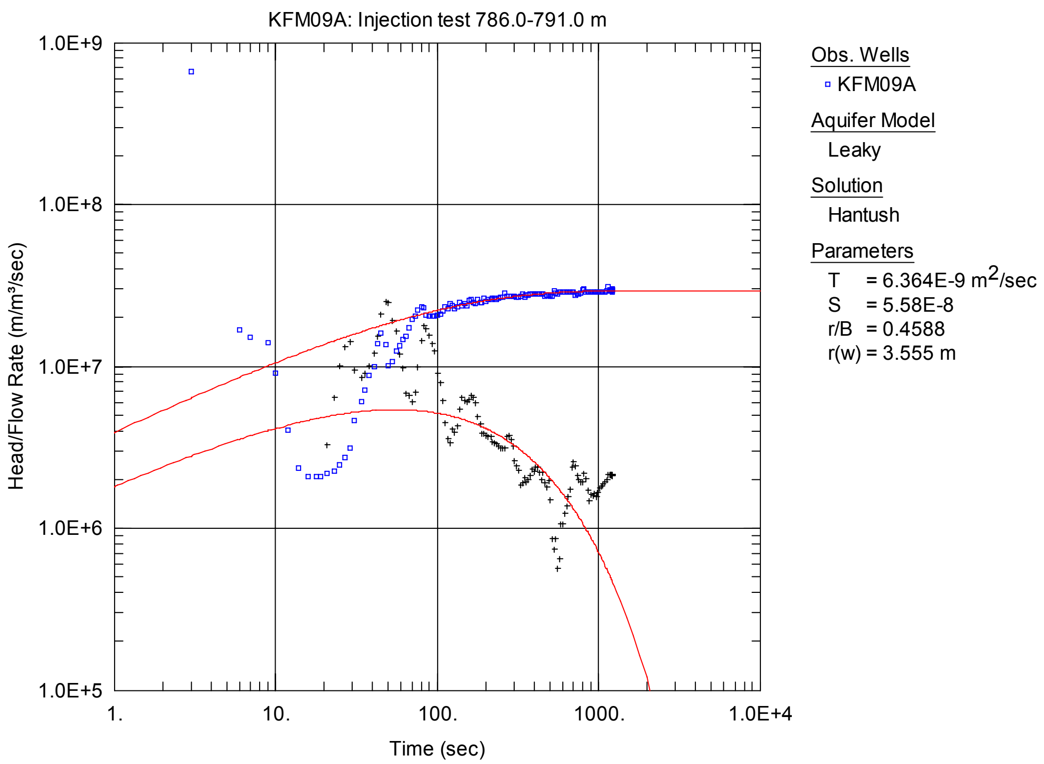


Figure A3-599. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 786.0-791.0 m in KFM09A.

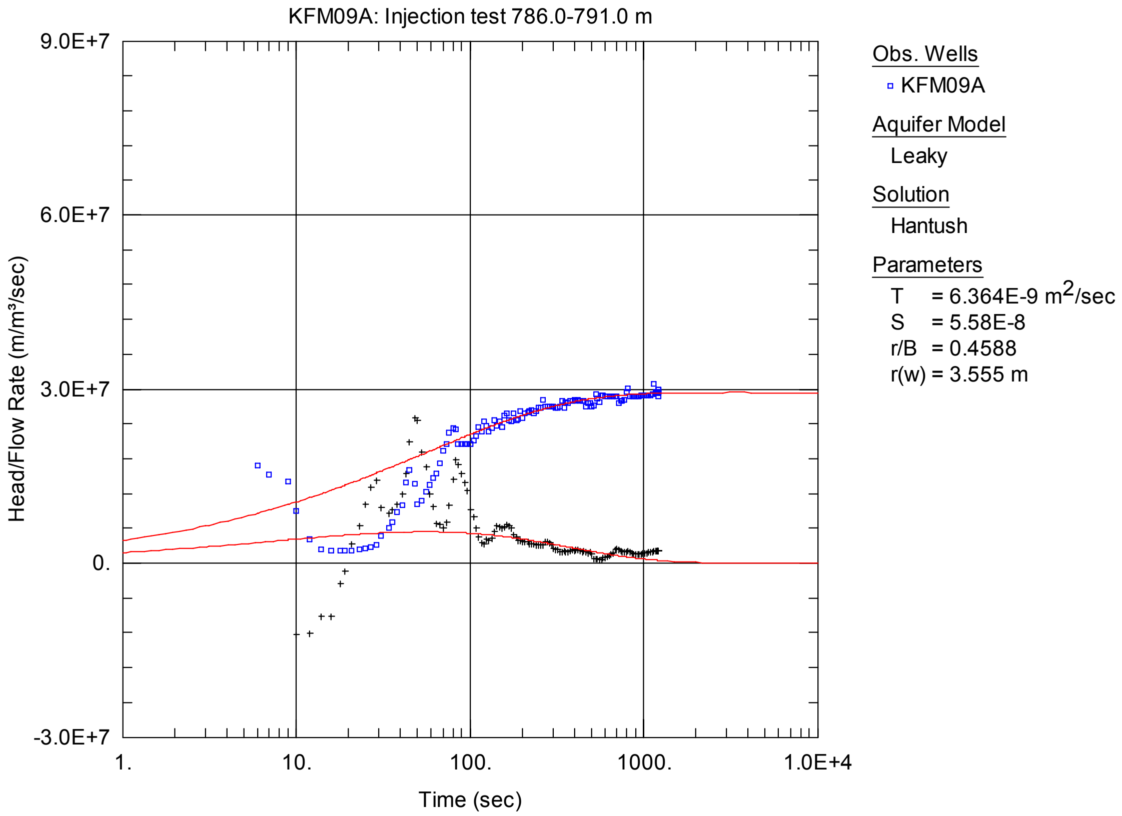


Figure A3-600. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 786.0-791.0 m in KFM09A.*

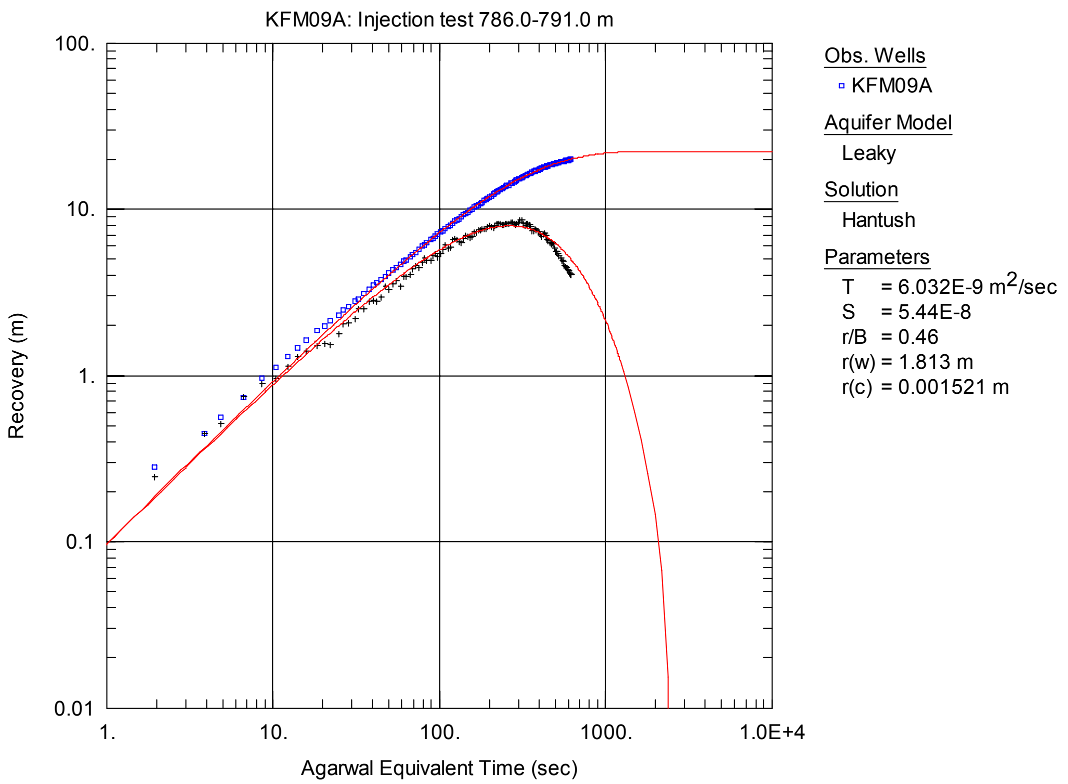


Figure A3-601. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 786.0-791.0 m in KFM09A. This evaluation is made with the Hantush model for a pseudo-spherical response.*

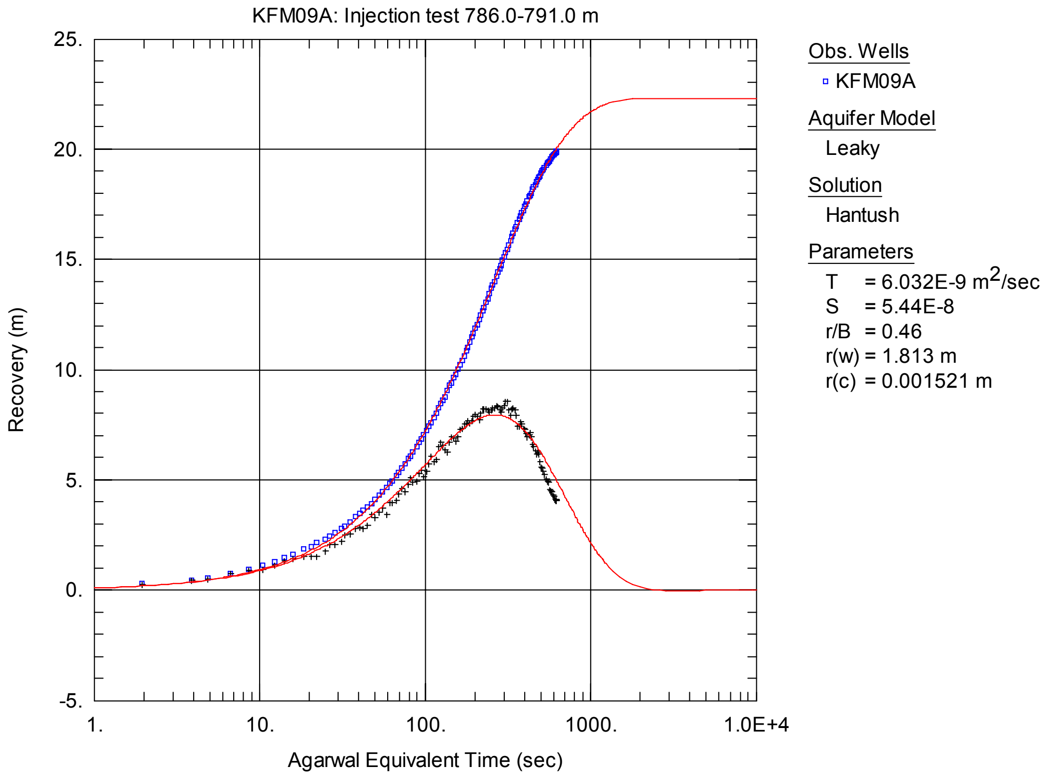


Figure A3-602. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 786.0-791.0 m in KFM09A. This evaluation is made with the Hantush model for a pseudo-spherical response.*

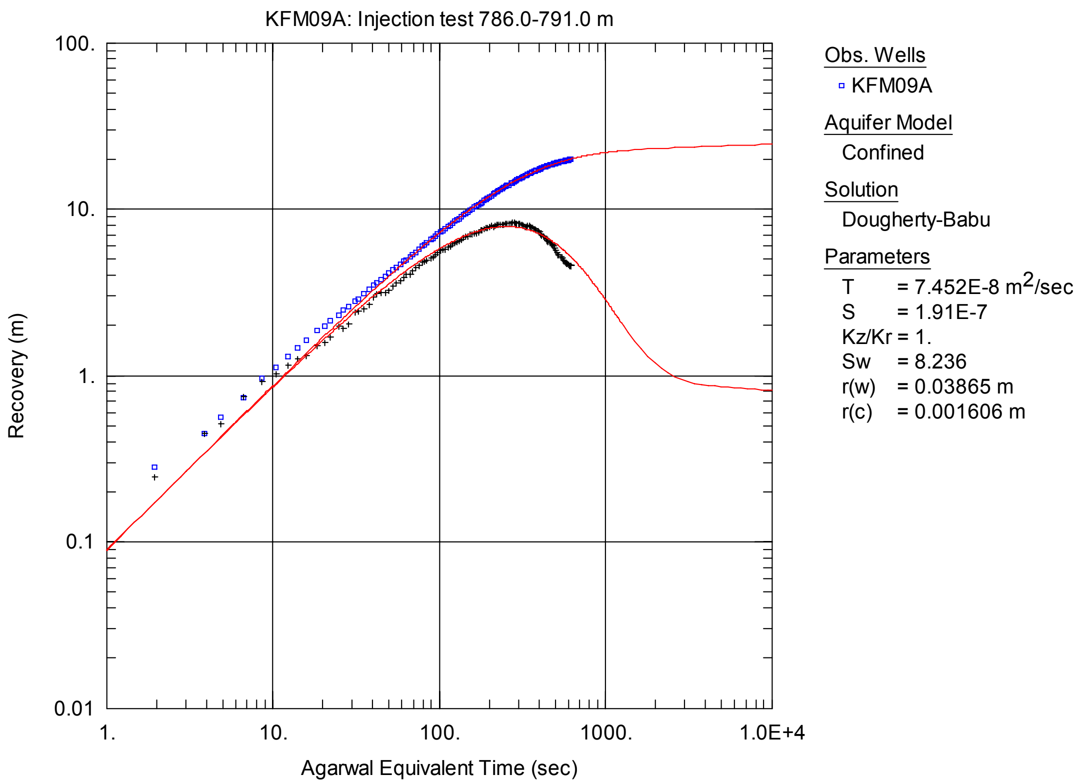


Figure A3-603. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 786.0-791.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

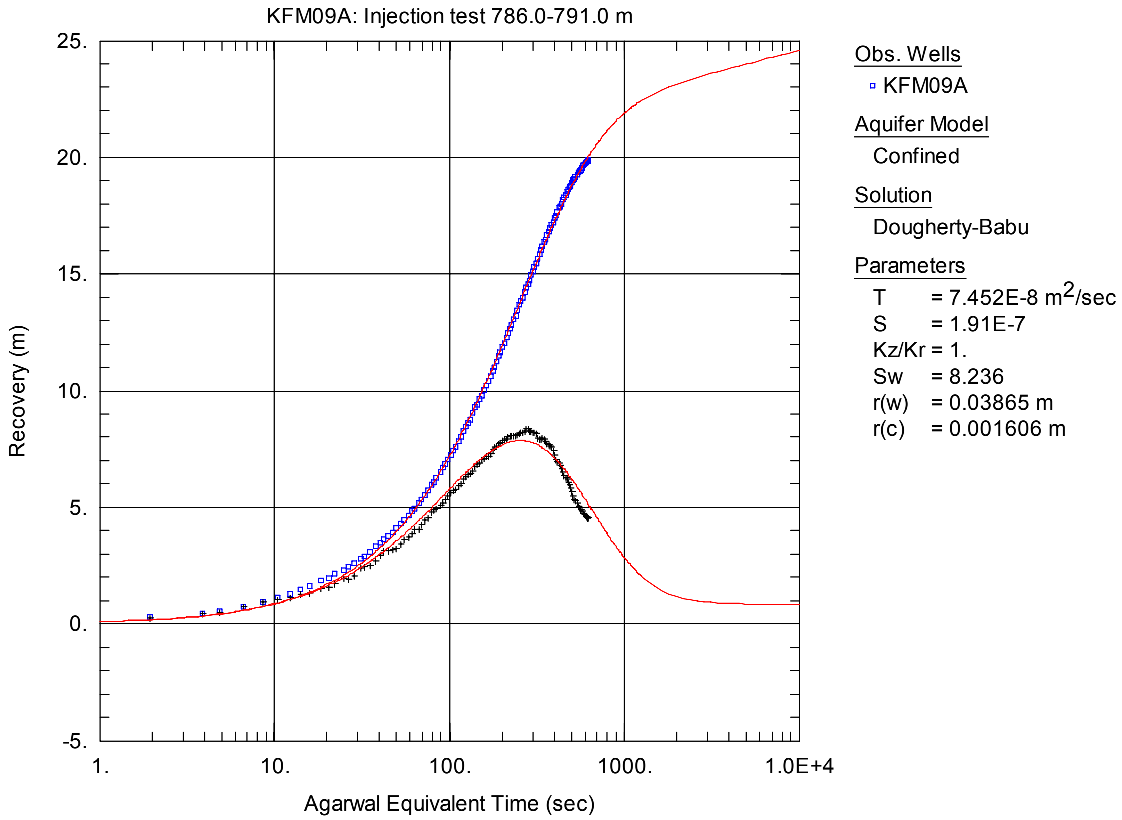
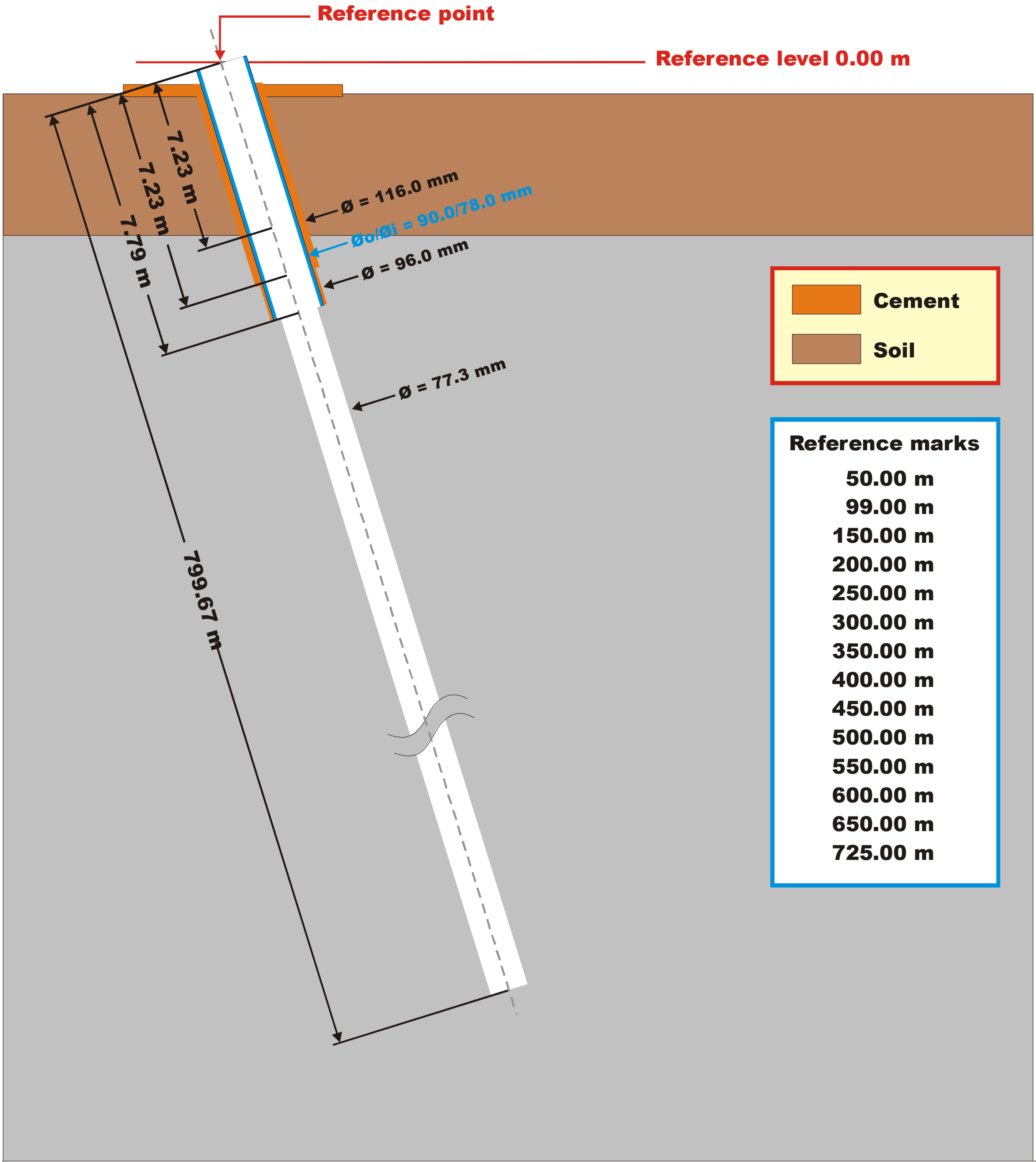


Figure A3-604. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 786.0-791.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

Appendix 4. Borehole technical data

Technical data

Borehole KFM09A



Drilling reference point

Northing: 6700115.04 (m), RT90 2,5 gon V 0:-15
Easting: 1630647.50 (m), RT90 2,5 gon V 0:-15
Elevation: 4.29 (m), RHB 70

Orientation

Bearing: 200.08°
Inclination: -59.46°

Drilling period

Drilling start date: 2005-09-05
Drilling stop date: 2005-10-27

2005-11-09 rev 2

Appendix 5. Sicada tables

Nomenclature plu_s_hole_test_d

Column	Datatype	Unit	Column Description	Alt. Symbol
site	CHAR		Investigation site name	
activity_type	CHAR		Activity type code	
start_date	DATE		Date (yymmdd hh:mm:ss)	
stop_date	DATE		Date (yymmdd hh:mm:ss)	
project	CHAR		project code	
idcode	CHAR		Object or borehole identification code	
secup	FLOAT	m	Upper section limit (m)	
seclow	FLOAT	m	Lower section limit (m)	
section_no	INTEGER	number	Section number	
test_type	CHAR		Test type code (1-7), see table description	
formation_type	CHAR		1: Rock, 2: Soil (superficial deposits)	
start_flow_period	DATE	yyyymmdd	Date & time of pumping/injection start (YYYY-MM-DD hh:mm:ss)	
stop_flow_period	DATE	yyyymmdd	Date & time of pumping/injection stop (YYYY-MM-DD hh:mm:ss)	
flow_rate_end_qp	FLOAT	m**3/s	Flow rate at the end of the flowing period	
value_type_qp	CHAR		0:true value,-1<lower meas.limit1:>upper meas.limit	
mean_flow_rate_qm	FLOAT	m**3/s	Arithmetic mean flow rate during flow period	
q_measl__l	FLOAT	m**3/s	Estimated lower measurement limit of flow rate	**Q-measl-L**
q_measl__u	FLOAT	m**3/s	Estimated upper measurement limit of flow rate	Q-measl-U
tot_volume_vp	FLOAT	m**3	Total volume of pumped or injected water	
dur_flow_phase_tp	FLOAT	s	Duration of the flowing period of the test	
dur_rec_phase_tf	FLOAT	s	Duration of the recovery period of the test	
initial_head_hi	FLOAT	m	Hydraulic head in test section at start of the flow period	
head_at_flow_end_hp	FLOAT	m	Hydraulic head in test section at stop of the flow period.	
final_head_hf	FLOAT	m	Hydraulic head in test section at stop of recovery period.	
initial_press_pi	FLOAT	kPa	Groundwater pressure in test section at start of flow period	
press_at_flow_end_pp	FLOAT	kPa	Groundwater pressure in test section at stop of flow period.	
final_press_pf	FLOAT	kPa	Ground water pressure at the end of the recovery period.	
fluid_temp_tew	FLOAT	oC	Measured section fluid temperature, see table description	
fluid_elcond_ecw	FLOAT	mS/m	Measured section fluid el. conductivity,see table descr.	
fluid_salinity_tdsw	FLOAT	mg/l	Total salinity of section fluid based on EC,see table descr.	
fluid_salinity_tdswm	FLOAT	mg/l	Tot. section fluid salinity based on water sampling,see...	
reference	CHAR		SKB report No for reports describing data and evaluation	
comments	VARCHAR		Short comment to data	
error_flag	CHAR		If error_flag = "*" then an error occured and an error	
in_use	CHAR		If in_use = "*" then the activity has been selected as	
sign	CHAR		Signature for QA data accknowledge (QA - OK)	
lp	FLOAT	m	Hydraulic point of application	

Nomenclature plu_s_hole_test_ed1

Column	Datatype	Unit	Column Description	Alt. Symbol
site	CHAR		Investigation site name	
activity_type	CHAR		Activity type code	
start_date	DATE		Date (yymmdd hh:mm:ss)	
stop_date	DATE		Date (yymmdd hh:mm:ss)	
project	CHAR		project code	

Column	Datatype	Unit	Column Description	Alt. Symbol
idcode	CHAR		Object or borehole identification code	
secup	FLOAT	m	Upper section limit (m)	
seclow	FLOAT	m	Lower section limit (m)	
section_no	INTEGER	number	Section number	
test_type	CHAR		Test type code (1-7), see table description!	
formation_type	CHAR		Formation type code. 1: Rock, 2: Soil (superficial deposits)	
lp	FLOAT	m	Hydraulic point of application for test section, see descr.	
seclen_class	FLOAT	m	Planned ordinary test interval during test campaign.	
spec_capacity_q_s	FLOAT	m**2/s	Specific capacity (Q/s) of test section, see table descript.	Q/s
value_type_q_s	CHAR		0:true value,-1:Q/s<lower meas.limit,1:Q/s>upper meas.limit	
transmissivity_tq	FLOAT	m**2/s	Tranmissivity based on Q/s, see table description	
value_type_tq	CHAR		0:true value,-1:TQ<lower meas.limit,1:TQ>upper meas.limit.	
bc_tq	CHAR		Best choice code. 1 means TQ is best choice of T, else 0	
transmissivity_moye	FLOAT	m**2/s	Transmissivity,TM, based on Moye (1967)	T_M
bc_tm	CHAR		Best choice code. 1 means Tmoye is best choice of T, else 0	
value_type_tm	CHAR		0:true value,-1:TM<lower meas.limit,1:TM>upper meas.limit.	
hydr_cond_moye	FLOAT	m/s	K_M: Hydraulic conductivity based on Moye (1967)	K_M
formation_width_b	FLOAT	m	b:Aquifer thickness repr. for T(generally b=Lw) ,see descr.	b
width_of_channel_b	FLOAT	m	B:Inferred width of formation for evaluated TB	
tb	FLOAT	m**3/s	TB:Flow capacity in 1D formation of T & width B, see descr.	
l_measl_tb	FLOAT	m**3/s	Estimated lower meas. limit for evaluated TB,see description	
u_measl_tb	FLOAT	m**3/s	Estimated upper meas. limit of evaluated TB,see description	
sb	FLOAT	m	SB:S=storativity,B=width of formation,1D model,see descript.	
assumed_sb	FLOAT	m	SB* : Assumed SB,S=storativity,B=width of formation,see...	
leakage_factor_lf	FLOAT	m	Lf:1D model for evaluation of Leakage factor	
transmissivity_tt	FLOAT	m**2/s	TT:Transmissivity of formation, 2D radial flow model,see...	T_T
value_type_tt	CHAR		0:true value,-1:TT<lower meas.limit,1:TT>upper meas.limit,	
bc_tt	CHAR		Best choice code. 1 means TT is best choice of T, else 0	
l_measl_q_s	FLOAT	m**2/s	Estimated lower meas. limit for evaluated TT,see table descr	Q/s-measl-L
u_measl_q_s	FLOAT	m**2/s	Estimated upper meas. limit for evaluated TT,see description	Q/s-measl-U
storativity_s	FLOAT		S:Storativity of formation based on 2D rad flow,see descr.	
assumed_s	FLOAT		Assumed Storativity,2D model evaluation,see table descr.	
bc_s	FLOAT		Best choice of S (Storativity) ,see descr.	
ri	FLOAT	m	Radius of influence	
ri_index	CHAR		ri index=index of radius of influence :-1,0 or 1, see descr.	
leakage_coeff	FLOAT	1/s	K'/b':2D rad flow model evaluation of leakage coeff,see desc	
hydr_cond_ksf	FLOAT	m/s	Ksf:3D model evaluation of hydraulic conductivity,see desc.	
value_type_ksf	CHAR		0:true value,-1:Ksf<lower meas.limit,1:Ksf>upper meas.limit,	
l_measl_ksf	FLOAT	m/s	Estimated lower meas.limit for evaluated Ksf,see table desc.	
u_measl_ksf	FLOAT	m/s	Estimated upper meas.limit for evaluated Ksf,see table descr	
spec_storage_ssf	FLOAT	1/m	Ssf:Specific storage,3D model evaluation,see table descr.	
assumed_ssf	FLOAT	1/m	Ssf*:Assumed Spec.storage,3D model evaluation,see table des.	
c	FLOAT	m**3/pa	C: Wellbore storage coefficient; flow or recovery period	C
cd	FLOAT		CD: Dimensionless wellbore storage coefficient	
skin	FLOAT		Skin factor;best estimate of flow/recovery period,see descr.	ξ
dt1	FLOAT	s	Estimated start time of evaluation, see table description	
dt2	FLOAT	s	Estimated stop time of evaluation. see table description	
t1	FLOAT	s	Start time for evaluated parameter from start flow period	t_1
t2	FLOAT	s	Stop time for evaluated parameter from start of flow period	t_2
dte1	FLOAT	s	Start time for evaluated parameter from start of recovery	dte_1
dte2	FLOAT	s	Stop time for evaluated parameter from start of recovery	dte_2
p_horner	FLOAT	kPa	p*:Horner extrapolated pressure, see table description	
transmissivity_t_nlr	FLOAT	m**2/s	T_NLR Transmissivity based on None Linear Regression...	

Column	Datatype	Unit	Column Description	Alt. Symbol
storativity_s_nlr	FLOAT		S_NLR=storativity based on None Linear Regression,see..	
value_type_t_nlr	CHAR		0:true value,-1:T_NLR<lower meas.limit,1:>upper meas.limit	
bc_t_nlr	CHAR		Best choice code. 1 means T_NLR is best choice of T, else 0	
c_nlr	FLOAT	m**3/pa	Wellbore storage coefficient, based on NLR, see descr.	
cd_nlr	FLOAT		Dimensionless wellbore storage constant, see table descrip.	
skin_nlr	FLOAT		Skin factor based on Non Linear Regression,see desc.	
transmissivity_t_grf	FLOAT	m**2/s	T_GRF:Transmissivity based on Genelized Radial Flow,see...	
value_type_t_grf	CHAR		0:true value,-1:T_GRF<lower meas.limit,1:>upper meas.limit	
bc_t_grf	CHAR		Best choice code. 1 means T_GRF is best choice of T, else 0	
storativity_s_grf	FLOAT		S_GRF:Storativity based on Generalized Radial Flow, see des.	
flow_dim_grf	FLOAT		Inferred flow dimesion based on Generalized Rad. Flow model	
comment	VARCHAR	no_unit	Short comment to the evaluated parameters	
error_flag	CHAR		If error_flag = "*" then an error occured and an error	
in_use	CHAR		If in_use = "*" then the activity has been selected as	
sign	CHAR		Signature for QA data accknowledge (QA - OK)	

Nomenclature plu_s_hole_test_obs

Column	Datatype	Unit	Column Description
site	CHAR		Investigation site name
activity_type	CHAR		Activity type code
idcode	CHAR		Object or borehole identification code
start_date	DATE		Date (yymmdd hh:mm:ss)
secup	FLOAT	m	Upper section limit (m)
seclow	FLOAT	m	Lower section limit (m)
obs_secup	FLOAT	m	Upper limit of observation section
obs_seclow	FLOAT	m	Lower limit of observation section
pi_above	FLOAT	kPa	Groundwater pressure above test section,start of flow period
pp_above	FLOAT	kPa	Groundwater pressure above test section,at stop flow period
pf_above	FLOAT	kPa	Groundwater pressure above test section at stop recovery per
pi_below	FLOAT	kPa	Groundwater pressure below test section at start flow period
pp_below	FLOAT	kPa	Groundwater pressure below test section at stop flow period
pf_below	FLOAT	kPa	Groundwater pressure below test section at stop recovery per
comments	VARCHAR		Comment text row (unformatted text)

KFM09A plu_s_hole_test_d. Left (This result table to SICADA includes more columns which are empty, these columns are not presented here.)

idcode	start_date	stop_date	secup	seclow	test_type	Formation_type	start_flow_period	stop_flow_period	flow_rate_end_qp	Value_type_qp	mean_flow_rate_qm
KFM09A	20051117 16:09	20051117 17:59	106.00	206.00	3	1	20051117 16:57:06	20051117 17:27:25	7.07E-05	0	9.33E-05
KFM09A	20051117 19:03	20051117 20:53	206.00	306.00	3	1	20051117 19:50:48	20051117 20:21:10	1.31E-06	0	1.62E-06
KFM09A	20051117 21:47	20051117 23:36	306.00	406.00	3	1	20051117 22:34:02	20051117 23:04:29	4.06E-06	0	7.19E-06
KFM09A	20051118 09:59	20051118 11:49	406.00	506.00	3	1	20051118 10:46:49	20051118 11:17:10	1.07E-05	0	3.77E-05
KFM09A	20051121 12:52	20051121 15:13	506.00	606.00	3	1	20051121 14:11:02	20051121 14:41:23	1.94E-06	0	8.12E-06
KFM09A	20051121 06:14	20051121 08:03	606.00	706.00	3	1	20051121 07:00:34	20051121 07:30:54	5.72E-07	0	8.03E-07
KFM09A	20051121 08:51	20051121 10:40	691.00	791.00	3	1	20051121 09:37:30	20051121 10:07:51	8.41E-07	0	1.23E-06
KFM09A	20051128 16:44	20051128 18:19	106.00	126.00	3	1	20051128 17:36:29	20051128 17:56:45	8.47E-06	0	9.98E-06
KFM09A	20051129 06:29	20051129 07:43	126.00	146.00	3	1	20051129 07:01:05	20051129 07:21:21	2.71E-05	0	4.44E-05
KFM09A	20051129 08:20	20051129 09:35	146.00	166.00	3	1	20051129 08:53:25	20051129 09:13:42	4.50E-06	0	1.26E-05
KFM09A	20051129 10:00	20051129 11:15	166.00	186.00	3	1	20051129 10:33:21	20051129 10:53:39	4.24E-05	0	4.98E-05
KFM09A	20051129 12:14	20051129 13:31	186.00	206.00	3	1	20051129 12:48:51	20051129 13:09:11	1.41E-07	0	1.63E-07
KFM09A	20051129 14:01	20051129 14:47	206.00	226.00	3	1	20051129 14:36:49	20051129 14:40:14		-1	
KFM09A	20051129 15:38	20051129 16:56	226.00	246.00	3	1	20051129 16:13:49	20051129 16:34:11	9.72E-07	0	1.18E-06
KFM09A	20051129 17:18	20051129 18:37	238.00	258.00	3	1	20051129 17:54:33	20051129 18:14:55	2.46E-07	0	3.84E-07
KFM09A	20051129 18:58	20051129 20:17	258.00	278.00	3	1	20051129 19:35:15	20051129 19:55:42	5.18E-08	0	9.90E-08
KFM09A	20051129 21:03	20051129 22:25	278.00	298.00	3	1	20051129 21:42:40	20051129 22:03:04	1.11E-07	0	1.57E-07
KFM09A	20051129 22:41	20051129 23:57	286.00	306.00	3	1	20051129 23:15:24	20051129 23:35:54	6.13E-08	0	9.62E-08
KFM09A	20051130 06:29	20051130 07:48	306.00	326.00	3	1	20051130 07:05:44	20051130 07:26:04	2.78E-07	0	6.73E-07
KFM09A	20051130 08:16	20051130 09:35	326.00	346.00	3	1	20051130 08:53:03	20051130 09:13:26	2.09E-08	0	4.56E-08
KFM09A	20051130 10:06	20051130 11:22	346.00	366.00	3	1	20051130 10:40:24	20051130 11:00:46	4.37E-08	0	5.89E-08
KFM09A	20051130 12:06	20051130 13:23	366.00	386.00	3	1	20051130 12:41:16	20051130 13:01:46	1.28E-06	0	1.60E-06
KFM09A	20051130 13:50	20051130 15:08	386.00	406.00	3	1	20051130 14:25:53	20051130 14:46:29	2.69E-06	0	5.50E-06
KFM09A	20051130 15:30	20051130 16:47	406.00	426.00	3	1	20051130 16:04:48	20051130 16:25:26	3.99E-07	0	4.89E-07
KFM09A	20051130 18:18	20051130 19:38	426.00	446.00	3	1	20051130 18:55:34	20051130 19:16:08	1.85E-05	0	4.93E-05
KFM09A	20051130 20:03	20051130 21:45	446.00	466.00	3	1	20051130 21:02:55	20051130 21:23:31	7.09E-08	0	9.94E-08
KFM09A	20051130 22:03	20051130 23:20	466.00	486.00	3	1	20051130 22:37:39	20051130 22:58:37	4.00E-08	0	7.55E-08

idcode	start_date	stop_date	secup	seclow	test_type	Formation_type	start_flow_period	stop_flow_period	flow_rate_end_qp	Value_type_qp	mean_flow_rate_qm
KFM09A	20051201 08:06	20051201 09:34	486.00	506.00	3	1	20051201 08:51:37	20051201 09:11:58	1.17E-07	0	2.67E-07
KFM09A	20051201 10:01	20051201 11:22	506.00	526.00	3	1	20051201 10:39:48	20051201 11:00:08	4.34E-08	0	7.76E-08
KFM09A	20051201 11:41	20051201 13:46	526.00	546.00	3	1	20051201 13:03:33	20051201 13:23:52	2.91E-06	0	9.83E-06
KFM09A	20051201 14:21	20051201 15:09	545.00	565.00	3	1	20051201 14:59:12	20051201 15:02:07		-1	
KFM09A	20051201 15:34	20051201 16:17	566.00	586.00	3	1	20051201 16:08:01	20051201 16:10:17		-1	
KFM09A	20051202 07:55	20051202 08:37	586.00	606.00	3	1	20051202 08:28:21	20051202 08:29:58		-1	
KFM09A	20051202 08:58	20051202 10:22	606.00	626.00	3	1	20051202 09:40:01	20051202 10:00:18	4.76E-07	0	7.39E-07
KFM09A	20051202 10:43	20051202 12:05	626.00	646.00	3	1	20051202 11:22:44	20051202 11:43:05	8.54E-08	0	1.15E-07
KFM09A	20051202 13:12	20051202 14:35	646.00	666.00	3	1	20051202 13:52:57	20051202 14:13:15	1.04E-07	0	1.27E-07
KFM09A	20051202 14:57	20051202 16:13	666.00	686.00	3	1	20051202 15:30:57	20051202 15:51:01	1.19E-08	0	3.11E-08
KFM09A	20051205 08:22	20051205 09:53	686.00	706.00	3	1	20051205 09:10:31	20051205 09:30:35	9.44E-09	0	2.33E-08
KFM09A	20051205 10:10	20051205 11:12	691.00	711.00	3	1	20051205 10:52:46	20051205 11:05:04		-1	
KFM09A	20051205 12:46	20051205 13:30	711.00	731.00	3	1	20051205 13:20:23	20051205 13:22:52		-1	
KFM09A	20051205 13:49	20051205 15:12	731.00	751.00	3	1	20051205 14:29:26	20051205 14:49:46	6.26E-08	0	8.05E-08
KFM09A	20051205 15:30	20051205 16:54	751.00	771.00	3	1	20051205 16:12:15	20051205 16:32:33	3.61E-07	0	1.07E-07
KFM09A	20051205 18:09	20051205 19:26	771.00	791.00	3	1	20051205 18:44:18	20051205 19:04:38	8.90E-07	0	4.69E-05
KFM09A	20051207 07:32	20051207 08:52	106.00	111.00	3	1	20051207 08:10:17	20051207 08:30:41	5.70E-07	0	6.88E-07
KFM09A	20051207 09:08	20051207 10:24	111.00	116.00	3	1	20051207 09:42:13	20051207 10:02:37	6.00E-08	0	7.52E-08
KFM09A	20051221 15:48	20051208 17:51	116.00	121.00	3	1	20051221 16:27:38	20051221 16:47:54	2.15E-06	0	1.42E-07
KFM09A	20051207 12:52	20051207 14:09	121.00	126.00	3	1	20051207 13:26:31	20051207 13:46:51	5.98E-06	0	6.93E-06
KFM09A	20051207 14:26	20051207 16:04	126.00	131.00	3	1	20051207 15:21:48	20051207 15:42:09	3.85E-08	0	1.12E-07
KFM09A	20051207 16:21	20051207 17:40	128.00	133.00	3	1	20051207 16:58:15	20051207 17:18:34	1.74E-05	0	2.61E-05
KFM09A	20051207 17:58	20051207 19:16	133.00	138.00	3	1	20051207 18:34:22	20051207 18:54:23	1.66E-05	0	2.67E-05
KFM09A	20051207 19:42	20051207 21:13	138.00	143.00	3	1	20051207 20:30:41	20051207 20:50:56	3.09E-07	0	3.51E-07
KFM09A	20051207 21:27	20051207 22:45	141.00	146.00	3	1	20051207 22:03:25	20051207 22:23:49	1.24E-06	0	2.35E-06
KFM09A	20051207 23:02	20051208 00:17	146.00	151.00	3	1	20051207 23:35:21	20051207 23:55:41	1.33E-06	0	5.33E-06
KFM09A	20051208 06:16	20051208 06:59	151.00	156.00	3	1	20051208 06:49:42	20051208 06:51:37		-1	
KFM09A	20051208 07:10	20051208 08:26	156.00	161.00	3	1	20051208 07:44:24	20051208 08:04:38	4.26E-06	0	1.07E-05
KFM09A	20051208 08:36	20051208 09:52	161.00	166.00	3	1	20051208 09:10:22	20051208 09:30:41	1.02E-07	0	1.07E-07
KFM09A	20051208 10:03	20051208 11:19	166.00	171.00	3	1	20051208 10:36:39	20051208 10:56:56	4.09E-05	0	4.69E-05
KFM09A	20051208 12:12	20051208 13:29	171.00	176.00	3	1	20051208 12:47:14	20051208 13:07:30	5.50E-08	0	8.37E-07

idcode	start_date	stop_date	secup	seclow	test_type	Formation_type	start_flow_period	stop_flow_period	flow_rate_end_qp	Value_type_qp	mean_flow_rate_qm
KFM09A	20051208 13:43	20051208 14:57	176.00	181.00	3	1	20051208 14:15:22	20051208 14:35:42	2.91E-07	0	3.41E-07
KFM09A	20051208 15:13	20051208 16:28	181.00	186.00	3	1	20051208 15:45:32	20051208 16:05:52	2.50E-07	0	1.90E-06
KFM09A	20051208 16:36	20051208 17:51	186.00	191.00	3	1	20051208 17:09:19	20051208 17:29:36	1.23E-07	0	1.42E-07
KFM09A	20051208 18:03	20051208 18:50	191.00	196.00	3	1	20051208 18:35:40	20051208 18:42:32		-1	
KFM09A	20051208 19:02	20051208 19:47	196.00	201.00	3	1	20051208 19:35:04	20051208 19:39:45		-1	
KFM09A	20051208 19:57	20051208 20:39	201.00	206.00	3	1	20051208 20:30:56	20051208 20:32:09		-1	
KFM09A	20051208 20:58	20051208 21:40	226.00	231.00	3	1	20051208 21:30:25	20051208 21:32:31		-1	
KFM09A	20051208 21:54	20051208 23:08	232.00	237.00	3	1	20051208 22:26:14	20051208 22:46:32	8.39E-07	0	8.63E-07
KFM09A	20051208 23:21	20051209 00:35	237.00	242.00	3	1	20051208 23:52:47	20051209 00:13:05	1.70E-06	0	1.86E-06
KFM09A	20051209 08:08	20051209 09:24	240.80	245.80	3	1	20051209 08:41:39	20051209 09:01:58	3.22E-07	0	4.57E-07
KFM09A	20051221 13:55	20051221 14:35	246.80	251.80	3	1	20051221 14:26:40	20051221 14:28:04		-1	
KFM09A	20051209 09:40	20051209 10:22	251.50	256.50	3	1	20051209 10:12:05	20051209 10:14:57		-1	
KFM09A	20051209 10:34	20051209 11:18	256.50	261.50	3	1	20051209 11:06:25	20051209 11:10:31		-1	
KFM09A	20051209 11:30	20051209 13:22	273.00	278.00	3	1	20051209 12:39:59	20051209 13:00:19	6.80E-08	0	1.00E-07
KFM09A	20051209 13:34	20051209 14:48	278.00	283.00	3	1	20051209 14:05:39	20051209 14:26:00	9.75E-08	0	1.44E-07
KFM09A	20051209 15:04	20051209 15:51	283.00	288.00	3	1	20051209 15:36:41	20051209 15:44:08		-1	
KFM09A	20051209 16:00	20051209 17:15	288.00	293.00	3	1	20051209 16:33:16	20051209 16:53:38	1.57E-08	0	2.83E-08
KFM09A	20051212 08:21	20051212 09:42	293.00	298.00	3	1	20051212 08:59:52	20051212 09:20:12	3.38E-08	0	4.10E-08
KFM09A	20051221 12:39	20051221 13:28	296.00	301.00	3	1	20051221 13:11:23	20051221 13:21:20		-1	
KFM09A	20051221 11:45	20051221 12:29	301.00	306.00	3	1	20051221 12:18:01	20051221 12:21:31		-1	
KFM09A	20051212 09:58	20051212 10:39	306.00	311.00	3	1	20051212 10:30:37	20051212 10:31:58		-1	
KFM09A	20051212 10:49	20051212 12:33	311.00	316.00	3	1	20051212 12:23:33	20051212 12:25:31		-1	
KFM09A	20051212 12:43	20051212 13:31	316.00	321.00	3	1	20051212 13:19:35	20051212 13:23:52		-1	
KFM09A	20051212 13:44	20051212 15:02	321.00	326.00	3	1	20051212 14:20:06	20051212 14:40:29	2.98E-07	0	6.68E-07
KFM09A	20051212 15:31	20051212 16:14	346.00	351.00	3	1	20051212 16:05:39	20051212 16:06:46		-1	
KFM09A	20051221 10:04	20051221 11:19	351.00	356.00	3	1	20051021 10:36:43	20051021 10:56:56	5.07E-08	0	6.90E-08
KFM09A	20051221 08:54	20051221 09:50	356.00	361.00	3	1	20051221 09:25:06	20051221 09:43:27		-1	
KFM09A	20051221 07:28	20051221 08:43	361.00	366.00	3	1	20051221 08:00:40	20051221 08:20:51	1.76E-08	0	9.48E-09
KFM09A	20051212 16:39	20051212 17:54	363.00	368.00	3	1	20051212 17:11:54	20051212 17:32:16	1.17E-08	0	1.62E-08
KFM09A	20051213 06:27	20051213 07:24	368.00	373.00	3	1	20051213 07:15:59	20051213 07:17:12		-1	
KFM09A	20051213 07:35	20051213 08:48	371.00	376.00	3	1	20051213 08:09:41	20051213 08:23:48	1.47E-06	0	2.13E-06
KFM09A	20051213 09:02	20051213 09:58	376.00	381.00	3	1	20051213 09:37:12	20051213 09:51:20		-1	

idcode	start_date	stop_date	secup	seclow	test_type	Formation_type	start_flow_period	stop_flow_period	flow_rate_end_qp	Value_type_qp	mean_flow_rate_qm
KFM09A	20051213 10:10	20051213 11:25	381.00	386.00	3	1	20051213 10:42:36	20051213 11:02:40		-1	
KFM09A	20051213 11:57	20051213 13:16	386.00	391.00	3	1	20051213 12:33:30	20051213 12:53:52	2.47E-06	0	5.33E-06
KFM09A	20051213 13:28	20051213 14:48	391.00	396.00	3	1	20051213 14:05:53	20051213 14:26:16	1.66E-07	0	1.87E-07
KFM09A	20051213 15:06	20051213 15:49	396.00	401.00	3	1	20051213 15:37:15	20051213 15:41:39		-1	
KFM09A	20051213 16:00	20051213 17:15	401.00	406.00	3	1	20051213 16:33:21	20051213 16:53:44	4.26E-07	0	4.98E-07
KFM09A	20051213 17:25	20051213 18:18	406.00	411.00	3	1	20051213 17:56:34	20051213 18:10:55		-1	
KFM09A	20051213 18:36	20051213 19:50	411.00	416.00	3	1	20051213 19:07:32	20051213 19:27:56	3.70E-07	0	5.52E-07
KFM09A	20051213 20:06	20051213 21:22	414.00	419.00	3	1	20051213 20:39:31	20051213 20:59:55	1.30E-08	0	1.05E-08
KFM09A	20051213 21:32	20051213 22:46	419.00	424.00	3	1	20051213 22:04:11	20051213 22:24:35	5.68E-08	0	6.90E-08
KFM09A	20051213 22:55	20051214 00:09	421.00	426.00	3	1	20051213 23:26:44	20051213 23:47:06	5.78E-08	0	7.13E-08
KFM09A	20051214 06:51	20051214 07:59	426.00	431.00	3	1	20051214 07:32:04	20051214 07:52:07		-1	
KFM09A	20051214 08:11	20051214 09:31	431.00	436.00	3	1	20051214 08:49:02	20051214 09:09:24	1.61E-05	0	5.02E-05
KFM09A	20051214 09:47	20051214 10:29	436.00	441.00	3	1	20051214 10:20:56	20051214 10:22:10		-1	
KFM09A	20051214 10:44	20051214 12:00	441.00	446.00	3	1	20051214 11:18:15	20051214 11:38:42	2.09E-07	0	1.94E-06
KFM09A	20051214 12:13	20051214 14:04	446.00	451.00	3	1	20051214 13:21:31	20051214 13:41:55	3.75E-08	0	1.55E-07
KFM09A	20051214 14:22	20051214 15:38	451.00	456.00	3	1	20051214 14:56:20	20051214 15:16:46	1.24E-08	0	1.48E-08
KFM09A	20051214 15:55	20051214 17:12	456.00	461.00	3	1	20051214 16:30:00	20051214 16:50:24	6.76E-08	0	5.90E-08
KFM09A	20051214 17:32	20051214 18:15	461.00	466.00	3	1	20051214 18:04:52	20051214 18:07:43		-1	
KFM09A	20051214 18:35	20051214 19:50	471.00	476.00	3	1	20051214 19:08:00	20051214 19:28:26	5.28E-08	0	7.96E-08
KFM09A	20051214 20:01	20051214 21:23	476.00	481.00	3	1	20051214 20:40:37	20051214 21:00:58	4.27E-08	0	5.18E-08
KFM09A	20051214 21:40	20051214 22:31	486.00	491.00	3	1	20051214 22:17:49	20051214 22:23:53		-1	
KFM09A	20051214 22:58	20051215 00:12	491.00	496.00	3	1	20051214 23:29:36	20051214 23:49:58	7.80E-08	0	1.03E-07
KFM09A	20051215 06:33	20051215 07:57	496.00	501.00	3	1	20051215 07:15:10	20051215 07:35:32	6.24E-08	0	1.75E-07
KFM09A	20051215 08:14	20051215 09:00	501.00	506.00	3	1	20051215 08:47:17	20051215 08:53:08		-1	
KFM09A	20051220 19:00	20051220 20:23	506.00	511.00	3	1	20051220 19:41:12	20051220 20:01:35	1.64E-08	0	1.77E-08
KFM09A	20051220 20:50	20051220 22:05	511.00	516.00	3	1	20051220 21:22:36	20051220 21:42:55	2.98E-08	0	2.82E-08
KFM09A	20051220 22:14	20051220 23:28	516.00	521.00	3	1	20051220 22:45:57	20051220 23:06:17	1.94E-08	0	2.24E-08
KFM09A	20051215 09:25	20051215 10:11	521.00	526.00	3	1	20051215 10:01:53	20051215 10:03:44		-1	
KFM09A	20051215 10:26	20051215 11:07	526.00	531.00	3	1	20051215 10:58:38	20051215 10:59:49		-1	
KFM09A	20051215 11:23	20051215 12:44	531.00	536.00	3	1	20051215 12:01:54	20051215 12:22:16	2.91E-06	0	1.06E-05
KFM09A	20051215 13:19	20051215 14:03	536.00	541.00	3	1	20051215 13:52:58	20051215 13:56:08		-1	
KFM09A	20051215 14:14	20051215 15:28	541.00	546.00	3	1	20051215 14:46:13	20051215 15:06:37	8.67E-09	0	5.55E-08

idcode	start_date	stop_date	secup	seclow	test_type	Formation_type	start_flow_period	stop_flow_period	flow_rate_end_qp	Value_type_qp	mean_flow_rate_qm
KFM09A	20051220 17:14	20051220 17:58	561.00	566.00	3	1	20051220 17:49:31	20051220 17:50:36		-1	
KFM09A	20051215 16:19	20051215 17:00	606.00	611.00	3	1	20051215 16:50:43	20051215 16:52:47		-1	
KFM09A	20051215 17:19	20051215 18:35	611.00	616.00	3	1	20051215 17:52:51	20051215 18:13:12	3.96E-07	0	6.14E-07
KFM09A	20051215 18:50	20051215 19:31	616.00	621.00	3	1	20051215 19:21:48	20051215 19:23:40		-1	
KFM09A	20051215 19:44	20051215 21:03	621.00	626.00	3	1	20051215 20:21:06	20051215 20:41:34	1.53E-07	0	2.22E-07
KFM09A	20051215 21:14	20051215 22:01	626.00	631.00	3	1	20051215 21:45:46	20051215 21:54:10		-1	
KFM09A	20051215 22:08	20051215 23:33	631.00	636.00	3	1	20051215 22:51:11	20051215 23:11:40	1.17E-08	0	2.06E-08
KFM09A	20051215 23:43	20051216 00:58	636.00	641.00	3	1	20051216 00:15:28	20051216 00:35:56	1.35E-07	0	1.34E-07
KFM09A	20051216 08:21	20051216 09:36	641.00	646.00	3	1	20051216 08:53:39	20051216 09:14:01	1.27E-08	0	9.09E-07
KFM09A	20051216 09:55	20051216 10:38	646.00	651.00	3	1	20051216 10:28:16	20051216 10:31:02		-1	
KFM09A	20051216 10:53	20051216 12:10	651.00	656.00	3	1	20051216 11:27:51	20051216 11:48:20	1.27E-07	0	2.02E-05
KFM09A	20051216 12:21	20051216 13:20	656.00	661.00	3	1	20051216 13:03:34	20051216 13:12:30		-1	
KFM09A	20051216 13:31	20051216 14:14	661.00	666.00	3	1	20051216 14:04:48	20051216 14:06:57		-1	
KFM09A	20051219 08:19	20051219 09:01	731.00	736.00	3	1	20051219 08:52:49	20051219 08:54:27		-1	
KFM09A	20051219 09:15	20051219 09:56	736.00	741.00	3	1	20051219 09:46:55	20051219 09:49:06		-1	
KFM09A	20051219 10:11	20051219 11:30	741.00	746.00	3	1	20051219 10:47:39	20051219 11:08:09	8.87E-08	0	7.57E-08
KFM09A	20051219 11:44	20051219 12:36	746.00	751.00	3	1	20051219 12:22:11	20051219 12:29:10		-1	
KFM09A	20051219 12:50	20051219 14:05	751.00	756.00	3	1	20051219 13:23:07	20051219 13:43:35	7.95E-08	0	1.26E-07
KFM09A	20051219 14:20	20051219 15:42	756.00	761.00	3	1	20051219 15:00:30	20051219 15:20:59	2.15E-07	0	3.66E-07
KFM09A	20051219 15:56	20051219 17:16	761.00	766.00	3	1	20051219 16:33:37	20051219 16:54:07	1.07E-07	0	1.57E-07
KFM09A	20051220 06:55	20051220 08:10	766.00	771.00	3	1	20051220 07:28:05	20051220 07:48:28	5.47E-08	0	7.57E-08
KFM09A	20051220 08:29	20051220 09:46	771.00	776.00	3	1	20051220 09:04:02	20051220 09:24:27	5.99E-08	0	6.39E-08
KFM09A	20051220 10:06	20051220 11:24	776.00	781.00	3	1	20051220 10:41:52	20051220 11:02:21	1.15E-07	0	1.40E-07
KFM09A	20051220 11:35	20051220 12:58	781.00	786.00	3	1	20051220 12:15:53	20051220 12:36:19	1.85E-07	0	2.36E-07
KFM09A	20051220 13:11	20051220 14:28	786.00	791.00	3	1	20051220 13:46:19	20051220 14:06:43	7.06E-07	0	9.09E-07
KFM09A	20051118 13:32	20051118 14:28	506.00 [1)]	606.00	3	1	20051118 14:18:02	20051118 14:26:00			
KFM09A	20051130 17:10	20051130 18:03	426.00[1)]	446.00	3	1	20051130 17:43:55	20051130 17:56:57			
KFM09A	20051207 10:38	20051207 12:39	116.00[1)]	121.00	3	1	20051207 12:36:48	20051207 12:38:34			

[1)] Incomplete test, interrupted and re-performed later.

KFM09A plu_s_hole_test_d. Right (This result table to SICADA includes more columns which are empty, these columns are not presented here.)

idcode	secup	seclow	q_measl__l	q_measl__u	tot_volume_vp	dur_flow_phase_tp	dur_rec_phase_tf	initial_press_pi	press_at_flow_end_pp	final_press_pf	fluid_temp_tew
KFM09A	106.00	206.00	1.7E-08	1.0E-03	1.70E-01	1819	1800	929.78	1114.19	948.54	7.92
KFM09A	206.00	306.00	1.7E-08	1.0E-03	2.95E-03	1822	1800	1746.27	1963.05	1759.94	8.08
KFM09A	306.00	406.00	1.7E-08	1.0E-03	1.31E-02	1827	1797	2542.61	2753.18	2631.48	8.87
KFM09A	406.00	506.00	1.7E-08	1.0E-03	6.87E-02	1821	1800	3314.26	3517.70	3472.12	9.51
KFM09A	506.00	606.00	1.7E-08	1.0E-03	1.48E-02	1821	1800	4075.97	4296.20	4263.63	10.58
KFM09A	606.00	706.00	1.7E-08	1.0E-03	1.46E-03	1820	1803	4781.92	4987.26	4843.19	11.54
KFM09A	691.00	791.00	1.7E-08	1.0E-03	2.24E-03	1821	1801	5371.98	5548.07	5405.64	12.22
KFM09A	106.00	126.00	1.7E-08	1.0E-03	1.22E-02	1216	1206	939.44	1152.92	946.07	7.29
KFM09A	126.00	146.00	1.7E-08	1.0E-03	5.40E-02	1216	1206	1108.50	1324.71	1158.02	7.35
KFM09A	146.00	166.00	1.7E-08	1.0E-03	1.54E-02	1217	1200	1277.24	1460.00	1389.29	7.52
KFM09A	166.00	186.00	1.7E-08	1.0E-03	6.07E-02	1218	1205	1439.66	1628.85	1451.67	7.50
KFM09A	186.00	206.00	1.7E-08	1.0E-03	1.99E-04	1220	1202	1609.00	1908.70	1627.19	7.82
KFM09A	206.00	226.00	5.1E-09	1.0E-03		205	321	1799.82	1971.07	1959.47	7.99
KFM09A	226.00	246.00	1.7E-08	1.0E-03	1.45E-03	1222	1200	1936.29	2142.18	1942.92	8.15
KFM09A	238.00	258.00	1.7E-08	1.0E-03	4.70E-04	1222	1197	2036.61	2246.50	2073.17	8.27
KFM09A	258.00	278.00	1.7E-08	1.0E-03	1.22E-04	1227	1194	2205.79	2409.18	2271.89	8.43
KFM09A	278.00	298.00	1.7E-08	1.0E-03	1.92E-04	1224	1194	2363.51	2574.60	2423.68	8.61
KFM09A	286.00	306.00	1.7E-08	1.0E-03	1.19E-04	1230	1191	2426.85	2640.10	2497.64	8.67
KFM09A	306.00	326.00	1.7E-08	1.0E-03	8.23E-04	1220	1203	2588.71	2788.52	2720.63	8.83
KFM09A	326.00	346.00	1.7E-08	1.0E-03	5.58E-05	1223	1202	2751.68	2952.80	2816.12	8.99
KFM09A	346.00	366.00	1.7E-08	1.0E-03	7.20E-05	1222	1200	2908.57	3113.84	2949.69	9.17
KFM09A	366.00	386.00	1.7E-08	1.0E-03	1.98E-03	1230	1189	3063.39	3264.59	3103.70	9.33
KFM09A	386.00	406.00	1.7E-08	1.0E-03	6.80E-03	1236	1185	3219.88	3419.73	3326.14	9.51
KFM09A	406.00	426.00	1.7E-08	1.0E-03	6.05E-04	1238	1184	3378.16	3578.01	3432.11	9.68
KFM09A	426.00	446.00	1.7E-08	1.0E-03	6.10E-02	1234	1185	3545.41	3765.49	3714.71	9.66
KFM09A	446.00	466.00	1.7E-08	1.0E-03	1.23E-04	1236	1184	3693.33	3922.81	3730.72	10.03
KFM09A	466.00	486.00	1.7E-08	1.0E-03	9.52E-05	1258	1162	3856.58	4029.33	3923.36	10.21

idcode	secup	seclow	q_measl__l	q_measl__u	tot_volume_vp	dur_flow_phase_tp	dur_rec_phase_tf	initial_press_pi	press_at_flow_end_pp	final_press_pf	fluid_temp_tew
KFM09A	486.00	506.00	1.7E-08	1.0E-03	3.27E-04	1221	1200	4001.32	4206.10	4108.27	10.39
KFM09A	506.00	526.00	1.7E-08	1.0E-03	9.50E-05	1220	1200	4171.74	4362.23	4210.38	10.56
KFM09A	526.00	546.00	1.7E-08	1.0E-03	1.20E-02	1219	1203	4303.10	4508.03	4472.57	10.73
KFM09A	545.00	565.00	5.1E-09	1.0E-03		175	321	4514.10	4661.19	4675.69	10.91
KFM09A	566.00	586.00	5.1E-09	1.0E-03		136	321	4631.11	4820.31	4823.61	11.09
KFM09A	586.00	606.00	5.1E-09	1.0E-03		97	322	4765.93	4982.58	4989.21	11.28
KFM09A	606.00	626.00	1.7E-08	1.0E-03	9.01E-04	1217	1205	4896.47	5096.82	4980.92	11.45
KFM09A	626.00	646.00	1.7E-08	1.0E-03	1.41E-04	1221	1200	5050.61	5258.42	5072.55	11.61
KFM09A	646.00	666.00	1.7E-08	1.0E-03	1.55E-04	1218	1205	5186.25	5389.93	5211.64	11.79
KFM09A	666.00	686.00	5.1E-09	1.0E-03	3.74E-05	1204	1221	5355.15	5533.99	5469.96	11.97
KFM09A	686.00	706.00	5.1E-09	1.0E-03	2.81E-05	1204	1221	5498.11	5687.43	5619.55	12.13
KFM09A	691.00	711.00	3.9E-09	1.0E-03		738	321	5561.73	5724.42	5713.38	12.17
KFM09A	711.00	731.00	3.9E-09	1.0E-03		149	321	5679.43	5864.34	5869.58	12.36
KFM09A	731.00	751.00	1.7E-08	1.0E-03	9.84E-05	1220	1203	5782.93	5995.56	5819.36	12.52
KFM09A	751.00	771.00	1.7E-08	1.0E-03	1.31E-04	1218	1203	5915.12	6118.38	1406.62	12.67
KFM09A	771.00	791.00	1.7E-08	1.0E+00	5.72E-02	1220	1184	6056.14	6271.55	1456.30	12.83
KFM09A	106.00	111.00	1.7E-08	1.0E-03	8.42E-04	1224	1195	948.90	1151.62	995.96	7.28
KFM09A	111.00	116.00	1.7E-08	1.0E-03	9.20E-05	1224	1197	993.19	1200.74	1037.91	7.30
KFM09A	116.00	121.00	1.7E-08	1.1E+01	1.73E-04	1216	1206	1025.62	1225.72	1627.41	7.26
KFM09A	121.00	126.00	1.7E-08	1.0E-03	8.47E-03	1220	1197	1074.34	1252.70	1076.55	7.31
KFM09A	126.00	131.00	1.7E-08	1.0E-03	1.37E-04	1221	1196	1121.53	1323.83	1249.86	7.42
KFM09A	128.00	133.00	1.7E-08	1.0E-03	3.18E-02	1219	1197	1131.88	1348.66	1163.76	7.30
KFM09A	133.00	138.00	1.7E-08	1.0E-03	3.21E-02	1201	1197	1174.24	1409.45	1217.29	7.36
KFM09A	138.00	143.00	1.7E-08	1.0E-03	4.28E-04	1215	1197	1215.08	1415.79	1219.50	7.51
KFM09A	141.00	146.00	1.7E-08	1.0E-03	2.88E-03	1224	1194	1240.89	1466.23	1321.06	7.53
KFM09A	146.00	151.00	1.7E-08	1.0E-03	6.51E-03	1220	1187	1284.09	1510.35	1450.22	7.53
KFM09A	151.00	156.00	5.1E-09	1.0E-03		115	321	1349.21	1565.72	1571.10	7.56
KFM09A	156.00	161.00	1.7E-08	1.0E-03	1.31E-02	1214	1197	1365.50	1573.10	1482.79	7.57
KFM09A	161.00	166.00	1.7E-08	1.0E-03	1.31E-04	1219	1199	1408.00	1586.50	1406.62	7.70
KFM09A	166.00	171.00	1.7E-08	1.0E-03	5.72E-02	1217	1200	1447.05	1626.80	1456.30	7.44
KFM09A	171.00	176.00	1.7E-08	1.0E-03	1.03E-03	1216	1184	1496.45	1703.03	1687.02	7.76

idcode	secup	seclow	q_measl__l	q_measl__u	tot_volume_vp	dur_flow_phase_tp	dur_rec_phase_tf	initial_press_pi	press_at_flow_end_pp	final_press_pf	fluid_temp_tew
KFM09A	176.00	181.00	1.7E-08	1.0E-03	4.15E-04	1220	1199	1534.00	1734.49	1557.86	7.76
KFM09A	181.00	186.00	1.7E-08	1.0E-03	2.35E-03	1220	1184	1575.38	1803.90	1780.30	7.77
KFM09A	186.00	191.00	1.7E-08	1.0E-03	1.73E-04	1217	1200	1616.92	1832.60	1627.41	7.81
KFM09A	191.00	196.00	5.3E-09	1.0E-03		412	322	1677.49	1875.23	1828.87	7.85
KFM09A	196.00	201.00	4.1E-09	1.0E-03		281	321	1710.62	1916.50	1891.79	7.88
KFM09A	201.00	206.00	5.3E-09	1.0E-03		73	322	1766.78	1957.48	1965.21	7.93
KFM09A	226.00	231.00	5.3E-09	1.0E-03		126	321	1961.89	2161.15	2158.94	8.13
KFM09A	232.00	237.00	1.7E-08	1.0E-03	1.05E-03	1218	1202	1992.95	2191.65	1995.02	8.20
KFM09A	237.00	242.00	1.7E-08	1.0E-03	2.27E-03	1218	1203	2032.55	2232.77	2040.28	8.25
KFM09A	240.80	245.80	1.7E-08	1.0E-03	5.58E-04	1219	1202	2060.01	2263.69	2071.18	8.29
KFM09A	246.80	251.80	4.1E-09	1.0E+01		84	322	2184.89	2323.99	2971.99	8.27
KFM09A	251.50	256.50	5.3E-09	1.0E-03		172	321	2217.45	2385.25	2408.43	8.35
KFM09A	256.50	261.50	6.5E-09	1.0E-03		246	321	2239.39	2427.20	2424.45	8.39
KFM09A	273.00	278.00	1.7E-08	1.0E-03	1.22E-04	1220	1200	2328.68	2560.78	2393.53	8.54
KFM09A	278.00	283.00	1.7E-08	1.0E-03	1.76E-04	1221	1202	2369.80	2576.30	2435.48	8.58
KFM09A	283.00	288.00	5.3E-09	1.0E-03		447	321	2409.26	2618.73	2574.58	8.62
KFM09A	288.00	293.00	1.0E-08	1.0E-03	3.40E-05	1222	1221	2459.90	2659.88	2540.35	8.67
KFM09A	293.00	298.00	1.7E-08	1.0E-03	5.00E-05	1220	1203	2493.43	2728.00	2549.74	8.71
KFM09A	296.00	301.00	4.1E-09	7.0E+00		597	322	2521.45	2730.23	3349.53	8.72
KFM09A	301.00	306.00	4.1E-09	8.0E+00		210	321	2567.81	2767.21	3301.51	8.73
KFM09A	306.00	311.00	6.5E-09	1.0E-03		81	321	2678.48	2831.80	2864.35	8.81
KFM09A	311.00	316.00	2.8E-09	1.0E-03		118	322	2652.96	2872.36	2868.77	8.85
KFM09A	316.00	321.00	4.1E-09	1.0E-03		257	321	2674.48	2942.73	2935.01	8.88
KFM09A	321.00	326.00	1.7E-08	1.0E-03	8.16E-04	1223	1202	2712.56	2913.42	2845.04	8.94
KFM09A	346.00	351.00	6.5E-09	1.0E-03		67	321	3017.39	3117.02	3125.44	9.14
KFM09A	351.00	356.00	1.7E-08	3.0E+00	8.44E-05	1213	1211	2958.18	3169.22	3512.92	9.19
KFM09A	356.00	361.00	4.1E-09	4.0E+00		1101	321	2991.17	3206.99	3532.23	9.25
KFM09A	361.00	366.00	4.1E-09	5.0E+00	1.14E-05	1211	1221	3026.22	3242.46	3698.38	9.25
KFM09A	363.00	368.00	5.0E-09	1.0E-03	1.95E-05	1222	1221	3062.65	3254.73	3095.07	9.29
KFM09A	368.00	373.00	5.3E-09	1.0E-03		73	321	3128.47	3316.41	3294.88	9.35
KFM09A	371.00	376.00	1.7E-08	1.0E-03	2.12E-03	847	1221	3108.19	3309.50	3140.33	9.38
KFM09A	376.00	381.00	5.0E-09	1.0E-03		848	321	3174.01	3361.53	3334.08	9.40

idcode	secup	seclow	q_measl__l	q_measl__u	tot_volume_vp	dur_flow_phase_tp	dur_rec_phase_tf	initial_press_pi	press_at_flow_end_pp	final_press_pf	fluid_temp_tew
KFM09A	381.00	386.00	5.3E-09	1.0E-03		1204	1221	3234.58	3403.07	3284.95	9.45
KFM09A	386.00	391.00	1.7E-08	1.0E-03	6.53E-03	1222	1200	3226.58	3437.98	3349.53	9.52
KFM09A	391.00	396.00	1.7E-08	1.0E-03	2.29E-04	1223	1202	3274.47	3481.73	3301.51	9.55
KFM09A	396.00	401.00	6.5E-09	1.0E-03		264	321	3321.10	3524.50	3485.87	9.57
KFM09A	401.00	406.00	1.7E-08	1.0E-03	6.09E-04	1223	1200	3346.08	3547.69	3369.95	9.61
KFM09A	406.00	411.00	5.3E-09	1.0E-03		861	321	3392.03	3584.11	3550.45	9.65
KFM09A	411.00	416.00	1.7E-08	1.0E-03	6.76E-04	1224	1200	3426.25	3621.31	3496.35	9.69
KFM09A	414.00	419.00	5.3E-09	1.0E-03	1.27E-05	1224	1221	3460.47	3654.12	3480.91	9.72
KFM09A	419.00	424.00	1.7E-08	1.0E-03	8.44E-05	1224	1200	3488.63	3692.58	3512.92	9.77
KFM09A	421.00	426.00	1.7E-08	1.0E-03	8.73E-05	1222	1200	3515.00	3708.32	3532.23	9.79
KFM09A	426.00	431.00	7.8E-09	1.0E-03		1203	322	3560.79	3773.30	3698.38	9.89
KFM09A	431.00	436.00	1.7E-08	1.0E-03	6.15E-02	1222	1200	3579.70	3802.83	3753.02	9.65
KFM09A	436.00	441.00	6.0E-09	1.0E-03		74	321	3649.79	3829.74	3837.47	10.00
KFM09A	441.00	446.00	1.7E-08	1.0E-03	2.41E-03	1227	1182	3661.40	3888.20	3871.14	10.03
KFM09A	446.00	451.00	1.7E-08	1.0E-03	1.90E-04	1224	1200	3702.24	3909.77	3866.72	10.02
KFM09A	451.00	456.00	5.3E-09	1.0E-03	1.78E-05	1226	1221	3761.02	3951.96	3840.22	10.05
KFM09A	456.00	461.00	1.7E-08	1.0E-03	7.22E-05	1224	1200	3787.78	3990.92	3815.94	10.09
KFM09A	461.00	466.00	2.8E-09	1.0E-03		171	322	3916.81	4031.76	4071.50	10.13
KFM09A	471.00	476.00	1.7E-08	1.0E-03	9.75E-05	1226	1199	3902.46	4111.10	3964.42	10.23
KFM09A	476.00	481.00	1.7E-08	1.0E-03	6.33E-05	1221	1203	3964.43	4153.74	4008.03	10.28
KFM09A	486.00	491.00	5.3E-09	1.0E-03		364	321	4047.08	4229.36	4217.76	10.36
KFM09A	491.00	496.00	1.7E-08	1.0E-03	1.26E-04	1222	1200	4063.22	4261.51	4095.23	10.41
KFM09A	496.00	501.00	1.7E-08	1.0E-03	2.15E-04	1222	1200	4090.13	4297.53	4222.18	10.46
KFM09A	501.00	506.00	5.0E-09	1.0E-03		351	321	4165.19	4330.23	4289.52	10.49
KFM09A	506.00	511.00	4.1E-09	1.0E-03	2.13E-05	1223	1221	4215.56	4366.80	4289.52	10.54
KFM09A	511.00	516.00	1.7E-08	1.0E-03	3.44E-05	1219	1206	4232.67	4403.23	4229.36	10.60
KFM09A	516.00	521.00	7.7E-09	1.0E-03	2.70E-05	1220	1221	4254.20	4440.03	4285.67	10.63
KFM09A	521.00	526.00	5.3E-09	1.0E-03		111	321	4405.30	4484.51	4539.01	10.67
KFM09A	526.00	531.00	5.3E-09	1.0E-03		71	321	4442.14	4520.81	4592.00	10.73
KFM09A	531.00	536.00	1.7E-08	1.0E-03	1.30E-02	1222	1199	4354.65	4571.03	4535.15	10.76
KFM09A	536.00	541.00	5.3E-09	1.0E-03		190	320	4479.13	4594.76	4560.54	10.86
KFM09A	541.00	546.00	5.3E-09	1.0E-03	6.67E-05	1224	1221	4437.45	4632.29	4613.53	10.88

idcode	secup	seclow	q_measl__l	q_measl__u	tot_volume_vp	dur_flow_phase_tp	dur_rec_phase_tf	initial_press_pi	press_at_flow_end_pp	final_press_pf	fluid_temp_tew
KFM09A	561.00	566.00	5.3E-09	1.0E-03		65	321	4726.95	4774.42	4801.19	11.02
KFM09A	606.00	611.00	4.1E-09	1.0E-03		124	322	5042.26	5120.24	5224.00	11.42
KFM09A	611.00	616.00	1.7E-08	1.0E-03	7.50E-04	1221	1200	4956.43	5148.26	5044.06	11.46
KFM09A	616.00	621.00	5.3E-09	1.0E-03		112	322	5077.59	5206.34	5272.02	11.51
KFM09A	621.00	626.00	1.7E-08	1.0E-03	2.73E-04	1228	1194	5032.46	5244.56	5127.97	11.55
KFM09A	626.00	631.00	4.1E-09	1.0E-03		504	322	5085.18	5263.75	5233.38	11.60
KFM09A	631.00	636.00	5.3E-09	1.0E-03	2.47E-05	1229	1220	5136.79	5301.28	5249.39	11.64
KFM09A	636.00	641.00	1.7E-08	1.0E-03	1.64E-04	1228	1194	5144.52	5335.36	5146.73	11.68
KFM09A	641.00	646.00	2.8E-09	1.0E-03	1.11E-03	1222	1221	5195.30	5374.69	5235.59	11.75
KFM09A	646.00	651.00	2.8E-09	1.0E-03		166	321	5309.69	5410.56	5419.40	11.78
KFM09A	651.00	656.00	1.7E-08	1.0E-03	9.65E-03	1229	1194	5248.56	5444.23	5280.30	11.82
KFM09A	656.00	661.00	6.5E-09	1.0E-03		536	321	5344.46	5486.74	5472.94	11.87
KFM09A	661.00	666.00	4.1E-09	1.0E-03		129	321				
KFM09A	731.00	736.00	5.3E-09	1.0E-03		98	321	5867.31	6009.44	5986.26	12.49
KFM09A	736.00	741.00	5.3E-09	1.0E-03		131	321	5860.27	6044.22	5996.20	12.57
KFM09A	741.00	746.00	1.7E-08	1.0E-03	9.31E-05	1230	1191	5881.11	6078.44	5914.50	12.59
KFM09A	746.00	751.00	5.3E-09	1.0E-03		419	321	5928.44	6112.66	6074.02	12.64
KFM09A	751.00	756.00	1.7E-08	1.0E-03	1.55E-04	1228	1194	5957.42	6143.29	6000.07	12.66
KFM09A	756.00	761.00	1.7E-08	1.0E-03	4.51E-04	1229	1189	5986.68	6192.63	6040.91	12.71
KFM09A	761.00	766.00	1.7E-08	1.0E-03	1.92E-04	1230	1199	6021.04	6221.97	6050.29	12.75
KFM09A	766.00	771.00	1.7E-08	1.0E-03	9.27E-05	1223	1187	6049.32	6239.82	6077.34	12.79
KFM09A	771.00	776.00	1.7E-08	1.0E-03	7.84E-05	1225	1187	6086.85	6319.41	6096.65	12.83
KFM09A	776.00	781.00	1.7E-08	1.0E-03	1.71E-04	1229	1187	6119.15	6309.34	6137.49	12.87
KFM09A	781.00	786.00	1.7E-08	1.0E-03	2.90E-04	1226	1187	6152.12	6325.44	6168.40	12.92
KFM09A	786.00	791.00	1.7E-08	1.0E-03	1.11E-03	1224	1187	6184.96	6388.23	6192.69	12.96
KFM09A	506.00 [1)]	606.00				478	24	4063.27	4265.15	4264.74	10.56
KFM09A	426.00 [1)]	446.00				782	253	3535.19	3703.67	3675.53	9.70
KFM09A	116.00 [1)]	121.00				106	13	1074.89	1242.69	1074.34	7.32

[1)] Incomplete test, interrupted and re-performed later.

KFM09A plu_s_hole_test_ed1. Left (This result table to SICADA includes more columns which are empty, these columns are not presented here.)

idcode	start_date	stop_date	secup	seclow	test_type	formation_type	spec_capacity_q_s	value_type_q_s	transmissivity_moye	bc_tm	value_type_tm	hydr_cond_moye	formation_width_b
KFM09A	20051117 16:09	20051117 17:59	106.00	206.00	3	1	3.76E-06	0	4.89E-06	0	0	4.89E-08	100.00
KFM09A	20051117 19:03	20051117 20:53	206.00	306.00	3	1	5.92E-08	0	7.69E-08	0	0	7.69E-10	100.00
KFM09A	20051117 21:47	20051117 23:36	306.00	406.00	3	1	1.89E-07	0	2.46E-07	0	0	2.46E-09	100.00
KFM09A	20051118 09:59	20051118 11:49	406.00	506.00	3	1	5.18E-07	0	6.74E-07	1	0	6.74E-09	100.00
KFM09A	20051121 12:52	20051121 15:13	506.00	606.00	3	1	8.66E-08	0	1.13E-07	1	0	1.13E-09	100.00
KFM09A	20051121 06:14	20051121 08:03	606.00	706.00	3	1	2.74E-08	0	3.56E-08	0	0	3.56E-10	100.00
KFM09A	20051121 08:51	20051121 10:40	691.00	791.00	3	1	4.69E-08	0	6.09E-08	0	0	6.09E-10	100.00
KFM09A	20051128 16:44	20051128 18:19	106.00	126.00	3	1	3.89E-07	0	4.06E-07	0	0	2.03E-08	20.00
KFM09A	20051129 06:29	20051129 07:43	126.00	146.00	3	1	1.23E-06	0	1.28E-06	0	0	6.42E-08	20.00
KFM09A	20051129 08:20	20051129 09:35	146.00	166.00	3	1	2.41E-07	0	2.52E-07	0	0	1.26E-08	20.00
KFM09A	20051129 10:00	20051129 11:15	166.00	186.00	3	1	2.20E-06	0	2.29E-06	0	0	1.15E-07	20.00
KFM09A	20051129 12:14	20051129 13:31	186.00	206.00	3	1	4.62E-09	0	4.82E-09	0	0	2.41E-10	20.00
KFM09A	20051129 14:01	20051129 14:47	206.00	226.00	3	1	2.55E-10	-1	2.66E-10	0	-1	1.33E-11	20.00
KFM09A	20051129 15:38	20051129 16:56	226.00	246.00	3	1	4.63E-08	0	4.83E-08	0	0	2.42E-09	20.00
KFM09A	20051129 17:18	20051129 18:37	238.00	258.00	3	1	1.15E-08	0	1.20E-08	0	0	6.00E-10	20.00
KFM09A	20051129 18:58	20051129 20:17	258.00	278.00	3	1	2.50E-09	0	2.61E-09	0	0	1.30E-10	20.00
KFM09A	20051129 21:03	20051129 22:25	278.00	298.00	3	1	5.15E-09	0	5.37E-09	0	0	2.69E-10	20.00
KFM09A	20051129 22:41	20051129 23:57	286.00	306.00	3	1	2.82E-09	0	2.95E-09	0	0	1.47E-10	20.00
KFM09A	20051130 06:29	20051130 07:48	306.00	326.00	3	1	1.37E-08	0	1.43E-08	0	0	7.13E-10	20.00
KFM09A	20051130 08:16	20051130 09:35	326.00	346.00	3	1	1.02E-09	0	1.06E-09	0	0	5.31E-11	20.00
KFM09A	20051130 10:06	20051130 11:22	346.00	366.00	3	1	2.09E-09	0	2.18E-09	0	0	1.09E-10	20.00
KFM09A	20051130 12:06	20051130 13:23	366.00	386.00	3	1	6.23E-08	0	6.50E-08	0	0	3.25E-09	20.00
KFM09A	20051130 13:50	20051130 15:08	386.00	406.00	3	1	1.32E-07	0	1.38E-07	1	0	6.89E-09	20.00
KFM09A	20051130 15:30	20051130 16:47	406.00	426.00	3	1	1.96E-08	0	2.04E-08	1	0	1.02E-09	20.00
KFM09A	20051130 18:18	20051130 19:38	426.00	446.00	3	1	8.24E-07	0	8.60E-07	1	0	4.30E-08	20.00
KFM09A	20051130 20:03	20051130 21:45	446.00	466.00	3	1	3.03E-09	0	3.16E-09	0	0	1.58E-10	20.00
KFM09A	20051130 22:03	20051130 23:20	466.00	486.00	3	1	2.27E-09	0	2.37E-09	0	0	1.19E-10	20.00
KFM09A	20051201 08:06	20051201 09:34	486.00	506.00	3	1	5.62E-09	0	5.86E-09	0	0	2.93E-10	20.00
KFM09A	20051201 10:01	20051201 11:22	506.00	526.00	3	1	2.24E-09	0	2.33E-09	0	0	1.17E-10	20.00

idcode	start_date	stop_date	secup	seclow	test_type	formation_type	spec_capacity_q_s	value_type_q_s	transmissivity_moye	bc_tm	value_type_tm	hydr_cond_moye	formation_width_b
KFM09A	20051201 11:41	20051201 13:46	526.00	546.00	3	1	1.39E-07	0	1.45E-07	1	0	7.27E-09	20.00
KFM09A	20051201 14:21	20051201 15:09	545.00	565.00	3	1	2.55E-10	-1	2.66E-10	0	-1	1.33E-11	20.00
KFM09A	20051201 15:34	20051201 16:17	566.00	586.00	3	1	2.55E-10	-1	2.66E-10	0	-1	1.33E-11	20.00
KFM09A	20051202 07:55	20051202 08:37	586.00	606.00	3	1	2.55E-10	-1	2.66E-10	0	-1	1.33E-11	20.00
KFM09A	20051202 08:58	20051202 10:22	606.00	626.00	3	1	2.33E-08	0	2.43E-08	0	0	1.22E-09	20.00
KFM09A	20051202 10:43	20051202 12:05	626.00	646.00	3	1	4.03E-09	0	4.21E-09	0	0	2.10E-10	20.00
KFM09A	20051202 13:12	20051202 14:35	646.00	666.00	3	1	5.01E-09	0	5.22E-09	0	0	2.61E-10	20.00
KFM09A	20051202 14:57	20051202 16:13	666.00	686.00	3	1	6.54E-10	0	6.82E-10	1	0	3.41E-11	20.00
KFM09A	20051205 08:22	20051205 09:53	686.00	706.00	3	1	4.89E-10	0	5.10E-10	0	0	2.55E-11	20.00
KFM09A	20051205 10:10	20051205 11:12	691.00	711.00	3	1	1.94E-10	-1	2.02E-10	0	-1	1.01E-11	20.00
KFM09A	20051205 12:46	20051205 13:30	711.00	731.00	3	1	1.94E-10	-1	2.02E-10	0	-1	1.01E-11	20.00
KFM09A	20051205 13:49	20051205 15:12	731.00	751.00	3	1	2.89E-09	0	3.01E-09	0	0	1.51E-10	20.00
KFM09A	20051205 15:30	20051205 16:54	751.00	771.00	3	1	1.74E-08	0	1.82E-08	0	0	9.10E-10	20.00
KFM09A	20051205 18:09	20051205 19:26	771.00	791.00	3	1	4.06E-08	0	4.23E-08	0	0	2.12E-09	20.00
KFM09A	20051207 07:32	20051207 08:52	106.00	111.00	3	1	2.76E-08	0	2.27E-08	0	0	4.54E-09	5.00
KFM09A	20051207 09:08	20051207 10:24	111.00	116.00	3	1	2.84E-09	0	2.33E-09	0	0	4.67E-10	5.00
KFM09A	20051221 15:48	20051208 17:51	116.00	121.00	3	1	1.06E-07	0	8.68E-08	0	0	1.74E-08	5.00
KFM09A	20051207 12:52	20051207 14:09	121.00	126.00	3	1	3.29E-07	0	2.71E-07	0	0	5.41E-08	5.00
KFM09A	20051207 14:26	20051207 16:04	126.00	131.00	3	1	1.87E-09	0	1.54E-09	0	0	3.07E-10	5.00
KFM09A	20051207 16:21	20051207 17:40	128.00	133.00	3	1	7.90E-07	0	6.50E-07	0	0	1.30E-07	5.00
KFM09A	20051207 17:58	20051207 19:16	133.00	138.00	3	1	6.94E-07	0	5.71E-07	0	0	1.14E-07	5.00
KFM09A	20051207 19:42	20051207 21:13	138.00	143.00	3	1	1.51E-08	0	1.24E-08	0	0	2.49E-09	5.00
KFM09A	20051207 21:27	20051207 22:45	141.00	146.00	3	1	5.38E-08	0	4.43E-08	0	0	8.86E-09	5.00
KFM09A	20051207 23:02	20051208 00:17	146.00	151.00	3	1	5.77E-08	0	4.75E-08	0	0	9.49E-09	5.00
KFM09A	20051208 06:16	20051208 06:59	151.00	156.00	3	1	2.55E-10	-1	2.10E-10	0	-1	4.20E-11	5.00
KFM09A	20051208 07:10	20051208 08:26	156.00	161.00	3	1	2.02E-07	0	1.66E-07	0	0	3.32E-08	5.00
KFM09A	20051208 08:36	20051208 09:52	161.00	166.00	3	1	5.60E-09	0	4.60E-09	1	0	9.21E-10	5.00
KFM09A	20051208 10:03	20051208 11:19	166.00	171.00	3	1	2.23E-06	0	1.84E-06	0	0	3.67E-07	5.00
KFM09A	20051208 12:12	20051208 13:29	171.00	176.00	3	1	2.61E-09	0	2.15E-09	1	0	4.30E-10	5.00
KFM09A	20051208 13:43	20051208 14:57	176.00	181.00	3	1	1.42E-08	0	1.17E-08	0	0	2.34E-09	5.00
KFM09A	20051208 15:13	20051208 16:28	181.00	186.00	3	1	1.07E-08	0	8.83E-09	1	0	1.77E-09	5.00
KFM09A	20051208 16:36	20051208 17:51	186.00	191.00	3	1	5.60E-09	0	4.60E-09	0	0	9.21E-10	5.00
KFM09A	20051208 18:03	20051208 18:50	191.00	196.00	3	1	2.64E-10	-1	2.17E-10	0	-1	4.35E-11	5.00

idcode	start_date	stop_date	secup	seclow	test_type	formation_type	spec_capacity_q_s	value_type_q_s	transmissivity_moye	bc_tm	value_type_tm	hydr_cond_moye	formation_width_b
KFM09A	20051208 19:02	20051208 19:47	196.00	201.00	3	1	2.04E-10	-1	1.68E-10	0	-1	3.36E-11	5.00
KFM09A	20051208 19:57	20051208 20:39	201.00	206.00	3	1	2.64E-10	-1	2.17E-10	0	-1	4.35E-11	5.00
KFM09A	20051208 20:58	20051208 21:40	226.00	231.00	3	1	2.64E-10	-1	2.17E-10	0	-1	4.35E-11	5.00
KFM09A	20051208 21:54	20051208 23:08	232.00	237.00	3	1	4.14E-08	0	3.41E-08	0	0	6.81E-09	5.00
KFM09A	20051208 23:21	20051209 00:35	237.00	242.00	3	1	8.31E-08	0	6.84E-08	0	0	1.37E-08	5.00
KFM09A	20051209 08:08	20051209 09:24	240.80	245.80	3	1	1.55E-08	0	1.27E-08	0	0	2.55E-09	5.00
KFM09A	20051221 13:55	20051221 14:35	246.80	251.80	3	1	2.04E-10	-1	1.68E-10	0	-1	3.36E-11	5.00
KFM09A	20051209 09:40	20051209 10:22	251.50	256.50	3	1	2.64E-10	-1	2.17E-10	0	-1	4.35E-11	5.00
KFM09A	20051209 10:34	20051209 11:18	256.50	261.50	3	1	3.27E-10	-1	2.69E-10	0	-1	5.37E-11	5.00
KFM09A	20051209 11:30	20051209 13:22	273.00	278.00	3	1	2.88E-09	0	2.37E-09	0	0	4.73E-10	5.00
KFM09A	20051209 13:34	20051209 14:48	278.00	283.00	3	1	4.63E-09	0	3.81E-09	0	0	7.62E-10	5.00
KFM09A	20051209 15:04	20051209 15:51	283.00	288.00	3	1	2.64E-10	-1	2.17E-10	0	-1	4.35E-11	5.00
KFM09A	20051209 16:00	20051209 17:15	288.00	293.00	3	1	7.71E-10	0	6.35E-10	1	0	1.27E-10	5.00
KFM09A	20051212 08:21	20051212 09:42	293.00	298.00	3	1	1.41E-09	0	1.16E-09	0	0	2.33E-10	5.00
KFM09A	20051221 12:39	20051221 13:28	296.00	301.00	3	1	2.04E-10	-1	1.68E-10	0	-1	3.36E-11	5.00
KFM09A	20051221 11:45	20051221 12:29	301.00	306.00	3	1	2.04E-10	-1	1.68E-10	0	-1	3.36E-11	5.00
KFM09A	20051212 09:58	20051212 10:39	306.00	311.00	3	1	3.25E-10	-1	2.67E-10	0	-1	5.35E-11	5.00
KFM09A	20051212 10:49	20051212 12:33	311.00	316.00	3	1	1.42E-10	-1	1.16E-10	0	-1	2.33E-11	5.00
KFM09A	20051212 12:43	20051212 13:31	316.00	321.00	3	1	2.04E-10	-1	1.67E-10	0	-1	3.35E-11	5.00
KFM09A	20051212 13:44	20051212 15:02	321.00	326.00	3	1	1.46E-08	0	1.20E-08	0	0	2.40E-09	5.00
KFM09A	20051212 15:31	20051212 16:14	346.00	351.00	3	1	3.27E-10	-1	2.69E-10	0	-1	5.37E-11	5.00
KFM09A	20051221 10:04	20051221 11:19	351.00	356.00	3	1	2.36E-09	0	1.94E-09	0	0	3.88E-10	5.00
KFM09A	20051221 08:54	20051221 09:50	356.00	361.00	3	1	2.04E-10	-1	1.67E-10	0	-1	3.35E-11	5.00
KFM09A	20051221 07:28	20051221 08:43	361.00	366.00	3	1	7.97E-10	0	6.56E-10	0	0	1.31E-10	5.00
KFM09A	20051212 16:39	20051212 17:54	363.00	368.00	3	1	5.99E-10	0	4.93E-10	0	0	9.86E-11	5.00
KFM09A	20051213 06:27	20051213 07:24	368.00	373.00	3	1	2.64E-10	-1	2.17E-10	0	-1	4.35E-11	5.00
KFM09A	20051213 07:35	20051213 08:48	371.00	376.00	3	1	7.16E-08	0	5.89E-08	0	0	1.18E-08	5.00
KFM09A	20051213 09:02	20051213 09:58	376.00	381.00	3	1	2.50E-10	-1	2.06E-10	0	-1	4.11E-11	5.00
KFM09A	20051213 10:10	20051213 11:25	381.00	386.00	3	1	2.64E-10	-1	2.17E-10	0	-1	4.34E-11	5.00
KFM09A	20051213 11:57	20051213 13:16	386.00	391.00	3	1	1.15E-07	0	9.43E-08	1	0	1.89E-08	5.00
KFM09A	20051213 13:28	20051213 14:48	391.00	396.00	3	1	7.87E-09	0	6.48E-09	0	0	1.30E-09	5.00
KFM09A	20051213 15:06	20051213 15:49	396.00	401.00	3	1	3.27E-10	-1	2.69E-10	0	-1	5.37E-11	5.00
KFM09A	20051213 16:00	20051213 17:15	401.00	406.00	3	1	2.07E-08	0	1.70E-08	0	0	3.41E-09	5.00
KFM09A	20051213 17:25	20051213 18:18	406.00	411.00	3	1	2.65E-10	-1	2.18E-10	0	-1	4.35E-11	5.00

idcode	start_date	stop_date	secup	seclow	test_type	formation_type	spec_capacity_q_s	value_type_q_s	transmissivity_moye	bc_tm	value_type_tm	hydr_cond_moye	formation_width_b
KFM09A	20051213 18:36	20051213 19:50	411.00	416.00	3	1	1.86E-08	0	1.53E-08	0	0	3.06E-09	5.00
KFM09A	20051213 20:06	20051213 21:22	414.00	419.00	3	1	6.59E-10	0	5.42E-10	0	0	1.08E-10	5.00
KFM09A	20051213 21:32	20051213 22:46	419.00	424.00	3	1	2.73E-09	0	2.25E-09	0	0	4.50E-10	5.00
KFM09A	20051213 22:55	20051214 00:09	421.00	426.00	3	1	2.93E-09	0	2.41E-09	0	0	4.82E-10	5.00
KFM09A	20051214 06:51	20051214 07:59	426.00	431.00	3	1	3.88E-10	-1	3.19E-10	0	-1	6.38E-11	5.00
KFM09A	20051214 08:11	20051214 09:31	431.00	436.00	3	1	7.09E-07	0	5.83E-07	1	0	1.17E-07	5.00
KFM09A	20051214 09:47	20051214 10:29	436.00	441.00	3	1	3.00E-10	-1	2.47E-10	0	-1	4.94E-11	5.00
KFM09A	20051214 10:44	20051214 12:00	441.00	446.00	3	1	9.04E-09	0	7.44E-09	1	0	1.49E-09	5.00
KFM09A	20051214 12:13	20051214 14:04	446.00	451.00	3	1	1.77E-09	0	1.46E-09	0	0	2.92E-10	5.00
KFM09A	20051214 14:22	20051214 15:38	451.00	456.00	3	1	6.35E-10	0	5.22E-10	1	0	1.04E-10	5.00
KFM09A	20051214 15:55	20051214 17:12	456.00	461.00	3	1	3.26E-09	0	2.69E-09	0	0	5.37E-10	5.00
KFM09A	20051214 17:32	20051214 18:15	461.00	466.00	3	1	1.42E-10	-1	1.16E-10	0	-1	2.33E-11	5.00
KFM09A	20051214 18:35	20051214 19:50	471.00	476.00	3	1	2.49E-09	0	2.04E-09	0	0	4.09E-10	5.00
KFM09A	20051214 20:01	20051214 21:23	476.00	481.00	3	1	2.21E-09	0	1.82E-09	0	0	3.64E-10	5.00
KFM09A	20051214 21:40	20051214 22:31	486.00	491.00	3	1	2.64E-10	-1	2.17E-10	0	-1	4.35E-11	5.00
KFM09A	20051214 22:58	20051215 00:12	491.00	496.00	3	1	3.86E-09	0	3.18E-09	0	0	6.35E-10	5.00
KFM09A	20051215 06:33	20051215 07:57	496.00	501.00	3	1	2.95E-09	0	2.43E-09	0	0	4.85E-10	5.00
KFM09A	20051215 08:14	20051215 09:00	501.00	506.00	3	1	2.50E-10	-1	2.06E-10	0	-1	4.11E-11	5.00
KFM09A	20051220 19:00	20051220 20:23	506.00	511.00	3	1	1.06E-09	0	8.76E-10	0	0	1.75E-10	5.00
KFM09A	20051220 20:50	20051220 22:05	511.00	516.00	3	1	1.44E-09	0	1.19E-09	0	0	2.37E-10	5.00
KFM09A	20051220 22:14	20051220 23:28	516.00	521.00	3	1	1.03E-09	0	8.43E-10	0	0	1.69E-10	5.00
KFM09A	20051215 09:25	20051215 10:11	521.00	526.00	3	1	2.64E-10	-1	2.17E-10	0	-1	4.35E-11	5.00
KFM09A	20051215 10:26	20051215 11:07	526.00	531.00	3	1	2.64E-10	-1	2.17E-10	0	-1	4.34E-11	5.00
KFM09A	20051215 11:23	20051215 12:44	531.00	536.00	3	1	1.32E-07	0	1.09E-07	1	0	2.17E-08	5.00
KFM09A	20051215 13:19	20051215 14:03	536.00	541.00	3	1	2.65E-10	-1	2.18E-10	0	-1	4.35E-11	5.00
KFM09A	20051215 14:14	20051215 15:28	541.00	546.00	3	1	4.36E-10	0	3.59E-10	0	0	7.18E-11	5.00
KFM09A	20051220 17:14	20051220 17:58	561.00	566.00	3	1	2.65E-10	-1	2.18E-10	0	-1	4.35E-11	5.00
KFM09A	20051215 16:19	20051215 17:00	606.00	611.00	3	1	2.04E-10	-1	1.68E-10	0	-1	3.36E-11	5.00
KFM09A	20051215 17:19	20051215 18:35	611.00	616.00	3	1	2.03E-08	0	1.67E-08	0	0	3.33E-09	5.00
KFM09A	20051215 18:50	20051215 19:31	616.00	621.00	3	1	2.65E-10	-1	2.18E-10	0	-1	4.35E-11	5.00
KFM09A	20051215 19:44	20051215 21:03	621.00	626.00	3	1	7.07E-09	0	5.82E-09	0	0	1.16E-09	5.00
KFM09A	20051215 21:14	20051215 22:01	626.00	631.00	3	1	2.04E-10	-1	1.67E-10	0	-1	3.35E-11	5.00
KFM09A	20051215 22:08	20051215 23:33	631.00	636.00	3	1	7.00E-10	0	5.76E-10	0	0	1.15E-10	5.00
KFM09A	20051215 23:43	20051216 00:58	636.00	641.00	3	1	6.96E-09	0	5.72E-09	0	0	1.14E-09	5.00

idcode	start_date	stop_date	secup	seclow	test_type	formation_type	spec_capacity_q_s	value_type_q_s	transmissivity_moye	bc_tm	value_type_tm	hydr_cond_moye	formation_width_b
KFM09A	20051216 08:21	20051216 09:36	641.00	646.00	3	1	6.92E-10	0	5.70E-10	0	0	1.14E-10	5.00
KFM09A	20051216 09:55	20051216 10:38	646.00	651.00	3	1	1.42E-10	-1	1.16E-10	0	-1	2.33E-11	5.00
KFM09A	20051216 10:53	20051216 12:10	651.00	656.00	3	1	6.35E-09	0	5.23E-09	0	0	1.05E-09	5.00
KFM09A	20051216 12:21	20051216 13:20	656.00	661.00	3	1	3.27E-10	-1	2.69E-10	0	-1	5.37E-11	5.00
KFM09A	20051216 13:31	20051216 14:14	661.00	666.00	3	1	2.04E-10	-1	1.68E-10	0	-1	3.36E-11	5.00
KFM09A	20051219 08:19	20051219 09:01	731.00	736.00	3	1	2.65E-10	-1	2.18E-10	0	-1	4.35E-11	5.00
KFM09A	20051219 09:15	20051219 09:56	736.00	741.00	3	1	2.65E-10	-1	2.18E-10	0	-1	4.35E-11	5.00
KFM09A	20051219 10:11	20051219 11:30	741.00	746.00	3	1	4.41E-09	0	3.63E-09	0	0	7.26E-10	5.00
KFM09A	20051219 11:44	20051219 12:36	746.00	751.00	3	1	2.65E-10	-1	2.18E-10	0	-1	4.35E-11	5.00
KFM09A	20051219 12:50	20051219 14:05	751.00	756.00	3	1	4.20E-09	0	3.45E-09	0	0	6.91E-10	5.00
KFM09A	20051219 14:20	20051219 15:42	756.00	761.00	3	1	1.03E-08	0	8.44E-09	0	0	1.69E-09	5.00
KFM09A	20051219 15:56	20051219 17:16	761.00	766.00	3	1	5.25E-09	0	4.32E-09	0	0	8.63E-10	5.00
KFM09A	20051220 06:55	20051220 08:10	766.00	771.00	3	1	2.82E-09	0	2.32E-09	0	0	4.64E-10	5.00
KFM09A	20051220 08:29	20051220 09:46	771.00	776.00	3	1	2.53E-09	0	2.08E-09	0	0	4.16E-10	5.00
KFM09A	20051220 10:06	20051220 11:24	776.00	781.00	3	1	5.95E-09	0	4.90E-09	0	0	9.80E-10	5.00
KFM09A	20051220 11:35	20051220 12:58	781.00	786.00	3	1	1.05E-08	0	8.62E-09	0	0	1.72E-09	5.00
KFM09A	20051220 13:11	20051220 14:28	786.00	791.00	3	1	3.41E-08	0	2.81E-08	0	0	5.61E-09	5.00
KFM09A	20051118 13:32	20051118 14:28	506.00 [1)]	606.00	3	1							100.00
KFM09A	20051130 17:10	20051130 18:03	426.00 [1)]	446.00	3	1							20.00
KFM09A	20051207 10:38	20051207 12:39	116.00 [1)]	121.00	3	1							5.00

[1)] Incomplete test, interrupted and re-performed later.

KFM09A plu_s_hole_test_ed1. Right (This result table to SICADA includes more columns which are empty, these columns are not presented here.)

idcode	secup	seclow	transmissivity_tt	value_type_tt	bc_tt	l_measl_q_s	u_measl_q_s	assumed_s	bc_s	ri	ri_index	c	skin	t1	t2	dte1	dte2
KFM09A	106.00	206.00	4.56E-07	0	1	8.9E-10	5.0E-04	4.73E-07	4.73E-07	62.84	-1		-6.79				
KFM09A	206.00	306.00	4.19E-08	0	1	7.5E-10	5.0E-04	1.43E-07	1.43E-07	34.41	0		-2.54	150	1800		
KFM09A	306.00	406.00	1.29E-07	0	1	7.8E-10	5.0E-04	2.51E-07	2.51E-07	45.55	1		-5.13				
KFM09A	406.00	506.00	1.14E-06	0	0	8.0E-10	5.0E-04	5.75E-07	5.75E-07	69.31	1		-5.76				
KFM09A	506.00	606.00	3.17E-07	0	0	7.4E-10	5.0E-04	2.35E-07	2.35E-07	44.31	1		-5.12				
KFM09A	606.00	706.00	1.64E-08	0	1	8.0E-10	5.0E-04	8.95E-08	8.95E-08	12.82	1	3.24E-10	-3.54	20	400		
KFM09A	691.00	791.00	6.92E-09	0	1	9.3E-10	5.0E-04	5.82E-08	5.82E-08	22.07	-1		-5.60				
KFM09A	106.00	126.00	2.51E-07	0	1	7.7E-10	5.0E-04	3.51E-07	3.51E-07	43.97	0		-3.14	100	1200		
KFM09A	126.00	146.00	5.35E-07	0	1	7.6E-10	5.0E-04	5.12E-07	5.12E-07	53.12	0		-4.71	550	1200		
KFM09A	146.00	166.00	4.22E-08	0	1	8.9E-10	5.0E-04	1.44E-07	1.44E-07	28.35	0						
KFM09A	166.00	186.00	6.19E-07	0	1	8.6E-10	5.0E-04	5.51E-07	5.51E-07	55.49	-1		-5.02				
KFM09A	186.00	206.00	3.28E-09	0	1	5.5E-10	5.0E-04	4.01E-08	4.01E-08	14.99	-1	5.75E-11	-1.13				
KFM09A	206.00	226.00		-1	0	2.6E-10	5.0E-04										
KFM09A	226.00	246.00	4.65E-08	0	1	7.9E-10	5.0E-04	1.51E-07	1.51E-07	28.85	0		-0.24	300	1200		
KFM09A	238.00	258.00	4.90E-09	0	1	7.8E-10	5.0E-04	4.90E-08	4.90E-08	16.43	0	5.01E-10	-3.44	200	1200		
KFM09A	258.00	278.00	1.46E-09	0	1	8.0E-10	5.0E-04	2.68E-08	2.68E-08	12.12	0	7.53E-11	-3.09				
KFM09A	278.00	298.00	2.59E-09	0	1	7.7E-10	5.0E-04	3.56E-08	3.56E-08	7.01	0		-3.42	10	300		
KFM09A	286.00	306.00	1.39E-09	0	1	7.7E-10	5.0E-04	2.61E-08	2.61E-08	11.95	-1		-3.56				
KFM09A	306.00	326.00	3.12E-08	0	1	8.2E-10	5.0E-04	1.24E-07	1.24E-07	7.53	1		-2.23	20	100		
KFM09A	326.00	346.00	4.17E-10	0	1	8.1E-10	5.0E-04	1.43E-08	1.43E-08	8.87	0		-3.21	30	1200		
KFM09A	346.00	366.00	7.25E-10	0	1	8.0E-10	5.0E-04	1.88E-08	1.88E-08	10.19	0	5.57E-11	-3.71	300	1200		
KFM09A	366.00	386.00	2.44E-08	0	1	8.1E-10	5.0E-04	1.09E-07	1.09E-07	24.54	0		-4.23	200	1200		
KFM09A	386.00	406.00	4.53E-08	0	0	8.2E-10	5.0E-04	2.60E-07	2.60E-07	38.40	1		-6.01				
KFM09A	406.00	426.00	2.31E-08	0	0	8.2E-10	5.0E-04	1.00E-07	1.00E-07	23.85	1		-1.36				
KFM09A	426.00	446.00	1.26E-06	0	0	7.4E-10	5.0E-04	6.49E-07	6.49E-07	60.65	1		-5.73				
KFM09A	446.00	466.00	1.97E-09	0	1	7.1E-10	5.0E-04	3.11E-08	3.11E-08	13.08	0		-1.90	200	1200		
KFM09A	466.00	486.00	1.86E-09	0	1	9.5E-10	5.0E-04	3.02E-08	3.02E-08	8.32	1		-2.90			100	500

idcode	secup	seclow	transmissivity_tt	value_type_tt	bc_tt	l_measl_q_s	u_measl_q_s	assumed_s	bc_s	ri	ri_index	c	skin	t1	t2	dte1	dte2
KFM09A	486.00	506.00	1.00E-09	0	1	8.0E-10	5.0E-04	2.21E-08	2.21E-08	11.14	1						
KFM09A	506.00	526.00	2.06E-10	0	1	8.6E-10	5.0E-04	1.00E-08	1.00E-08	7.44	0		-5.47				
KFM09A	526.00	546.00	4.12E-07	0	0	8.0E-10	5.0E-04	2.67E-07	2.67E-07	38.65	0		-4.72			100	1400
KFM09A	545.00	565.00		-1	0	2.6E-10	5.0E-04										
KFM09A	566.00	586.00		-1	0	2.6E-10	5.0E-04										
KFM09A	586.00	606.00		-1	0	2.6E-10	5.0E-04										
KFM09A	606.00	626.00	1.28E-08	0	1	8.2E-10	5.0E-04	7.92E-08	7.92E-08	10.44	1		-3.99	50	300		
KFM09A	626.00	646.00	2.70E-09	0	1	7.9E-10	5.0E-04	3.64E-08	3.64E-08	14.16	-1	7.25E-11	-1.83				
KFM09A	646.00	666.00	4.21E-09	0	1	8.0E-10	5.0E-04	4.54E-08	4.54E-08	15.82	0		-0.94	50	1200		
KFM09A	666.00	686.00	2.40E-11	0	0	2.8E-10	5.0E-04	1.83E-08	1.83E-08	10.05	1		-6.35				
KFM09A	686.00	706.00	9.24E-11	0	1	2.6E-10	5.0E-04	6.73E-09	6.73E-09	6.10	1						
KFM09A	691.00	711.00		-1	0	1.9E-10	5.0E-04										
KFM09A	711.00	731.00		-1	0	1.9E-10	5.0E-04										
KFM09A	731.00	751.00	3.41E-09	0	1	7.7E-10	5.0E-04	4.09E-08	4.09E-08	15.03	-1	6.28E-11	0.71				
KFM09A	751.00	771.00	3.50E-09	0	1	8.0E-10	5.0E-04	4.14E-08	4.14E-08	15.22	1		-5.20				
KFM09A	771.00	791.00	6.54E-09	0	1	7.6E-10	5.0E-04	5.66E-08	5.66E-08	17.81	-1	1.41E-09	-5.10				
KFM09A	106.00	111.00	1.32E-08	0	1	8.1E-10	5.0E-04	8.04E-08	8.04E-08	21.26	-1		-2.89				
KFM09A	111.00	116.00	1.04E-09	0	1	7.9E-10	5.0E-04	2.26E-08	2.26E-08	11.26	-1		-3.22				
KFM09A	116.00	121.00	4.25E-08	0	1	8.2E-10	5.0E-04	1.44E-07	1.44E-07	16.28	0		-4.44	50	400		
KFM09A	121.00	126.00	1.69E-07	0	1	9.2E-10	5.0E-04	2.88E-07	2.88E-07	21.51	0		-3.66	80	350		
KFM09A	126.00	131.00	6.83E-10	0	1	8.1E-10	5.0E-04	1.83E-08	1.83E-08	10.02	1						
KFM09A	128.00	133.00	2.69E-07	0	1	7.5E-10	5.0E-04	3.63E-07	3.63E-07	45.08	-1		-4.87				
KFM09A	133.00	138.00	2.10E-07	0	1	7.0E-10	5.0E-04	3.21E-07	3.21E-07	41.99	0		-4.48				
KFM09A	138.00	143.00	8.19E-09	0	1	8.1E-10	5.0E-04	6.33E-08	6.33E-08	18.68	0		-2.86	100	1200		
KFM09A	141.00	146.00	2.77E-08	0	1	7.3E-10	5.0E-04	1.16E-07	1.16E-07	25.58	0		-3.50				
KFM09A	146.00	151.00	7.80E-09	0	1	7.2E-10	5.0E-04	6.18E-08	6.18E-08	18.36	1						
KFM09A	151.00	156.00		-1	0	2.6E-10	5.0E-04										
KFM09A	156.00	161.00	3.44E-08	0	1	7.9E-10	5.0E-04	1.30E-07	1.30E-07	26.90	0						
KFM09A	161.00	166.00	4.85E-09	0	0	9.2E-10	5.0E-04	4.75E-08	4.75E-08	16.31	-1		0.00				
KFM09A	166.00	171.00	1.13E-06	0	1	9.1E-10	5.0E-04	7.44E-07	7.44E-07	64.48	-1		-3.98				
KFM09A	171.00	176.00		0	0	7.9E-10	5.0E-04	3.25E-08	3.25E-08	13.46							

idcode	secup	seclow	transmissivity_tt	value_type_tt	bc_tt	l_measl_q_s	u_measl_q_s	assumed_s	bc_s	ri	ri_index	c	skin	t1	t2	dte1	dte2
KFM09A	176.00	181.00	4.78E-09	0	1	8.2E-10	5.0E-04	4.84E-08	4.84E-08	16.33	0	7.41E-11	-3.96	50	1200		
KFM09A	181.00	186.00		0	0	7.2E-10	5.0E-04	6.58E-08	6.58E-08	19.20							
KFM09A	186.00	191.00	4.58E-09	0	1	7.6E-10	5.0E-04	4.74E-08	4.74E-08	16.16	0	2.51E-11	-0.92	40	1200		
KFM09A	191.00	196.00		-1	0	2.6E-10	5.0E-04										
KFM09A	196.00	201.00		-1	0	2.0E-10	5.0E-04										
KFM09A	201.00	206.00		-1	0	2.6E-10	5.0E-04										
KFM09A	226.00	231.00		-1	0	2.6E-10	5.0E-04										
KFM09A	232.00	237.00	6.48E-08	0	1	8.2E-10	5.0E-04	1.78E-07	1.78E-07	31.56	-1		3.62				
KFM09A	237.00	242.00	7.88E-08	0	1	8.2E-10	5.0E-04	1.96E-07	1.96E-07	32.90	0		-0.90	50	1200		
KFM09A	240.80	245.80	4.95E-09	0	1	8.0E-10	5.0E-04	4.92E-08	4.92E-08	16.60	-1		-3.88				
KFM09A	246.80	251.80		-1	0	2.0E-10	5.0E-04										
KFM09A	251.50	256.50		-1	0	2.6E-10	5.0E-04										
KFM09A	256.50	261.50		-1	0	3.3E-10	5.0E-04										
KFM09A	273.00	278.00	2.00E-09	0	1	7.0E-10	5.0E-04	3.13E-08	3.13E-08	5.36	0	3.85E-11	-2.81	30	200		
KFM09A	278.00	283.00	1.47E-09	0	1	7.9E-10	5.0E-04	2.68E-08	2.68E-08	7.84	1		-4.20	60	500		
KFM09A	283.00	288.00		-1	0	2.6E-10	5.0E-04										
KFM09A	288.00	293.00	6.90E-11	0	0	4.9E-10	5.0E-04	1.76E-08	1.76E-08	9.95	0	1.73E-11	-5.42				
KFM09A	293.00	298.00	6.79E-10	0	1	7.0E-10	5.0E-04	1.82E-08	1.82E-08	10.02	0	1.72E-11	-2.68	10	1200		
KFM09A	296.00	301.00		-1	0	2.0E-10	5.0E-04										
KFM09A	301.00	306.00		-1	0	2.0E-10	5.0E-04										
KFM09A	306.00	311.00		-1	0	3.3E-10	5.0E-04										
KFM09A	311.00	316.00		-1	0	1.4E-10	5.0E-04										
KFM09A	316.00	321.00		-1	0	2.0E-10	5.0E-04										
KFM09A	321.00	326.00	2.01E-08	0	1	8.1E-10	5.0E-04	9.92E-08	9.92E-08	9.54	1		-3.28	30	200		
KFM09A	346.00	351.00		-1	0	3.3E-10	5.0E-04										
KFM09A	351.00	356.00	1.42E-09	0	1	7.8E-10	5.0E-04	2.63E-08	2.63E-08	12.05	0	1.74E-11	-1.68	30	1200		
KFM09A	356.00	361.00		-1	0	2.0E-10	5.0E-04										
KFM09A	361.00	366.00	2.32E-10	0	1	1.9E-10	5.0E-04	1.07E-08	1.07E-08	7.67	0		-2.96	20	1200		
KFM09A	363.00	368.00	2.32E-10	0	1	2.5E-10	5.0E-04	1.07E-08	1.07E-08	7.66	0	1.84E-11	-2.93	30	1200		
KFM09A	368.00	373.00		-1	0	2.6E-10	5.0E-04										
KFM09A	371.00	376.00	3.05E-08	0	1	8.1E-10	5.0E-04	1.22E-07	1.22E-07	18.36	0		-5.05	100	600		
KFM09A	376.00	381.00		-1	0	2.5E-10	5.0E-04										

idcode	secup	seclow	transmissivity_tt	value_type_tt	bc_tt	l_measl_q_s	u_measl_q_s	assumed_s	bc_s	ri	ri_index	c	skin	t1	t2	dte1	dte2
KFM09A	381.00	386.00		-1	0	2.6E-10	5.0E-04										
KFM09A	386.00	391.00	8.27E-08	0	0	7.7E-10	5.0E-04	2.15E-07	2.15E-07	34.73	1						
KFM09A	391.00	396.00	1.42E-09	0	1	7.9E-10	5.0E-04	2.64E-08	2.64E-08	6.03	-1		-4.46	20	300		
KFM09A	396.00	401.00		-1	0	3.3E-10	5.0E-04										
KFM09A	401.00	406.00	2.04E-08	0	1	8.1E-10	5.0E-04	1.00E-07	1.00E-07	10.71	1	1.30E-10	-0.66	100	250		
KFM09A	406.00	411.00		-1	0	2.6E-10	5.0E-04										
KFM09A	411.00	416.00	2.37E-08	0	1	8.4E-10	5.0E-04	1.08E-07	1.08E-07	7.03	0		-1.98	20	100		
KFM09A	414.00	419.00	3.17E-10	0	1	2.7E-10	5.0E-04	1.25E-08	1.25E-08	8.29	0		-1.85	30	1200		
KFM09A	419.00	424.00	1.95E-09	0	1	8.0E-10	5.0E-04	3.09E-08	3.09E-08	9.23	0	1.61E-11	-1.79	30	600		
KFM09A	421.00	426.00	1.68E-09	0	1	8.5E-10	5.0E-04	2.87E-08	2.87E-08	12.57	0	1.90E-11	-2.50	20	1200		
KFM09A	426.00	431.00		-1	0	3.9E-10	5.0E-04										
KFM09A	431.00	436.00	1.51E-06	0	0	7.3E-10	5.0E-04	5.35E-07	5.35E-07	54.77	1		-5.47				
KFM09A	436.00	441.00		-1	0	3.0E-10	5.0E-04										
KFM09A	441.00	446.00	4.01E-08	0	0	7.2E-10	5.0E-04	6.04E-08	6.04E-08	18.44	1		-6.42				
KFM09A	446.00	451.00	8.19E-10	0	1	7.9E-10	5.0E-04	2.00E-08	2.00E-08	10.51	1		-6.02				
KFM09A	451.00	456.00	1.57E-10	0	0	2.7E-10	5.0E-04	1.60E-08	1.60E-08	9.49	0		-3.30				
KFM09A	456.00	461.00	2.00E-09	0	1	8.1E-10	5.0E-04	3.13E-08	3.13E-08	9.29	1		-1.04	20	600		
KFM09A	461.00	466.00		-1	0	1.4E-10	5.0E-04										
KFM09A	471.00	476.00	2.93E-10	0	1	7.8E-10	5.0E-04	1.20E-08	1.20E-08	8.22	-1		-5.33				
KFM09A	476.00	481.00	1.65E-09	0	1	8.6E-10	5.0E-04	2.84E-08	2.84E-08	3.61	1		-1.97	20	100		
KFM09A	486.00	491.00		-1	0	2.6E-10	5.0E-04										
KFM09A	491.00	496.00	1.58E-09	0	1	8.2E-10	5.0E-04	2.78E-08	2.78E-08	12.38	0	7.15E-11	-3.36	60	1200		
KFM09A	496.00	501.00	2.97E-10	0	1	7.9E-10	5.0E-04	1.21E-08	1.21E-08	8.15	1						
KFM09A	501.00	506.00		-1	0	2.5E-10	5.0E-04										
KFM09A	506.00	511.00	4.79E-10	0	1	2.6E-10	5.0E-04	1.53E-08	1.53E-08	9.28	-1		0.00				
KFM09A	511.00	516.00	4.65E-10	0	1	8.1E-10	5.0E-04	1.51E-08	1.51E-08	9.19	-1		-1.98				
KFM09A	516.00	521.00	2.41E-10	0	1	4.1E-10	5.0E-04	1.09E-08	1.09E-08	7.81	0	1.56E-11	-3.69				
KFM09A	521.00	526.00		-1	0	2.6E-10	5.0E-04										
KFM09A	526.00	531.00		-1	0	2.6E-10	5.0E-04										
KFM09A	531.00	536.00	4.23E-07	0	0	7.6E-10	5.0E-04	2.31E-07	2.31E-07	35.98	1		-4.75			100	5000
KFM09A	536.00	541.00		-1	0	2.6E-10	5.0E-04										
KFM09A	541.00	546.00	3.09E-09	0	1	2.7E-10	5.0E-04	3.89E-08	3.89E-08	2.99	1		-3.26	10	50		

idcode	secup	seclow	transmissivity_tt	value_type_tt	bc_tt	l_measl_q_s	u_measl_q_s	assumed_s	bc_s	ri	ri_index	c	skin	t1	t2	dte1	dte2
KFM09A	561.00	566.00		-1	0	2.6E-10	5.0E-04										
KFM09A	606.00	611.00		-1	0	2.0E-10	5.0E-04										
KFM09A	611.00	616.00	1.56E-08	0	1	8.5E-10	5.0E-04	8.75E-08	8.75E-08	8.96	1		-3.50	30	200		
KFM09A	616.00	621.00		-1	0	2.6E-10	5.0E-04										
KFM09A	621.00	626.00	2.38E-09	0	1	7.7E-10	5.0E-04	3.41E-08	3.41E-08	7.92	1		-4.28	40	400		
KFM09A	626.00	631.00		-1	0	2.0E-10	5.0E-04										
KFM09A	631.00	636.00	2.58E-10	0	1	3.2E-10	5.0E-04	1.12E-08	1.12E-08	2.27	1	1.71E-11	-3.98	30	100		
KFM09A	636.00	641.00	6.19E-09	0	1	8.6E-10	5.0E-04	5.51E-08	5.51E-08	17.42	0	2.64E-11	0.08	20	1200		
KFM09A	641.00	646.00	9.03E-11	0	1	1.5E-10	5.0E-04	6.65E-09	6.65E-09	6.11	0		-4.31				
KFM09A	646.00	651.00		-1	0	1.4E-10	5.0E-04										
KFM09A	651.00	656.00	3.71E-09	0	1	8.4E-10	5.0E-04	4.26E-08	4.26E-08	15.33	0		-2.52	40	1200		
KFM09A	656.00	661.00		-1	0	3.3E-10	5.0E-04										
KFM09A	661.00	666.00															
KFM09A	731.00	736.00		-1	0	2.6E-10	5.0E-04										
KFM09A	736.00	741.00		-1	0	2.6E-10	5.0E-04										
KFM09A	741.00	746.00	2.75E-09	0	1	8.3E-10	5.0E-04	3.67E-08	3.67E-08	7.11	0	1.92E-11	-0.91	40	300		
KFM09A	746.00	751.00		-1	0	2.6E-10	5.0E-04										
KFM09A	751.00	756.00	1.04E-09	0	1	8.8E-10	5.0E-04	2.26E-08	2.26E-08	8.51	-1			200	700		
KFM09A	756.00	761.00	5.14E-09	0	1	7.9E-10	5.0E-04	5.02E-08	5.02E-08	16.63	0		-3.58	70	1200		
KFM09A	761.00	766.00	7.00E-10	0	1	8.1E-10	5.0E-04	1.85E-08	1.85E-08	10.23	-1		-5.02				
KFM09A	766.00	771.00	7.66E-10	0	1	8.6E-10	5.0E-04	1.94E-08	1.94E-08	10.43	-1	7.66E-11	-3.86				
KFM09A	771.00	776.00	6.84E-10	0	1	7.0E-10	5.0E-04	1.83E-08	1.83E-08	10.15	-1		-3.54				
KFM09A	776.00	781.00	1.88E-09	0	1	8.6E-10	5.0E-04	3.04E-08	3.04E-08	12.93	0	7.00E-11	-3.69	100	1200		
KFM09A	781.00	786.00	6.16E-10	0	1	9.4E-10	5.0E-04	1.74E-08	1.74E-08	9.89	-1		-5.89				
KFM09A	786.00	791.00	6.36E-09	0	1	8.0E-10	5.0E-04	5.58E-08	5.58E-08	17.71	0	6.30E-10	-4.52				

KFM09A plu_s_hole_test_obs (This result table to SICADA includes more columns which are empty, these columns are not presented here.)

idcode	start_date	stop_date	secup	seclow	obs_secup	obs_seclow	pi_above	pp_above	pf_above	pi_below	pp_below	pf_below	comments
KFM09A	20051117 16:09	20051117 17:59	106.00	206.00	7.79	105.00	938.78	938.36	938.36				
KFM09A	20051117 16:09	20051117 17:59	106.00	206.00	207.00	799.67				1792.58	1793.95	1794.77	
KFM09A	20051117 19:03	20051117 20:53	206.00	306.00	7.79	205.00	944.46	943.92	943.92				
KFM09A	20051117 19:03	20051117 20:53	206.00	306.00	307.00	799.67				2608.72	2610.37	2611.60	
KFM09A	20051117 21:47	20051117 23:36	306.00	406.00	7.79	305.00	910.90	910.90	910.36				
KFM09A	20051117 21:47	20051117 23:36	306.00	406.00	407.00	799.67				3403.22	3405.41	3407.06	
KFM09A	20051118 09:59	20051118 11:49	406.00	506.00	7.79	405.00	858.19	857.91	858.05				
KFM09A	20051118 09:59	20051118 11:49	406.00	506.00	507.00	799.67				4184.43	4188.82	4191.57	
KFM09A	20051121 12:52	20051121 15:13	506.00	606.00	7.79	505.00	818.01	815.81	821.72				
KFM09A	20051121 12:52	20051121 15:13	506.00	606.00	607.00	799.67				4947.58	4948.68	4949.22	
KFM09A	20051121 06:14	20051121 08:03	606.00	706.00	7.79	605.00	693.26	692.84	692.84				
KFM09A	20051121 06:14	20051121 08:03	606.00	706.00	707.00	799.67				5659.22	5661.27	5662.50	
KFM09A	20051121 08:51	20051121 10:40	691.00	791.00	7.79	690.00	586.37	585.41	599.74				
KFM09A	20051121 08:51	20051121 10:40	691.00	791.00	792.00	799.67				6238.42	6243.76	6242.12	
KFM09A	20051128 16:44	20051128 18:19	106.00	126.00	7.79	105.00	943.46	943.32	943.32				
KFM09A	20051128 16:44	20051128 18:19	106.00	126.00	127.00	799.67				1128.14	1129.23	1129.23	
KFM09A	20051129 06:29	20051129 07:43	126.00	146.00	7.79	125.00	961.18	964.76	961.18				
KFM09A	20051129 06:29	20051129 07:43	126.00	146.00	147.00	799.67				1299.06	1299.61	1298.52	
KFM09A	20051129 08:20	20051129 09:35	146.00	166.00	7.79	145.00	958.79	962.51	960.86				
KFM09A	20051129 08:20	20051129 09:35	146.00	166.00	167.00	799.67				1463.96	1464.92	1463.96	
KFM09A	20051129 10:00	20051129 11:15	166.00	186.00	7.79	165.00	954.47	957.78	953.91				
KFM09A	20051129 10:00	20051129 11:15	166.00	186.00	187.00	799.67				1633.25	1633.79	1633.79	
KFM09A	20051129 12:14	20051129 13:31	186.00	206.00	7.79	185.00	948.78	953.60	951.95				
KFM09A	20051129 12:14	20051129 13:31	186.00	206.00	207.00	799.67				1798.01	1798.56	1799.24	
KFM09A	20051129 14:01	20051129 14:47	206.00	226.00	7.79	205.00	947.77	948.33	949.42				
KFM09A	20051129 14:01	20051129 14:47	206.00	226.00	227.00	799.67				1963.32	1963.59	1963.59	

idcode	start_date	stop_date	secup	seclow	obs_secup	obs_seclow	pi_above	pp_above	pf_above	pi_below	pp_below	pf_below	comments
KFM09A	20051129 15:38	20051129 16:56	226.00	246.00	7.79	225.00	938.22	943.45	940.29				
KFM09A	20051129 15:38	20051129 16:56	226.00	246.00	247.00	799.67				2128.49	2129.03	2129.59	
KFM09A	20051129 17:18	20051129 18:37	238.00	258.00	7.79	237.00	934.81	934.39	937.01				
KFM09A	20051129 17:18	20051129 18:37	238.00	258.00	259.00	799.67				2226.01	2226.82	2227.10	
KFM09A	20051129 18:58	20051129 20:17	258.00	278.00	7.79	257.00	933.38	929.52	930.62				
KFM09A	20051129 18:58	20051129 20:17	258.00	278.00	279.00	799.67				2389.81	2390.36	2390.91	
KFM09A	20051129 21:03	20051129 22:25	278.00	298.00	7.79	277.00	927.00	925.89	922.04				
KFM09A	20051129 21:03	20051129 22:25	278.00	298.00	299.00	799.67				2549.77	2550.87	2551.42	
KFM09A	20051129 22:41	20051129 23:57	286.00	306.00	7.79	285.00	921.14	919.49	921.14				
KFM09A	20051129 22:41	20051129 23:57	286.00	306.00	307.00	799.67				2611.00	2612.23	2613.33	
KFM09A	20051130 06:29	20051130 07:48	306.00	326.00	7.79	305.00	914.76	916.00	914.21				
KFM09A	20051130 06:29	20051130 07:48	306.00	326.00	327.00	799.67				2774.38	2774.38	2774.94	
KFM09A	20051130 08:16	20051130 09:35	326.00	346.00	7.79	325.00	903.28	903.97	905.07				
KFM09A	20051130 08:16	20051130 09:35	326.00	346.00	347.00	799.67				2932.72	2933.27	2933.81	
KFM09A	20051130 10:06	20051130 11:22	346.00	366.00	7.79	345.00	895.93	894.56	897.03				
KFM09A	20051130 10:06	20051130 11:22	346.00	366.00	367.00	799.67				3093.23	3093.78	3093.78	
KFM09A	20051130 12:06	20051130 13:23	366.00	386.00	7.79	365.00	883.49	886.79	888.44				
KFM09A	20051130 12:06	20051130 13:23	366.00	386.00	387.00	799.67				3250.46	3251.42	3252.11	
KFM09A	20051130 13:50	20051130 15:08	386.00	406.00	7.79	385.00	872.14	873.66	873.80				
KFM09A	20051130 13:50	20051130 15:08	386.00	406.00	407.00	799.67				3407.28	3408.78	3409.33	
KFM09A	20051130 15:30	20051130 16:47	406.00	426.00	7.79	405.00	865.21	864.11	865.21				
KFM09A	20051130 15:30	20051130 16:47	406.00	426.00	427.00	799.67				3564.37	3565.47	3566.56	
KFM09A	20051130 18:18	20051130 19:38	426.00	446.00	7.79	425.00	852.77	854.83	853.87				
KFM09A	20051130 18:18	20051130 19:38	426.00	446.00	447.00	799.67				3730.38	3732.01	3732.57	
KFM09A	20051130 20:03	20051130 21:45	446.00	466.00	7.79	445.00	840.32	842.80	836.47				
KFM09A	20051130 20:03	20051130 21:45	446.00	466.00	467.00	799.67				3887.60	3888.28	3888.69	
KFM09A	20051130 22:03	20051130 23:20	466.00	486.00	7.79	465.00	825.13	824.58	827.33				
KFM09A	20051130 22:03	20051130 23:20	466.00	486.00	487.00	799.67				4036.74	4038.80	4040.45	
KFM09A	20051201 08:06	20051201 09:34	486.00	506.00	7.79	485.00	813.24	813.93	811.59				
KFM09A	20051201 08:06	20051201 09:34	486.00	506.00	507.00	799.67				4187.67	4189.46	4190.55	
KFM09A	20051201 10:01	20051201 11:22	506.00	526.00	7.79	505.00	794.46	797.48	798.04				
KFM09A	20051201 10:01	20051201 11:22	506.00	526.00	527.00	799.67				4340.66	4342.17	4343.40	

idcode	start_date	stop_date	secup	seclow	obs_secup	obs_seclow	pi_above	pp_above	pf_above	pi_below	pp_below	pf_below	comments
KFM09A	20051201 11:41	20051201 13:46	526.00	546.00	7.79	525.00	776.23	775.68	775.68				
KFM09A	20051201 11:41	20051201 13:46	526.00	546.00	547.00	799.67				4497.61	4497.88	4498.44	
KFM09A	20051201 14:21	20051201 15:09	545.00	565.00	7.79	544.00	843.61	843.06	842.92				
KFM09A	20051201 14:21	20051201 15:09	545.00	565.00	566.00	799.67				4637.86	4638.13	4638.13	
KFM09A	20051201 15:34	20051201 16:17	566.00	586.00	7.79	565.00	823.27	823.14	823.14				
KFM09A	20051201 15:34	20051201 16:17	566.00	586.00	587.00	799.67				4793.72	4793.72	4794.27	
KFM09A	20051202 07:55	20051202 08:37	586.00	606.00	7.79	585.00	802.83	802.56	802.42				
KFM09A	20051202 07:55	20051202 08:37	586.00	606.00	607.00	799.67				4940.00	4940.00	4940.54	
KFM09A	20051202 08:58	20051202 10:22	606.00	626.00	7.79	605.00	782.13	781.72	782.27				
KFM09A	20051202 08:58	20051202 10:22	606.00	626.00	627.00	799.67				5089.54	5090.10	5090.64	
KFM09A	20051202 10:43	20051202 12:05	626.00	646.00	7.79	625.00	676.40	675.72	675.99				
KFM09A	20051202 10:43	20051202 12:05	626.00	646.00	647.00	799.67				5235.55	5236.37	5236.93	
KFM09A	20051202 13:12	20051202 14:35	646.00	666.00	7.79	645.00	738.51	737.54	738.10				
KFM09A	20051202 13:12	20051202 14:35	646.00	666.00	667.00	799.67				5379.90	5381.00	5381.55	
KFM09A	20051202 14:57	20051202 16:13	666.00	686.00	7.79	665.00	629.20	628.93	628.51				
KFM09A	20051202 14:57	20051202 16:13	666.00	686.00	687.00	799.67				5521.80	5522.48	5522.89	
KFM09A	20051205 08:22	20051205 09:53	686.00	706.00	7.79	685.00	690.62	692.27	693.92				
KFM09A	20051205 08:22	20051205 09:53	686.00	706.00	707.00	799.67				5660.53	5661.22	5661.49	
KFM09A	20051205 10:10	20051205 11:12	691.00	711.00	7.79	690.00	601.52	600.28	601.38				
KFM09A	20051205 10:10	20051205 11:12	691.00	711.00	712.00	799.67				5695.46	5696.01	5696.01	
KFM09A	20051205 12:46	20051205 13:30	711.00	731.00	7.79	710.00	573.37	572.97	571.87				
KFM09A	20051205 12:46	20051205 13:30	711.00	731.00	732.00	799.67				5832.14	5832.56	5832.42	
KFM09A	20051205 13:49	20051205 15:12	731.00	751.00	7.79	730.00	542.48	542.89	538.49				
KFM09A	20051205 13:49	20051205 15:12	731.00	751.00	752.00	799.67				5968.29	5968.56	5968.83	
KFM09A	20051205 15:30	20051205 16:54	751.00	771.00	7.79	750.00	507.99	507.85	508.41				
KFM09A	20051205 15:30	20051205 16:54	751.00	771.00	772.00	799.67				6104.56	6104.70	6105.24	
KFM09A	20051205 18:09	20051205 19:26	771.00	791.00	7.79	770.00	475.99	476.68	477.78				
KFM09A	20051205 18:09	20051205 19:26	771.00	791.00	792.00	799.67				6234.67	6240.97	6238.92	
KFM09A	20051207 07:32	20051207 08:52	106.00	111.00	7.79	105.00	971.33	973.12	970.79				
KFM09A	20051207 07:32	20051207 08:52	106.00	111.00	112.00	799.67				1005.56	1004.74	1004.87	

idcode	start_date	stop_date	secup	seclow	obs_secup	obs_seclow	pi_above	pp_above	pf_above	pi_below	pp_below	pf_below	comments
KFM09A	20051207 09:08	20051207 10:24	111.00	116.00	7.79	110.00	967.12	971.94	972.08				
KFM09A	20051207 09:08	20051207 10:24	111.00	116.00	117.00	799.67				1047.60	1046.51	1045.41	
KFM09A	20051221 15:48	20051208 17:51	116.00	121.00	7.79	115.00	964.65	964.65	964.65				
KFM09A	20051221 15:48	20051208 17:51	116.00	121.00	122.00	799.67				1078.83	1079.93	1080.48	
KFM09A	20051207 12:52	20051207 14:09	121.00	126.00	7.79	120.00	966.41	970.82	969.72				
KFM09A	20051207 12:52	20051207 14:09	121.00	126.00	127.00	799.67				1131.42	1131.42	1130.87	
KFM09A	20051207 14:26	20051207 16:04	126.00	131.00	7.79	125.00	968.12	965.50	967.15				
KFM09A	20051207 14:26	20051207 16:04	126.00	131.00	132.00	799.67				1172.51	1173.06	1172.51	
KFM09A	20051207 16:21	20051207 17:40	128.00	133.00	7.79	127.00	969.68	969.00	969.54				
KFM09A	20051207 16:21	20051207 17:40	128.00	133.00	134.00	799.67				1189.09	1194.43	1191.69	
KFM09A	20051207 17:58	20051207 19:16	133.00	138.00	7.79	132.00	965.88	969.75	966.44				
KFM09A	20051207 17:58	20051207 19:16	133.00	138.00	139.00	799.67				1231.68	1232.23	1231.68	
KFM09A	20051207 19:42	20051207 21:13	138.00	143.00	7.79	137.00	967.19	968.29	965.53				
KFM09A	20051207 19:42	20051207 21:13	138.00	143.00	144.00	799.67				1272.77	1272.49	1272.77	
KFM09A	20051207 21:27	20051207 22:45	141.00	146.00	7.79	140.00	962.51	962.64	963.33				
KFM09A	20051207 21:27	20051207 22:45	141.00	146.00	147.00	799.67				1297.69	1297.97	1297.42	
KFM09A	20051207 23:02	20051208 00:17	146.00	151.00	7.79	145.00	962.42	962.98	962.42				
KFM09A	20051207 23:02	20051208 00:17	146.00	151.00	152.00	799.67				1339.05	1339.19	1339.05	
KFM09A	20051208 06:16	20051208 06:59	151.00	156.00	7.79	150.00	965.79	965.51	965.37				
KFM09A	20051208 06:16	20051208 06:59	151.00	156.00	157.00	799.67				1381.24	1381.24	1381.24	
KFM09A	20051208 07:10	20051208 08:26	156.00	161.00	7.79	155.00	965.57	965.57	960.62				
KFM09A	20051208 07:10	20051208 08:26	156.00	161.00	162.00	799.67				1422.32	1423.42	1423.42	
KFM09A	20051208 08:36	20051208 09:52	161.00	166.00	7.79	160.00	964.66	962.46	964.66				
KFM09A	20051208 08:36	20051208 09:52	161.00	166.00	167.00	799.67				1464.10	1463.83	1463.42	
KFM09A	20051208 10:03	20051208 11:19	166.00	171.00	7.79	165.00	958.10	962.65	962.65				
KFM09A	20051208 10:03	20051208 11:19	166.00	171.00	172.00	799.67				1508.88	1509.43	1508.88	
KFM09A	20051208 12:12	20051208 13:29	171.00	176.00	7.79	170.00	958.45	958.45	958.45				
KFM09A	20051208 12:12	20051208 13:29	171.00	176.00	177.00	799.67				1549.84	1550.52	1550.52	
KFM09A	20051208 13:43	20051208 14:57	176.00	181.00	7.79	175.00	957.95	957.53	957.53				
KFM09A	20051208 13:43	20051208 14:57	176.00	181.00	182.00	799.67				1590.52	1591.06	1591.61	
KFM09A	20051208 15:13	20051208 16:28	181.00	186.00	7.79	180.00	956.63	956.08	956.08				
KFM09A	20051208 15:13	20051208 16:28	181.00	186.00	187.00	799.67				1631.59	1632.15	1632.69	

idcode	start_date	stop_date	secup	seclow	obs_secup	obs_seclow	pi_above	pp_above	pf_above	pi_below	pp_below	pf_below	comments
KFM09A	20051208 16:36	20051208 17:51	186.00	191.00	7.79	185.00	955.17	954.76	954.62				
KFM09A	20051208 16:36	20051208 17:51	186.00	191.00	192.00	799.67				1673.78	1674.32	1674.88	
KFM09A	20051208 18:03	20051208 18:50	191.00	196.00	7.79	190.00	953.71	953.71	953.71				
KFM09A	20051208 18:03	20051208 18:50	191.00	196.00	197.00	799.67				1714.60	1714.87	1714.87	
KFM09A	20051208 19:02	20051208 19:47	196.00	201.00	7.79	195.00	953.08	952.80	953.35				
KFM09A	20051208 19:02	20051208 19:47	196.00	201.00	202.00	799.67				1755.42	1755.96	1755.96	
KFM09A	20051208 19:57	20051208 20:39	201.00	206.00	7.79	200.00	951.76	951.62	951.35				
KFM09A	20051208 19:57	20051208 20:39	201.00	206.00	207.00	799.67				1796.91	1796.64	1797.05	
KFM09A	20051208 20:58	20051208 21:40	226.00	231.00	7.79	225.00	945.16	945.16	945.16				
KFM09A	20051208 20:58	20051208 21:40	226.00	231.00	232.00	799.67				2002.07	2002.07	2002.49	
KFM09A	20051208 21:54	20051208 23:08	232.00	237.00	7.79	231.00	943.24	942.83	942.96				
KFM09A	20051208 21:54	20051208 23:08	232.00	237.00	238.00	799.67				2050.15	2052.48	2052.90	
KFM09A	20051208 23:21	20051209 00:35	237.00	242.00	7.79	236.00	941.65	941.51	941.51				
KFM09A	20051208 23:21	20051209 00:35	237.00	242.00	243.00	799.67				2091.78	2092.88	2093.43	
KFM09A	20051209 08:08	20051209 09:24	240.80	245.80	7.79	239.80	940.36	940.36	939.81				
KFM09A	20051209 08:08	20051209 09:24	240.80	245.80	246.80	799.67				2119.73	2120.55	2121.37	
KFM09A	20051221 13:55	20051221 14:35	246.80	251.80	7.79	245.80	936.51	936.51	936.51				
KFM09A	20051221 13:55	20051221 14:35	246.80	251.80	252.80	799.67				2155.47	2155.61	2156.43	
KFM09A	20051209 09:40	20051209 10:22	251.50	256.50	7.79	250.50	936.76	936.62	936.49				
KFM09A	20051209 09:40	20051209 10:22	251.50	256.50	257.50	799.67				2208.47	2208.61	2209.02	
KFM09A	20051209 10:34	20051209 11:18	256.50	261.50	7.79	255.50	935.03	935.03	935.03				
KFM09A	20051209 10:34	20051209 11:18	256.50	261.50	262.50	799.67				2248.74	2249.01	2249.01	
KFM09A	20051209 11:30	20051209 13:22	273.00	278.00	7.79	272.00	929.01	929.01	929.01				
KFM09A	20051209 11:30	20051209 13:22	273.00	278.00	279.00	799.67				2384.88	2385.43	2385.98	
KFM09A	20051209 13:34	20051209 14:48	278.00	283.00	7.79	277.00	927.55	927.41	927.55				
KFM09A	20051209 13:34	20051209 14:48	278.00	283.00	284.00	799.67				2423.36	2424.73	2424.87	
KFM09A	20051209 15:04	20051209 15:51	283.00	288.00	7.79	282.00	925.96	925.82	925.54				
KFM09A	20051209 15:04	20051209 15:51	283.00	288.00	289.00	799.67				2463.21	2463.63	2463.77	
KFM09A	20051209 16:00	20051209 17:15	288.00	293.00	7.79	287.00	924.08	924.08	924.08				
KFM09A	20051209 16:00	20051209 17:15	288.00	293.00	294.00	799.67				2504.58	2505.40	2506.50	
KFM09A	20051212 08:21	20051212 09:42	293.00	298.00	7.79	292.00	923.18	923.73	924.83				
KFM09A	20051212 08:21	20051212 09:42	293.00	298.00	299.00	799.67				2542.66	2542.66	2542.66	

idcode	start_date	stop_date	secup	seclow	obs_secup	obs_seclow	pi_above	pp_above	pf_above	pi_below	pp_below	pf_below	comments
KFM09A	20051221 12:39	20051221 13:28	296.00	301.00	7.79	295.00	920.42	920.56	920.42				
KFM09A	20051221 12:39	20051221 13:28	296.00	301.00	302.00	799.67				2558.54	2559.09	2559.63	
KFM09A	20051221 11:45	20051221 12:29	301.00	306.00	7.79	300.00	917.86	917.86	918.42				
KFM09A	20051221 11:45	20051221 12:29	301.00	306.00	307.00	799.67				2595.26	2595.53	2596.35	
KFM09A	20051212 09:58	20051212 10:39	306.00	311.00	7.79	305.00	917.10	916.97	916.41				
KFM09A	20051212 09:58	20051212 10:39	306.00	311.00	312.00	799.67				2648.39	2648.39	2648.39	
KFM09A	20051212 10:49	20051212 12:33	311.00	316.00	7.79	310.00	917.15	917.02	917.15				
KFM09A	20051212 10:49	20051212 12:33	311.00	316.00	317.00	799.67				2687.83	2688.25	2687.83	
KFM09A	20051212 12:43	20051212 13:31	316.00	321.00	7.79	315.00	914.87	914.59	914.59				
KFM09A	20051212 12:43	20051212 13:31	316.00	321.00	322.00	799.67				2728.10	2728.37	2728.37	
KFM09A	20051212 13:44	20051212 15:02	321.00	326.00	7.79	320.00	912.73	910.38	912.04				
KFM09A	20051212 13:44	20051212 15:02	321.00	326.00	327.00	799.67				2767.81	2768.37	2768.91	
KFM09A	20051212 15:31	20051212 16:14	346.00	351.00	7.79	345.00	896.35	896.49	896.49				
KFM09A	20051212 15:31	20051212 16:14	346.00	351.00	352.00	799.67				2966.27	2966.68	2966.68	
KFM09A	20051221 10:04	20051221 11:19	351.00	356.00	7.79	350.00	895.85	895.99	896.13				
KFM09A	20051221 10:04	20051221 11:19	351.00	356.00	357.00	799.67				2999.56	3000.65	3001.75	
KFM09A	20051221 08:54	20051221 09:50	356.00	361.00	7.79	355.00	892.47	892.88	893.02				
KFM09A	20051221 08:54	20051221 09:50	356.00	361.00	362.00	799.67				3037.62	3038.86	3039.00	
KFM09A	20051221 07:28	20051221 08:43	361.00	366.00	7.79	360.00	888.39	889.35	889.35				
KFM09A	20051221 07:28	20051221 08:43	361.00	366.00	367.00	799.67				3071.87	3073.65	3075.70	
KFM09A	20051212 16:39	20051212 17:54	363.00	368.00	7.79	362.00	888.98	888.98	888.98				
KFM09A	20051212 16:39	20051212 17:54	363.00	368.00	369.00	799.67				3099.80	3100.49	3101.45	
KFM09A	20051213 06:27	20051213 07:24	368.00	373.00	7.79	367.00	890.70	890.83	890.83				
KFM09A	20051213 06:27	20051213 07:24	368.00	373.00	374.00	799.67				3141.44	3141.44	3141.44	
KFM09A	20051213 07:35	20051213 08:48	371.00	376.00	7.79	370.00	889.19	889.05	886.43				
KFM09A	20051213 07:35	20051213 08:48	371.00	376.00	377.00	799.67				3165.55	3166.10	3166.65	
KFM09A	20051213 09:02	20051213 09:58	376.00	381.00	7.79	375.00	886.50	883.61	884.98				
KFM09A	20051213 09:02	20051213 09:58	376.00	381.00	382.00	799.67				3205.40	3205.95	3205.54	
KFM09A	20051213 10:10	20051213 11:25	381.00	386.00	7.79	380.00	883.66	881.88	882.98				
KFM09A	20051213 10:10	20051213 11:25	381.00	386.00	387.00	799.67				3244.71	3245.53	3245.53	
KFM09A	20051213 11:57	20051213 13:16	386.00	391.00	7.79	385.00	880.55	880.42	878.75				
KFM09A	20051213 11:57	20051213 13:16	386.00	391.00	392.00	799.67				3283.88	3284.57	3285.52	

idcode	start_date	stop_date	secup	seclow	obs_secup	obs_seclow	pi_above	pp_above	pf_above	pi_below	pp_below	pf_below	comments
KFM09A	20051213 13:28	20051213 14:48	391.00	396.00	7.79	390.00	877.86	875.10	877.86				
KFM09A	20051213 13:28	20051213 14:48	391.00	396.00	397.00	799.67				3324.97	3325.51	3326.07	
KFM09A	20051213 15:06	20051213 15:49	396.00	401.00	7.79	395.00	874.60	873.36	873.09				
KFM09A	20051213 15:06	20051213 15:49	396.00	401.00	402.00	799.67				3363.18	3363.32	3363.32	
KFM09A	20051213 16:00	20051213 17:15	401.00	406.00	7.79	400.00	872.18	869.42	872.18				
KFM09A	20051213 16:00	20051213 17:15	401.00	406.00	407.00	799.67				3403.03	3403.86	3404.40	
KFM09A	20051213 17:25	20051213 18:18	406.00	411.00	7.79	405.00	866.86	868.79	868.52				
KFM09A	20051213 17:25	20051213 18:18	406.00	411.00	412.00	799.67				3442.61	3443.17	3442.75	
KFM09A	20051213 18:36	20051213 19:50	411.00	416.00	7.79	410.00	863.61	865.41	865.96				
KFM09A	20051213 18:36	20051213 19:50	411.00	416.00	417.00	799.67				3480.83	3481.65	3482.20	
KFM09A	20051213 20:06	20051213 21:22	414.00	419.00	7.79	413.00	864.32	864.04	861.56				
KFM09A	20051213 20:06	20051213 21:22	414.00	419.00	420.00	799.67				3504.39	3505.20	3505.76	
KFM09A	20051213 21:32	20051213 22:46	419.00	424.00	7.79	418.00	857.90	857.90	857.35				
KFM09A	20051213 21:32	20051213 22:46	419.00	424.00	425.00	799.67				3542.45	3543.55	3544.11	
KFM09A	20051213 22:55	20051214 00:09	421.00	426.00	7.79	420.00	857.53	856.99	858.09				
KFM09A	20051213 22:55	20051214 00:09	421.00	426.00	427.00	799.67				3558.34	3559.44	3559.99	
KFM09A	20051214 06:51	20051214 07:59	426.00	431.00	7.79	425.00	857.17	853.87	855.53				
KFM09A	20051214 06:51	20051214 07:59	426.00	431.00	432.00	799.67				3597.80	3598.34	3598.34	
KFM09A	20051214 08:11	20051214 09:31	431.00	436.00	7.79	430.00	854.76	854.76	854.07				
KFM09A	20051214 08:11	20051214 09:31	431.00	436.00	437.00	799.67				3641.20	3644.35	3644.35	
KFM09A	20051214 09:47	20051214 10:29	436.00	441.00	7.79	435.00	852.33	852.06	852.06				
KFM09A	20051214 09:47	20051214 10:29	436.00	441.00	442.00	799.67				3683.25	3683.25	3683.25	
KFM09A	20051214 10:44	20051214 12:00	441.00	446.00	7.79	440.00	848.67	848.39	846.74				
KFM09A	20051214 10:44	20051214 12:00	441.00	446.00	447.00	799.67				3719.96	3721.61	3721.61	
KFM09A	20051214 12:13	20051214 14:04	446.00	451.00	7.79	445.00	844.32	845.29	845.83				
KFM09A	20051214 12:13	20051214 14:04	446.00	451.00	452.00	799.67				3760.91	3761.59	3762.15	
KFM09A	20051214 14:22	20051214 15:38	451.00	456.00	7.79	450.00	842.17	842.46	840.53				
KFM09A	20051214 14:22	20051214 15:38	451.00	456.00	457.00	799.67				3797.62	3798.85	3799.95	
KFM09A	20051214 15:55	20051214 17:12	456.00	461.00	7.79	455.00	839.21	837.41	839.07				
KFM09A	20051214 15:55	20051214 17:12	456.00	461.00	462.00	799.67				3836.65	3837.88	3838.84	
KFM09A	20051214 17:32	20051214 18:15	461.00	466.00	7.79	460.00	836.37	836.09	836.51				
KFM09A	20051214 17:32	20051214 18:15	461.00	466.00	467.00	799.67				3875.54	3875.68	3876.10	

idcode	start_date	stop_date	secup	seclow	obs_secup	obs_seclow	pi_above	pp_above	pf_above	pi_below	pp_below	pf_below	comments
KFM09A	20051214 18:35	20051214 19:50	471.00	476.00	7.79	470.00	829.18	829.18	828.08				
KFM09A	20051214 18:35	20051214 19:50	471.00	476.00	477.00	799.67				3952.23	3953.89	3954.98	
KFM09A	20051214 20:01	20051214 21:23	476.00	481.00	7.79	475.00	826.34	826.20	826.07				
KFM09A	20051214 20:01	20051214 21:23	476.00	481.00	482.00	799.67				3992.38	3993.34	3994.43	
KFM09A	20051214 21:40	20051214 22:31	486.00	491.00	7.79	485.00	861.26	860.98	860.98				
KFM09A	20051214 21:40	20051214 22:31	486.00	491.00	492.00	799.67				4070.03	4070.03	4070.03	
KFM09A	20051214 22:58	20051215 00:12	491.00	496.00	7.79	490.00	858.42	856.77	857.32				
KFM09A	20051214 22:58	20051215 00:12	491.00	496.00	497.00	799.67				4108.38	4109.47	4110.02	
KFM09A	20051215 06:33	20051215 07:57	496.00	501.00	7.79	495.00	853.52	852.83	853.11				
KFM09A	20051215 06:33	20051215 07:57	496.00	501.00	502.00	799.67				4145.63	4146.73	4147.83	
KFM09A	20051215 08:14	20051215 09:00	501.00	506.00	7.79	500.00	807.49	807.21	807.76				
KFM09A	20051215 08:14	20051215 09:00	501.00	506.00	507.00	799.67				4184.11	4184.52	4184.52	
KFM09A	20051220 19:00	20051220 20:23	506.00	511.00	7.79	505.00	806.16	806.30	805.75				
KFM09A	20051220 19:00	20051220 20:23	506.00	511.00	512.00	799.67				4220.68	4222.87	4224.52	
KFM09A	20051220 20:50	20051220 22:05	511.00	516.00	7.79	510.00	797.41	794.65	794.38				
KFM09A	20051220 20:50	20051220 22:05	511.00	516.00	517.00	799.67				4262.59	4263.97	4265.06	
KFM09A	20051220 22:14	20051220 23:28	516.00	521.00	7.79	515.00	794.02	794.84	795.67				
KFM09A	20051220 22:14	20051220 23:28	516.00	521.00	522.00	799.67				4299.57	4301.36	4302.86	
KFM09A	20051215 09:25	20051215 10:11	521.00	526.00	7.79	520.00	792.29	792.15	792.57				
KFM09A	20051215 09:25	20051215 10:11	521.00	526.00	527.00	799.67				4337.92	4338.19	4338.47	
KFM09A	20051215 10:26	20051215 11:07	526.00	531.00	7.79	525.00	789.04	788.91	787.80				
KFM09A	20051215 10:26	20051215 11:07	526.00	531.00	532.00	799.67				4375.17	4375.17	4375.73	
KFM09A	20051215 11:23	20051215 12:44	531.00	536.00	7.79	530.00	785.10	782.62	784.14				
KFM09A	20051215 11:23	20051215 12:44	531.00	536.00	537.00	799.67				4416.27	4417.22	4417.36	
KFM09A	20051215 13:19	20051215 14:03	536.00	541.00	7.79	535.00	777.58	777.72	777.17				
KFM09A	20051215 13:19	20051215 14:03	536.00	541.00	542.00	799.67				4454.61	4454.61	4454.61	
KFM09A	20051215 14:14	20051215 15:28	541.00	546.00	7.79	540.00	773.92	773.51	773.51				
KFM09A	20051215 14:14	20051215 15:28	541.00	546.00	547.00	799.67				4492.55	4493.09	4493.50	
KFM09A	20051220 17:14	20051220 17:58	561.00	566.00	7.79	560.00	760.10	760.10	760.52				
KFM09A	20051220 17:14	20051220 17:58	561.00	566.00	567.00	799.67				4643.07	4643.07	4643.07	
KFM09A	20051215 16:19	20051215 17:00	606.00	611.00	7.79	605.00	712.54	712.12	711.58				
KFM09A	20051215 16:19	20051215 17:00	606.00	611.00	612.00	799.67				4977.25	4977.25	4977.25	

idcode	start_date	stop_date	secup	seclow	obs_secup	obs_seclow	pi_above	pp_above	pf_above	pi_below	pp_below	pf_below	comments
KFM09A	20051215 17:19	20051215 18:35	611.00	616.00	7.79	610.00	706.40	706.40	706.26				
KFM09A	20051215 17:19	20051215 18:35	611.00	616.00	617.00	799.67				5014.09	5014.77	5015.04	
KFM09A	20051215 18:50	20051215 19:31	616.00	621.00	7.79	615.00	701.91	701.50	701.50				
KFM09A	20051215 18:50	20051215 19:31	616.00	621.00	622.00	799.67				5051.48	5051.20	5051.76	
KFM09A	20051215 19:44	20051215 21:03	621.00	626.00	7.79	620.00	696.18	695.63	695.63				
KFM09A	20051215 19:44	20051215 21:03	621.00	626.00	627.00	799.67				5087.91	5088.18	5088.45	
KFM09A	20051215 21:14	20051215 22:01	626.00	631.00	7.79	625.00	690.32	690.32	690.32				
KFM09A	20051215 21:14	20051215 22:01	626.00	631.00	632.00	799.67				5124.61	5124.75	5125.17	
KFM09A	20051215 22:08	20051215 23:33	631.00	636.00	7.79	630.00	684.99	684.72	684.45				
KFM09A	20051215 22:08	20051215 23:33	631.00	636.00	637.00	799.67				5160.77	5161.32	5161.87	
KFM09A	20051215 23:43	20051216 00:58	636.00	641.00	7.79	635.00	679.13	678.86	679.13				
KFM09A	20051215 23:43	20051216 00:58	636.00	641.00	642.00	799.67				5197.61	5198.02	5198.02	
KFM09A	20051216 08:21	20051216 09:36	641.00	646.00	7.79	640.00	672.72	672.72	672.72				
KFM09A	20051216 08:21	20051216 09:36	641.00	646.00	647.00	799.67				5232.40	5233.08	5233.64	
KFM09A	20051216 09:55	20051216 10:38	646.00	651.00	7.79	645.00	667.82	667.68	667.95				
KFM09A	20051216 09:55	20051216 10:38	646.00	651.00	652.00	799.67				5270.33	5270.33	5270.89	
KFM09A	20051216 10:53	20051216 12:10	651.00	656.00	7.79	650.00	661.82	661.53	661.53				
KFM09A	20051216 10:53	20051216 12:10	651.00	656.00	657.00	799.67				5307.04	5307.32	5307.04	
KFM09A	20051216 12:21	20051216 13:20	656.00	661.00	7.79	655.00	655.67	655.67	655.67				
KFM09A	20051216 12:21	20051216 13:20	656.00	661.00	662.00	799.67				5343.20	5343.20	5343.20	
KFM09A	20051216 13:31	20051216 14:14	661.00	666.00	667.00	799.67	649.39	649.39	649.26				
KFM09A	20051216 13:31	20051216 14:14	661.00	666.00	667.00	667.00				5379.36	5379.22	5379.36	
KFM09A	20051219 08:19	20051219 09:01	731.00	736.00	7.79	730.00	557.22	556.94	556.66				
KFM09A	20051219 08:19	20051219 09:01	731.00	736.00	737.00	799.67				5867.48	5867.48	5867.48	
KFM09A	20051219 09:15	20051219 09:56	736.00	741.00	7.79	735.00	548.59	548.59	548.59				
KFM09A	20051219 09:15	20051219 09:56	736.00	741.00	742.00	799.67				5902.00	5902.13	5902.00	
KFM09A	20051219 10:11	20051219 11:30	741.00	746.00	7.79	740.00	541.76	539.98	539.98				
KFM09A	20051219 10:11	20051219 11:30	741.00	746.00	747.00	799.67				5936.37	5936.51	5936.51	
KFM09A	20051219 11:44	20051219 12:36	746.00	751.00	7.79	745.00	533.55	533.55	533.55				
KFM09A	20051219 11:44	20051219 12:36	746.00	751.00	752.00	799.67				5970.48	5970.48	5970.48	
KFM09A	20051219 12:50	20051219 14:05	751.00	756.00	7.79	750.00	524.93	524.11	524.93				
KFM09A	20051219 12:50	20051219 14:05	751.00	756.00	757.00	799.67				6004.58	6006.09	6005.00	

idcode	start_date	stop_date	secup	seclow	obs_secup	obs_seclow	pi_above	pp_above	pf_above	pi_below	pp_below	pf_below	comments
KFM09A	20051219 14:20	20051219 15:42	756.00	761.00	7.79	755.00	516.73	516.32	516.87				
KFM09A	20051219 14:20	20051219 15:42	756.00	761.00	762.00	799.67				6038.00	6038.40	6038.40	
KFM09A	20051219 15:56	20051219 17:16	761.00	766.00	7.79	760.00	509.21	508.11	507.70				
KFM09A	20051219 15:56	20051219 17:16	761.00	766.00	767.00	799.67				6071.83	6074.02	6072.38	
KFM09A	20051220 06:55	20051220 08:10	766.00	771.00	7.79	765.00	498.80	498.66	498.52				
KFM09A	20051220 06:55	20051220 08:10	766.00	771.00	772.00	799.67				6105.65	6105.52	6105.79	
KFM09A	20051220 08:29	20051220 09:46	771.00	776.00	7.79	770.00	489.90	490.04	489.90				
KFM09A	20051220 08:29	20051220 09:46	771.00	776.00	777.00	799.67				6138.67	6139.76	6139.21	
KFM09A	20051220 10:06	20051220 11:24	776.00	781.00	7.79	775.00	481.56	480.73	479.08				
KFM09A	20051220 10:06	20051220 11:24	776.00	781.00	782.00	799.67				6172.08	6172.35	6172.08	
KFM09A	20051220 11:35	20051220 12:58	781.00	786.00	7.79	780.00	469.90	470.18	471.01				
KFM09A	20051220 11:35	20051220 12:58	781.00	786.00	787.00	799.67				6204.54	6207.14	6206.04	
KFM09A	20051220 13:11	20051220 14:28	786.00	791.00	7.79	785.00	462.38	462.38	462.38				
KFM09A	20051220 13:11	20051220 14:28	786.00	791.00	792.00	799.67				6240.56	6243.85	6240.01	
KFM09A	20051118 13:32	20051118 14:28	506.00	606.00	7.79	505.00	789.23	789.09	789.23				Incomplete test, interrupted and re-performed later.
KFM09A	20051118 13:32	20051118 14:28	506.00	606.00	607.00	799.67				4942.10	4943.06	4942.65	Incomplete test, interrupted and re-performed later.
KFM09A	20051130 17:10	20051130 18:03	426.00	446.00	7.79	425.00	855.53	855.39	854.97				Incomplete test, interrupted and re-performed later.
KFM09A	20051130 17:10	20051130 18:03	426.00	446.00	447.00	799.67				3726.67	3728.72	3728.72	Incomplete test, interrupted and re-performed later.
KFM09A	20051207 10:38	20051207 12:39	116.00	121.00	7.79	115.00	970.07	969.51	970.07				Incomplete test, interrupted and re-performed later.
KFM09A	20051207 10:38	20051207 12:39	116.00	121.00	122.00	799.67				1088.56	1088.70	1088.70	Incomplete test, interrupted and re-performed later.

Appendix 2.1. General test data

Borehole:	KFM09A
Testtype:	CHir (Constant Head injection and recovery)
Field crew:	C. Hjerne, K. Gokall-Norman, T. Svensson, A. Lindquist, J. Harrström, E. Gustavsson
General comment:	

Test section secup	**Test section seclow**	**Test start**	**Start of flow period**	**Stop of flow period**	**Test stop**	**Total flow time t_p**	**Total recovery time t_F**
(m)	(m)	YYYYMMDD hh:mm	YYYYMMDD hh:mm:ss	YYYYMMDD hh:mm:ss	YYYYMMDD hh:mm	(min)	(min)
106.00	206.00	20051117 16:09	20051117 16:57:06	20051117 17:27:25	20051117 17:59	30	30
206.00	306.00	20051117 19:03	20051117 19:50:48	20051117 20:21:10	20051117 20:53	30	30
306.00	406.00	20051117 21:47	20051117 22:34:02	20051117 23:04:29	20051117 23:36	30	30
406.00	506.00	20051118 09:59	20051118 10:46:49	20051118 11:17:10	20051118 11:49	30	30
506.00	606.00	20051121 12:52	20051121 14:11:02	20051121 14:41:23	20051121 15:13	30	30
606.00	706.00	20051121 06:14	20051121 07:00:34	20051121 07:30:54	20051121 08:03	30	30
691.00	791.00	20051121 08:51	20051121 09:37:30	20051121 10:07:51	20051121 10:40	30	30
106.00	126.00	20051128 16:44	20051128 17:36:29	20051128 17:56:45	20051128 18:19	20	20
126.00	146.00	20051129 06:29	20051129 07:01:05	20051129 07:21:21	20051129 07:43	20	20
146.00	166.00	20051129 08:20	20051129 08:53:25	20051129 09:13:42	20051129 09:35	20	20
166.00	186.00	20051129 10:00	20051129 10:33:21	20051129 10:53:39	20051129 11:15	20	20
186.00	206.00	20051129 12:14	20051129 12:48:51	20051129 13:09:11	20051129 13:31	20	20
206.00	226.00	20051129 14:01	20051129 14:36:49	20051129 14:40:14	20051129 14:47	3	5
226.00	246.00	20051129 15:38	20051129 16:13:49	20051129 16:34:11	20051129 16:56	20	20
238.00	258.00	20051129 17:18	20051129 17:54:33	20051129 18:14:55	20051129 18:37	20	20
258.00	278.00	20051129 18:58	20051129 19:35:15	20051129 19:55:42	20051129 20:17	20	20
278.00	298.00	20051129 21:03	20051129 21:42:40	20051129 22:03:04	20051129 22:25	20	20
286.00	306.00	20051129 22:41	20051129 23:15:24	20051129 23:35:54	20051129 23:57	21	20
306.00	326.00	20051130 06:29	20051130 07:05:44	20051130 07:26:04	20051130 07:48	20	20
326.00	346.00	20051130 08:16	20051130 08:53:03	20051130 09:13:26	20051130 09:35	20	20
346.00	366.00	20051130 10:06	20051130 10:40:24	20051130 11:00:46	20051130 11:22	20	20
366.00	386.00	20051130 12:06	20051130 12:41:16	20051130 13:01:46	20051130 13:23	21	20
386.00	406.00	20051130 13:50	20051130 14:25:53	20051130 14:46:29	20051130 15:08	21	20
406.00	426.00	20051130 15:30	20051130 16:04:48	20051130 16:25:26	20051130 16:47	21	20
426.00	446.00	20051130 18:18	20051130 18:55:34	20051130 19:16:08	20051130 19:38	21	20
446.00	466.00	20051130 20:03	20051130 21:02:55	20051130 21:23:31	20051130 21:45	21	20
466.00	486.00	20051130 22:03	20051130 22:37:39	20051130 22:58:37	20051130 23:20	21	19
486.00	506.00	20051201 08:06	20051201 08:51:37	20051201 09:11:58	20051201 09:34	20	20
506.00	526.00	20051201 10:01	20051201 10:39:48	20051201 11:00:08	20051201 11:22	20	20
526.00	546.00	20051201 11:41	20051201 13:03:33	20051201 13:23:52	20051201 13:46	20	20
545.00	565.00	20051201 14:21	20051201 14:59:12	20051201 15:02:07	20051201 15:09	3	5
566.00	586.00	20051201 15:34	20051201 16:08:01	20051201 16:10:17	20051201 16:17	2	5
586.00	606.00	20051202 07:55	20051202 08:28:21	20051202 08:29:58	20051202 08:37	2	5
606.00	626.00	20051202 08:58	20051202 09:40:01	20051202 10:00:18	20051202 10:22	20	20
626.00	646.00	20051202 10:43	20051202 11:22:44	20051202 11:43:05	20051202 12:05	20	20
646.00	666.00	20051202 13:12	20051202 13:52:57	20051202 14:13:15	20051202 14:35	20	20
666.00	686.00	20051202 14:57	20051202 15:30:57	20051202 15:51:01	20051202 16:13	20	20
686.00	706.00	20051205 08:22	20051205 09:10:31	20051205 09:30:35	20051205 09:53	20	20
691.00	711.00	20051205 10:10	20051205 10:52:46	20051205 11:05:04	20051205 11:12	12	5
711.00	731.00	20051205 12:46	20051205 13:20:23	20051205 13:22:52	20051205 13:30	2	5
731.00	751.00	20051205 13:49	20051205 14:29:26	20051205 14:49:46	20051205 15:12	20	20
751.00	771.00	20051205 15:30	20051205 16:12:15	20051205 16:32:33	20051205 16:54	20	20
771.00	791.00	20051205 18:09	20051205 18:44:18	20051205 19:04:38	20051205 19:26	20	20
106.00	111.00	20051207 07:32	20051207 08:10:17	20051207 08:30:41	20051207 08:52	20	20
111.00	116.00	20051207 09:08	20051207 09:42:13	20051207 10:02:37	20051207 10:24	20	20
116.00	121.00	20051221 15:48	20051221 16:27:38	20051221 16:47:54	20051208 17:51	20	20
121.00	126.00	20051207 12:52	20051207 13:26:31	20051207 13:46:51	20051207 14:09	20	20
126.00	131.00	20051207 14:26	20051207 15:21:48	20051207 15:42:09	20051207 16:04	20	20
128.00	133.00	20051207 16:21	20051207 16:58:15	20051207 17:18:34	20051207 17:40	20	20
133.00	138.00	20051207 17:58	20051207 18:34:22	20051207 18:54:23	20051207 19:16	20	20
138.00	143.00	20051207 19:42	20051207 20:30:41	20051207 20:50:56	20051207 21:13	20	20
141.00	146.00	20051207 21:27	20051207 22:03:25	20051207 22:23:49	20051207 22:45	20	20
146.00	151.00	20051207 23:02	20051207 23:35:21	20051207 23:55:41	20051208 00:17	20	20
151.00	156.00	20051208 06:16	20051208 06:49:42	20051208 06:51:37	20051208 06:59	2	5
156.00	161.00	20051208 07:10	20051208 07:44:24	20051208 08:04:38	20051208 08:26	20	20
161.00	166.00	20051208 08:36	20051208 09:10:22	20051208 09:30:41	20051208 09:52	20	20
166.00	171.00	20051208 10:03	20051208 10:36:39	20051208 10:56:56	20051208 11:19	20	20
171.00	176.00	20051208 12:12	20051208 12:47:14	20051208 13:07:30	20051208 13:29	20	20

Test section secup (m)	Test section seclow (m)	Test start YYYYMMDD hh:mm	Start of flow period YYYYMMDD hh:mm:ss	Stop of flow period YYYYMMDD hh:mm:ss	Test stop YYYYMMDD hh:mm	Total flow time t_p (min)	Total recovery time t_F (min)
176.00	181.00	20051208 13:43	20051208 14:15:22	20051208 14:35:42	20051208 14:57	20	20
181.00	186.00	20051208 15:13	20051208 15:45:32	20051208 16:05:52	20051208 16:28	20	20
186.00	191.00	20051208 16:36	20051208 17:09:19	20051208 17:29:36	20051208 17:51	20	20
191.00	196.00	20051208 18:03	20051208 18:35:40	20051208 18:42:32	20051208 18:50	7	5
196.00	201.00	20051208 19:02	20051208 19:35:04	20051208 19:39:45	20051208 19:47	5	5
201.00	206.00	20051208 19:57	20051208 20:30:56	20051208 20:32:09	20051208 20:39	1	5
226.00	231.00	20051208 20:58	20051208 21:30:25	20051208 21:32:31	20051208 21:40	2	5
232.00	237.00	20051208 21:54	20051208 22:26:14	20051208 22:46:32	20051208 23:08	20	20
237.00	242.00	20051208 23:21	20051208 23:52:47	20051209 00:13:05	20051209 00:35	20	20
240.80	245.80	20051209 08:08	20051209 08:41:39	20051209 09:01:58	20051209 09:24	20	20
246.80	251.80	20051221 13:55	20051221 14:26:40	20051221 14:28:04	20051221 14:35	1	5
251.50	256.50	20051209 09:40	20051209 10:12:05	20051209 10:14:57	20051209 10:22	3	5
256.50	261.50	20051209 10:34	20051209 11:06:25	20051209 11:10:31	20051209 11:18	4	5
273.00	278.00	20051209 11:30	20051209 12:39:59	20051209 13:00:19	20051209 13:22	20	20
278.00	283.00	20051209 13:34	20051209 14:05:39	20051209 14:26:00	20051209 14:48	20	20
283.00	288.00	20051209 15:04	20051209 15:36:41	20051209 15:44:08	20051209 15:51	7	5
288.00	293.00	20051209 16:00	20051209 16:33:16	20051209 16:53:38	20051209 17:15	20	20
293.00	298.00	20051212 08:21	20051212 08:59:52	20051212 09:20:12	20051212 09:42	20	20
296.00	301.00	20051221 12:39	20051221 13:11:23	20051221 13:21:20	20051221 13:28	10	5
301.00	306.00	20051221 11:45	20051221 12:18:01	20051221 12:21:31	20051221 12:29	4	5
306.00	311.00	20051212 09:58	20051212 10:30:37	20051212 10:31:58	20051212 10:39	1	5
311.00	316.00	20051212 10:49	20051212 12:23:33	20051212 12:25:31	20051212 12:33	2	5
316.00	321.00	20051212 12:43	20051212 13:19:35	20051212 13:23:52	20051212 13:31	4	5
321.00	326.00	20051212 13:44	20051212 14:20:06	20051212 14:40:29	20051212 15:02	20	20
346.00	351.00	20051212 15:31	20051212 16:05:39	20051212 16:06:46	20051212 16:14	1	5
351.00	356.00	20051221 10:04	20051021 10:36:43	20051021 10:56:56	20051221 11:19	20	20
356.00	361.00	20051221 08:54	20051221 09:25:06	20051221 09:43:27	20051221 09:50	18	5
361.00	366.00	20051221 07:28	20051221 08:00:40	20051221 08:20:51	20051221 08:43	20	20
363.00	368.00	20051212 16:39	20051212 17:11:54	20051212 17:32:16	20051212 17:54	20	20
368.00	373.00	20051213 06:27	20051213 07:15:59	20051213 07:17:12	20051213 07:24	1	5
371.00	376.00	20051213 07:35	20051213 08:09:41	20051213 08:23:48	20051213 08:48	14	20
376.00	381.00	20051213 09:02	20051213 09:37:12	20051213 09:51:20	20051213 09:58	14	5
381.00	386.00	20051213 10:10	20051213 10:42:36	20051213 11:02:40	20051213 11:25	20	20
386.00	391.00	20051213 11:57	20051213 12:33:30	20051213 12:53:52	20051213 13:16	20	20
391.00	396.00	20051213 13:28	20051213 14:05:53	20051213 14:26:16	20051213 14:48	20	20
396.00	401.00	20051213 15:06	20051213 15:37:15	20051213 15:41:39	20051213 15:49	4	5
401.00	406.00	20051213 16:00	20051213 16:33:21	20051213 16:53:44	20051213 17:15	20	20
406.00	411.00	20051213 17:25	20051213 17:56:34	20051213 18:10:55	20051213 18:18	14	5
411.00	416.00	20051213 18:36	20051213 19:07:32	20051213 19:27:56	20051213 19:50	20	20
414.00	419.00	20051213 20:06	20051213 20:39:31	20051213 20:59:55	20051213 21:22	20	20
419.00	424.00	20051213 21:32	20051213 22:04:11	20051213 22:24:35	20051213 22:46	20	20
421.00	426.00	20051213 22:55	20051213 23:26:44	20051213 23:47:06	20051214 00:09	20	20
426.00	431.00	20051214 06:51	20051214 07:32:04	20051214 07:52:07	20051214 07:59	20	5
431.00	436.00	20051214 08:11	20051214 08:49:02	20051214 09:09:24	20051214 09:31	20	20
436.00	441.00	20051214 09:47	20051214 10:20:56	20051214 10:22:10	20051214 10:29	1	5
441.00	446.00	20051214 10:44	20051214 11:18:15	20051214 11:38:42	20051214 12:00	20	20
446.00	451.00	20051214 12:13	20051214 13:21:31	20051214 13:41:55	20051214 14:04	20	20
451.00	456.00	20051214 14:22	20051214 14:56:20	20051214 15:16:46	20051214 15:38	20	20
456.00	461.00	20051214 15:55	20051214 16:30:00	20051214 16:50:24	20051214 17:12	20	20
461.00	466.00	20051214 17:32	20051214 18:04:52	20051214 18:07:43	20051214 18:15	3	5
471.00	476.00	20051214 18:35	20051214 19:08:00	20051214 19:28:26	20051214 19:50	20	20
476.00	481.00	20051214 20:01	20051214 20:40:37	20051214 21:00:58	20051214 21:23	20	20
486.00	491.00	20051214 21:40	20051214 22:17:49	20051214 22:23:53	20051214 22:31	6	5
491.00	496.00	20051214 22:58	20051214 23:29:36	20051214 23:49:58	20051215 00:12	20	20
496.00	501.00	20051215 06:33	20051215 07:15:10	20051215 07:35:32	20051215 07:57	20	20
501.00	506.00	20051215 08:14	20051215 08:47:17	20051215 08:53:08	20051215 09:00	6	5
506.00	511.00	20051220 19:00	20051220 19:41:12	20051220 20:01:35	20051220 20:23	20	20
511.00	516.00	20051220 20:50	20051220 21:22:36	20051220 21:42:55	20051220 22:05	20	20
516.00	521.00	20051220 22:14	20051220 22:45:57	20051220 23:06:17	20051220 23:28	20	20
521.00	526.00	20051215 09:25	20051215 10:01:53	20051215 10:03:44	20051215 10:11	2	5
526.00	531.00	20051215 10:26	20051215 10:58:38	20051215 10:59:49	20051215 11:07	1	5
531.00	536.00	20051215 11:23	20051215 12:01:54	20051215 12:22:16	20051215 12:44	20	20
536.00	541.00	20051215 13:19	20051215 13:52:58	20051215 13:56:08	20051215 14:03	3	5
541.00	546.00	20051215 14:14	20051215 14:46:13	20051215 15:06:37	20051215 15:28	20	20
561.00	566.00	20051220 17:14	20051220 17:49:31	20051220 17:50:36	20051220 17:58	1	5
606.00	611.00	20051215 16:19	20051215 16:50:43	20051215 16:52:47	20051215 17:00	2	5
611.00	616.00	20051215 17:19	20051215 17:52:51	20051215 18:13:12	20051215 18:35	20	20
616.00	621.00	20051215 18:50	20051215 19:21:48	20051215 19:23:40	20051215 19:31	2	5
621.00	626.00	20051215 19:44	20051215 20:21:06	20051215 20:41:34	20051215 21:03	20	20

Test section secup	Test section seclow	Test start	Start of flow period	Stop of flow period	Test stop	Total flow time t_p	Total recovery time t_F
(m)	(m)	YYYYMMDD hh:mm	YYYYMMDD hh:mm:ss	YYYYMMDD hh:mm:ss	YYYYMMDD hh:mm	(min)	(min)
626.00	631.00	20051215 21:14	20051215 21:45:46	20051215 21:54:10	20051215 22:01	8	5
631.00	636.00	20051215 22:08	20051215 22:51:11	20051215 23:11:40	20051215 23:33	20	20
636.00	641.00	20051215 23:43	20051216 00:15:28	20051216 00:35:56	20051216 00:58	20	20
641.00	646.00	20051216 08:21	20051216 08:53:39	20051216 09:14:01	20051216 09:36	20	20
646.00	651.00	20051216 09:55	20051216 10:28:16	20051216 10:31:02	20051216 10:38	3	5
651.00	656.00	20051216 10:53	20051216 11:27:51	20051216 11:48:20	20051216 12:10	20	20
656.00	661.00	20051216 12:21	20051216 13:03:34	20051216 13:12:30	20051216 13:20	9	5
661.00	666.00	20051216 13:31	20051216 14:04:48	20051216 14:06:57	20051216 14:14	2	5
731.00	736.00	20051219 08:19	20051219 08:52:49	20051219 08:54:27	20051219 09:01	2	5
736.00	741.00	20051219 09:15	20051219 09:46:55	20051219 09:49:06	20051219 09:56	2	5
741.00	746.00	20051219 10:11	20051219 10:47:39	20051219 11:08:09	20051219 11:30	21	20
746.00	751.00	20051219 11:44	20051219 12:22:11	20051219 12:29:10	20051219 12:36	7	5
751.00	756.00	20051219 12:50	20051219 13:23:07	20051219 13:43:35	20051219 14:05	20	20
756.00	761.00	20051219 14:20	20051219 15:00:30	20051219 15:20:59	20051219 15:42	20	20
761.00	766.00	20051219 15:56	20051219 16:33:37	20051219 16:54:07	20051219 17:16	21	20
766.00	771.00	20051220 06:55	20051220 07:28:05	20051220 07:48:28	20051220 08:10	20	20
771.00	776.00	20051220 08:29	20051220 09:04:02	20051220 09:24:27	20051220 09:46	20	20
776.00	781.00	20051220 10:06	20051220 10:41:52	20051220 11:02:21	20051220 11:24	20	20
781.00	786.00	20051220 11:35	20051220 12:15:53	20051220 12:36:19	20051220 12:58	20	20
786.00	791.00	20051220 13:11	20051220 13:46:19	20051220 14:06:43	20051220 14:28	20	20
506.00 [1)]	606.00	20051118 13:32	20051118 14:18:02	20051118 14:26:00	20051118 14:28	8	0
426.00 [1)]	446.00	20051130 17:10	20051130 17:43:55	20051130 17:56:57	20051130 18:03	13	4
116.00 [1)]	121.00	20051207 10:38	20051207 12:36:48	20051207 12:38:34	20051207 12:39	2	0

[1)] The tests were interrupted for various reasons or did not provide satisfying data for the evaluation and were hence re-performed later

Appendix 2.2 Pressure and flow data

Summary of pressure and flow data for all tests in KFM09A

Test section		Pressure			Flow		
secup	seclow	p_i	p_p	p_F	Q_p 1)	Q_m 2)	V_p 2)
(m)	(m)	(kPa)	(kPa)	(kPa)	(m^3/s)	(m^3/s)	(m^3)
106.00	206.00	929.78	1114.19	948.54	7.07E-05	9.33E-05	1.70E-01
206.00	306.00	1746.27	1963.05	1759.94	1.31E-06	1.62E-06	2.95E-03
306.00	406.00	2542.61	2753.18	2631.48	4.06E-06	7.19E-06	1.31E-02
406.00	506.00	3314.26	3517.7	3472.12	1.07E-05	3.77E-05	6.87E-02
506.00	606.00	4075.97	4296.2	4263.63	1.94E-06	8.12E-06	1.48E-02
606.00	706.00	4781.92	4987.26	4843.19	5.72E-07	8.03E-07	1.46E-03
691.00	791.00	5371.98	5548.07	5405.64	8.41E-07	1.23E-06	2.24E-03
106.00	126.00	939.44	1152.92	946.07	8.47E-06	9.98E-06	1.22E-02
126.00	146.00	1108.5	1324.71	1158.02	2.71E-05	4.44E-05	5.40E-02
146.00	166.00	1277.24	1460	1389.29	4.5E-06	1.26E-05	1.54E-02
166.00	186.00	1439.66	1628.85	1451.67	4.24E-05	4.98E-05	6.07E-02
186.00	206.00	1609	1908.7	1627.19	1.41E-07	1.63E-07	1.99E-04
206.00	226.00	1799.82	1971.07	1959.47			
226.00	246.00	1936.29	2142.18	1942.92	9.72E-07	1.18E-06	1.45E-03
238.00	258.00	2036.61	2246.5	2073.17	2.46E-07	3.84E-07	4.70E-04
258.00	278.00	2205.79	2409.18	2271.89	5.18E-08	9.9E-08	1.22E-04
278.00	298.00	2363.51	2574.6	2423.68	1.11E-07	1.57E-07	1.92E-04
286.00	306.00	2426.85	2640.1	2497.64	6.13E-08	9.62E-08	1.19E-04
306.00	326.00	2588.71	2788.52	2720.63	2.78E-07	6.73E-07	8.23E-04
326.00	346.00	2751.68	2952.8	2816.12	2.09E-08	4.56E-08	5.58E-05
346.00	366.00	2908.57	3113.84	2949.69	4.37E-08	5.89E-08	7.20E-05
366.00	386.00	3063.39	3264.59	3103.70	1.28E-06	1.6E-06	1.98E-03
386.00	406.00	3219.88	3419.73	3326.14	2.69E-06	5.5E-06	6.80E-03
406.00	426.00	3378.16	3578.01	3432.11	3.99E-07	4.89E-07	6.05E-04
426.00	446.00	3545.41	3765.49	3714.71	1.85E-05	4.93E-05	6.10E-02
446.00	466.00	3693.33	3922.81	3730.72	7.09E-08	9.94E-08	1.23E-04
466.00	486.00	3856.58	4029.33	3923.36	4E-08	7.55E-08	9.52E-05
486.00	506.00	4001.32	4206.1	4108.27	1.17E-07	2.67E-07	3.27E-04
506.00	526.00	4171.74	4362.23	4210.38	4.34E-08	7.76E-08	9.50E-05
526.00	546.00	4303.1	4508.03	4472.57	2.91E-06	9.83E-06	1.20E-02
545.00	565.00	4514.1	4661.19	4675.69			
566.00	586.00	4631.11	4820.31	4823.61			
586.00	606.00	4765.93	4982.58	4989.21			
606.00	626.00	4896.47	5096.82	4980.92	4.76E-07	7.39E-07	9.01E-04
626.00	646.00	5050.61	5258.42	5072.55	8.54E-08	1.15E-07	1.41E-04
646.00	666.00	5186.25	5389.93	5211.64	1.04E-07	1.27E-07	1.55E-04
666.00	686.00	5355.15	5533.99	5469.96	1.19E-08	3.11E-08	3.74E-05
686.00	706.00	5498.11	5687.43	5619.55	9.44E-09	2.33E-08	2.81E-05
691.00	711.00	5561.73	5724.42	5713.38			
711.00	731.00	5679.43	5864.34	5869.58			
731.00	751.00	5782.93	5995.56	5819.36	6.26E-08	8.05E-08	9.84E-05
751.00	771.00	5915.12	6118.38	1406.62	3.61E-07	1.07E-07	1.31E-04
771.00	791.00	6056.14	6271.55	1456.30	8.9E-07	4.69E-05	5.72E-02
106.00	111.00	948.9	1151.62	995.96	5.7E-07	6.88E-07	8.42E-04
111.00	116.00	993.19	1200.74	1037.91	6E-08	7.52E-08	9.20E-05
116.00	121.00	1025.62	1225.72	1627.41	2.15E-06	1.42E-07	1.73E-04
121.00	126.00	1074.34	1252.7	1076.55	5.98E-06	6.93E-06	8.47E-03
126.00	131.00	1121.53	1323.83	1249.86	3.85E-08	1.12E-07	1.37E-04
128.00	133.00	1131.88	1348.66	1163.76	1.74E-05	2.61E-05	3.18E-02
133.00	138.00	1174.24	1409.45	1217.29	1.66E-05	2.67E-05	3.21E-02
138.00	143.00	1215.08	1415.79	1219.50	3.09E-07	3.51E-07	4.28E-04
141.00	146.00	1240.89	1466.23	1321.06	1.24E-06	2.35E-06	2.88E-03
146.00	151.00	1284.09	1510.35	1450.22	1.33E-06	5.33E-06	6.51E-03
151.00	156.00	1349.21	1565.72	1571.10			
156.00	161.00	1365.5	1573.1	1482.79	4.26E-06	1.07E-05	1.31E-02
161.00	166.00	1408	1586.5	1406.62	1.02E-07	1.07E-07	1.31E-04
166.00	171.00	1447.05	1626.8	1456.30	4.09E-05	4.69E-05	5.72E-02
171.00	176.00	1496.45	1703.03	1687.02	5.5E-08	8.37E-07	1.03E-03
176.00	181.00	1534	1734.49	1557.86	2.91E-07	3.41E-07	4.15E-04
181.00	186.00	1575.38	1803.9	1780.30	2.5E-07	1.9E-06	2.35E-03
186.00	191.00	1616.92	1832.6	1627.41	1.23E-07	1.42E-07	1.73E-04
191.00	196.00	1677.49	1875.23	1828.87			
196.00	201.00	1710.62	1916.5	1891.79			
201.00	206.00	1766.78	1957.48	1965.21			
226.00	231.00	1961.89	2161.15	2158.94			

Test section		Pressure			Flow		
secup	seclow	p_i	p_p	p_F	Q_p 1)	Q_m 2)	V_p 2)
(m)	(m)	(kPa)	(kPa)	(kPa)	(m^3/s)	(m^3/s)	(m^3)
232.00	237.00	1992.95	2191.65	1995.02	8.39E-07	8.63E-07	1.05E-03
237.00	242.00	2032.55	2232.77	2040.28	1.7E-06	1.86E-06	2.27E-03
240.80	245.80	2060.01	2263.69	2071.18	3.22E-07	4.57E-07	5.58E-04
246.80	251.80	2184.89	2323.99	2971.99			
251.50	256.50	2217.45	2385.25	2408.43			
256.50	261.50	2239.39	2427.2	2424.45			
273.00	278.00	2328.68	2560.78	2393.53	6.8E-08	1E-07	1.22E-04
278.00	283.00	2369.8	2576.3	2435.48	9.75E-08	1.44E-07	1.76E-04
283.00	288.00	2409.26	2618.73	2574.58			
288.00	293.00	2459.9	2659.88	2540.35	1.57E-08	2.83E-08	3.40E-05
293.00	298.00	2493.43	2728	2549.74	3.38E-08	4.1E-08	5.00E-05
296.00	301.00	2521.45	2730.23	3349.53			
301.00	306.00	2567.81	2767.21	3301.51			
306.00	311.00	2678.48	2831.8	2864.35			
311.00	316.00	2652.96	2872.36	2868.77			
316.00	321.00	2674.48	2942.73	2935.01			
321.00	326.00	2712.56	2913.42	2845.04	2.98E-07	6.68E-07	8.16E-04
346.00	351.00	3017.39	3117.02	3125.44			
351.00	356.00	2958.18	3169.22	3512.92	5.07E-08	6.9E-08	8.44E-05
356.00	361.00	2991.17	3206.99	3532.23			
361.00	366.00	3026.221	3242.46	3698.38	1.76E-08	9.48E-09	1.14E-05
363.00	368.00	3062.65	3254.73	3095.07	1.17E-08	1.62E-08	1.95E-05
368.00	373.00	3128.47	3316.41	3294.88			
371.00	376.00	3108.19	3309.5	3140.33	1.47E-06	2.13E-06	2.12E-03
376.00	381.00	3174.01	3361.53	3334.08			
381.00	386.00	3234.58	3403.07	3284.95			
386.00	391.00	3226.58	3437.98	3349.53	2.47E-06	5.33E-06	6.53E-03
391.00	396.00	3274.47	3481.73	3301.51	1.66E-07	1.87E-07	2.29E-04
396.00	401.00	3321.1	3524.5	3485.87			
401.00	406.00	3346.08	3547.69	3369.95	4.26E-07	4.98E-07	6.09E-04
406.00	411.00	3392.03	3584.11	3550.45			
411.00	416.00	3426.25	3621.31	3496.35	3.7E-07	5.52E-07	6.76E-04
414.00	419.00	3460.47	3654.12	3480.91	1.3E-08	1.05E-08	1.27E-05
419.00	424.00	3488.626	3692.58	3512.92	5.68E-08	6.9E-08	8.44E-05
421.00	426.00	3515	3708.32	3532.23	5.78E-08	7.13E-08	8.73E-05
426.00	431.00	3560.79	3773.3	3698.38			
431.00	436.00	3579.7	3802.83	3753.02	1.61E-05	5.02E-05	6.15E-02
436.00	441.00	3649.79	3829.74	3837.47			
441.00	446.00	3661.4	3888.2	3871.14	2.09E-07	1.94E-06	2.41E-03
446.00	451.00	3702.236	3909.77	3866.72	3.75E-08	1.55E-07	1.90E-04
451.00	456.00	3761.02	3951.96	3840.22	1.24E-08	1.48E-08	1.78E-05
456.00	461.00	3787.78	3990.92	3815.94	6.76E-08	5.9E-08	7.22E-05
461.00	466.00	3916.81	4031.76	4071.50			
471.00	476.00	3902.457	4111.1	3964.42	5.28E-08	7.96E-08	9.75E-05
476.00	481.00	3964.425	4153.74	4008.03	4.27E-08	5.18E-08	6.33E-05
486.00	491.00	4047.08	4229.36	4217.76			
491.00	496.00	4063.22	4261.51	4095.23	7.8E-08	1.03E-07	1.26E-04
496.00	501.00	4090.13	4297.53	4222.18	6.24E-08	1.75E-07	2.15E-04
501.00	506.00	4165.19	4330.23	4289.52			
506.00	511.00	4215.56	4366.8	4289.52	1.64E-08	1.77E-08	2.13E-05
511.00	516.00	4232.67	4403.23	4229.36	2.98E-08	2.82E-08	3.44E-05
516.00	521.00	4254.199	4440.03	4285.67	1.94E-08	2.24E-08	2.70E-05
521.00	526.00	4405.3	4484.51	4539.01			
526.00	531.00	4442.14	4520.81	4592.00			
531.00	536.00	4354.65	4571.03	4535.15	2.91E-06	1.06E-05	1.30E-02
536.00	541.00	4479.13	4594.76	4560.54			
541.00	546.00	4437.45	4632.29	4613.53	8.67E-09	5.55E-08	6.67E-05
561.00	566.00	4726.95	4774.42	4801.19			
606.00	611.00	5042.26	5120.24	5224.00			
611.00	616.00	4956.43	5148.26	5044.06	3.96E-07	6.14E-07	7.50E-04
616.00	621.00	5077.59	5206.34	5272.02			
621.00	626.00	5032.46	5244.56	5127.97	1.53E-07	2.22E-07	2.73E-04
626.00	631.00	5085.18	5263.75	5233.38			
631.00	636.00	5136.79	5301.28	5249.39	1.17E-08	2.06E-08	2.47E-05
636.00	641.00	5144.52	5335.36	5146.73	1.35E-07	1.34E-07	1.64E-04
641.00	646.00	5195.3	5374.69	5235.59	1.27E-08	9.09E-07	1.11E-03
646.00	651.00	5309.69	5410.56	5419.40			
651.00	656.00	5248.56	5444.23	5280.30	1.27E-07	2.02E-05	9.65E-03
656.00	661.00	5344.46	5486.74	5472.94			
661.00	666.00	5426.71	5523.99	5534.21			
731.00	736.00	5867.31	6009.44	5986.26			

Test section		Pressure			Flow		
secup	seclow	p_i	p_p	p_F	Q_p [1]	Q_m [2]	V_p [2]
(m)	(m)	(kPa)	(kPa)	(kPa)	(m^3/s)	(m^3/s)	(m^3)
736.00	741.00	5860.27	6044.22	5996.20			
741.00	746.00	5881.11	6078.44	5914.50	8.87E-08	7.57E-08	9.31E-05
746.00	751.00	5928.44	6112.66	6074.02			
751.00	756.00	5957.42	6143.29	6000.07	7.95E-08	1.26E-07	1.55E-04
756.00	761.00	5986.68	6192.63	6040.91	2.15E-07	3.66E-07	4.51E-04
761.00	766.00	6021.04	6221.97	6050.29	1.07E-07	1.57E-07	1.92E-04
766.00	771.00	6049.32	6239.82	6077.34	5.47E-08	7.57E-08	9.27E-05
771.00	776.00	6086.85	6319.41	6096.65	5.99E-08	6.39E-08	7.84E-05
776.00	781.00	6119.15	6309.34	6137.49	1.15E-07	1.4E-07	1.71E-04
781.00	786.00	6152.12	6325.44	6168.40	1.85E-07	2.36E-07	2.90E-04
786.00	791.00	6184.96	6388.23	6192.69	7.06E-07	9.09E-07	1.11E-03
506.00 [3]	606.00	4063.27	4265.15	4264.74			
426.00 [3]	446.00	3535.19	3703.67	3675.53			
116.00 [3]	121.00	1074.89	1242.69	1074.34			

[1] No value indicates a flow below measurement limit (measurement limit is unique for each test but nominally 1.67 E-8 m^3/s).
[2] No value indicates that the parameter could not be calculated due to low and uncertain flow rates during a major part of flow period
[3] The tests were interrupted for various reasons or did not provide satisfying data for the evaluation and were hence re-performed later.

p_i	Pressure in test section before start of flow period
p_p	Pressure in test section before stop of flow period
p_F	Pressure in test section at the end of recovery period
Q_p	Flow rate just before stop of flow period
Q_m	Mean (arithmetic) flow rate during flow period
V_p	Total volume injected during the flow period

Appendix 3. Test diagrams – Injection Tests

In the following pages diagrams are presented for all test sections. A linear diagram of pressure and flow rate is presented for each test. For most tests are lin-log and log-log diagrams presented, from injection and recovery period respectively.

Nomenclature for Aqtesolv:

T	=	transmissivity (m^2/s)
S	=	storativity (-)
K_z/K_r	=	ratio of hydraulic conductivities in the vertical and radial direction (set to 1)
Sw	=	skin factor
r(w)	=	borehole radius (m)
r(c)	=	effective casing radius (m)
C	=	well loss constant (set to 0)
r/B	=	leakage factor (-)

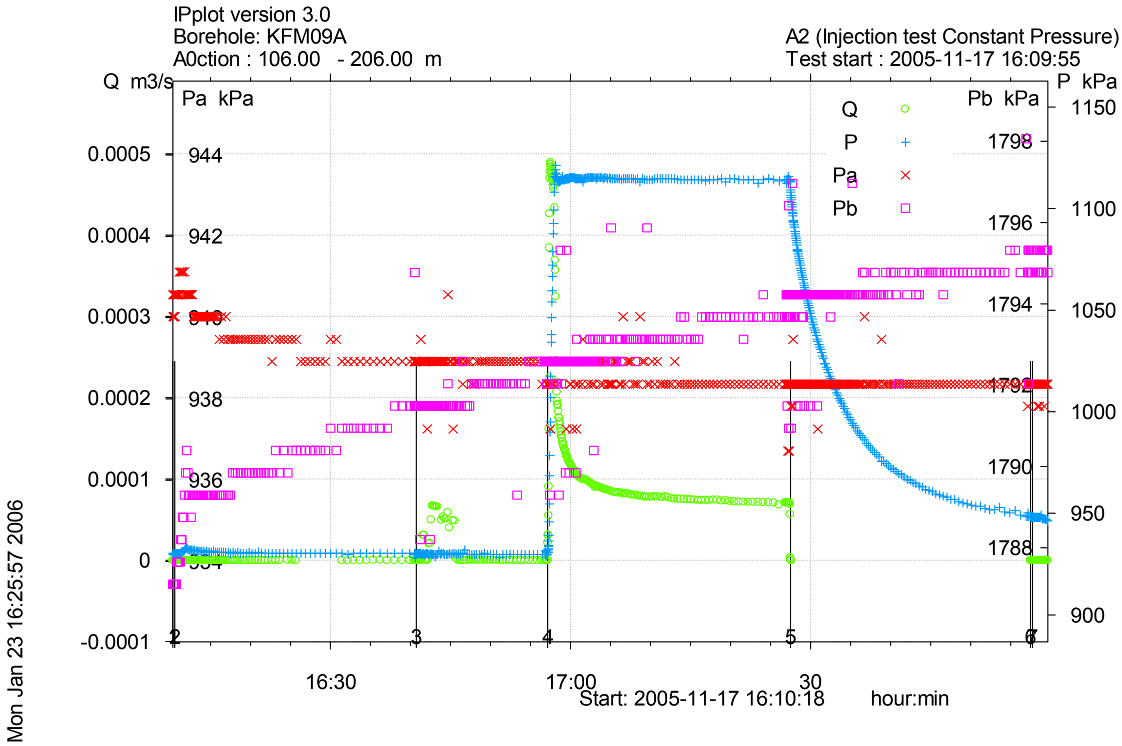


Figure A3-2. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 106.0-206.0 m in borehole KFM09A.*

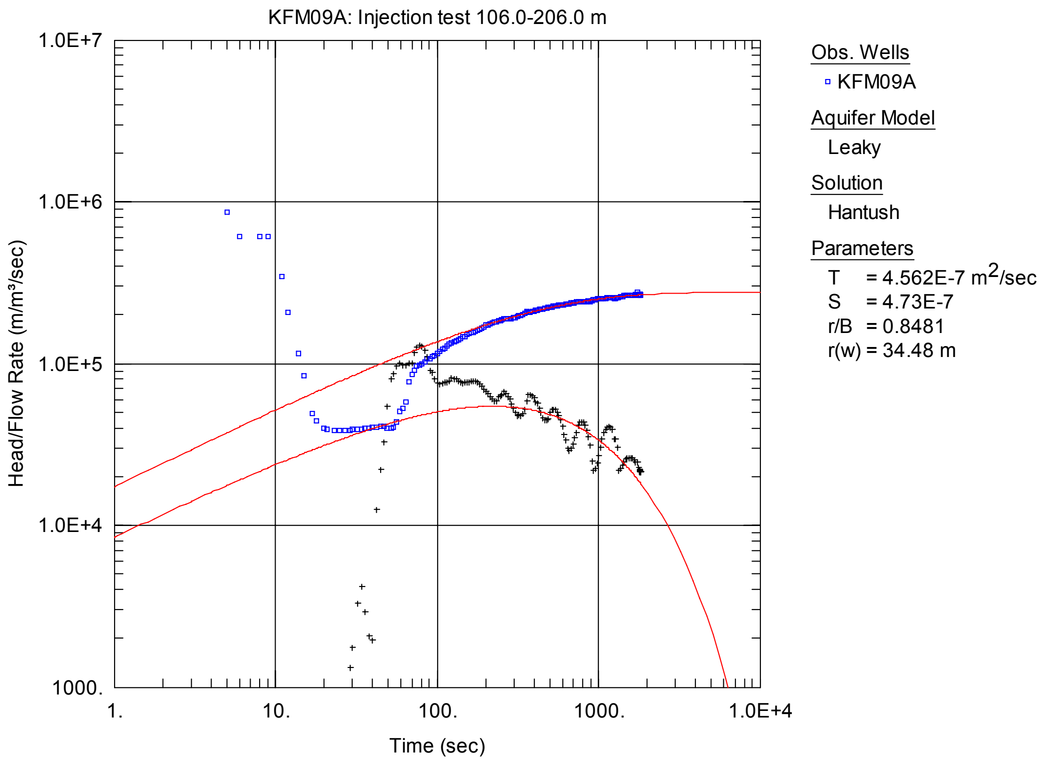


Figure A3-3. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 106.0-206.0 m in KFM09A.*

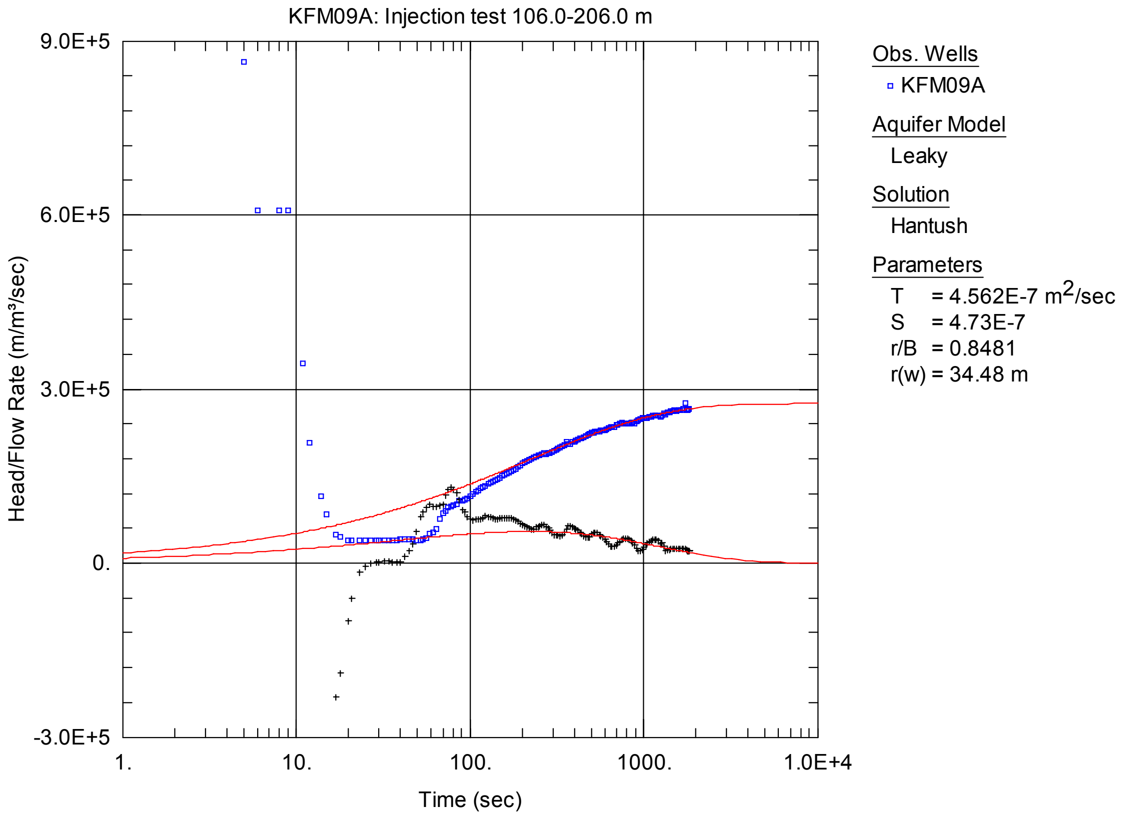


Figure A3-4. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 106.0-206.0 m in KFM09A.*

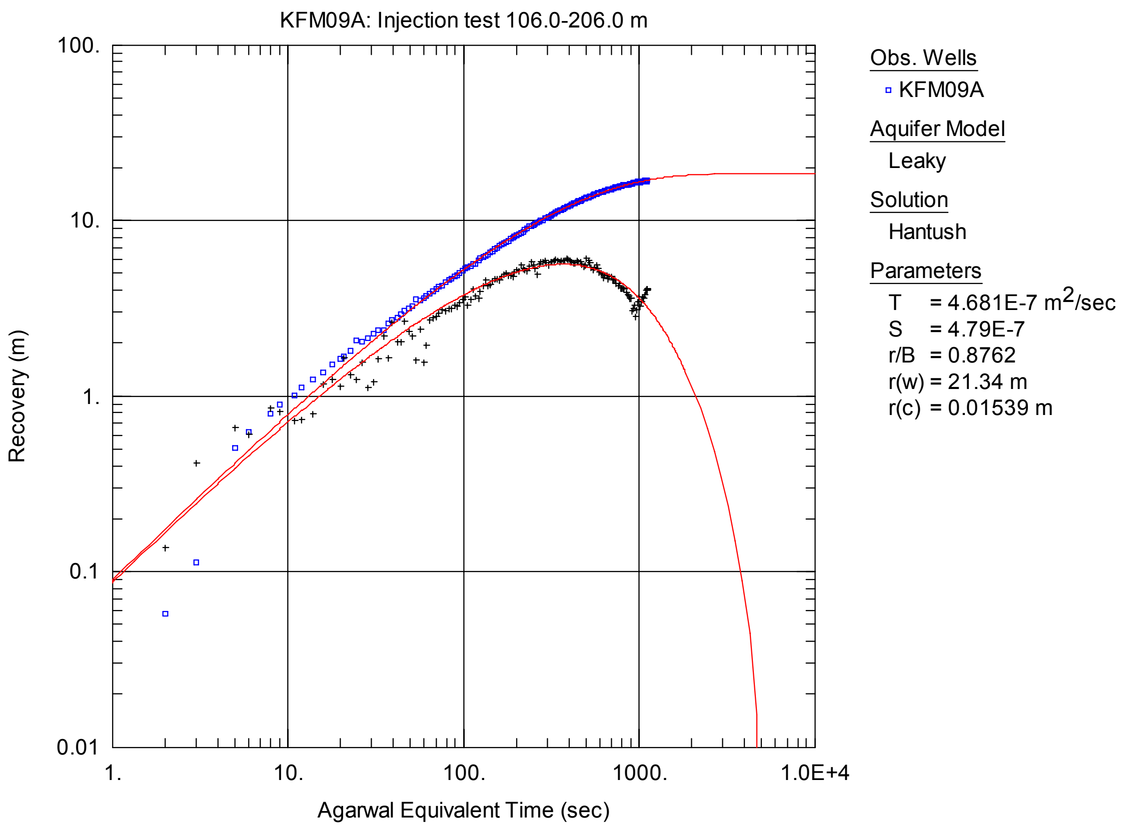


Figure A3-5. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 106.0-206.0 m in KFM09A.*

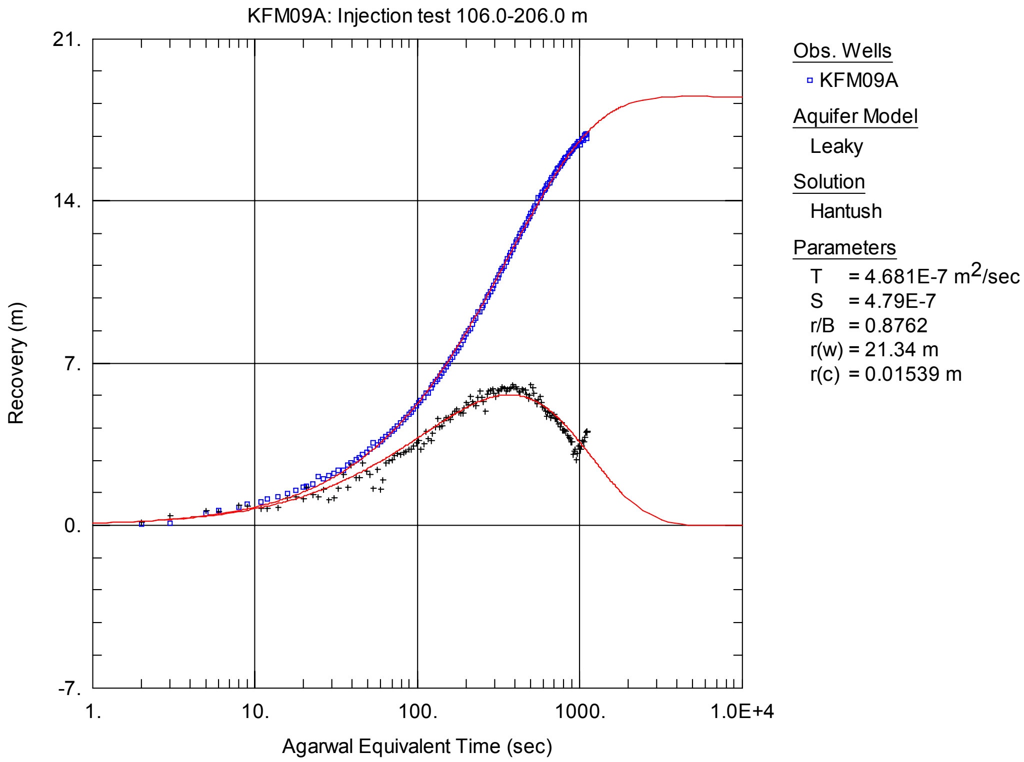


Figure A3-6. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 106.0-206.0 m in KFM09A.*

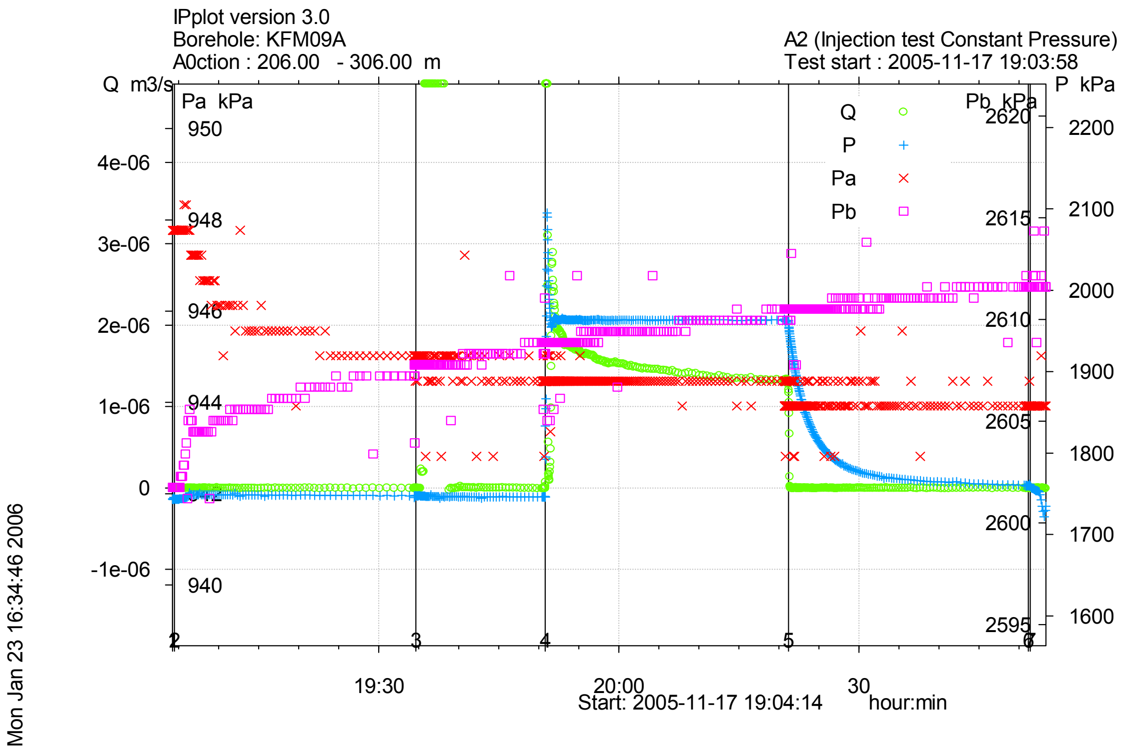


Figure A3-7. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 206.0-306.0 m in borehole KFM09A.*

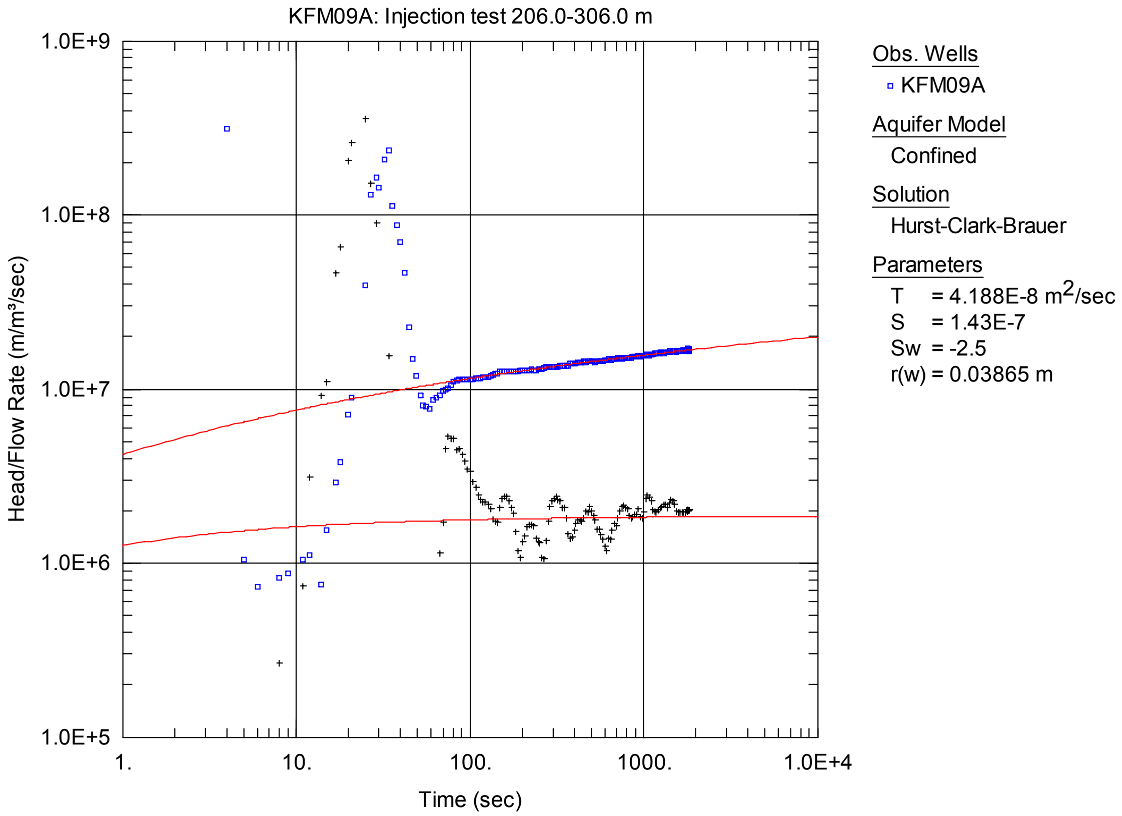


Figure A3-8. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 206.0-306.0 m in KFM09A.*

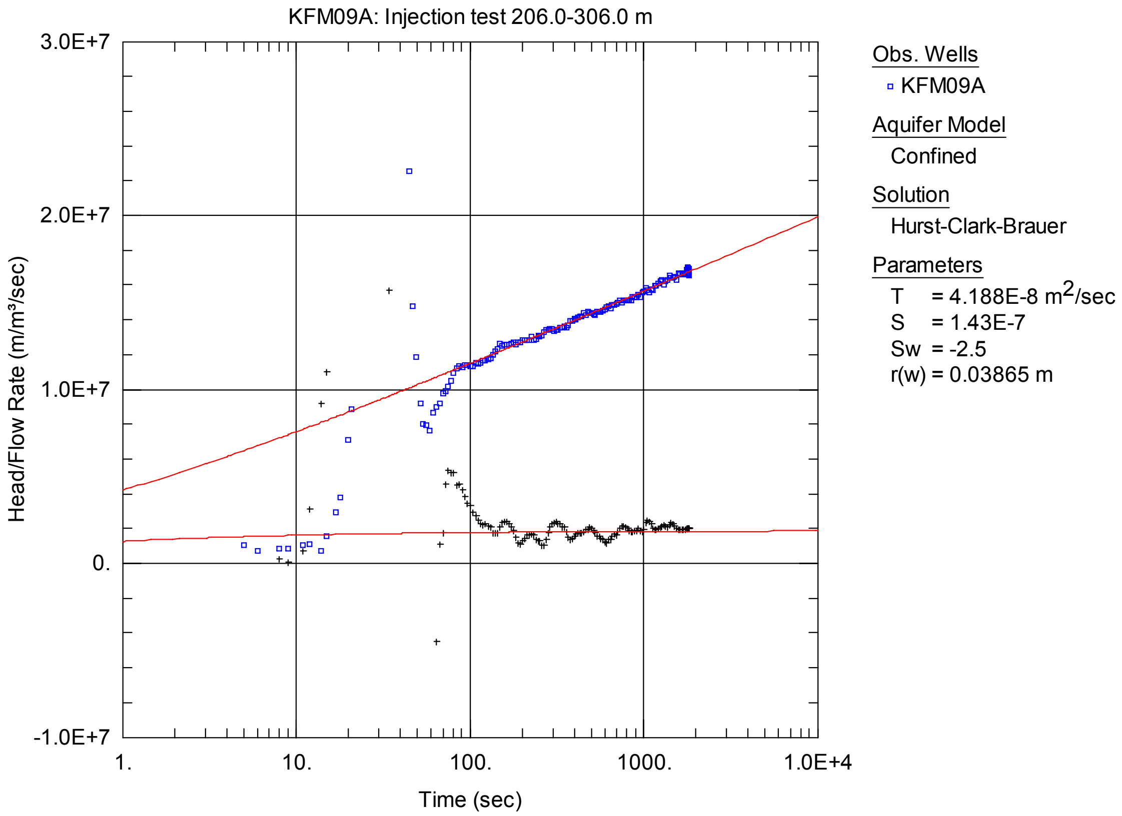


Figure A3-9. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 206.0-306.0 m in KFM09A.*

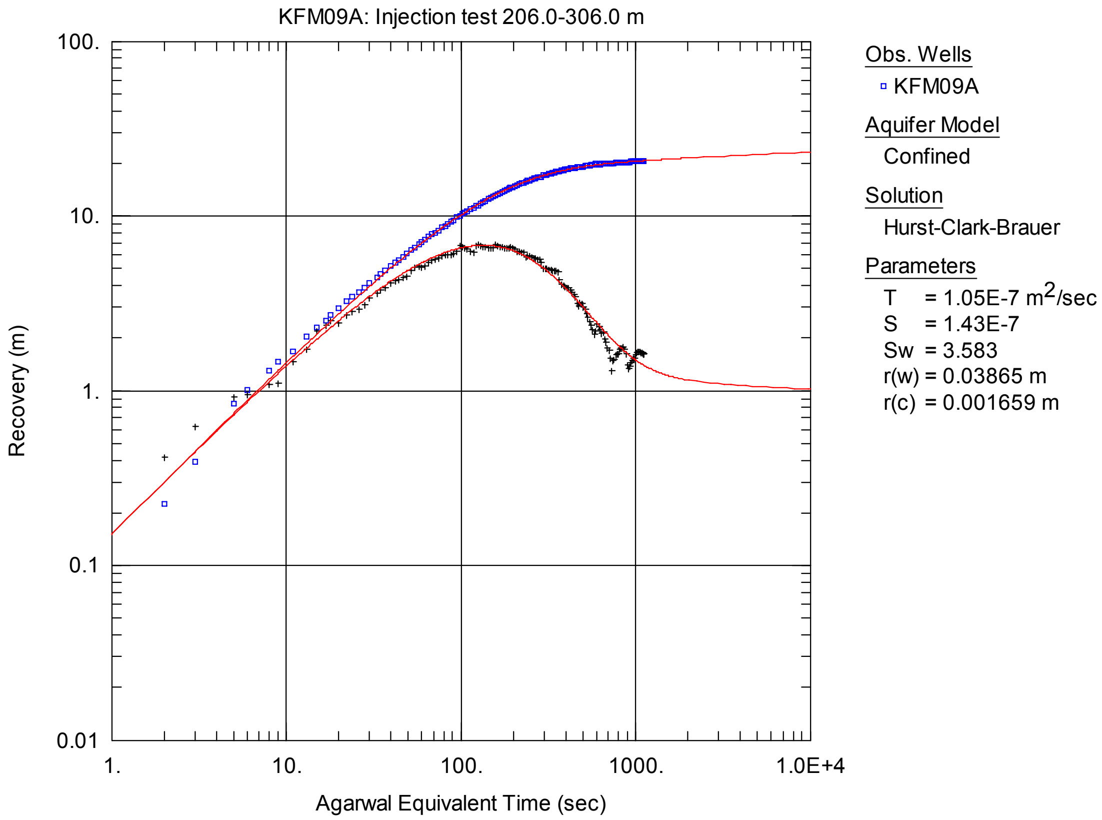


Figure A3-10. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 206.0-306.0 m in KFM09A.*

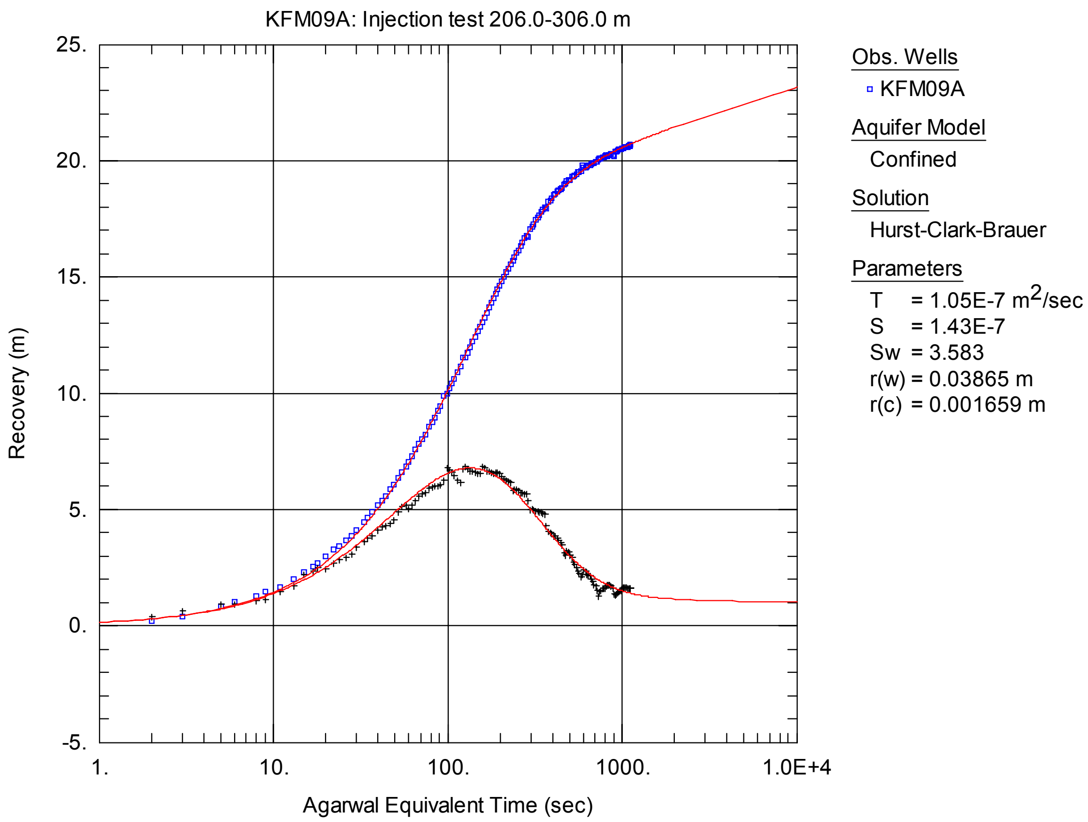


Figure A3-11. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 206.0-306.0 m in KFM09A.*

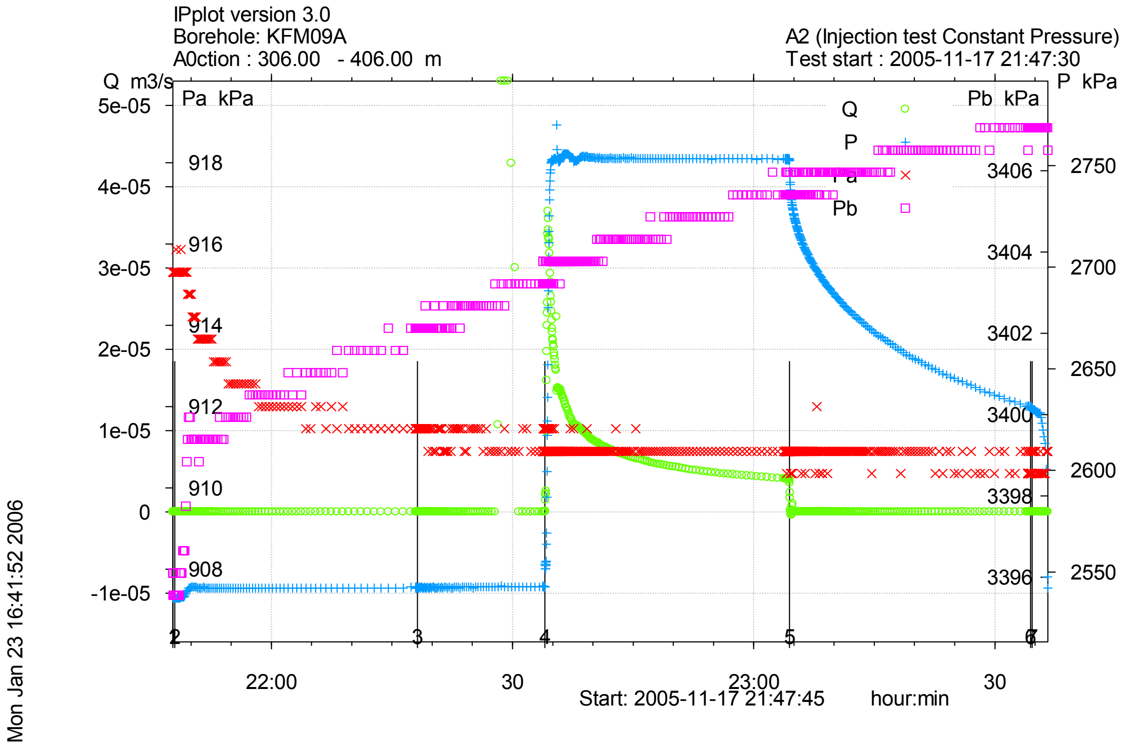


Figure A3-12. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 306.0-406.0 m in borehole KFM09A.*

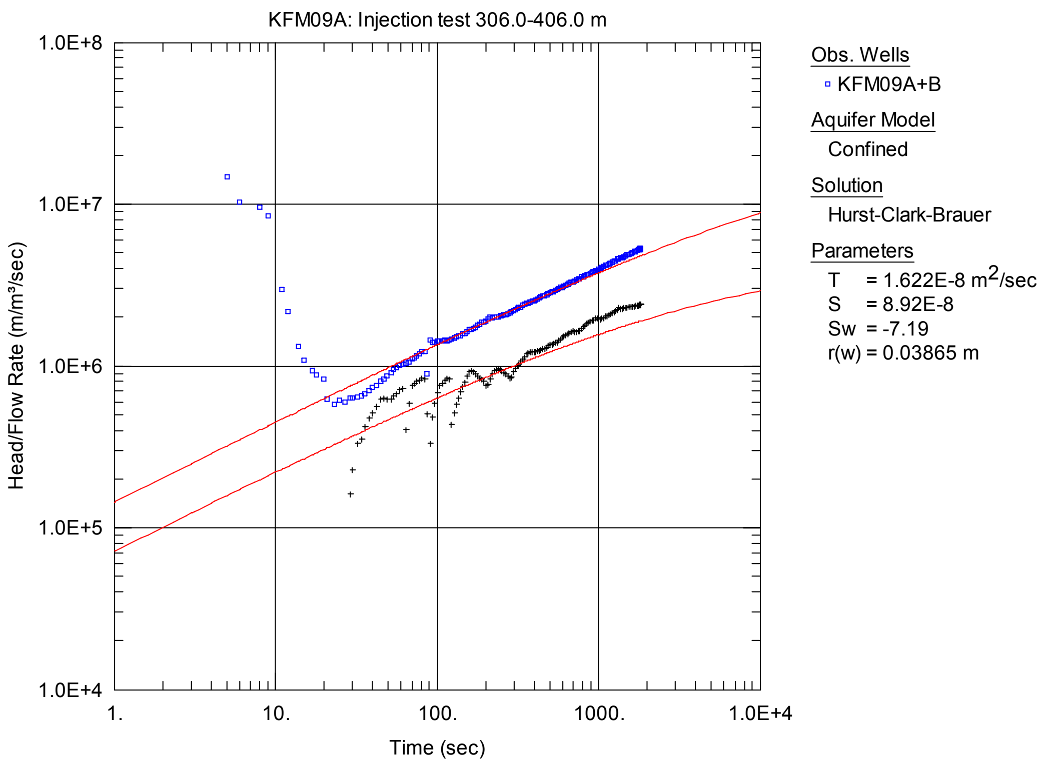


Figure A3-13. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 306.0-406.0 m in KFM09A.*

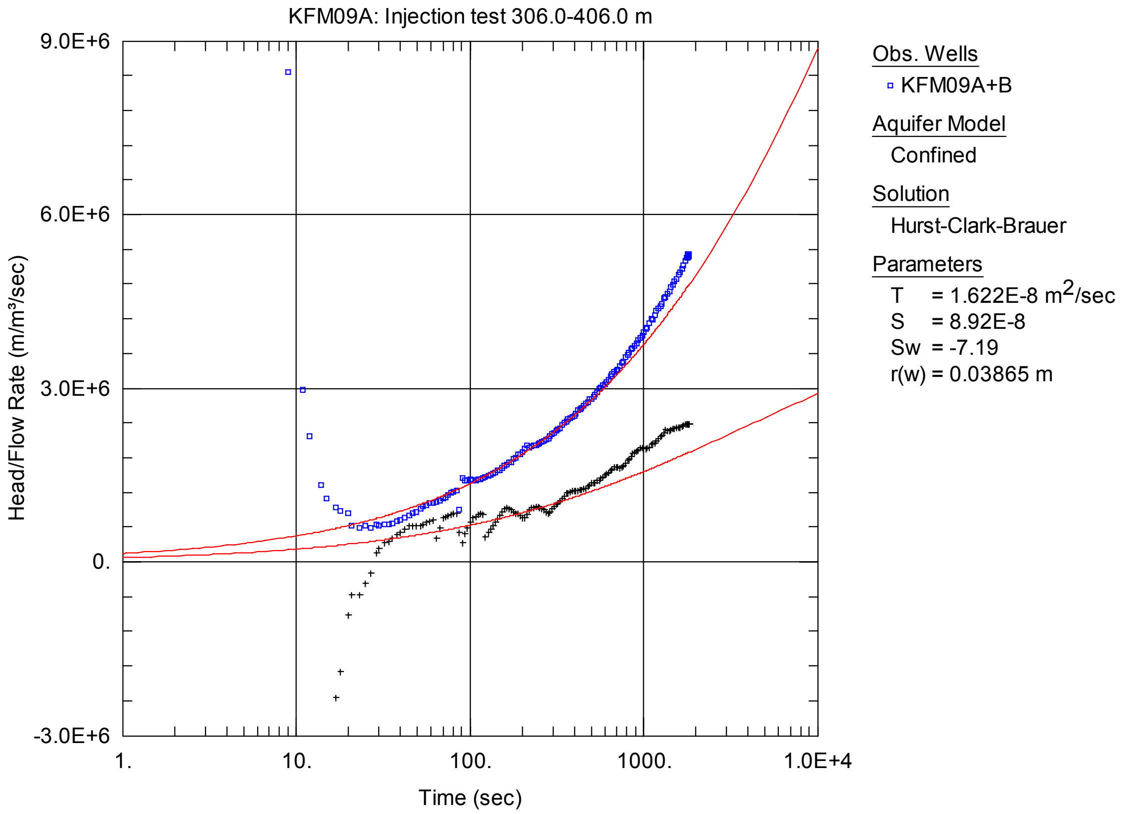


Figure A3-14. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 306.0-406.0 m in KFM09A.*

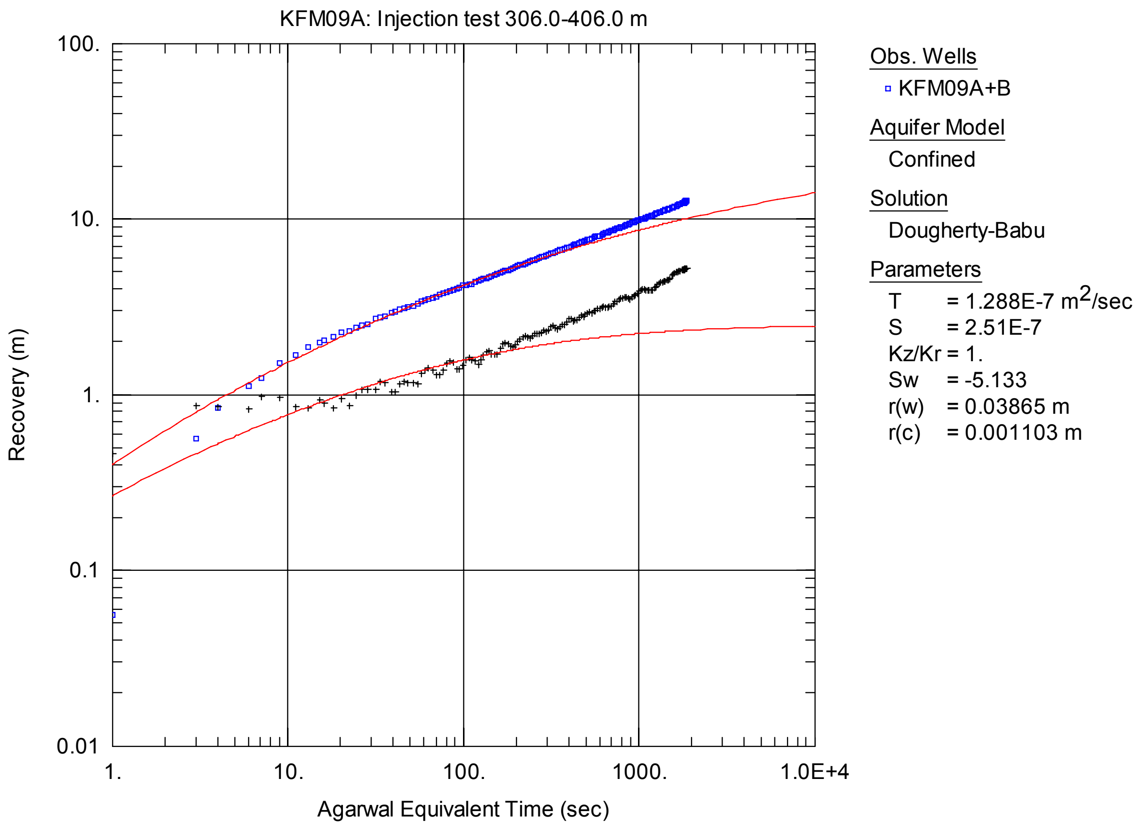


Figure A3-15. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 306.0-406.0x m in KFM09A.*

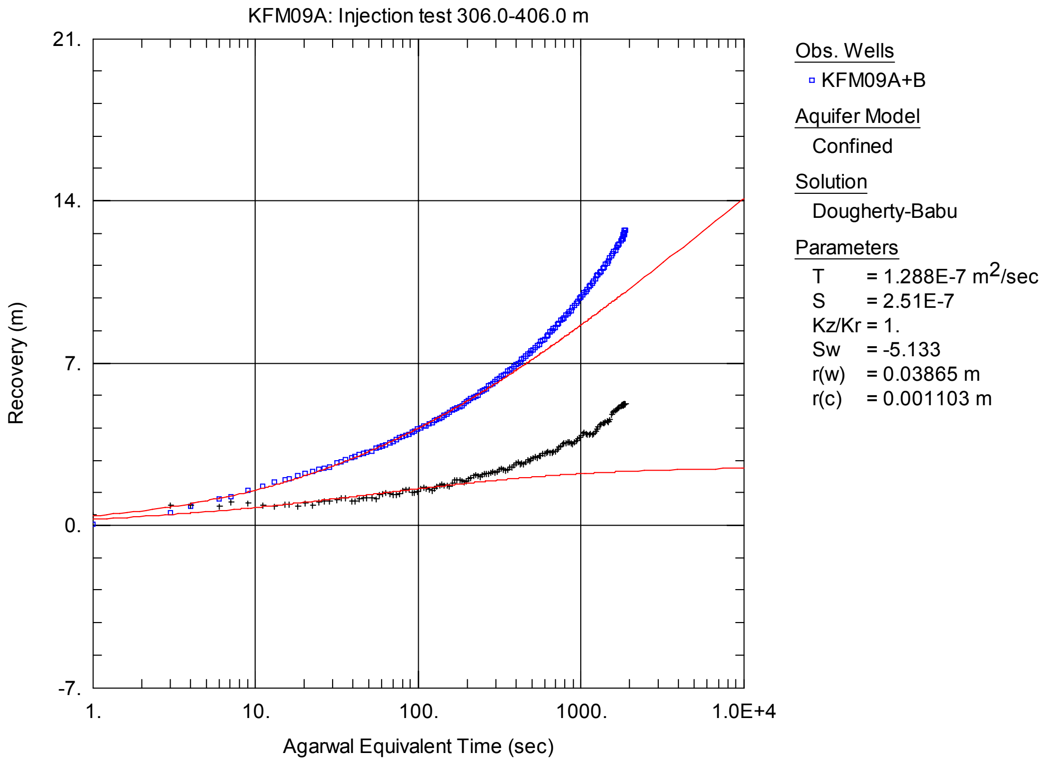


Figure A3-16. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 306.0-406.0 m in KFM09A.*

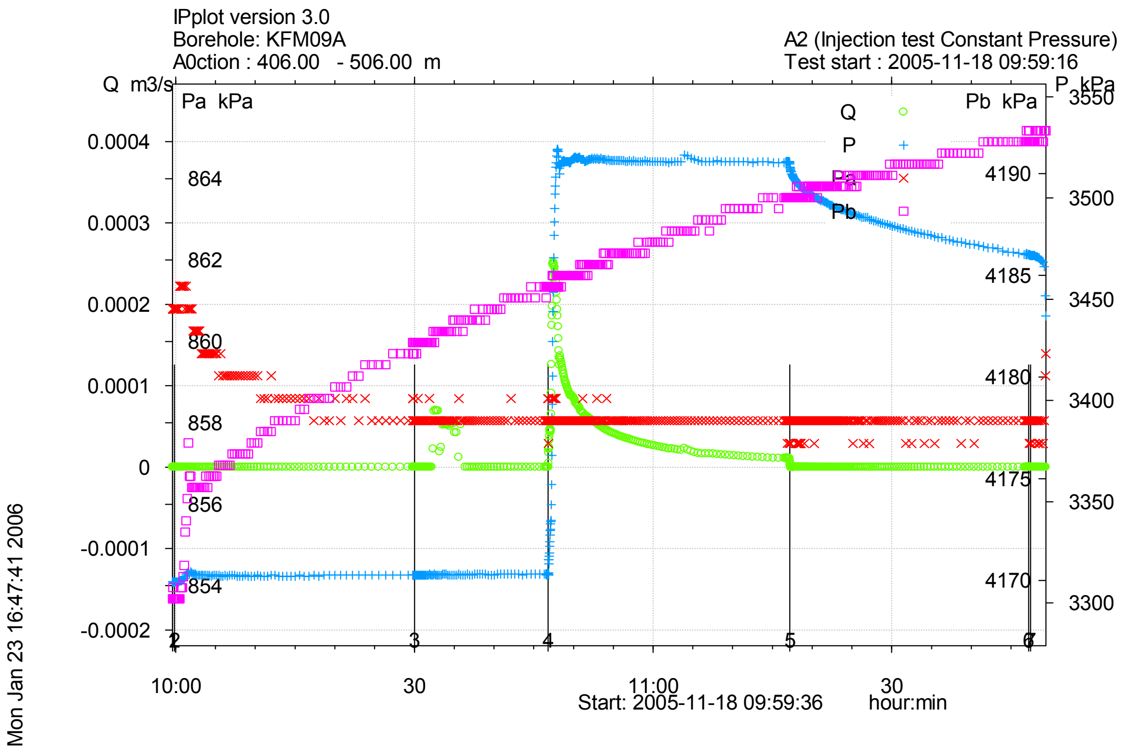


Figure A3-17. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 406.0-506.0 m in borehole KFM09A.*

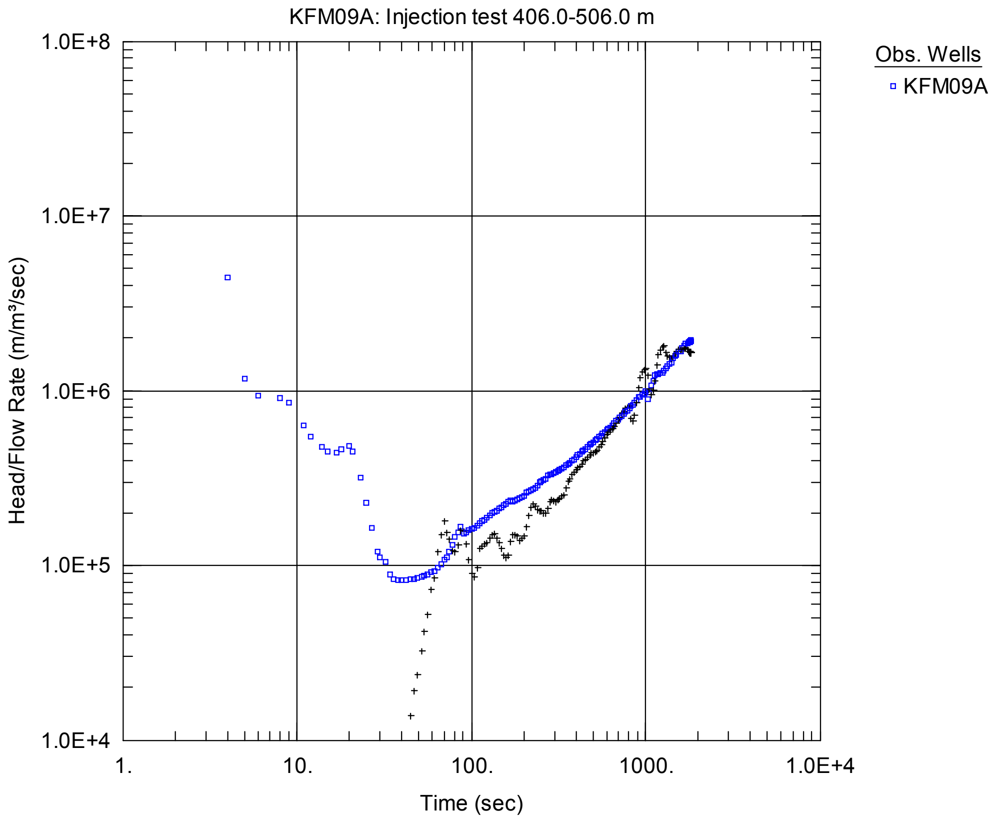


Figure A3-18. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 406.0-506.0 m in KFM09A.*

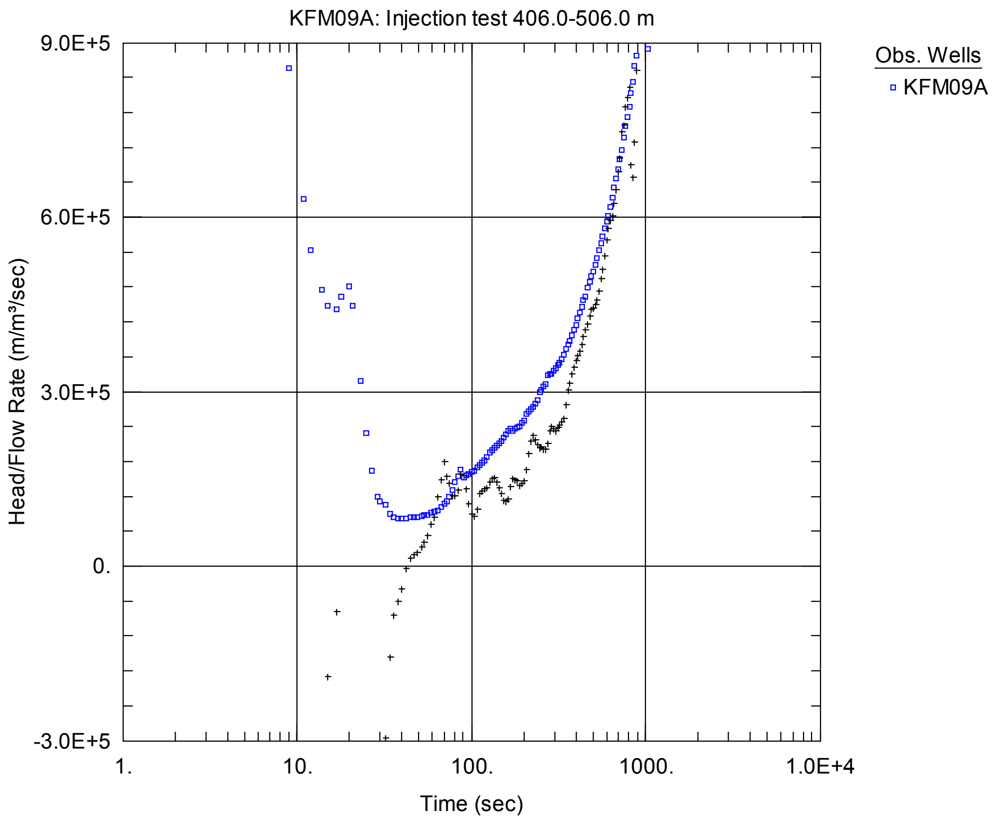


Figure A3-19. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 406.0-506.0 m in KFM09A.*

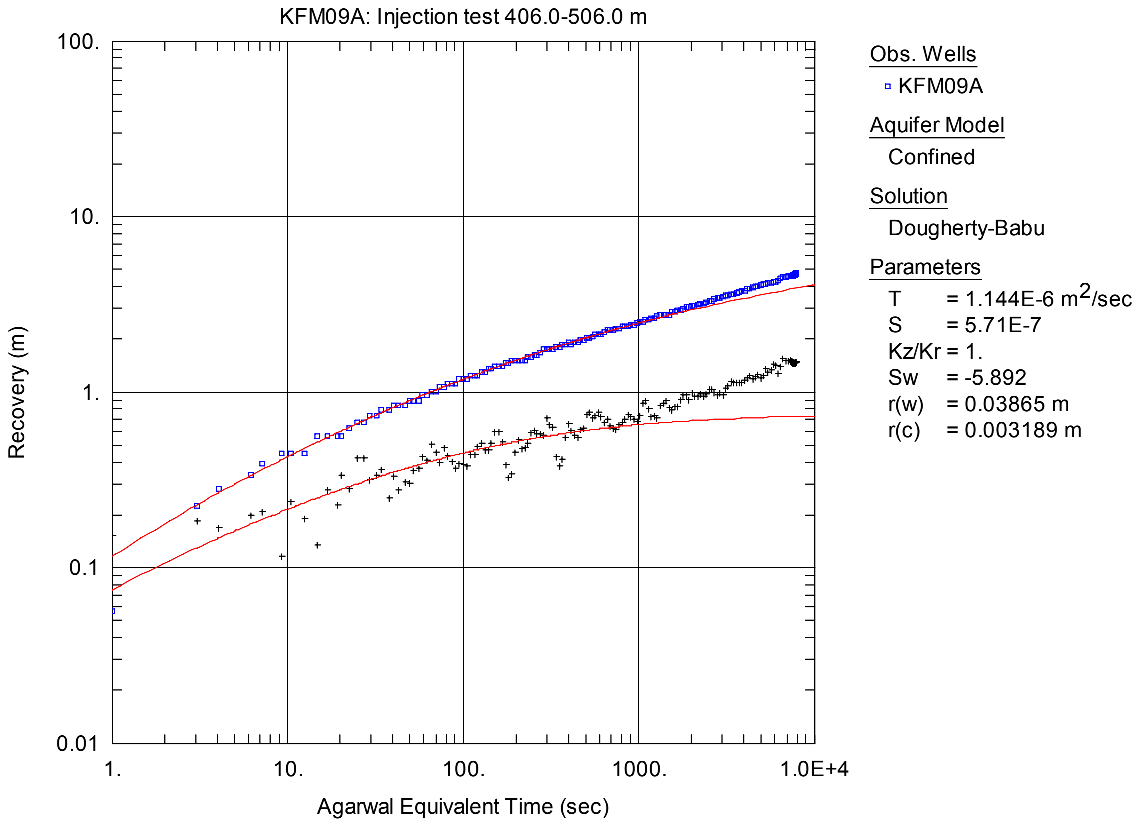


Figure A3-20. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 406.0-506.0 m in KFM09A.*

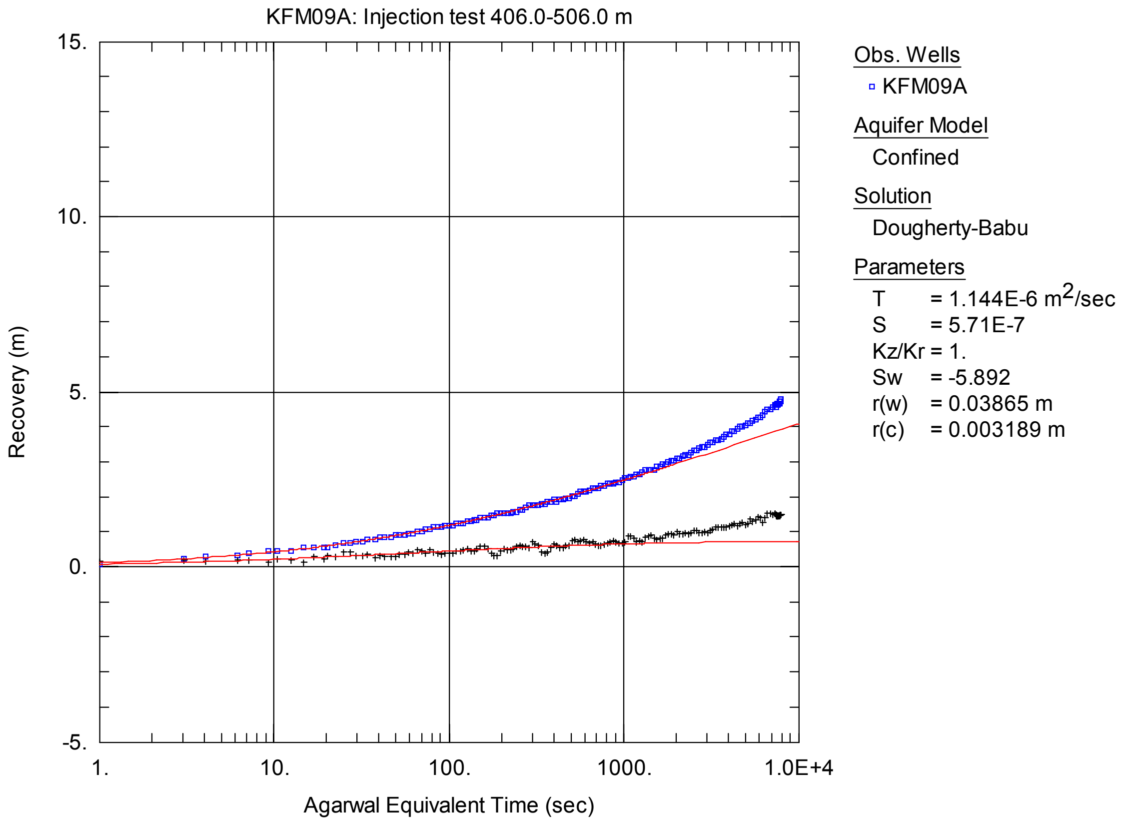


Figure A3-21. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 406.0-506.0 m in KFM09A.*

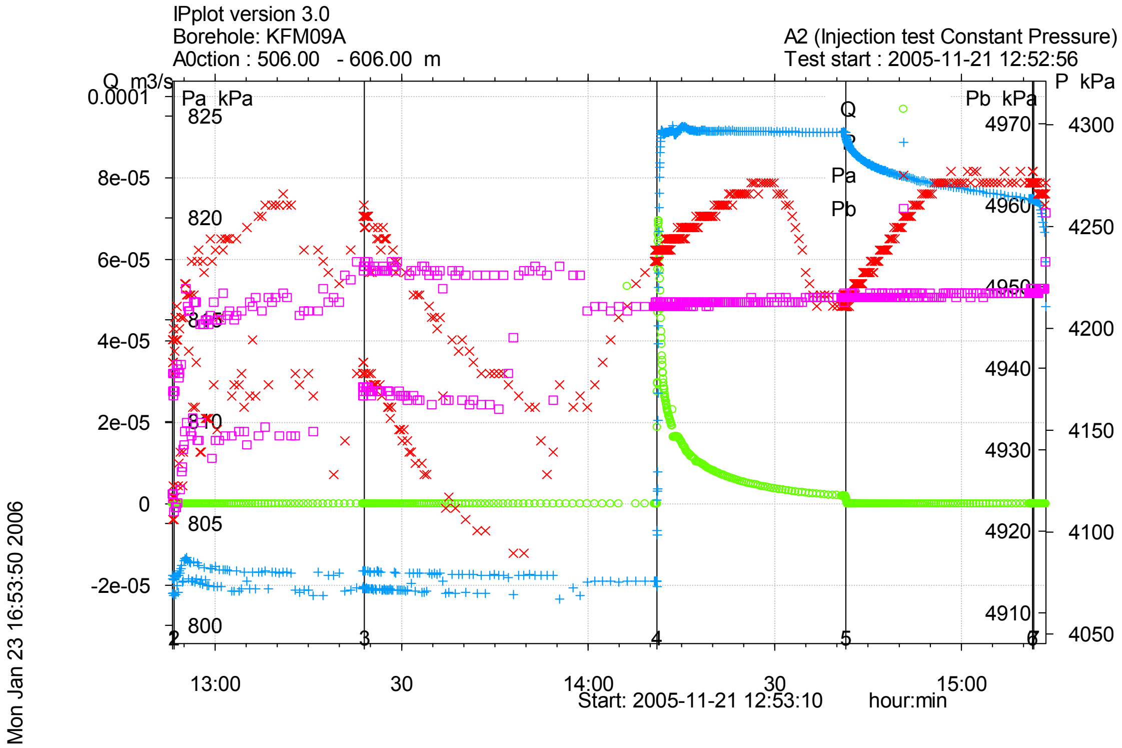


Figure A3-22. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 506.0-606.0 m in borehole KFM09A.*

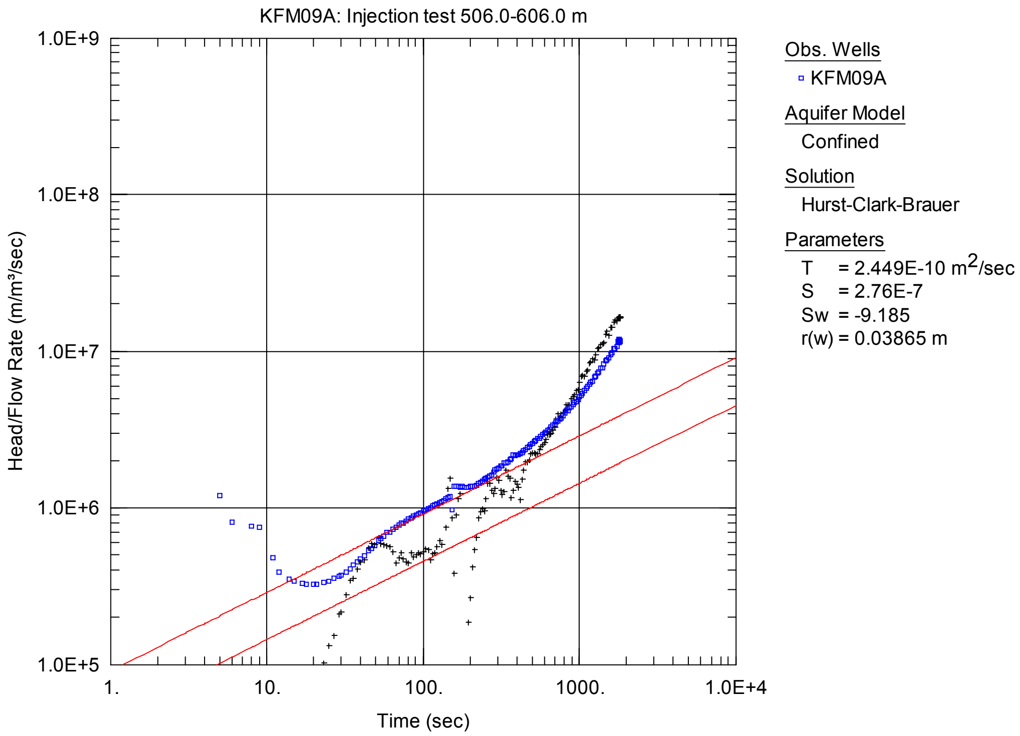


Figure A3-23. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 506.0-606.0 m in KFM09A. No unambiguous transit evaluation of transmissivity on this period is possible.*

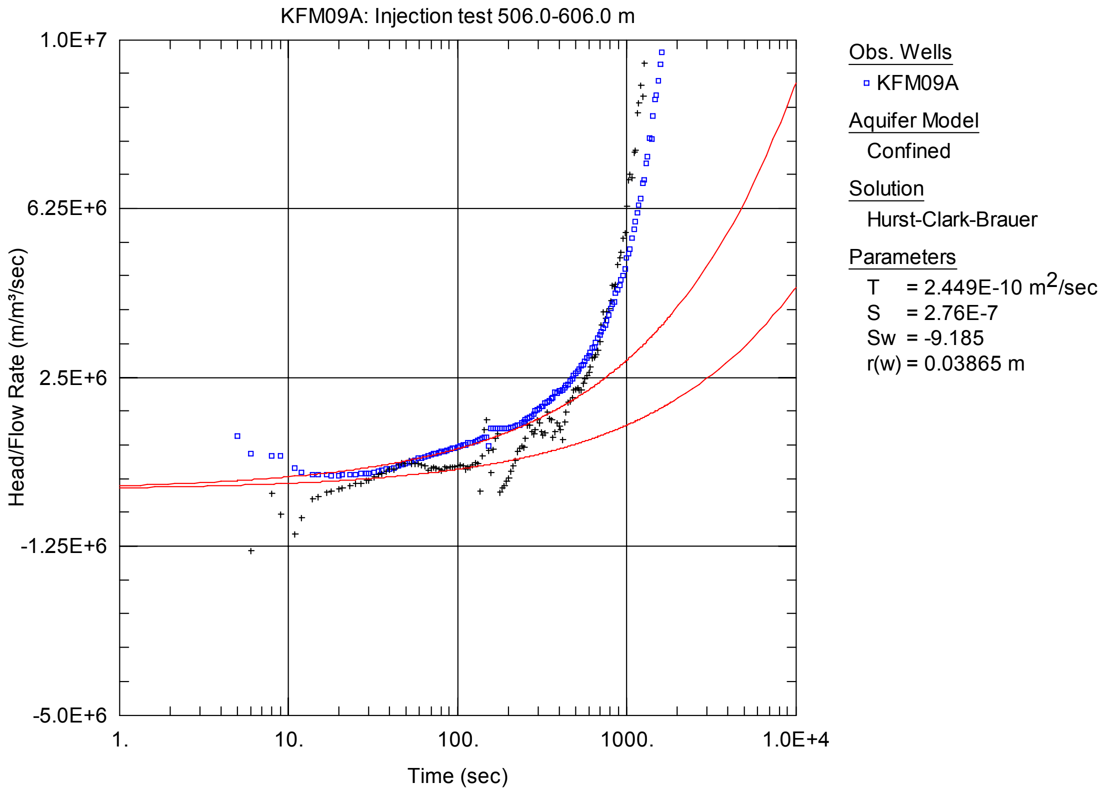


Figure A3-24. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 506.0-606.0 m in KFM09A. No unambiguous transit evaluation of transmissivity on this period is possible.*

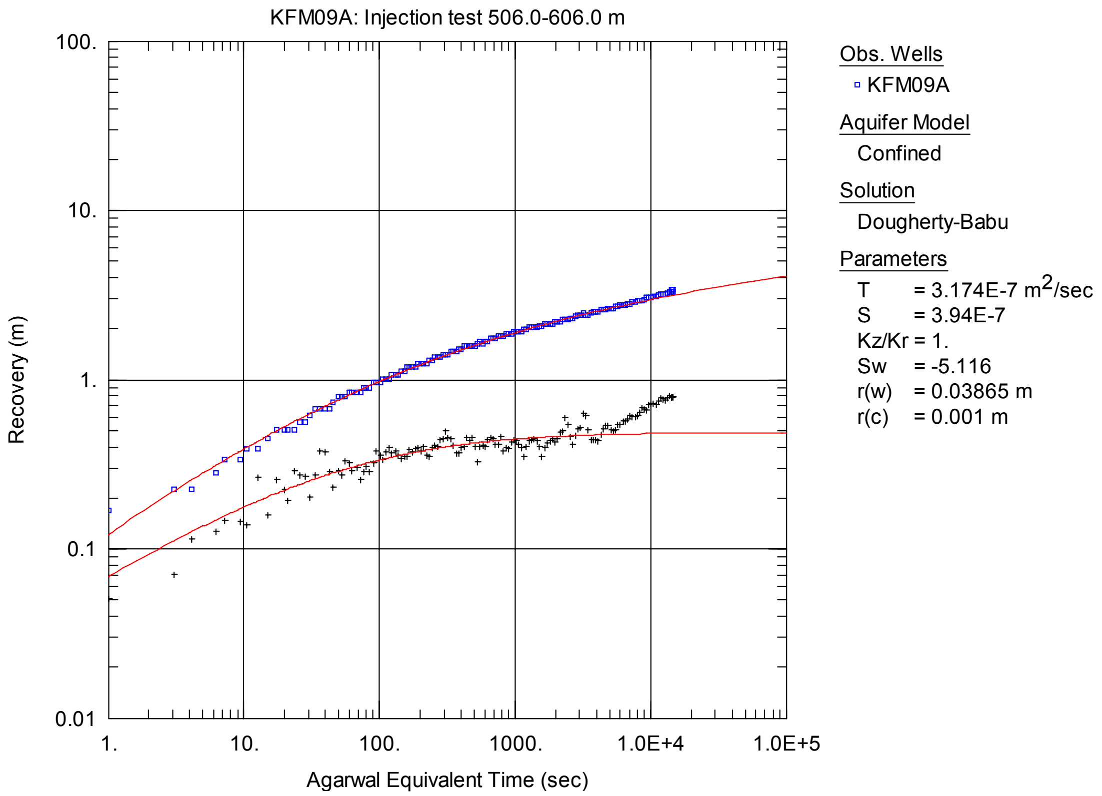


Figure A3-25. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 506.0-606.0 m in KFM09A.*

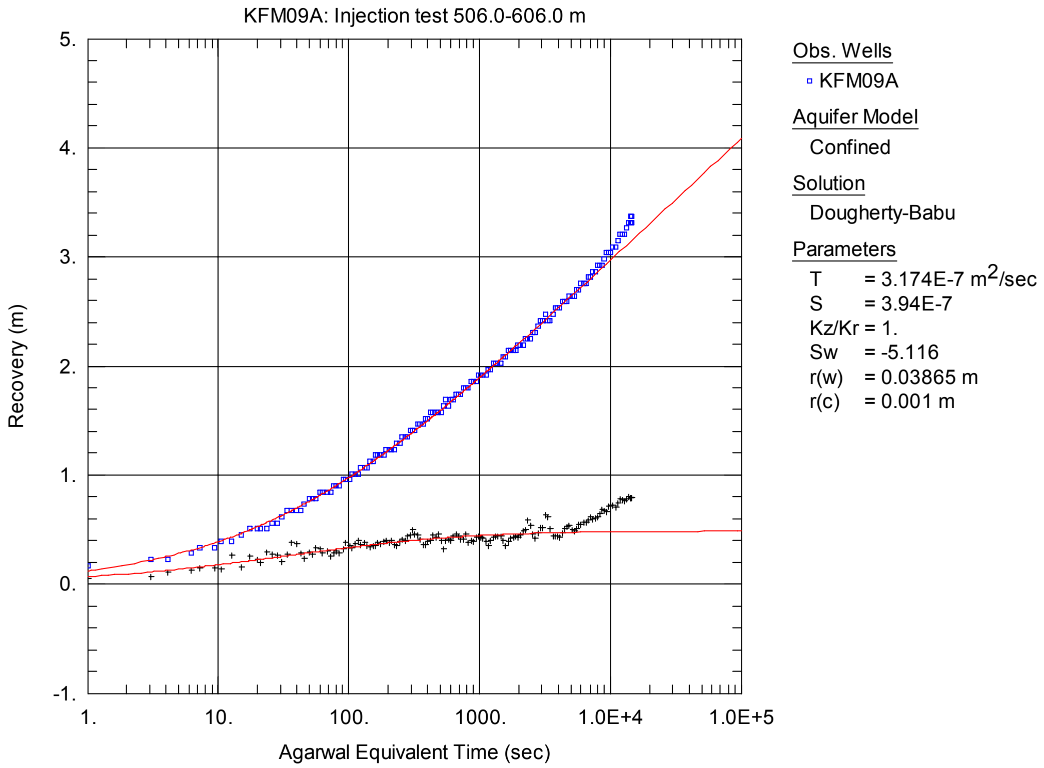


Figure A3-26. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 506.0-606.0 m in KFM09A.*

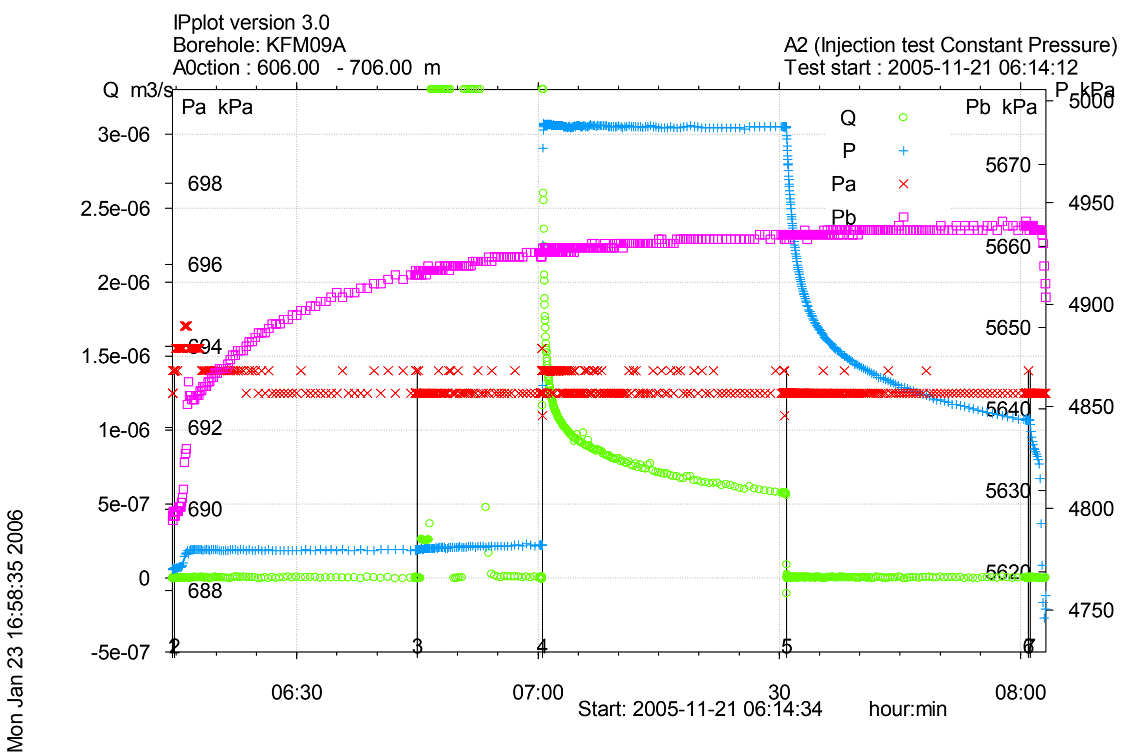


Figure A3-27. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 606.0-706.0 m in borehole KFM09A.*

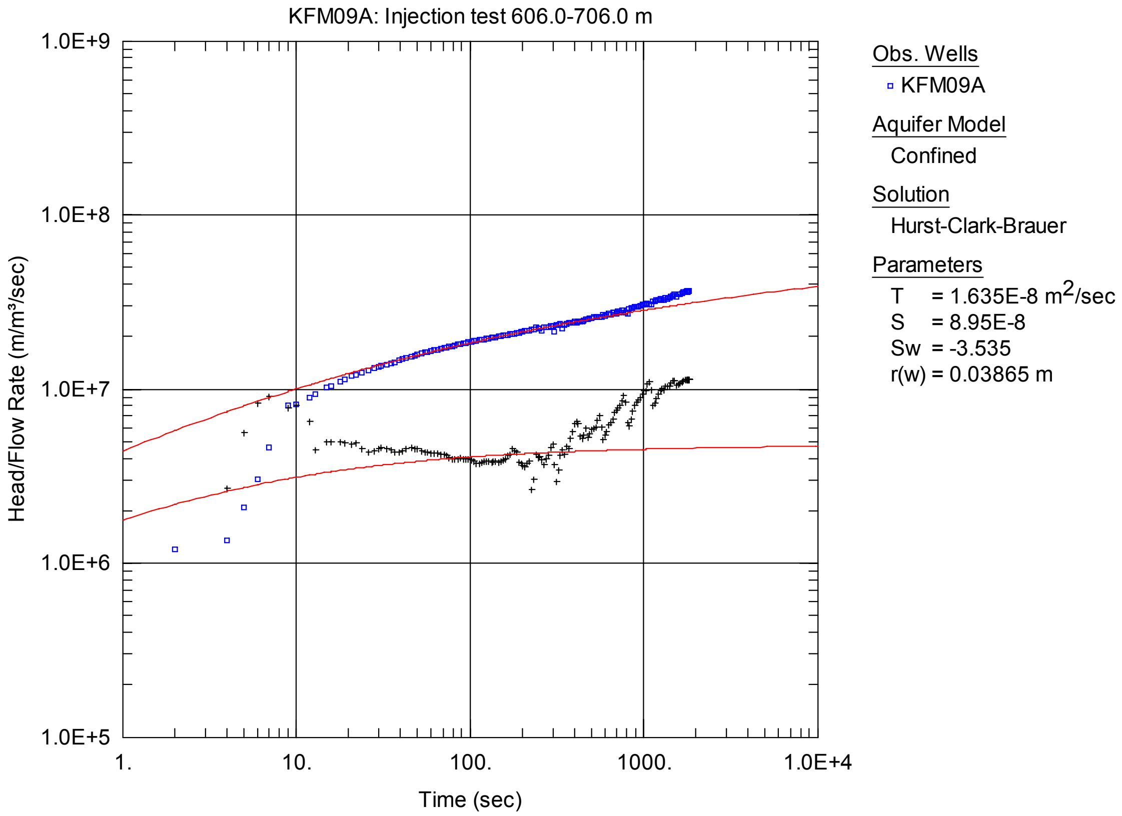


Figure A3-28. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 606.0-706.0 m in KFM09A.*

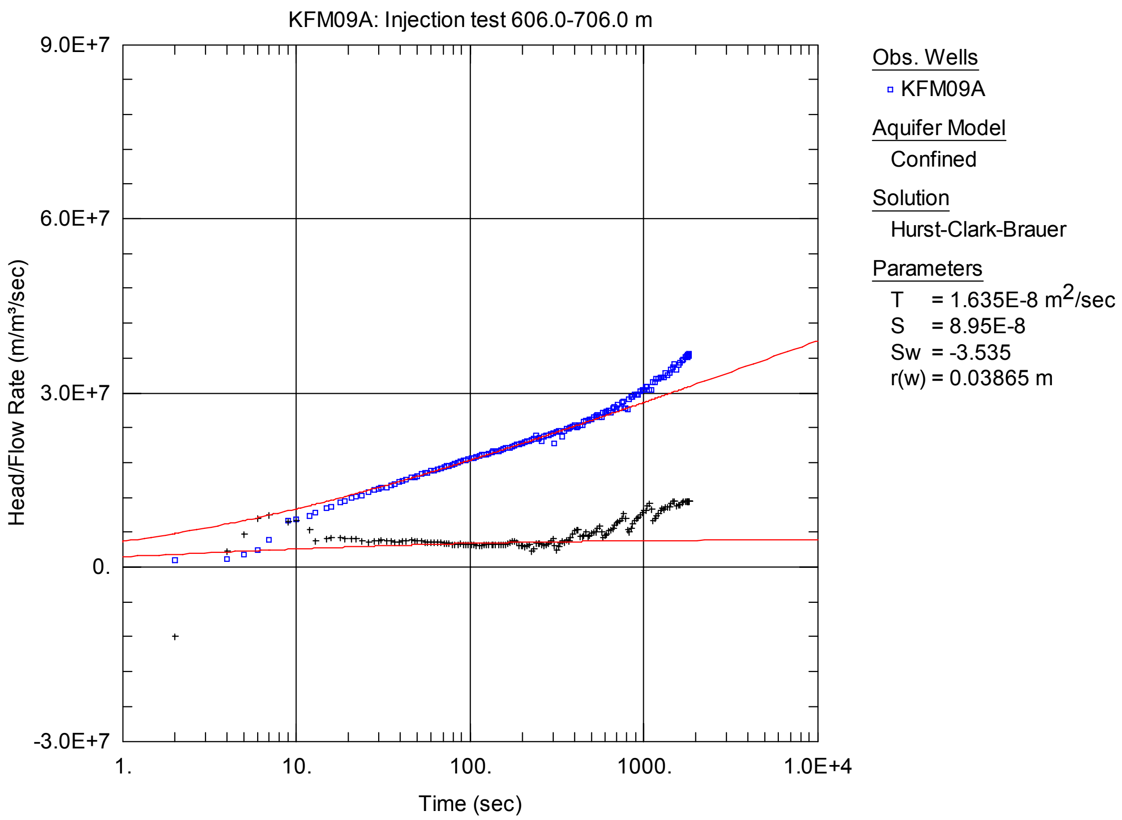


Figure A3-29. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 606.0-706.0 m in KFM09A.*

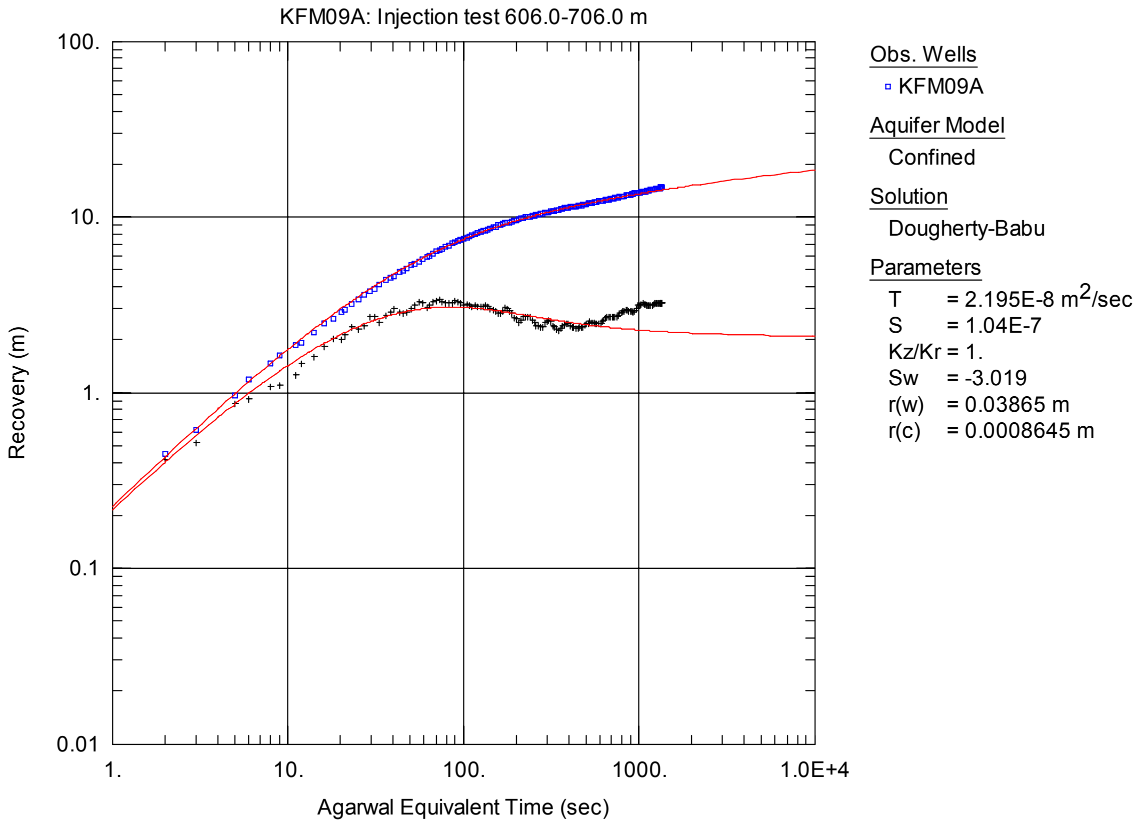


Figure A3-30. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 606.0-706.0 m in KFM09A.*

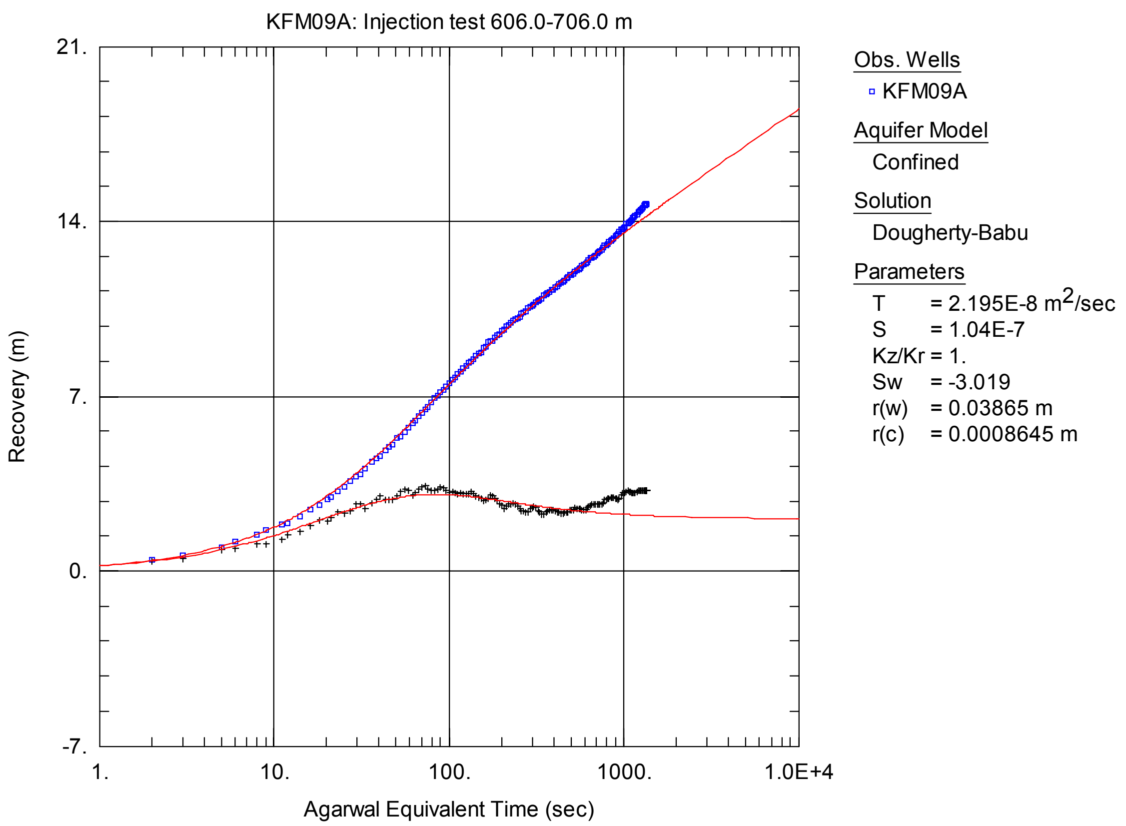


Figure A3-31. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 606.0-706.0 m in KFM09A.*

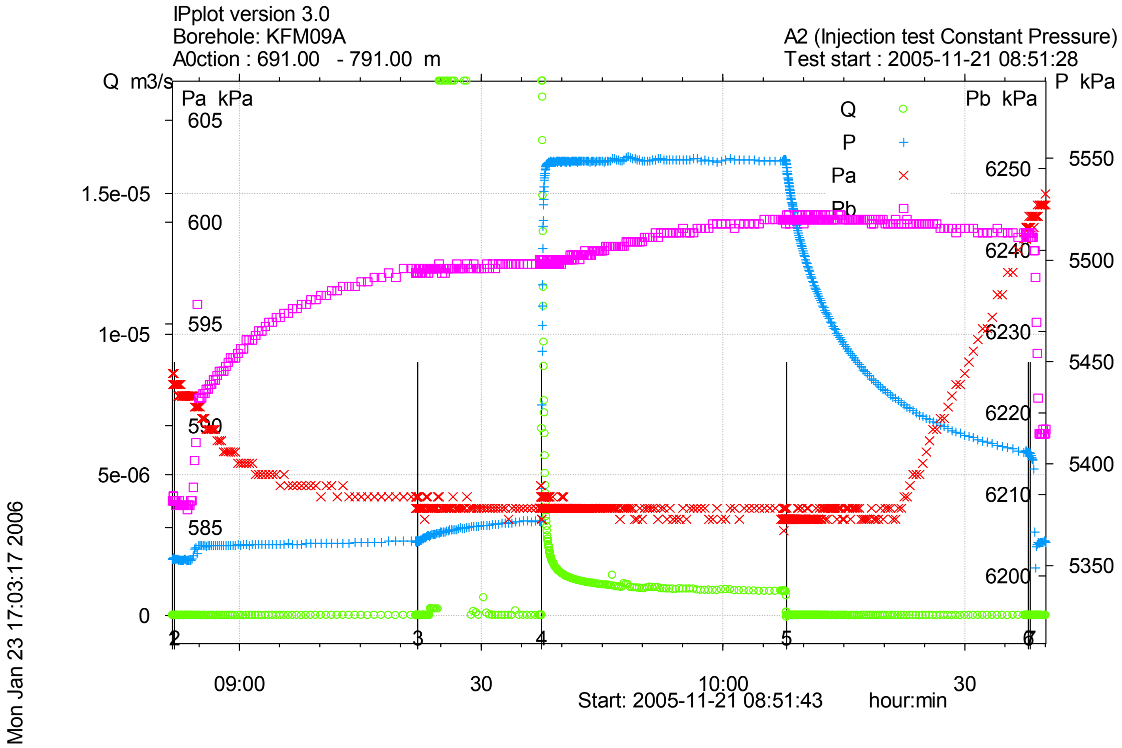


Figure A3-32. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 691.0-791.0 m in borehole KFM09A.*

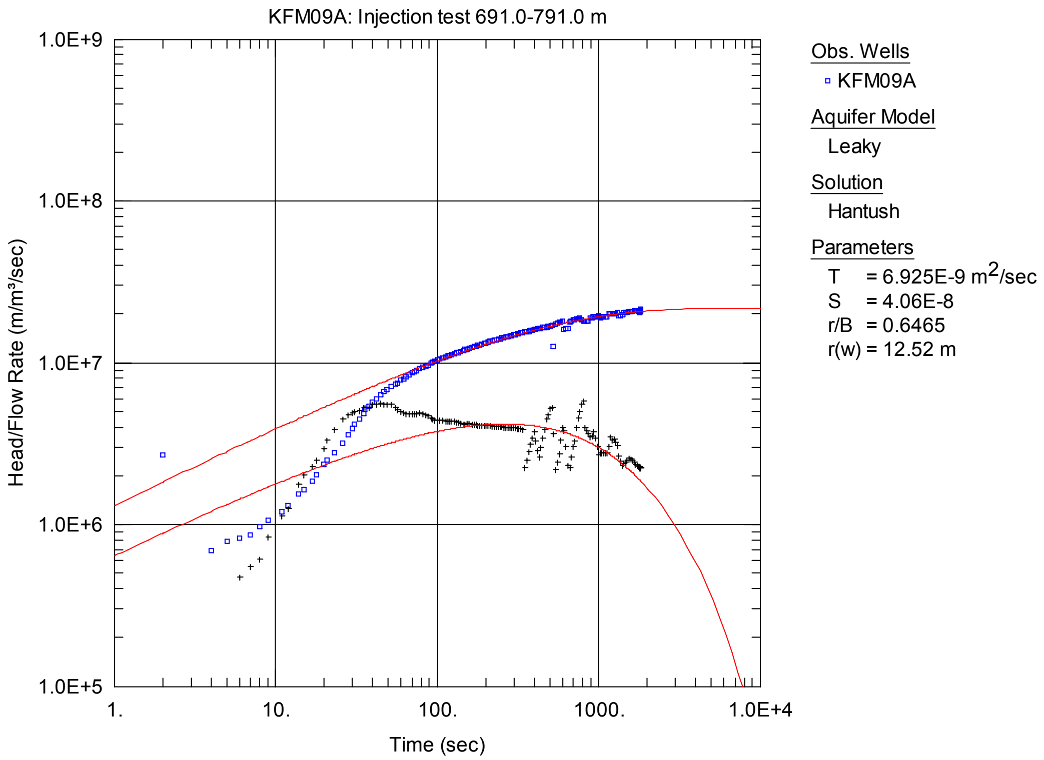


Figure A3-33. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 691.0-791.0 m in KFM09A.*

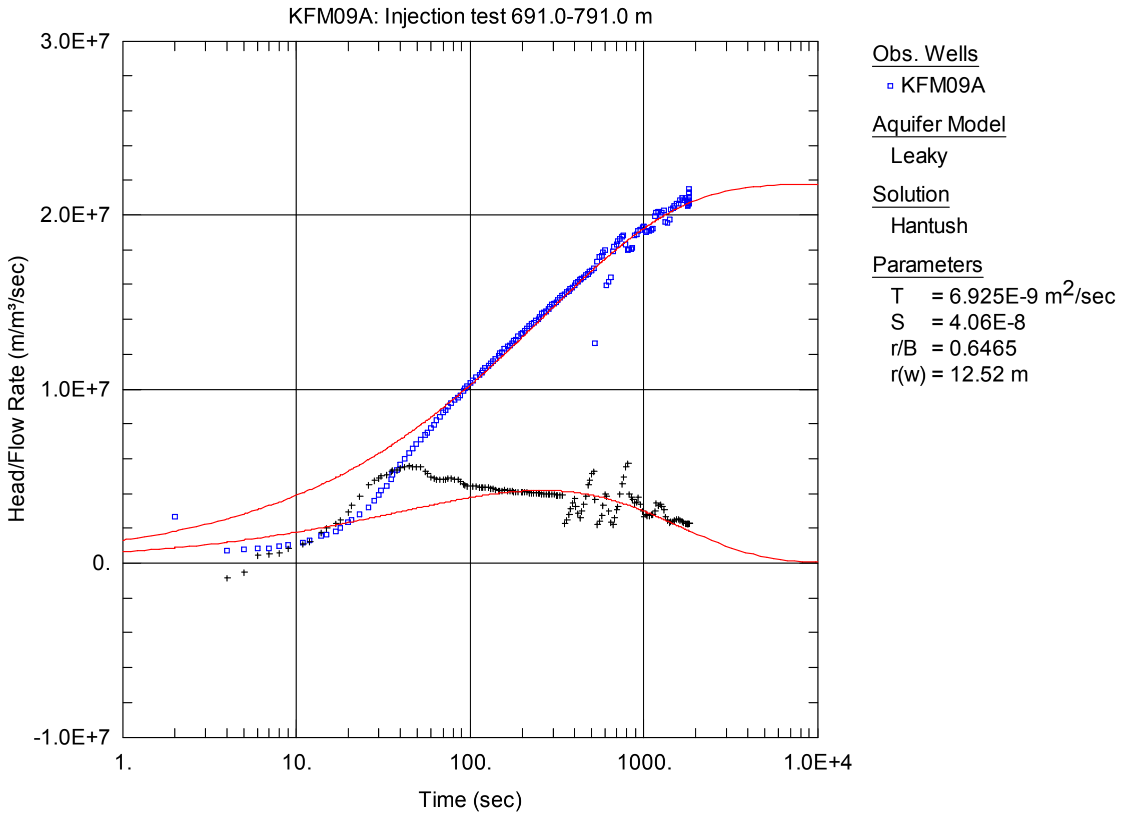


Figure A3-34. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 691.0-791.0 m in KFM09A.*

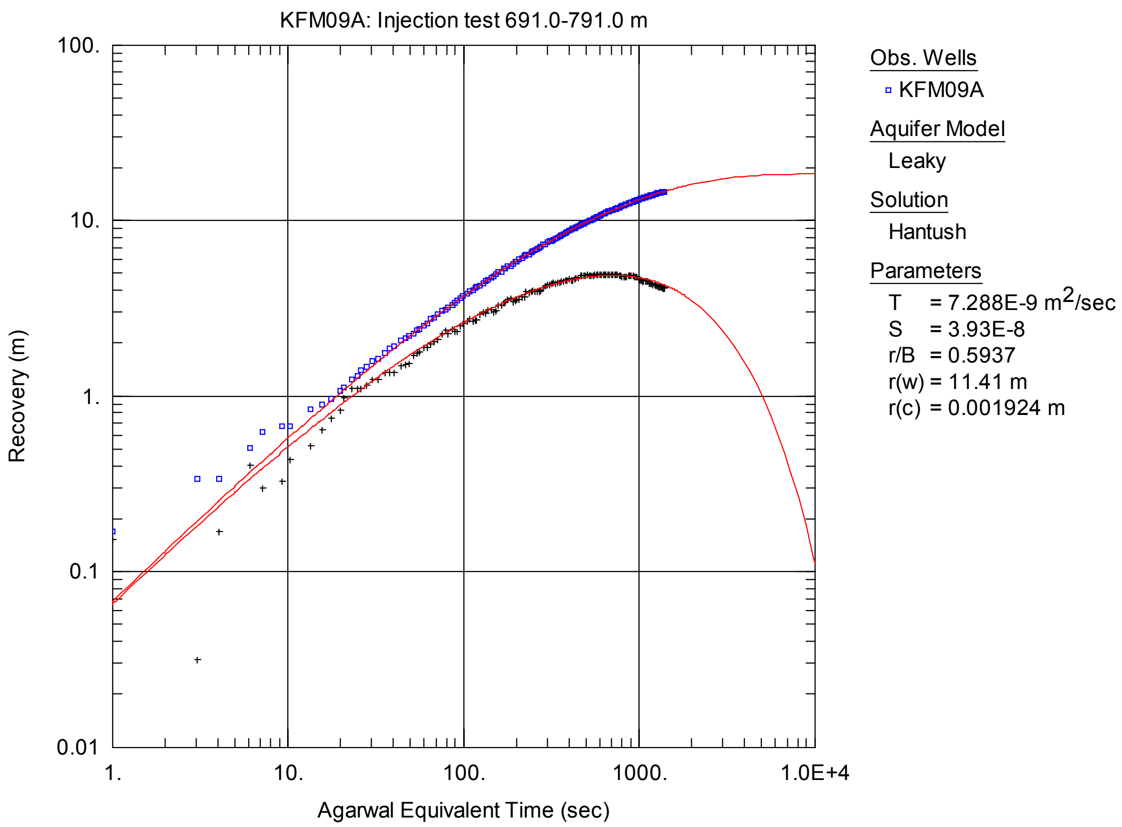


Figure A3-35. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 691.0-791.0 m in KFM09A.*

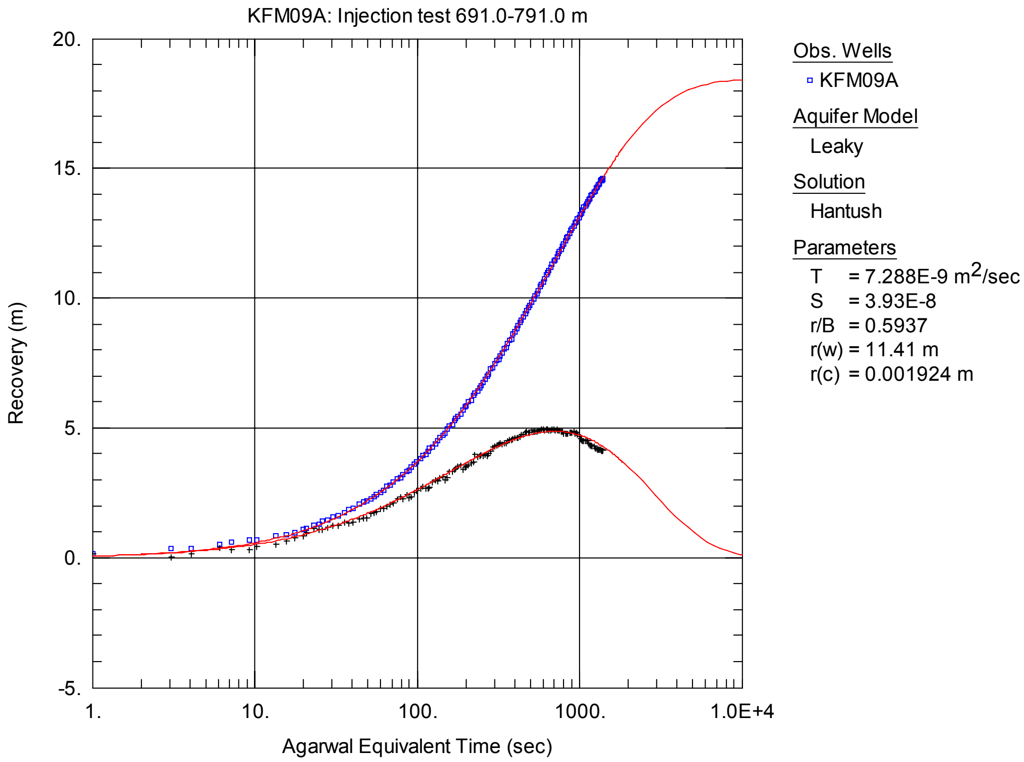


Figure A3-36. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 691.0-791.0 m in KFM09A.*

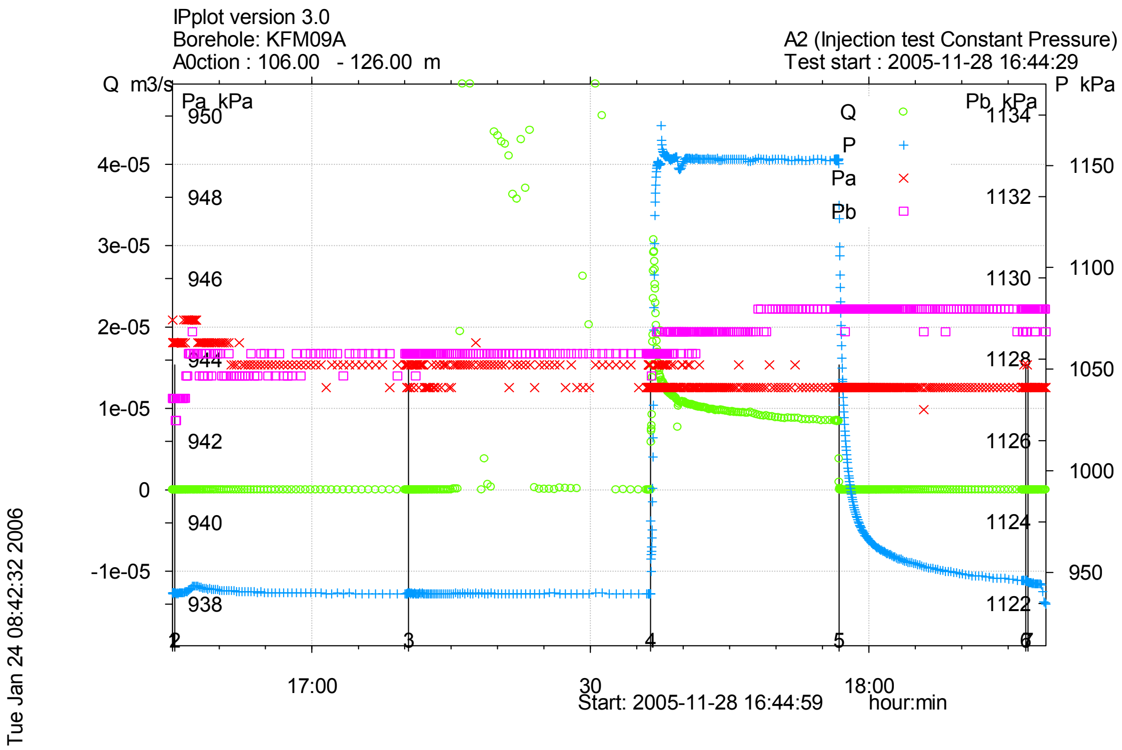


Figure A3-37. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 106.0-126.0 m in borehole KFM09A.*

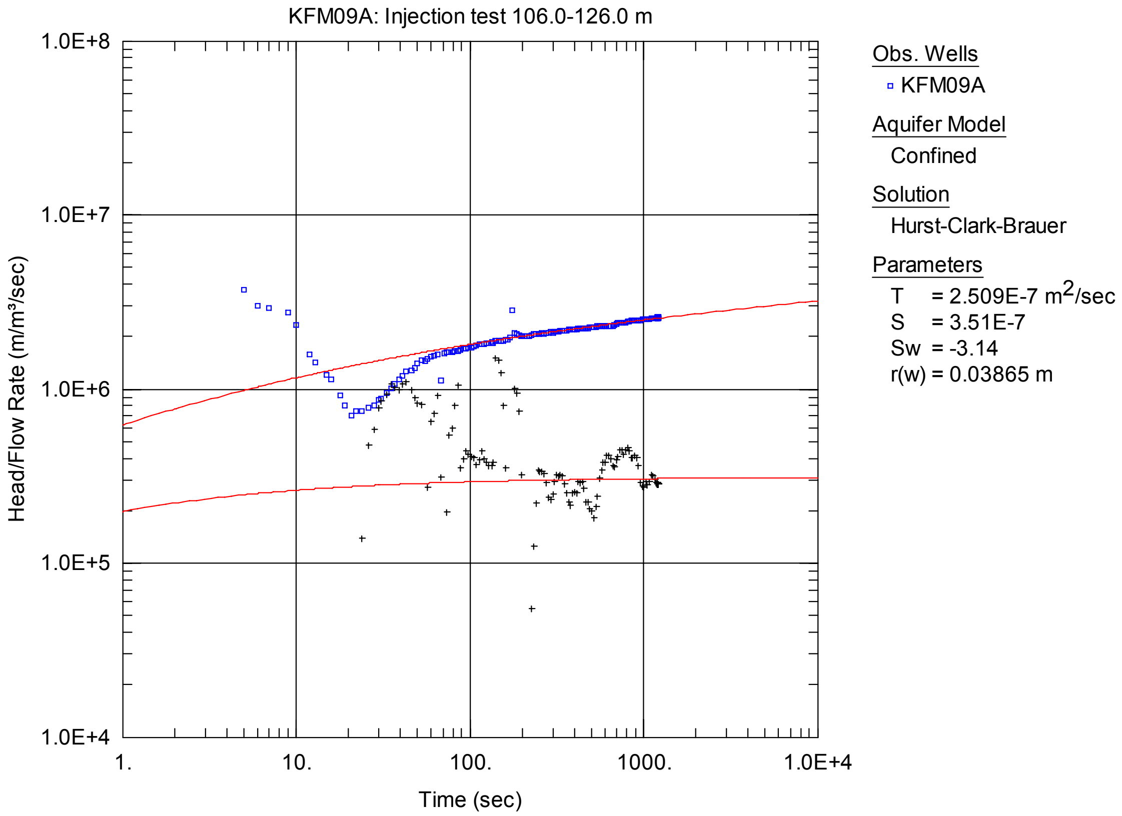


Figure A3-38. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 106.0-126.0 m in KFM09A.*

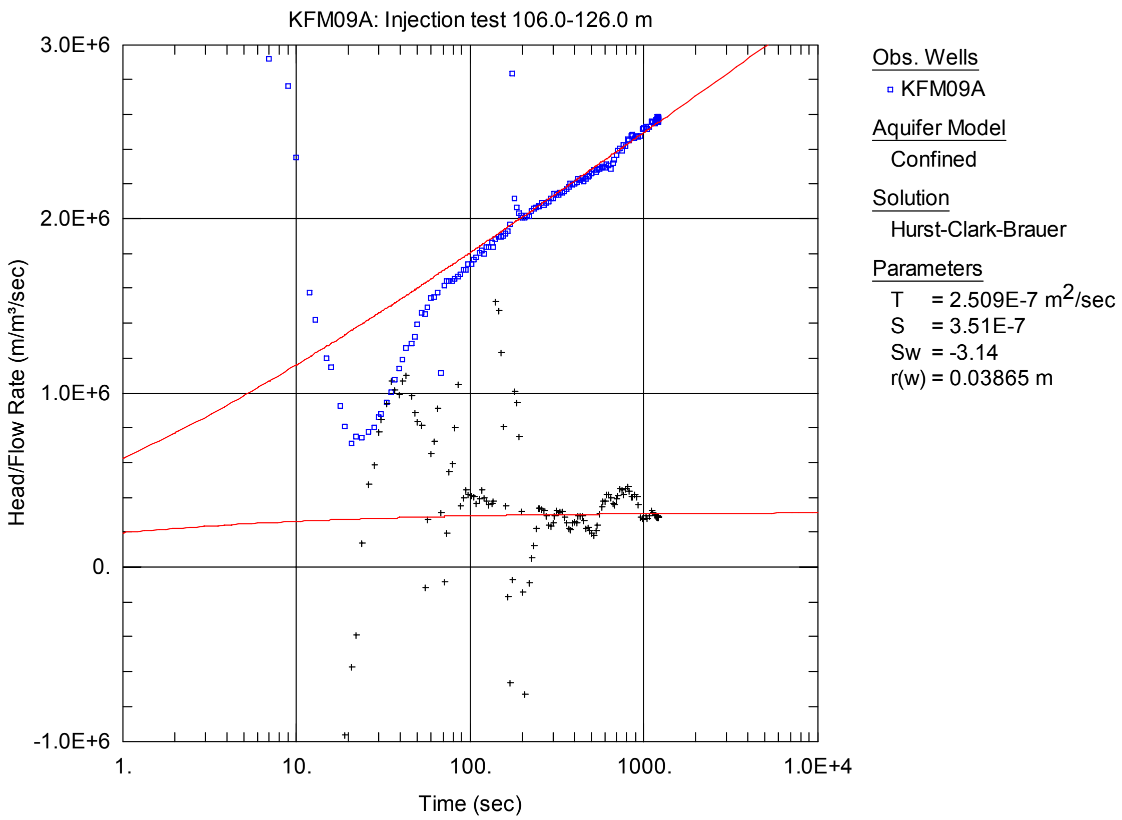


Figure A3-39. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 106.0-126.0 m in KFM09A.*

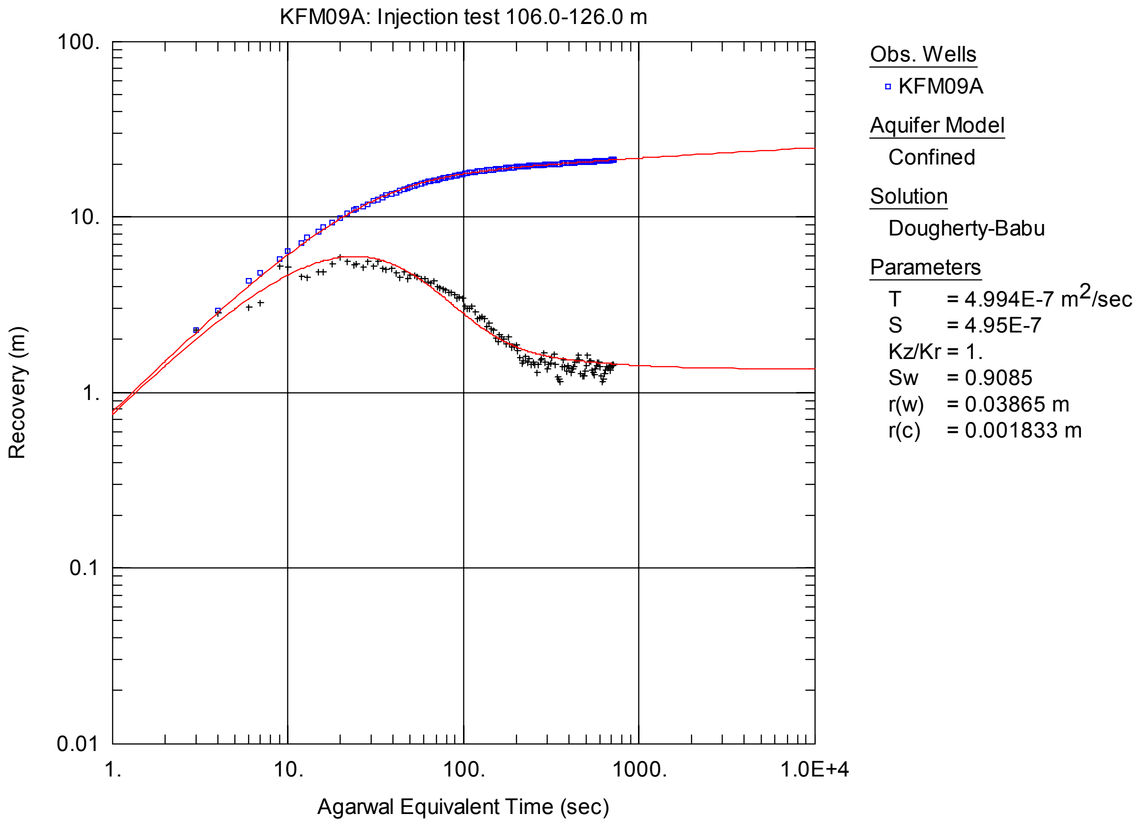


Figure A3-40. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 106.0-126.0 m in KFM09A.*

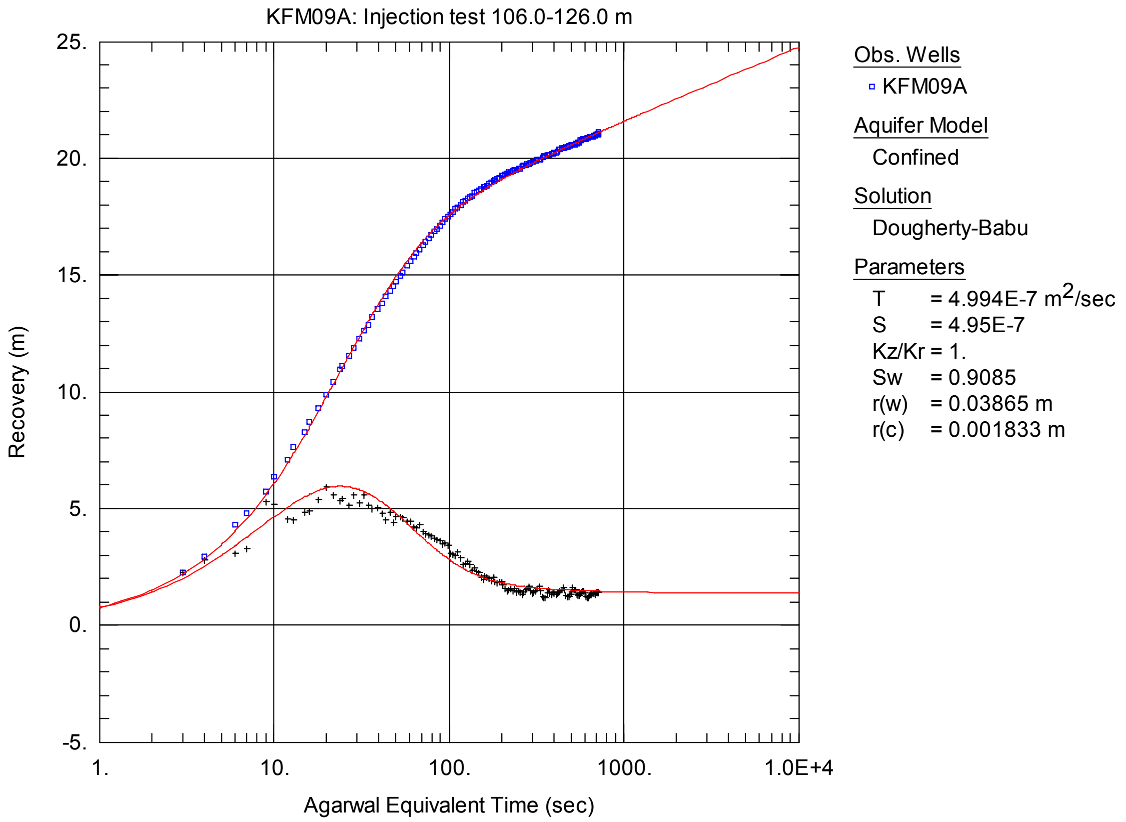


Figure A3-41. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 106.0-126.0 m in KFM09A.*

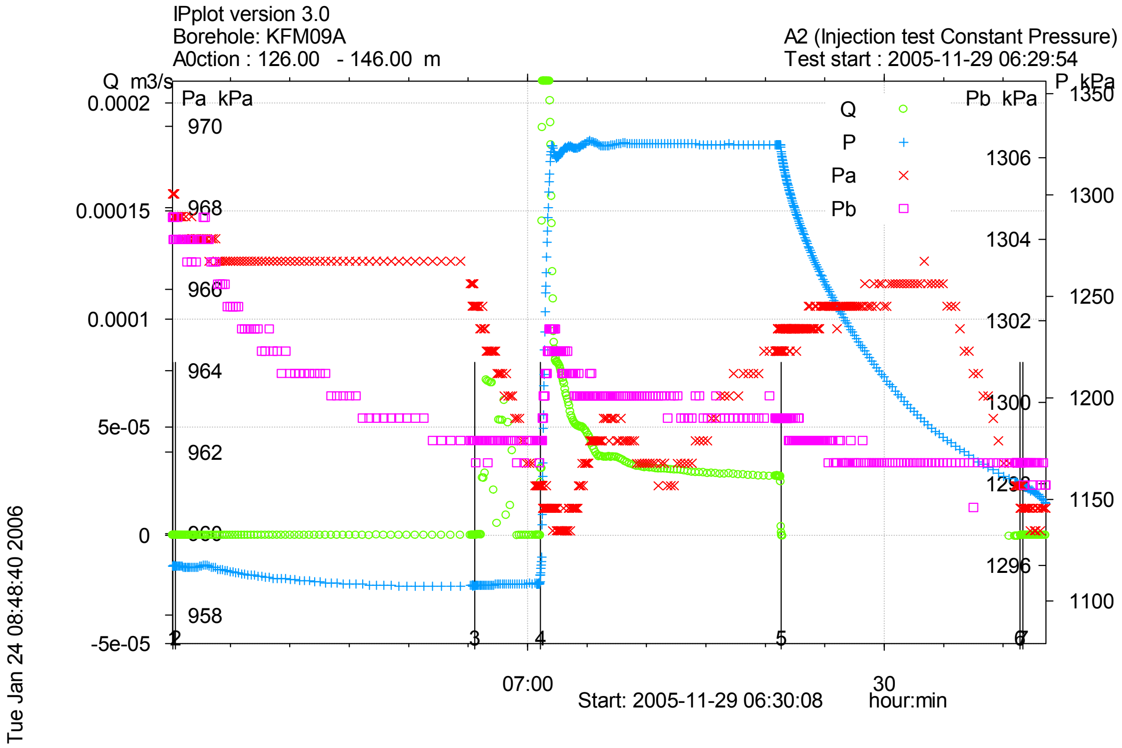


Figure A3-42. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 126.0-146.0 m in borehole KFM09A.*

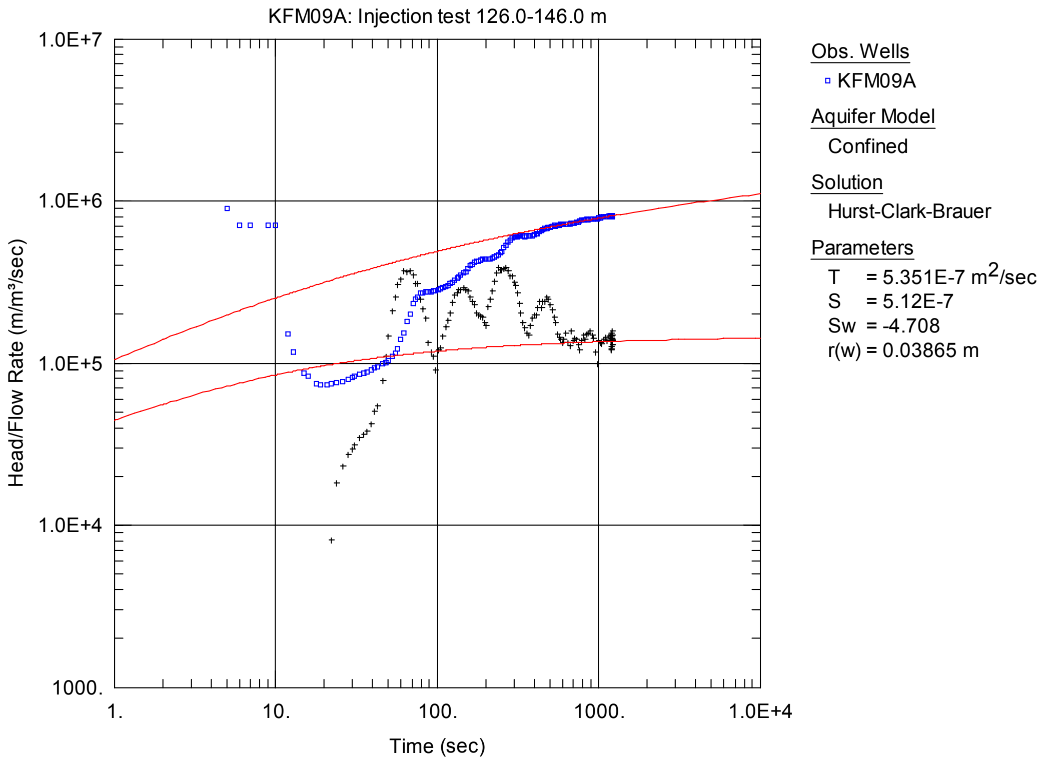


Figure A3-43. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 126.0-146.0 m in KFM09A.*

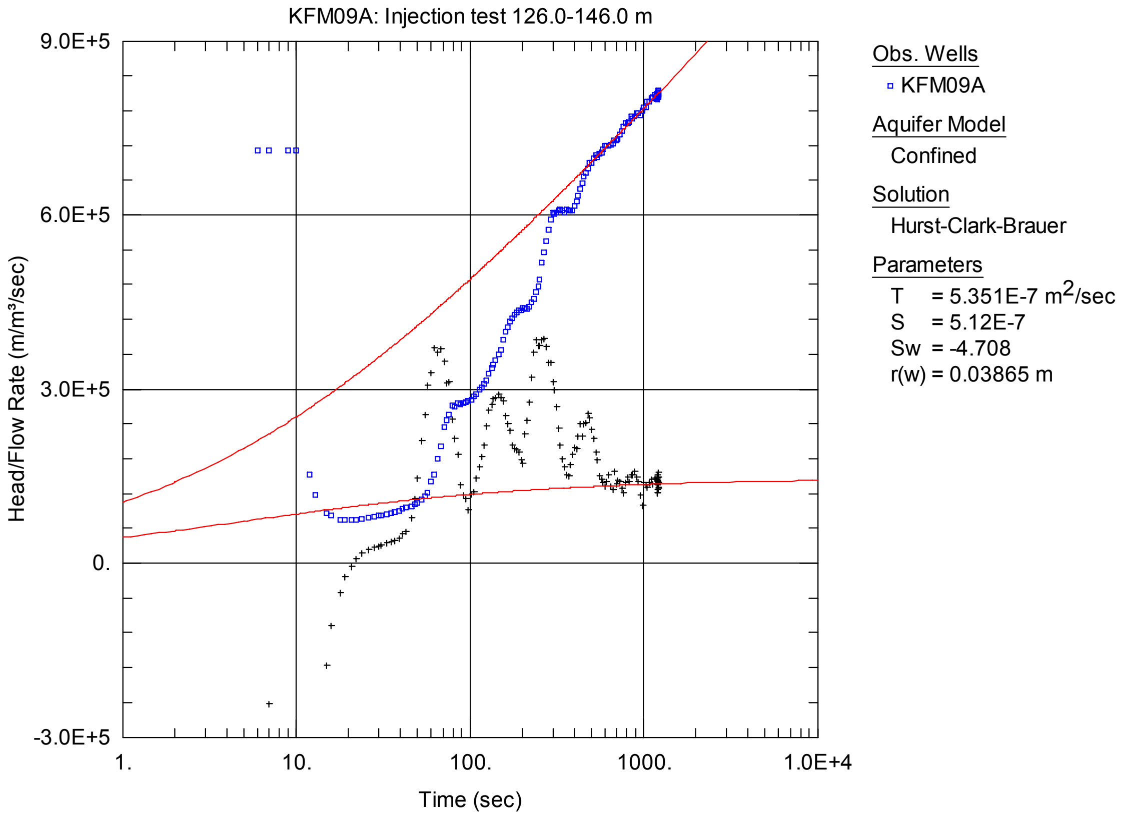


Figure A3-44. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 126.0-146.0 m in KFM09A.*

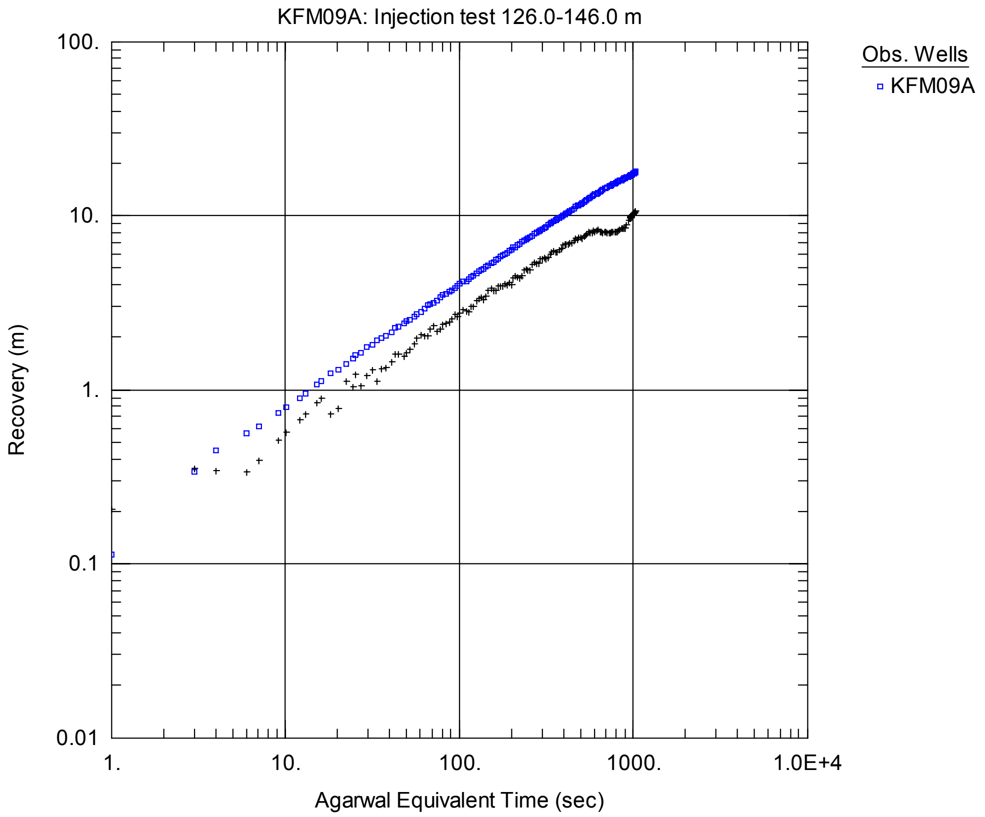


Figure A3-45. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 126.0-146.0 m in KFM09A.*

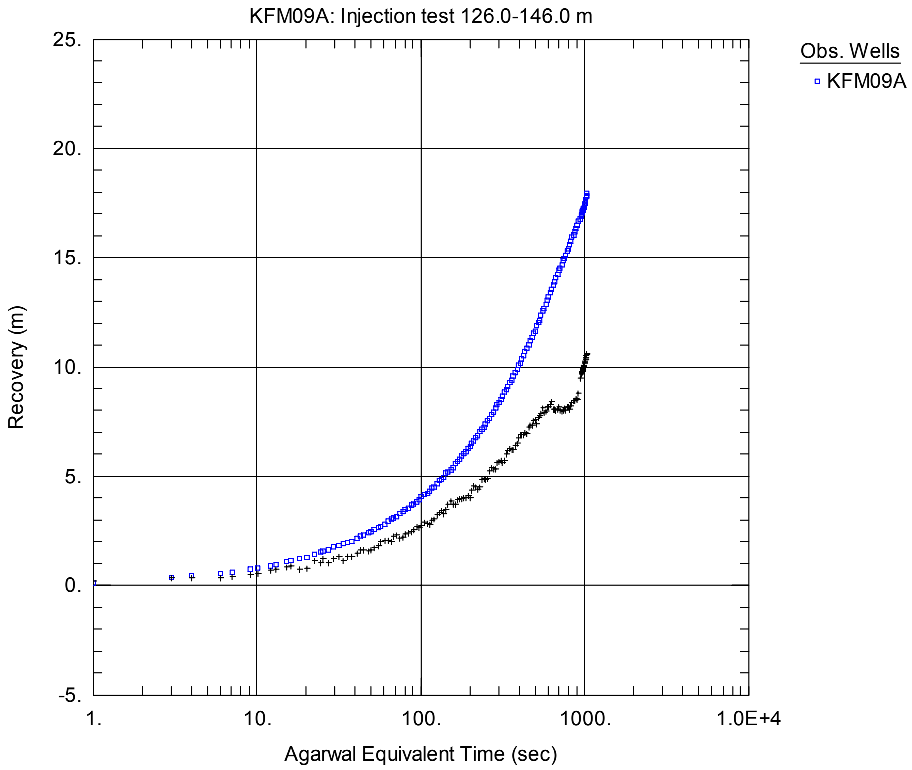


Figure A3-46. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 126.0-146.0 m in KFM09A.*

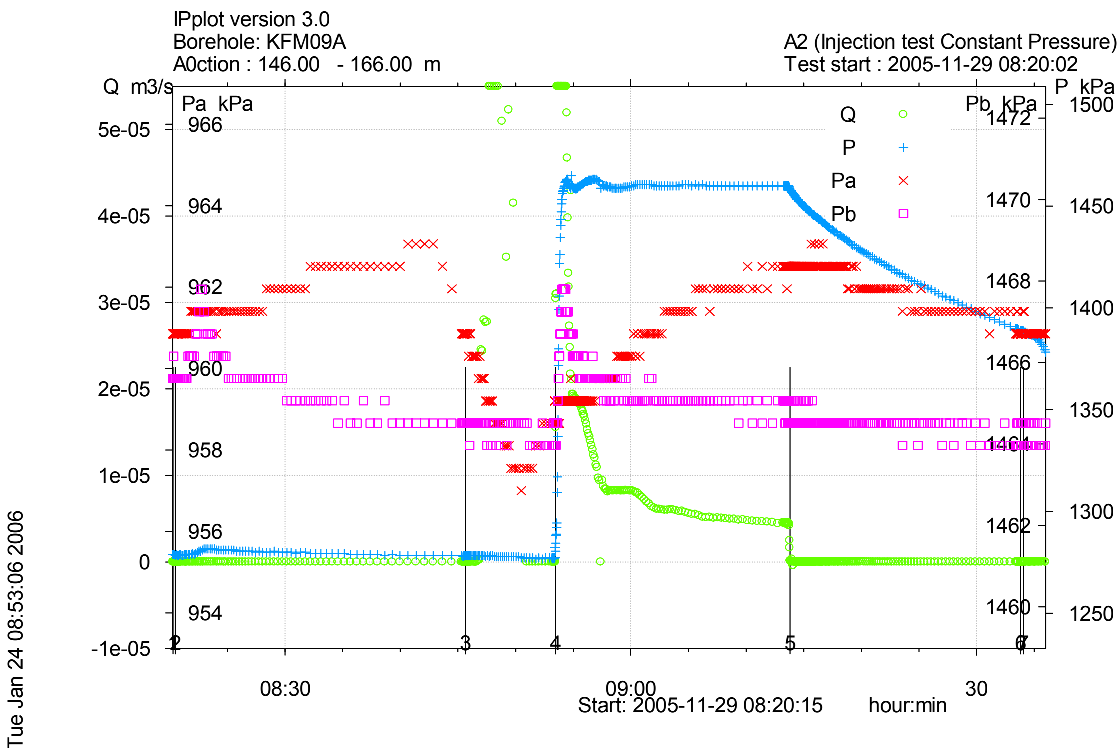


Figure A3-47. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 146.0-166.0 m in borehole KFM09A.*

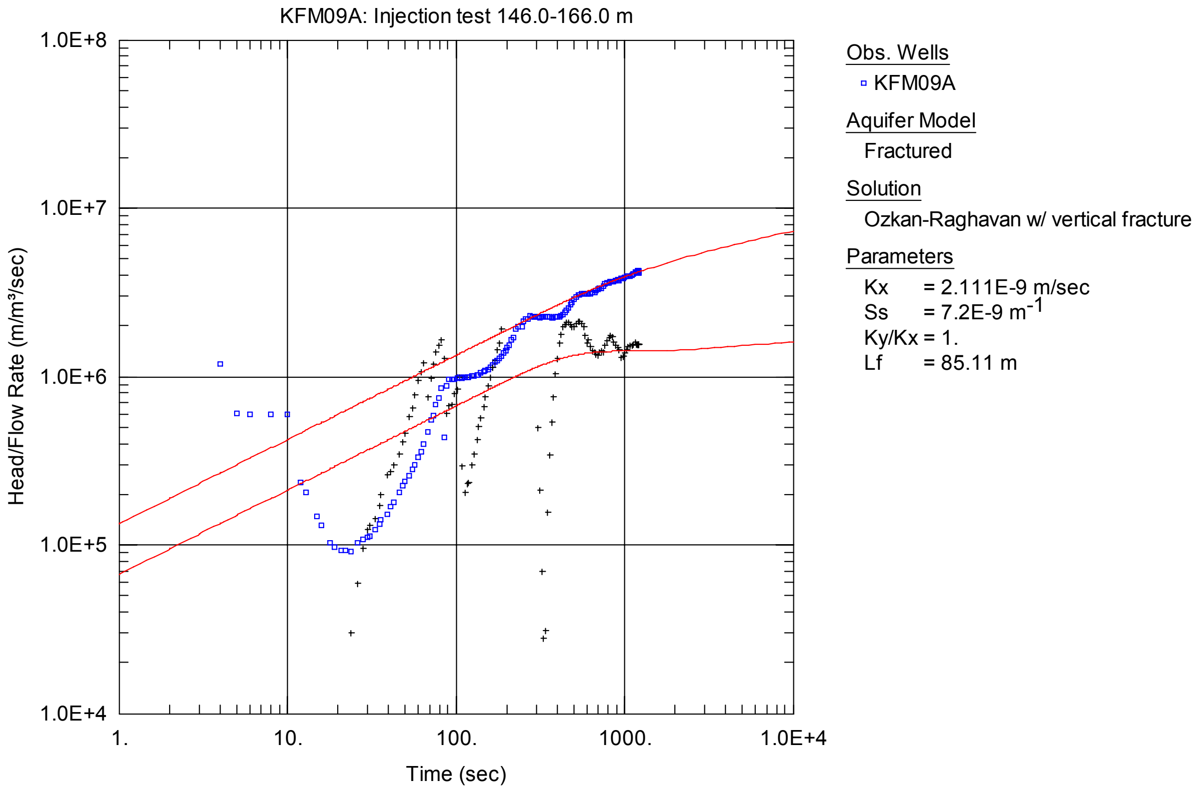


Figure A3-48. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 146.0-166.0 m in KFM09A.*

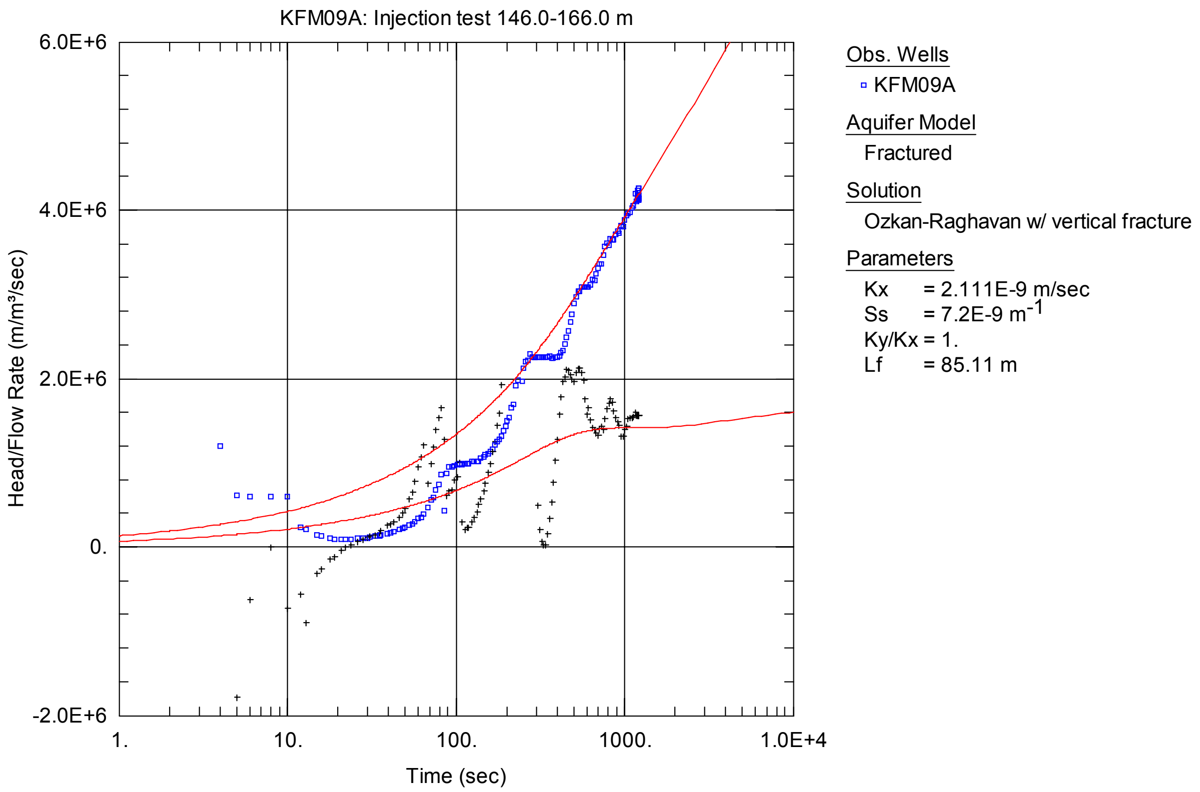


Figure A3-49. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 146.0-166.0 m in KFM09A.*

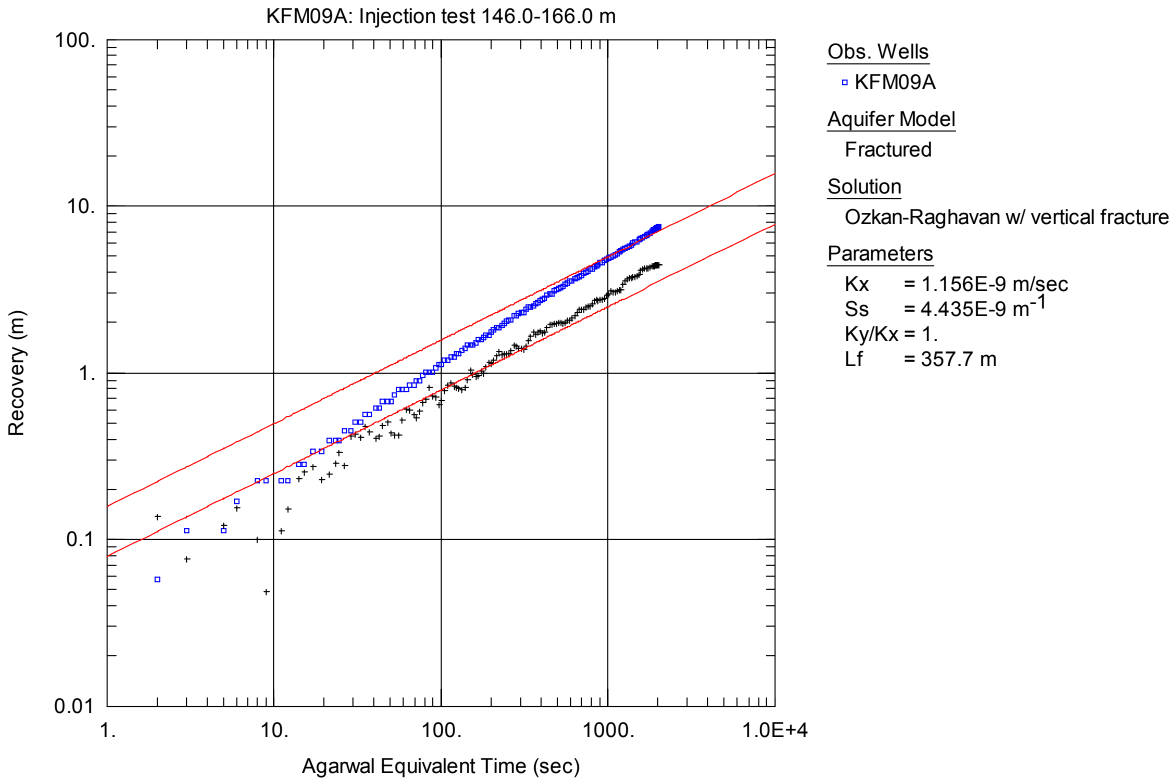


Figure A3-50. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 146.0-166.0 m in KFM09A. No unambiguous transient evaluation of transmissivity on this period is possible.*

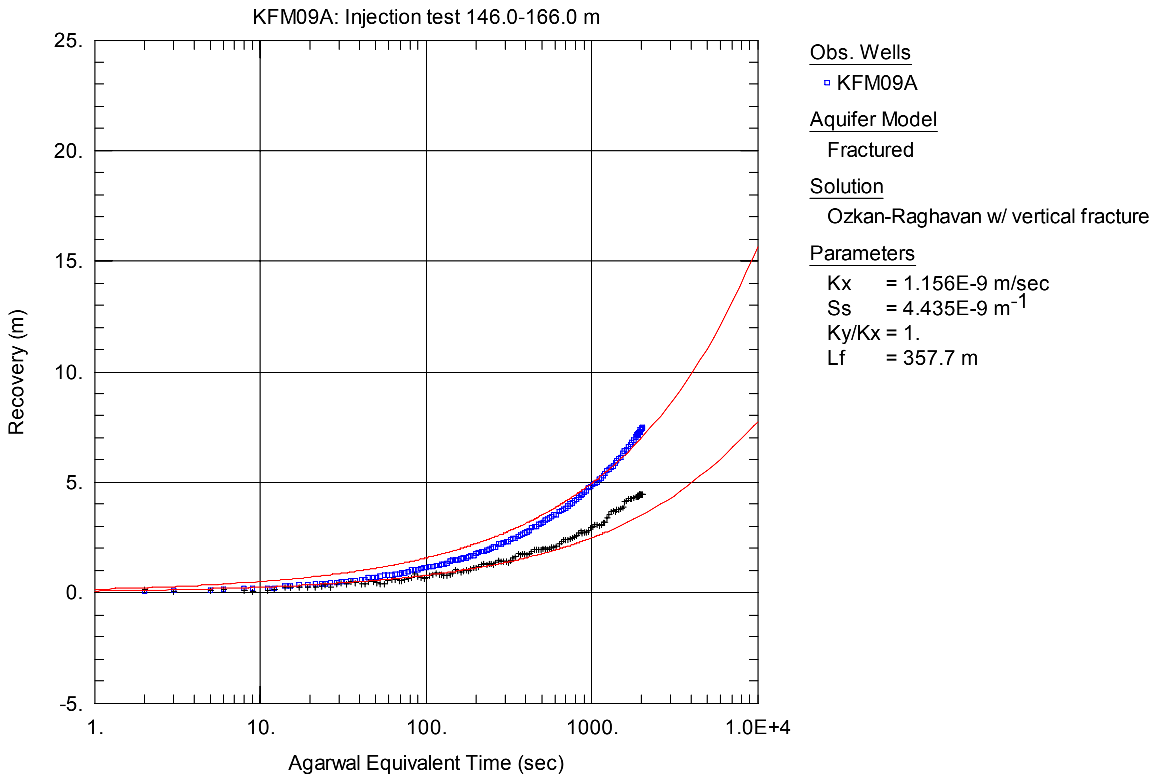


Figure A3-51. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 146.0-166.0 m in KFM09A. No unambiguous transient evaluation of transmissivity on this period is possible.*

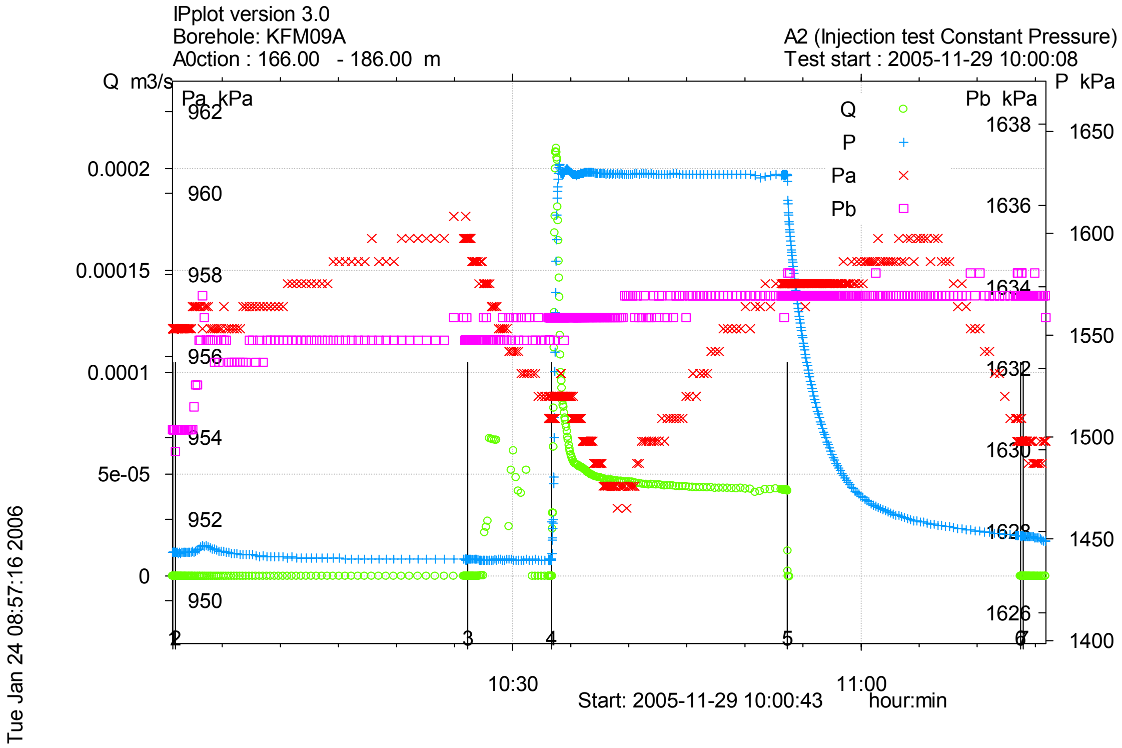


Figure A3-52. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 166.0-186.0 m in borehole KFM09A.*

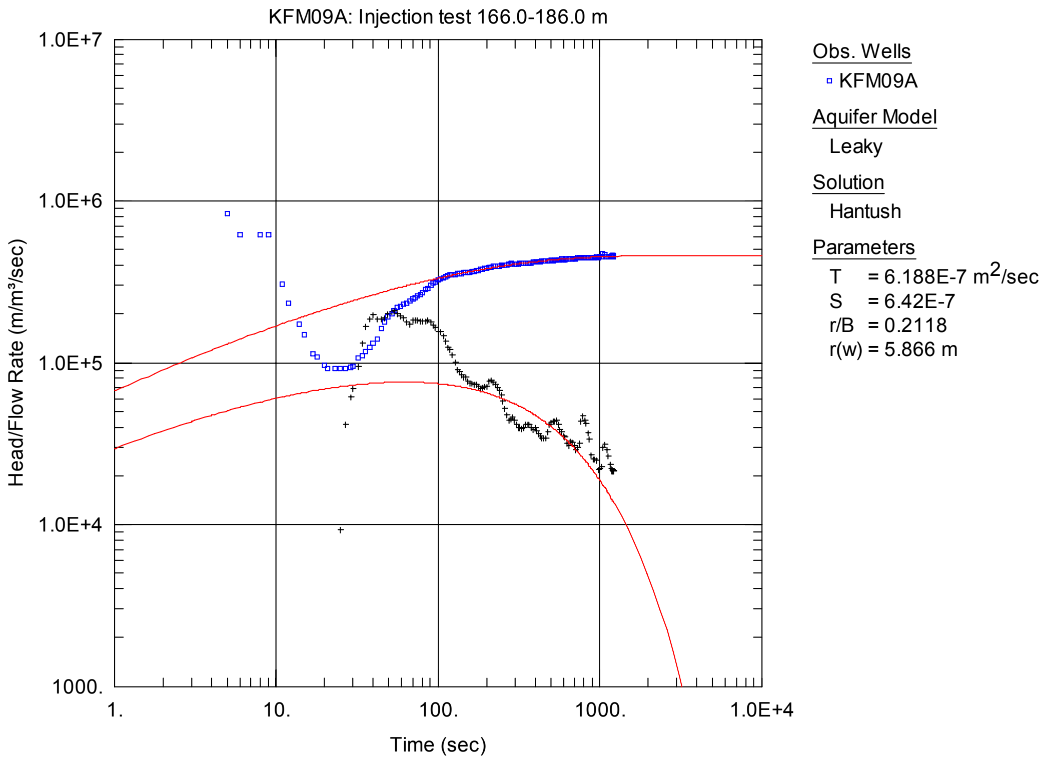


Figure A3-53. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 166.0-186.0 m in KFM09A.*

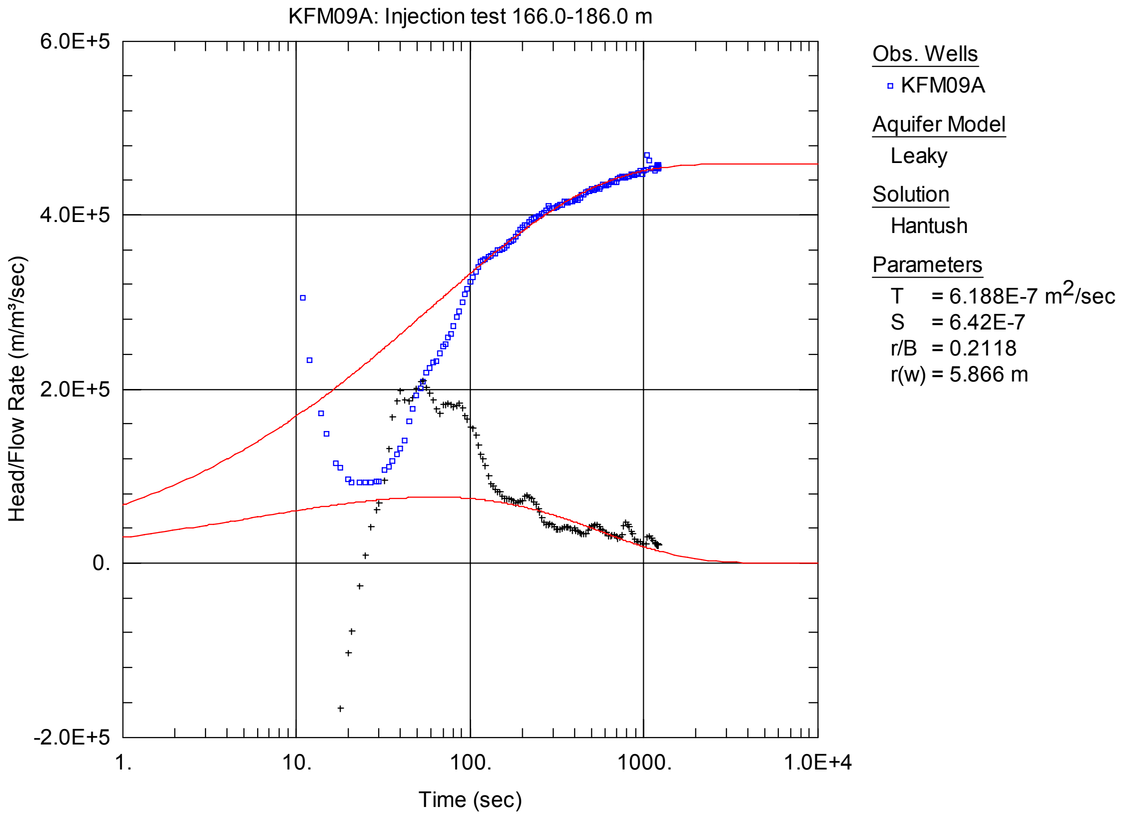


Figure A3-54. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 166.0-186.0 m in KFM09A.*

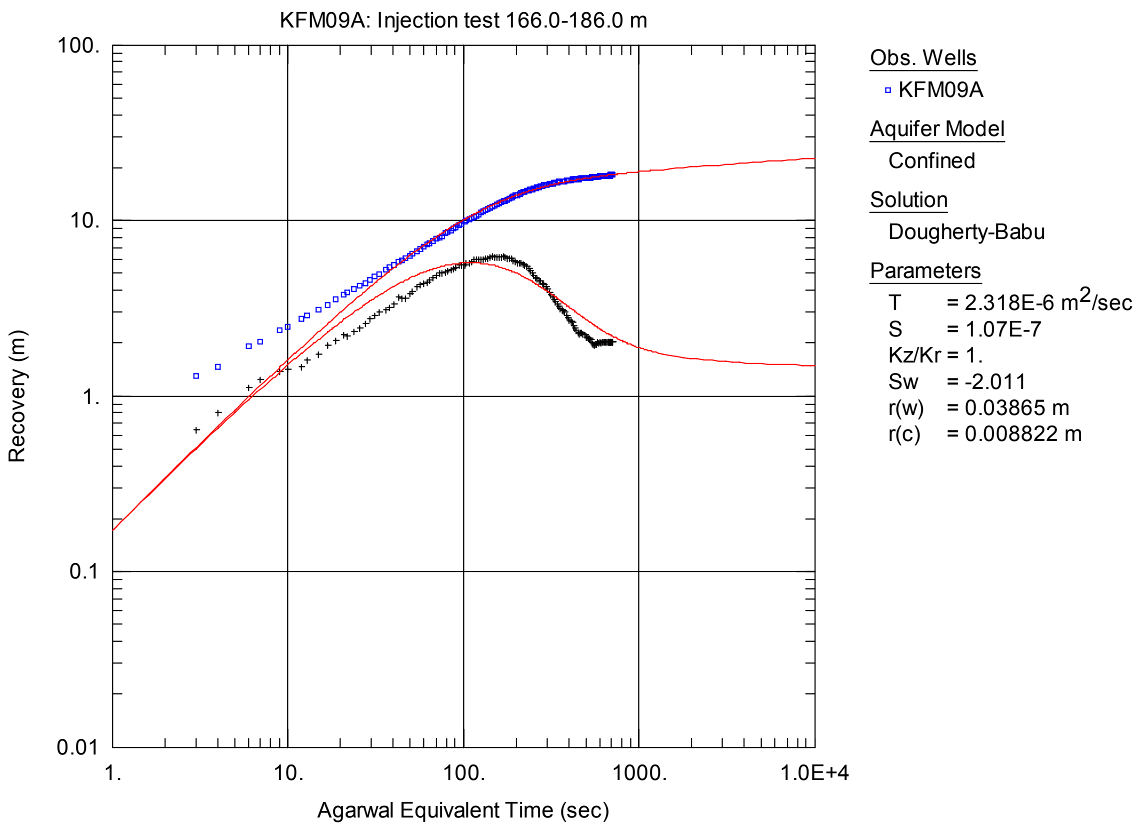


Figure A3-55. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 166.0-186.0 m in KFM09A.*

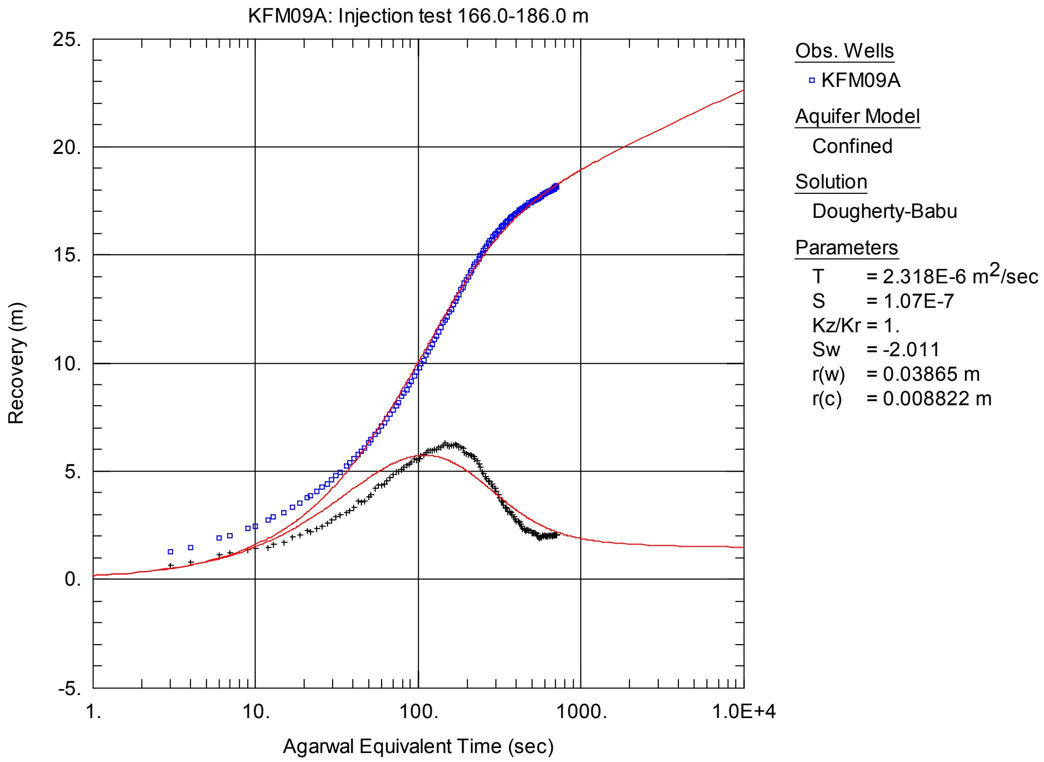


Figure A3-56. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 166.0-186.0 m in KFM09A.*

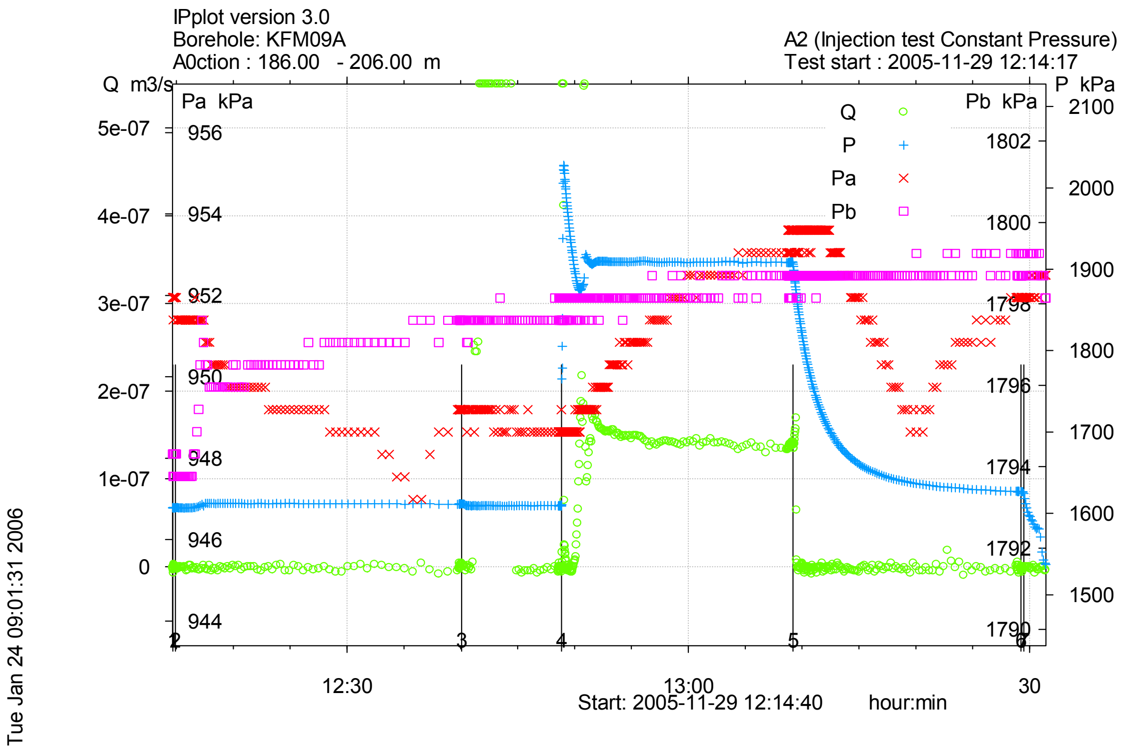


Figure A3-57. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 186.0-206.0 m in borehole KFM09A.*

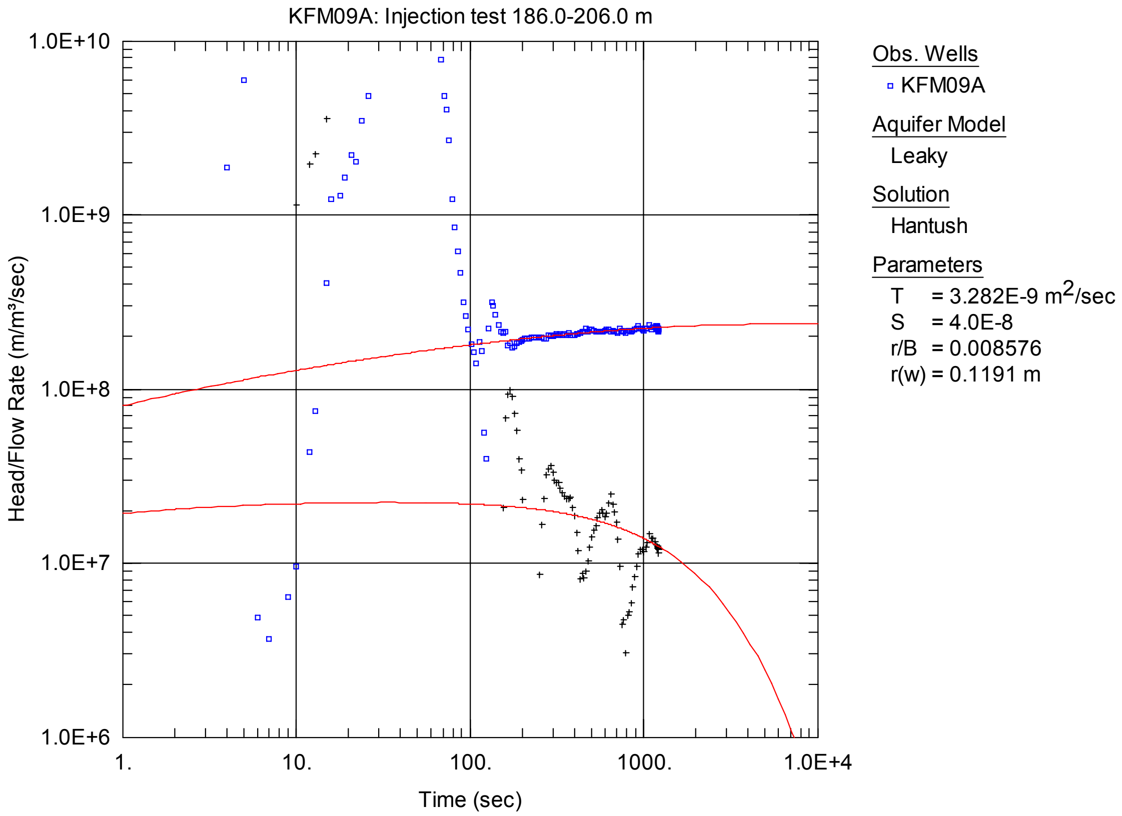


Figure A3-58. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 186.0-206.0 m in KFM09A.*

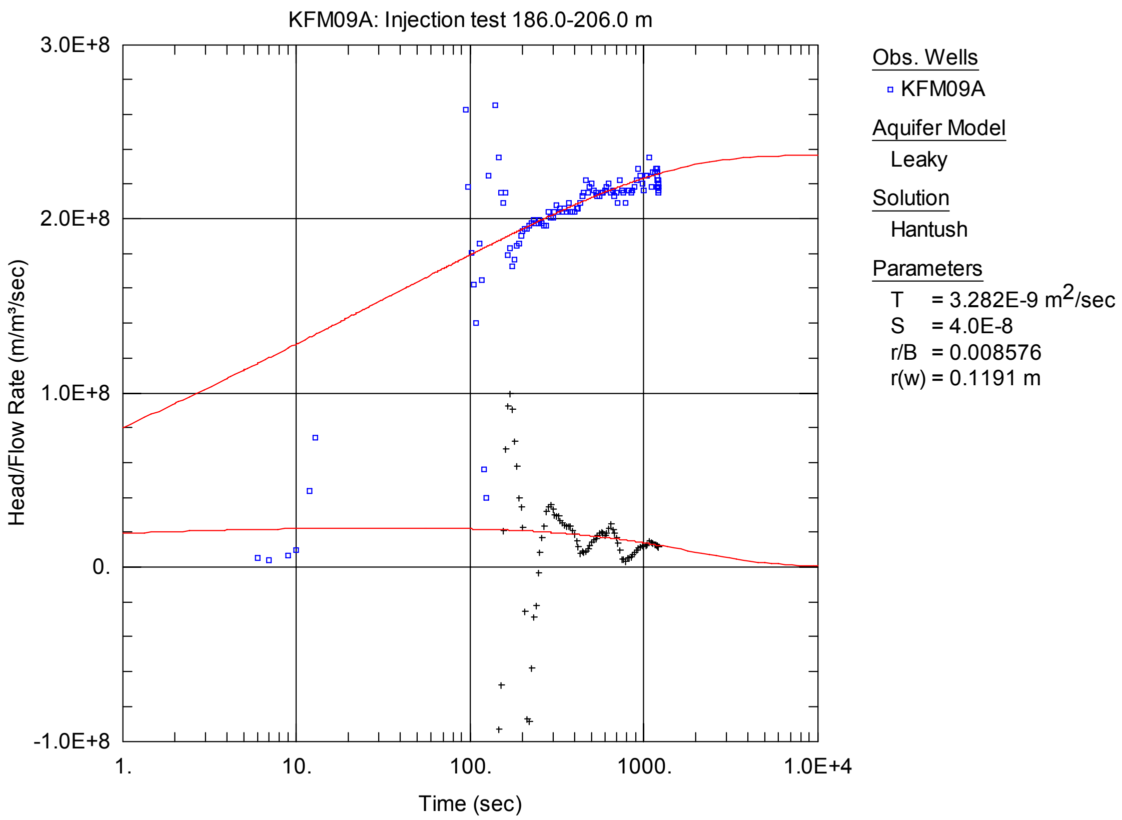


Figure A3-59. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 186.0-206.0 m in KFM09A.*

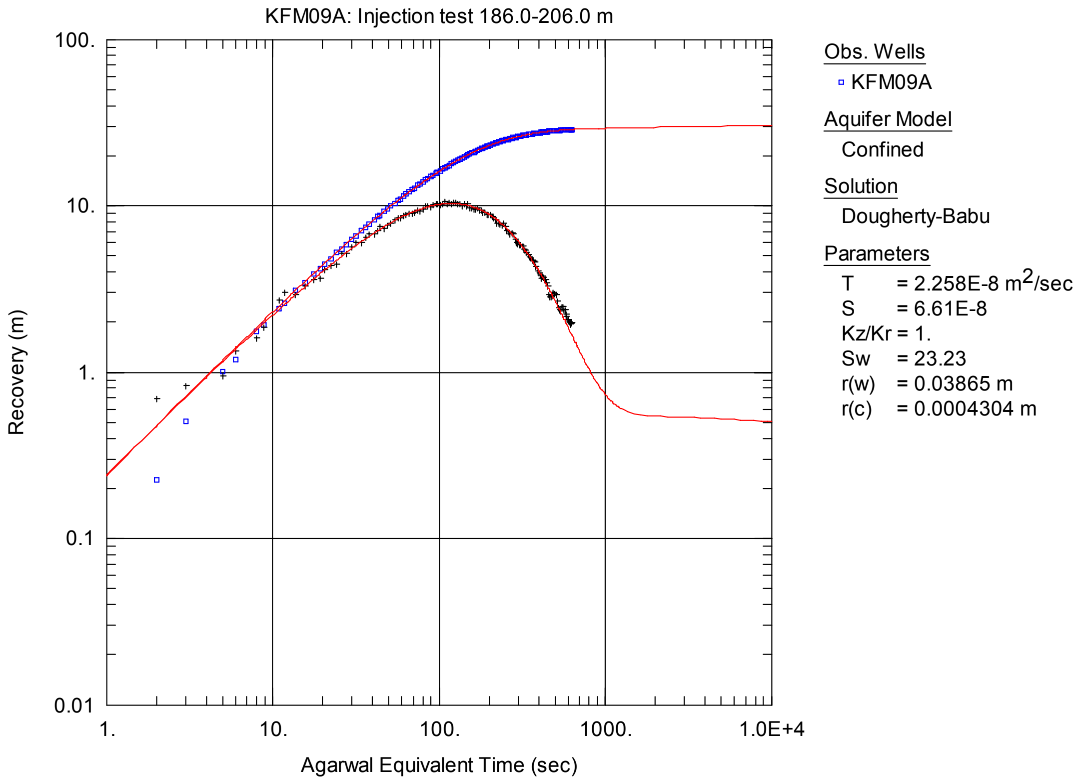


Figure A3-60. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 186.0-206.0 m in KFM09A. The transient evaluation on the recovery period is not regarded as representative.*

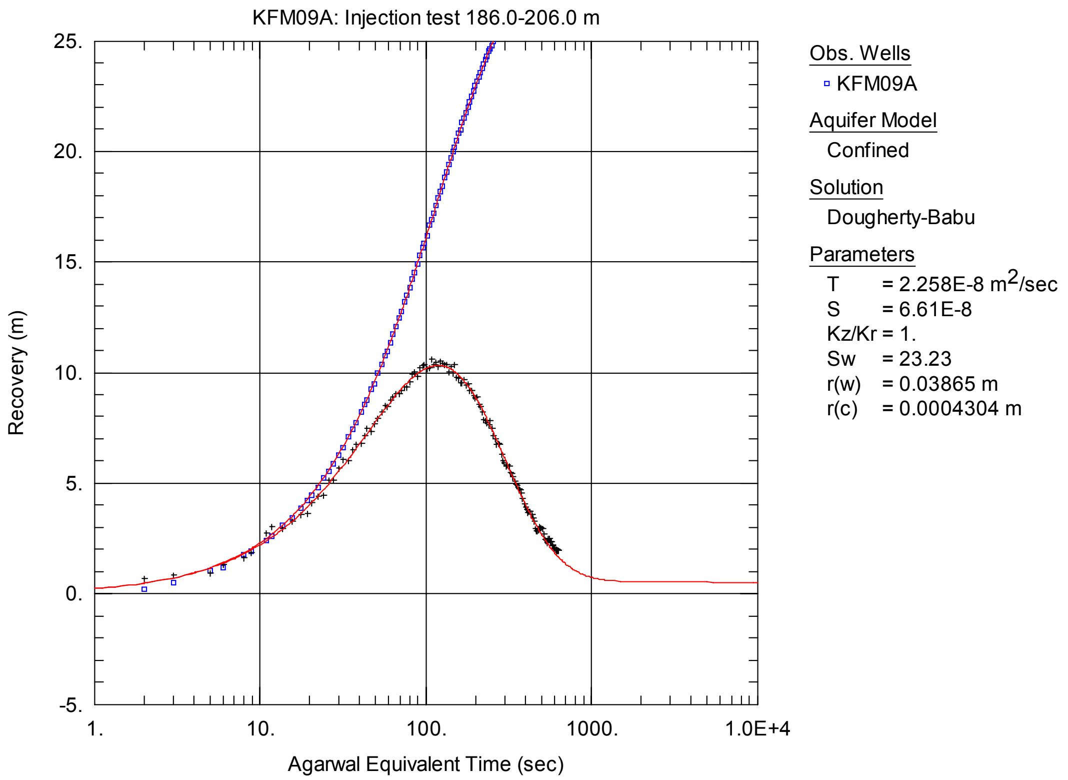


Figure A3-61. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in 186.0-206.0 m in KFM09A. The transient evaluation on the recovery period is not regarded as representative.*

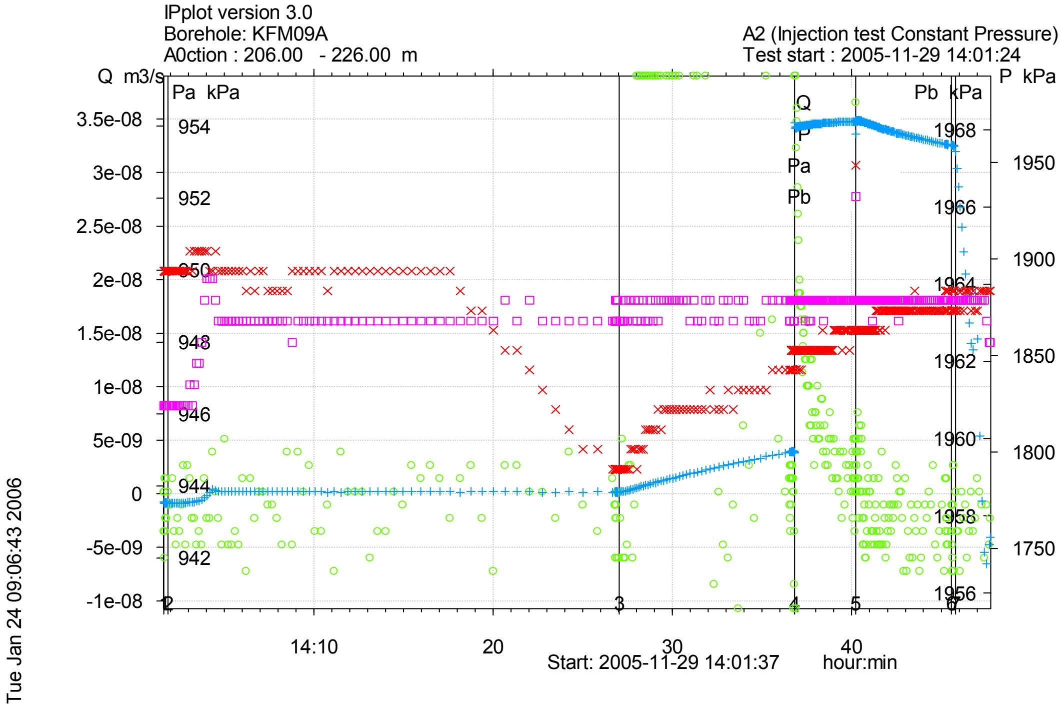


Figure A3-62. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 206.0-226.0 m in borehole KFM09A.*

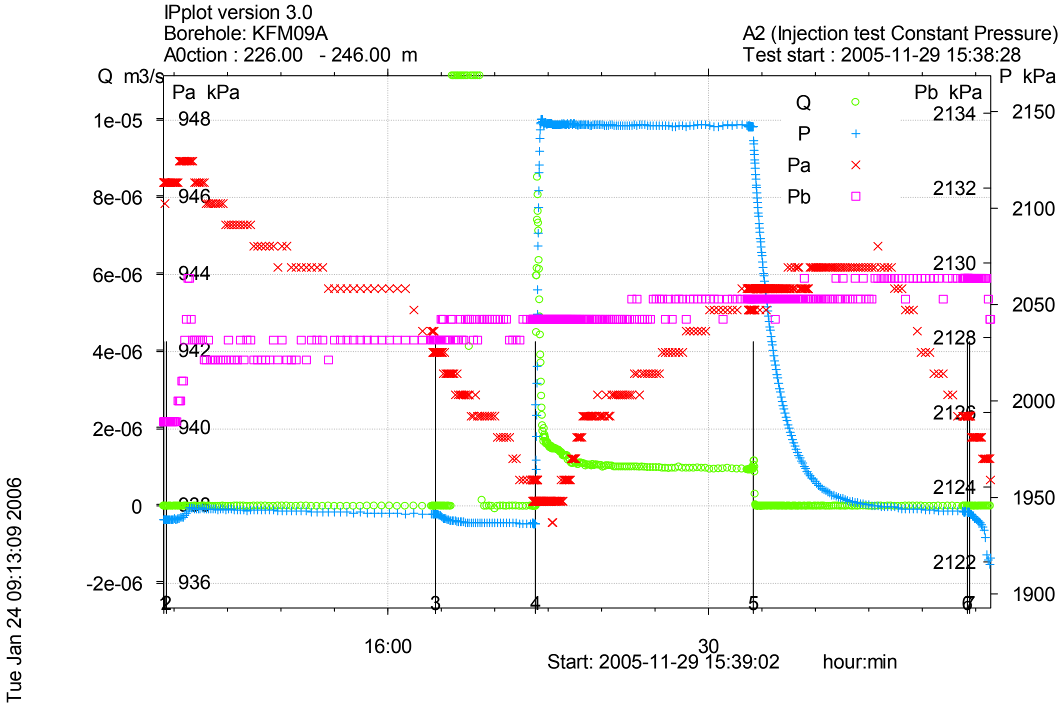


Figure A3-63. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 226.0-246.0 m in borehole KFM09A.*

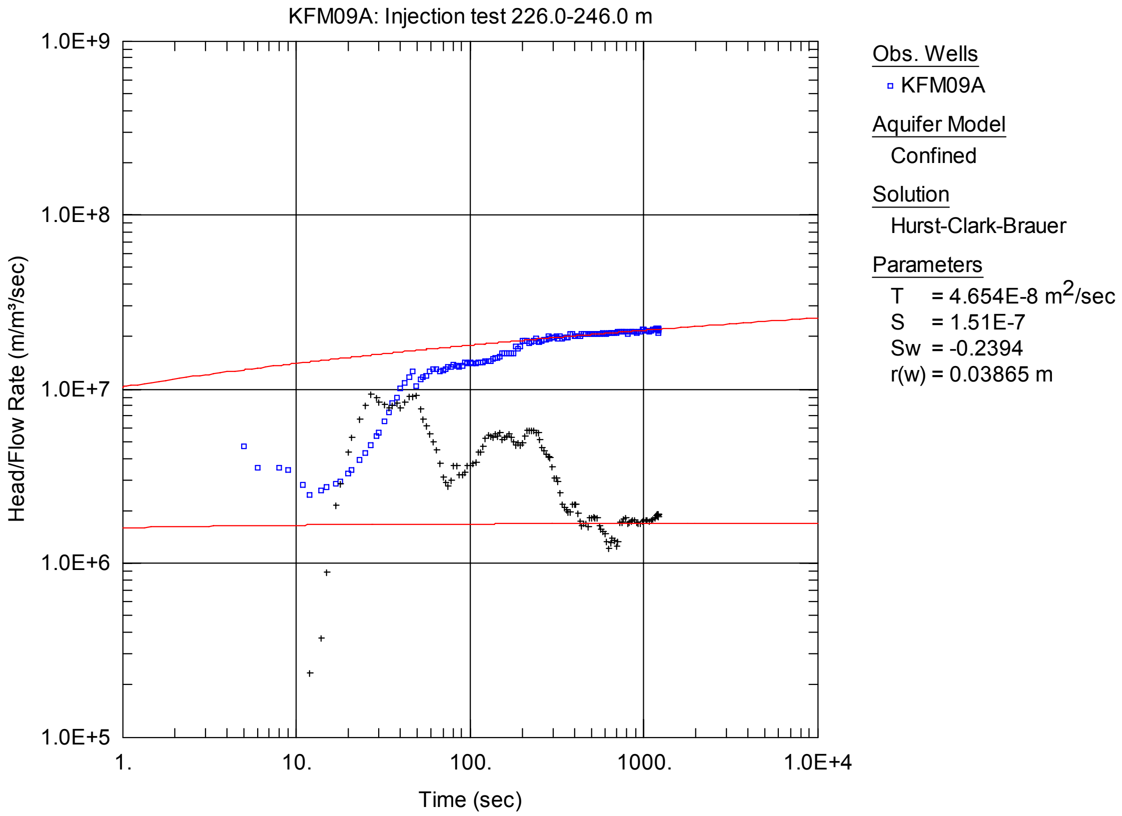


Figure A3-64. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 226.0-246.0 m in KFM09A.*

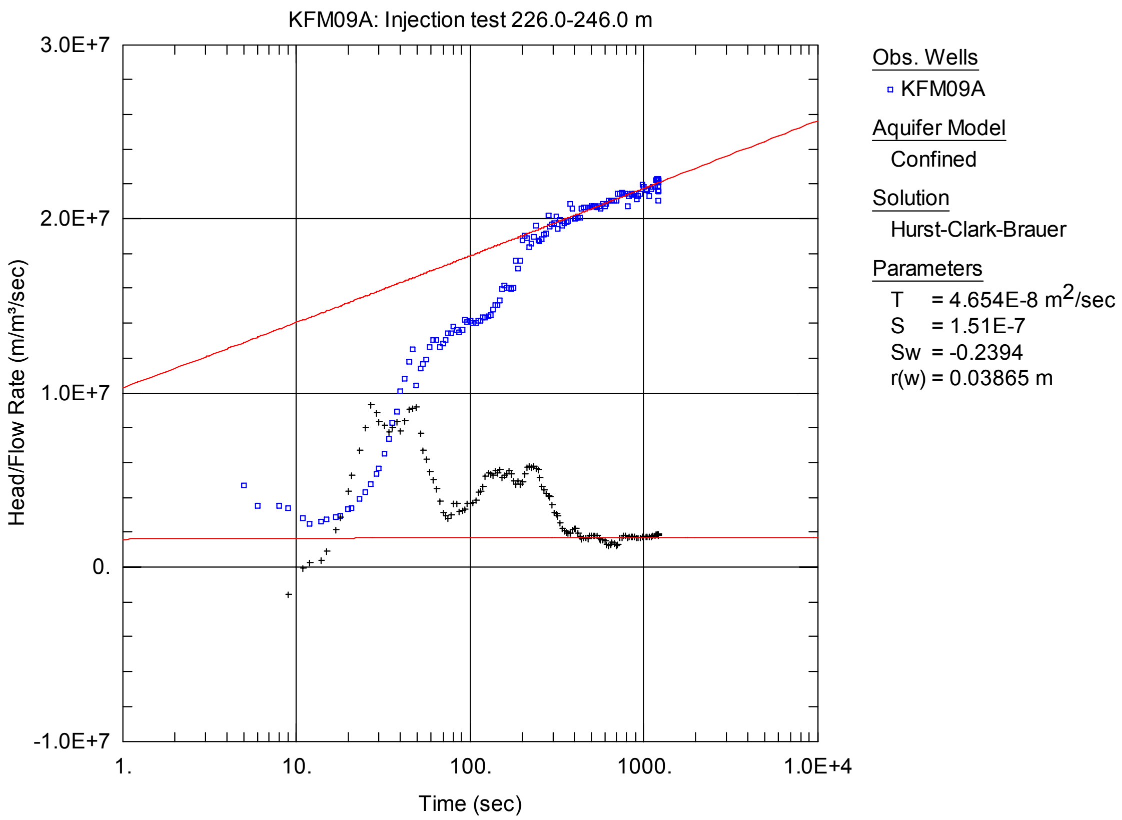


Figure A3-65. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 226.0-246.0 m in KFM09A.*

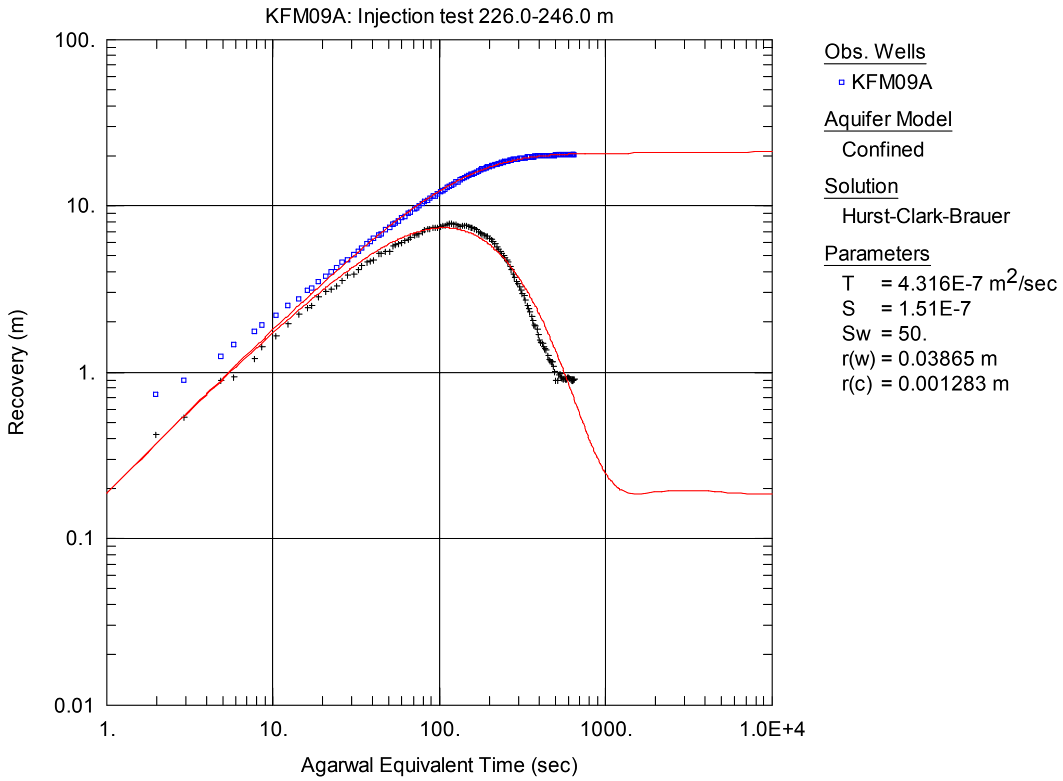


Figure A3-66. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in 226.0-246.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.*

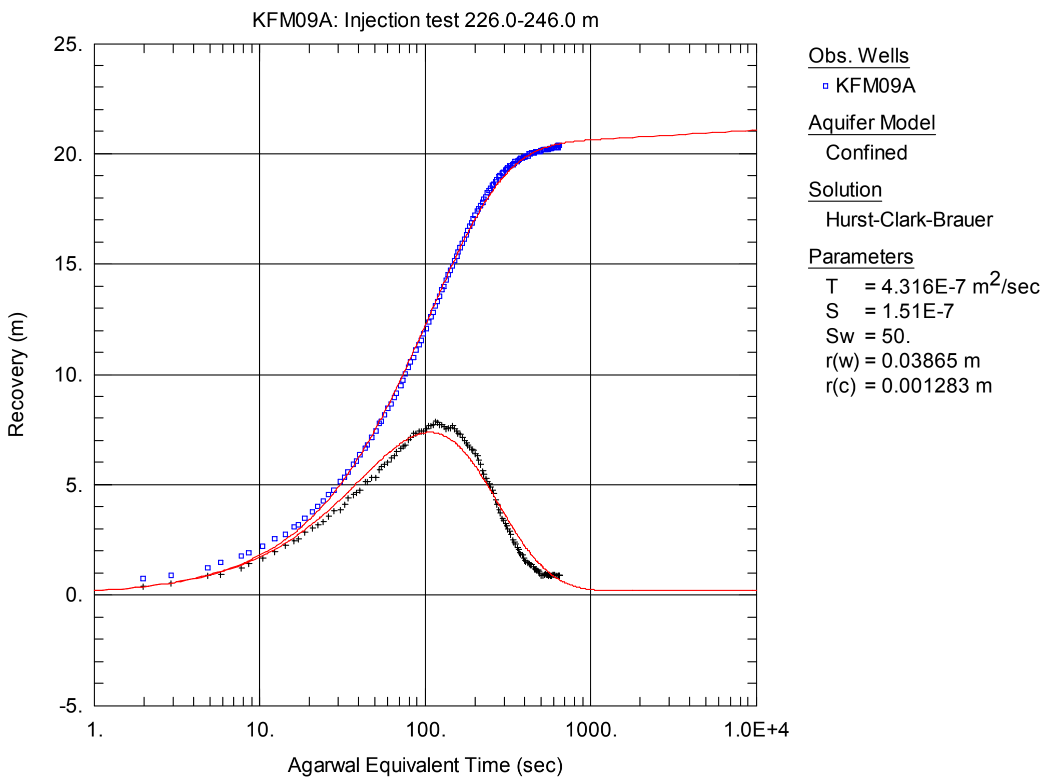


Figure A3-67. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 226.0-246.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period*

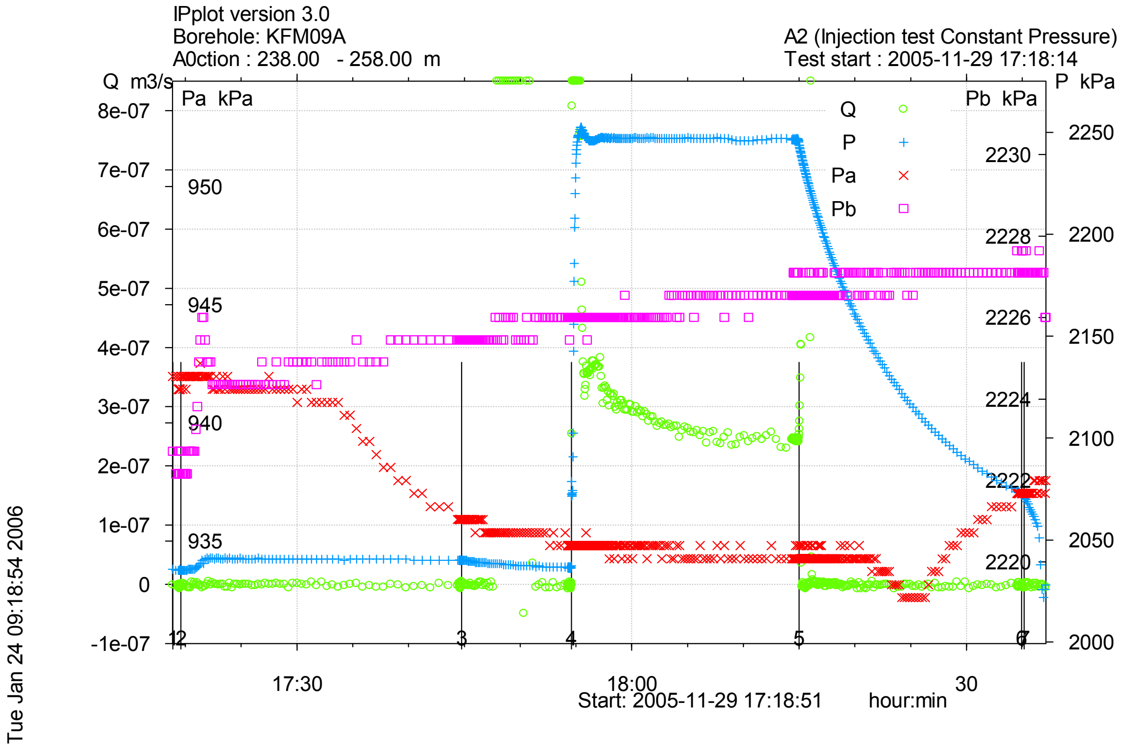


Figure A3-68. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 238.0-258.0 m in borehole KFM09A.*

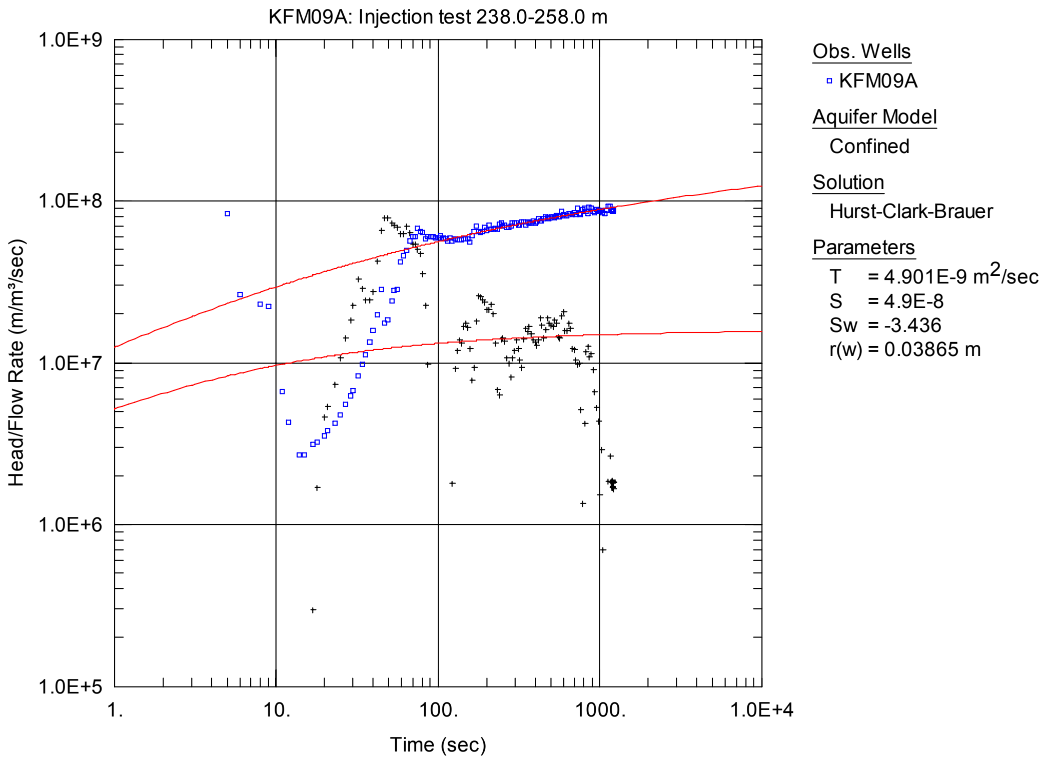


Figure A3-69. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 238.0-258.0 m in KFM09A.*

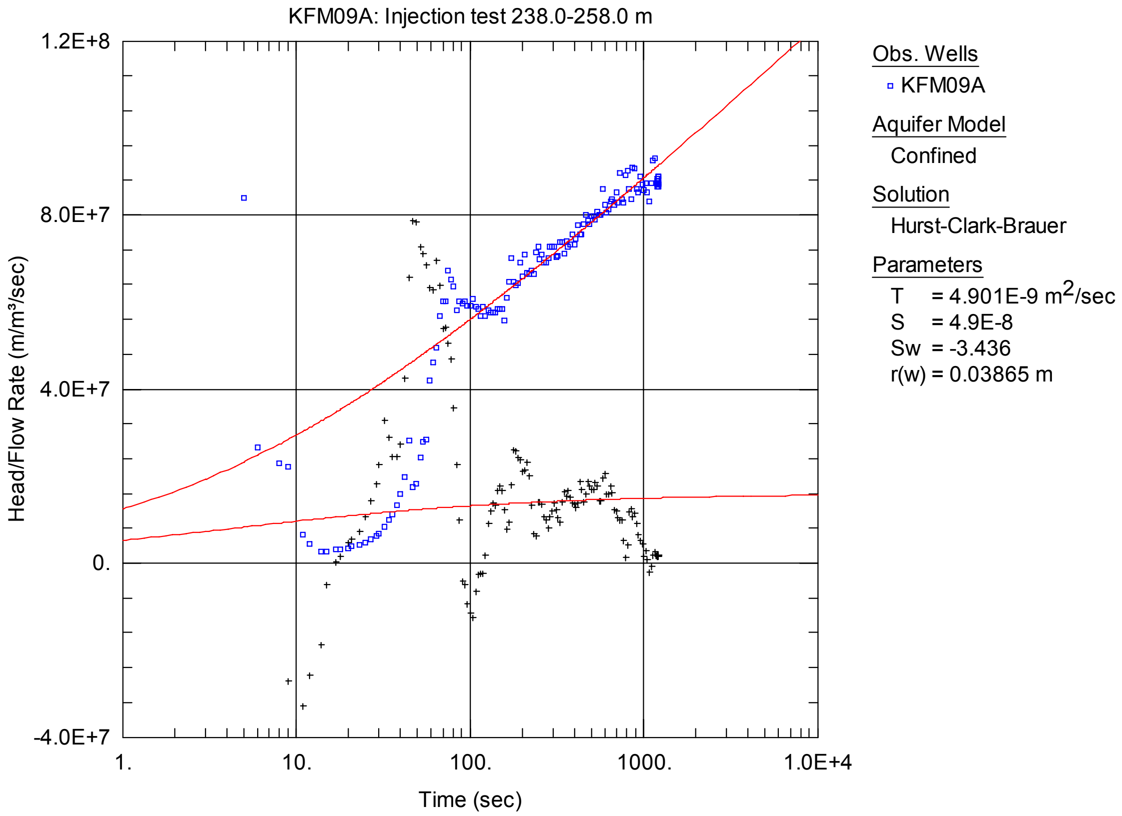


Figure A3-70. Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 238.0-258.0 m in KFM09A.

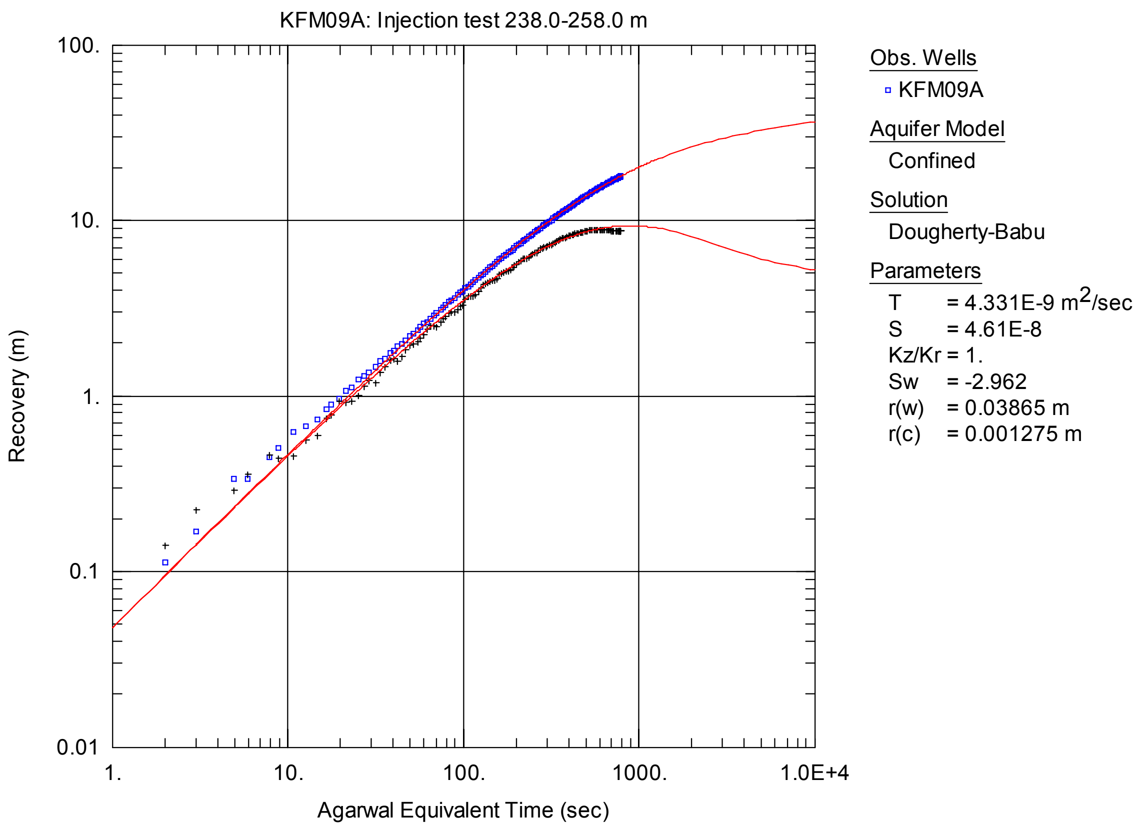


Figure A3-71. Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 238.0-258.0 m in KFM09A.

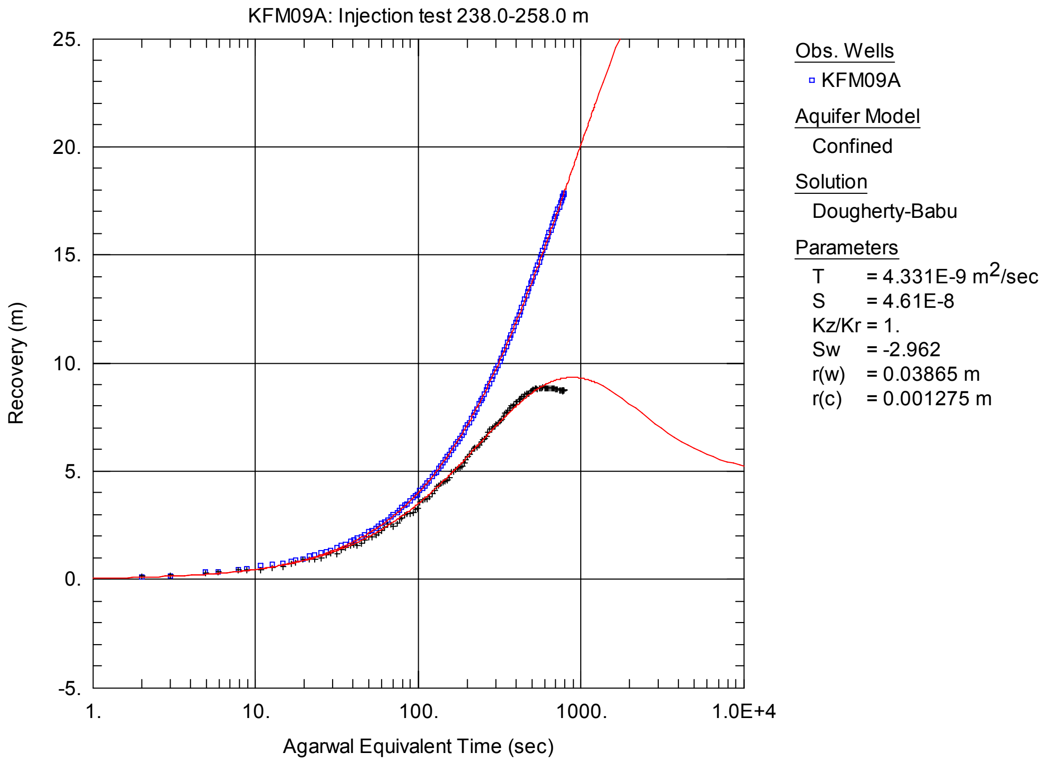


Figure A3-72. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in 238.0-258.0 m in KFM09A.*

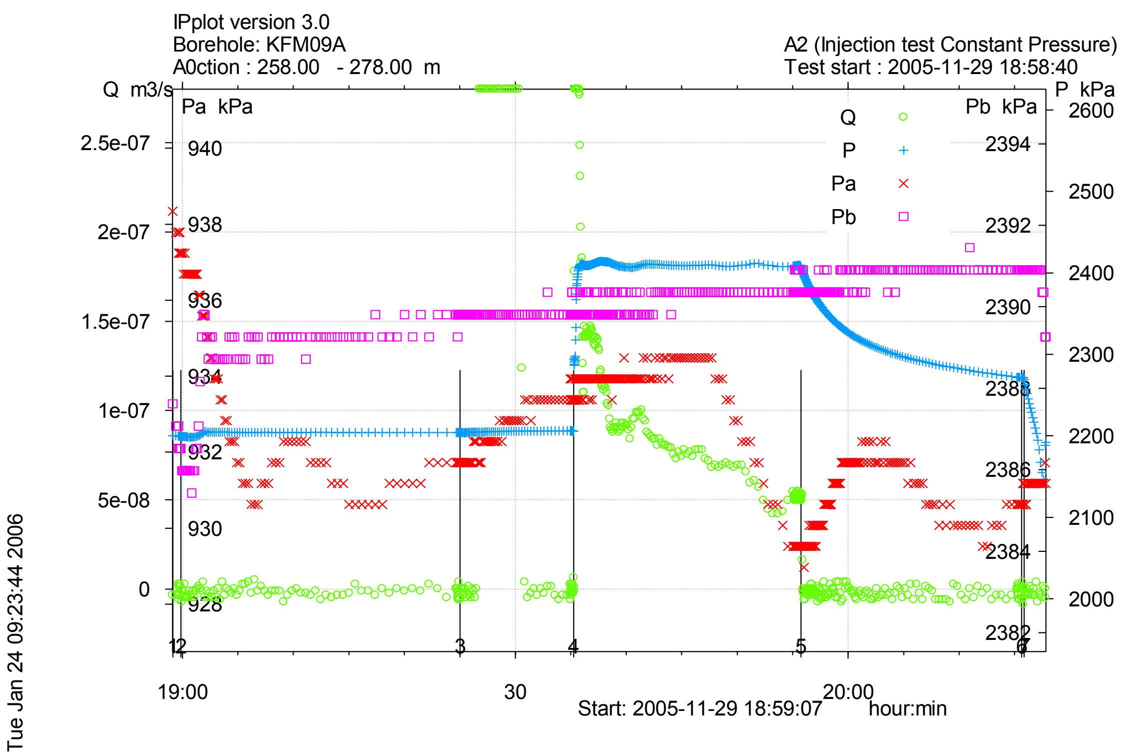


Figure A3-73. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 258.0-278.0 m in borehole KFM09A.*

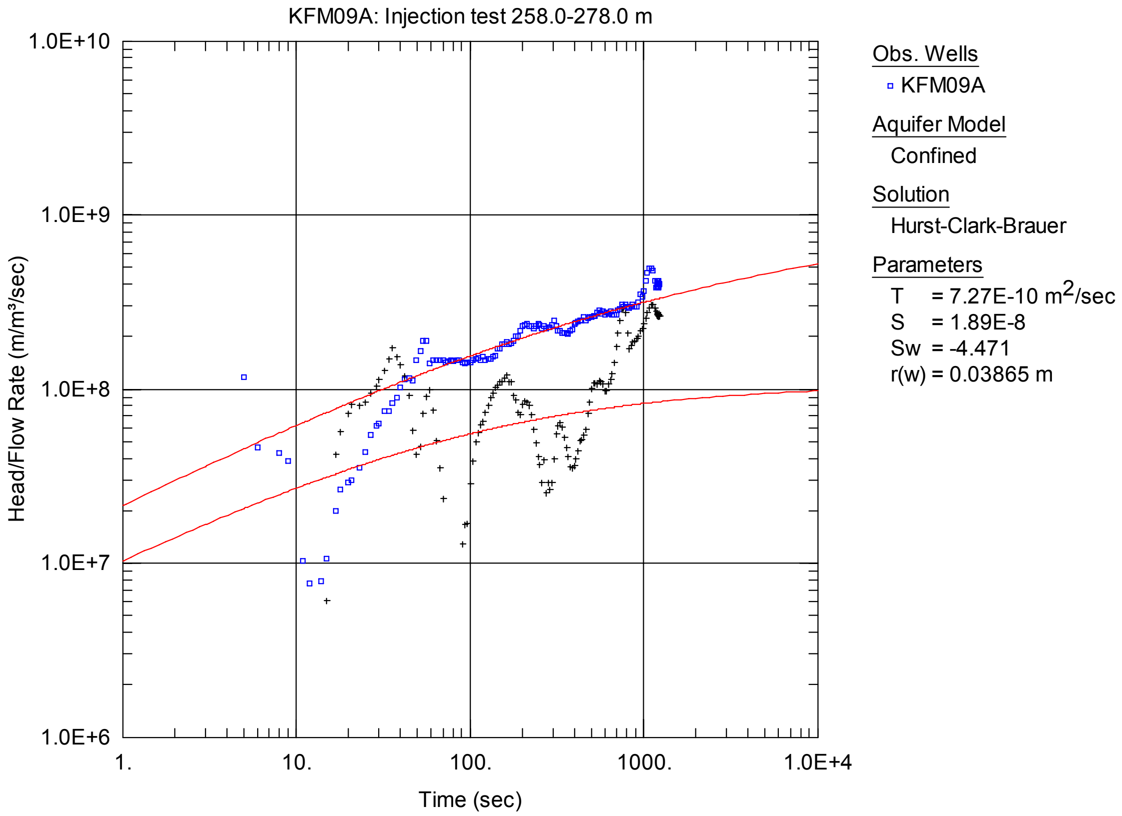


Figure A3-74. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 258.0-278.0 m in KFM09A.*

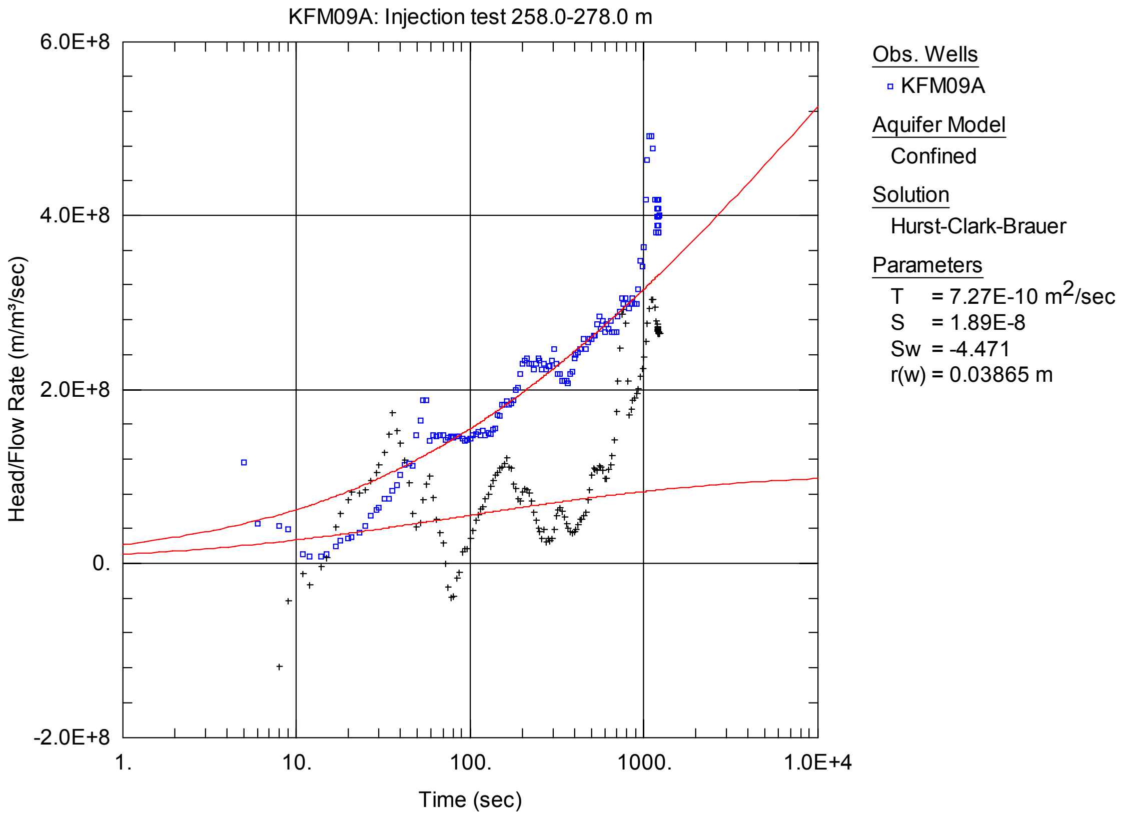


Figure A3-75. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 258.0-278.0 m in KFM09A.*

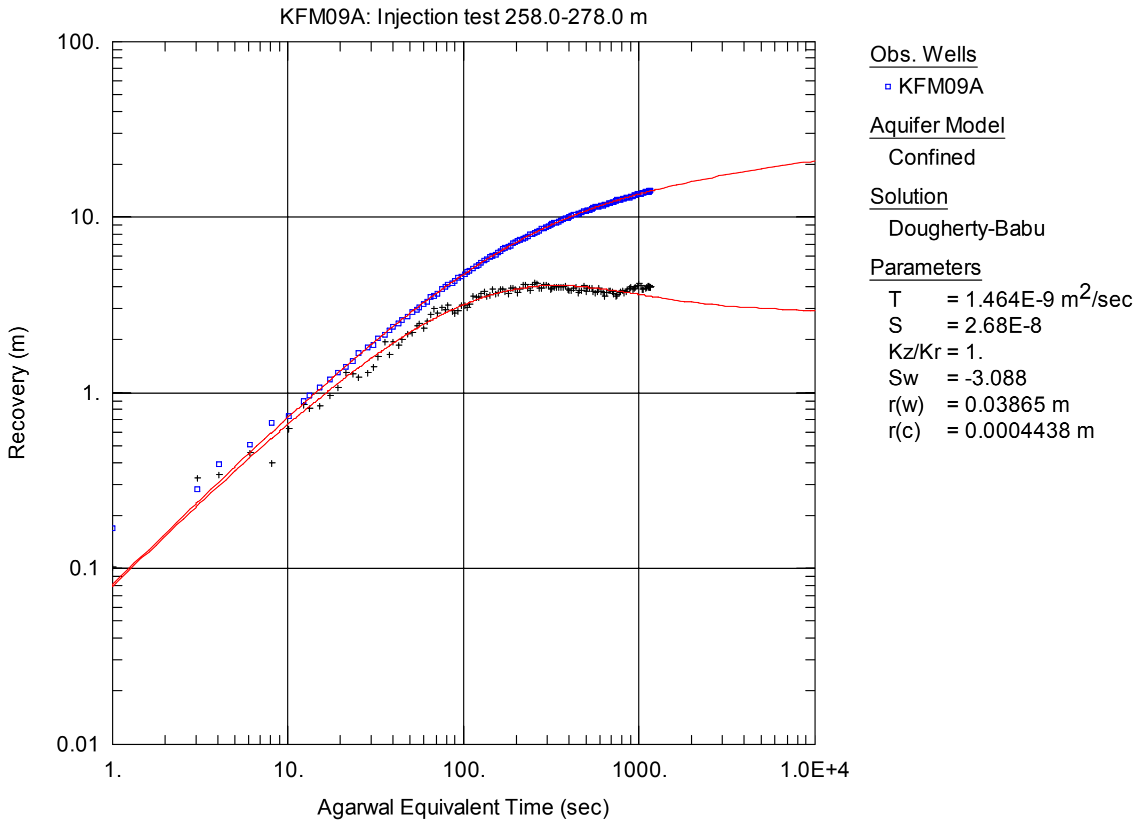


Figure A3-76. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 258.0-278.0 m in KFM09A.*

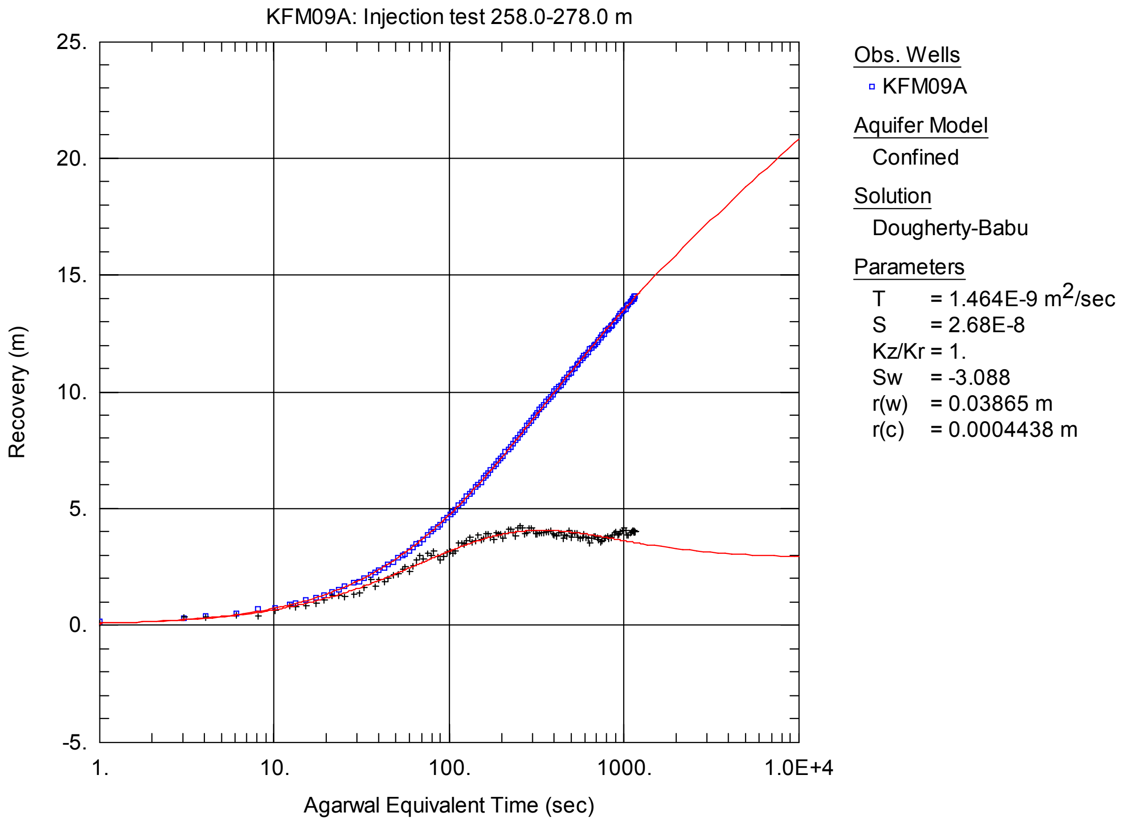


Figure A3-77. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 258.0-278.0 m in KFM09A.*

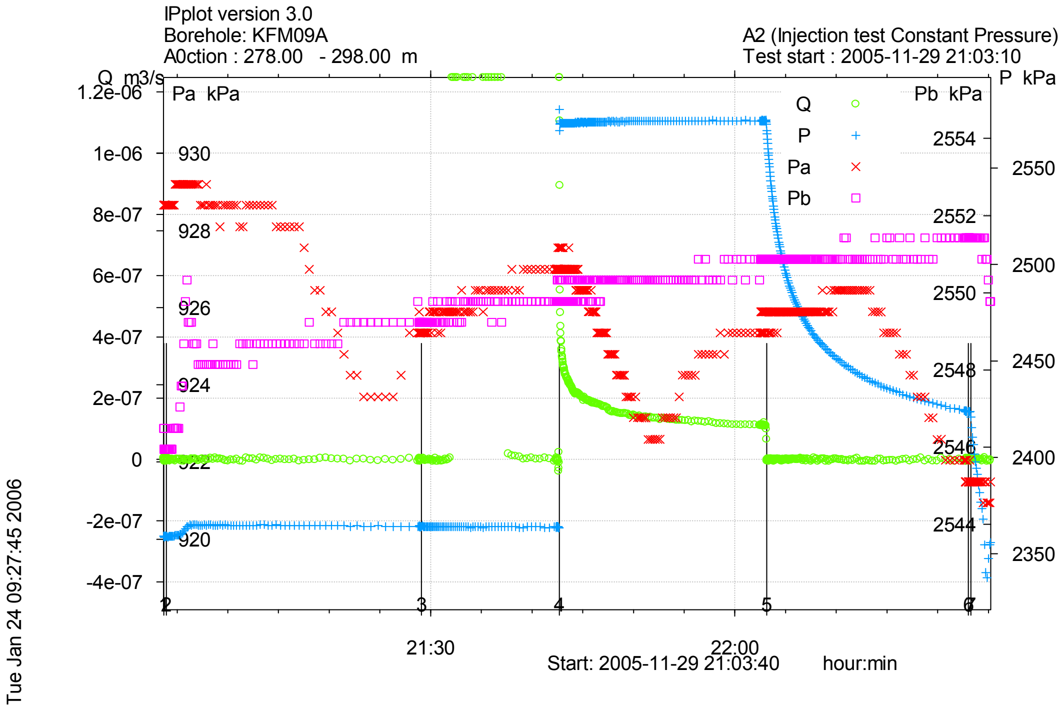


Figure A3-78. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 278.0-298.0 m in borehole KFM09A.*

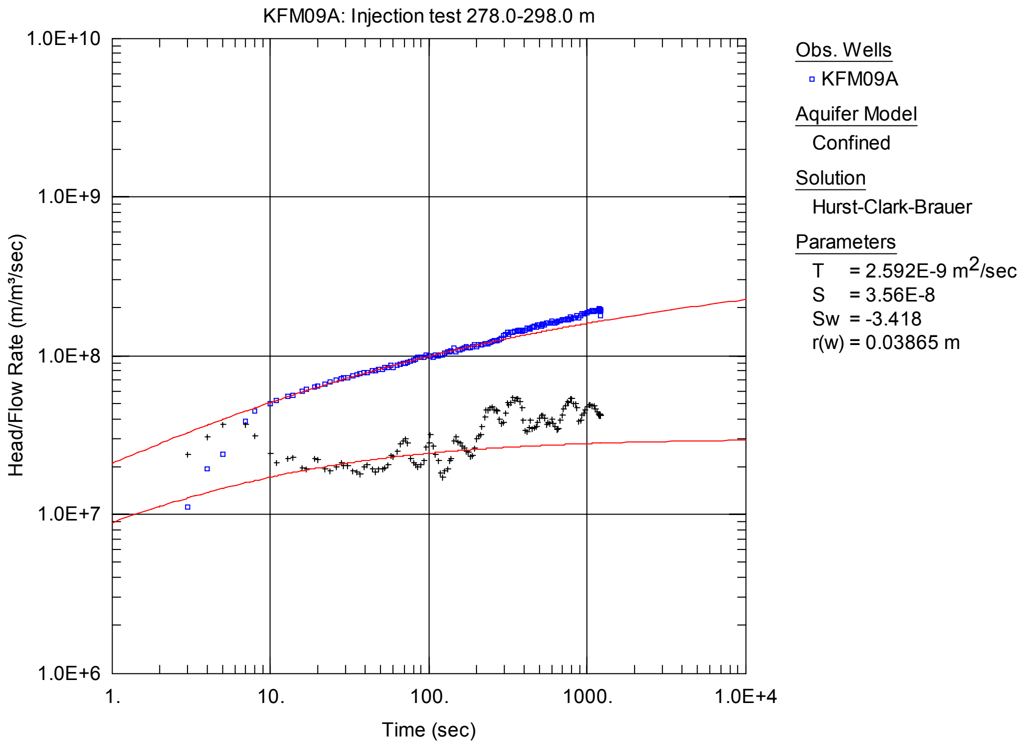


Figure A3-79. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 278.0-298.0 m in KFM09A. This plot shows the first of two different PRF:s during the injection period in this section.*

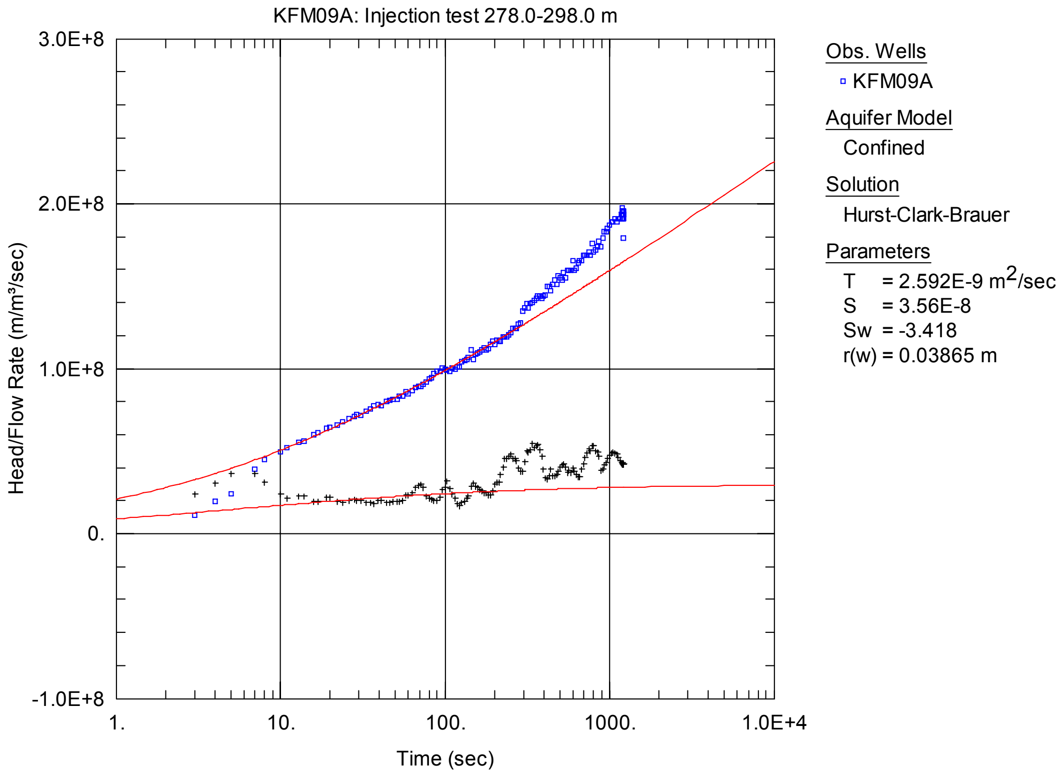


Figure A3-80. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 278.0-298.0x m in KFM09A. This plot shows the first of two different PRF:s during the injection period in this section.*

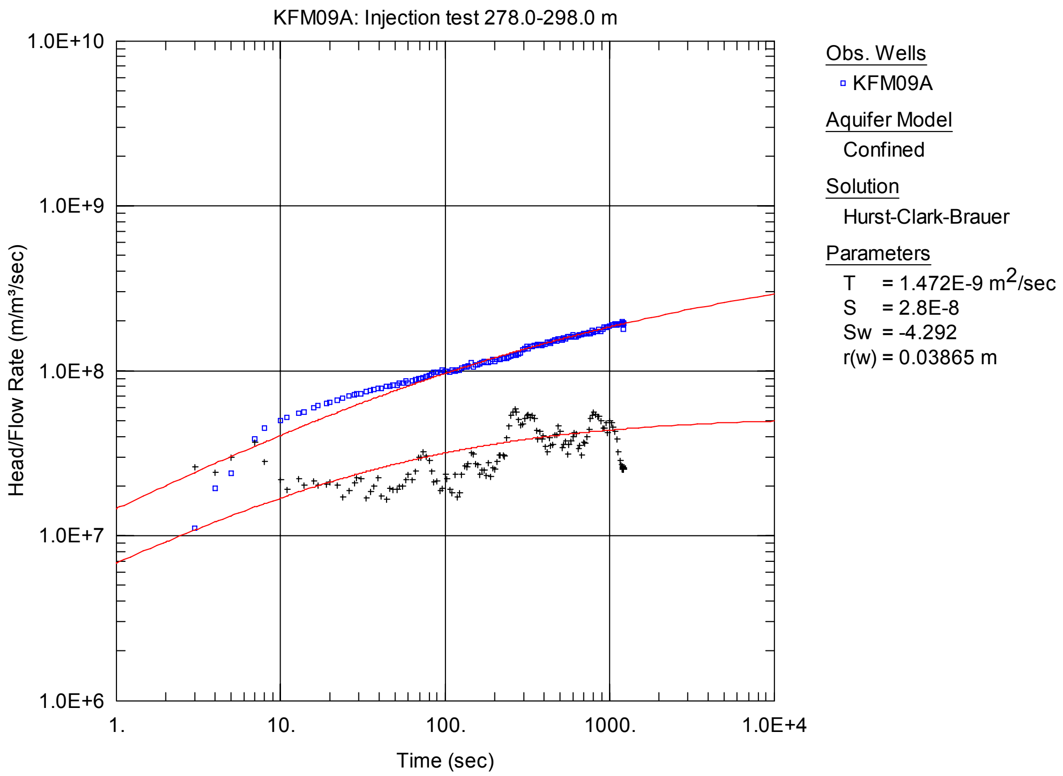


Figure A3-81. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 278.0-298.0 m in KFM09A. This plot shows the second of two different PRF:s during the injection period in this section.*

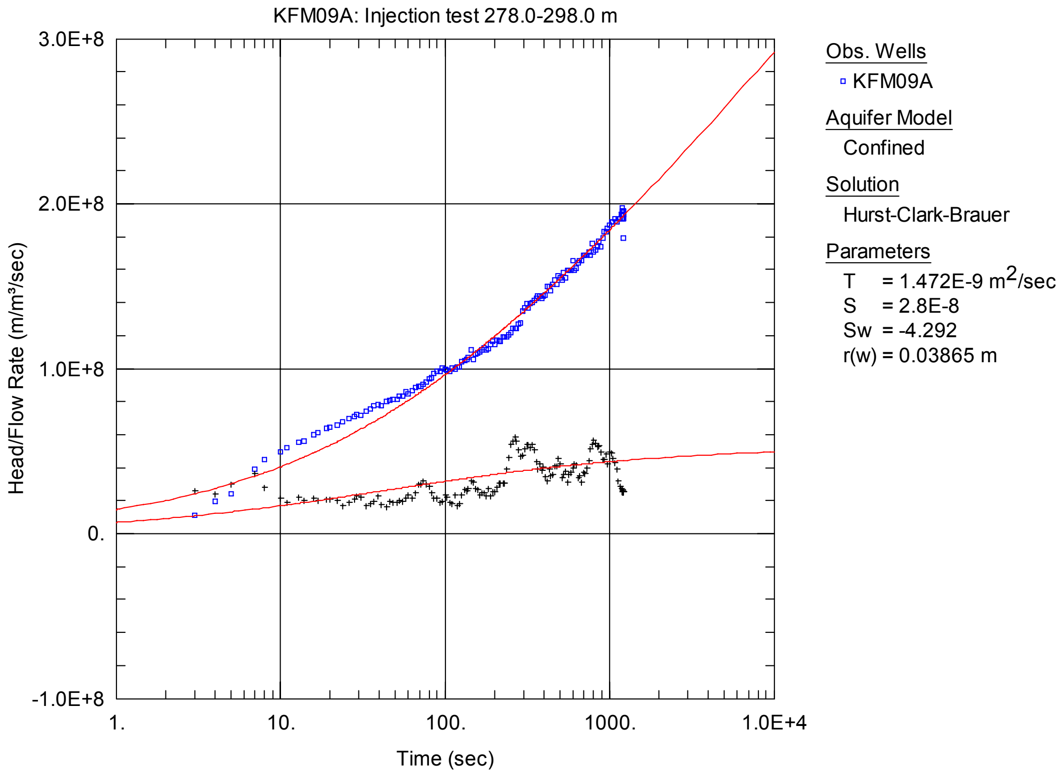


Figure A3-82. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 278.0-298.0 m in KFM09A. This plot shows the second of two different PRF:s during the injection period in this section.*

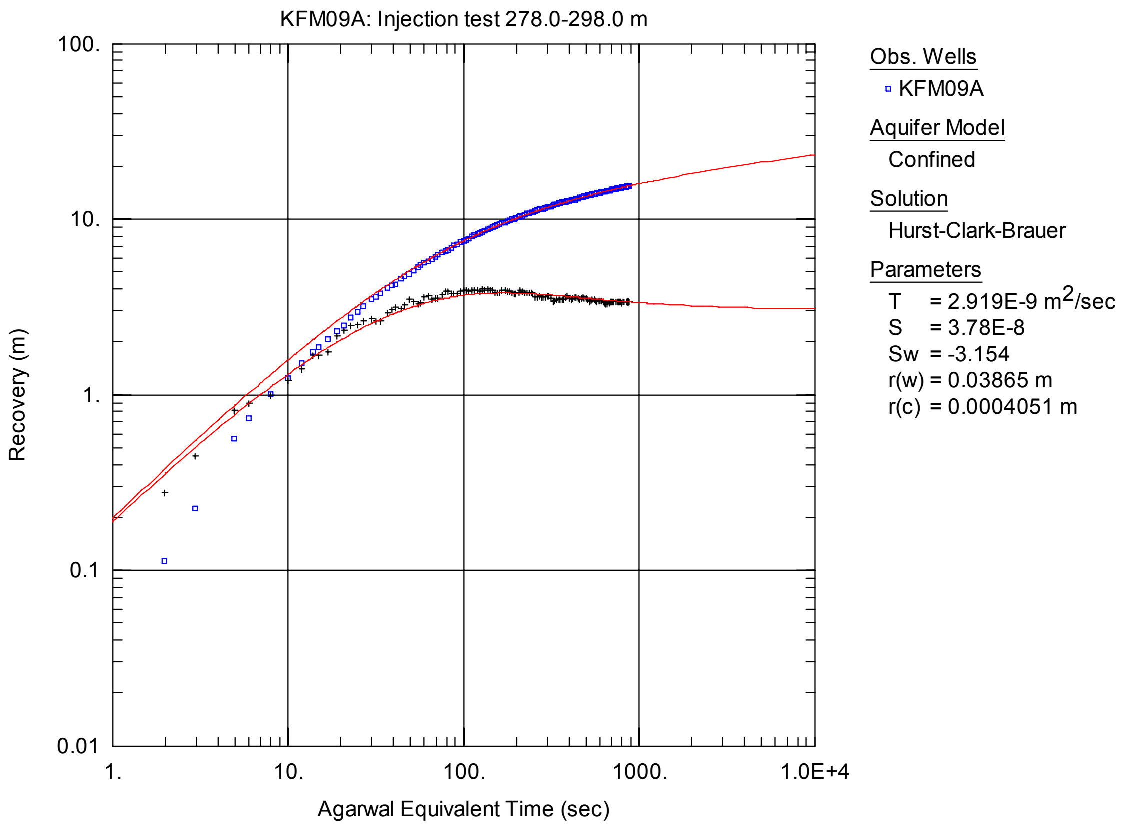


Figure A3-83. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 278.0-298.0 m in KFM09A.*

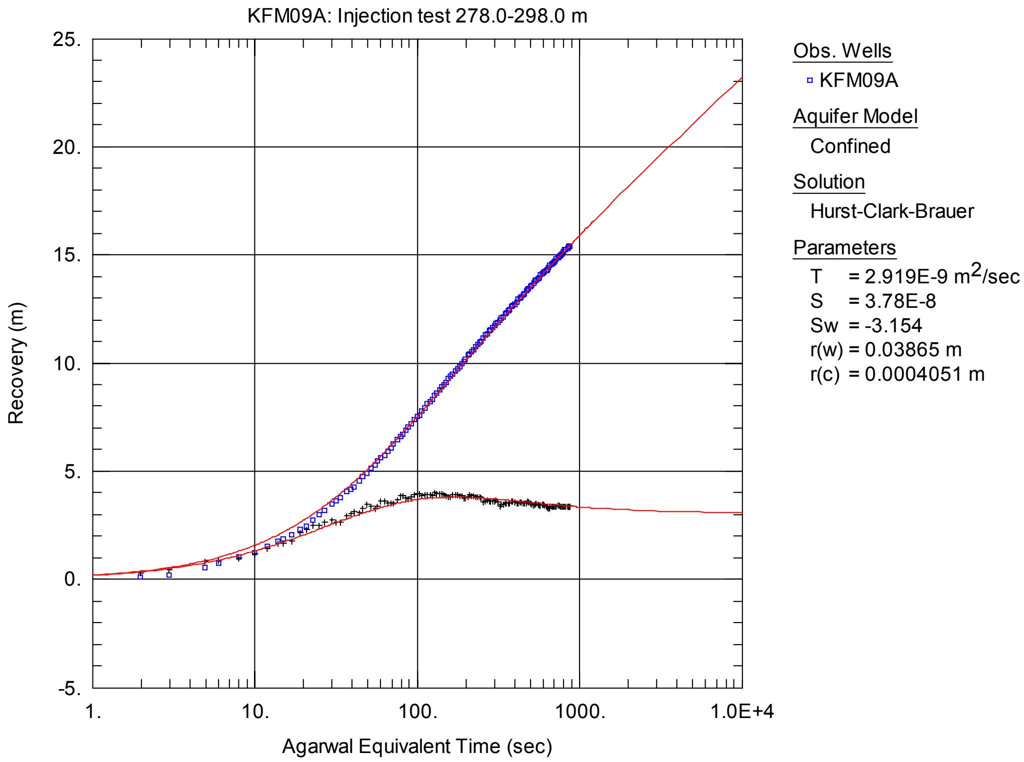


__Figure A3-84.__ Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in 278.0-298.0 m in KFM09A.

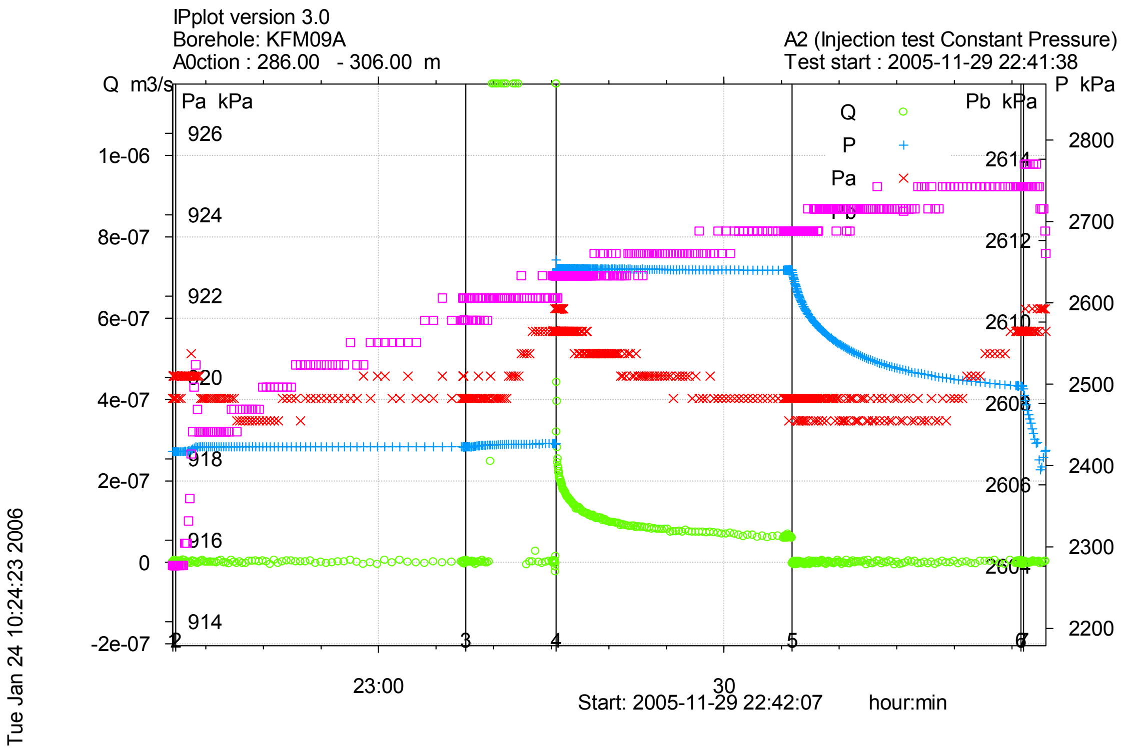


__Figure A3-85.__ Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 286.0-306.0 m in borehole KFM09A.

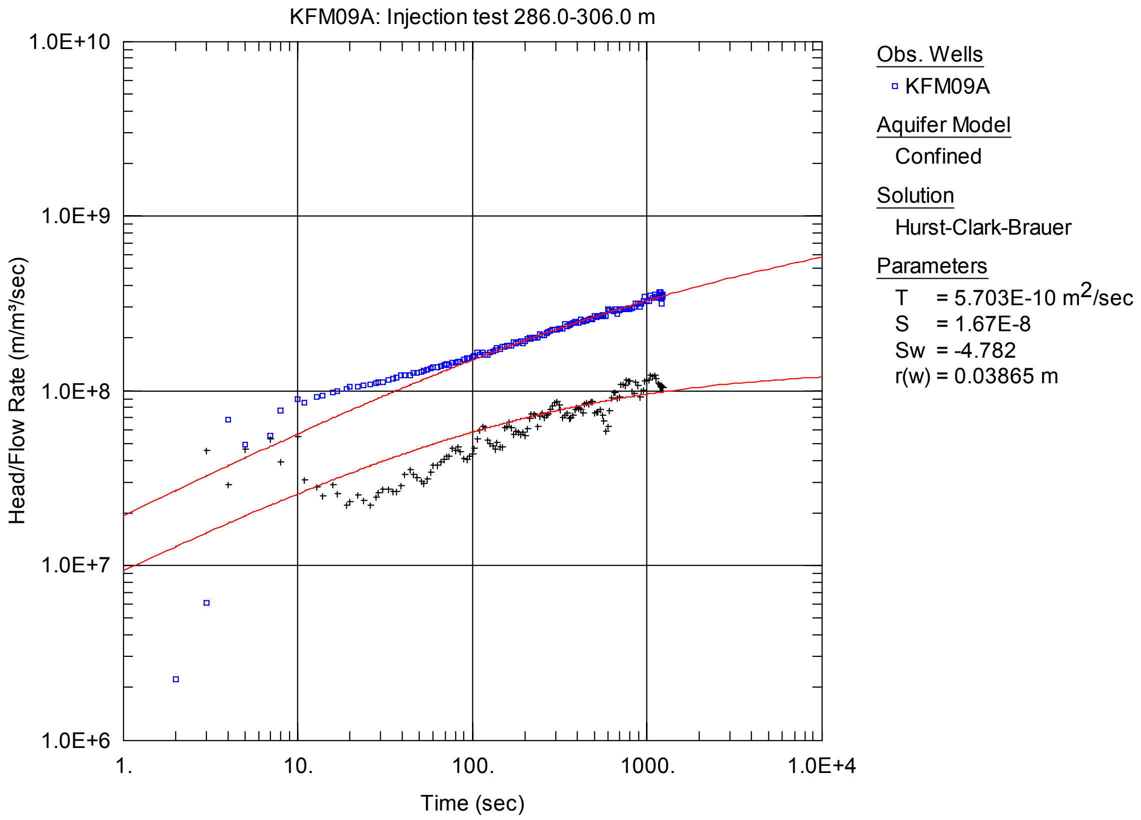


Figure A3-86. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 286.0-306.0 m in KFM09A.*

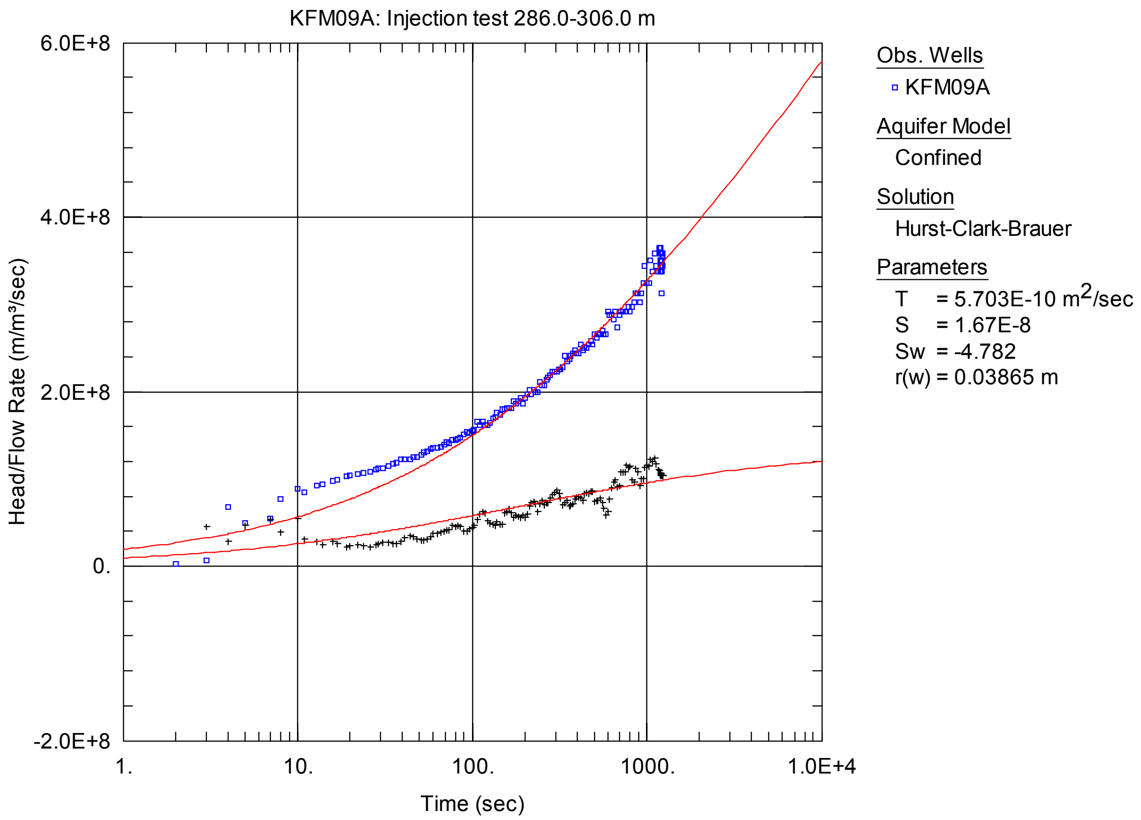


Figure A3-87. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 286.0-306.0 m in KFM09A.*

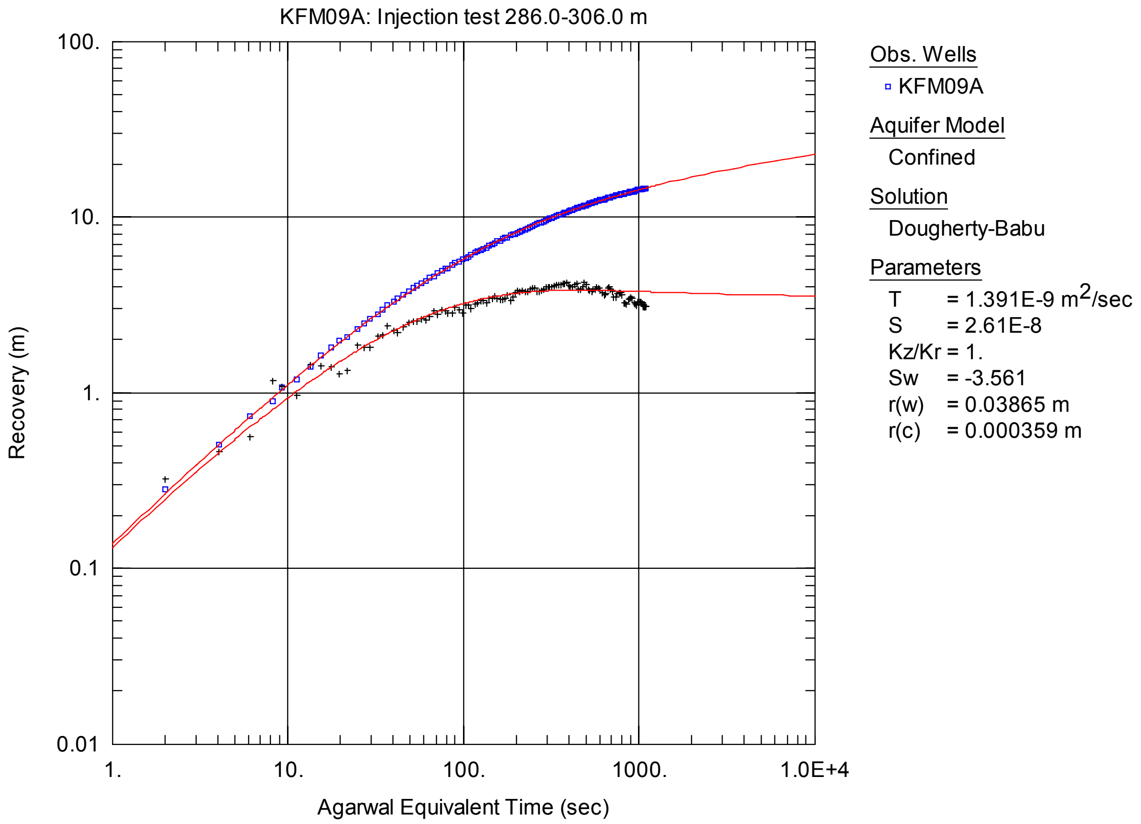


Figure A3-88. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 286.0-306.0 m in KFM09A.*

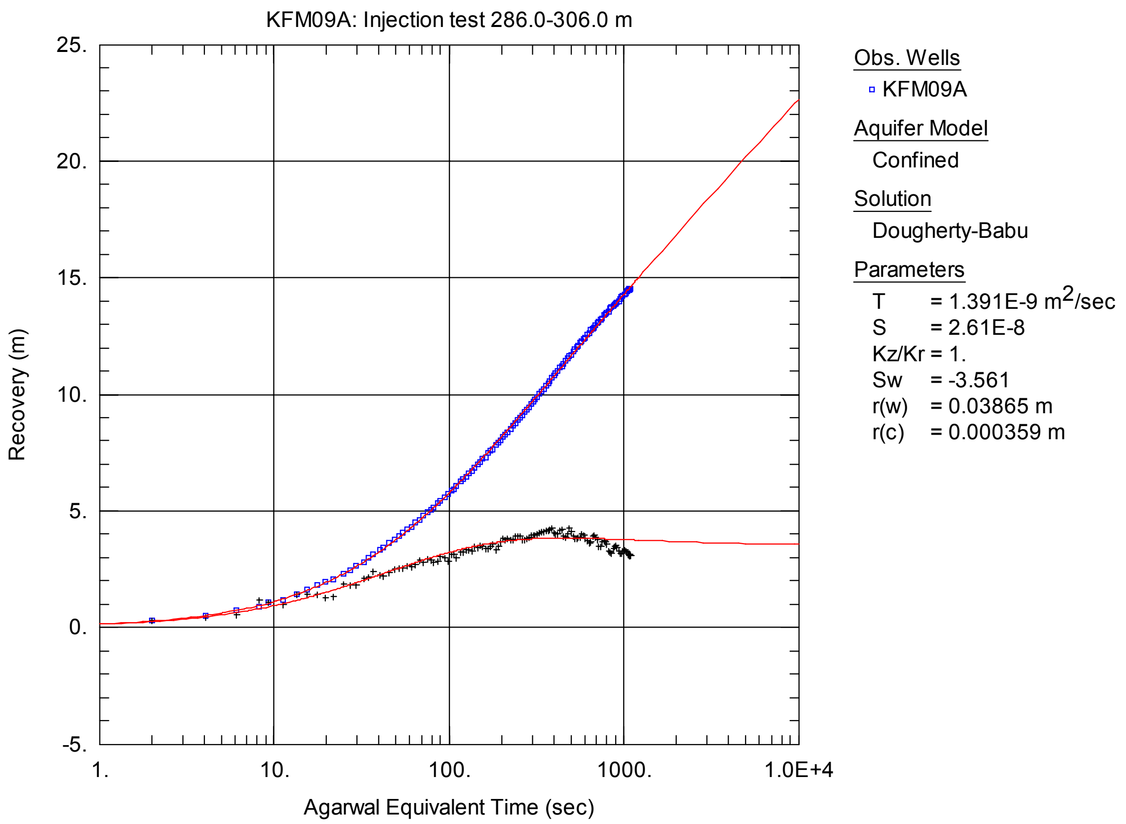


Figure A3-89. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 286.0-306.0 m in KFM09A.*

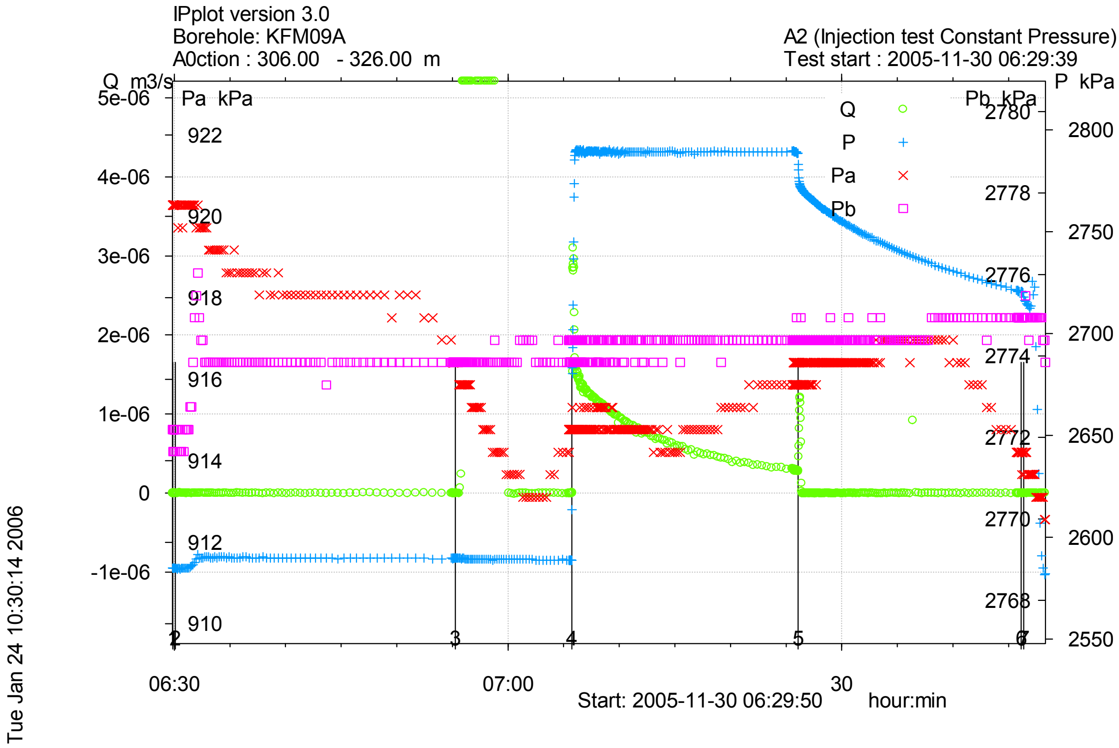


Figure A3-90. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 306.0-326.0 m in borehole KFM09A.*

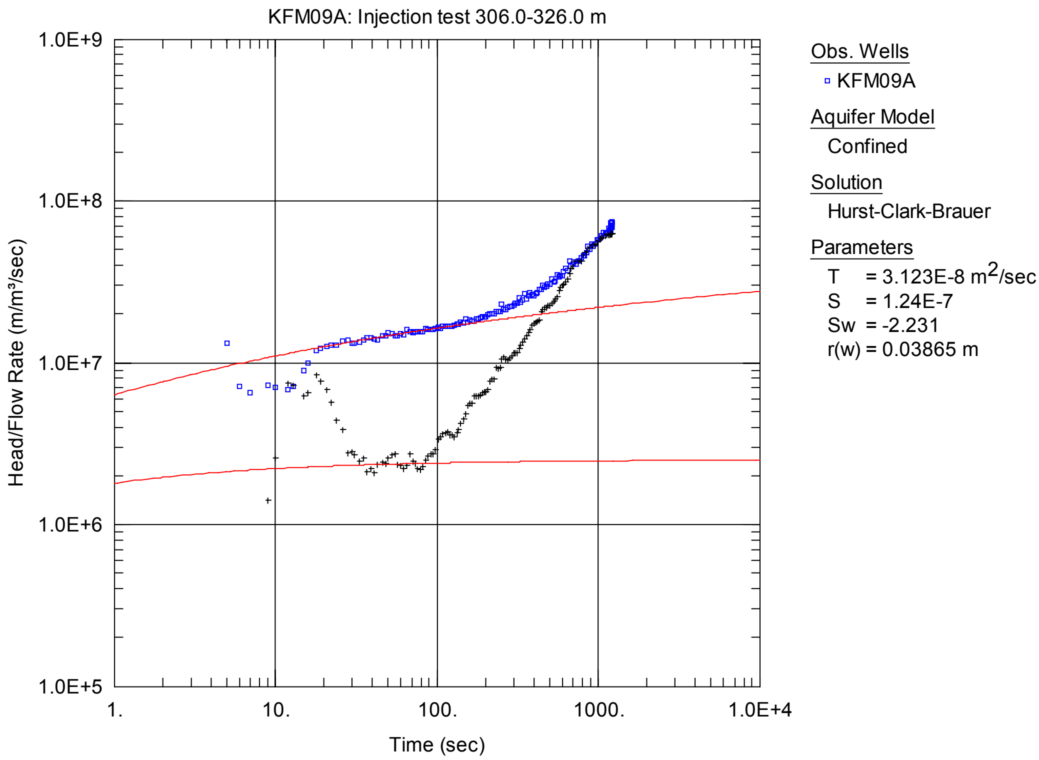


Figure A3-91. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 306.0-326.0 m in KFM09A.*

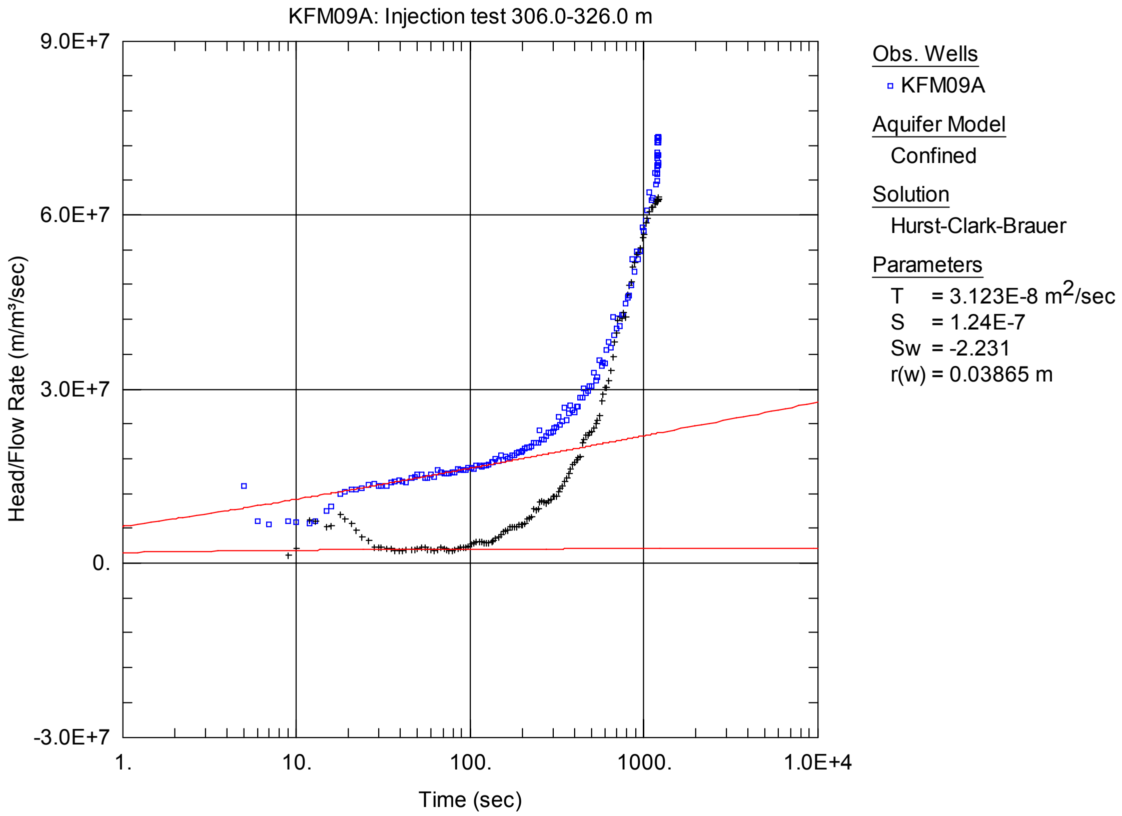


Figure A3-92. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 306.0-326.0 m in KFM09A.*

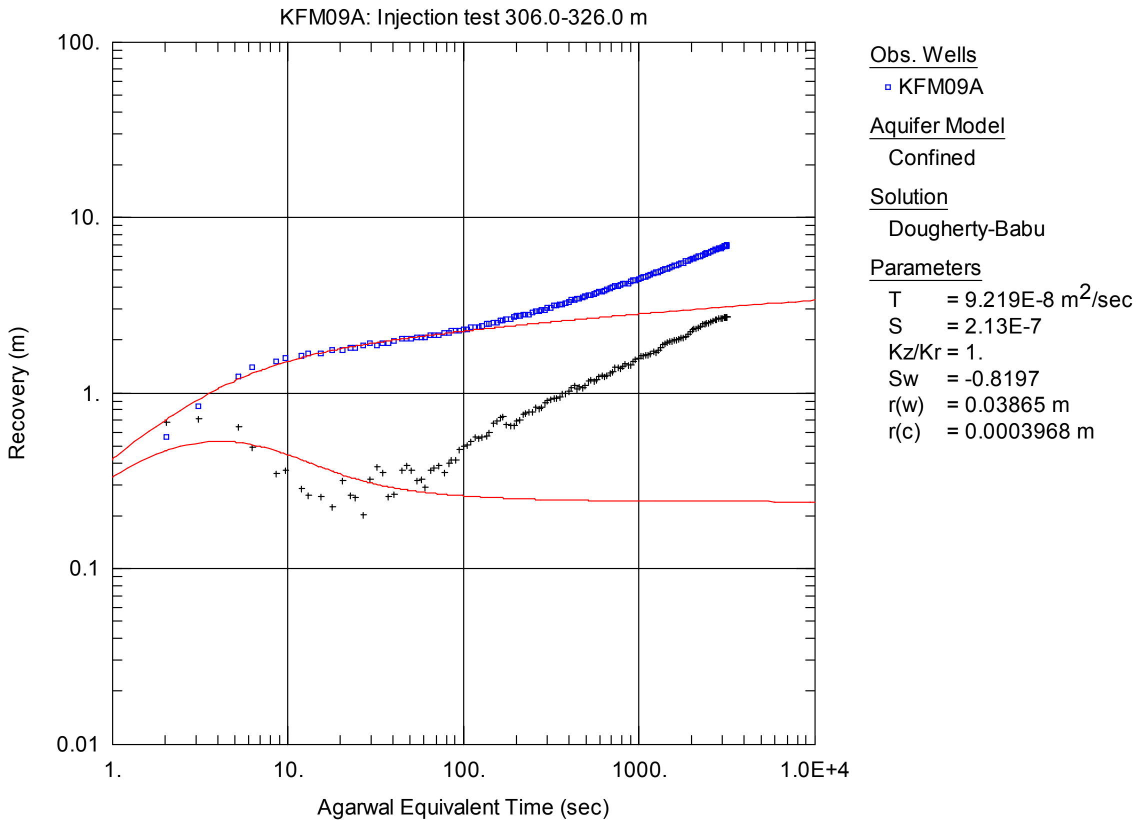


Figure A3-93. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 306.0-326.0 m in KFM09A.*

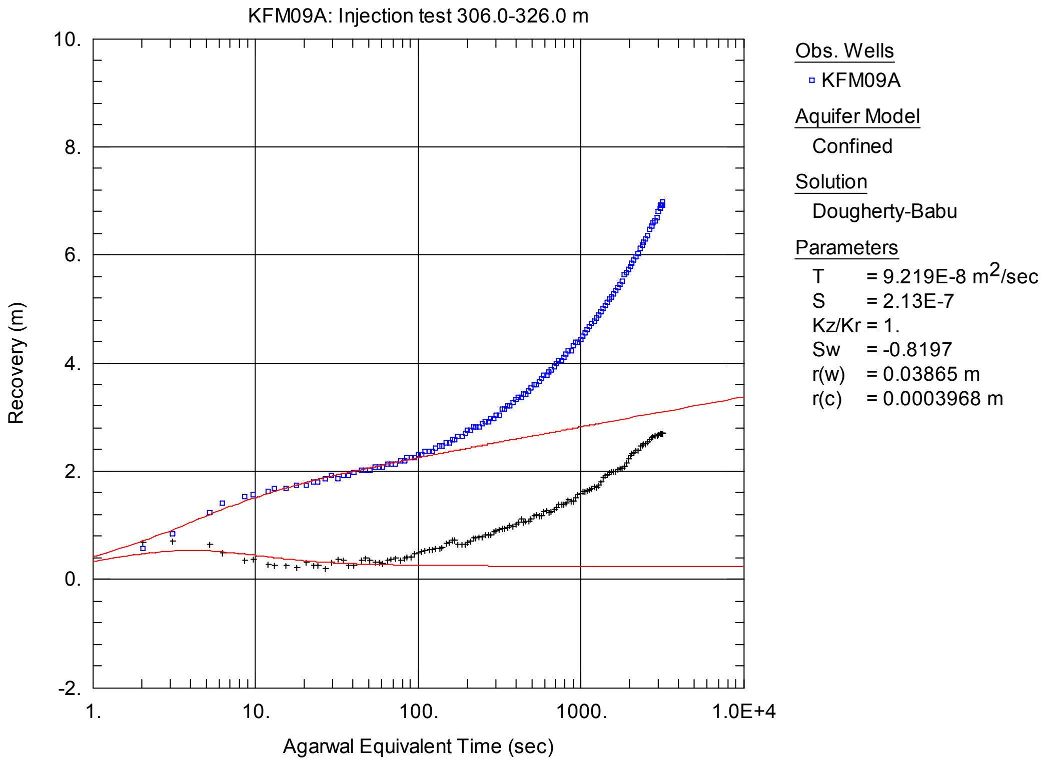


Figure A3-94. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 306.0-326.0 m in KFM09A.*

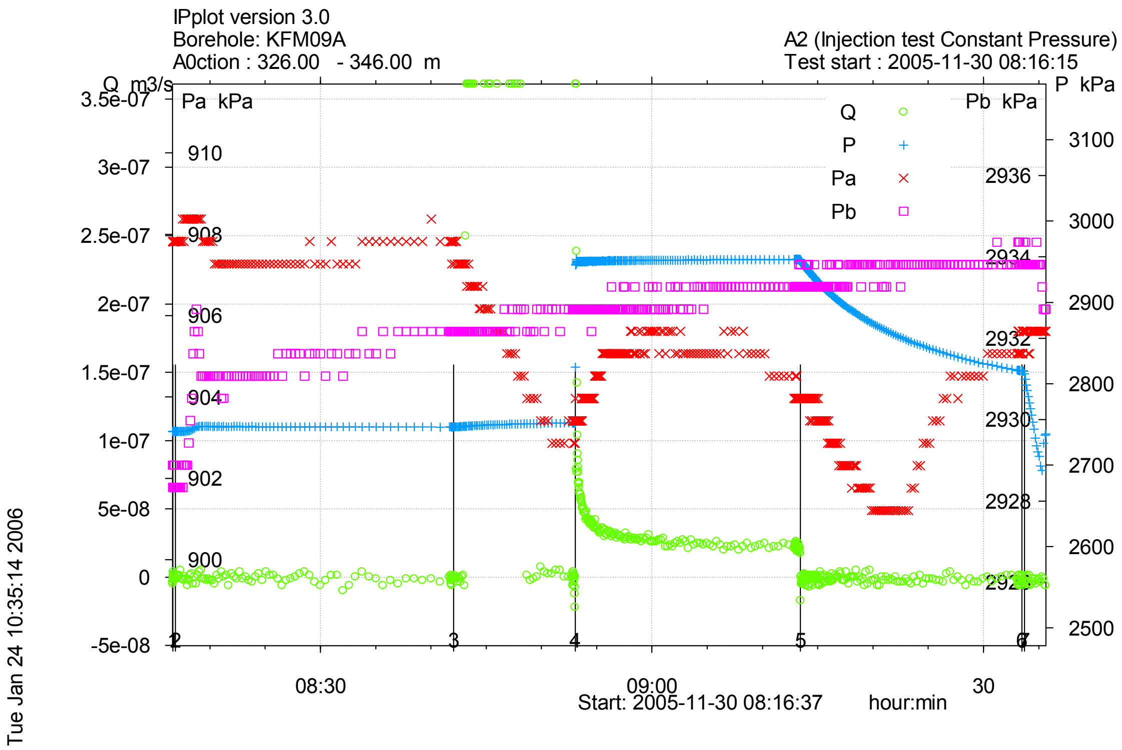


Figure A3-95. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 326.0-346.0 m in borehole KFM09A.*

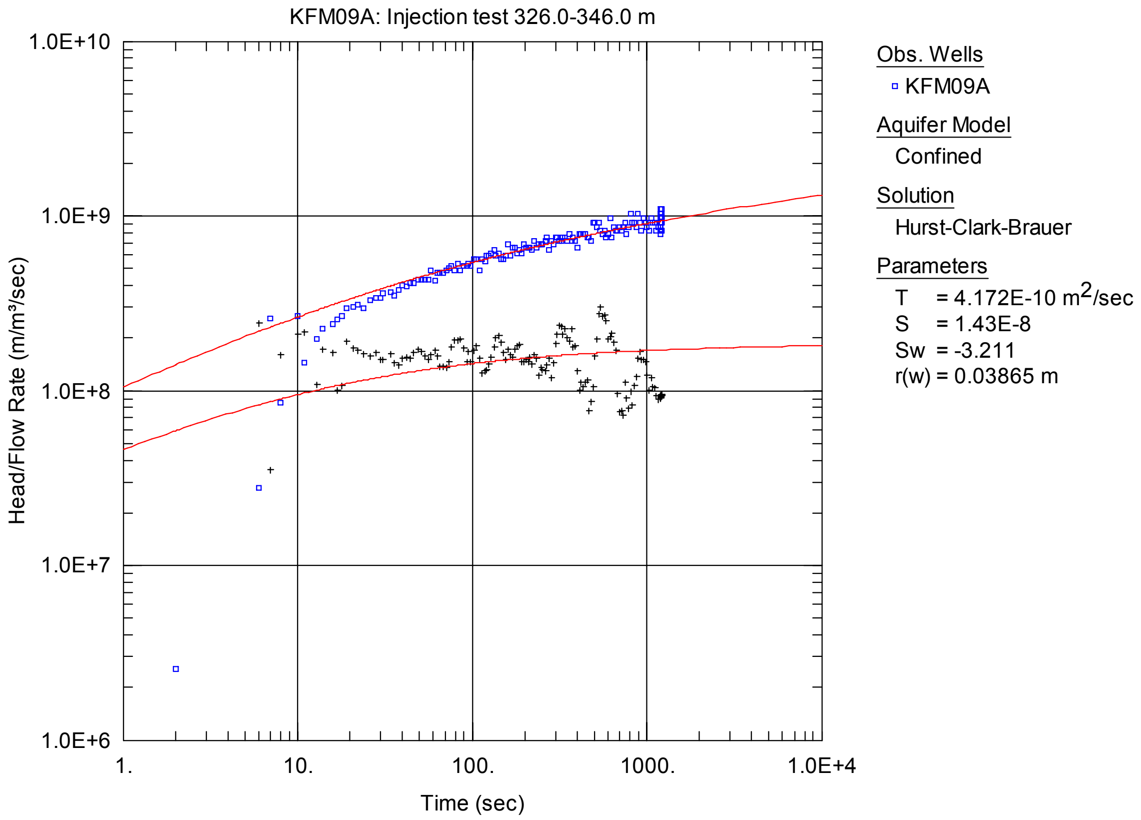


Figure A3-96. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in 326.0-346.0 m in KFM09A.*

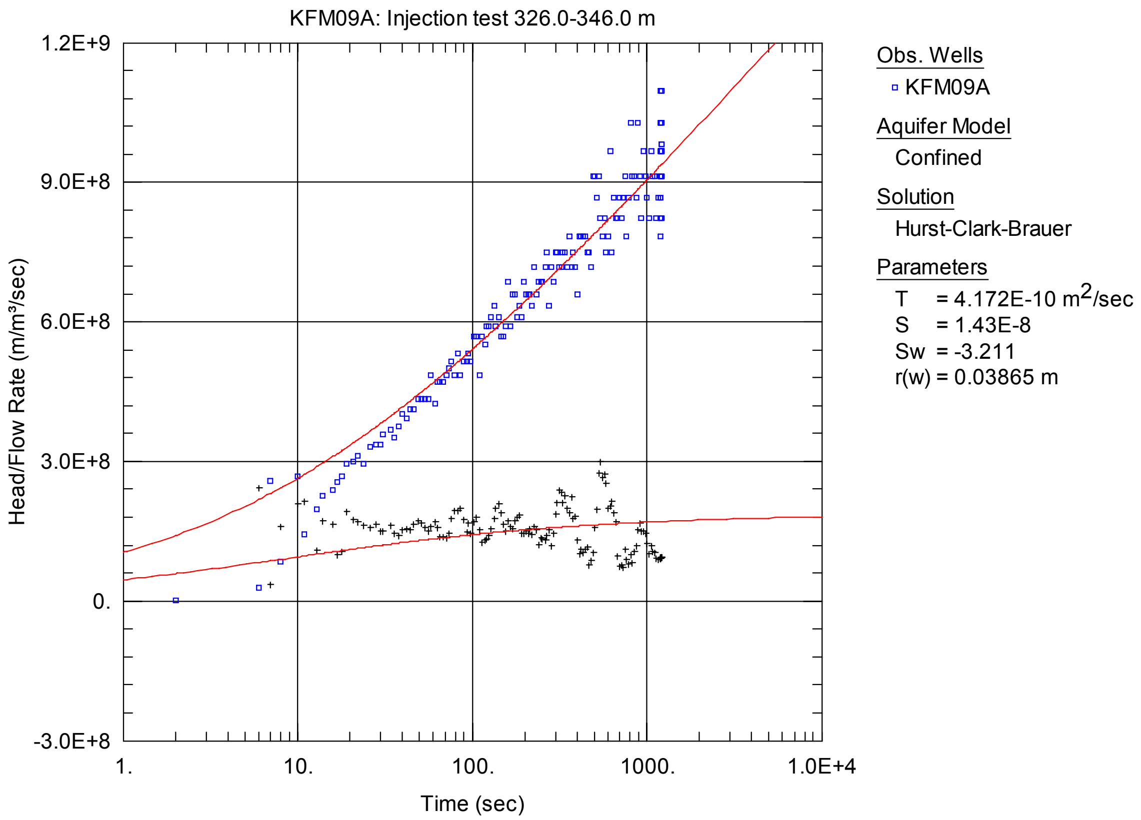


Figure A3-97. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 326.0-346.0 m in KFM09A.*

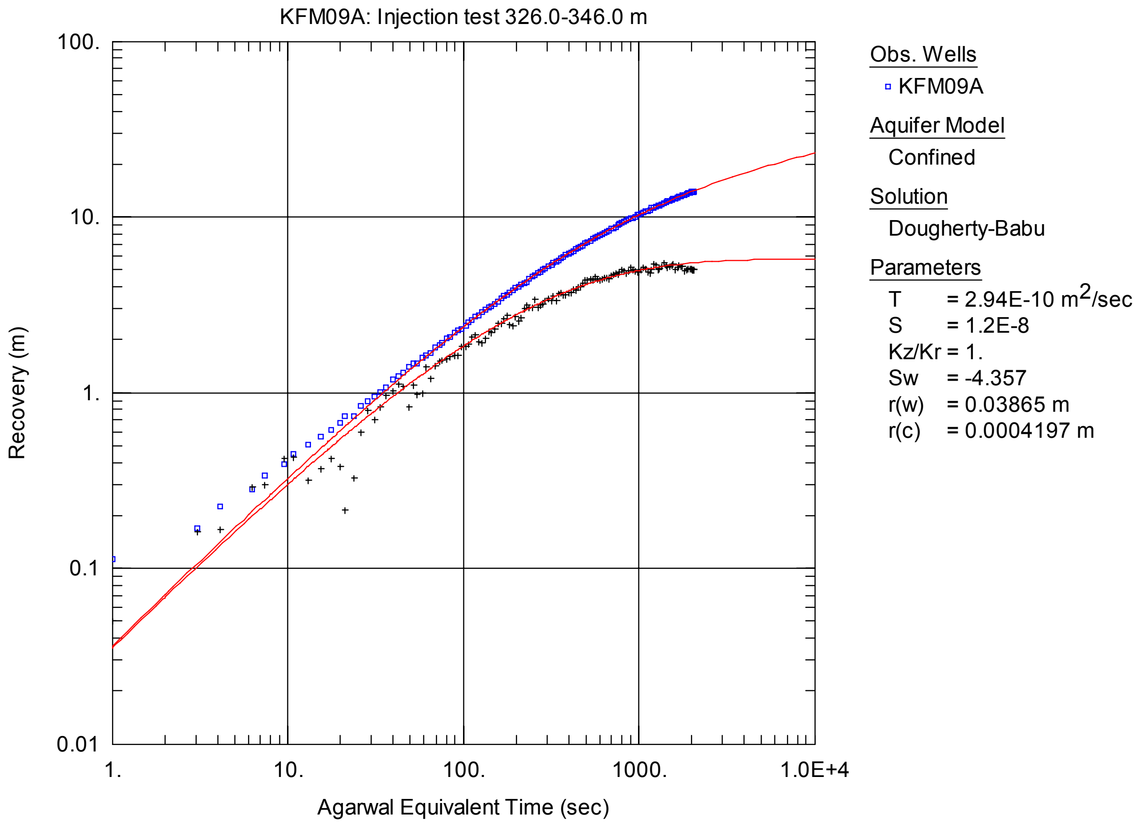


Figure A3-98. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 326.0-346.0 m in KFM09A.*

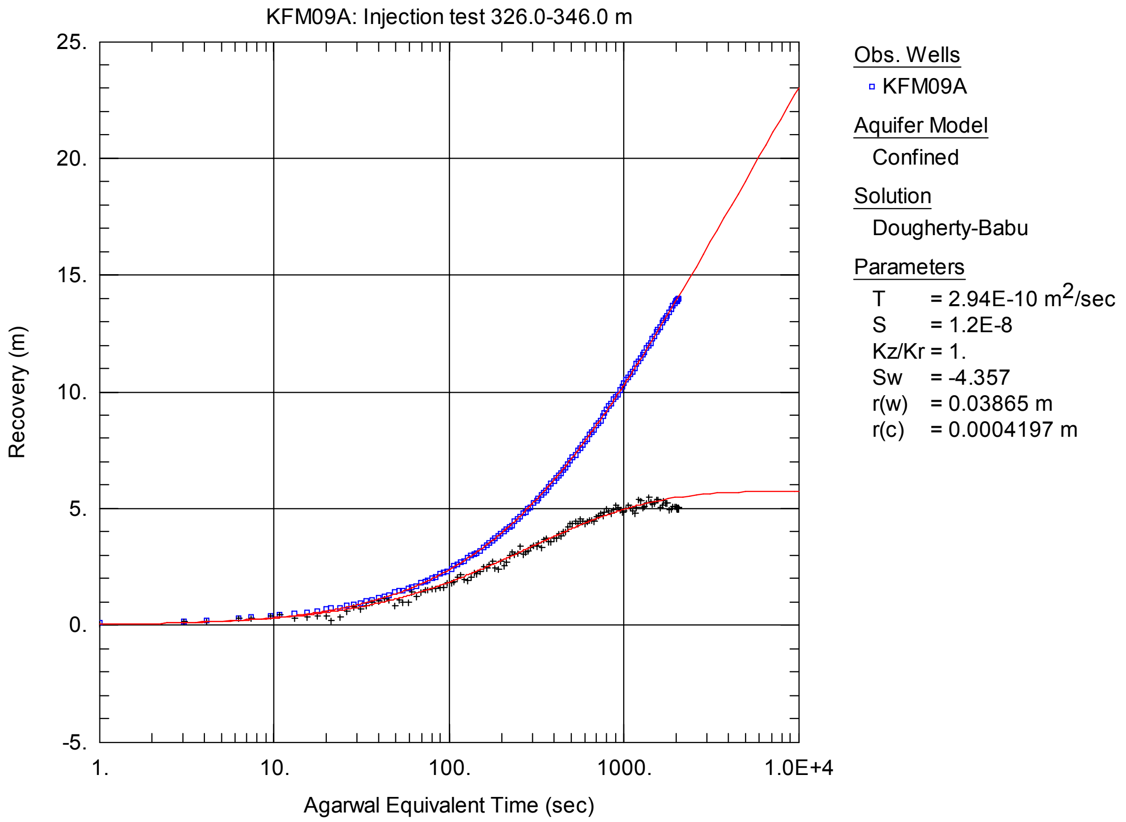


Figure A3-99. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 326.0-346.0 m in KFM09A.*

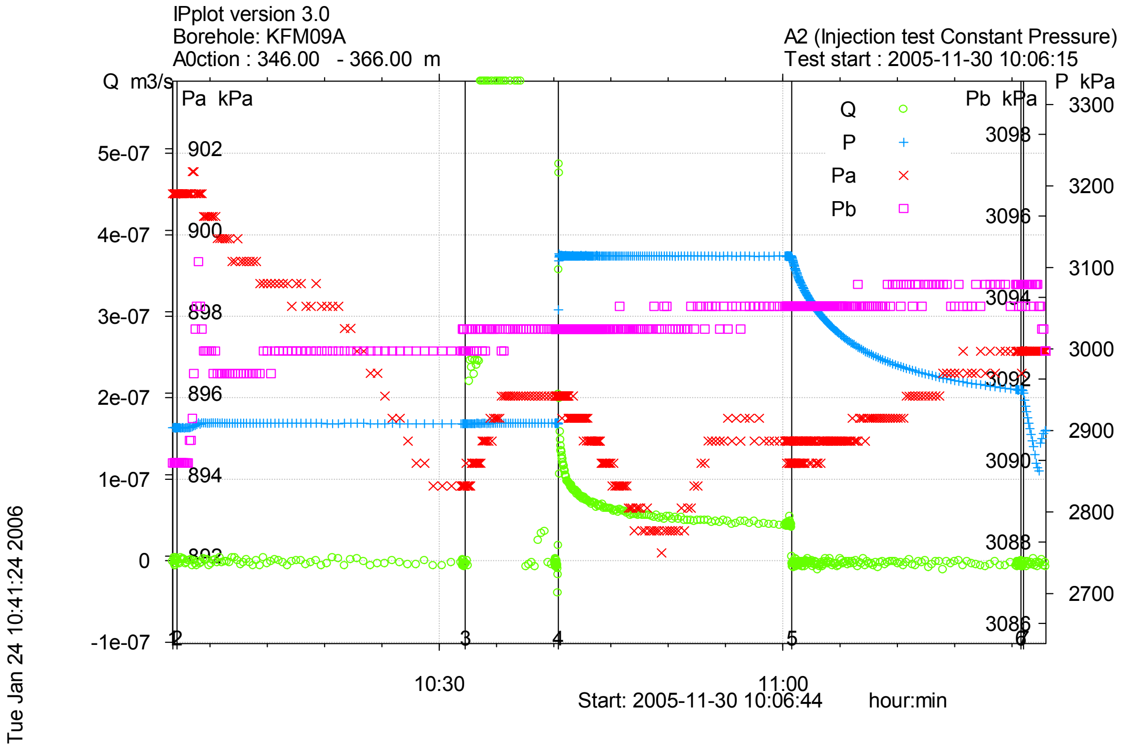


***Figure A3-100.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 346.0-366.0 m in borehole KFM09A.*

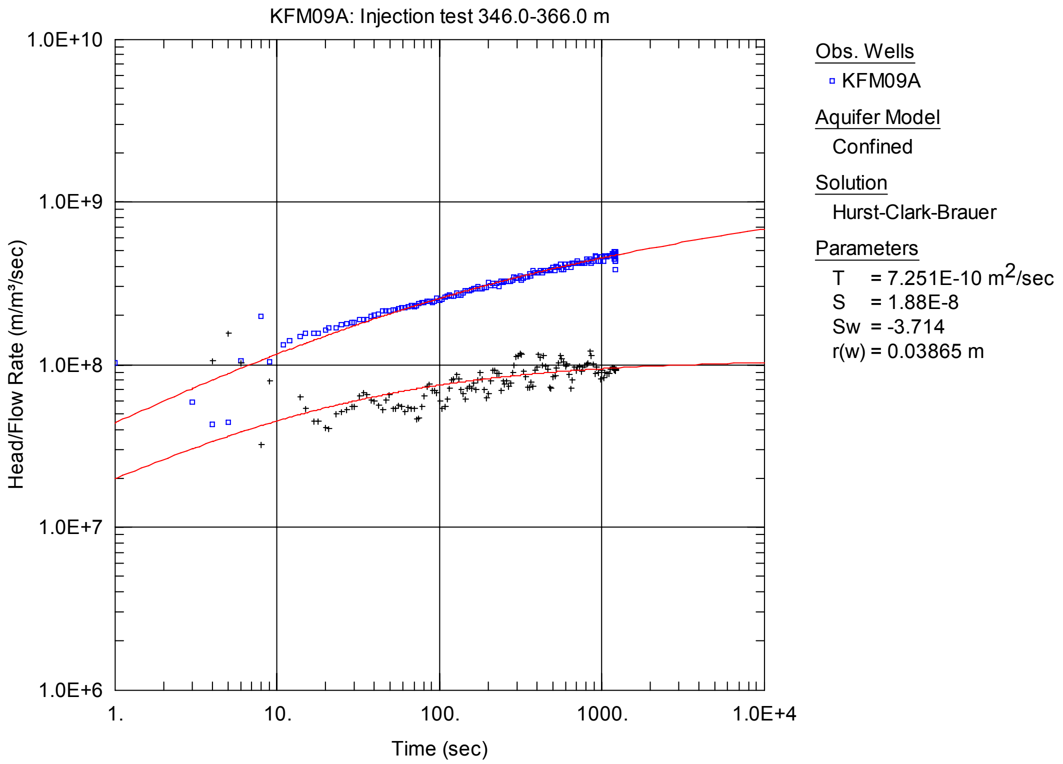


***Figure A3-101.** Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 346.0-366.0 m in KFM09A.*

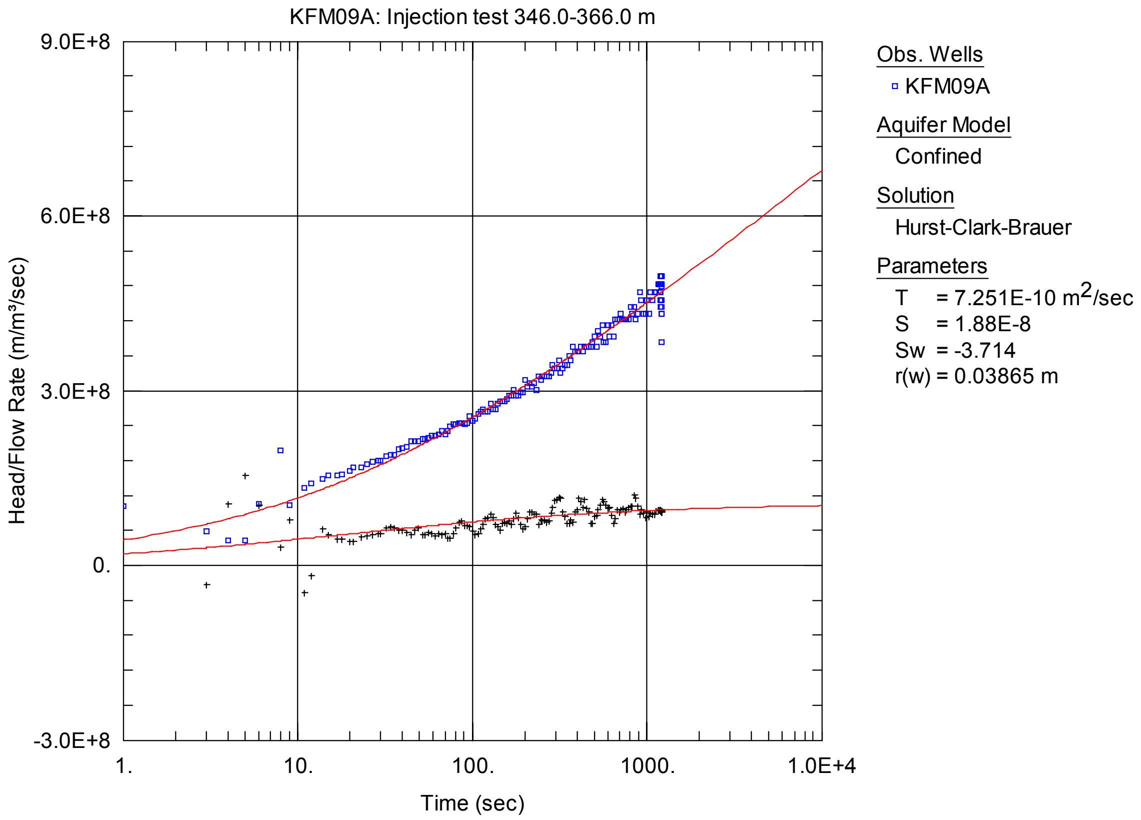


Figure A3-102. Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in 346.0-366.0 m in KFM09A.

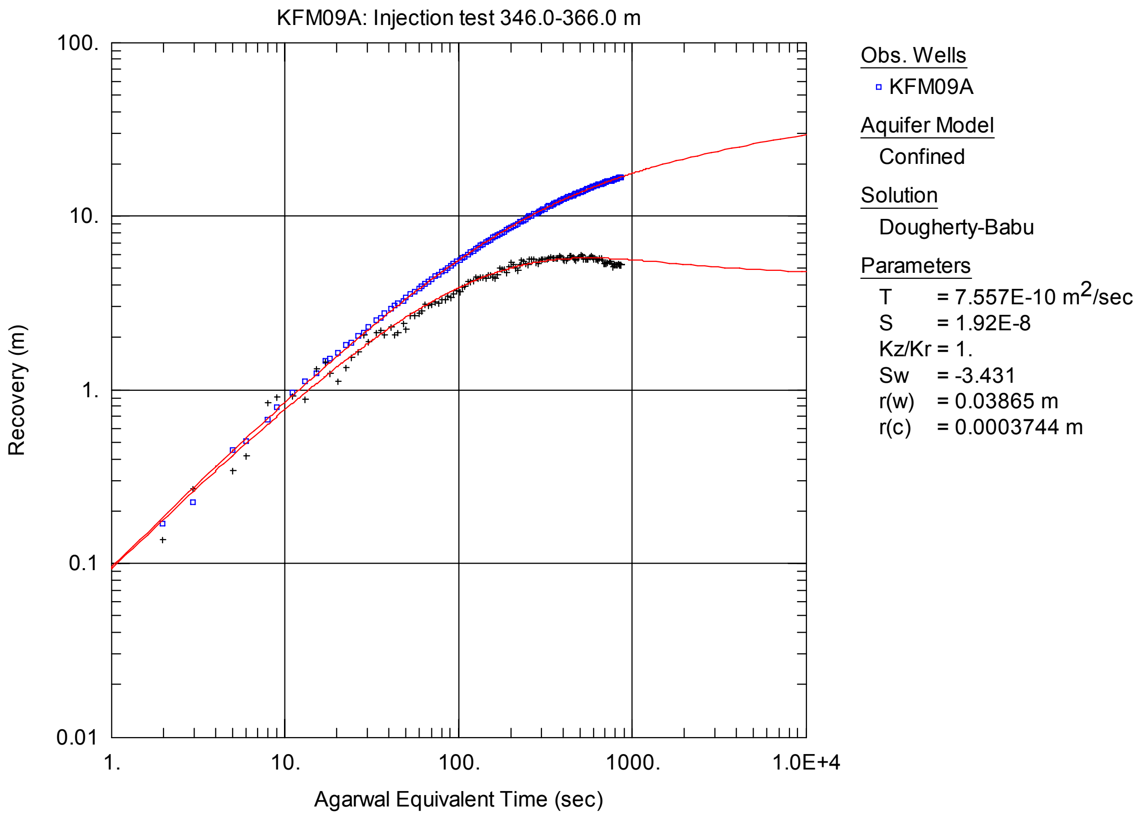


Figure A3-103. Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 346.0-366.0 m in KFM09A.

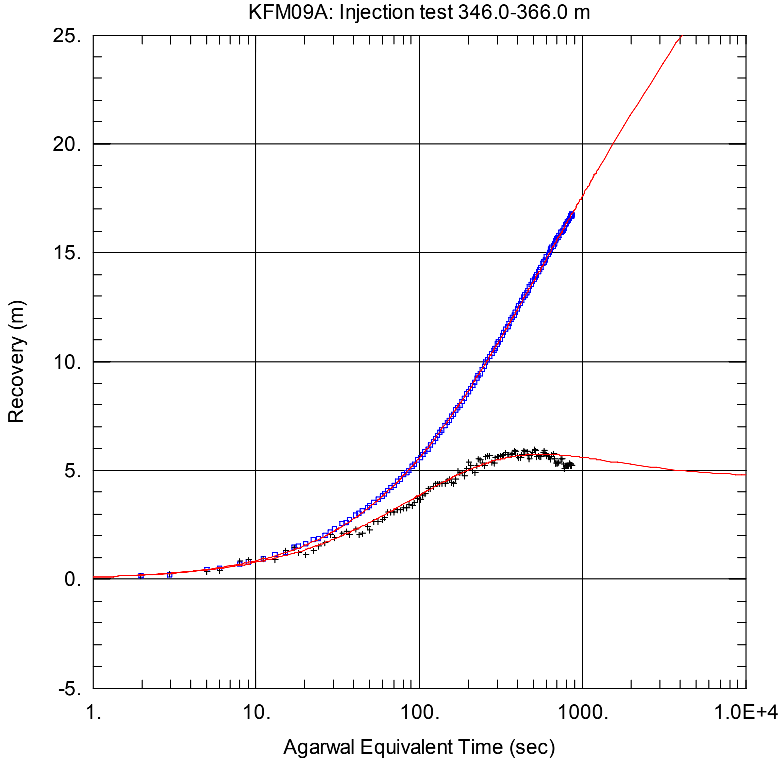


Figure A3-104. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 346.0-366.0 m in KFM09A.*

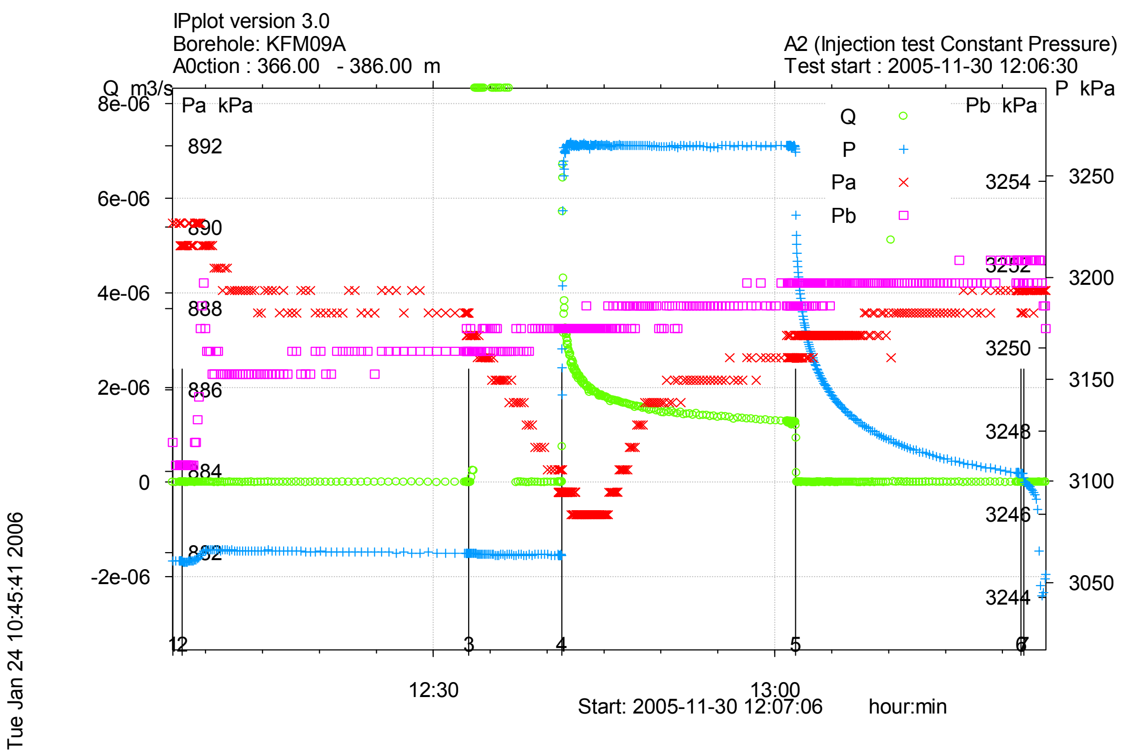


Figure A3-105. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 366.0-386.0 m in borehole KFM09A.*

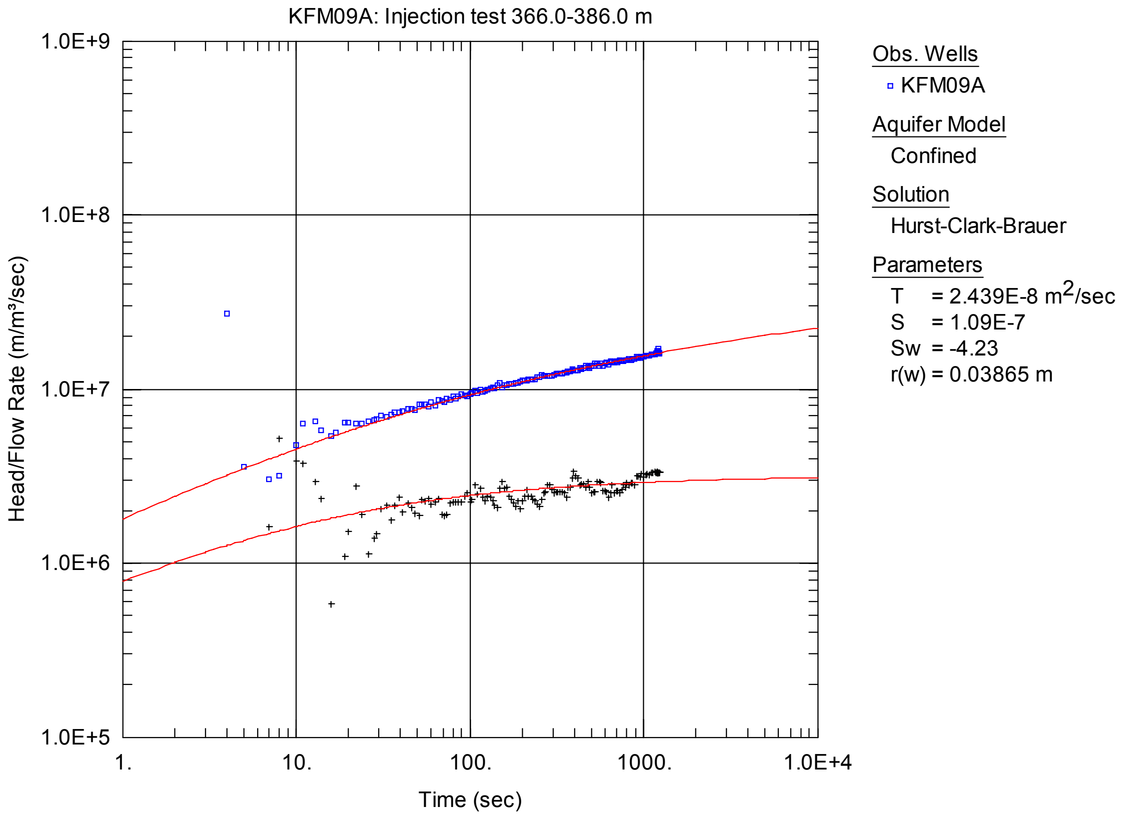


__Figure A3-106.__ Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 366.0-386.0 m in KFM09A.

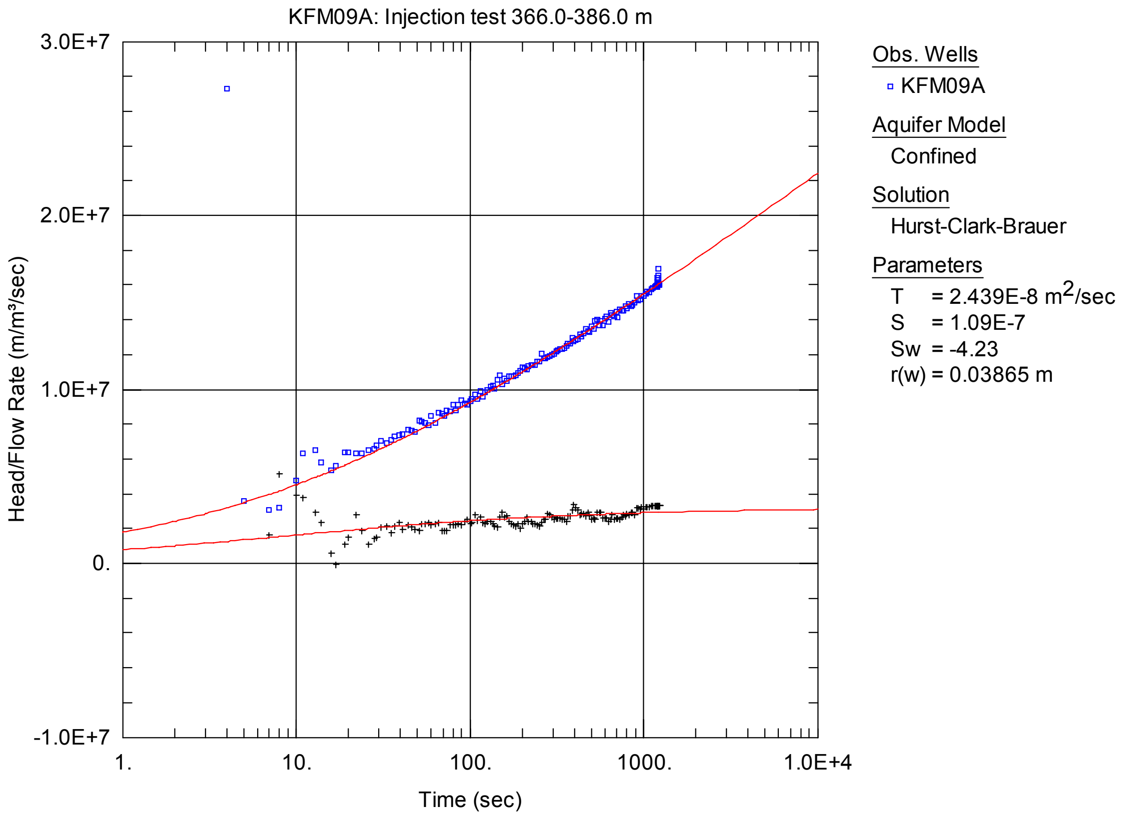


__Figure A3-107.__ Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 366.0-386.0 m in KFM09A.

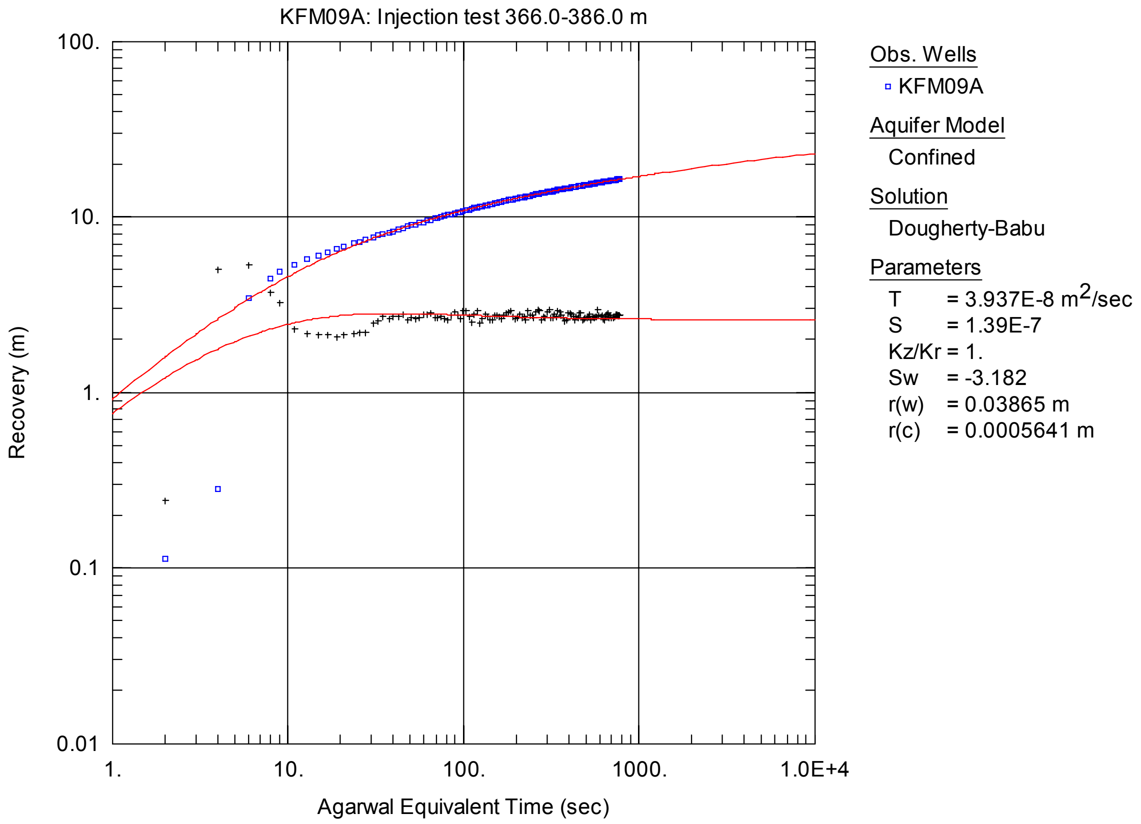


***Figure A3-108.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 366.0-386.0 m in KFM09A.*

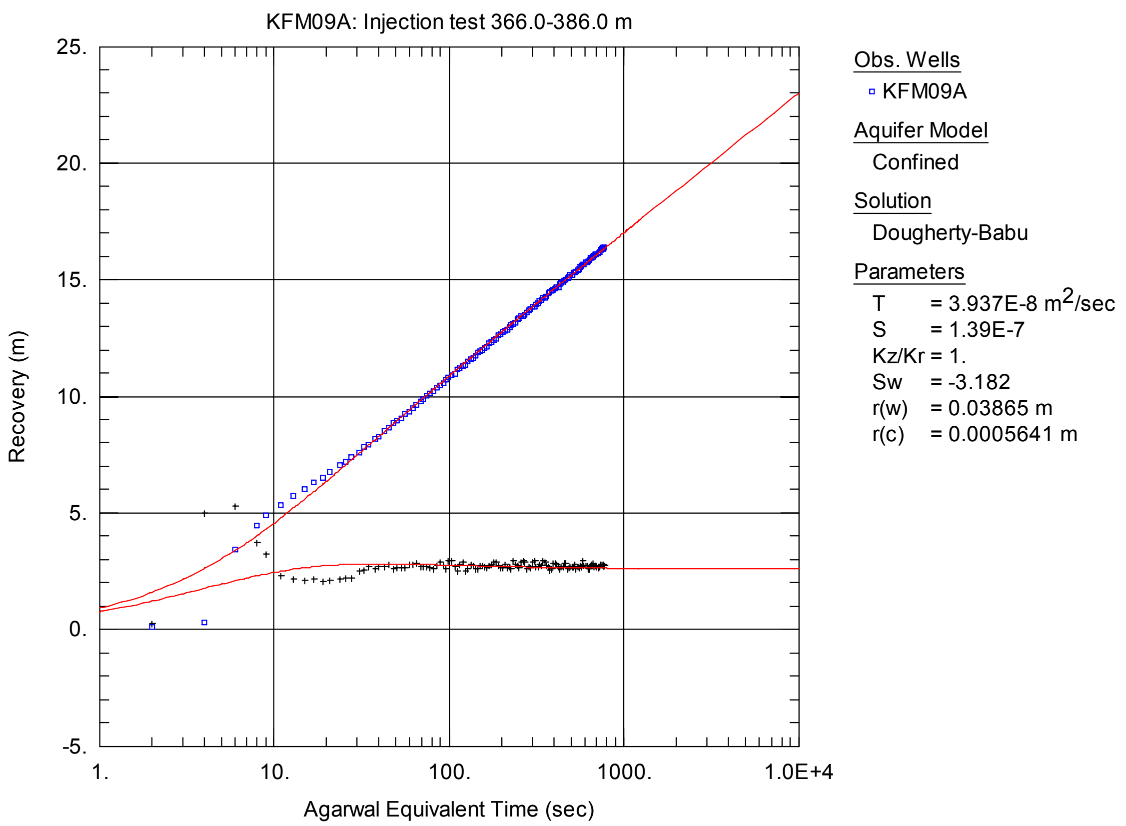


***Figure A3-109.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 366.0-386.0 m in KFM09A.*

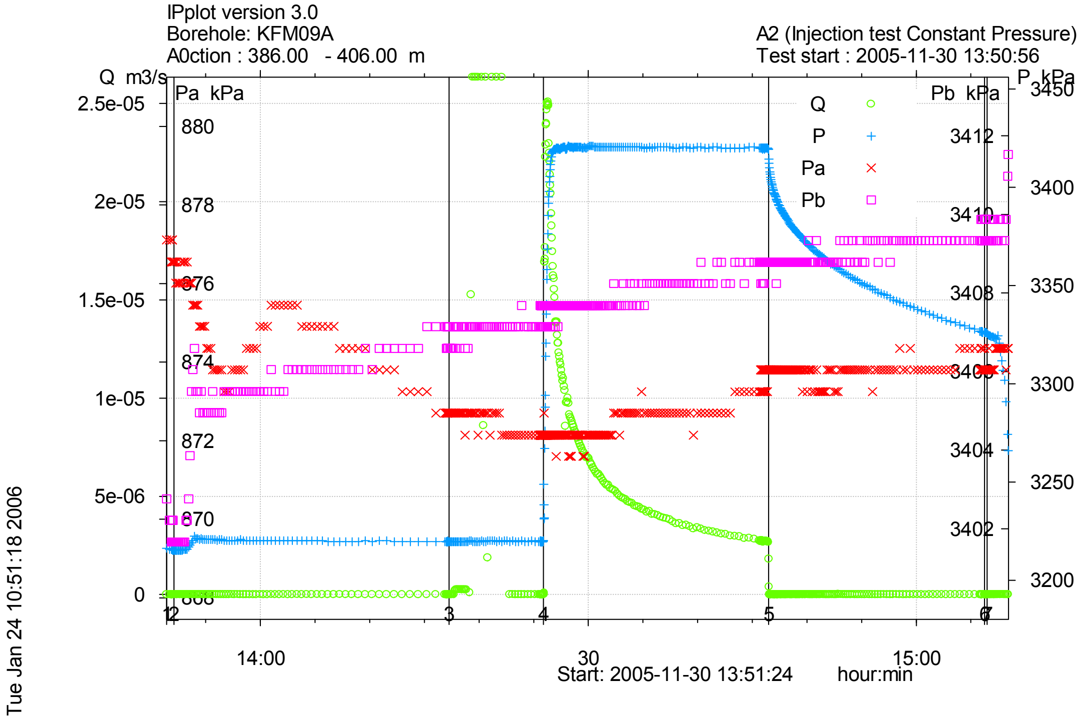


Figure A3-110. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 386.0-406.0 m in borehole KFM09A.

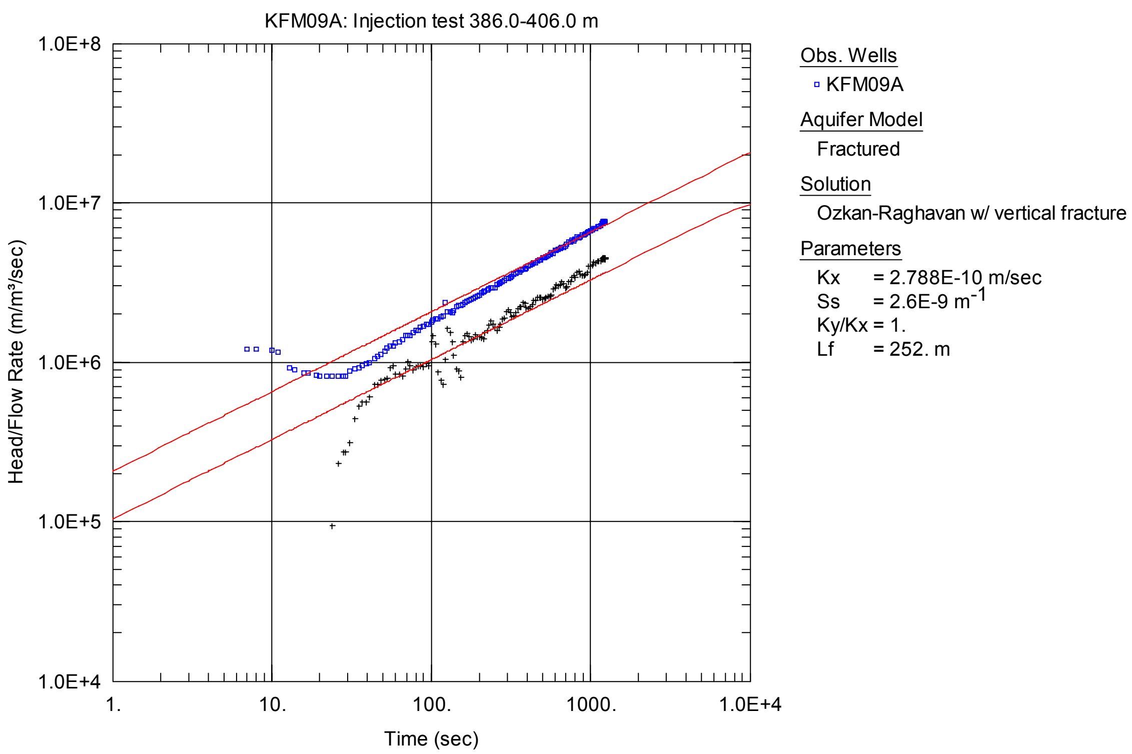


Figure A3-111. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 386.0-406.0 m in KFM09A. No transient evaluation is possible on the injection period.

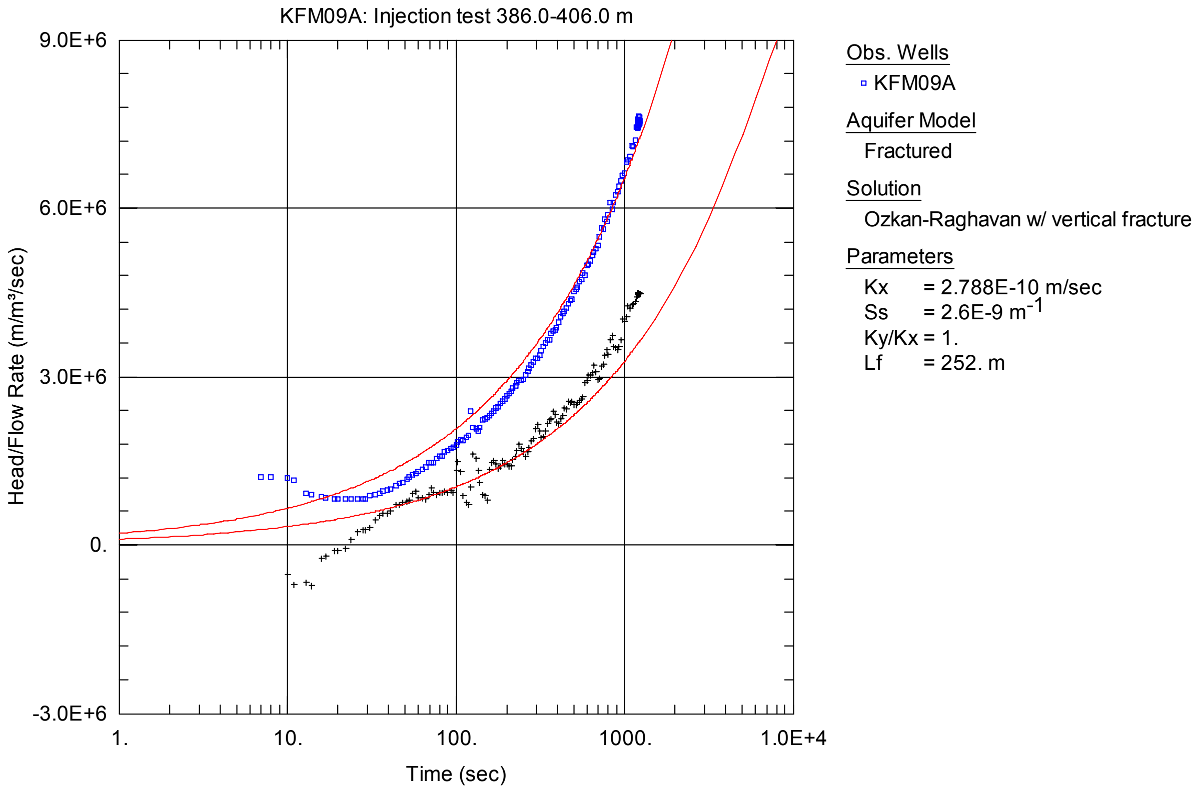


__Figure A3-112.__ Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 386.0-406.0 m in KFM09A. No transient evaluation is possible on the injection period.

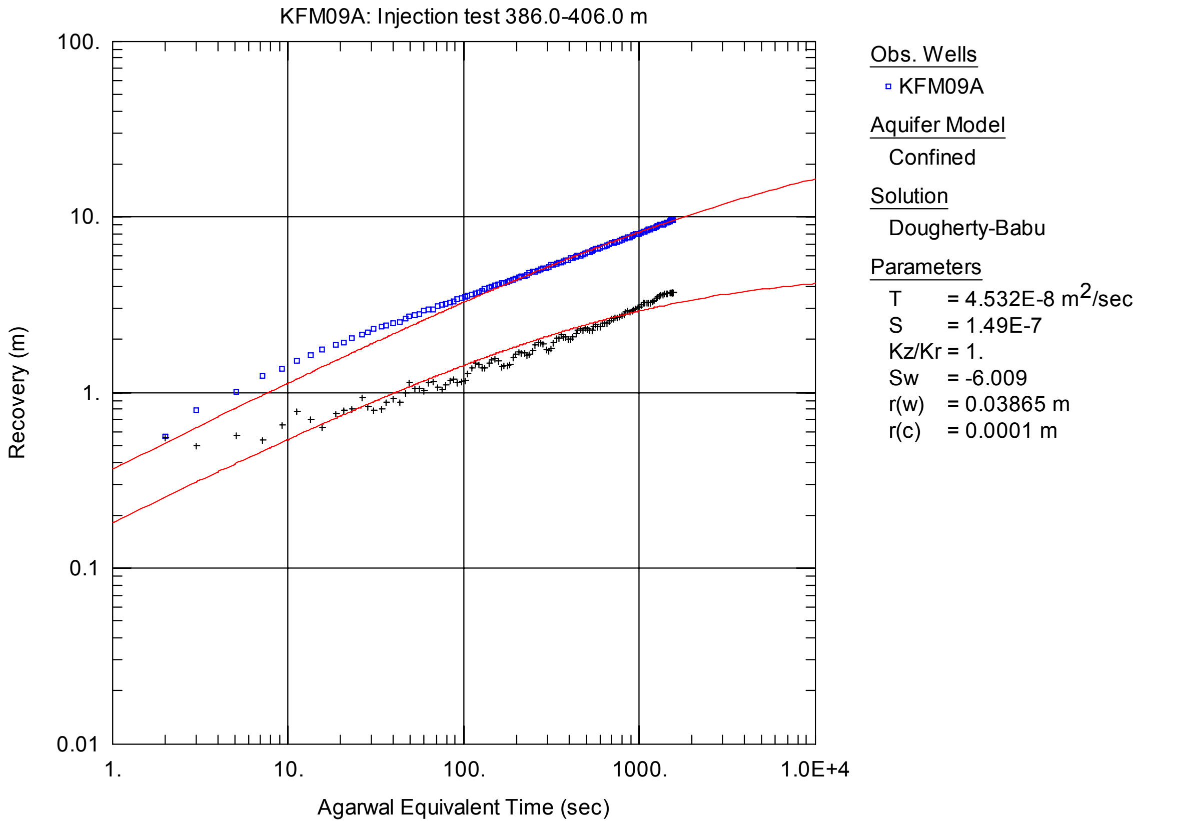


__Figure A3-113.__ Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 386.0-406.0 m in KFM09A.

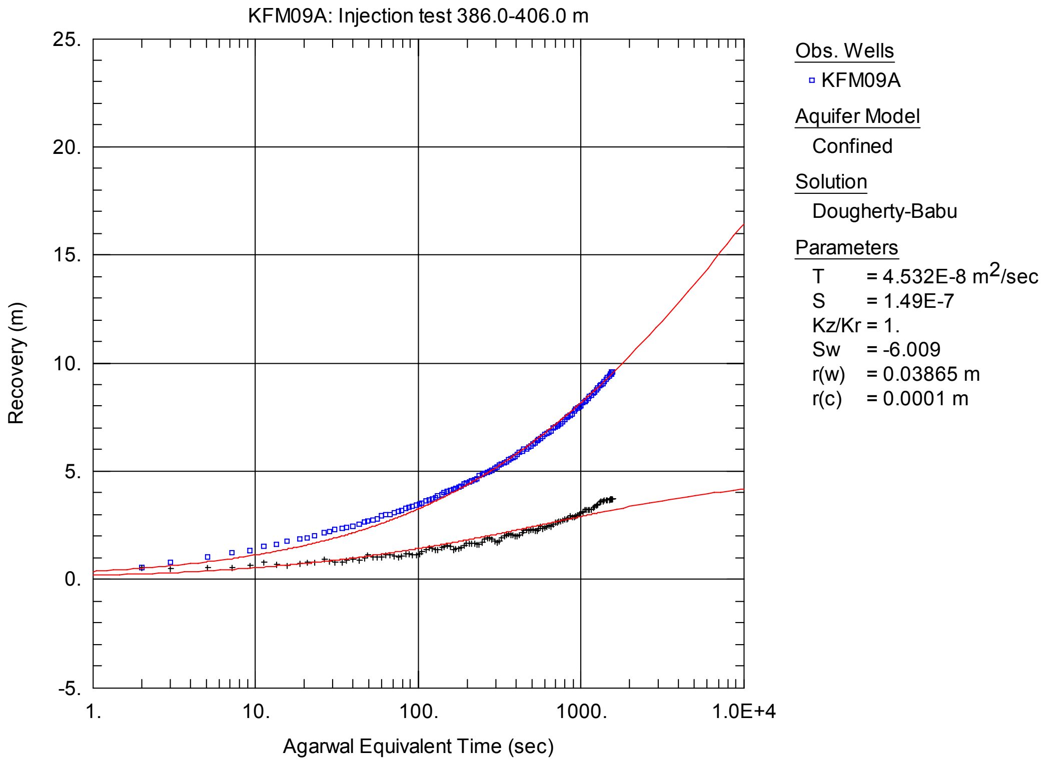


Figure A3-114. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in 386.0-406.0 m in KFM09A.*

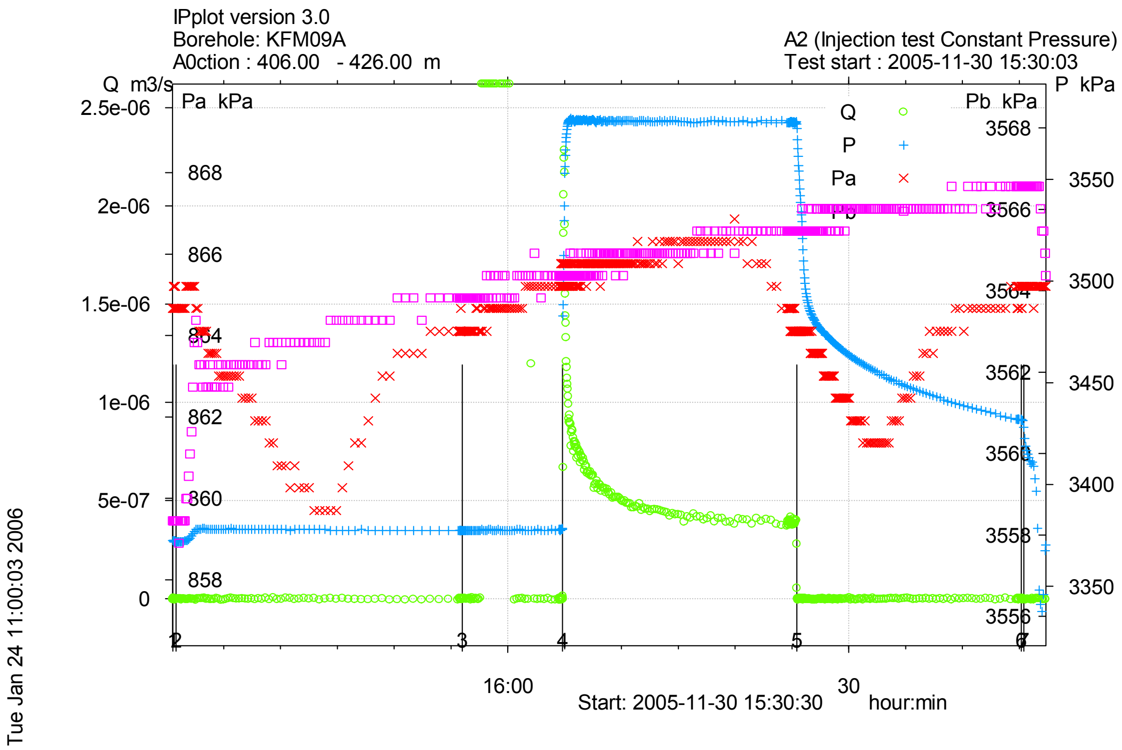


Figure A3-115. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 406.0-426.0 m in borehole KFM09A.*

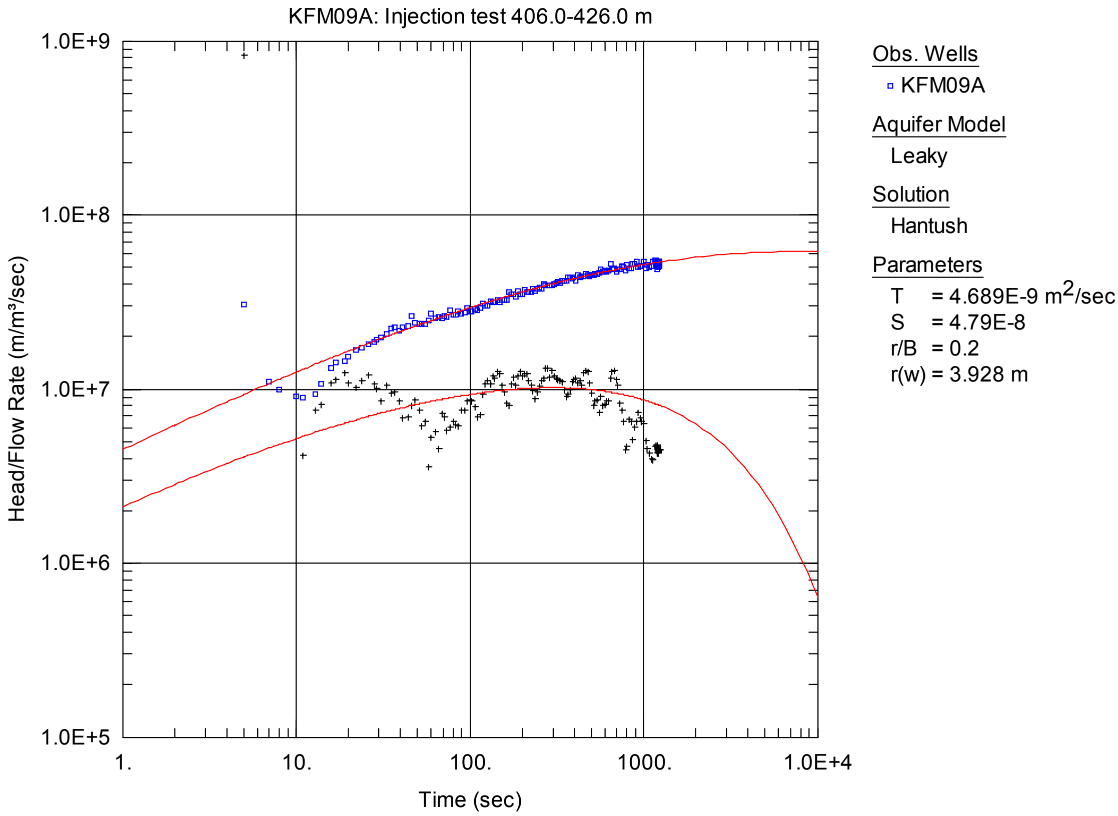


Figure A3-116. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 406.0-426.0 m in KFM09A.*

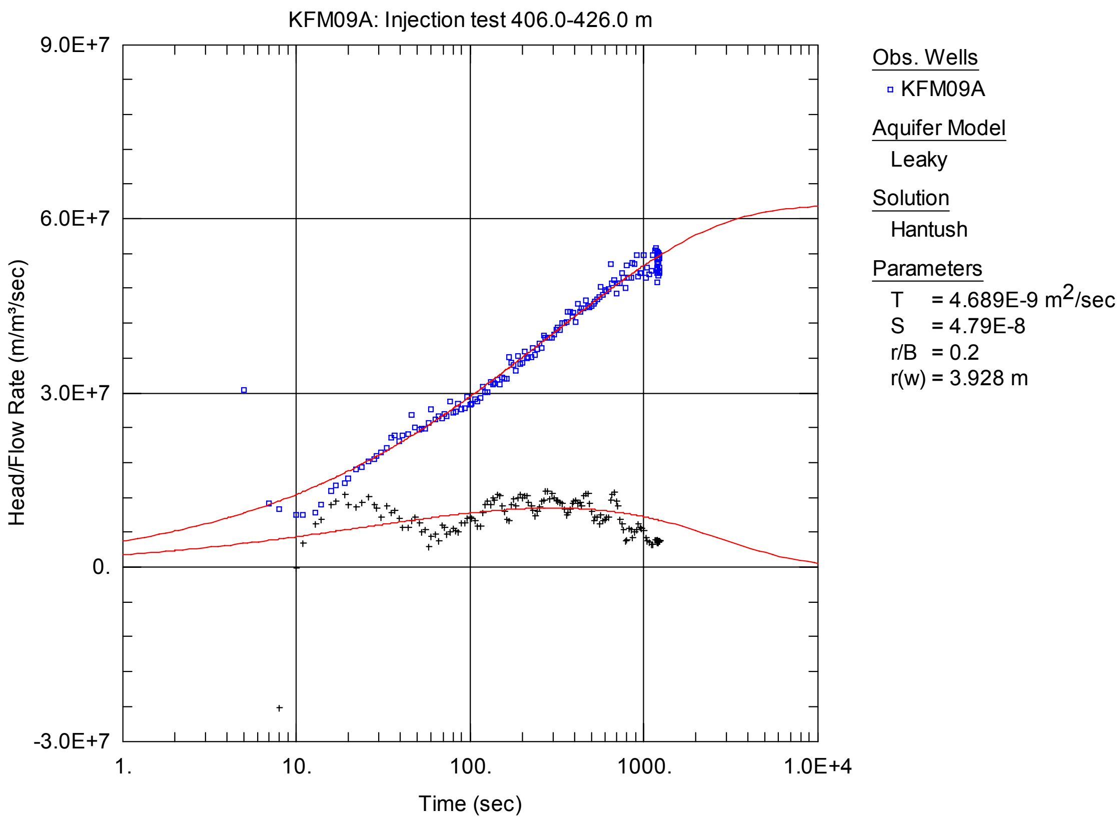


Figure A3-117. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 406.0-426.0 m in KFM09A.*

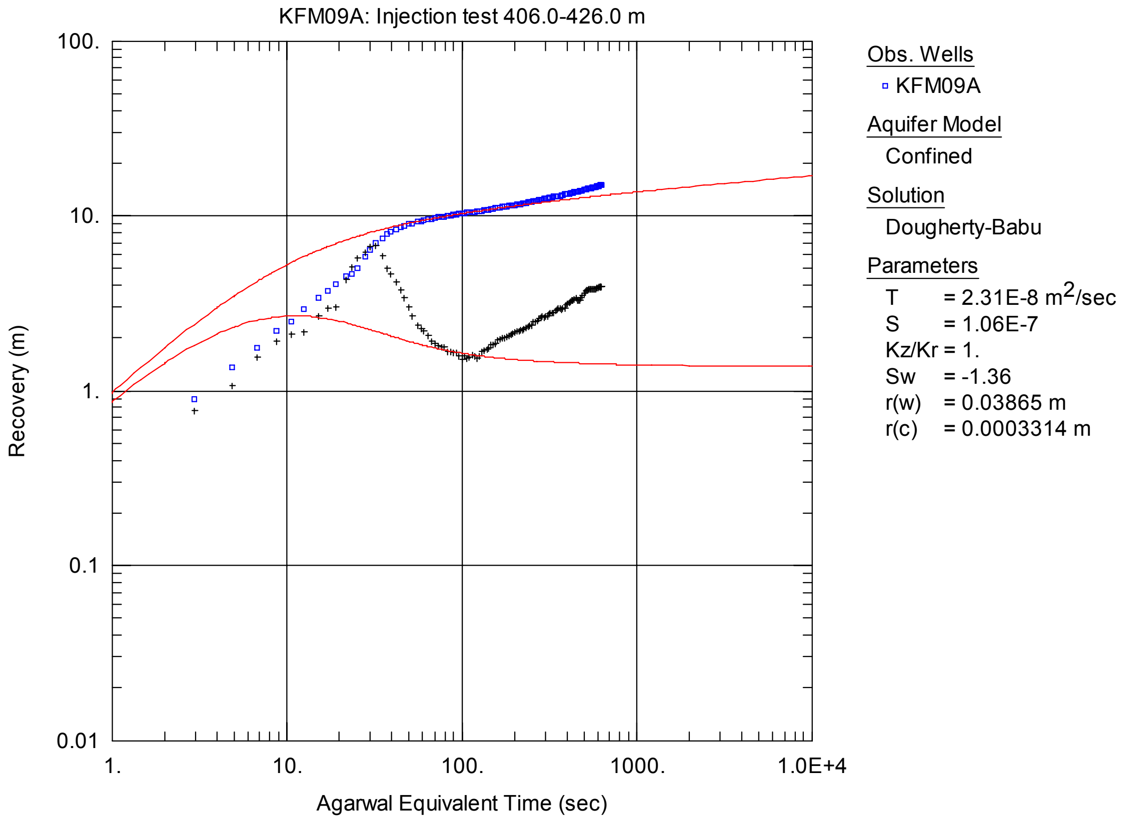


Figure A3-118. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 406.0-426.0 m in KFM09A.*

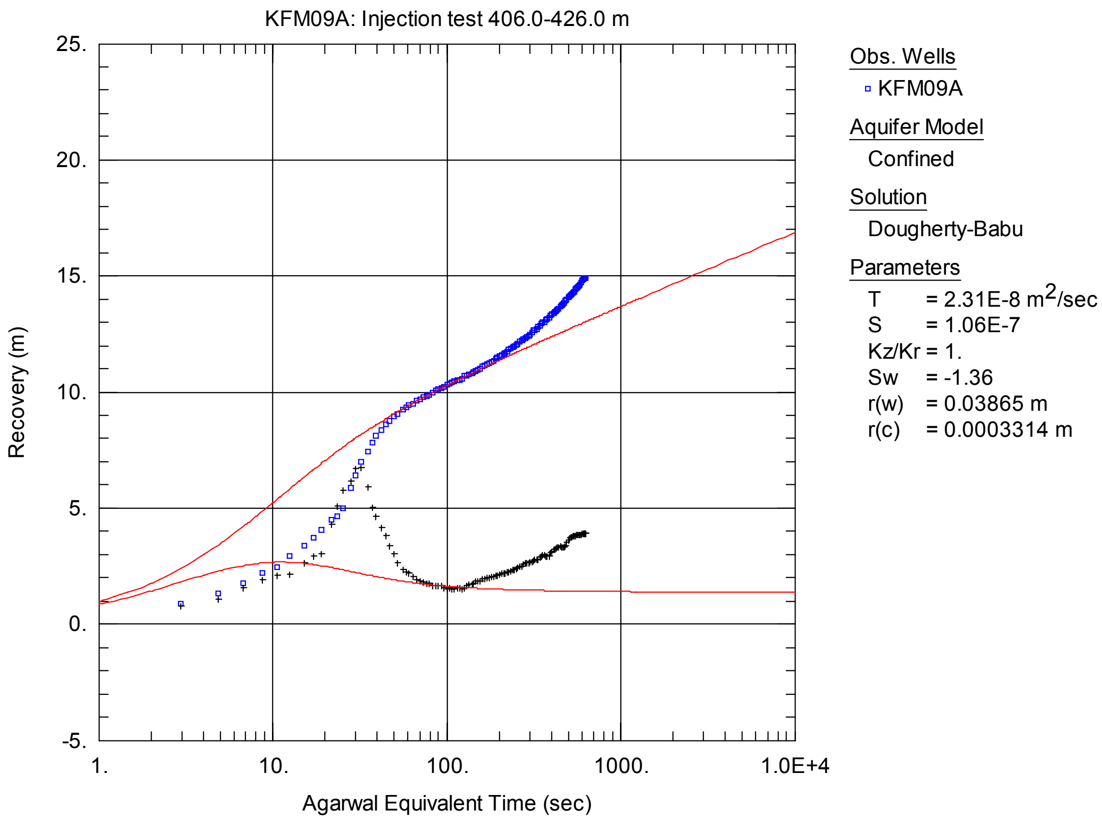


Figure A3-119. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 406.0-426.0 m in KFM09A.*

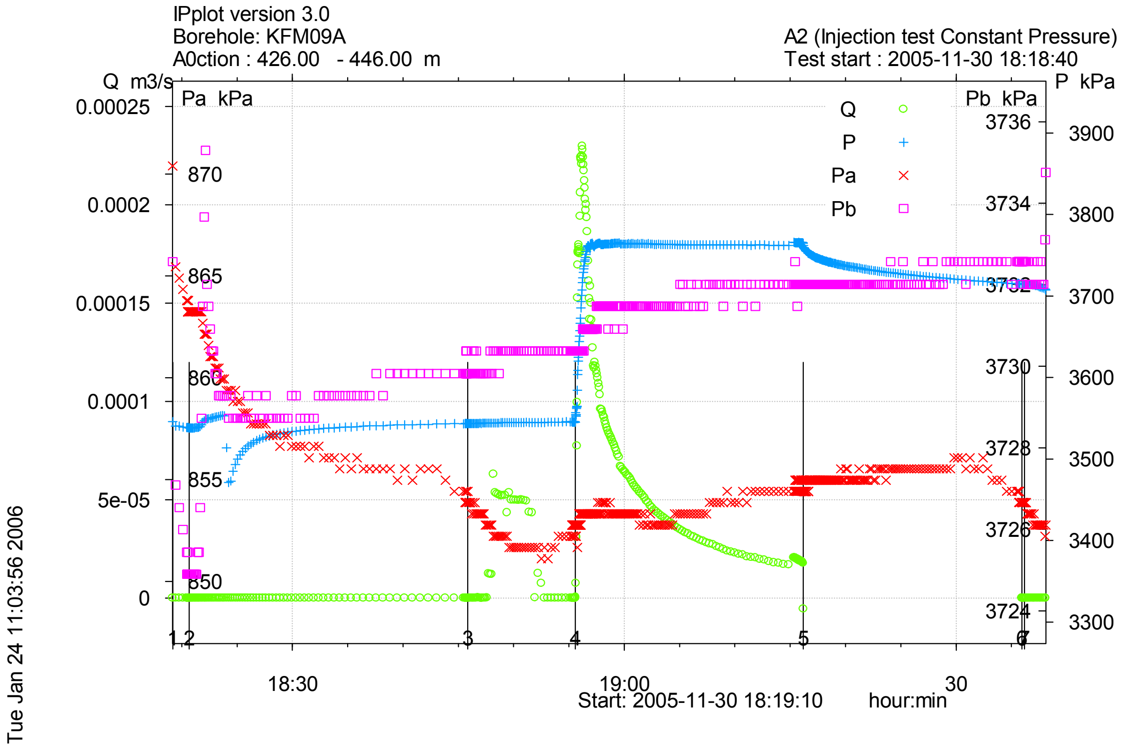


__Figure A3-120.__ Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in 426.0-446.0 m in borehole KFM09A.

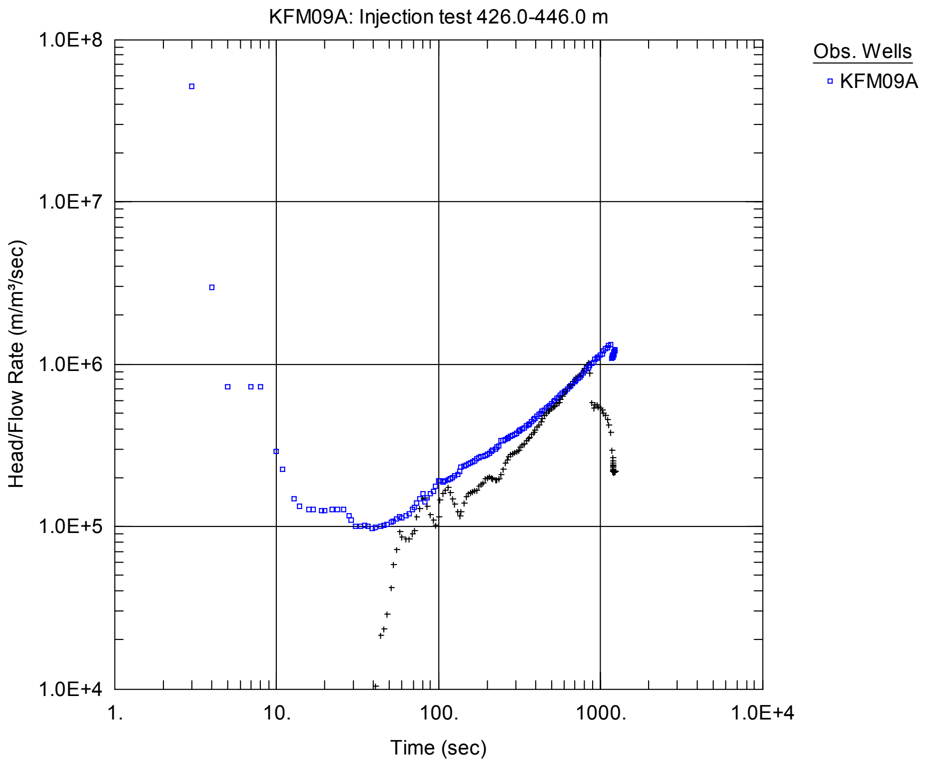


__Figure A3-121.__ Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 426.0-446.0 m in KFM09A.

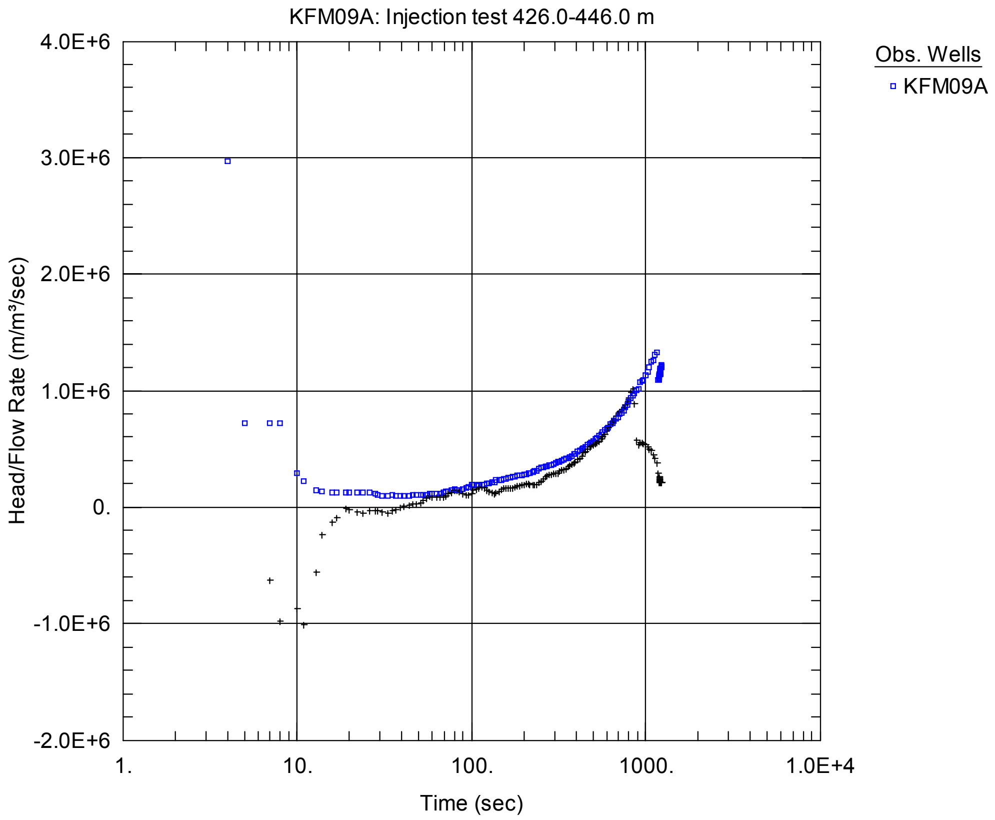


Figure A3-122. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 426.0-446.0 m in KFM09A.*

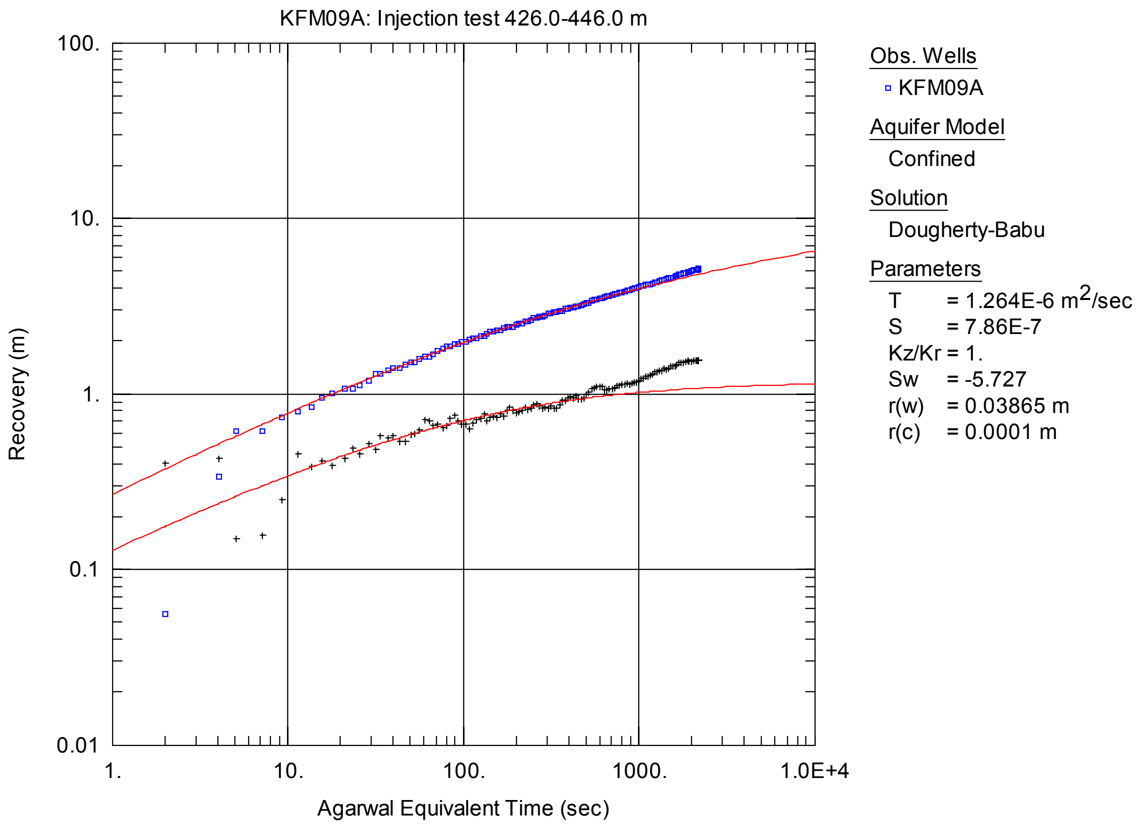


Figure A3-123. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 426.0-446.0 m in KFM09A.*

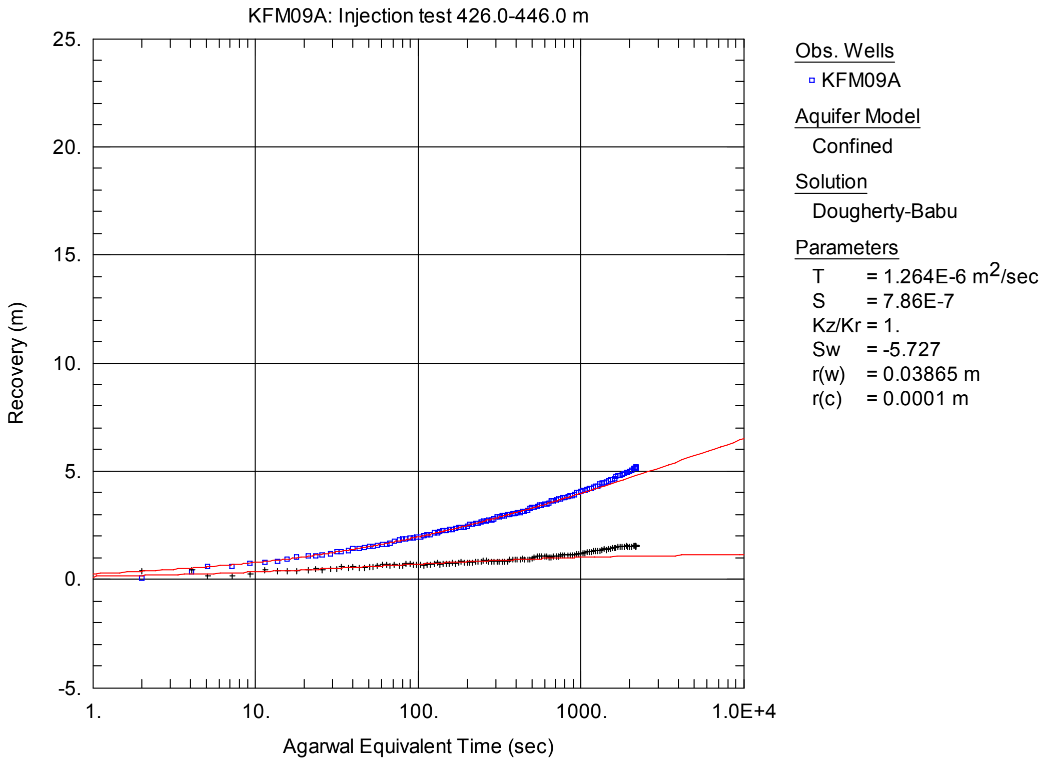


Figure A3-124. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 426.0-446.0 m in KFM09A.*

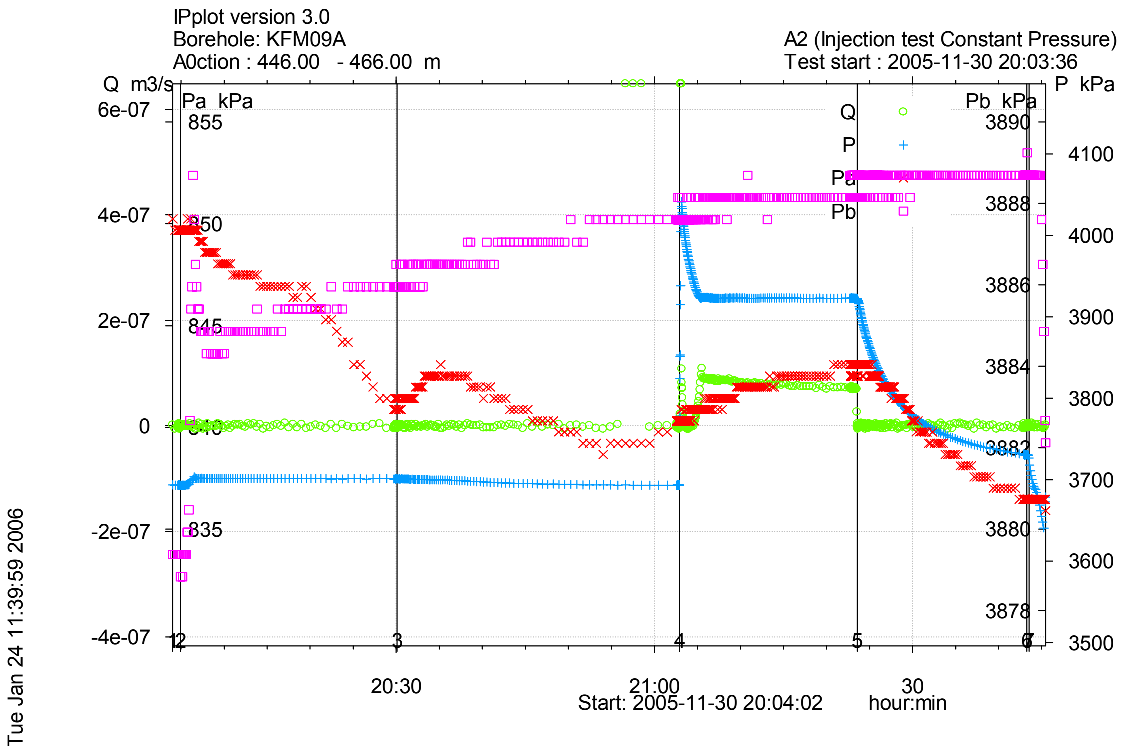


Figure A3-125. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 446.0-466.0 m in borehole KFM09A.*

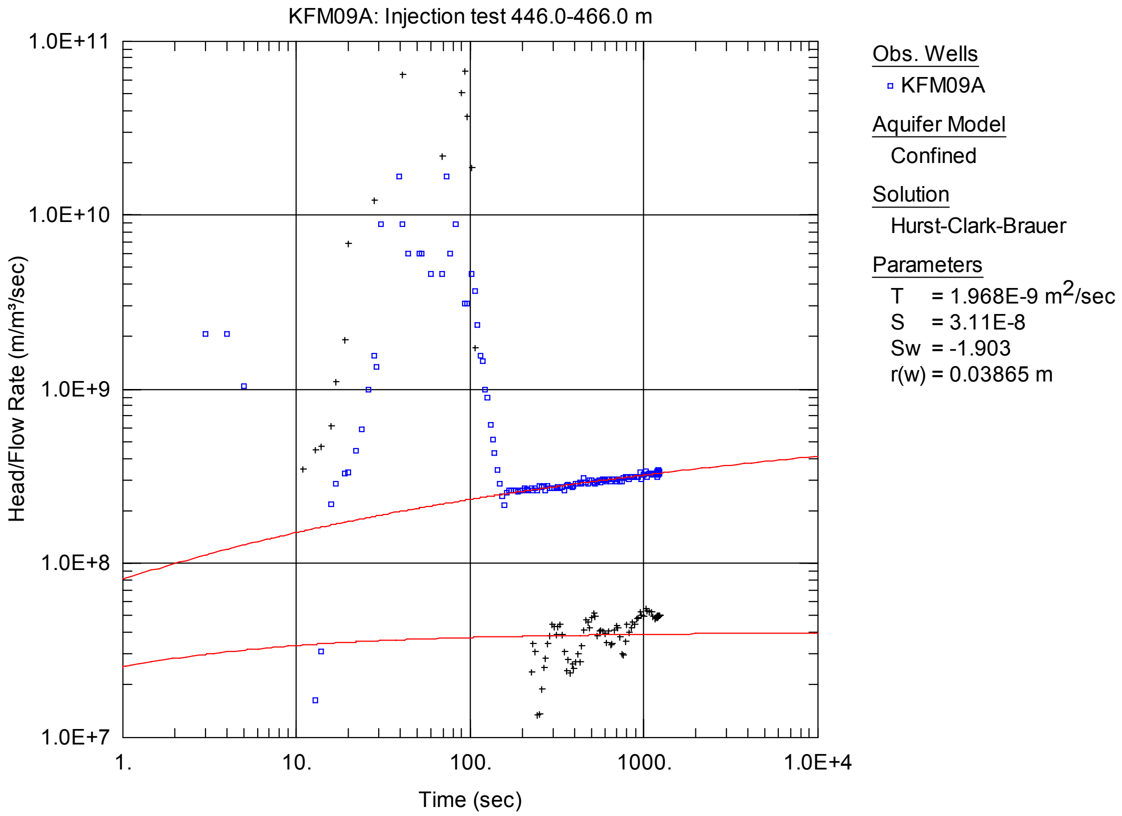


Figure A3-126. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 446.0-466.0 m in KFM09A.*

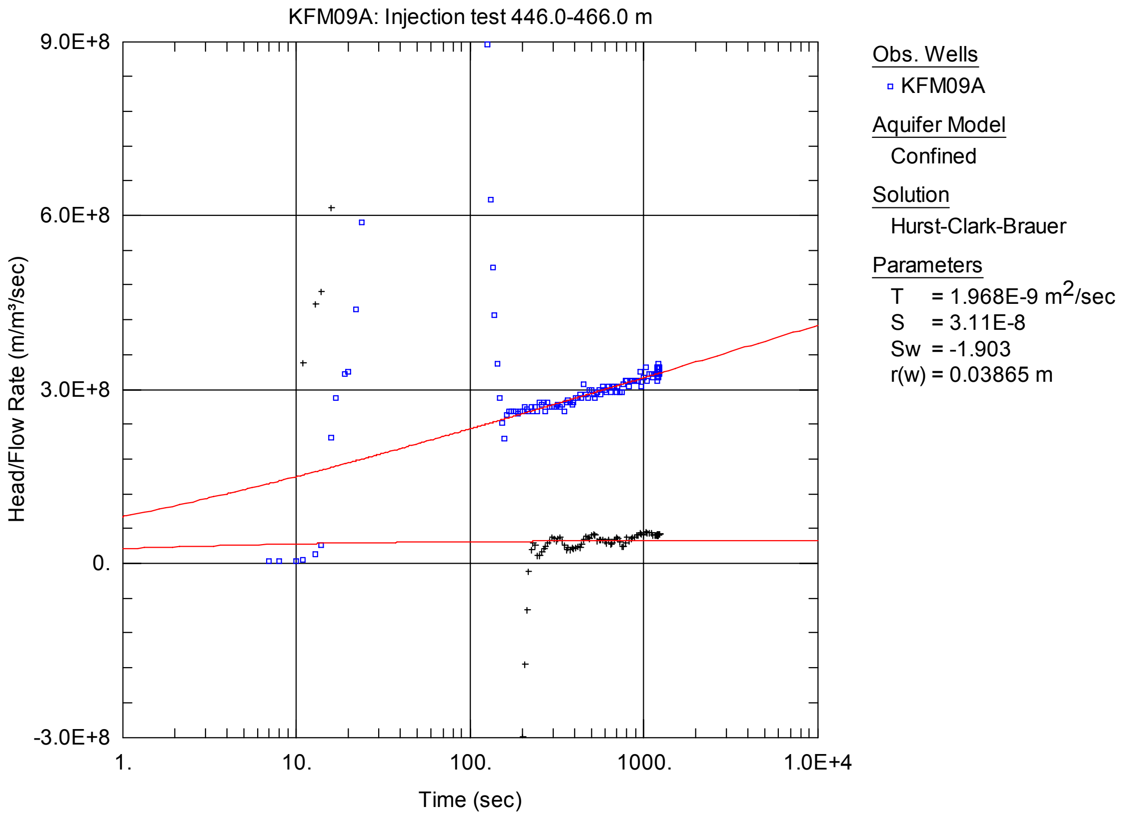


Figure A3-127. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 446.0-466.0 m in KFM09A.*

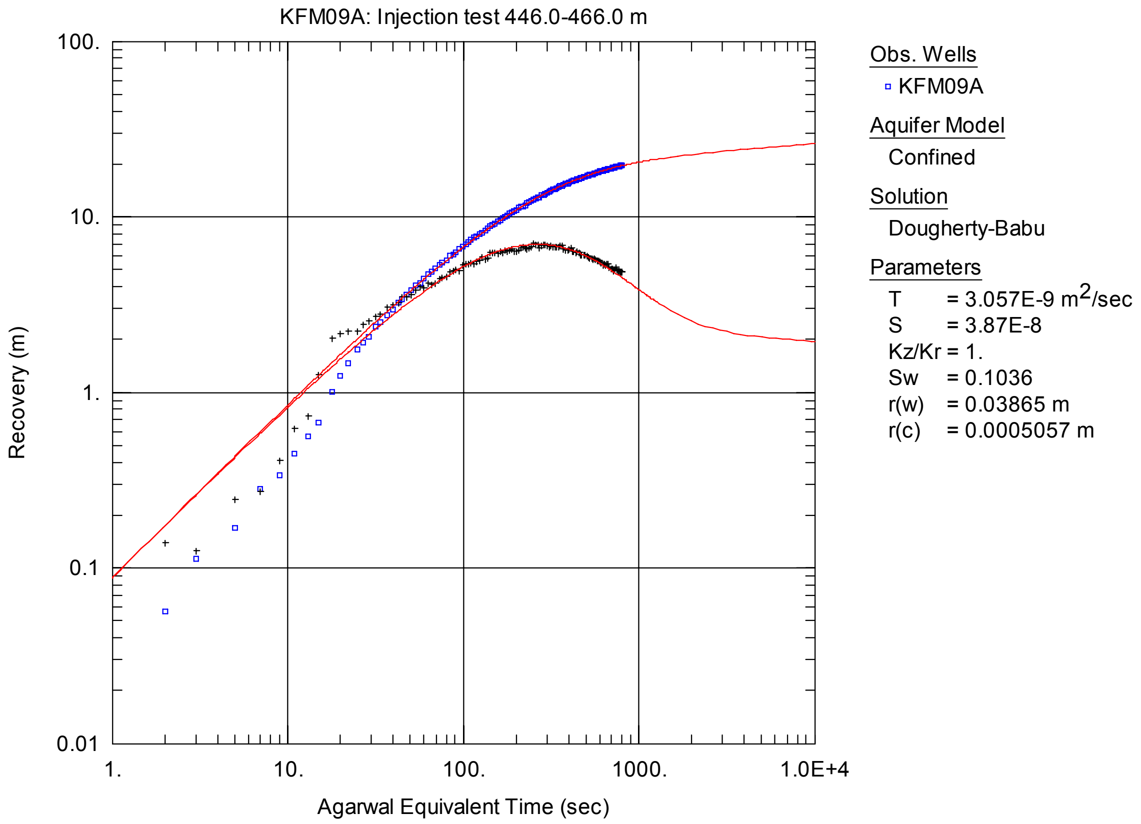


Figure A3-128. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in 446.0-466.0 m in KFM09A.*

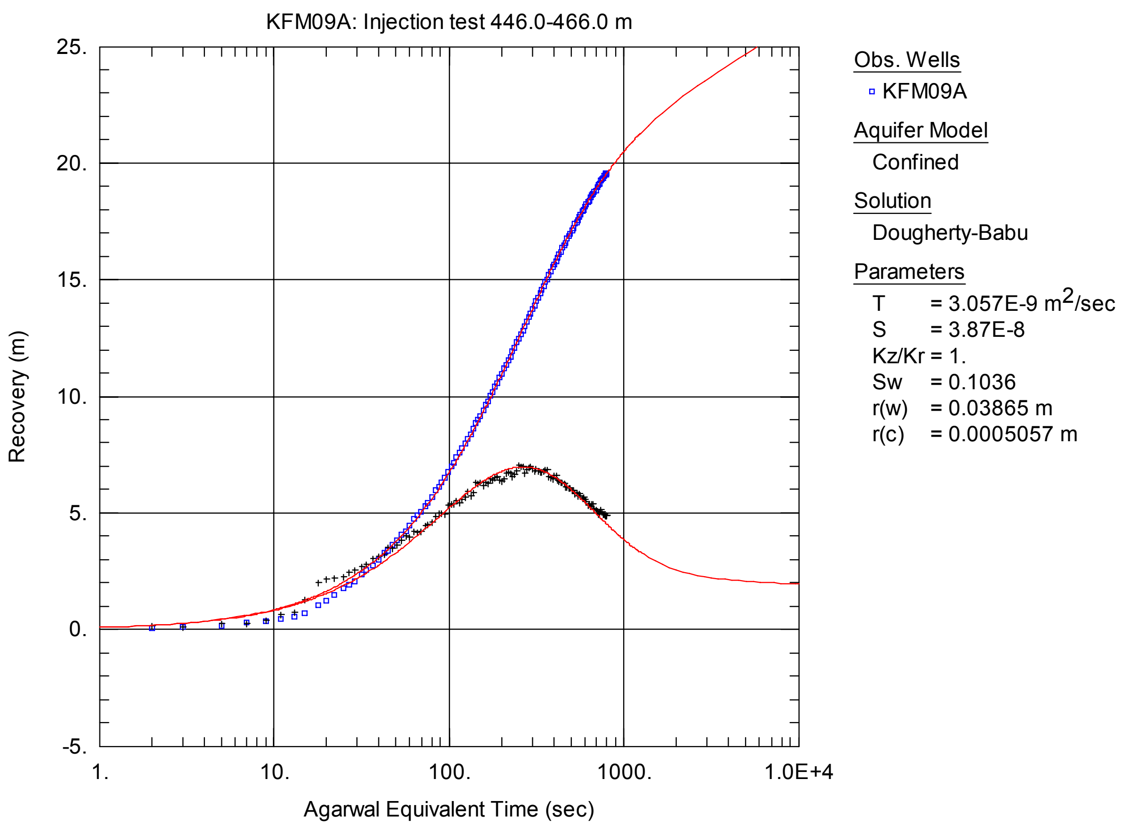


Figure A3-129. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 446.0-466.0 m in KFM09A.*

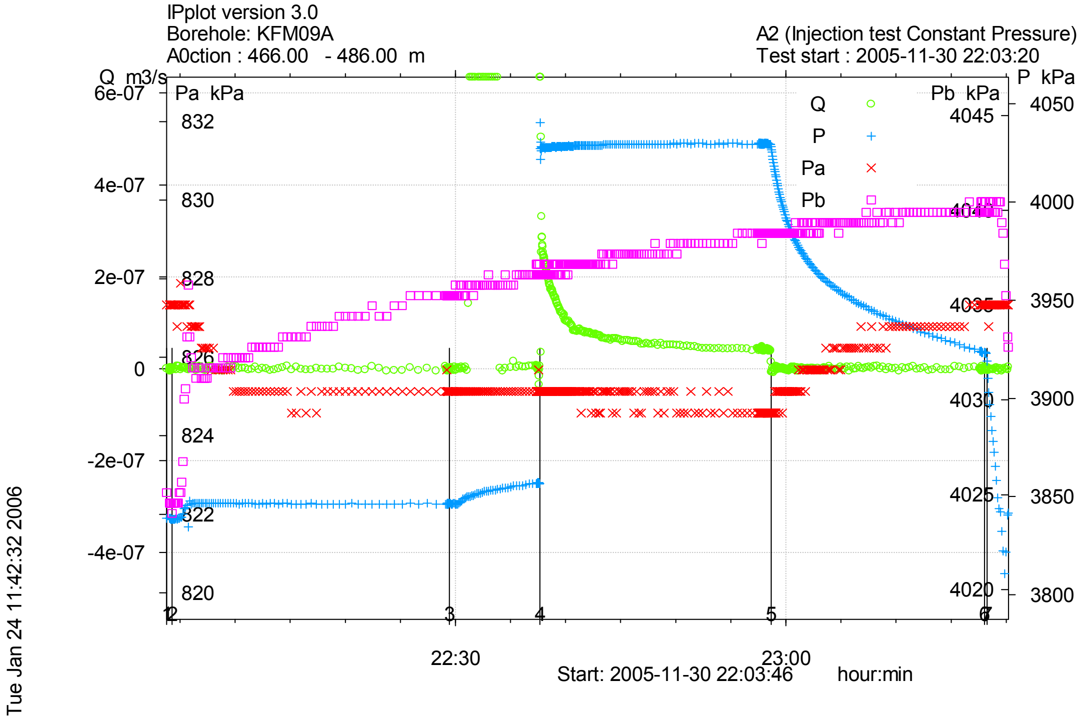


Figure A3-130. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 466.0-486.0 m in borehole KFM09A.*

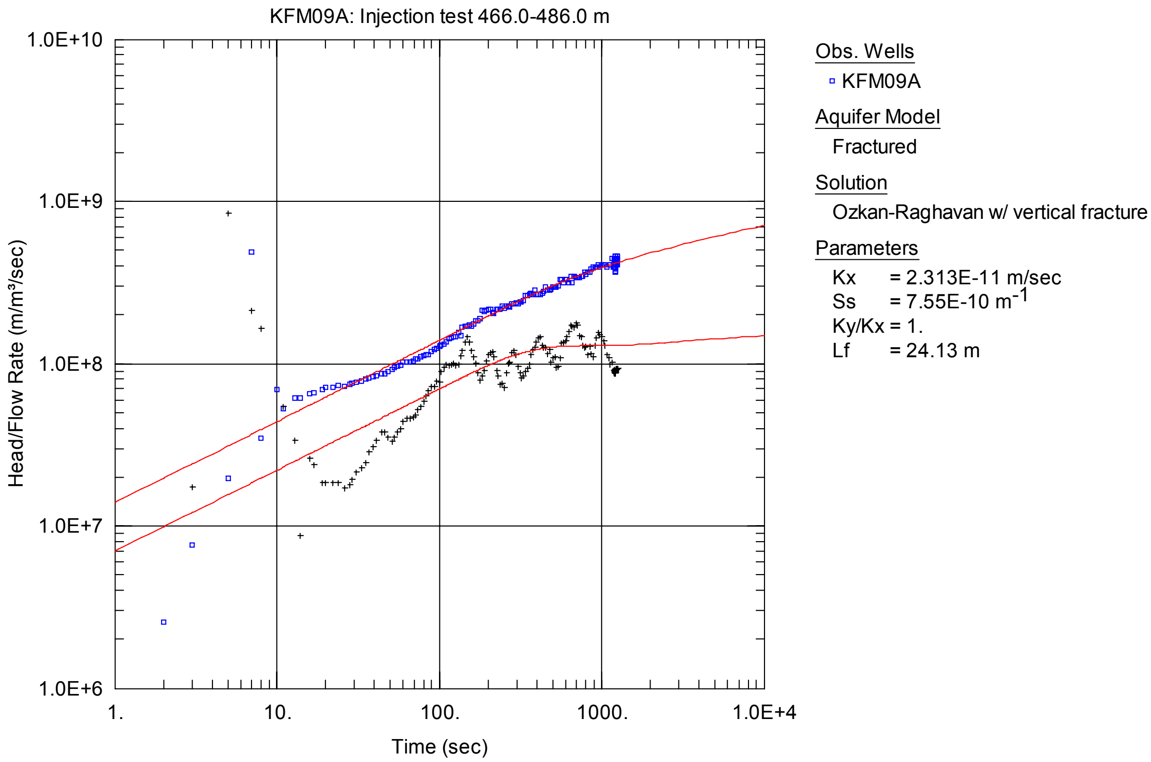


Figure A3-131. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 466.0-486.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

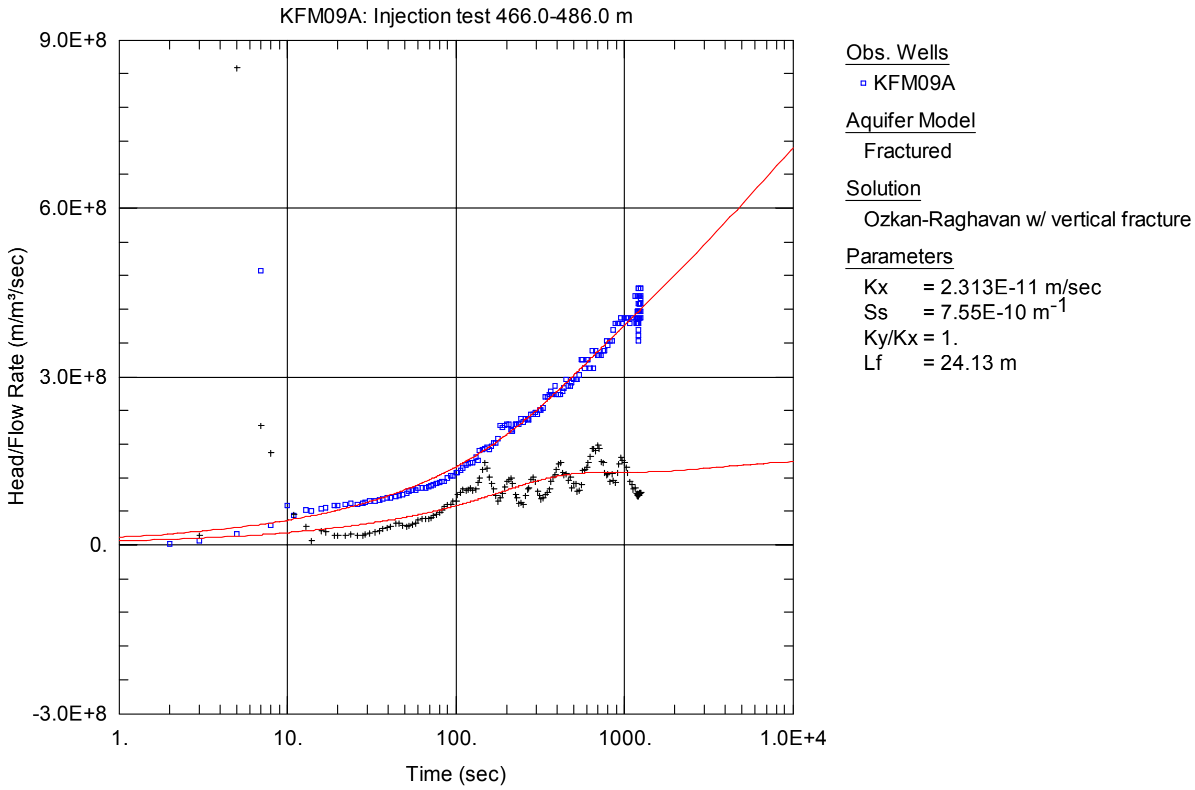


Figure A3-132. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 466.0-486.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

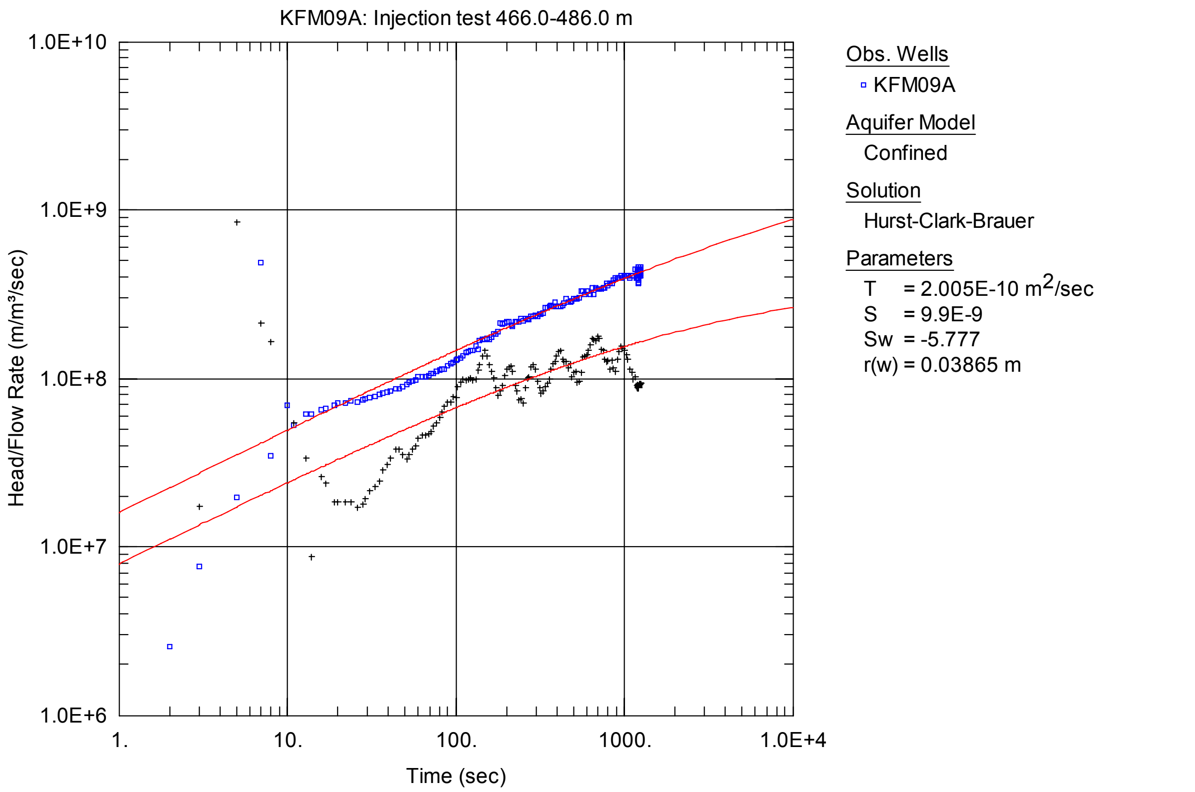


Figure A3-133. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 466.0-486.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for pseudo-radial flow.*

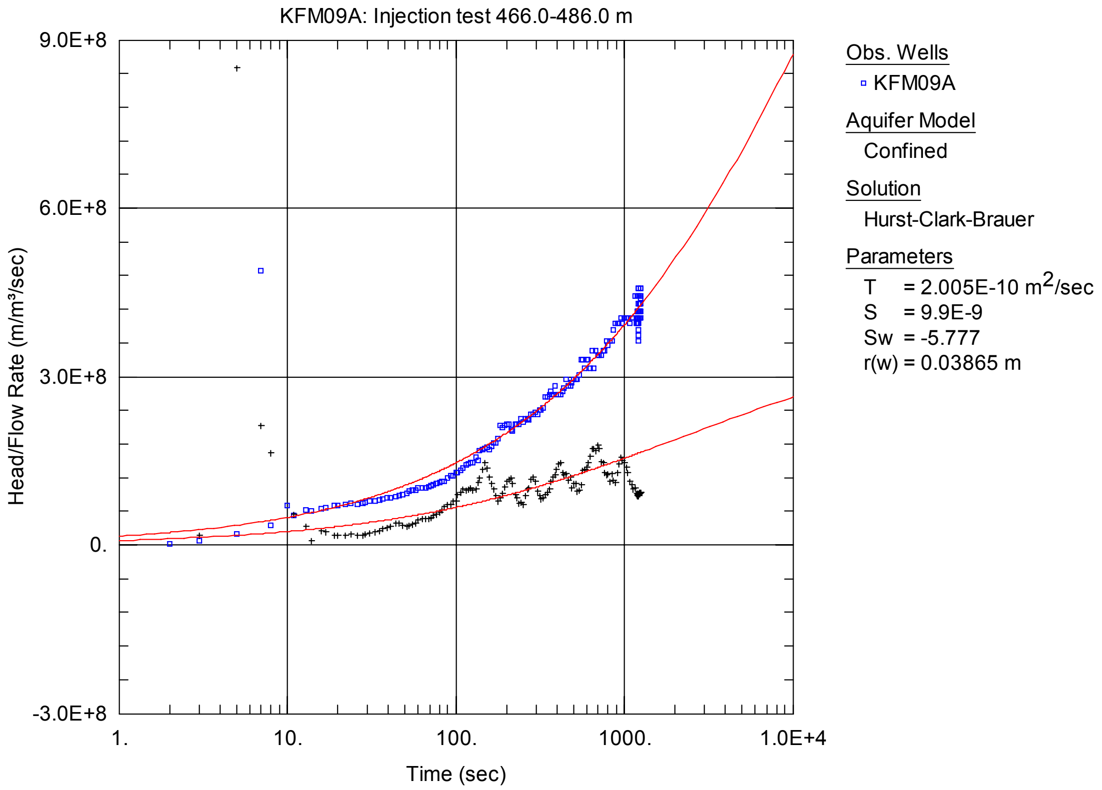


Figure A3-134. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 466.0-486.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for pseudo-radial flow.*

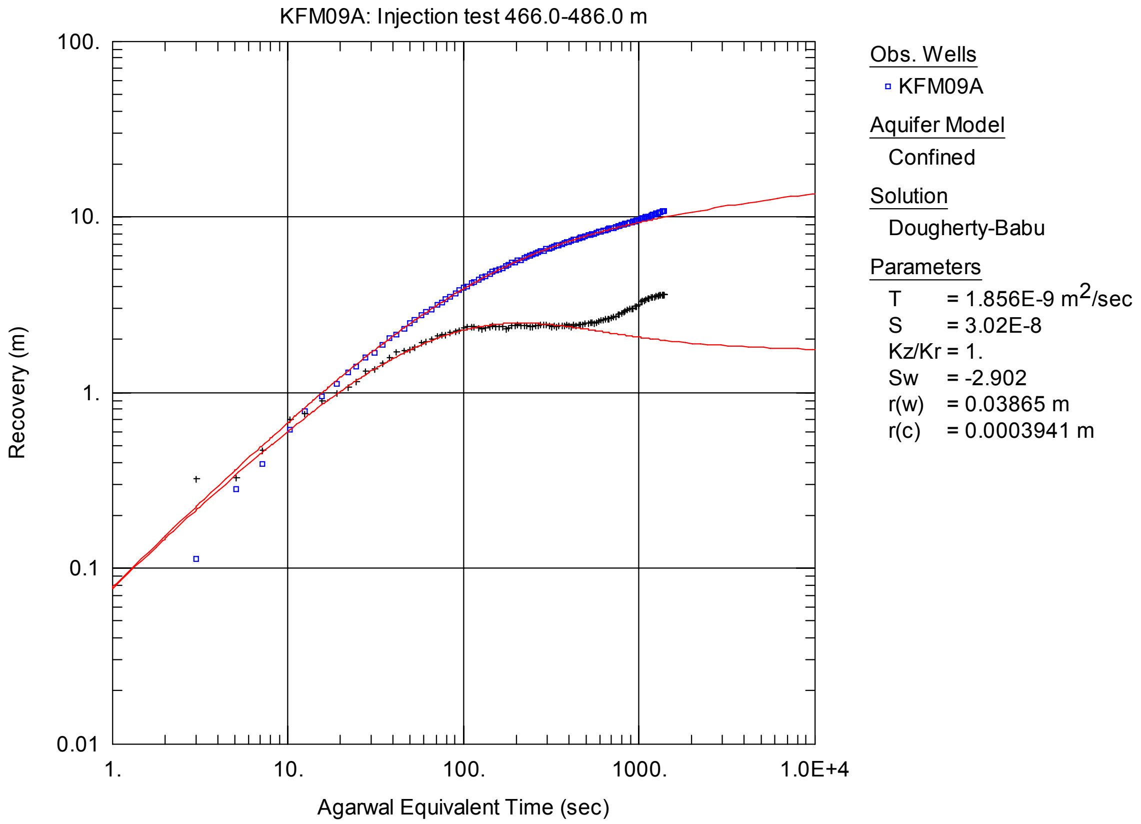


Figure A3-135. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 466.0-486.0 m in KFM09A.*

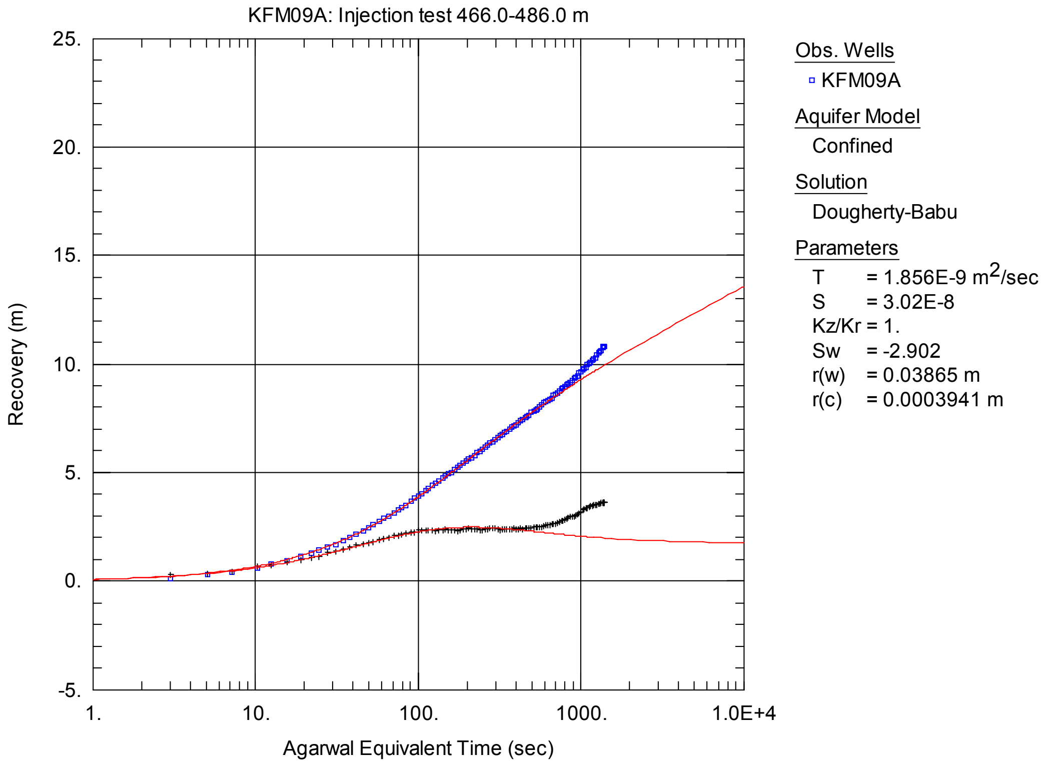


***Figure A3-136.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 466.0-486.0 m in KFM09A.*

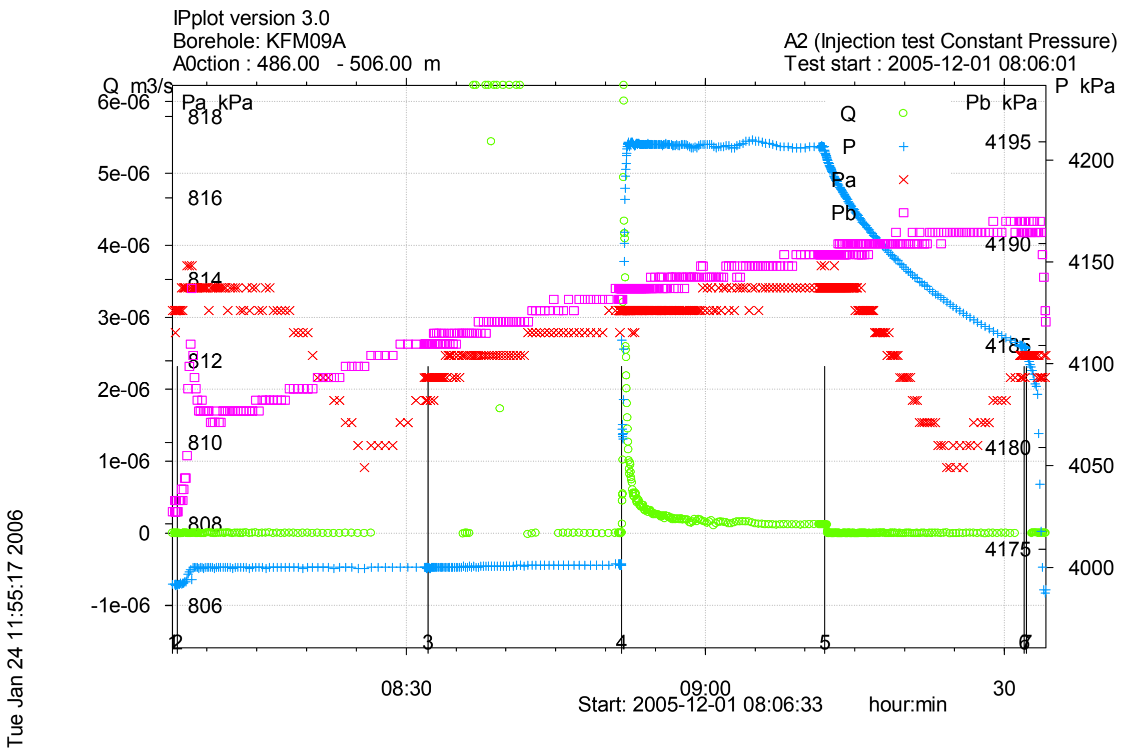


***Figure A3-137.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 486.0-506.0 m in borehole KFM09A.*

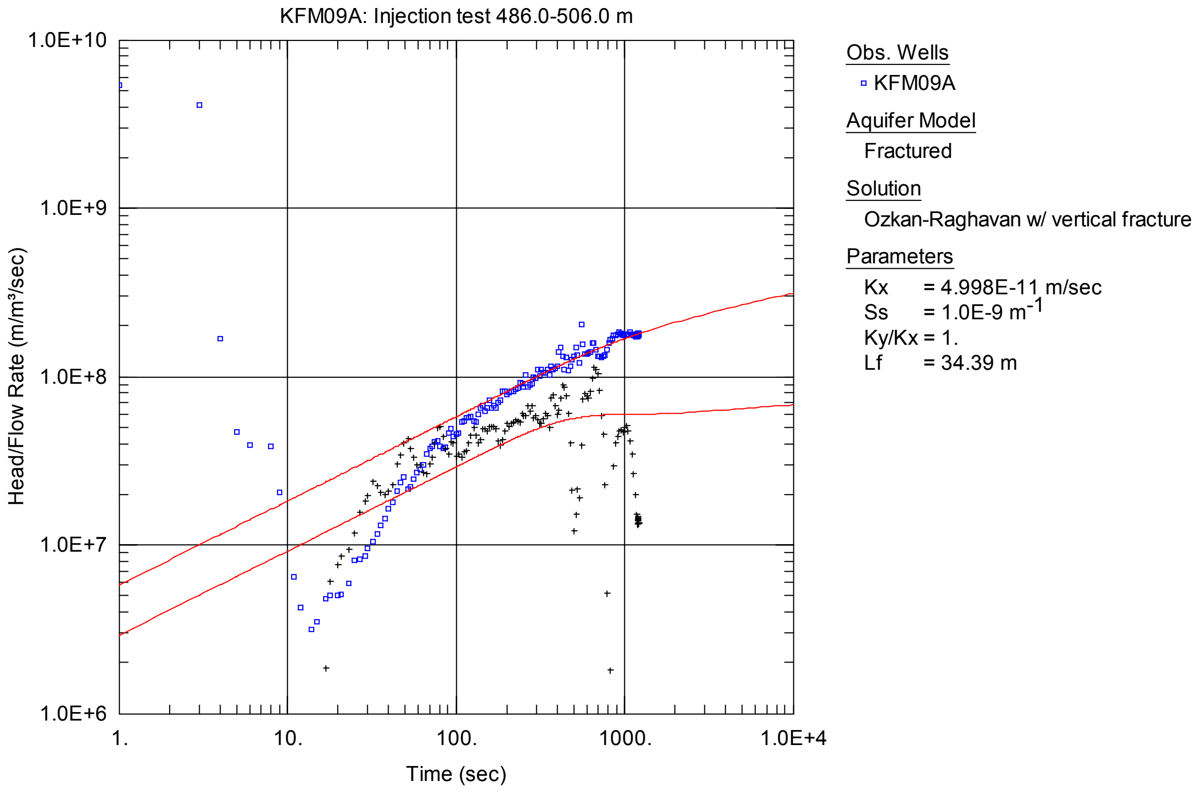


Figure A3-138. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 486.0-506.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

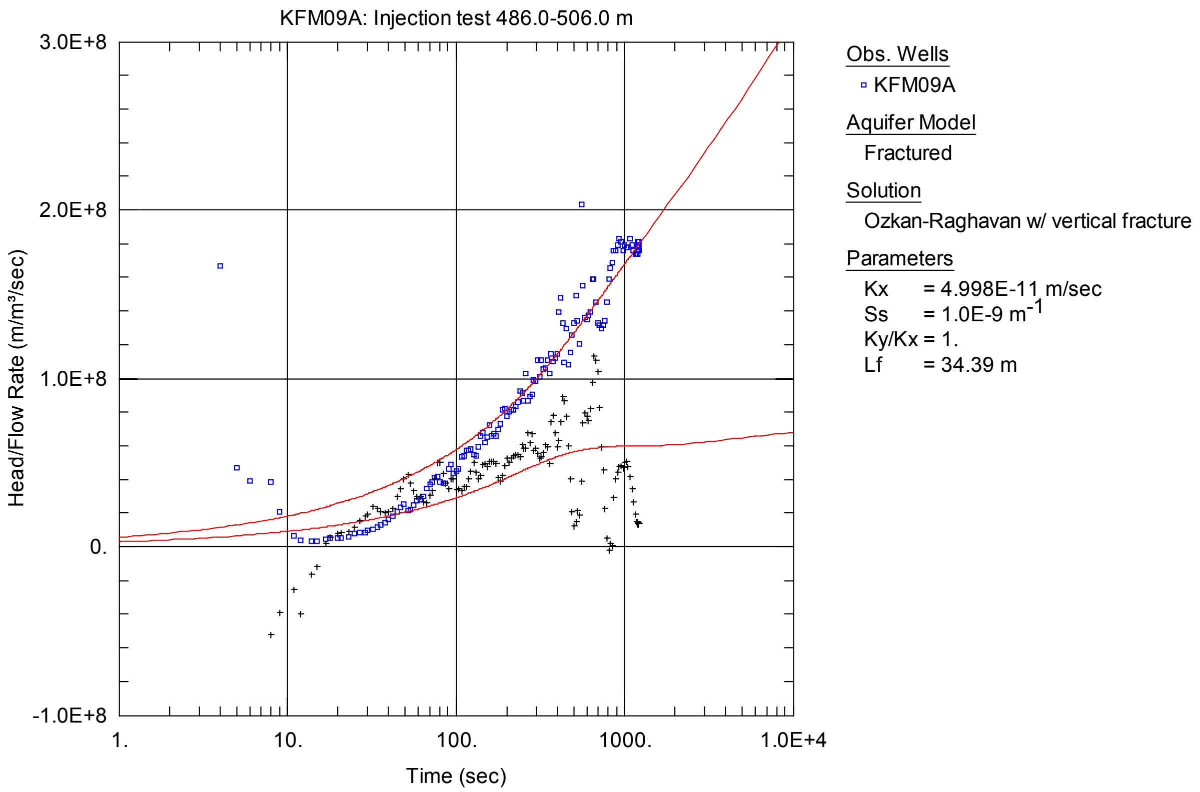


Figure A3-139. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 486.0-506.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

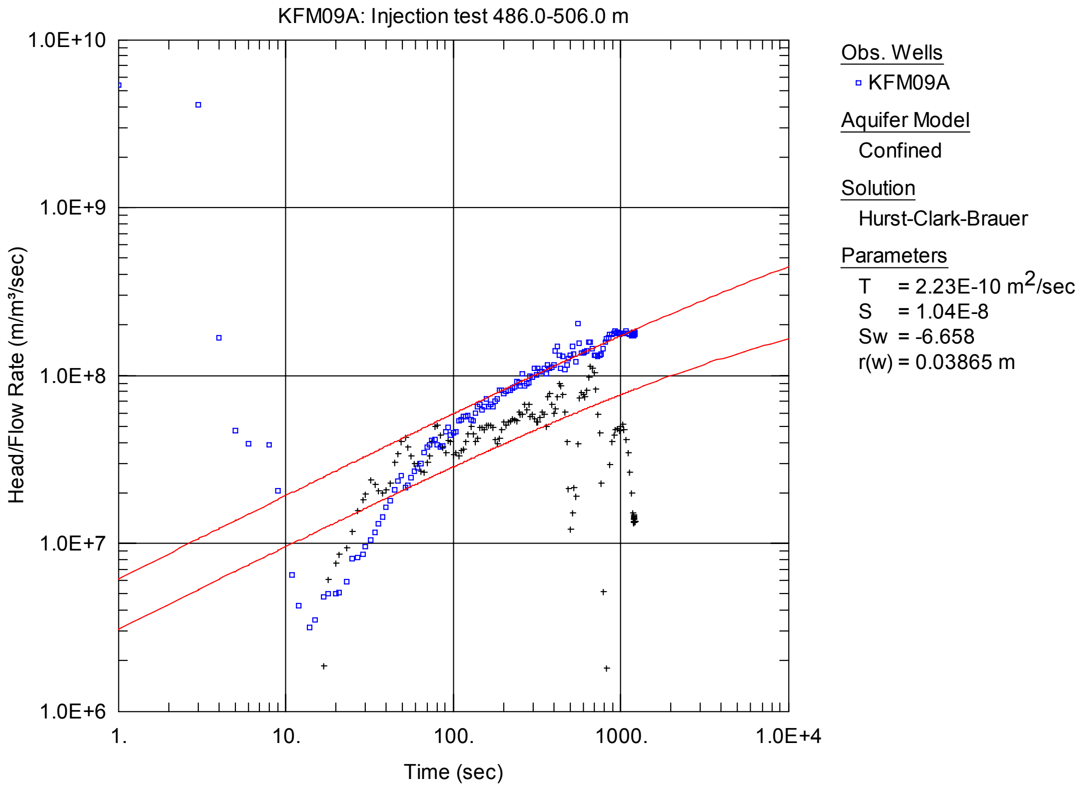


Figure A3-140. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 486.0-506.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for pseudo-radial flow.*

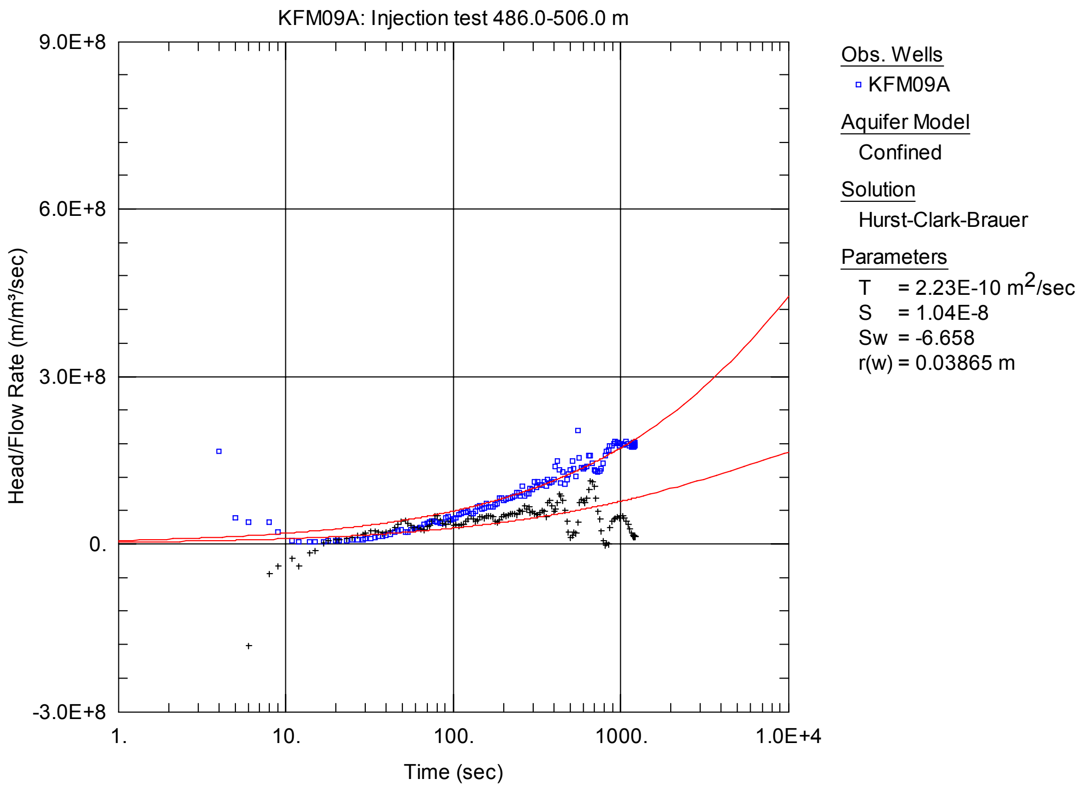


Figure A3-141. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 486.0-506.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for pseudo-radial flow.*

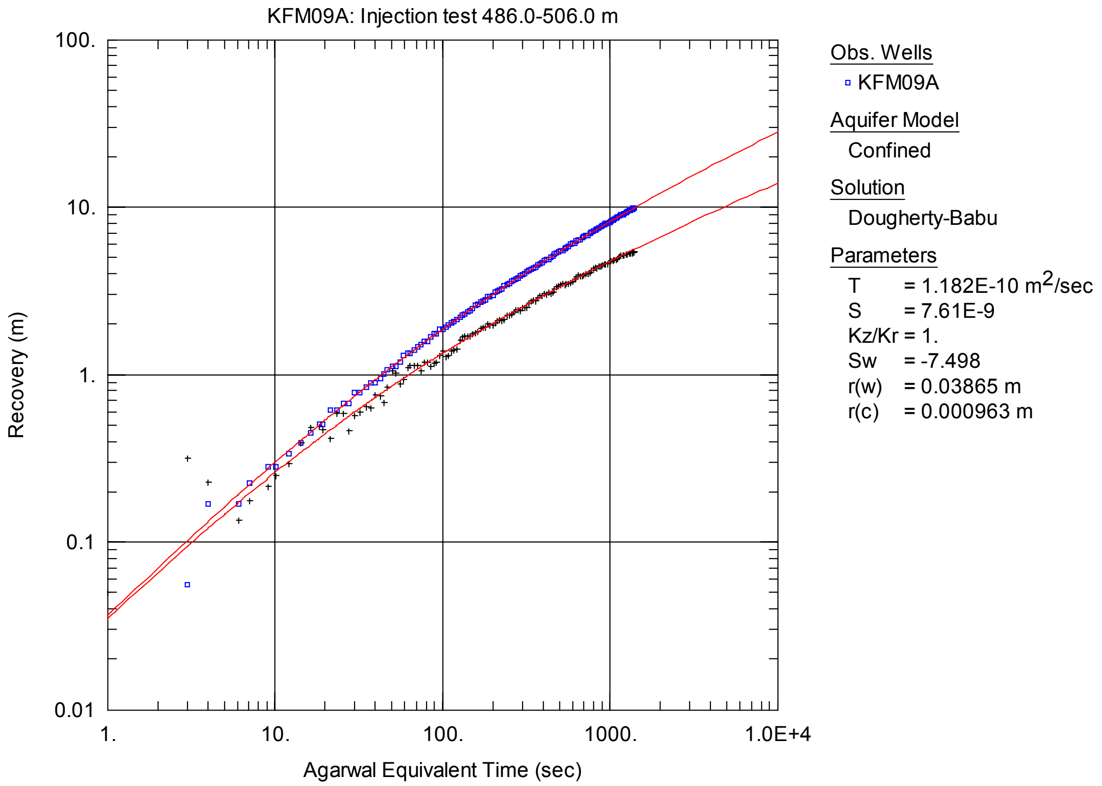


Figure A3-142. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 486.0-506.0 m in KFM09A. The transient evaluation on the recovery period is not regarded as representative.*

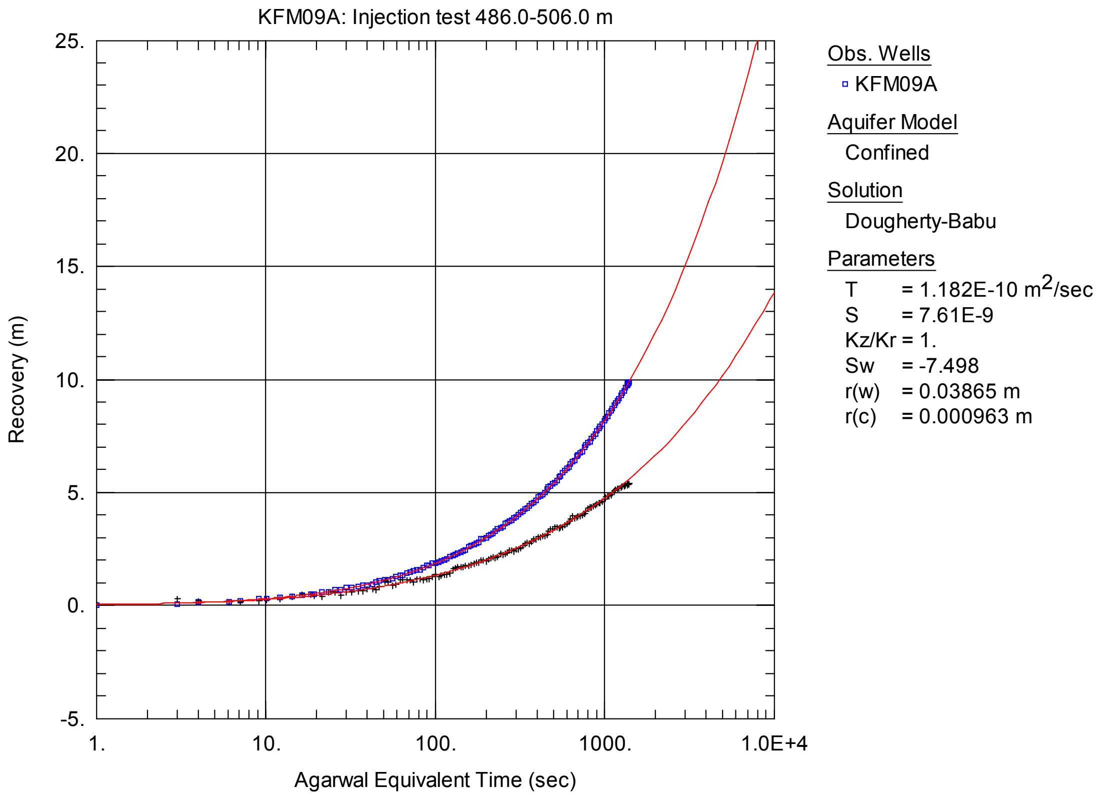


Figure A3-143. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 486.0-506.0 m in KFM09A. The transient evaluation on the recovery period is not regarded as representative.*

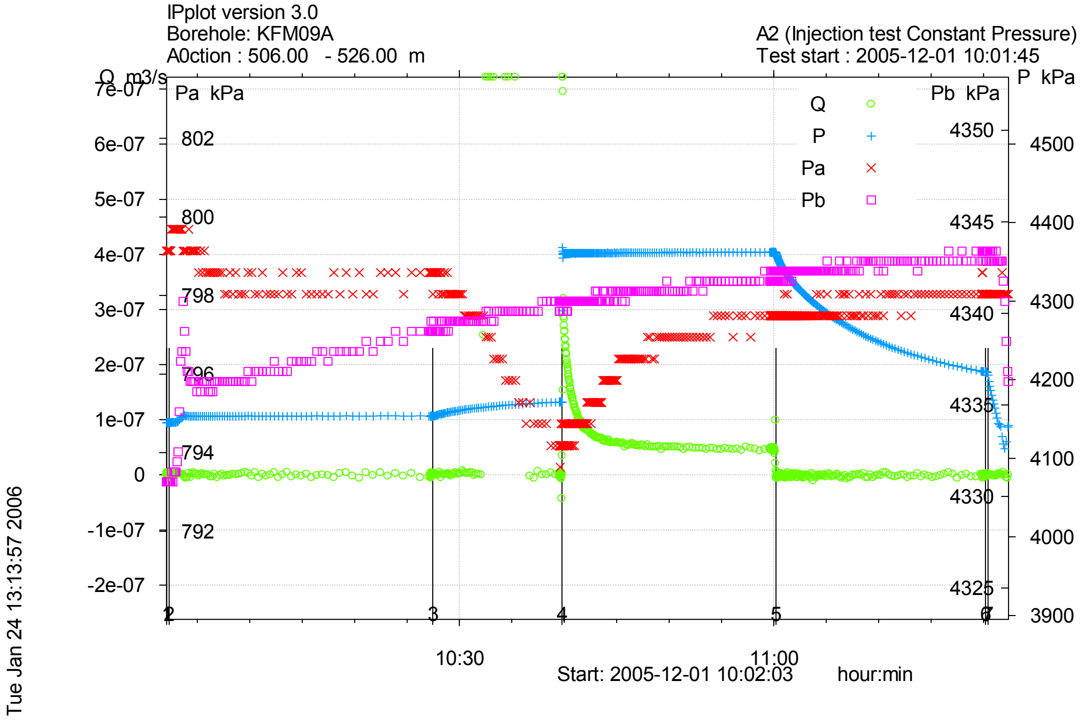


Figure A3-144. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 506.0-526.0 m in borehole KFM09A.*

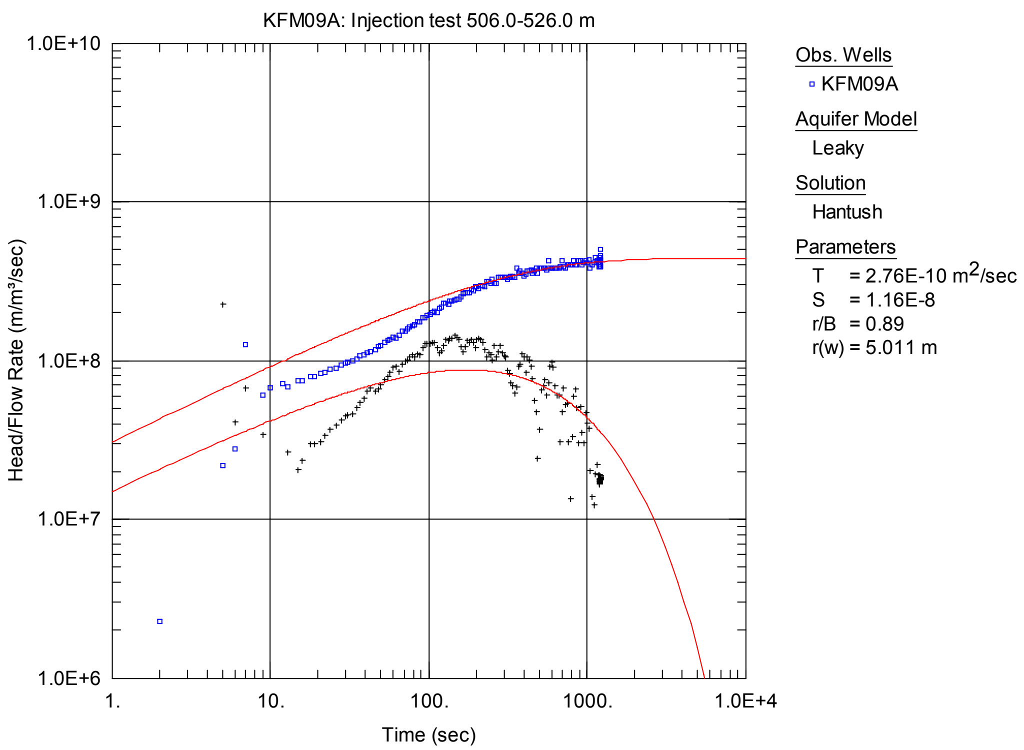


Figure A3-145. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 506.0-526.0 m in KFM09A. No unambiguous evaluation could be made on the injection period.*

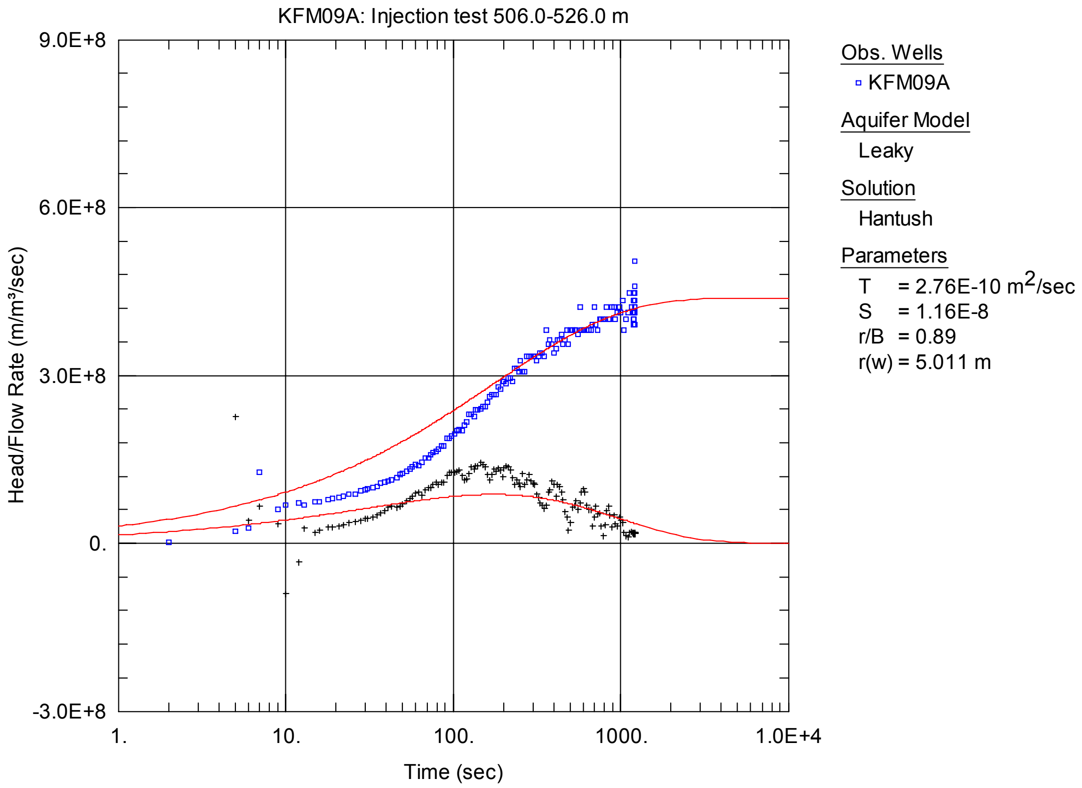


Figure A3-146. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 506.0-526.0 m in KFM09A. No unambiguous evaluation could be made on the injection period.*

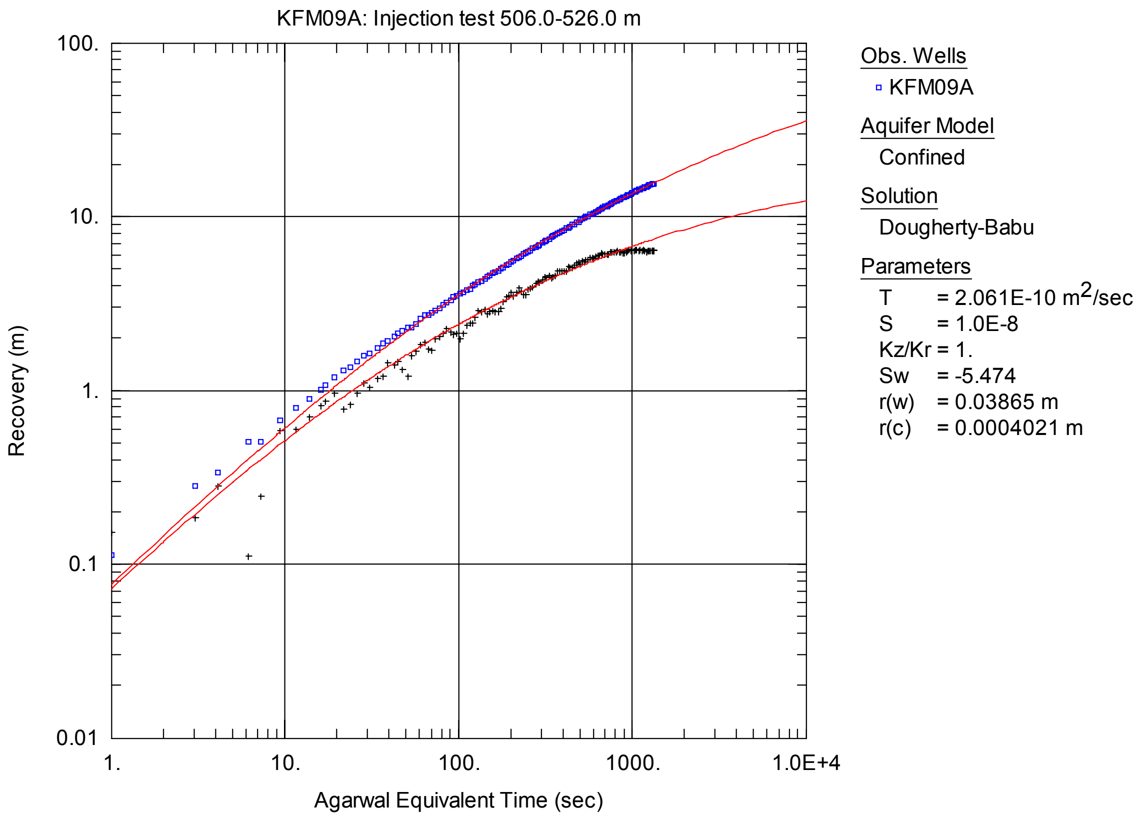


Figure A3-147. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 506.0-526.0 m in KFM09A.*

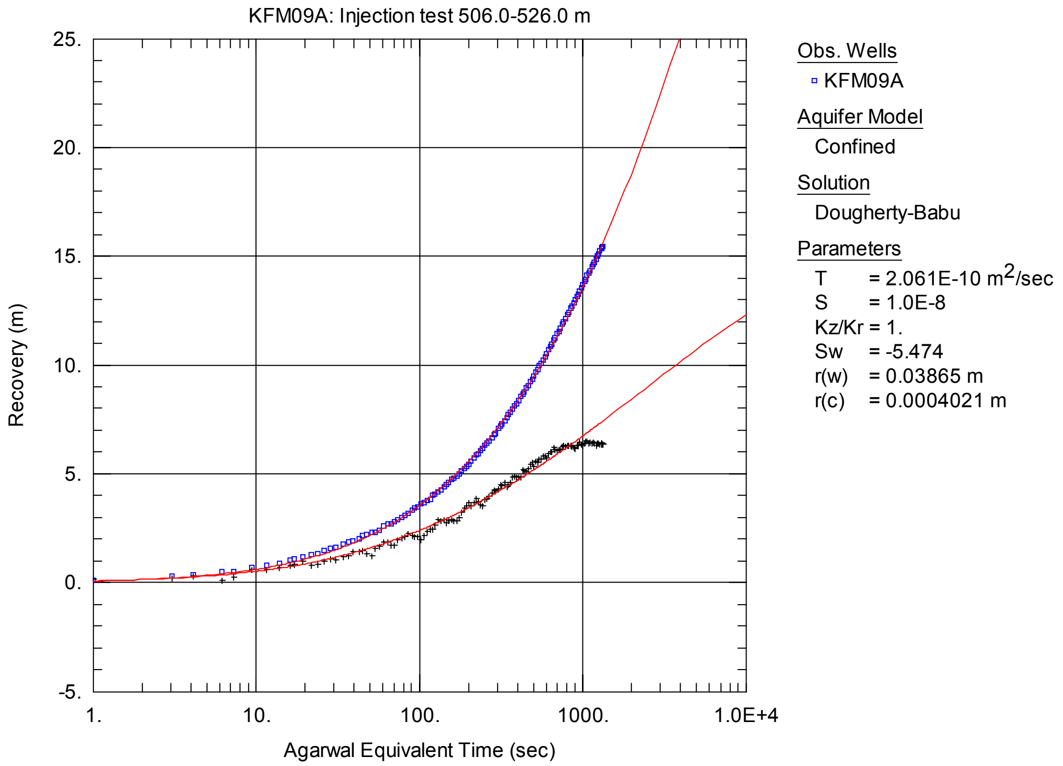


Figure A3-148. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 506.0-526.0 m in KFM09A.*

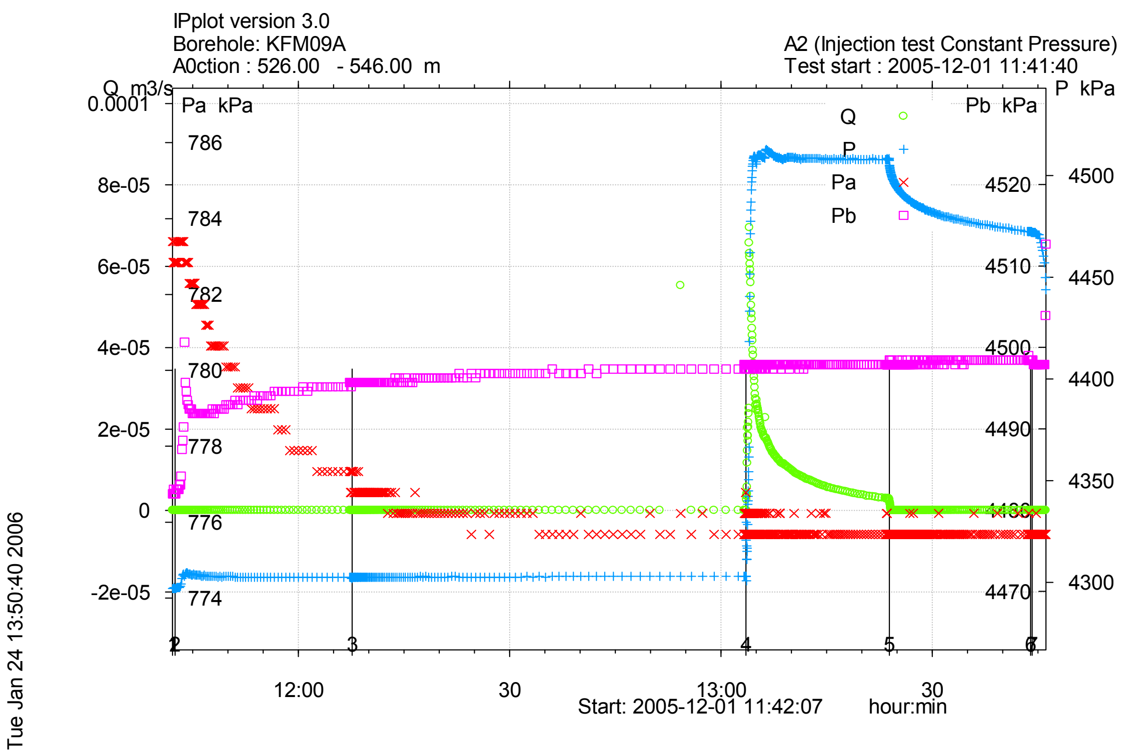


Figure A3-149. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 526.0-546.0 m in borehole KFM09A.*

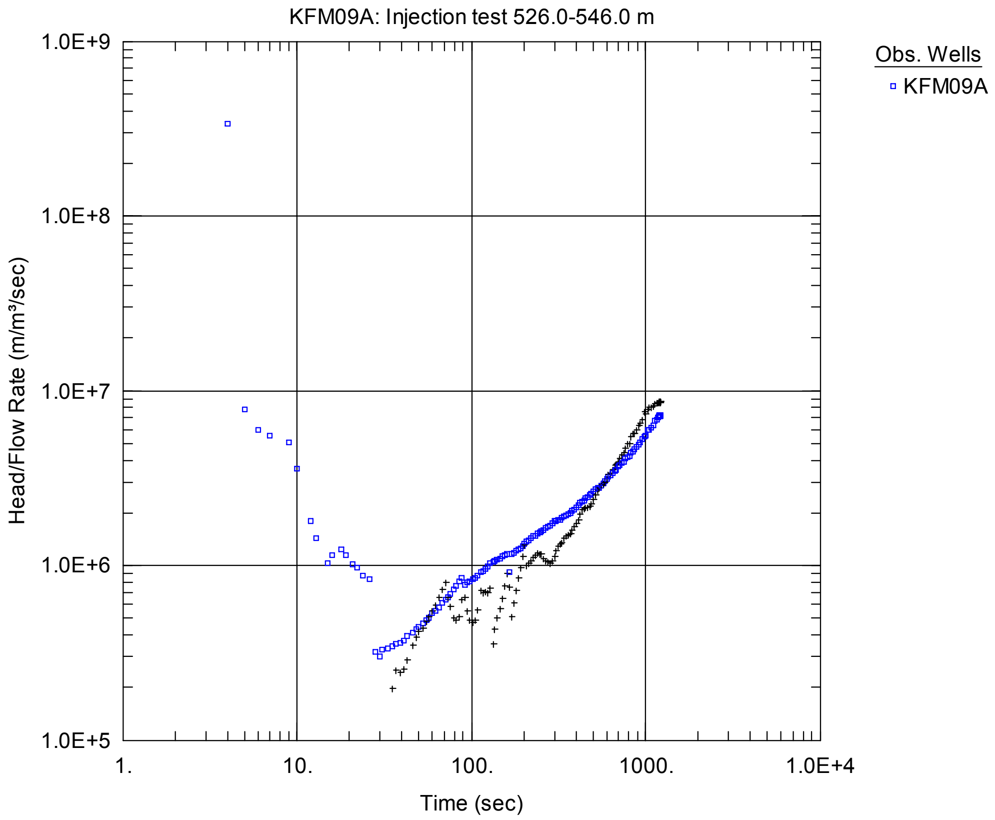


***Figure A3-150.** Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 526.0-546.0 m in KFM09A.*

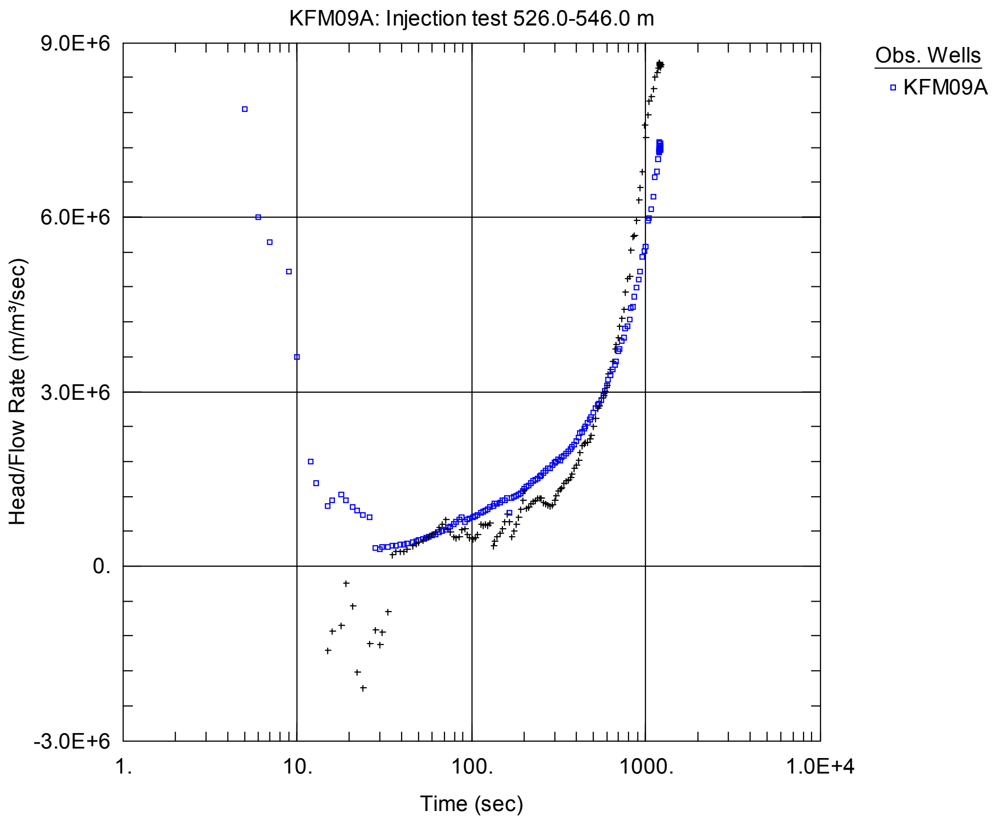


***Figure A3-151.** Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 526.0-546.0 m in KFM09A.*

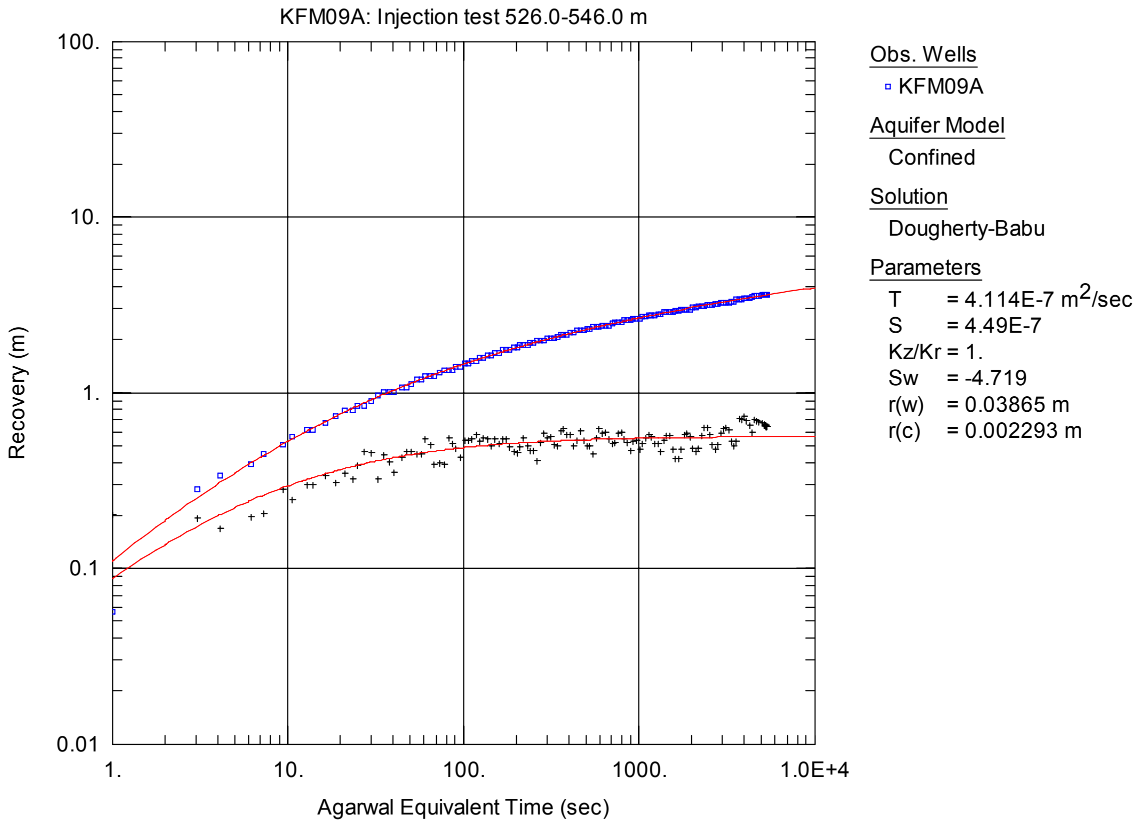


Figure A3-152. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 526.0-546.0 m in KFM09A.*

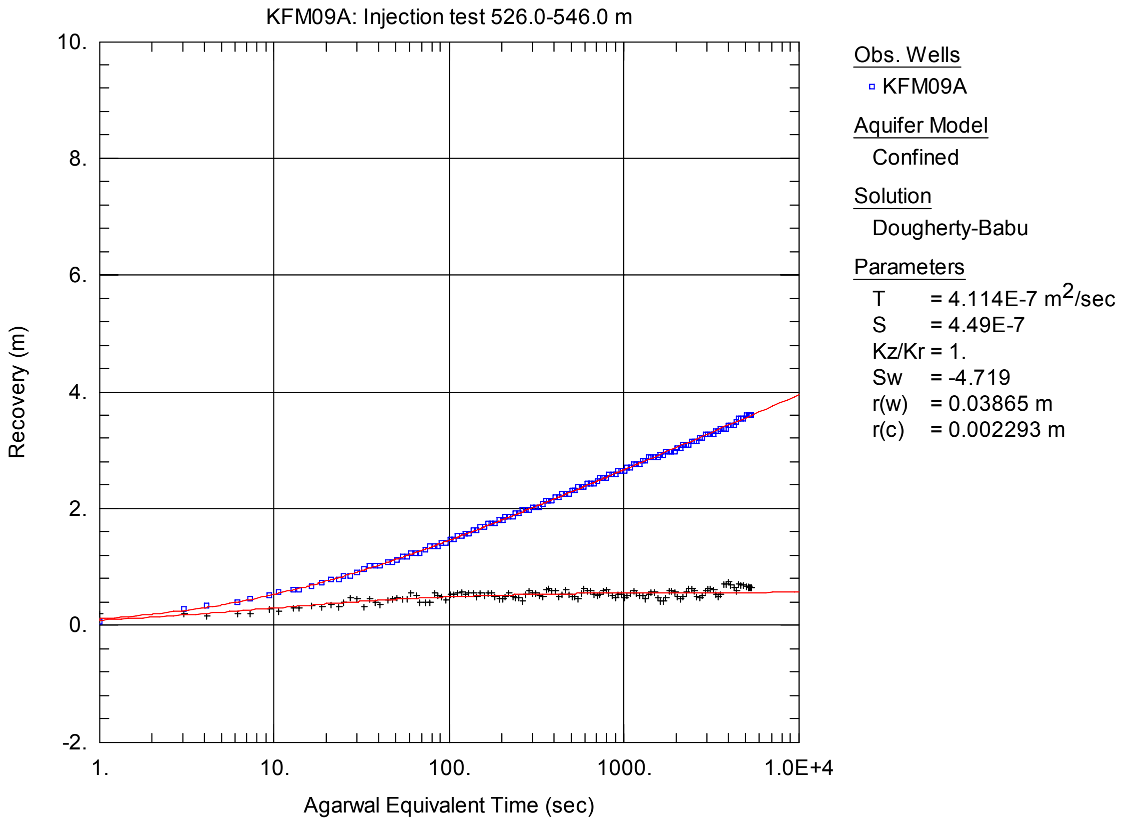


Figure A3-153. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 526.0-546.0 m in KFM09A.*

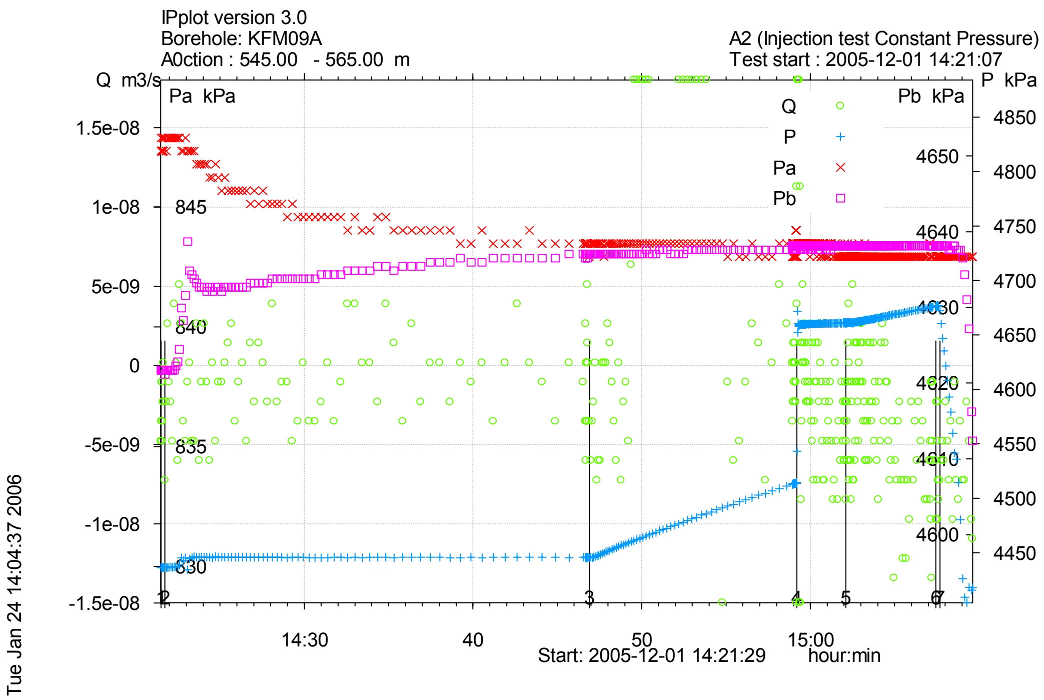


Figure A3-154. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 545.0-565.0 m in borehole KFM09A.

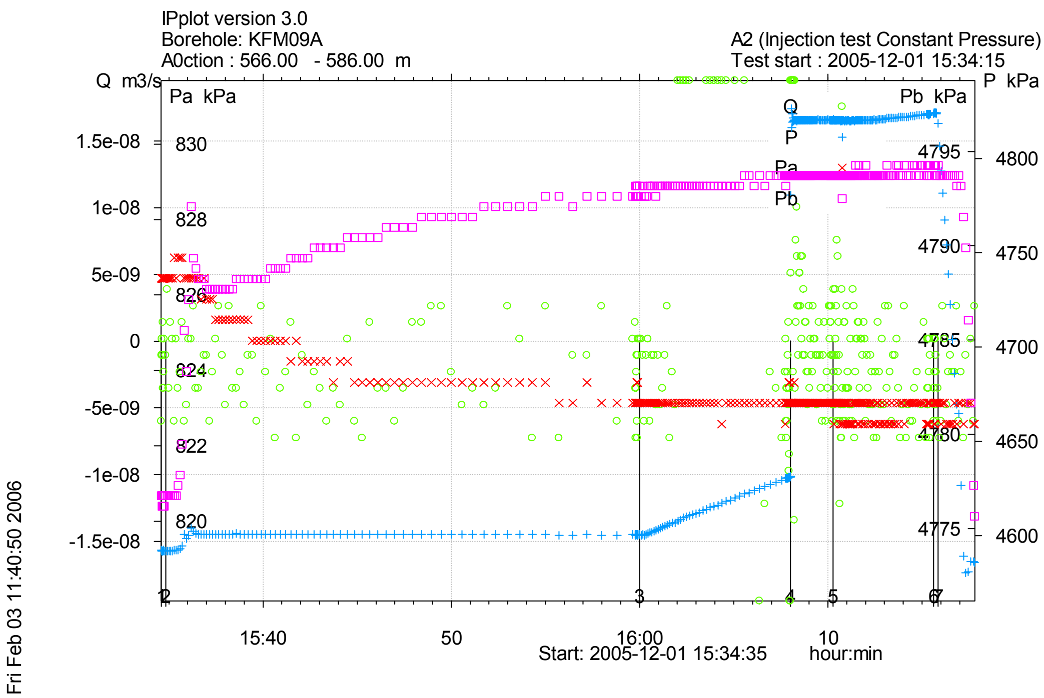


Figure A3-155. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 566.0-586.0 m in borehole KFM09A.

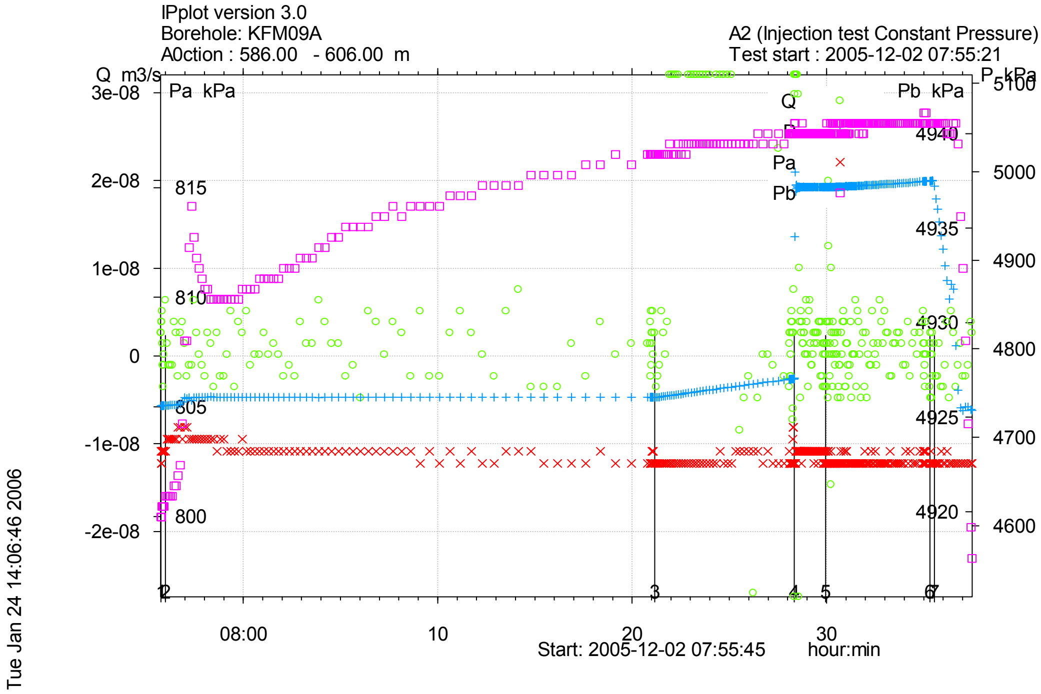


Figure A3-156. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 586.0-606.0 m in borehole KFM09A.*

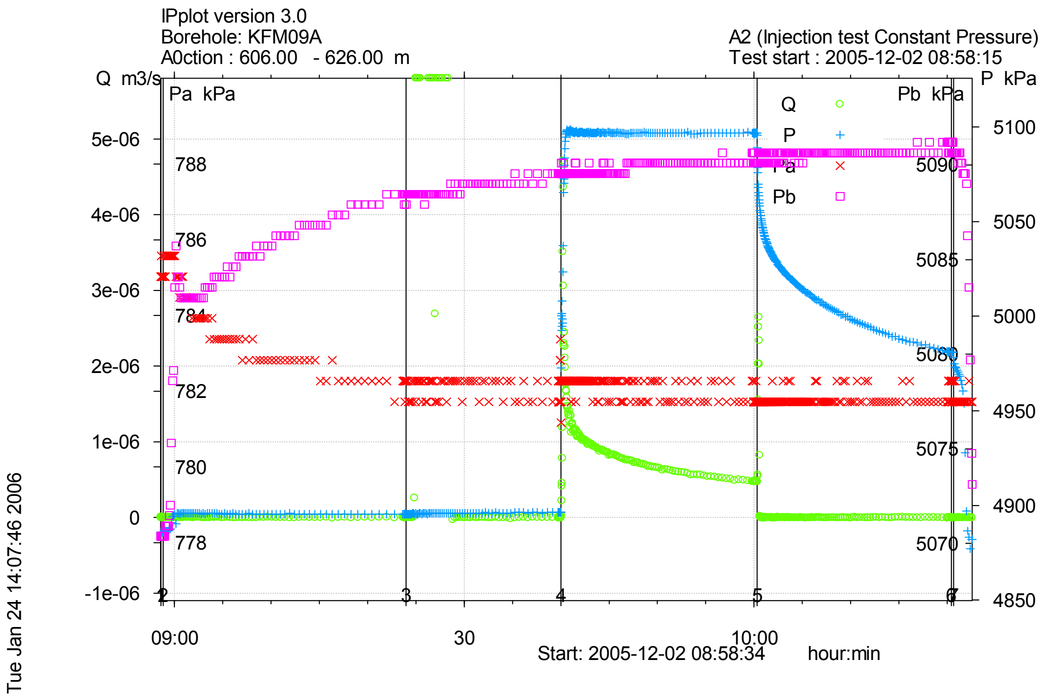


Figure A3-157. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 606.0-626.0 m in borehole KFM09A.*

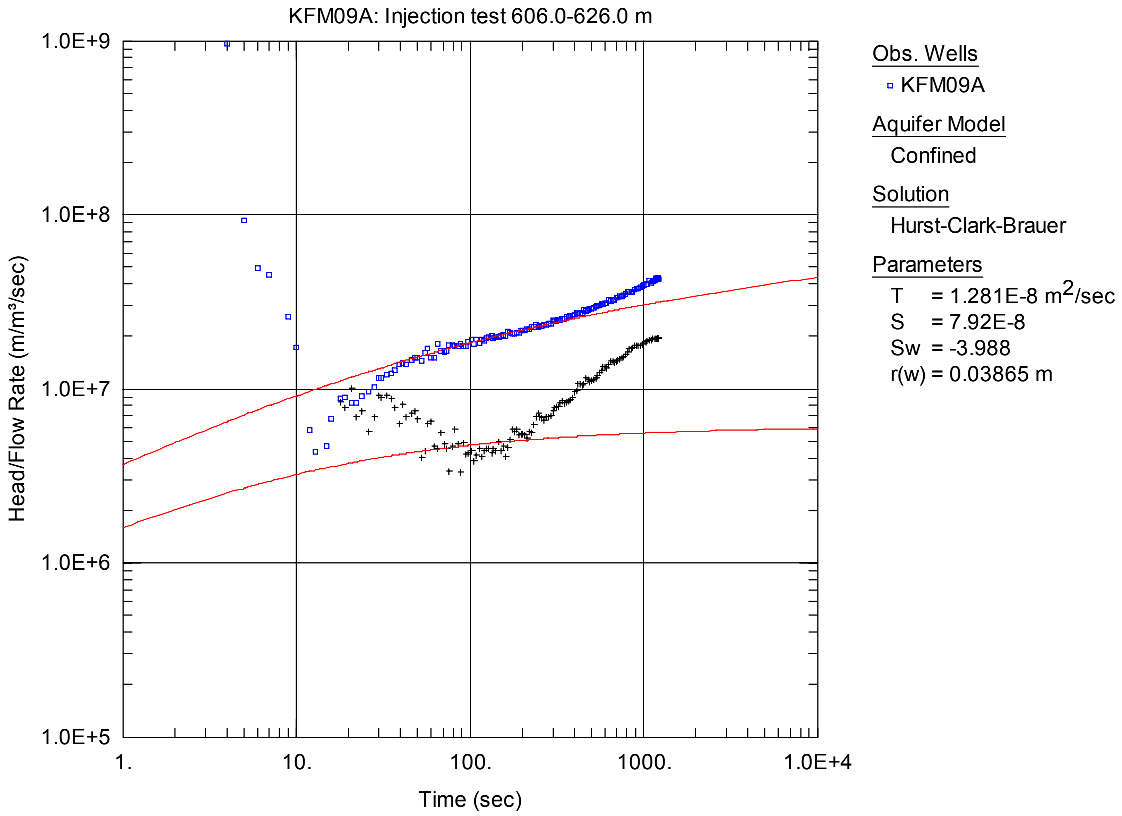


Figure A3-158. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 606.0-626.0 m in KFM09A.*

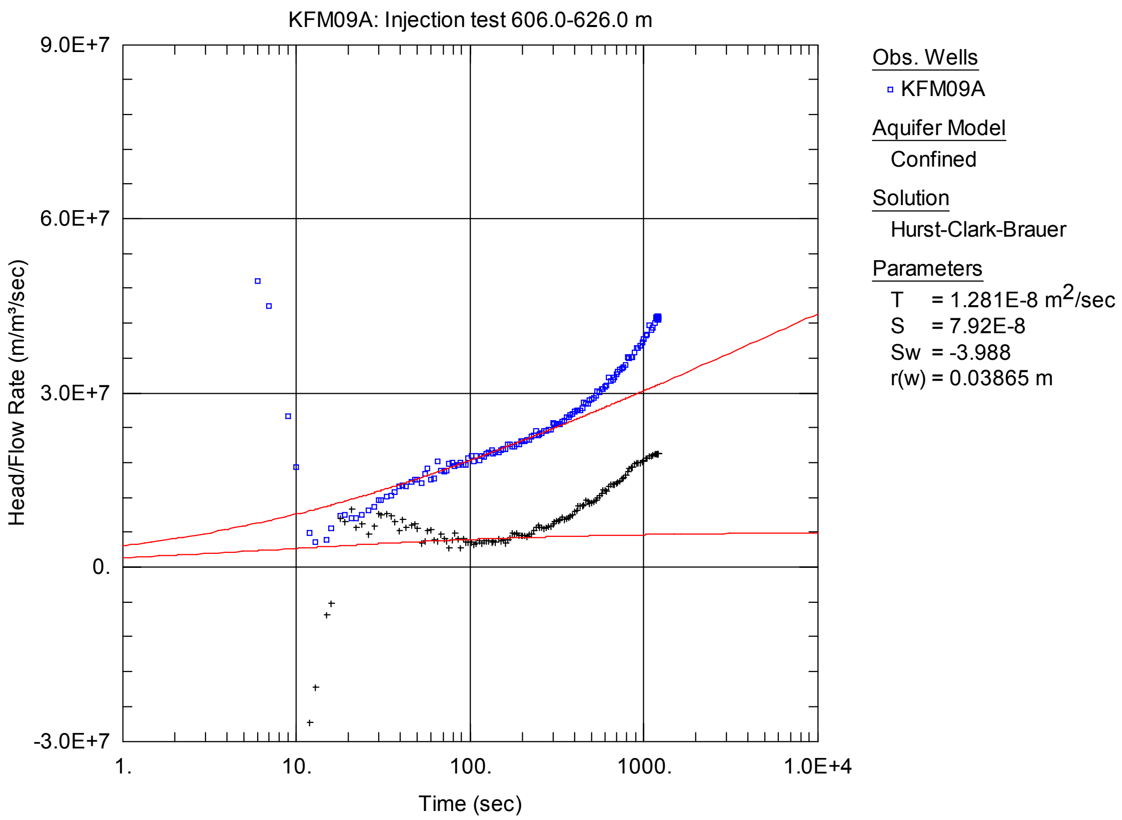


Figure A3-159. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 606.0-626.0 m in KFM09A.*

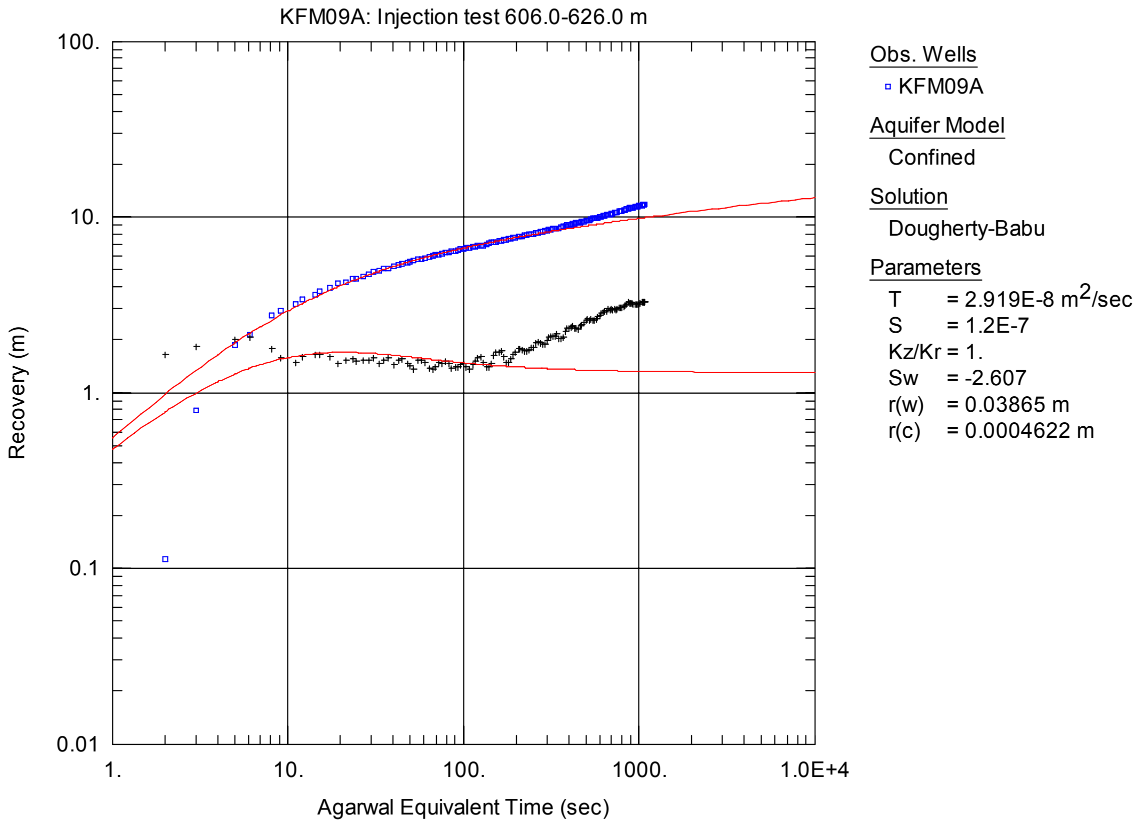


Figure A3-160. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 606.0-626.0 m in KFM09A.*

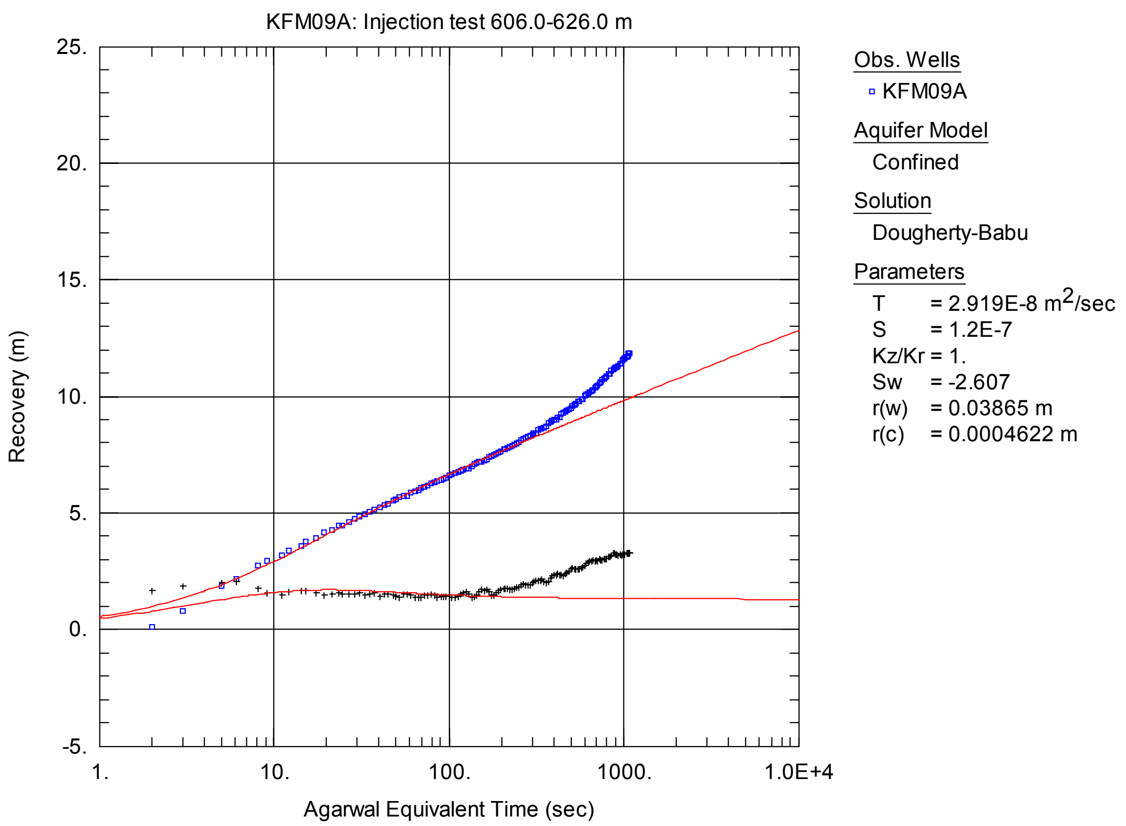


Figure A3-161. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 606.0-626.0 m in KFM09A.*

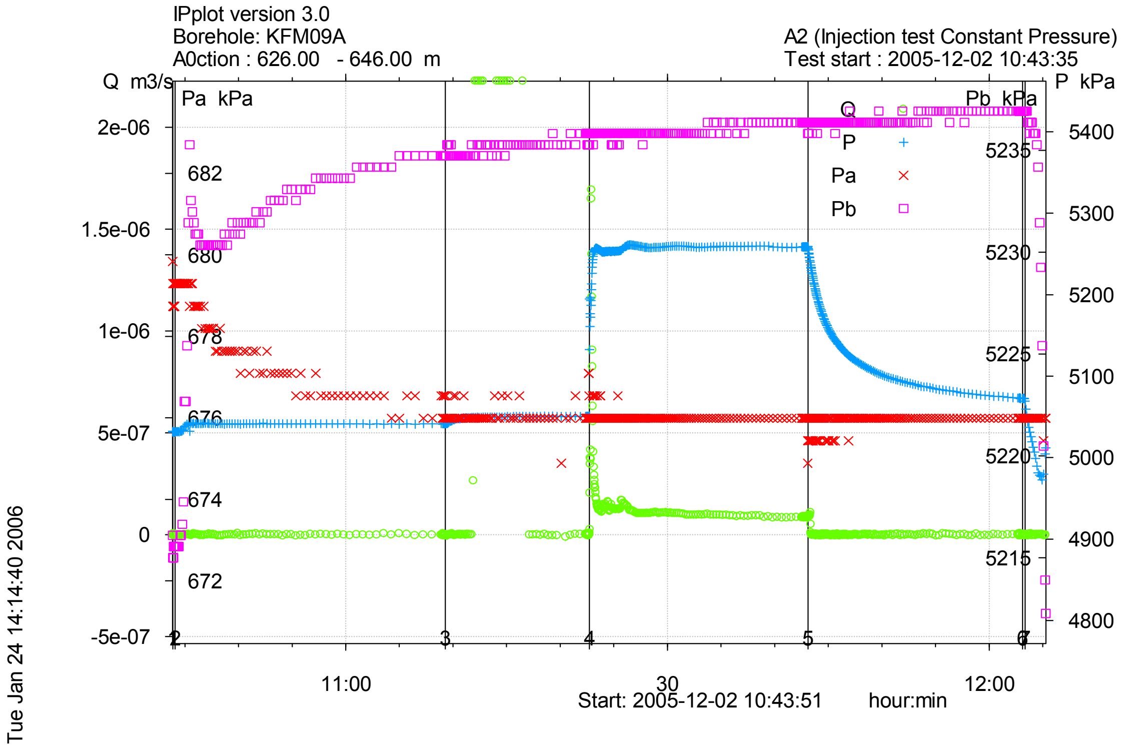


Figure A3-162. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in 626.0-646.0 m in borehole KFM09A.*

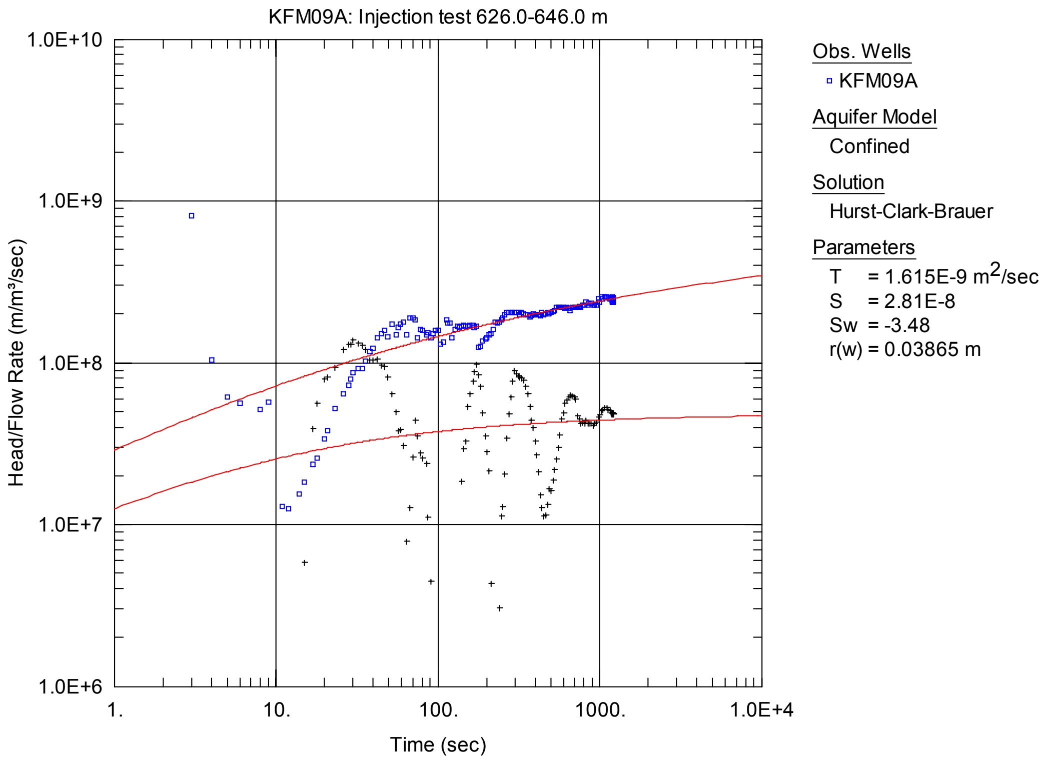


Figure A3-163. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 626.0-646.0 m in KFM09A.*

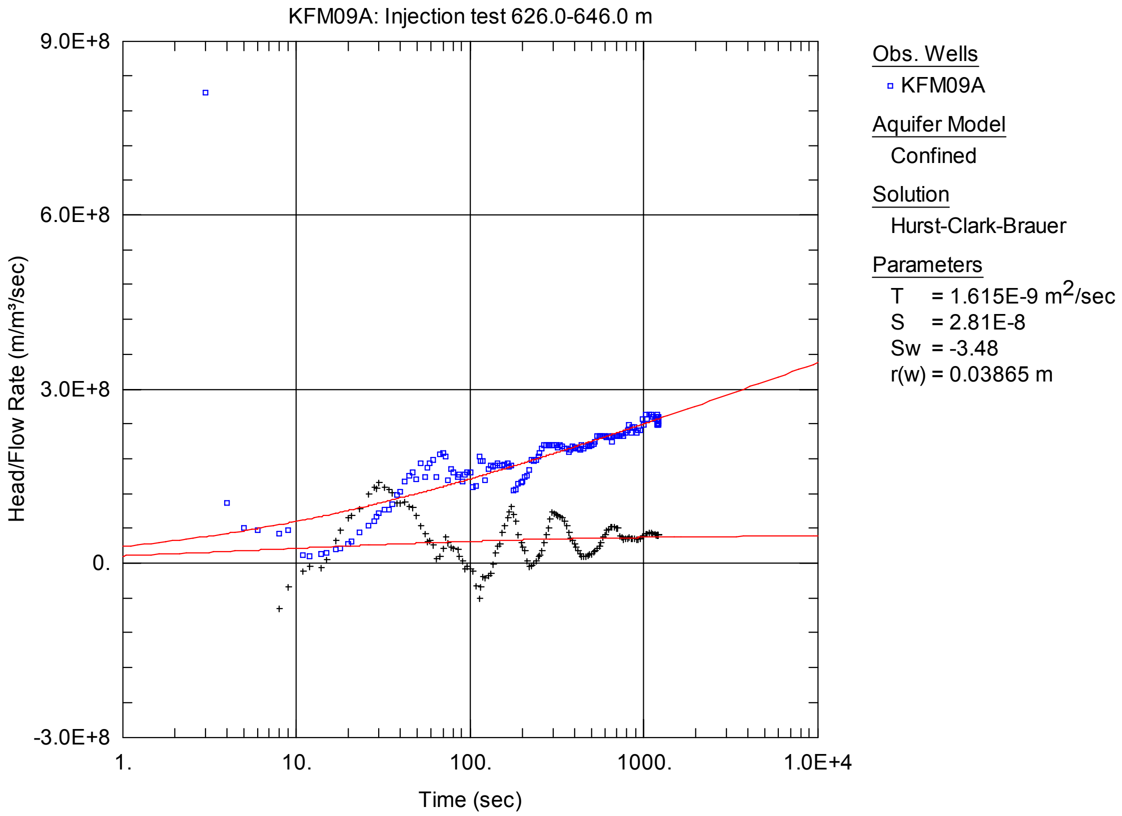


Figure A3-164. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in 626.0-646.0 m in KFM09A.*

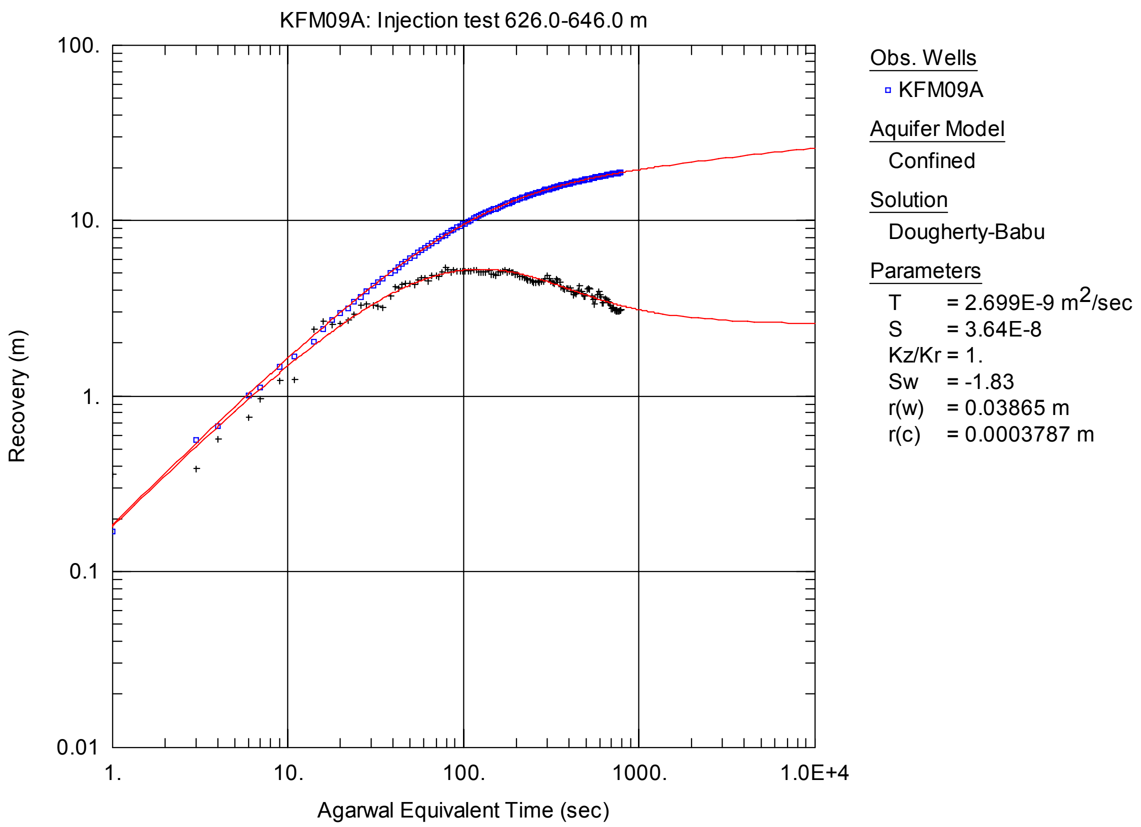


Figure A3-165. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 626.0-646.0 m in KFM09A.*

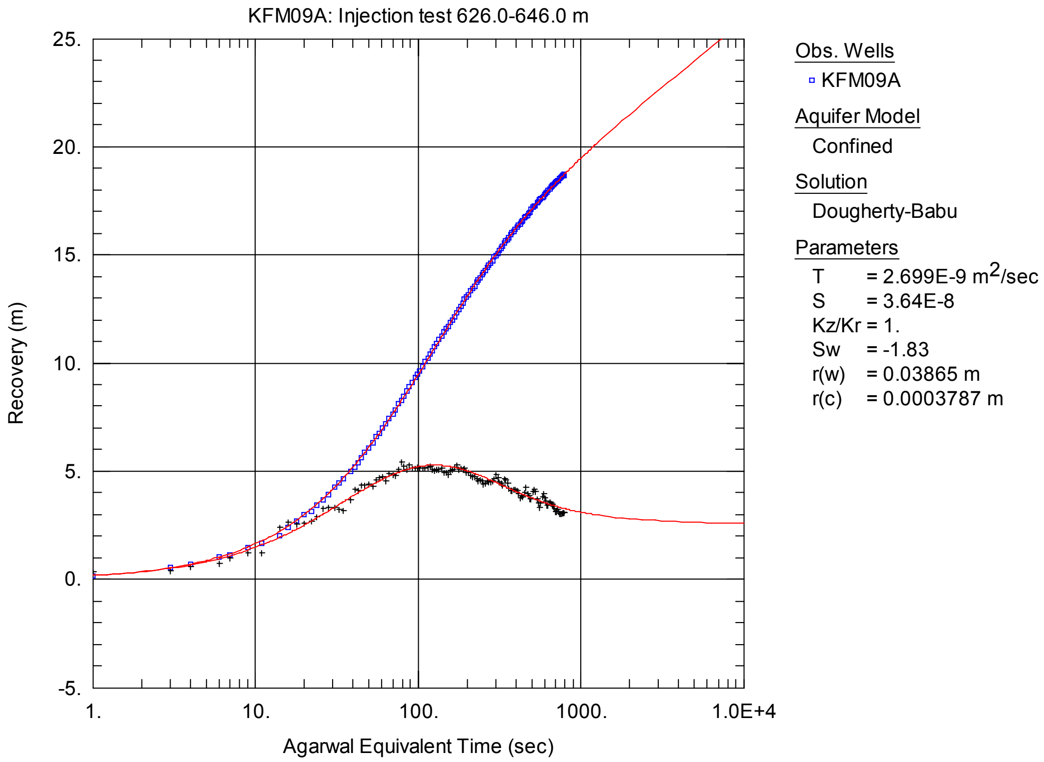


Figure A3-166. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 626.0-646.0 m in KFM09A.*

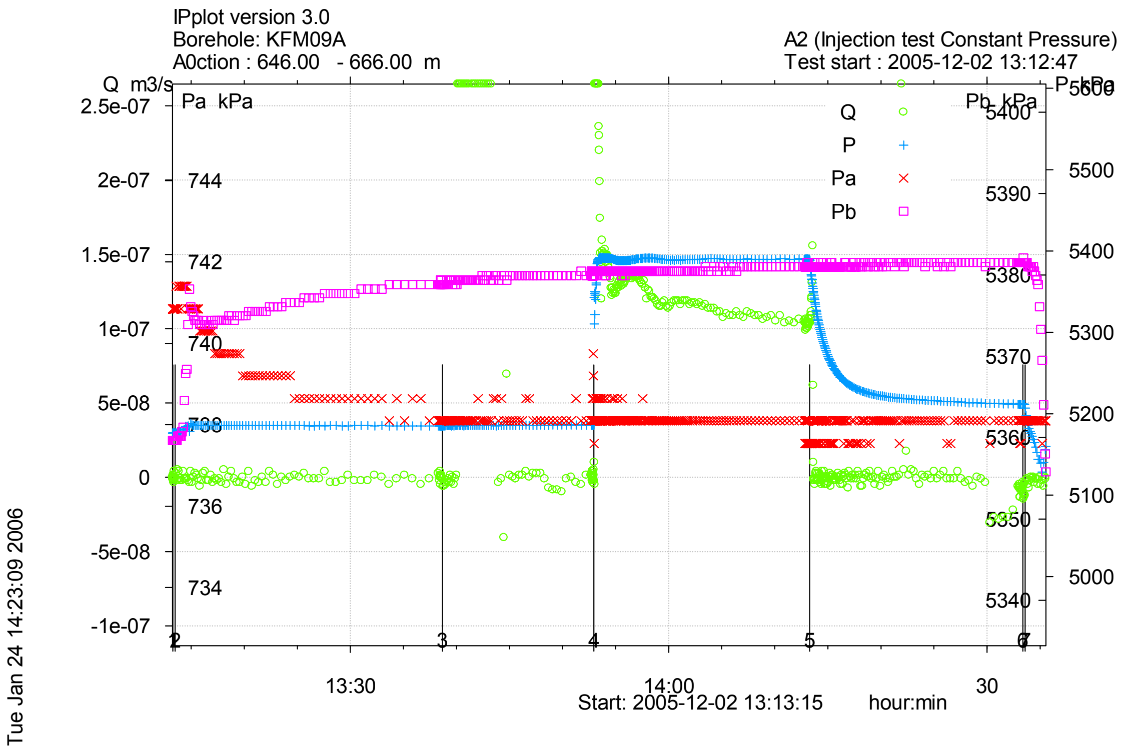


Figure A3-167. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 646.0-666.0 m in borehole KFM09A.*

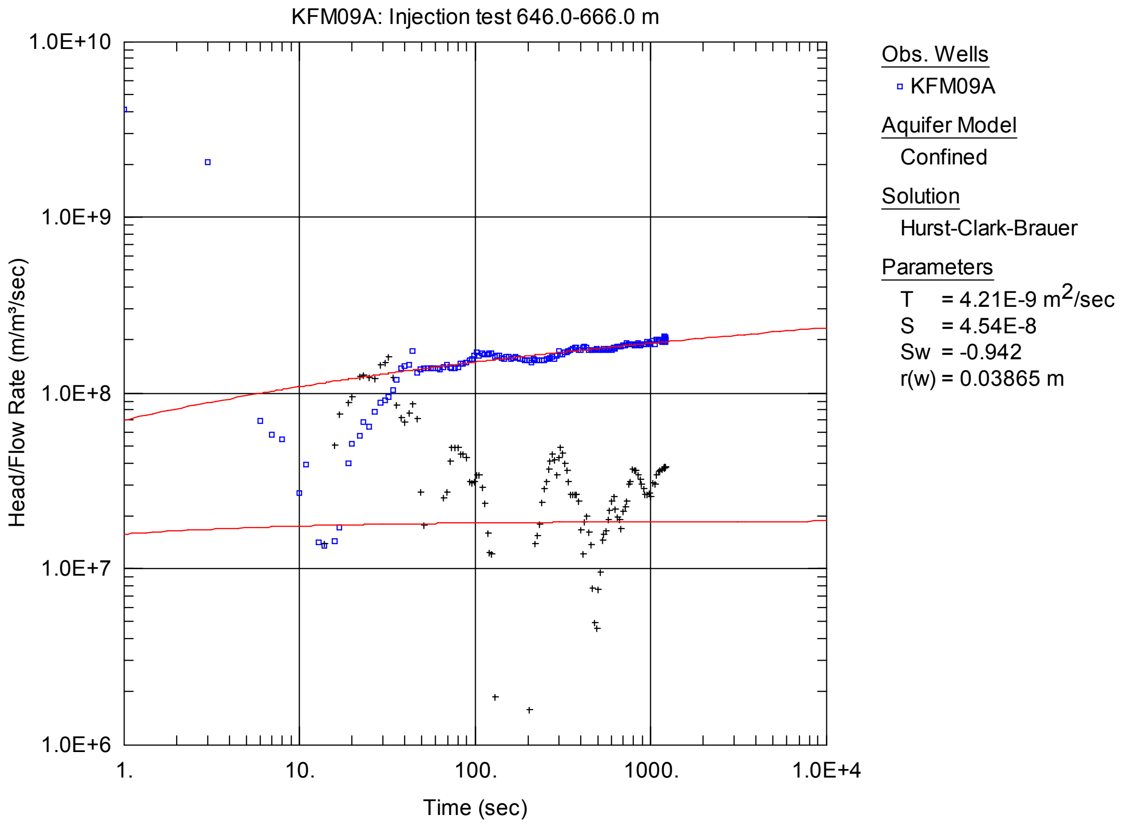


Figure A3-168. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 646.0-666.0 m in KFM09A.*

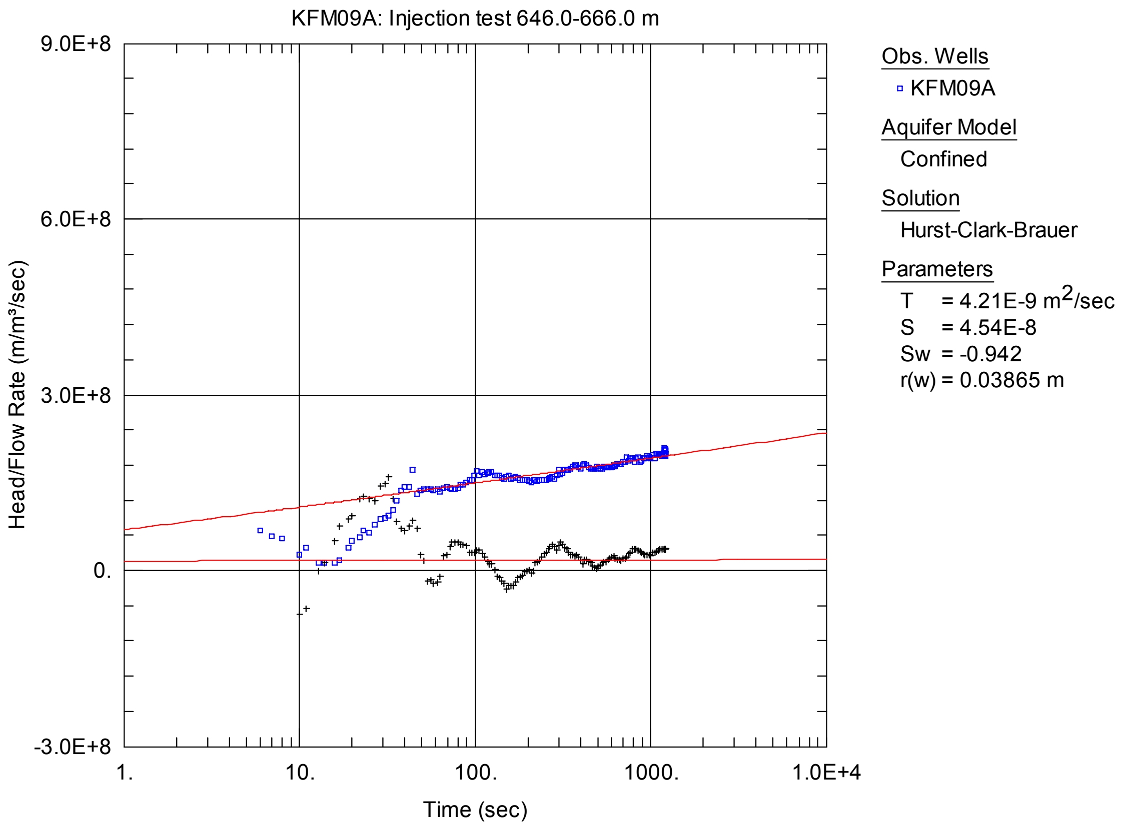


Figure A3-169. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 646.0-666.0m in KFM09A.*

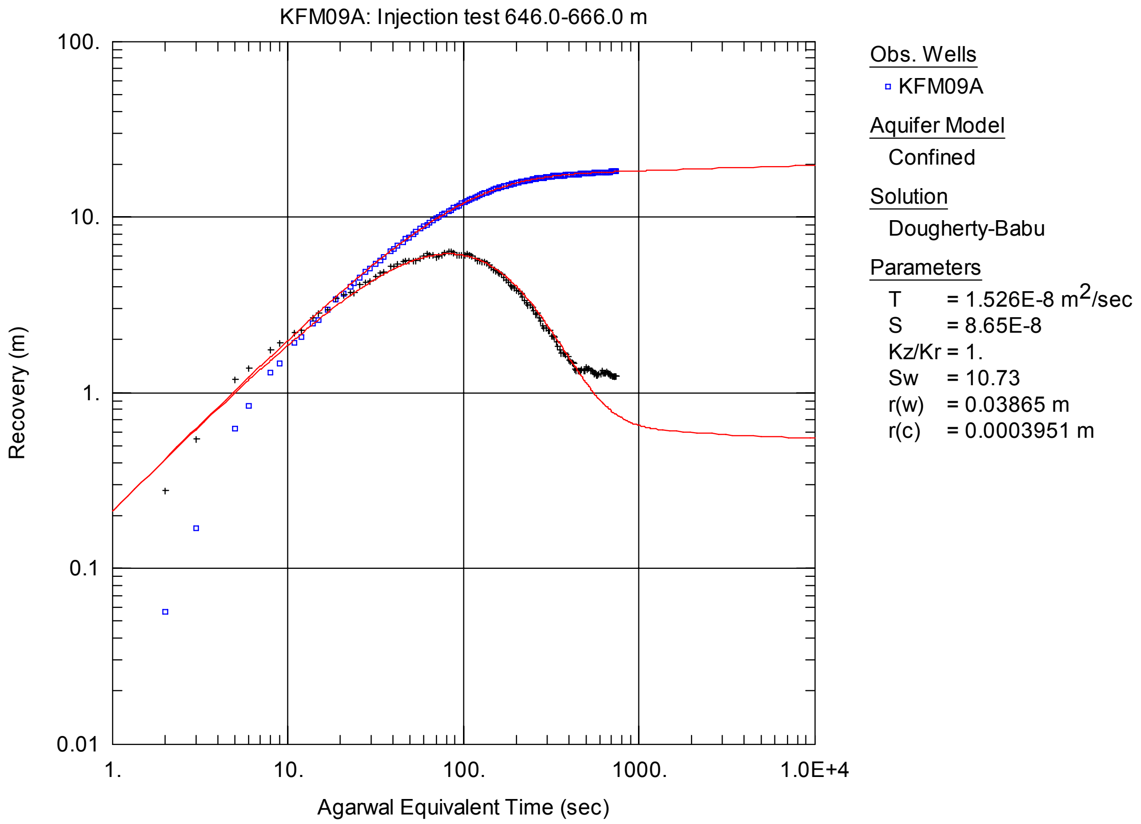


Figure A3-170. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 646.0-666.0 m in KFM09A.*

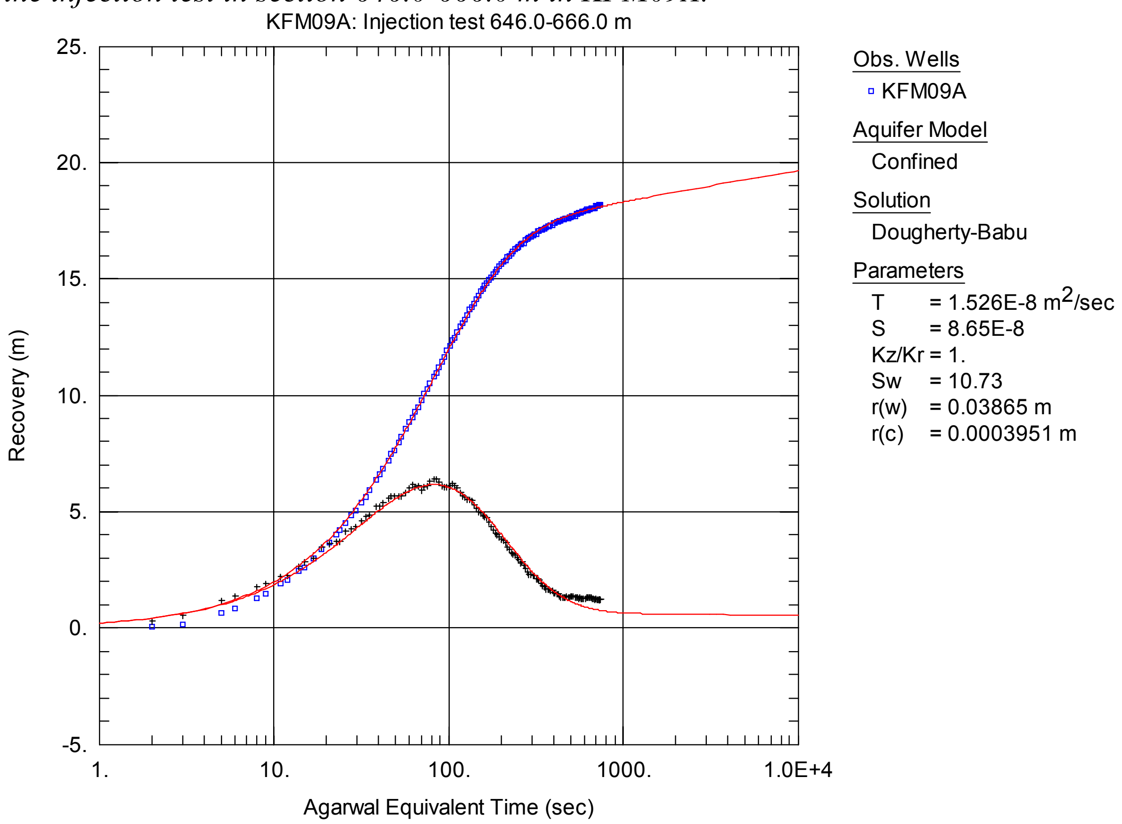


Figure A3-171. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 646.0-666.0 m in KFM09A.*

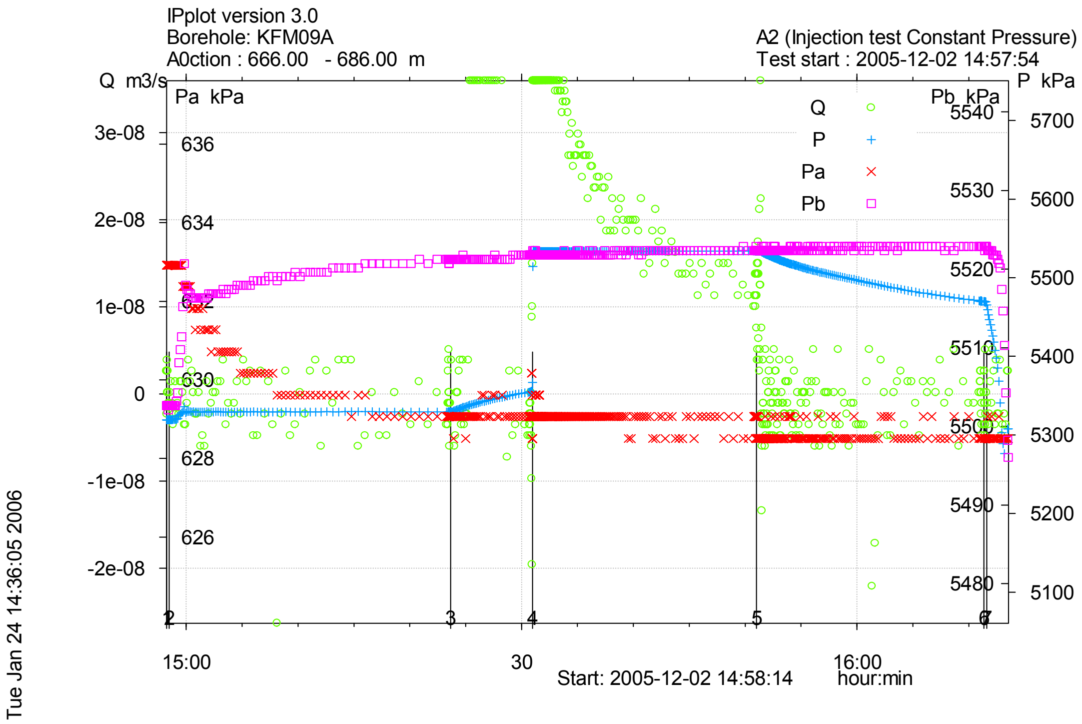


***Figure A3-172.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 666.0-686.0 m in borehole KFM09A.*

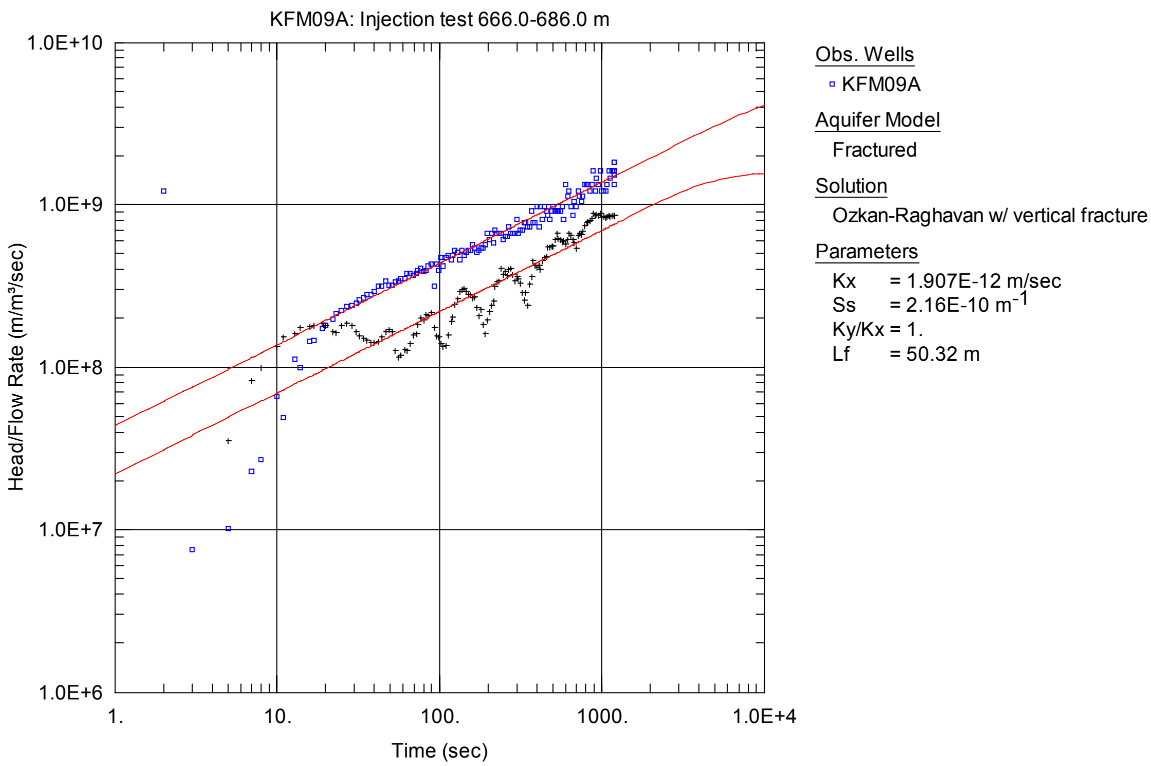


***Figure A3-173.** Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 666.0-686.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

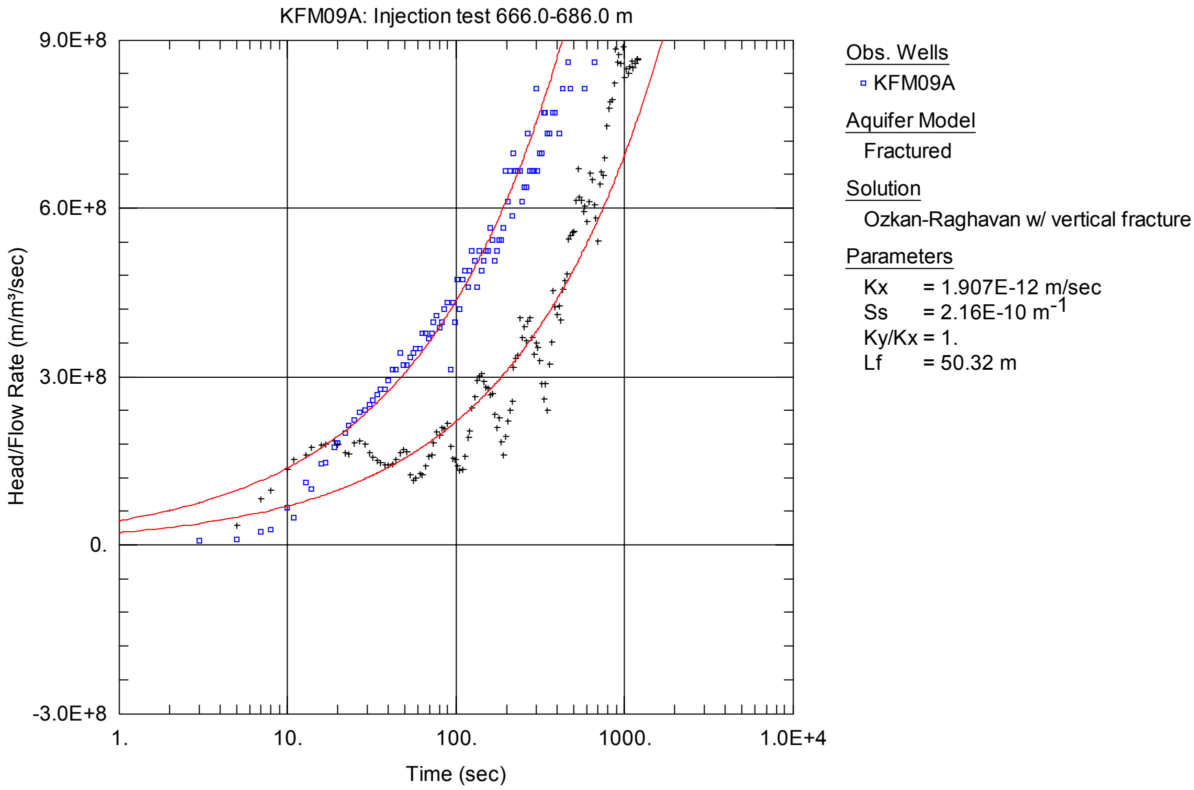


Figure A3-174. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 666.0-686.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

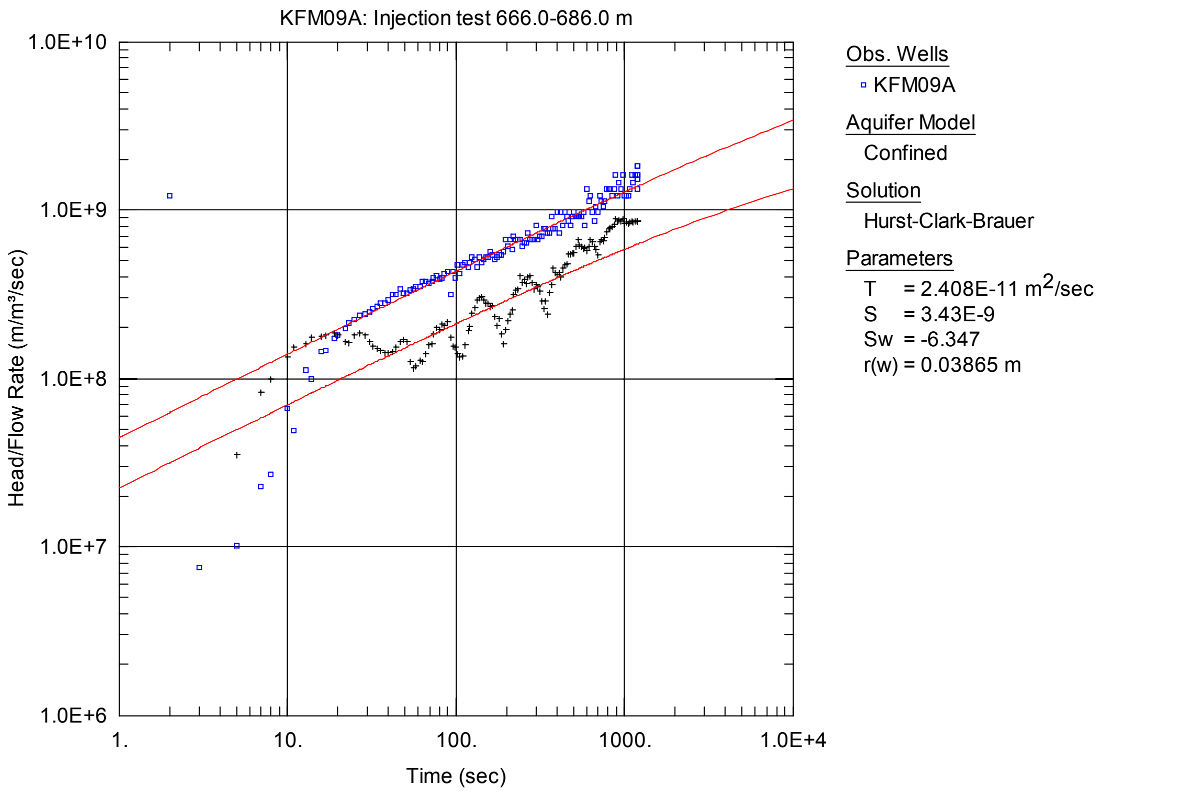


Figure A3-175. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 666.0-686.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for pseudo-radial flow.*

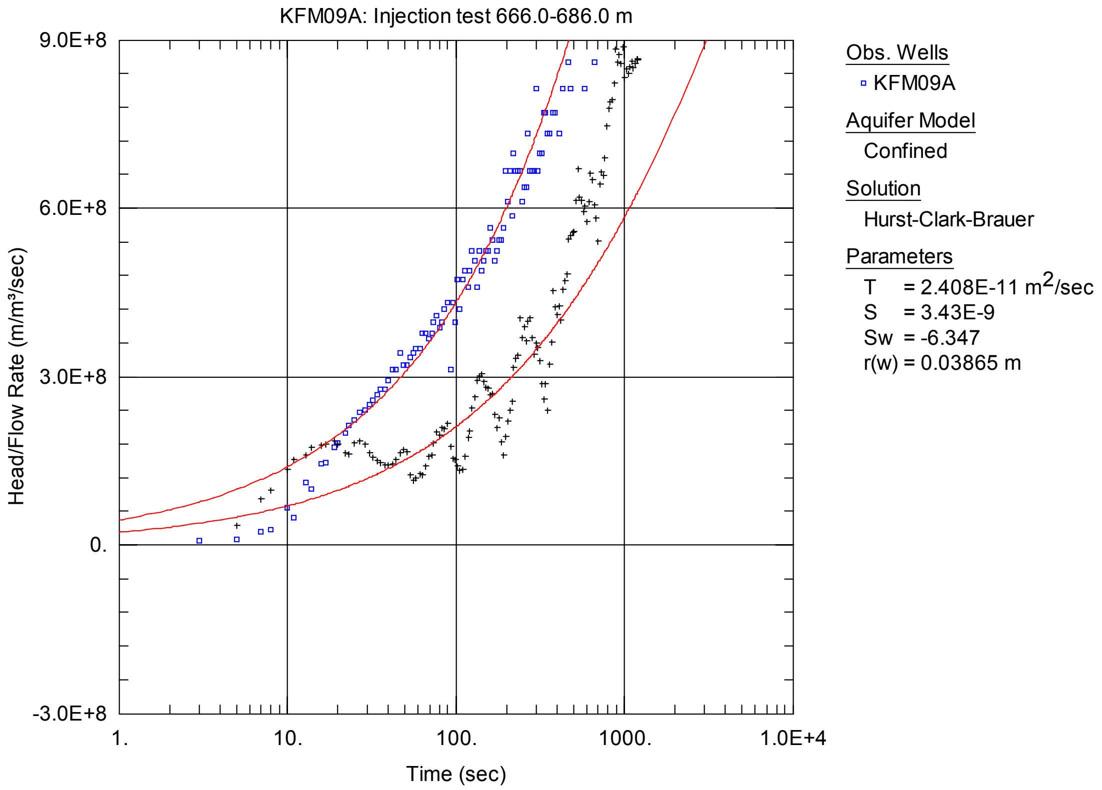


Figure A3-176. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 666.0-686.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for pseudo-radial flow.*

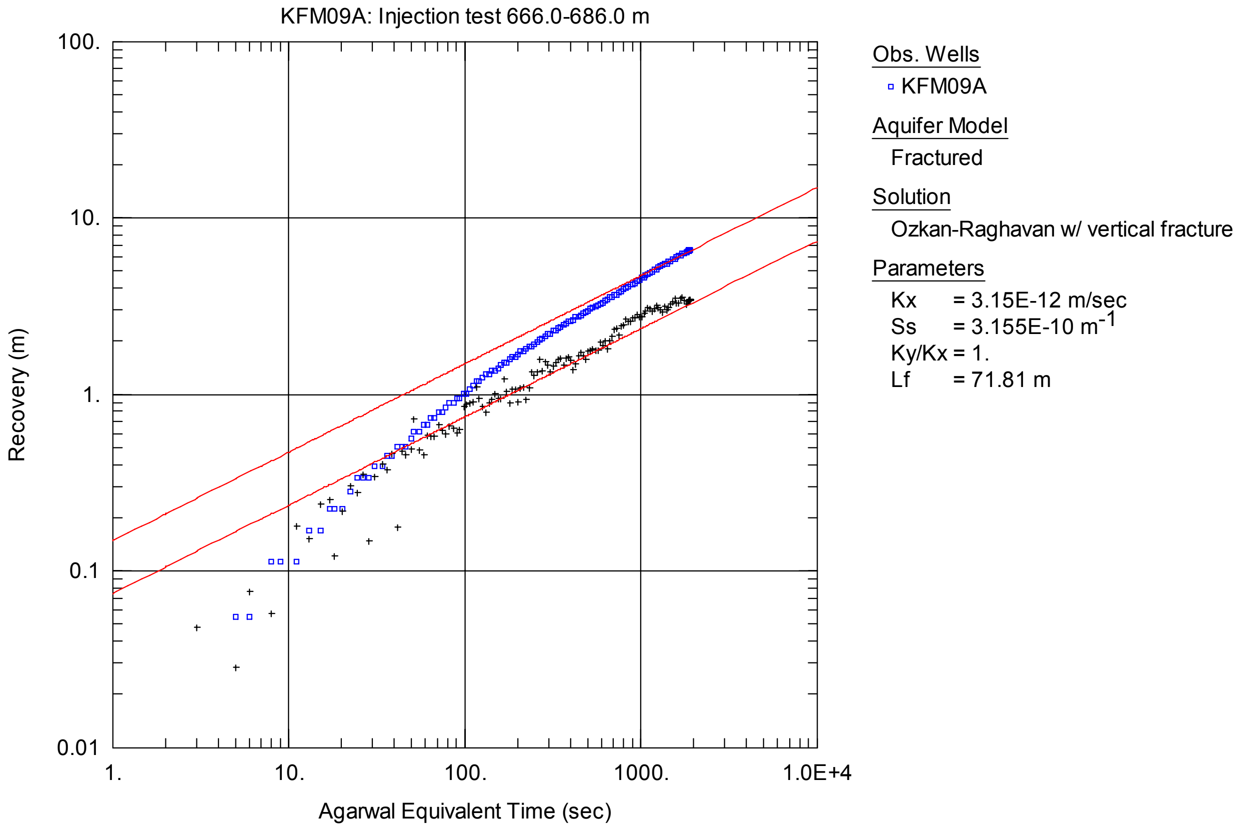


Figure A3-177. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 666.0-686.0 m in KFM09A.*

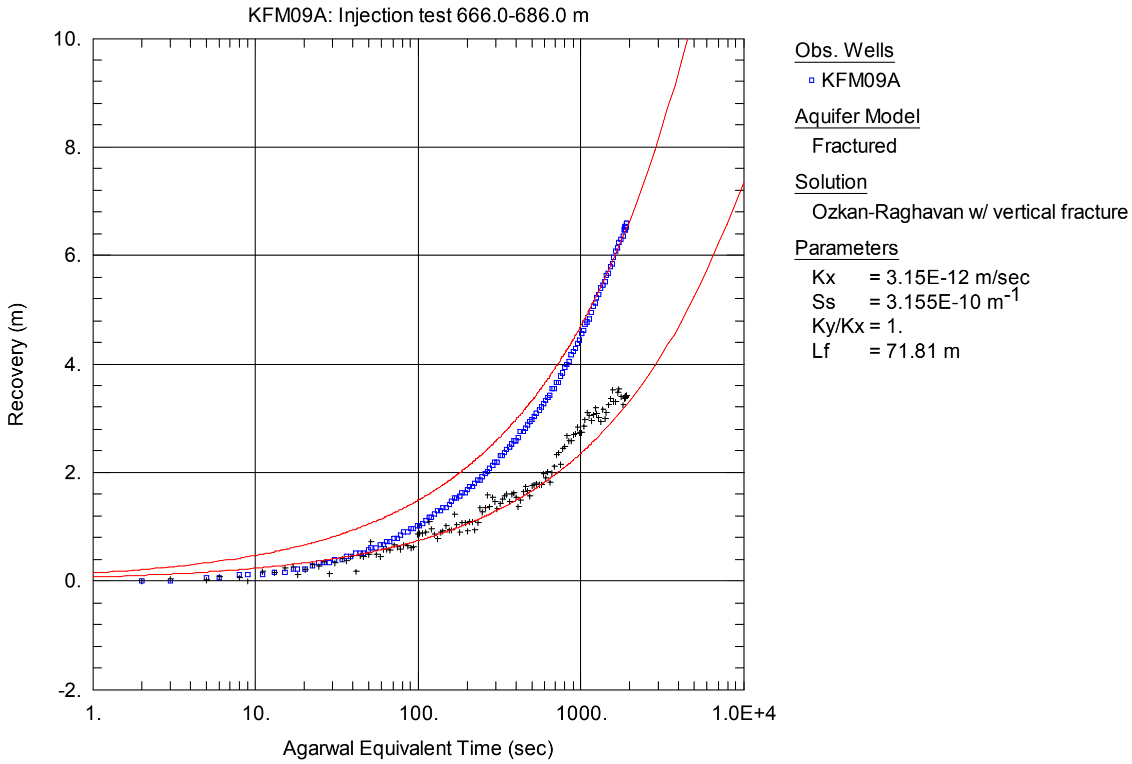


Figure A3-178. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 666.0-686.0 m in KFM09A.*

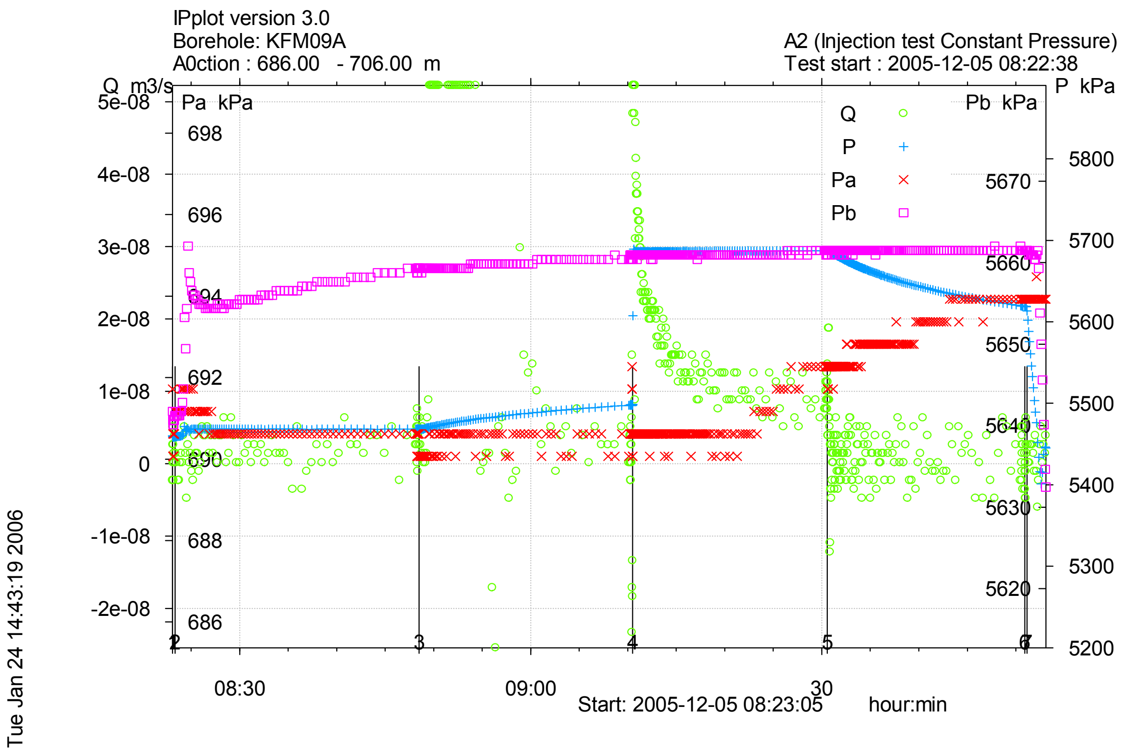


Figure A3-179. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 686.0-706.0 m in borehole KFM09A.*

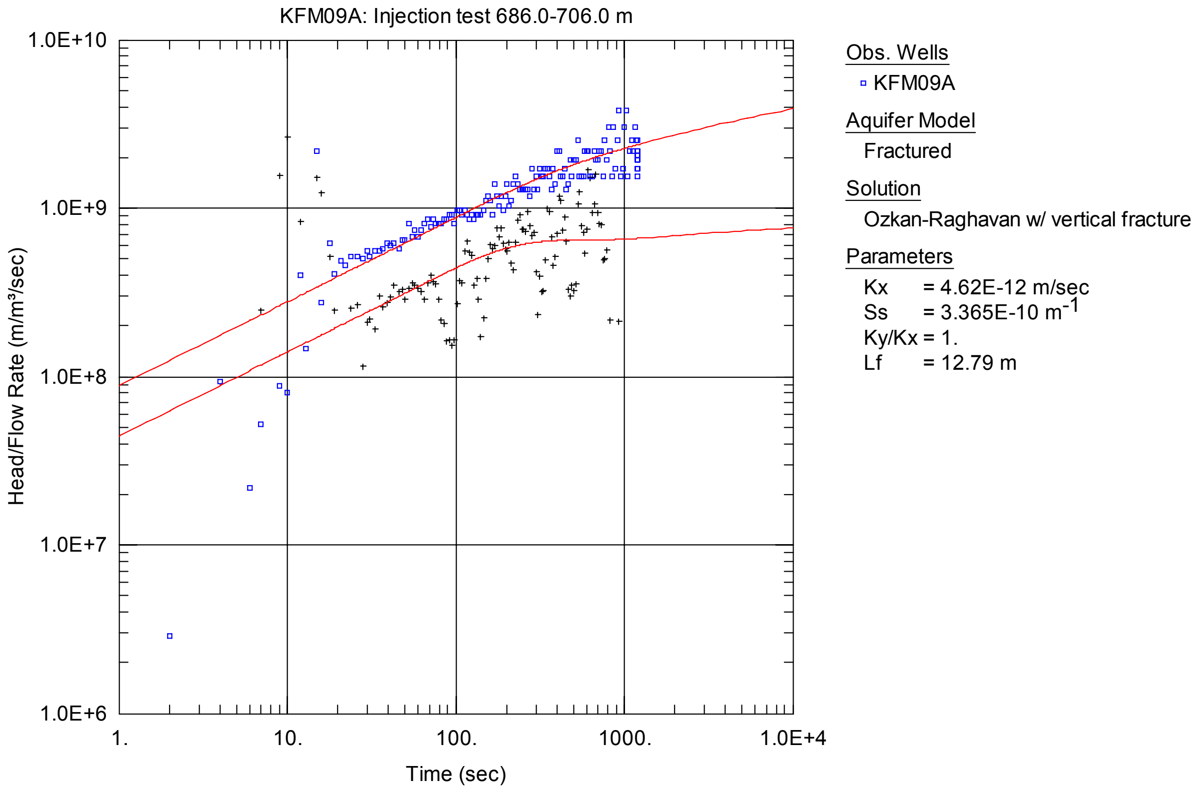


Figure A3-180. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 686.0-706.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

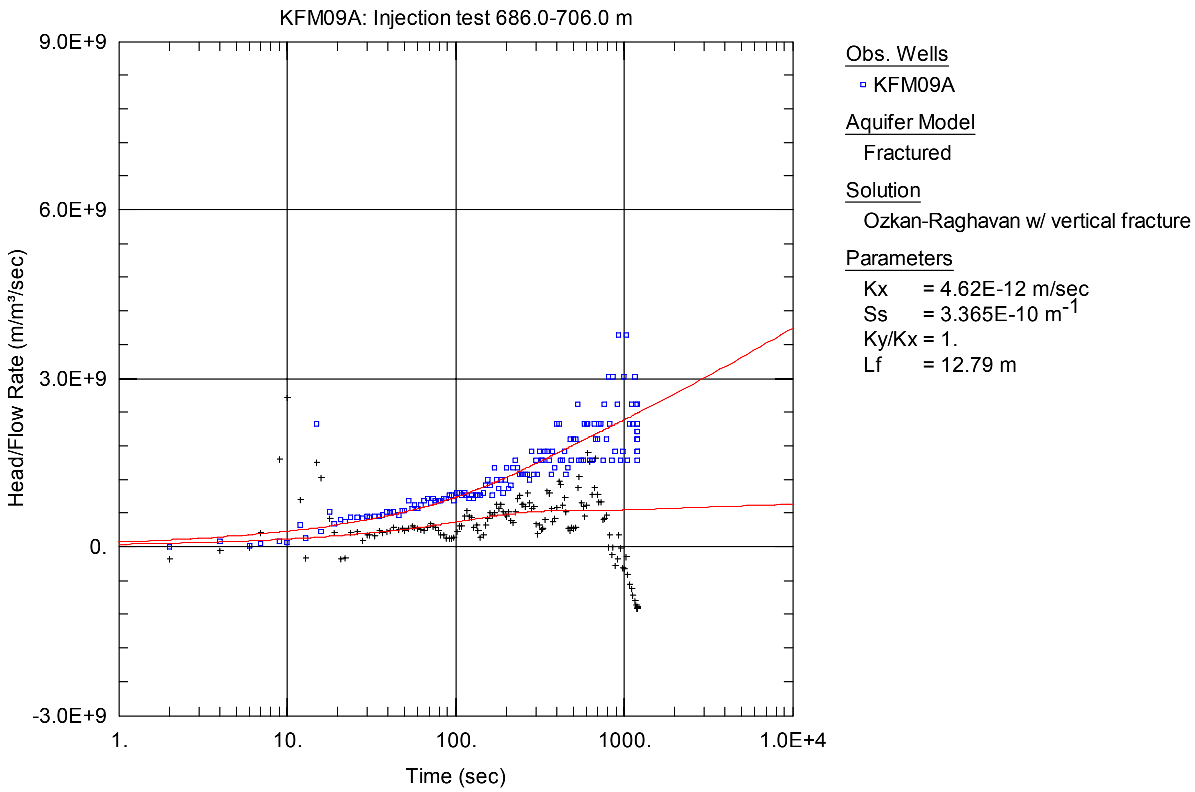


Figure A3-181. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 686.0-706.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

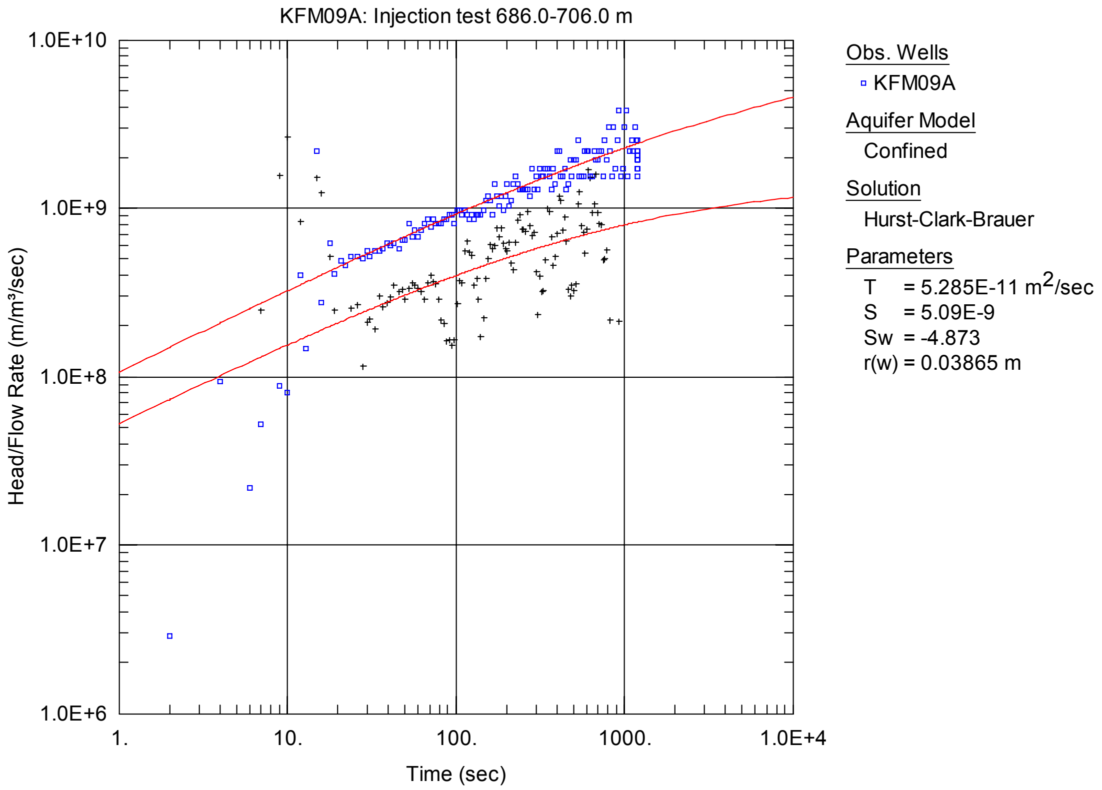


Figure A3-182. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 686.0-706.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for pseudo-radial flow.*

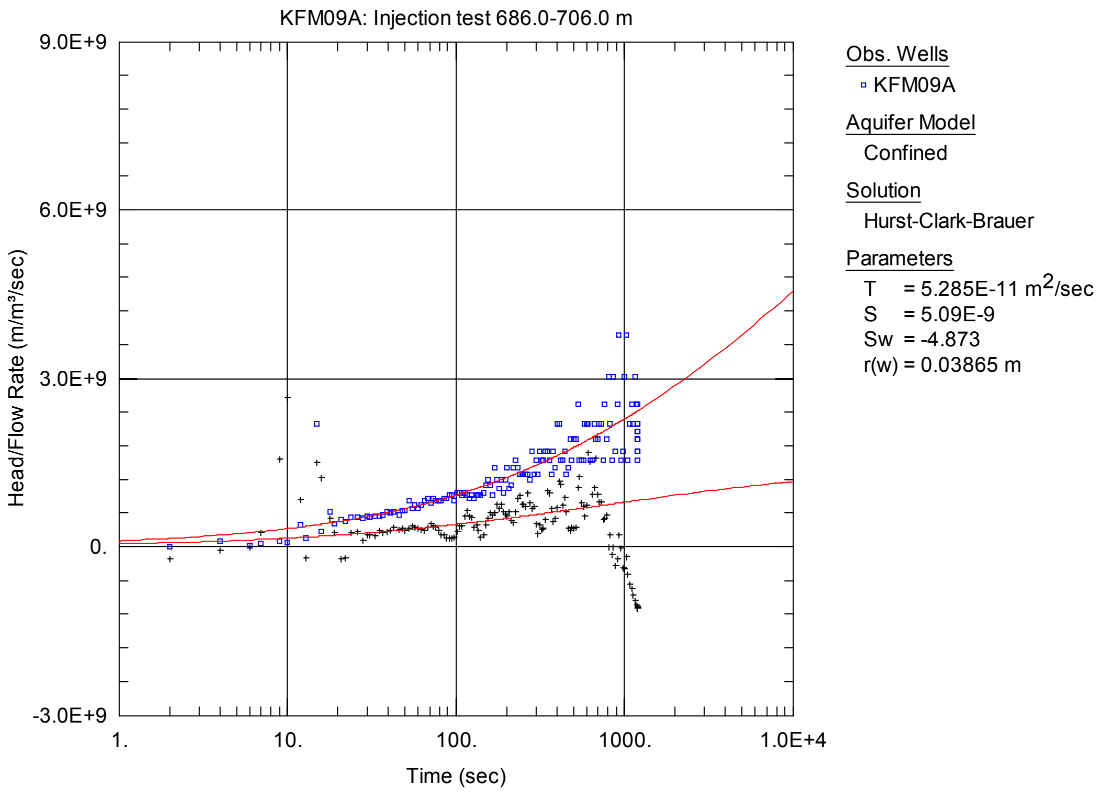


Figure A3-183. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 686.0-706.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for pseudo-radial flow.*

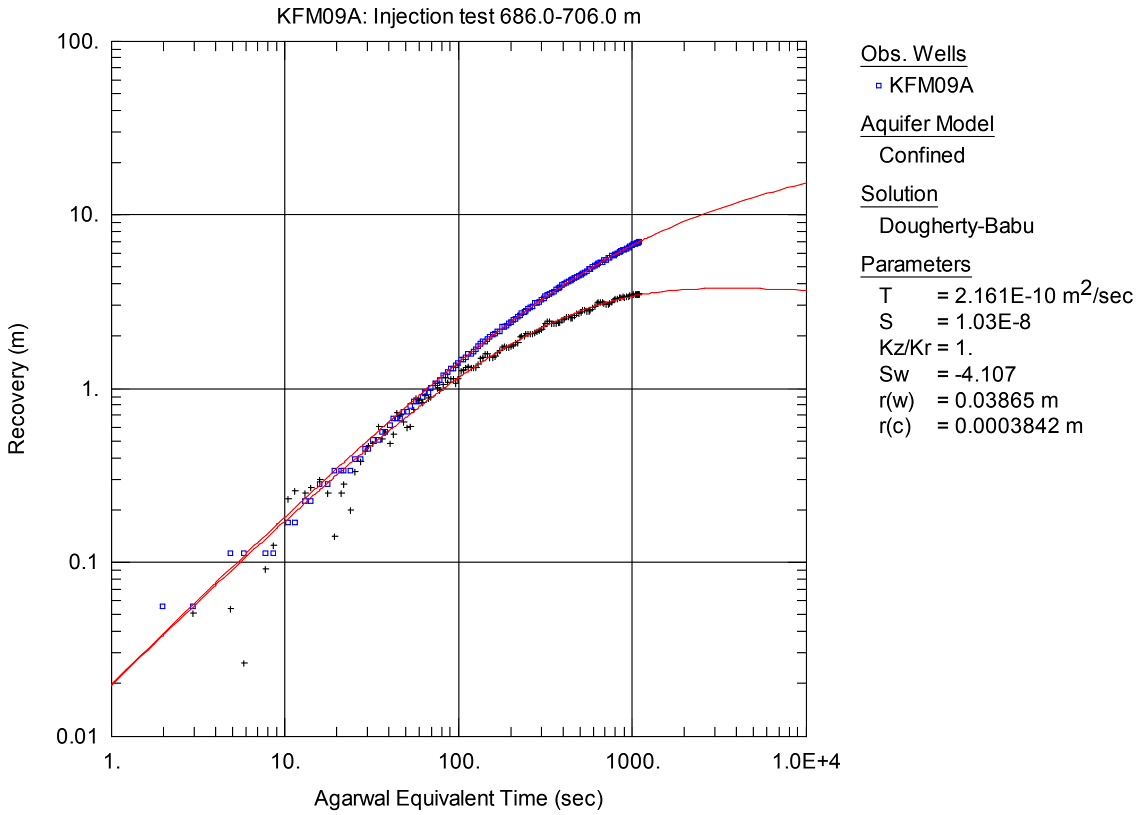


Figure A3-184. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 686.0-706.0m in KFM09A.*

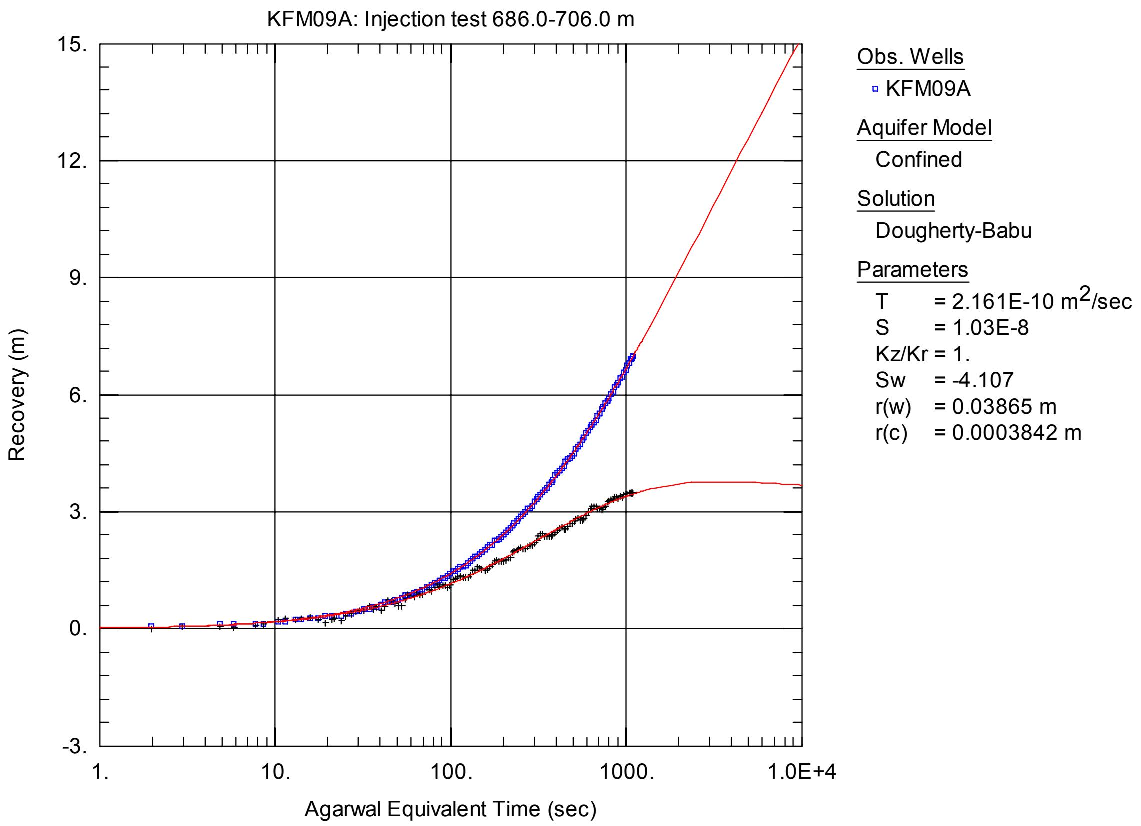


Figure A3-185. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 686.0-706.0 m in KFM09A.*

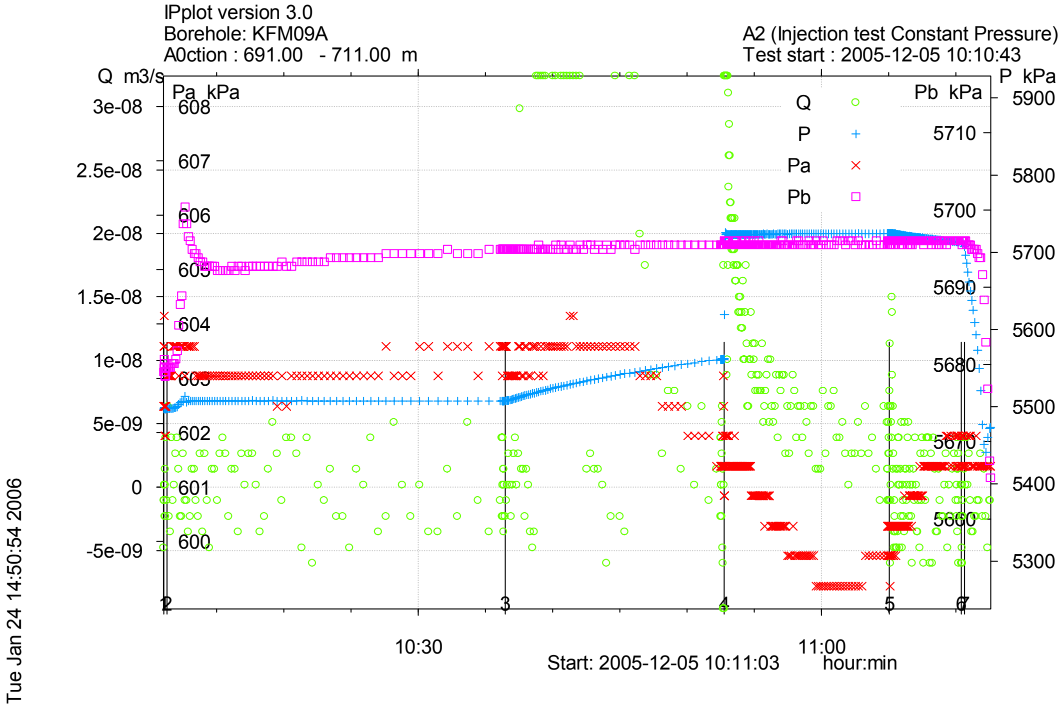


Figure A3-186. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 691.0-711.0 m in borehole KFM09A.*

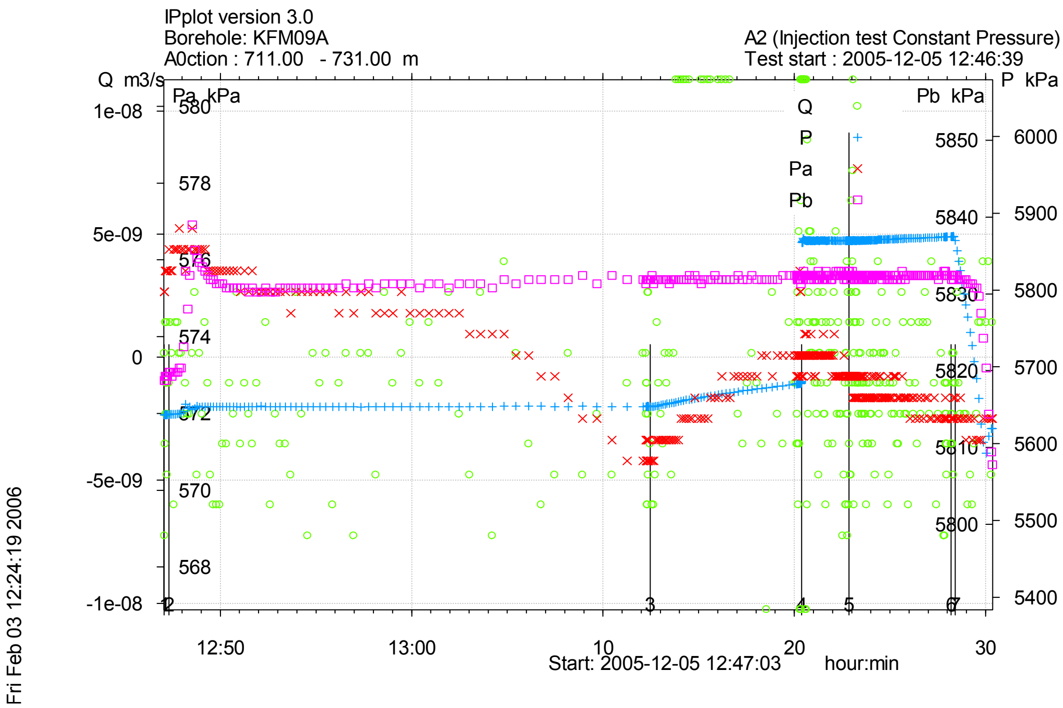


Figure A3-187. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 711.0-731.0 m in borehole KFM09A.*

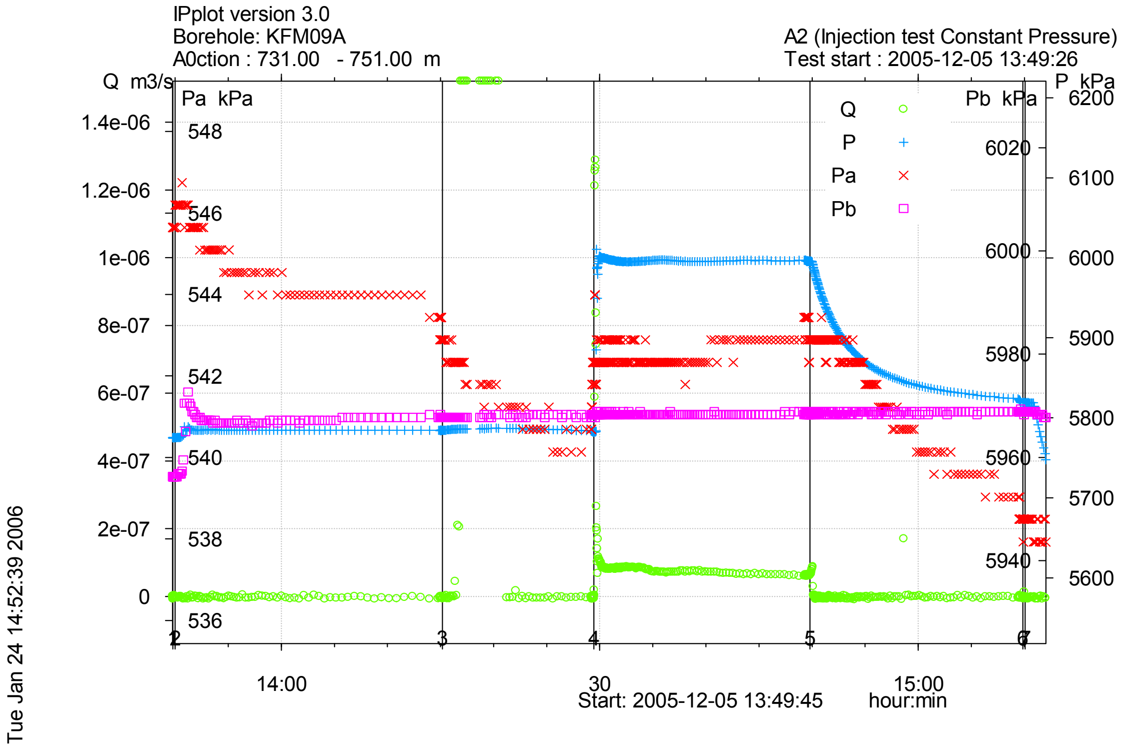


Figure A3-188. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 731.0-751.0 m in borehole KFM09A.*

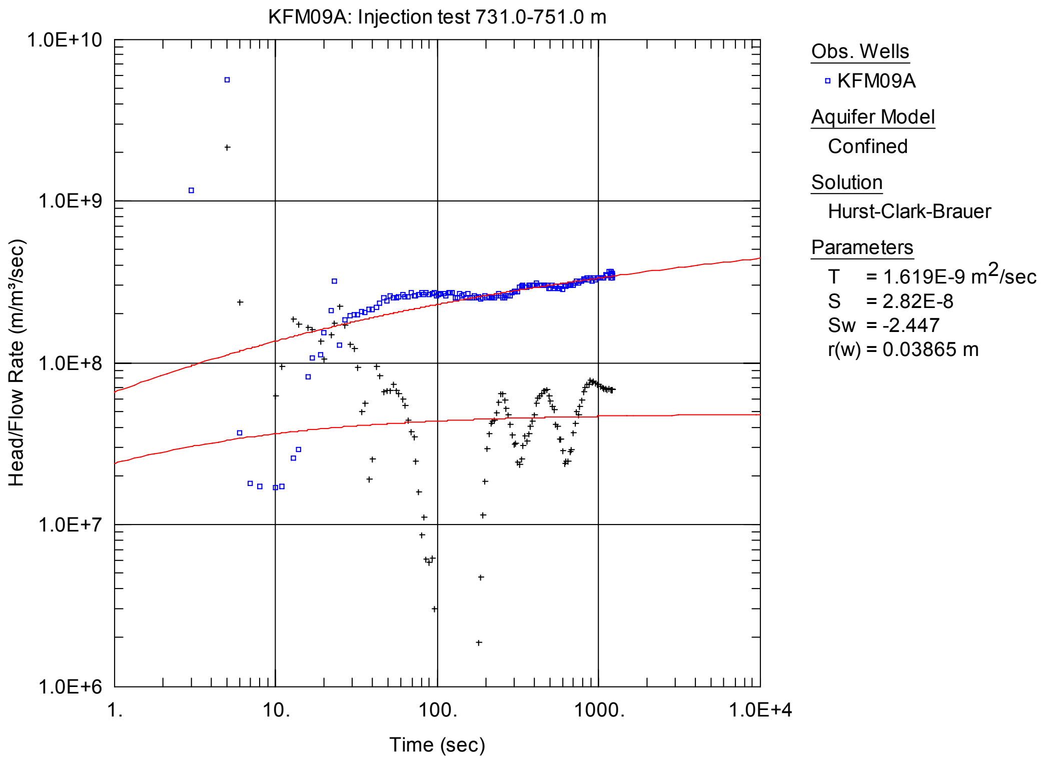


Figure A3-189. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 731.0-751.0 m in KFM09A.*

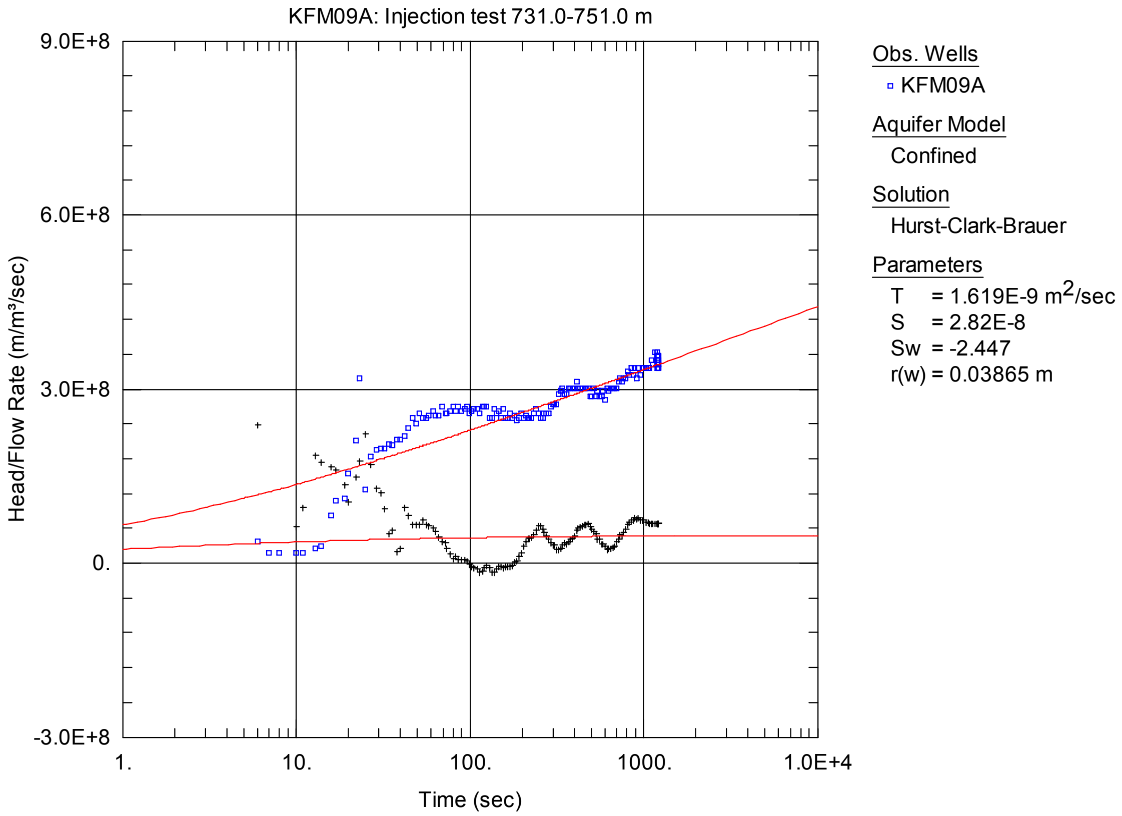


Figure A3-190. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 731.0-751.0 m in KFM09A.*

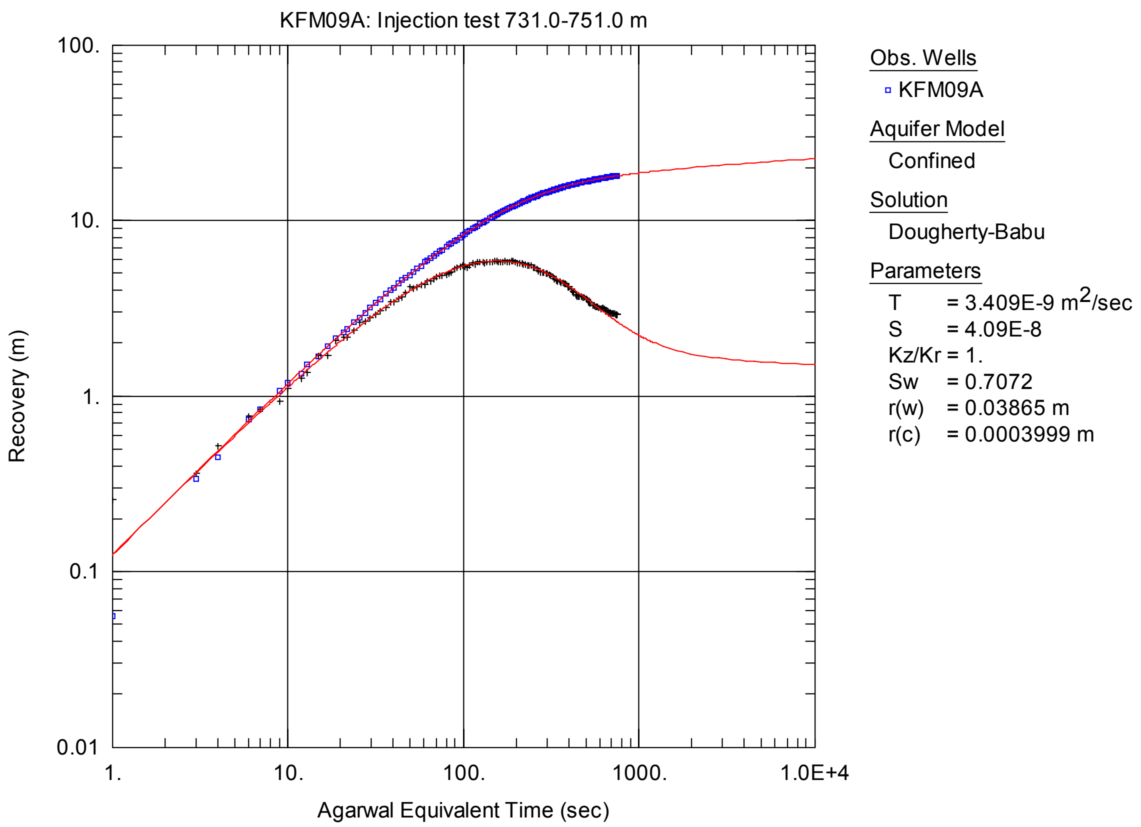


Figure A3-191. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in 731.0-751.0 m in KFM09A.*

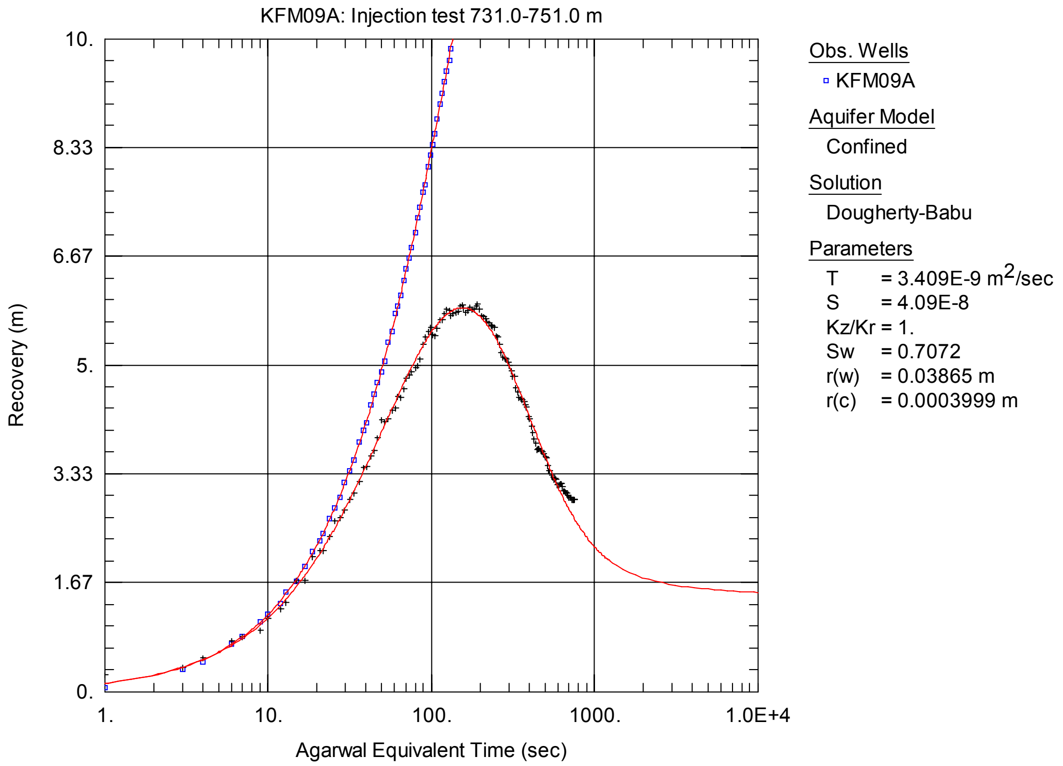


Figure A3-192. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 731.0-751.0 m in KFM09A.*

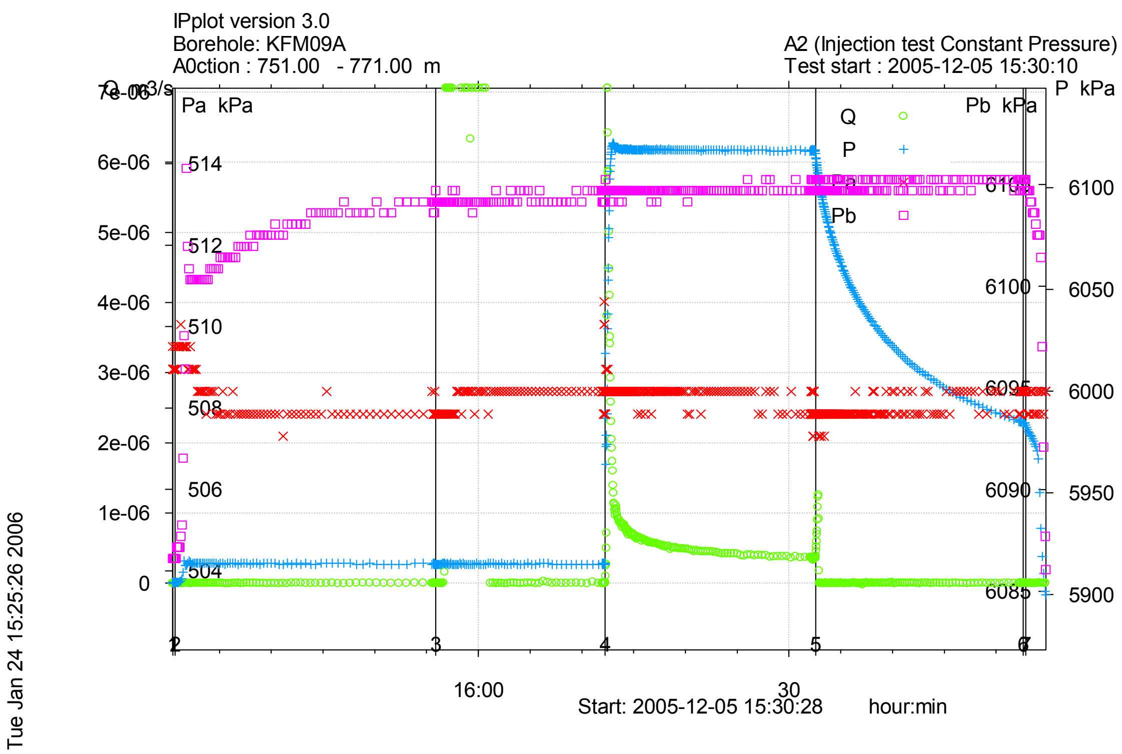


Figure A3-193. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 751.0-771.0 m in borehole KFM09A.*

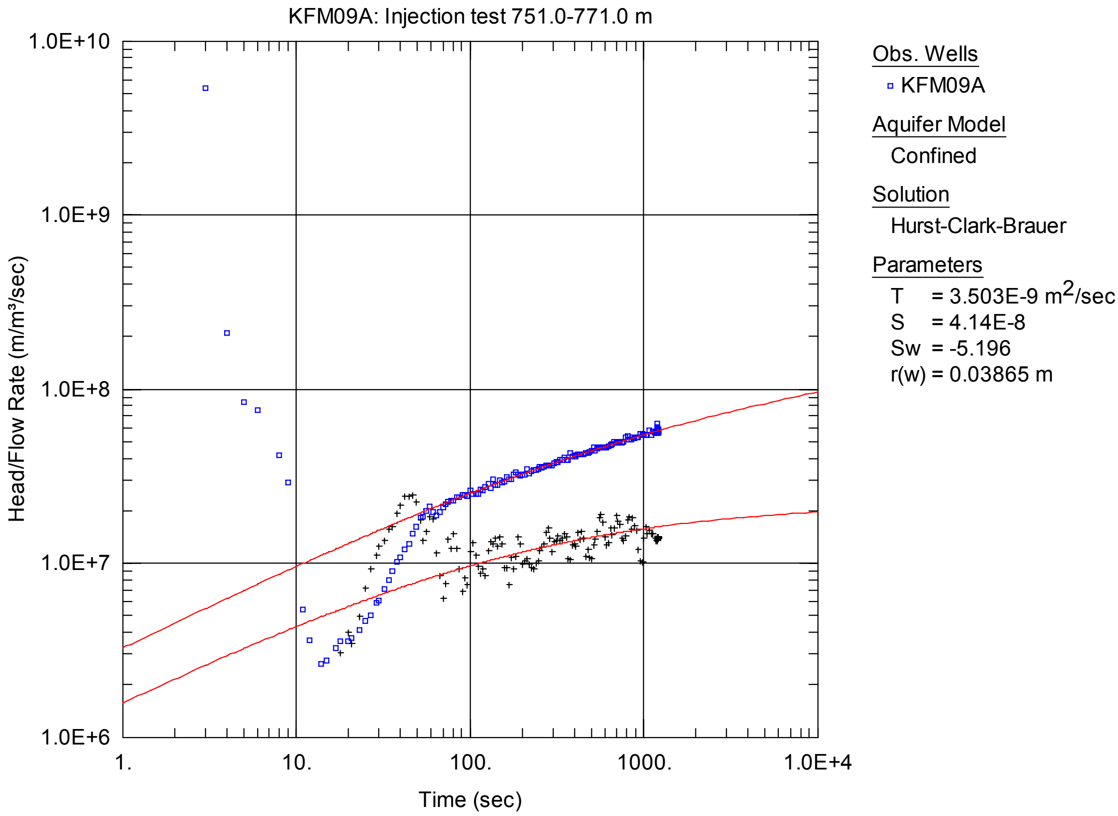


Figure A3-194. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 751.0-771.0 m in KFM09A.*

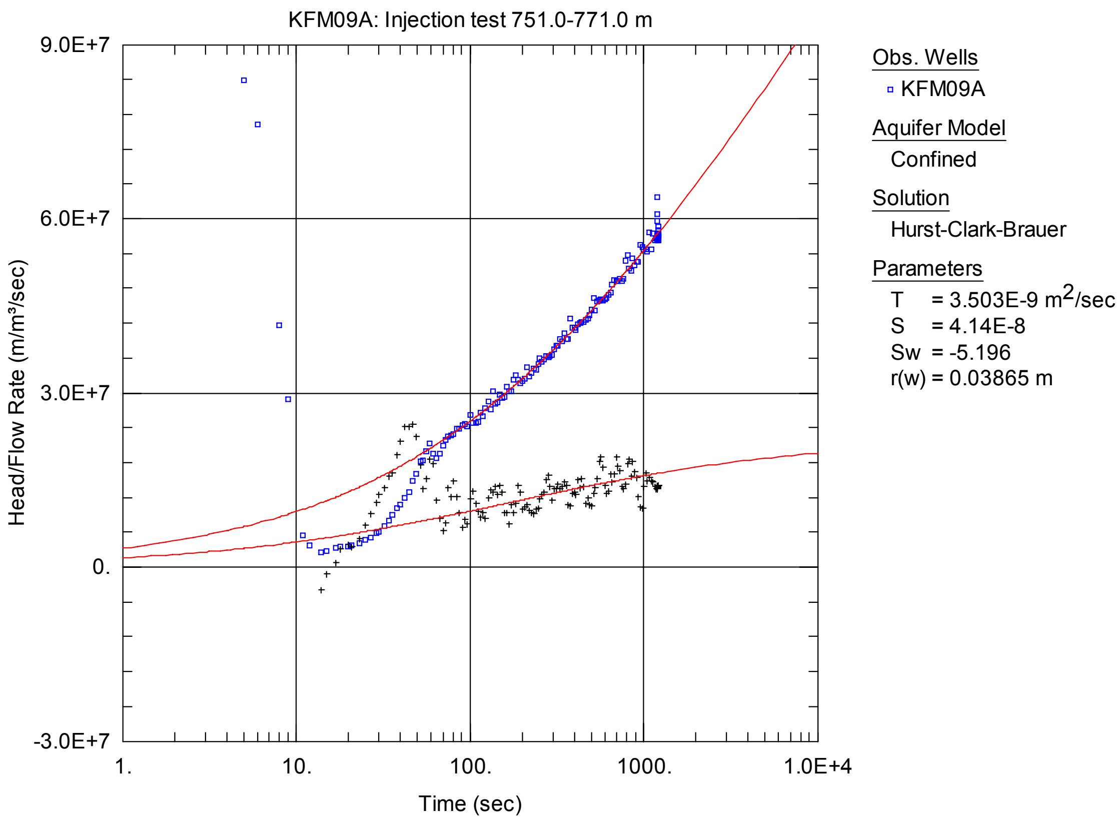


Figure A3-195. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in 751.0-771.0 m in KFM09A.*

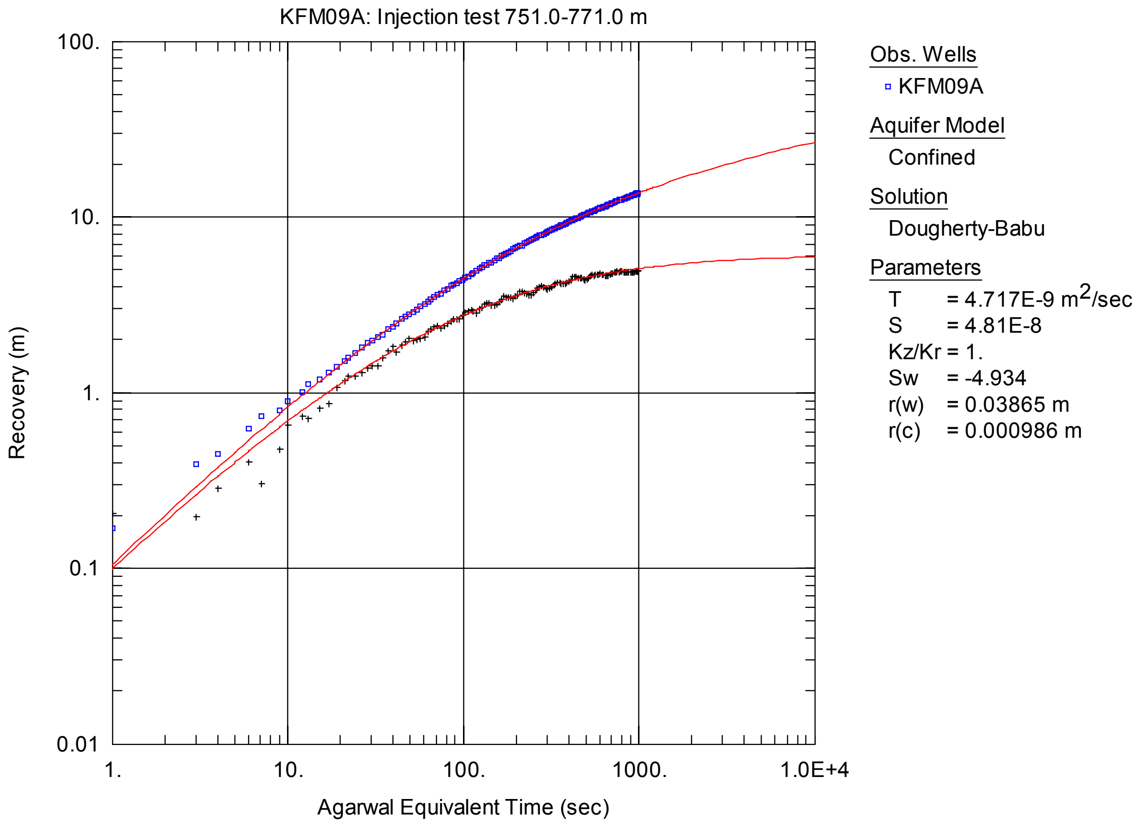


Figure A3-196. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 751.0-771.0 m in KFM09A.*

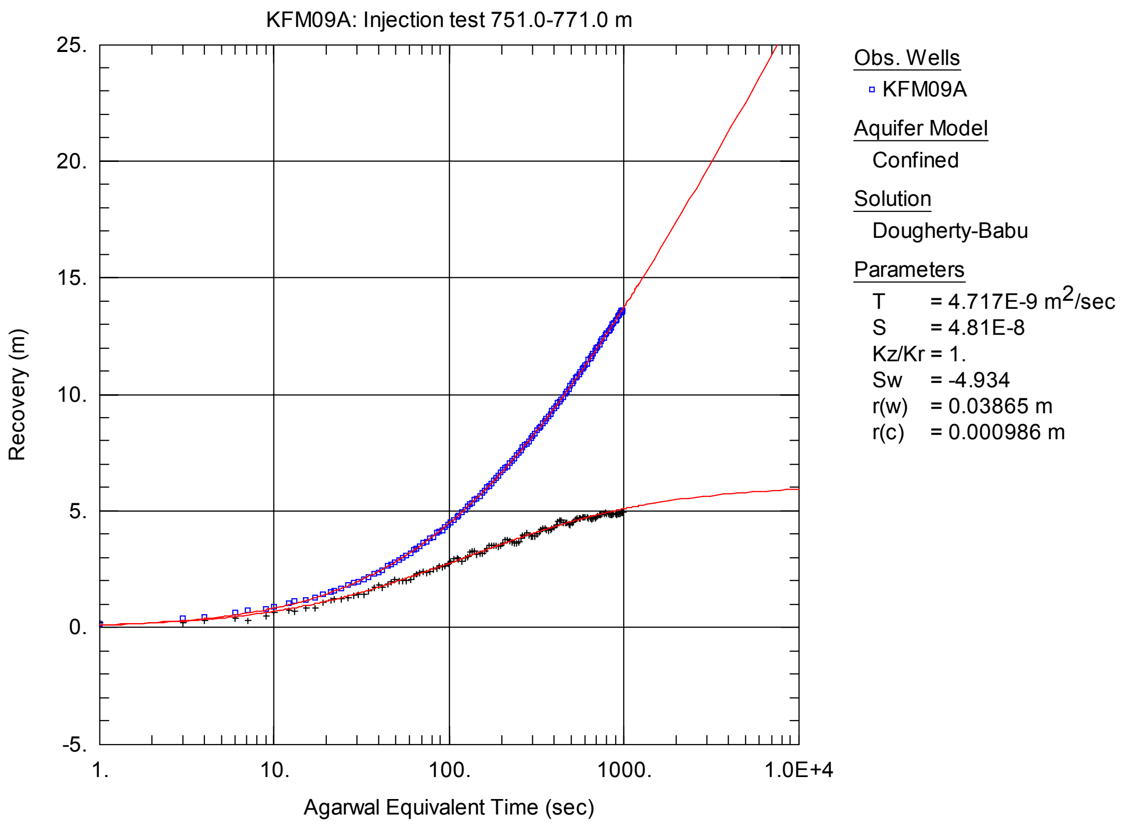


Figure A3-197. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 751.0-771.0 m in KFM09A.*

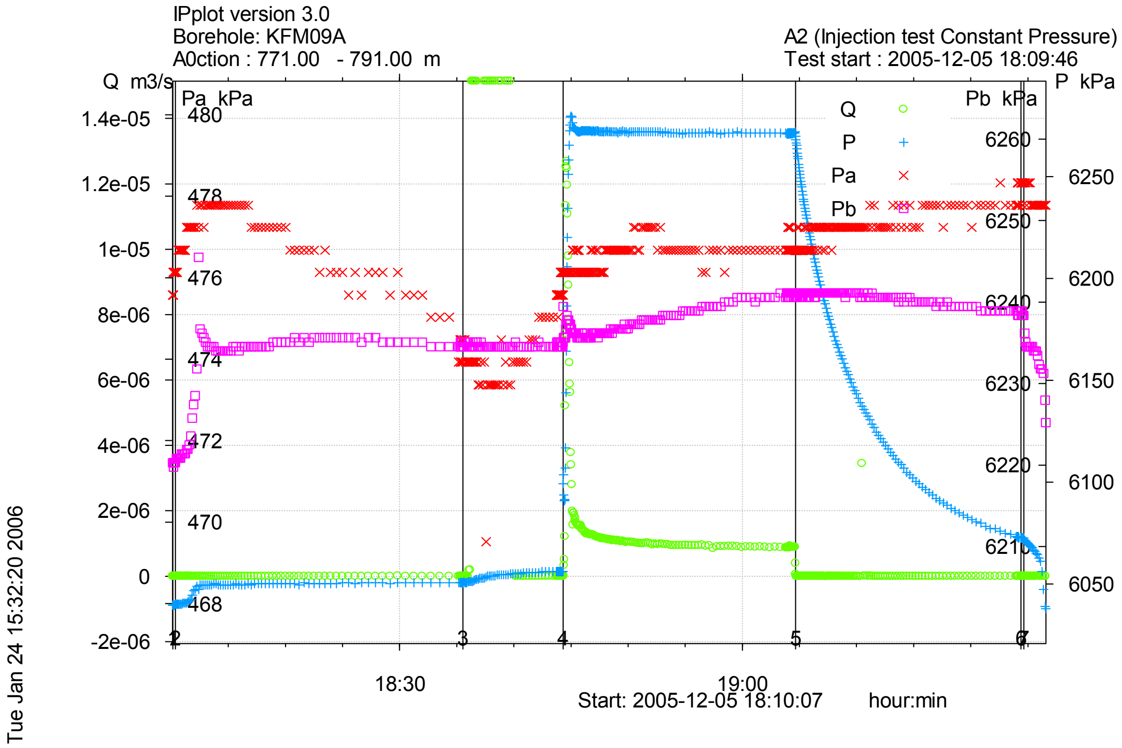


Figure A3-198. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 771.0-791.0 m in borehole KFM09A.*

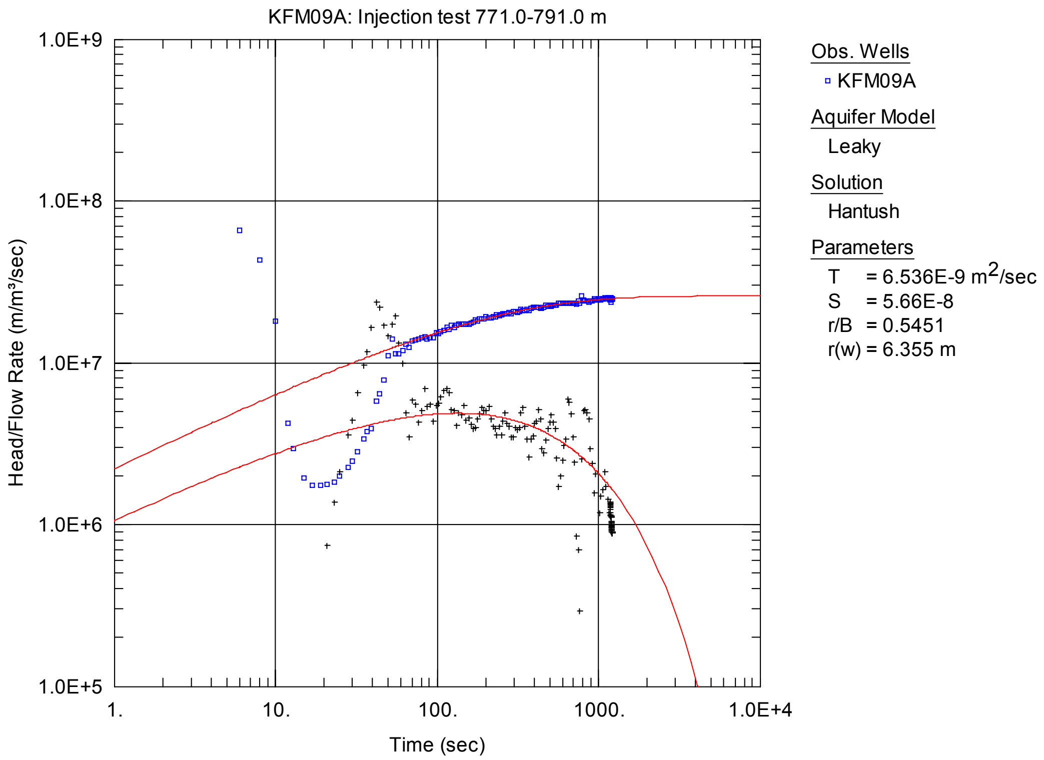


Figure A3-199. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 771.0-791.0 m in KFM09A.*

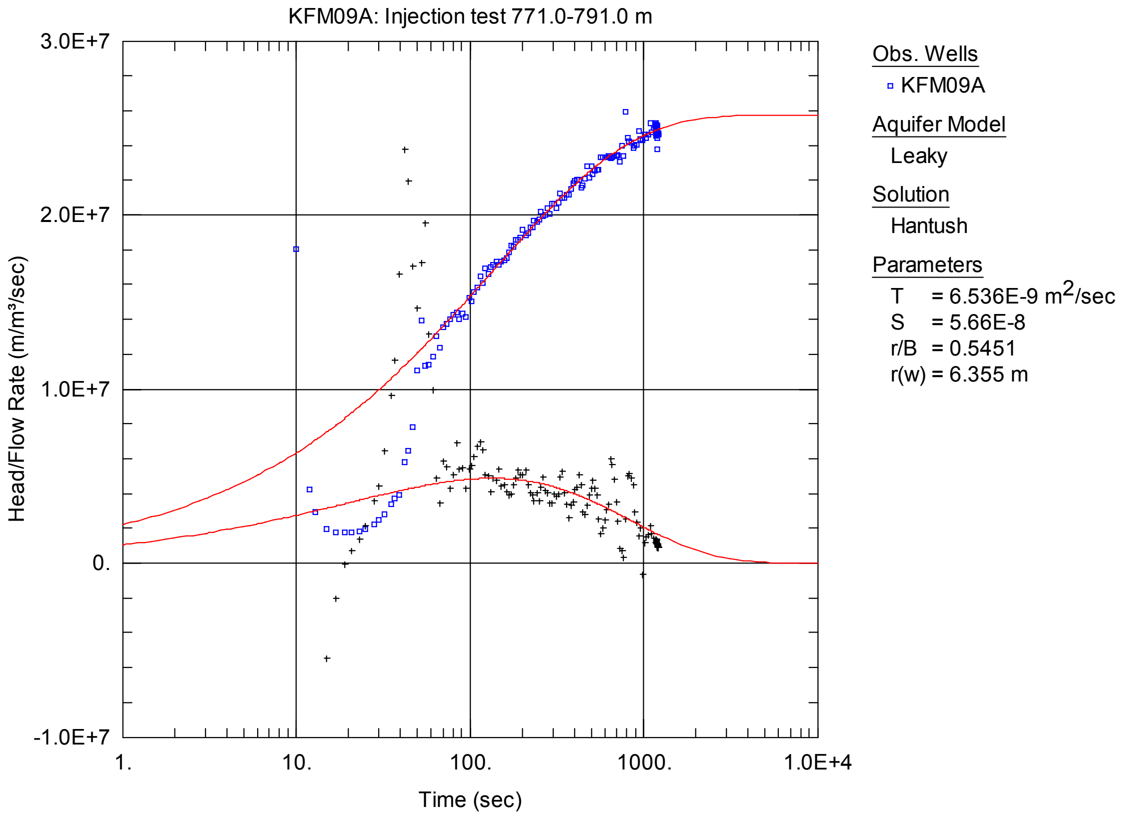


Figure A3-200. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 771.0-791.0 m in KFM09A.*

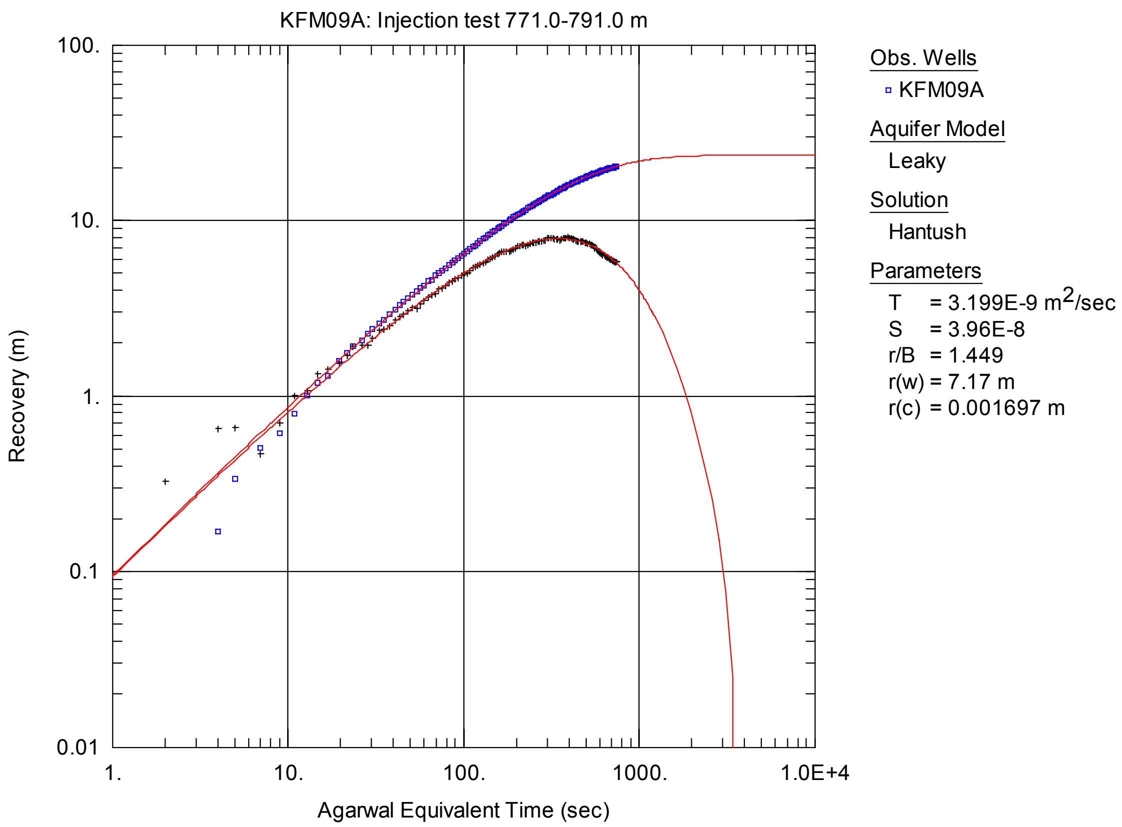


Figure A3-201. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 771.0-791.0 m in KFM09A.*

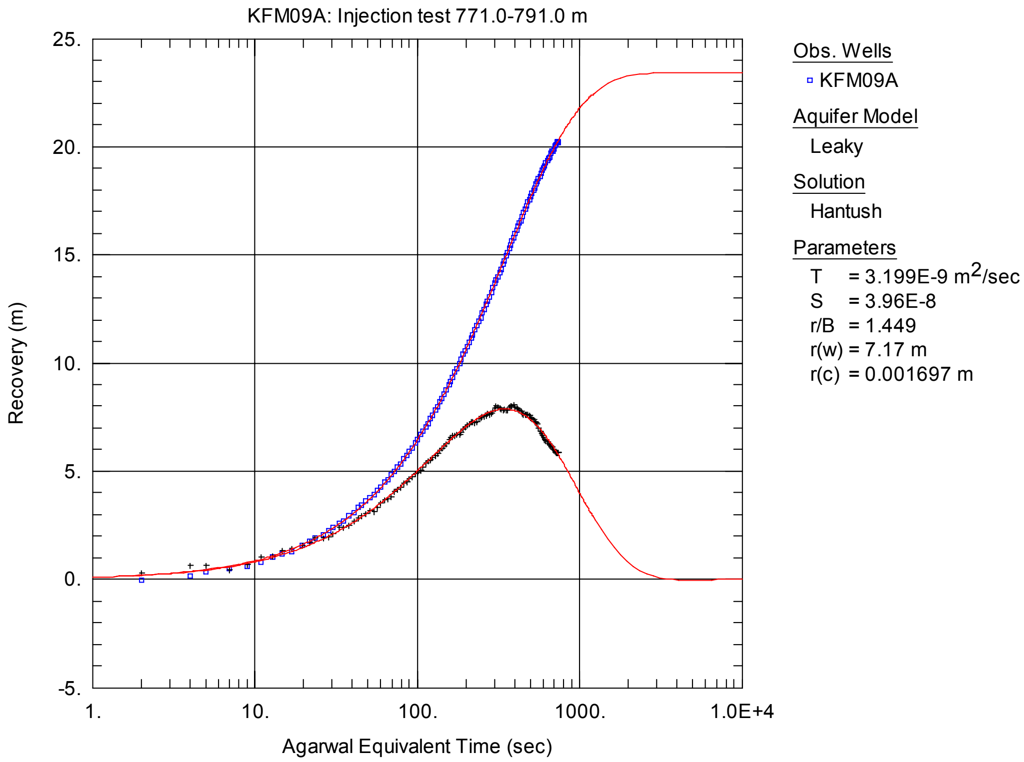


Figure A3-202. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 771.0-791.0 m in KFM09A.*

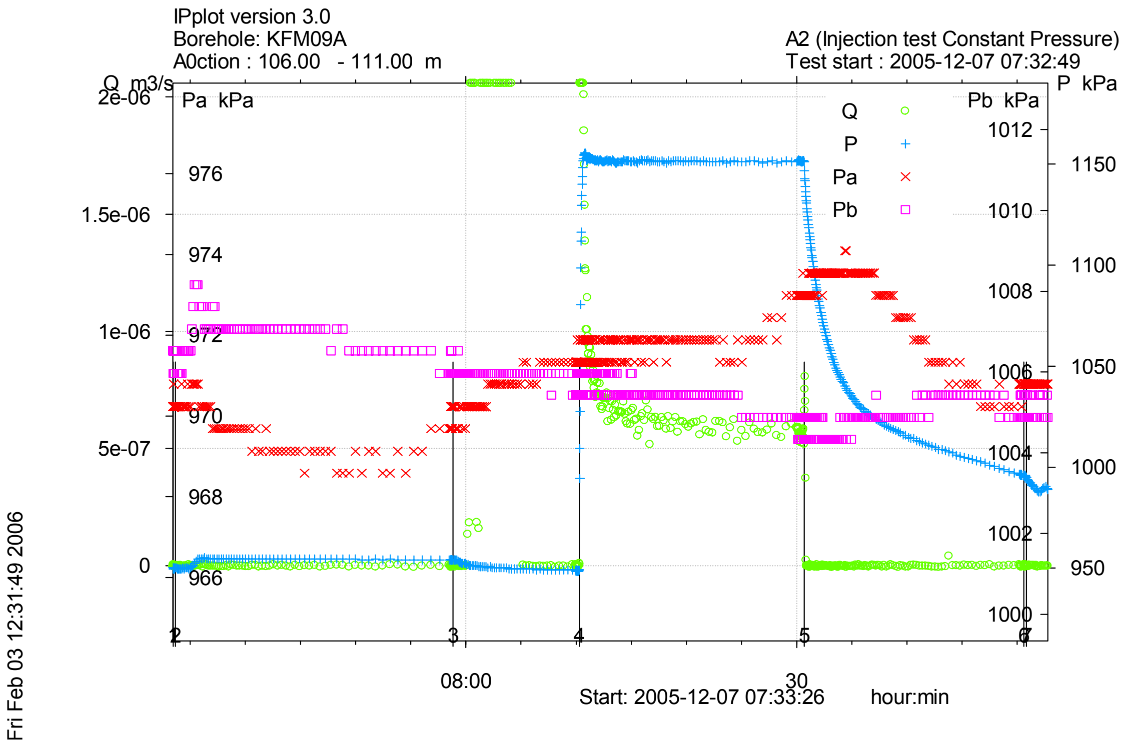


Figure A3-203. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 106.0-111.0 m in borehole KFM09A.*

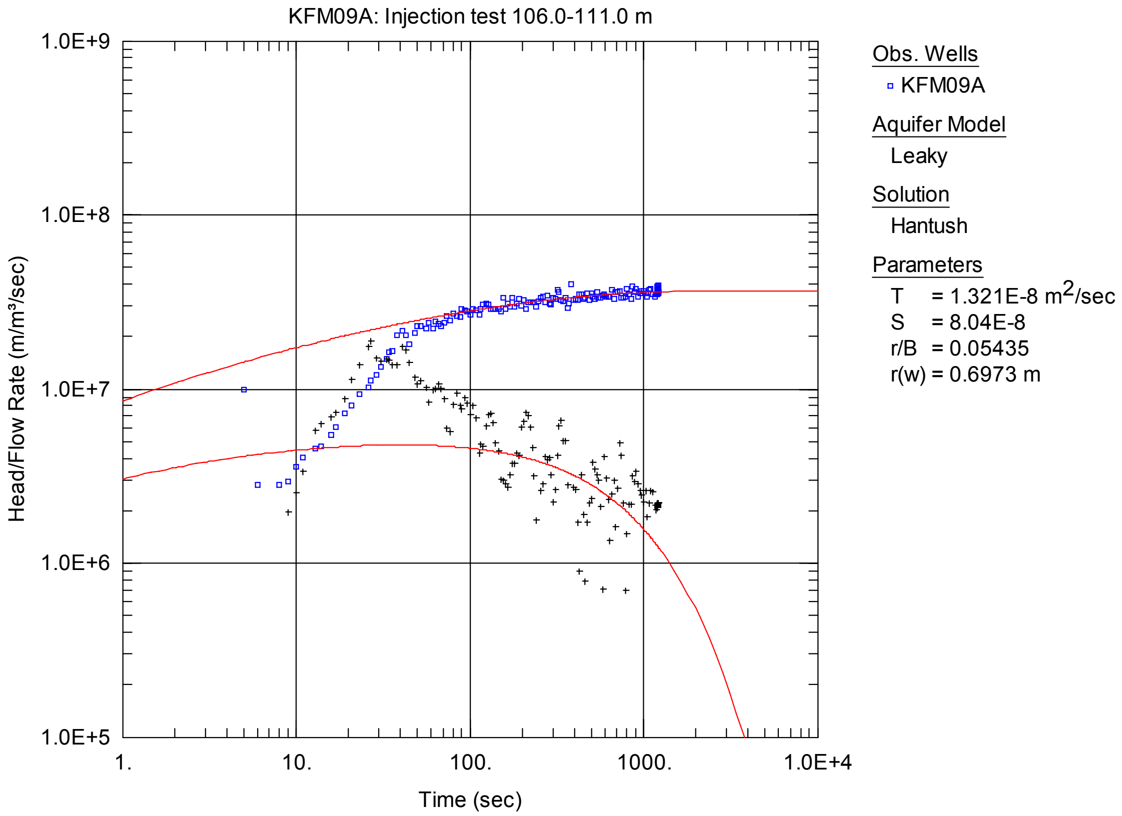


***Figure A3-204.** Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 106.0-111.0 m in KFM09A.*

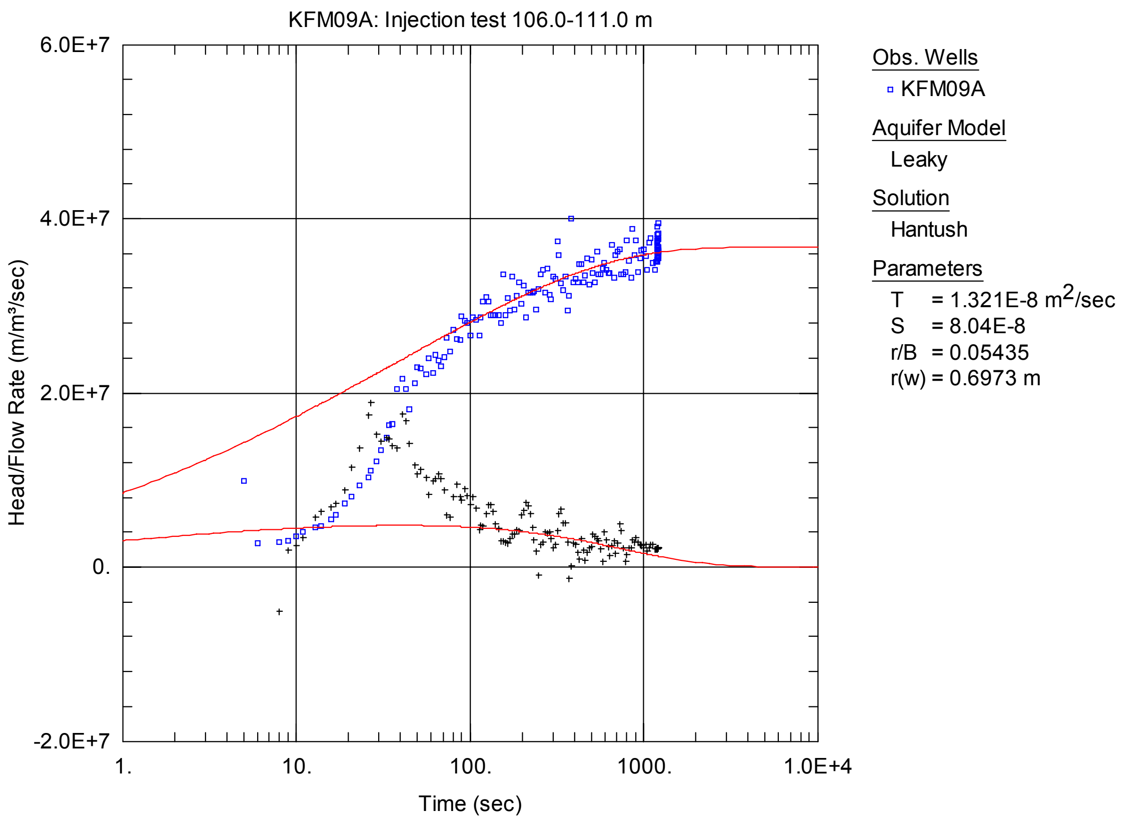


***Figure A3-205.** Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 106.0-111.0 m in KFM09A.*

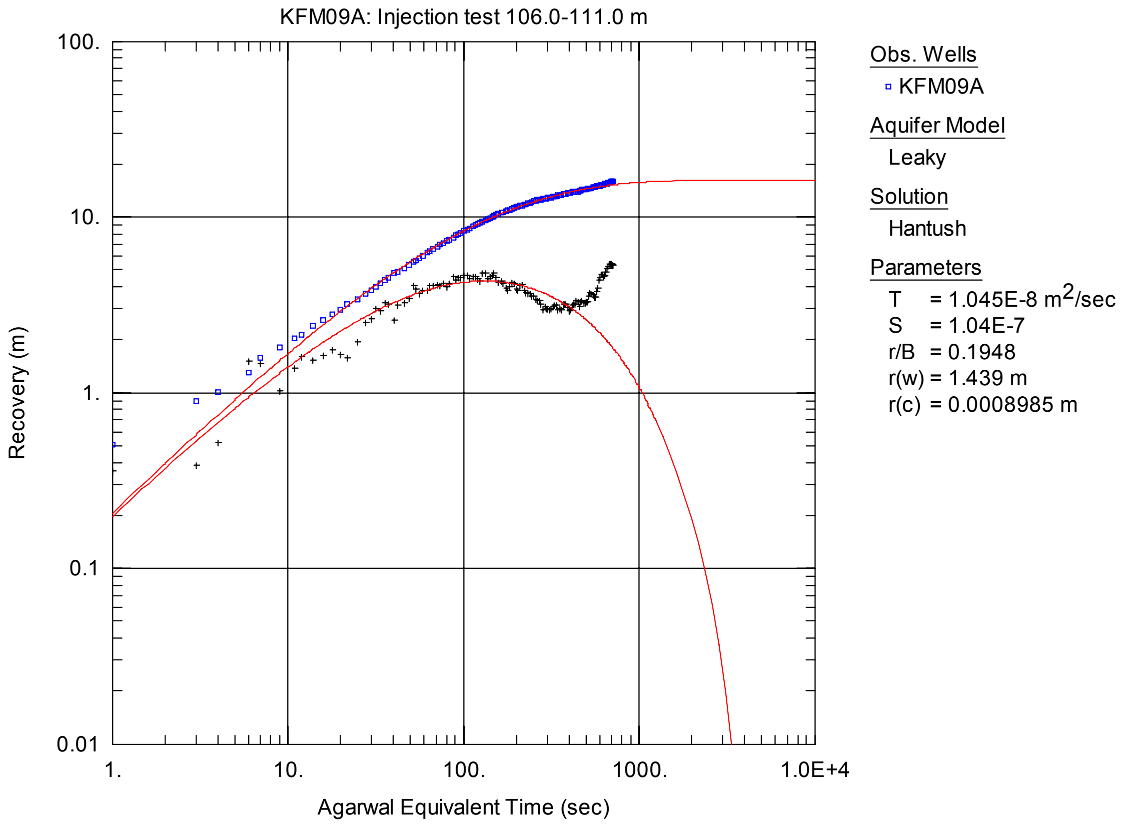


Figure A3-206. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 106.0-111.0 m in KFM09A.*

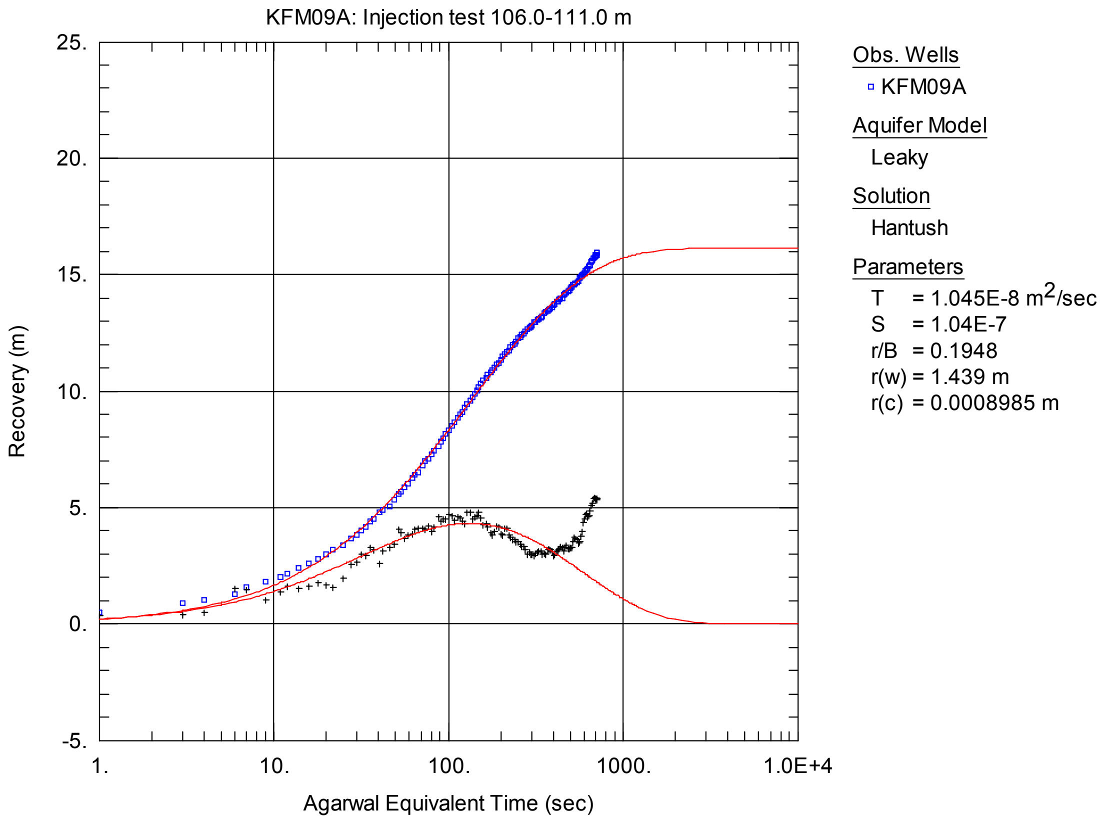


Figure A3-207. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 106.0-111.0 m in KFM09A.*

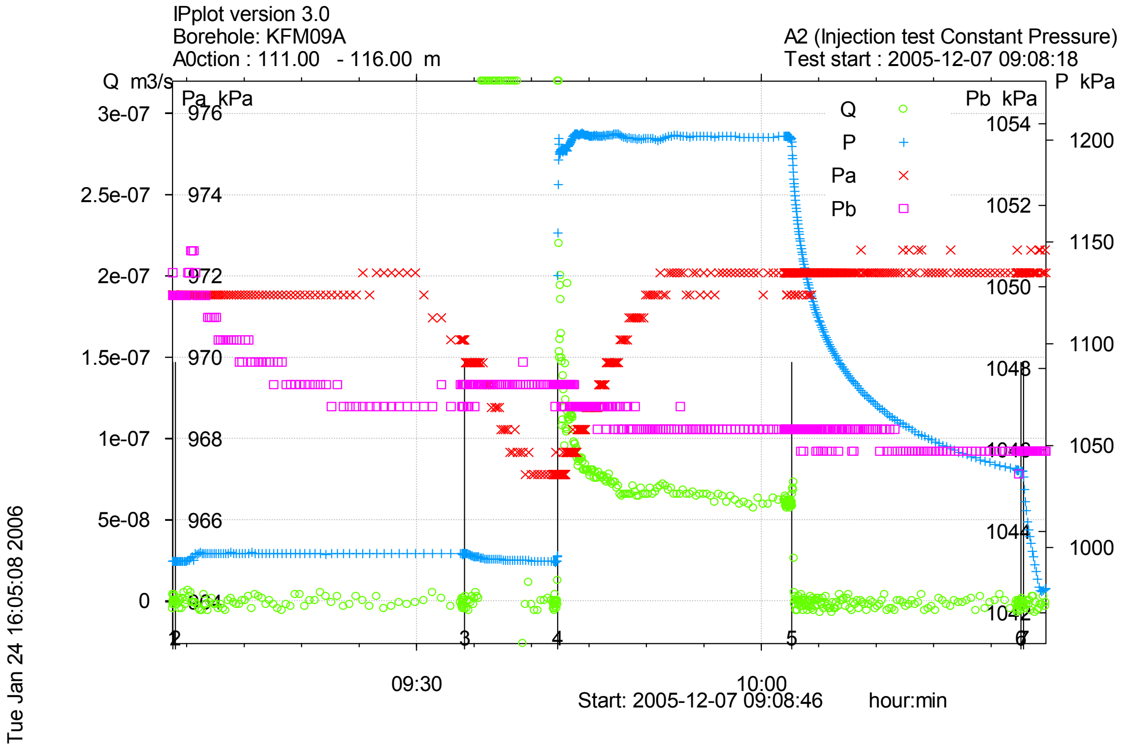


Figure A3-208. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 111.0-116.0 m in borehole KFM09A.*

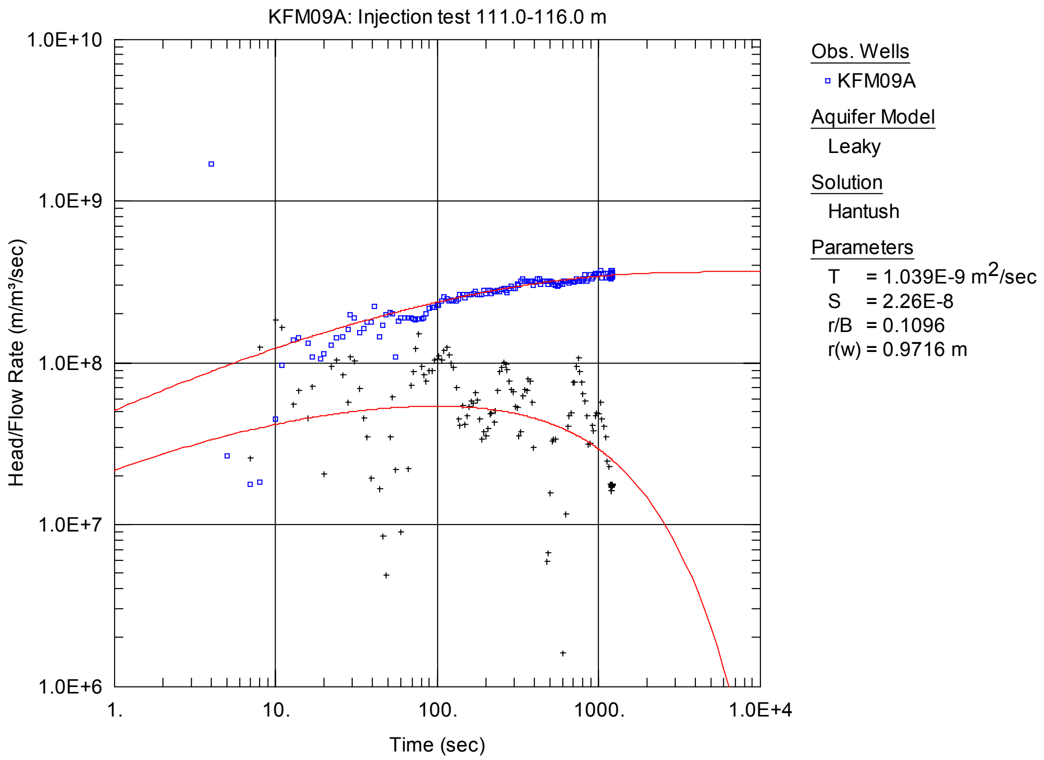


Figure A3-209. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 111.0-116.0 m in KFM09A.*

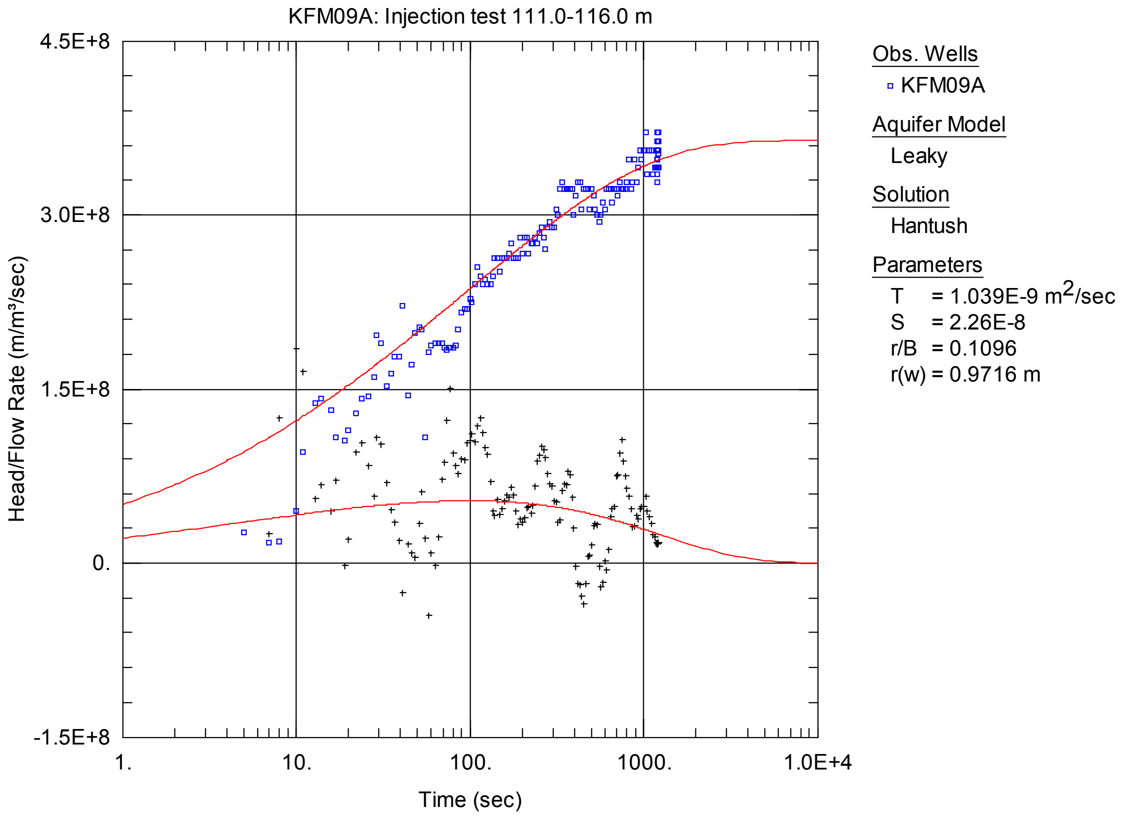


__Figure A3-210.__ Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 111.0-116.0 m in KFM09A.

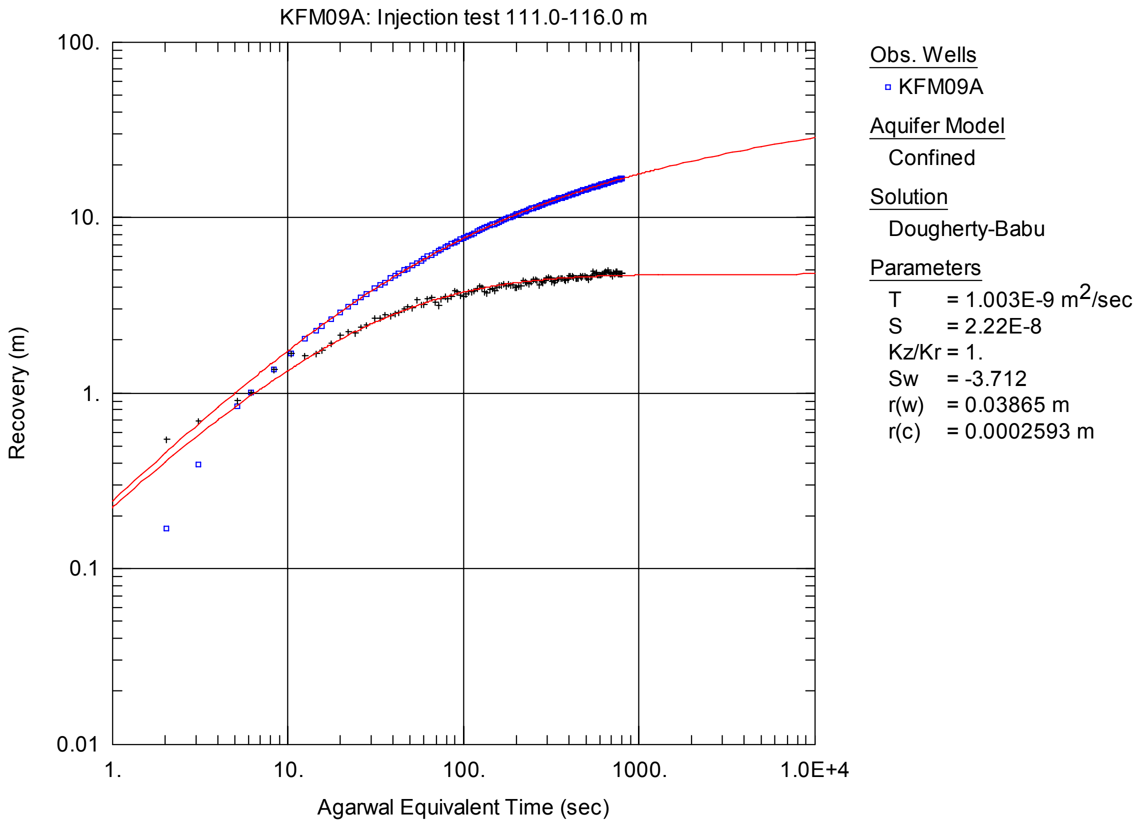


__Figure A3-211.__ Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 111.0-116.0 m in KFM09A.

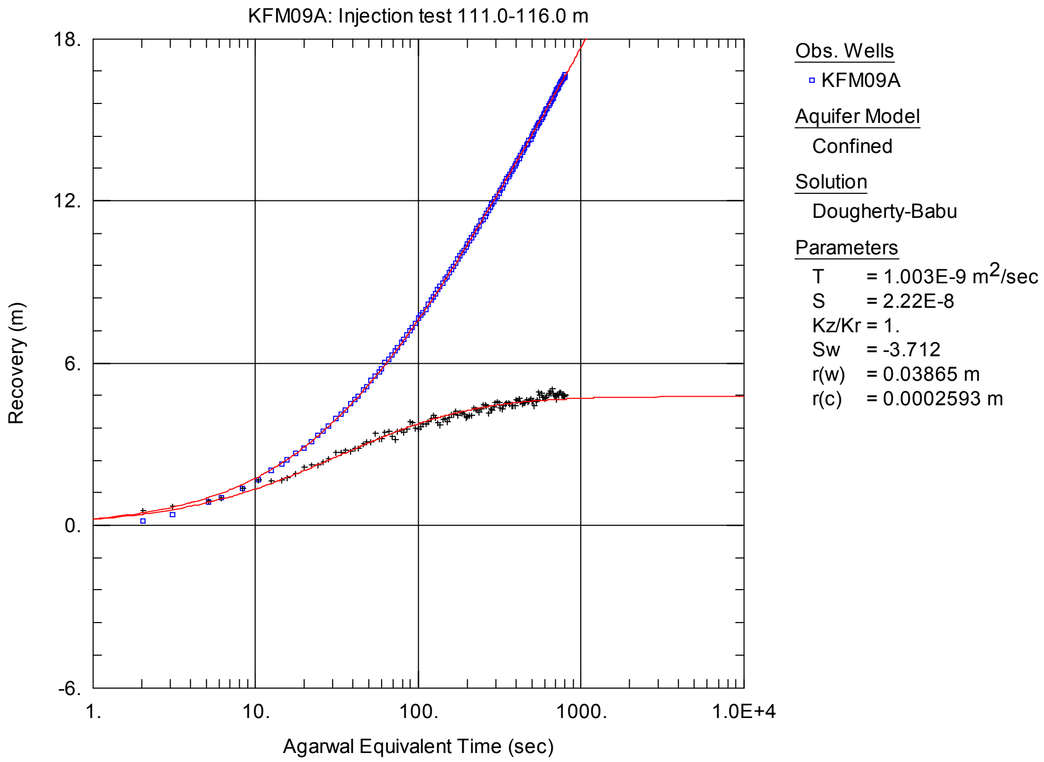


Figure A3-212. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 111.0-116.0 m in KFM09A.*

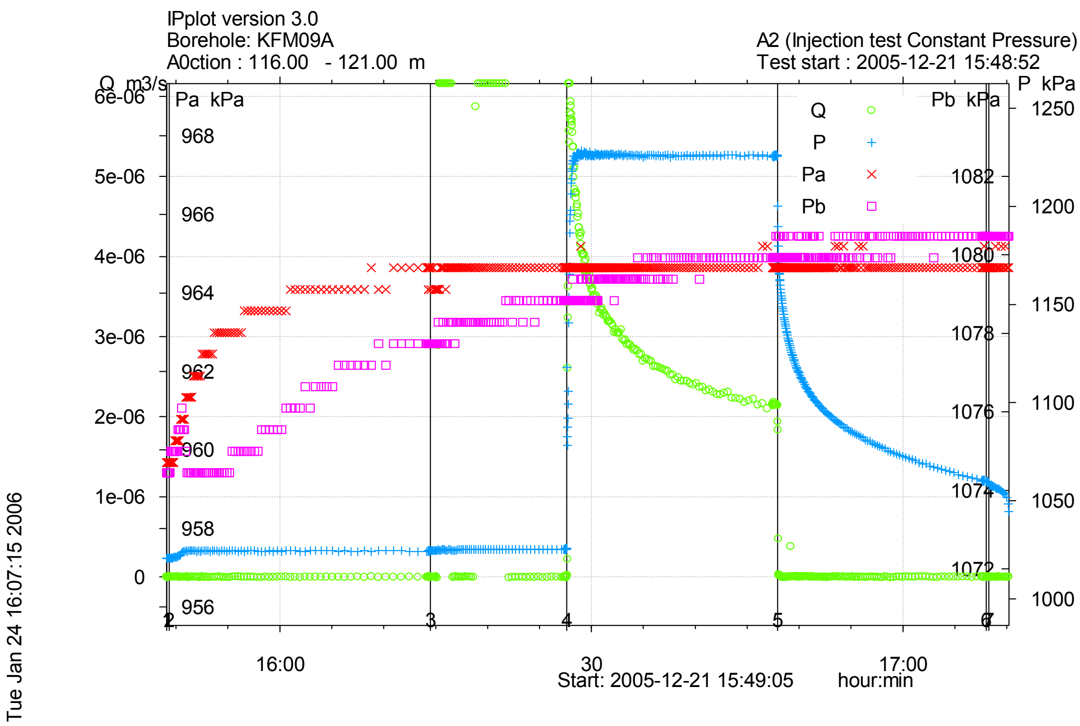


Figure A3-213. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 116.0-121.0 m in borehole KFM09A.*

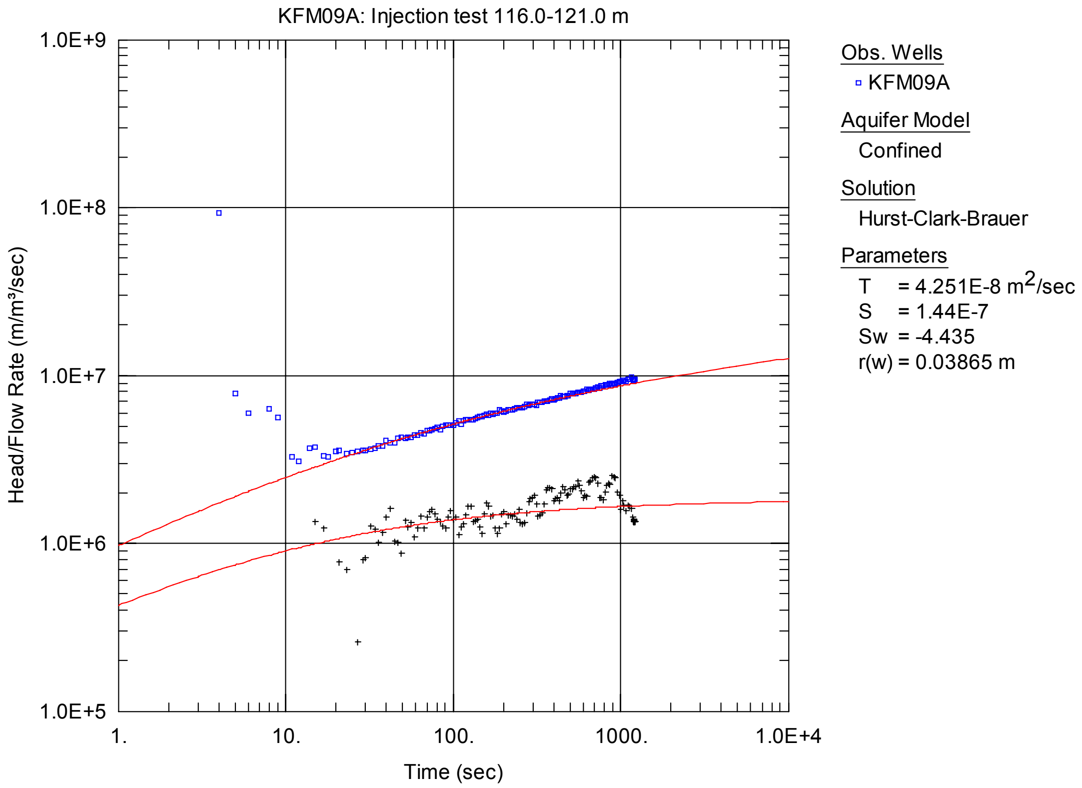


Figure A3-214. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 116.0-121.0 m in KFM09A. This plot shows the first of two different PRF:s during the injection period in this section.*

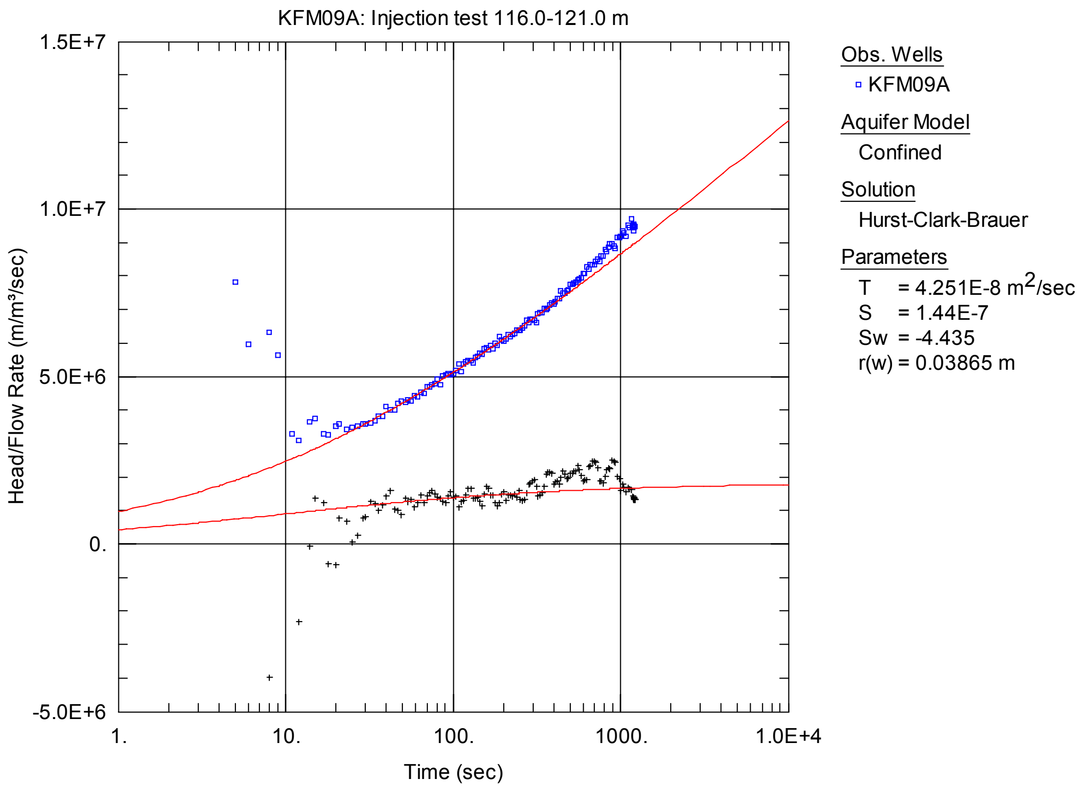


Figure A3-215. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 116.0-121.0 m in KFM09A. This plot shows the first of two different PRF:s during the injection period in this section.*

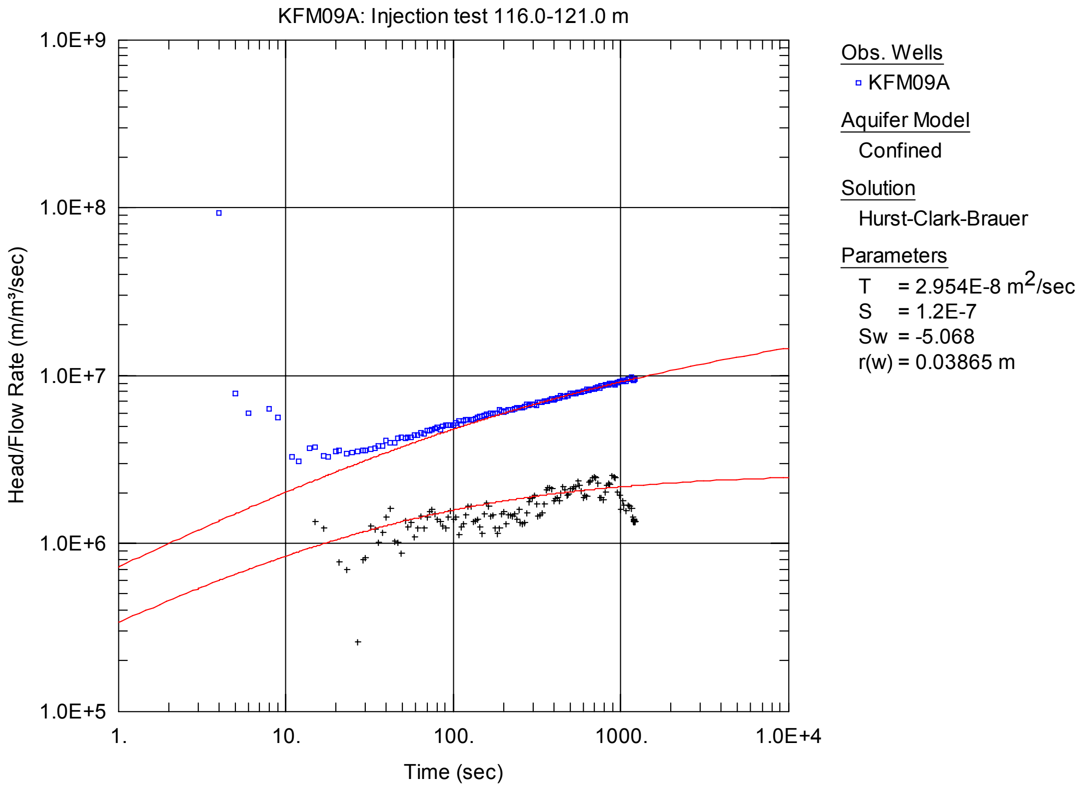


Figure A3-216. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 116.0-121.0 m in KFM09A. This plot shows a fit to the second of two different PRF:s during the injection period in this section.*

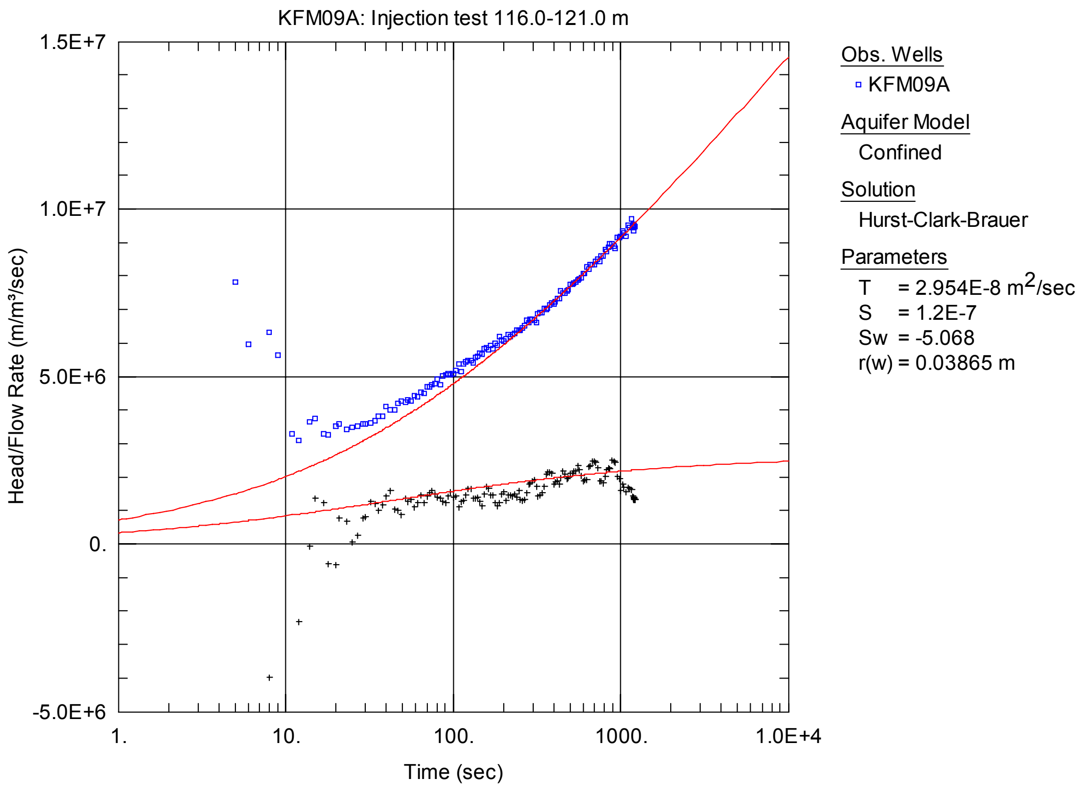


Figure A3-217. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 116.0-121.0 m in KFM09A. This plot shows a fit to the second of two different PRF:s during the injection period in this section.*

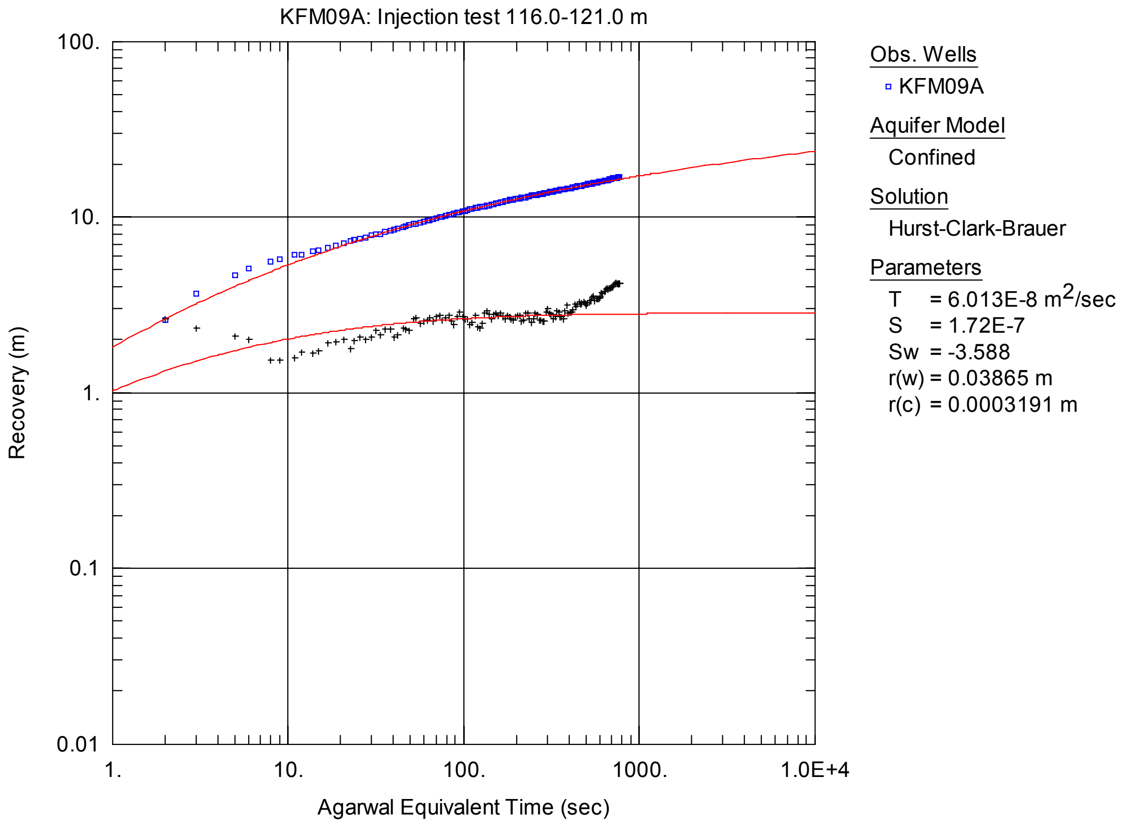


Figure A3-218. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 116.0-121.0 m in KFM09A.*

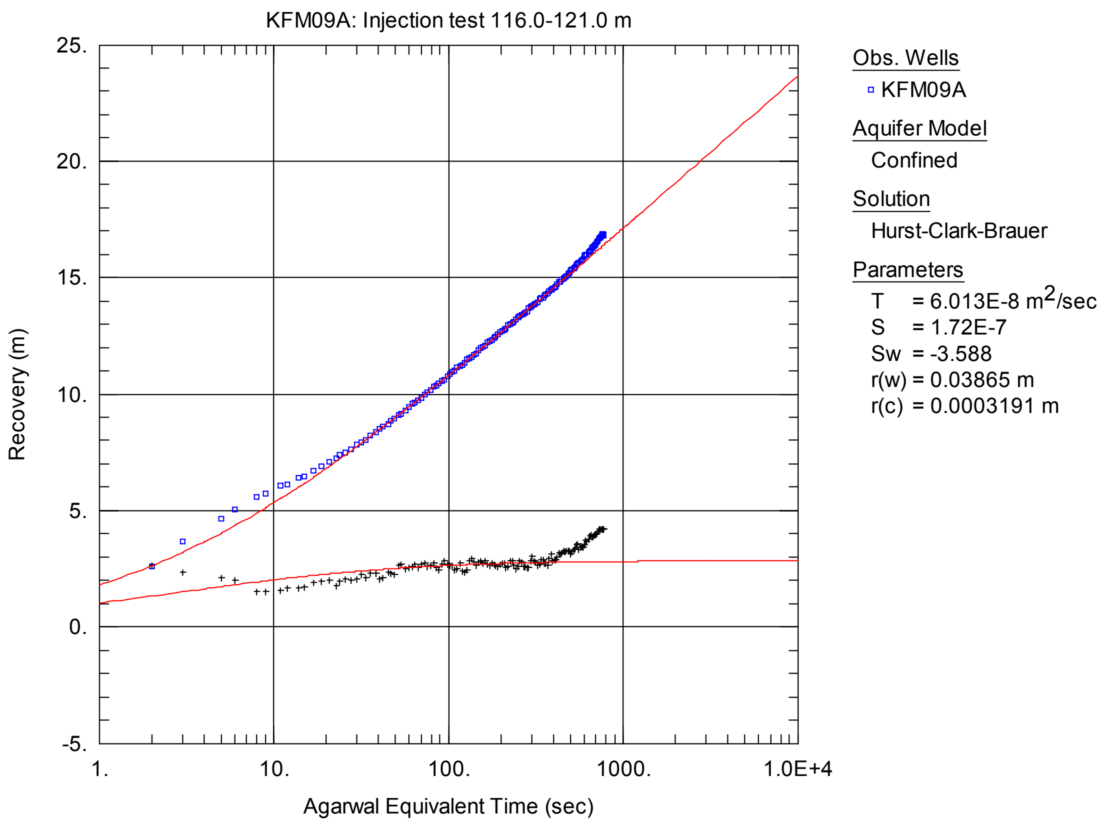


Figure A3-219. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 116.0-121.0 m in KFM09A.*

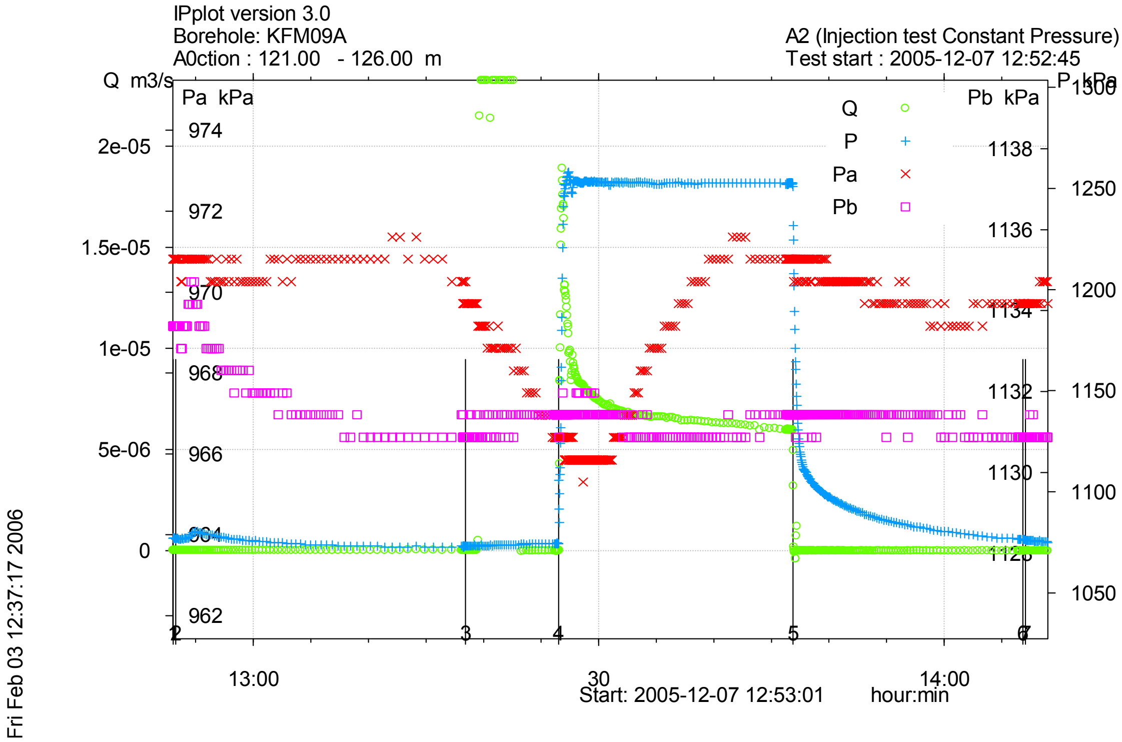


Figure A3-220. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 121.0-126.0 m in borehole KFM09A.*

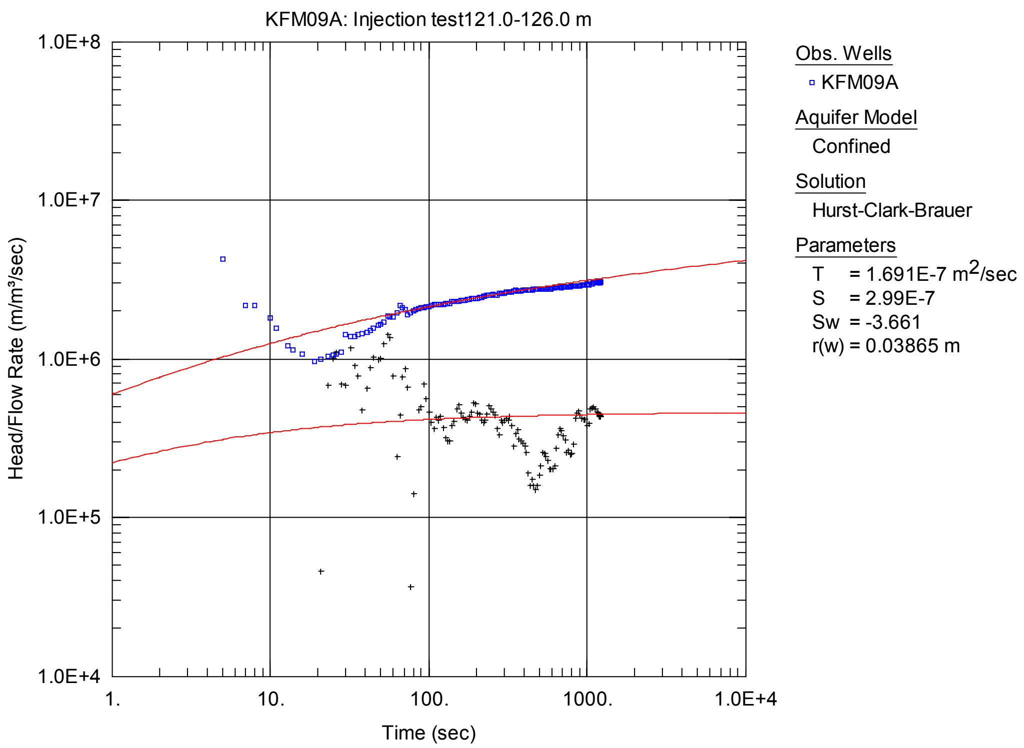


Figure A3-221. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 121.0-126.0 m in KFM09A. This plot shows a fit to the first of two different PRF:s during the injection period in this section.*

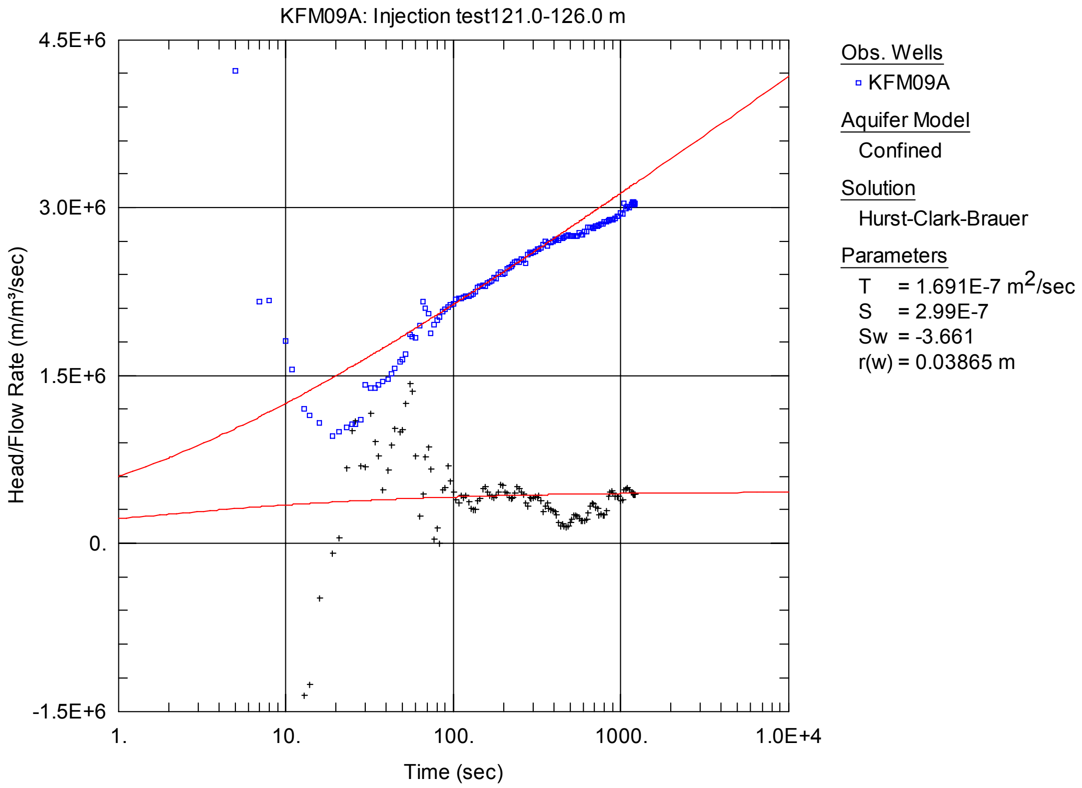


Figure A3-222. Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 121.0-126.0 m in KFM09A. This plot shows a fit to the first of two different PRF:s during the injection period in this section.

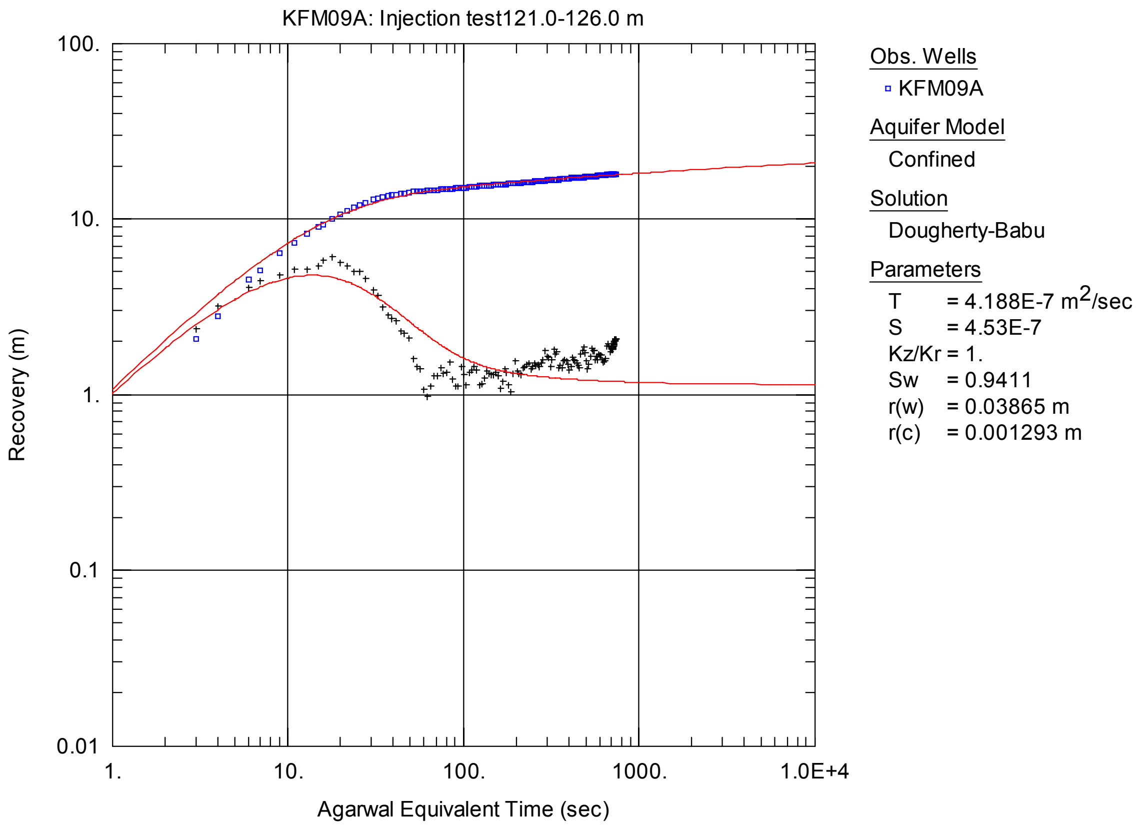


Figure A3-223. Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 121.0-126.0 m in KFM09A.

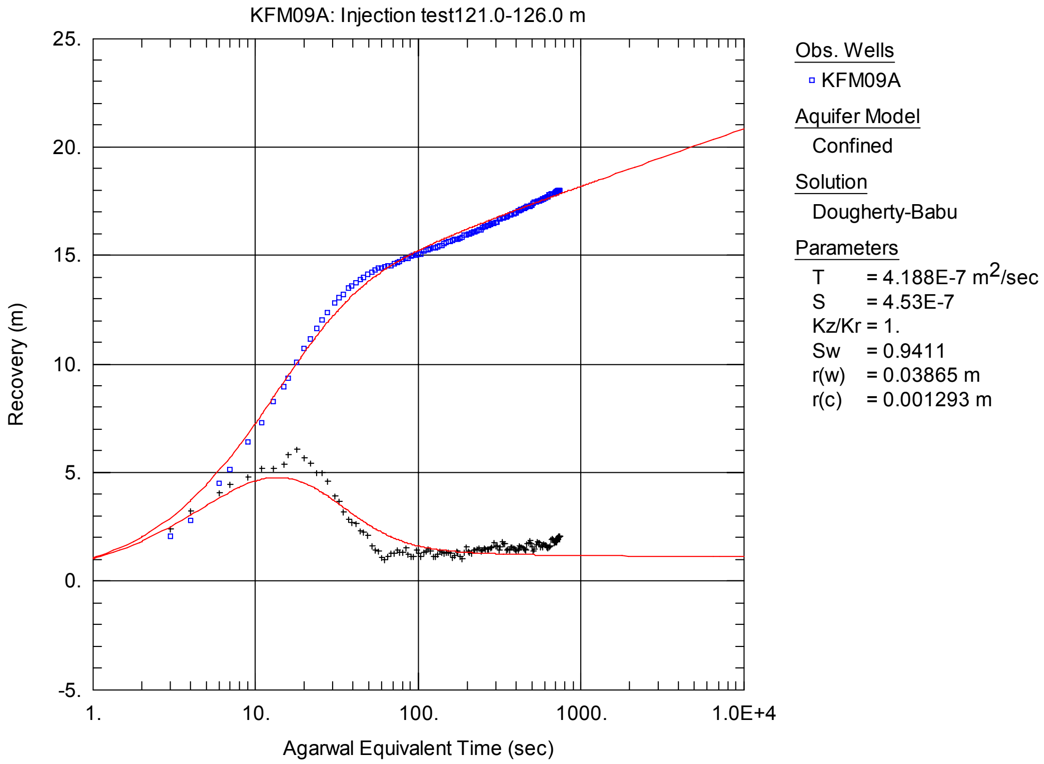


Figure A3-224. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 121.0-126.0 m in KFM09A.*

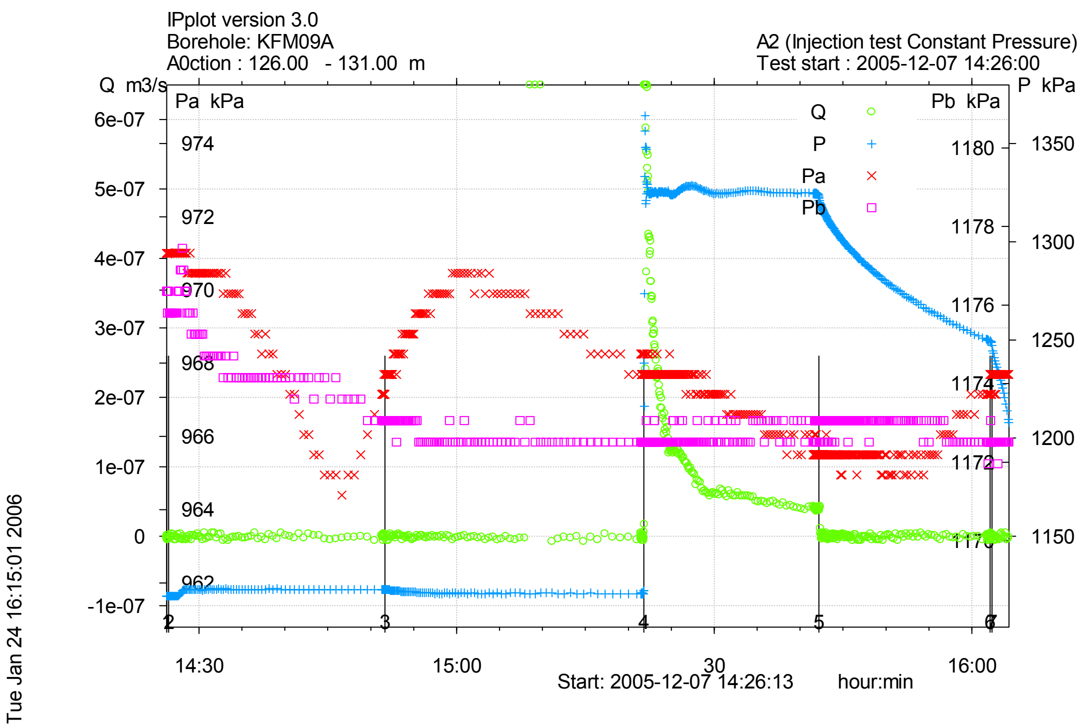


Figure A3-225. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 126.0-131.0 m in borehole KFM09A.*

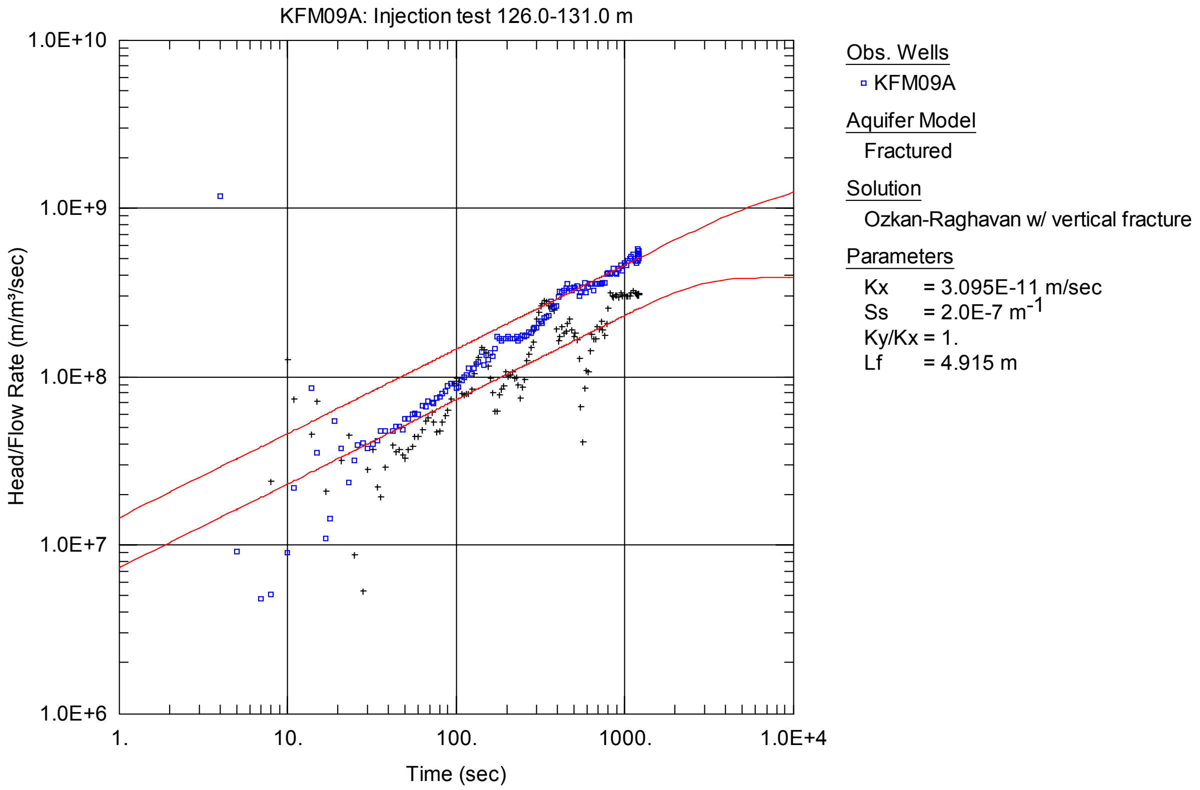


Figure A3-226. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 126.0-131.0 m in KFM09A. No unambiguous transient evaluation is possible on the injection period.*

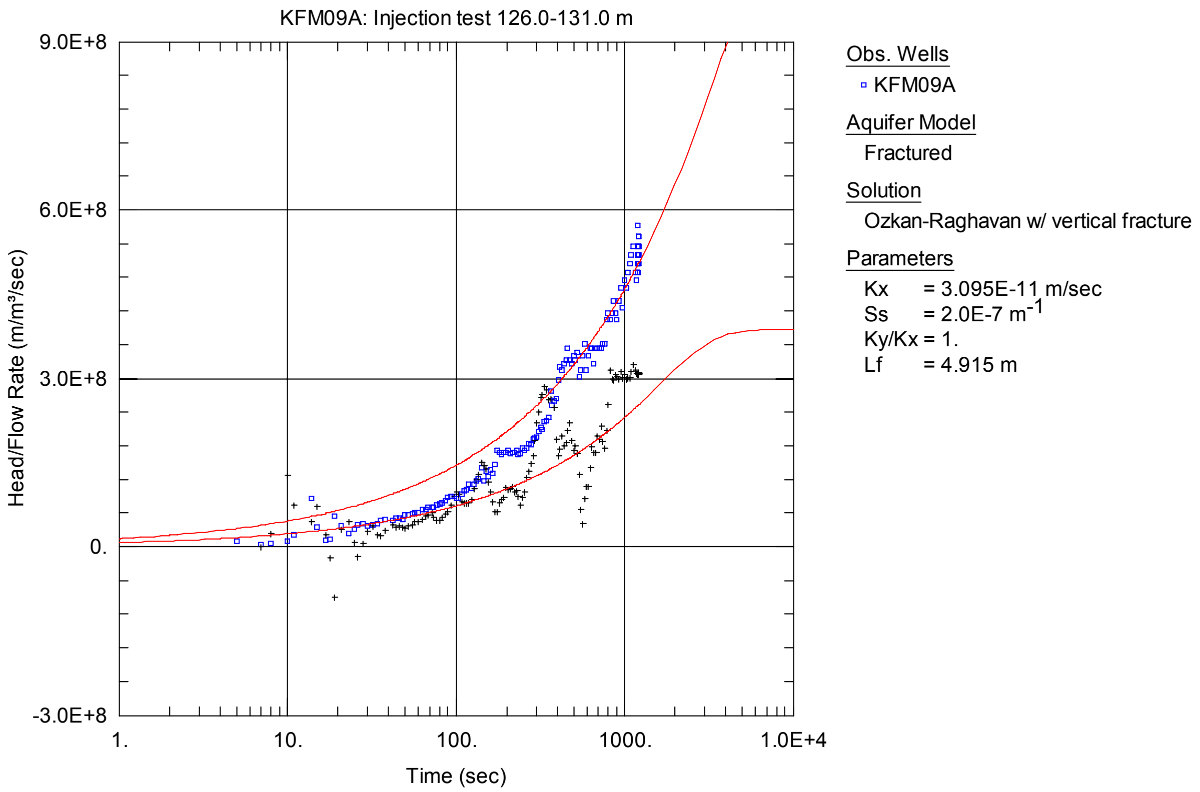


Figure A3-227. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 126.0-131.0 m in KFM09A. No unambiguous transient evaluation is possible on the injection period.*

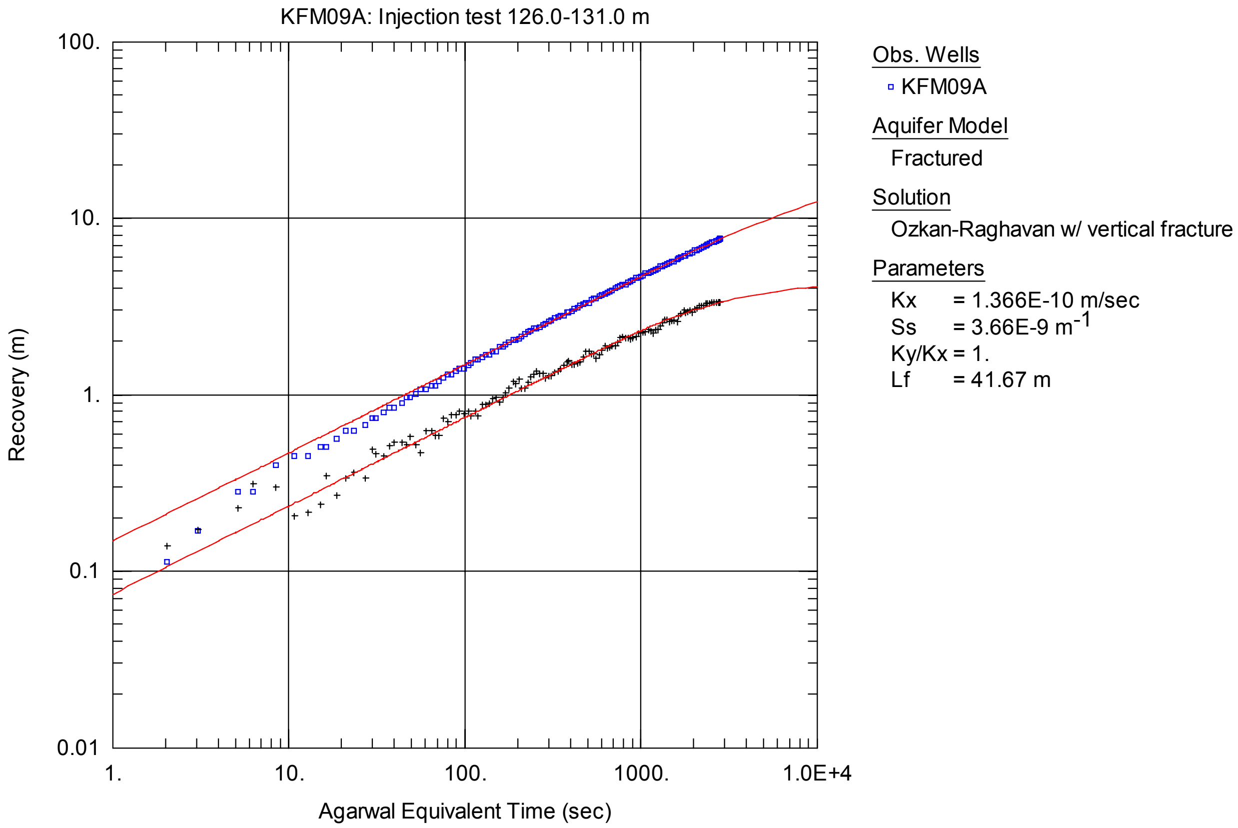


Figure A3-228. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 126.0-131.0 m in KFM09A.*

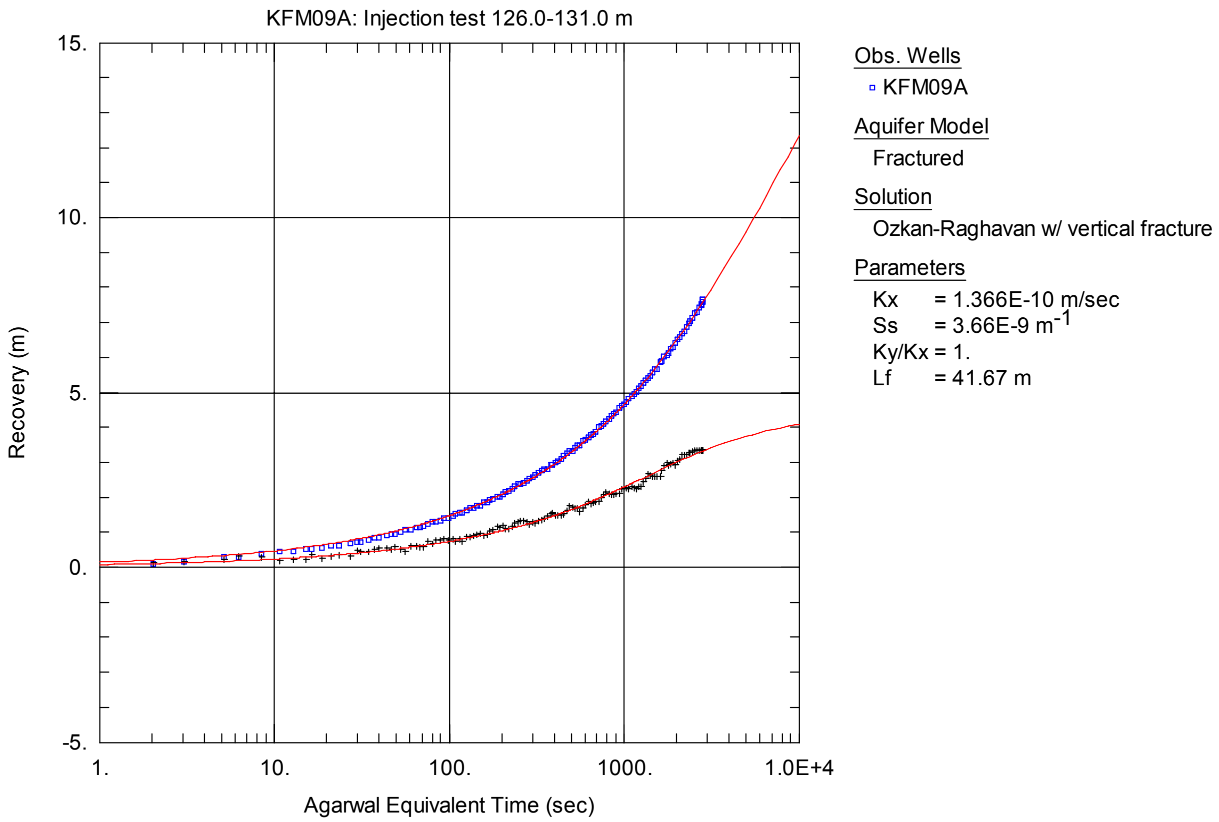


Figure A3-229. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 126.0-131.0 m in KFM09A.*

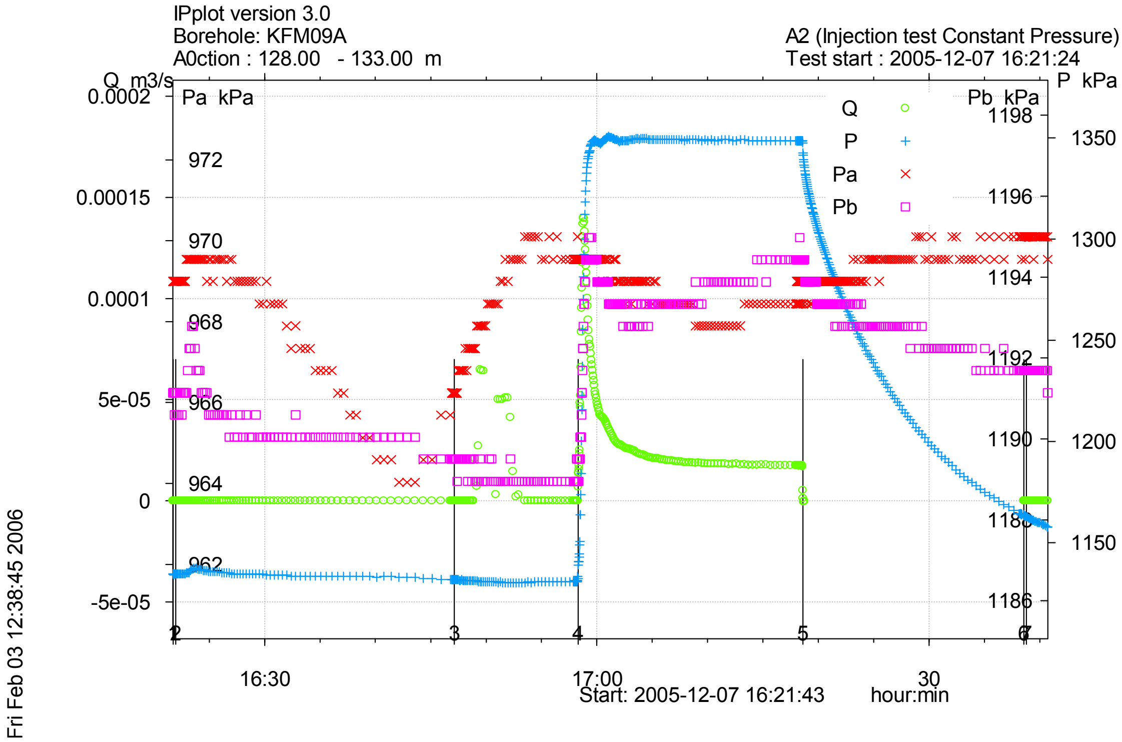


Figure A3-230. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 128.0-133.0 m in borehole KFM09A.*

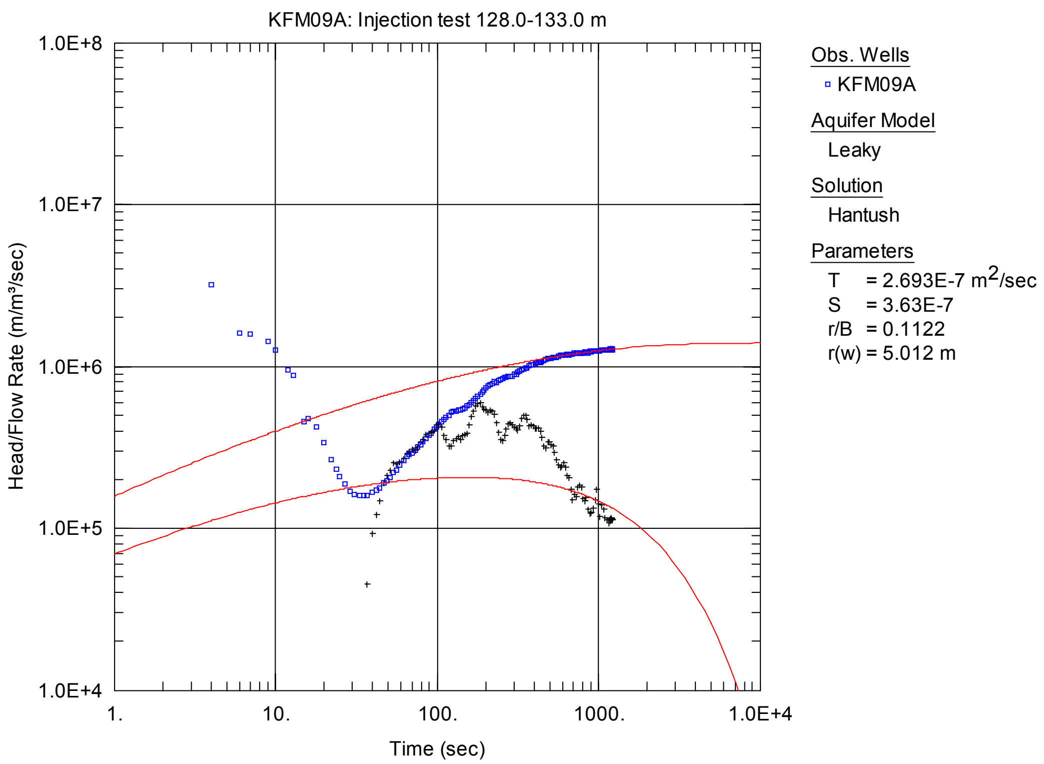


Figure A3-231. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 128.0-133.0 m in KFM09A.*

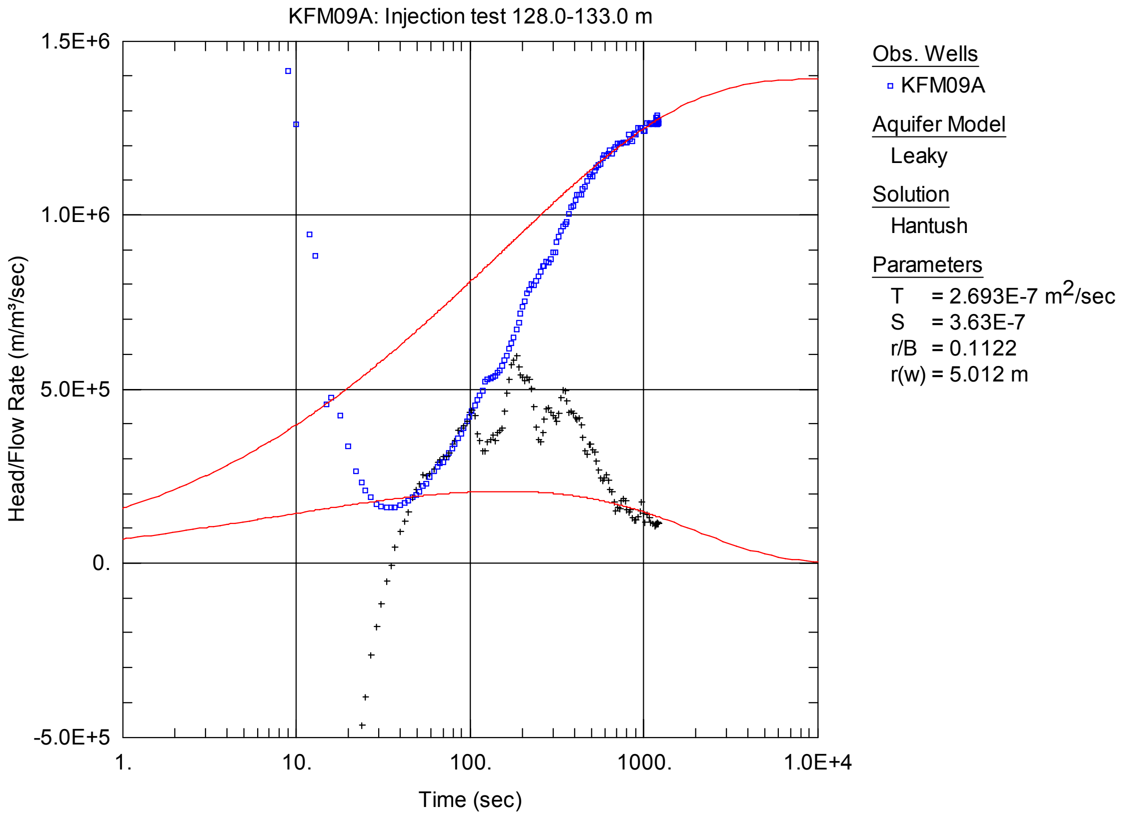


***Figure A3-232.** Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 128.0-133.0 m in KFM09A.*

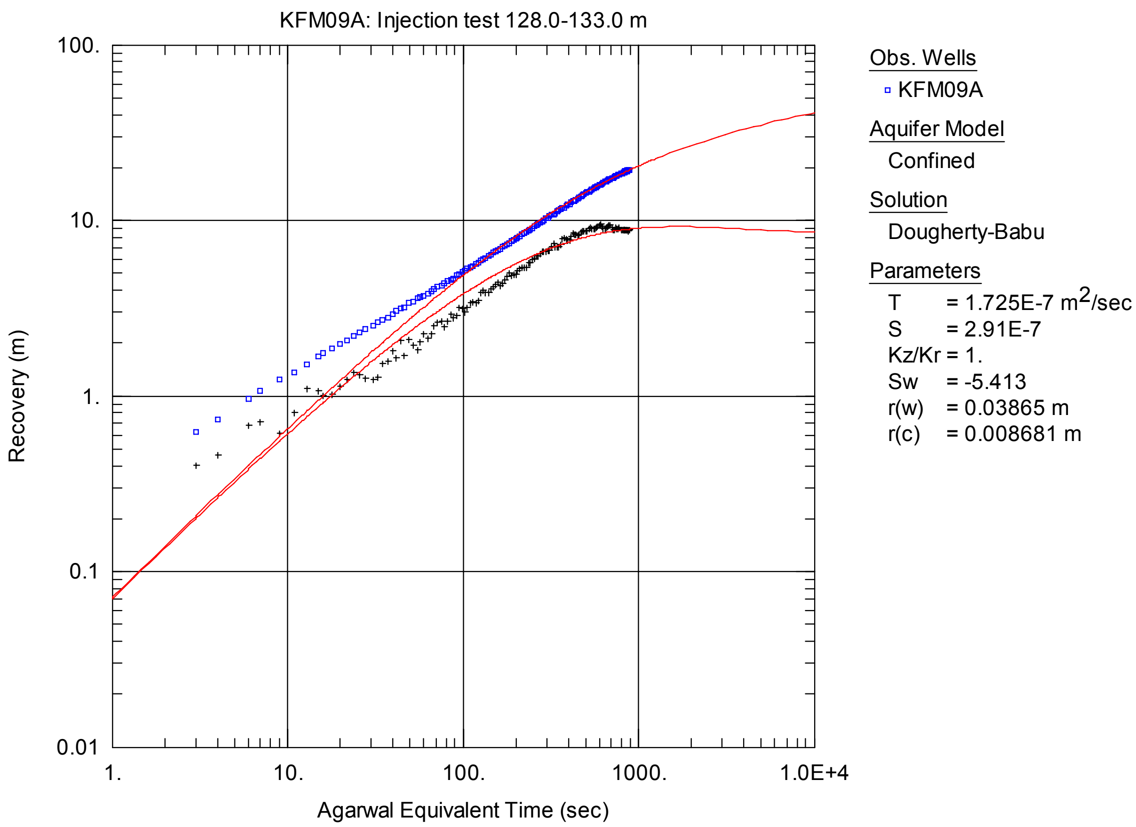


***Figure A3-233.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 128.0-133.0 m in KFM09A.*

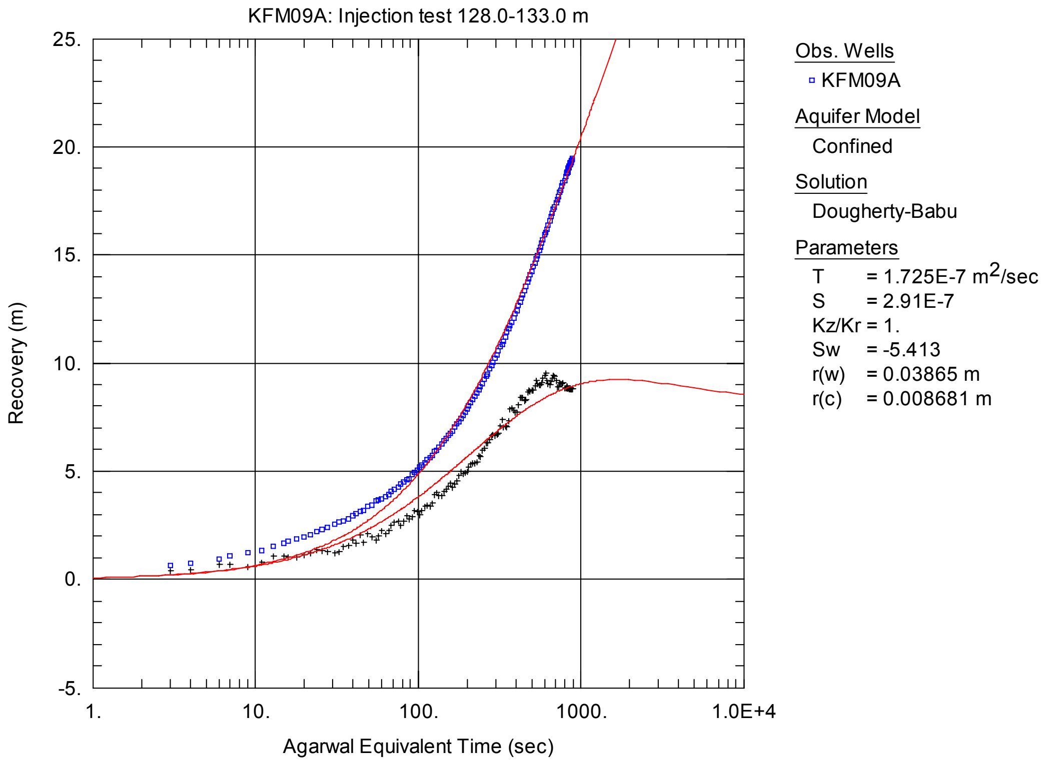


Figure A3-234. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 128.0-133.0 m in KFM09A.*

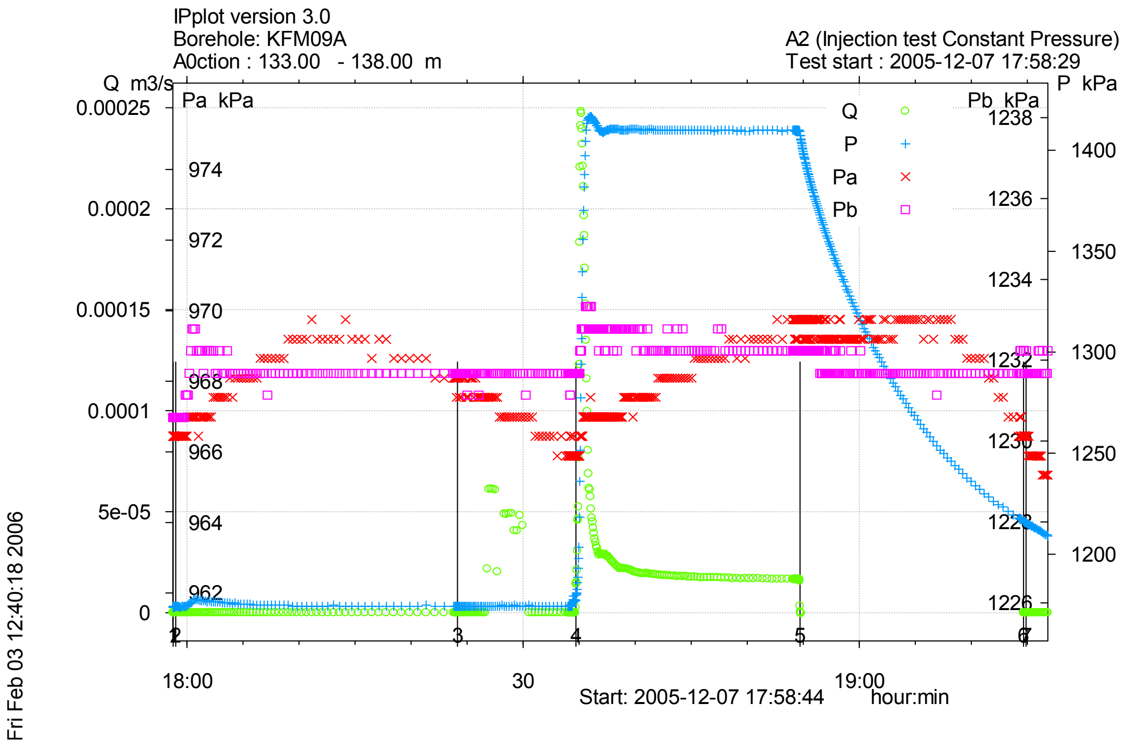


Figure A3-235. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 133.0-138.0 m in borehole KFM09A.*

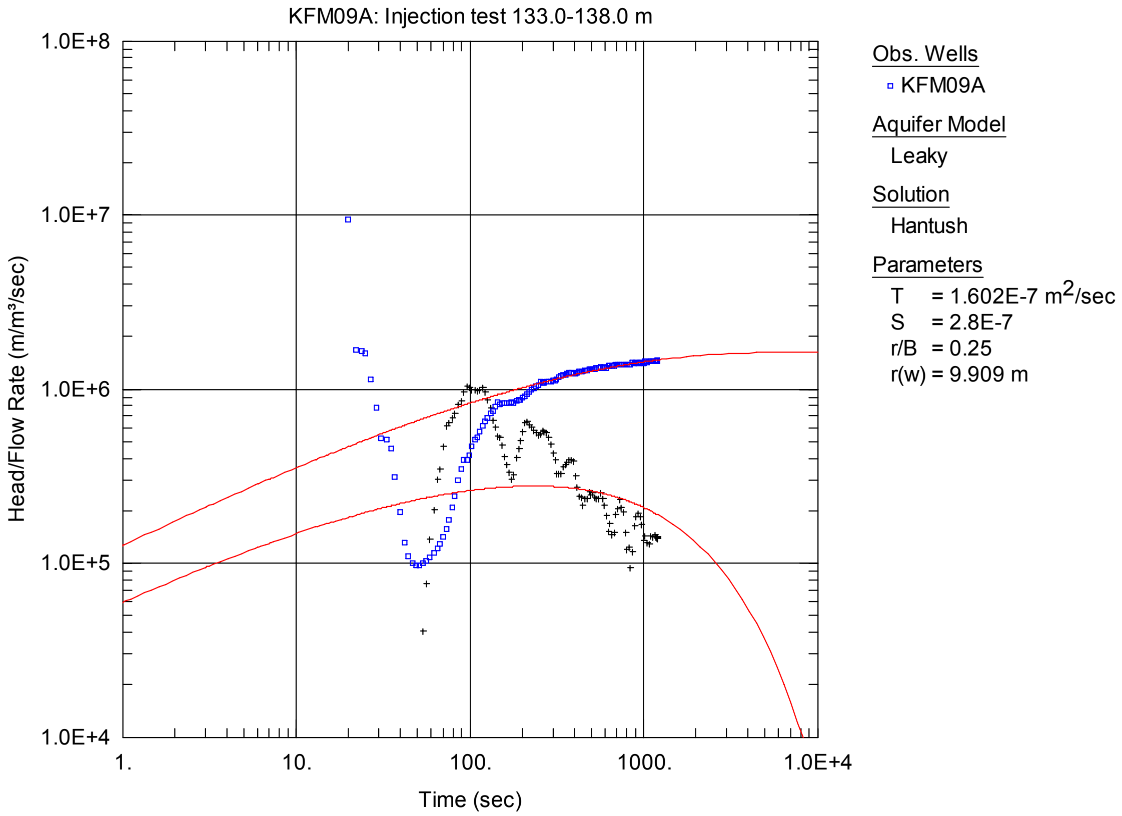


Figure A3-236. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 133.0-138.0 m in KFM09A.*

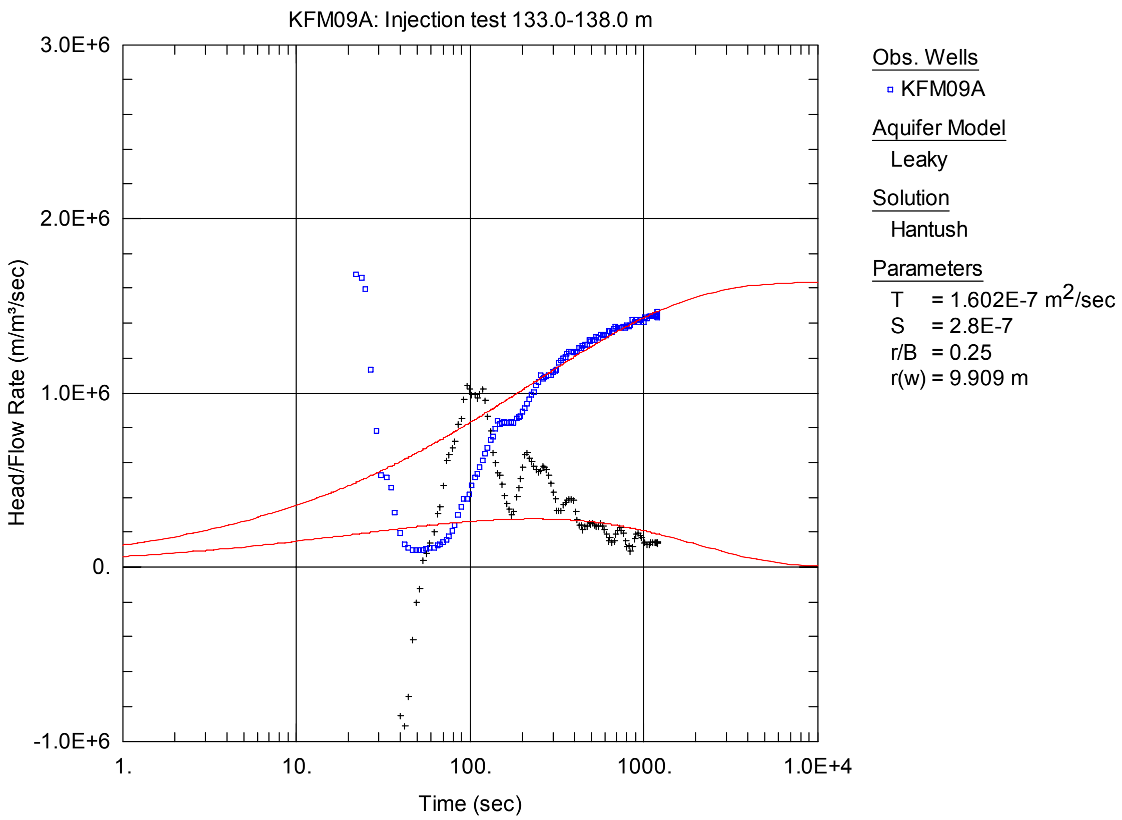


Figure A3-237. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 133.0-138.0 m in KFM09A.*

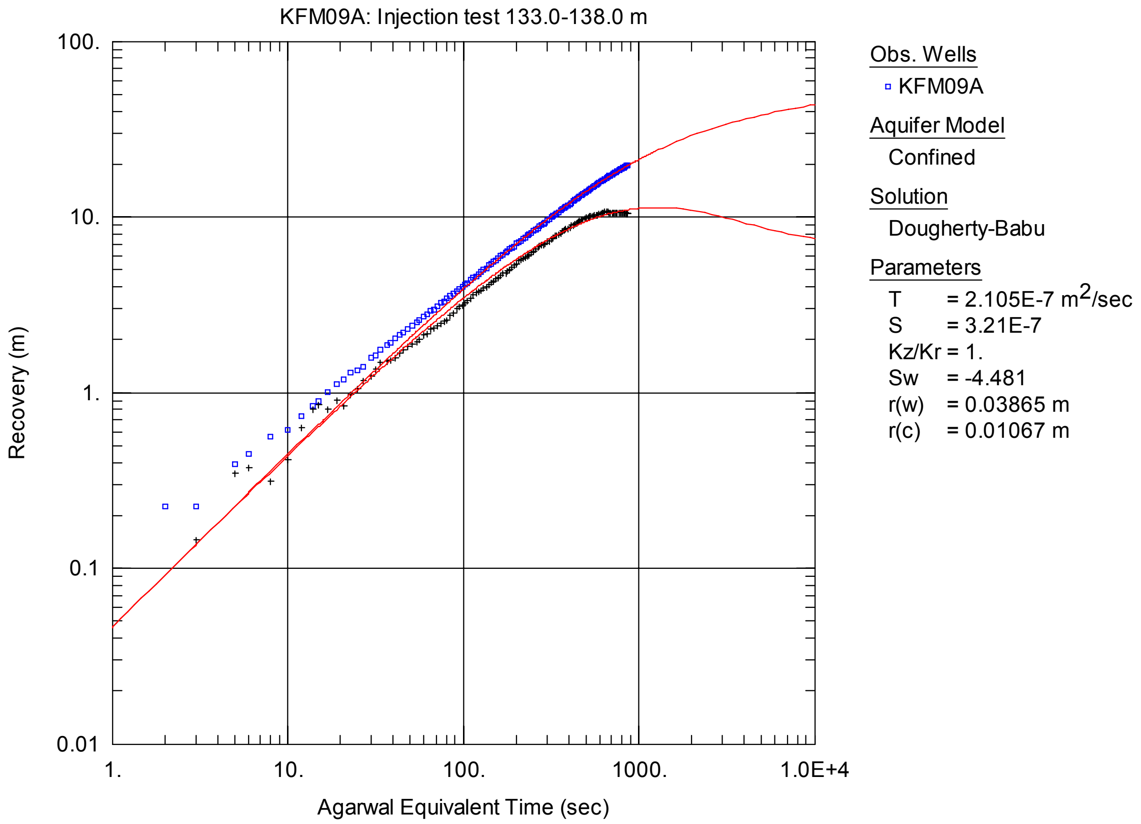


***Figure A3-238.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 133.0-138.0 m in KFM09A.*

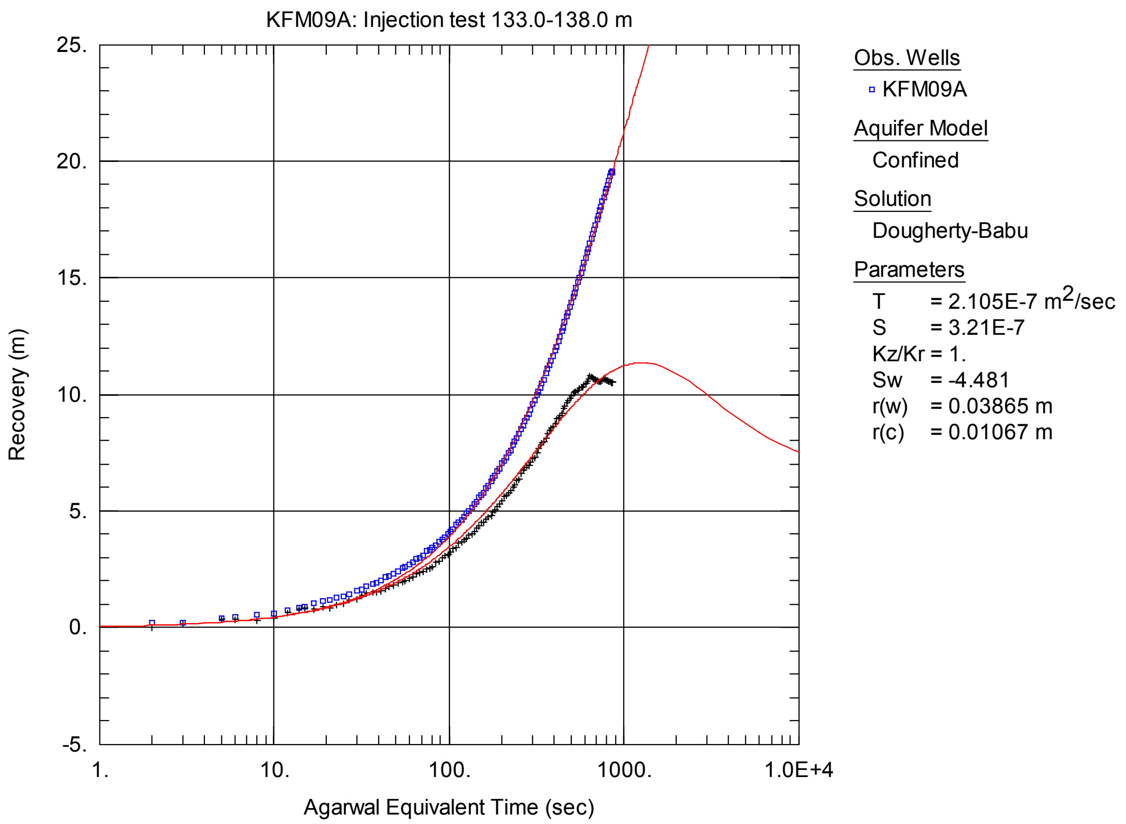


***Figure A3-239.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 133.0-138.0 m in KFM09A.*

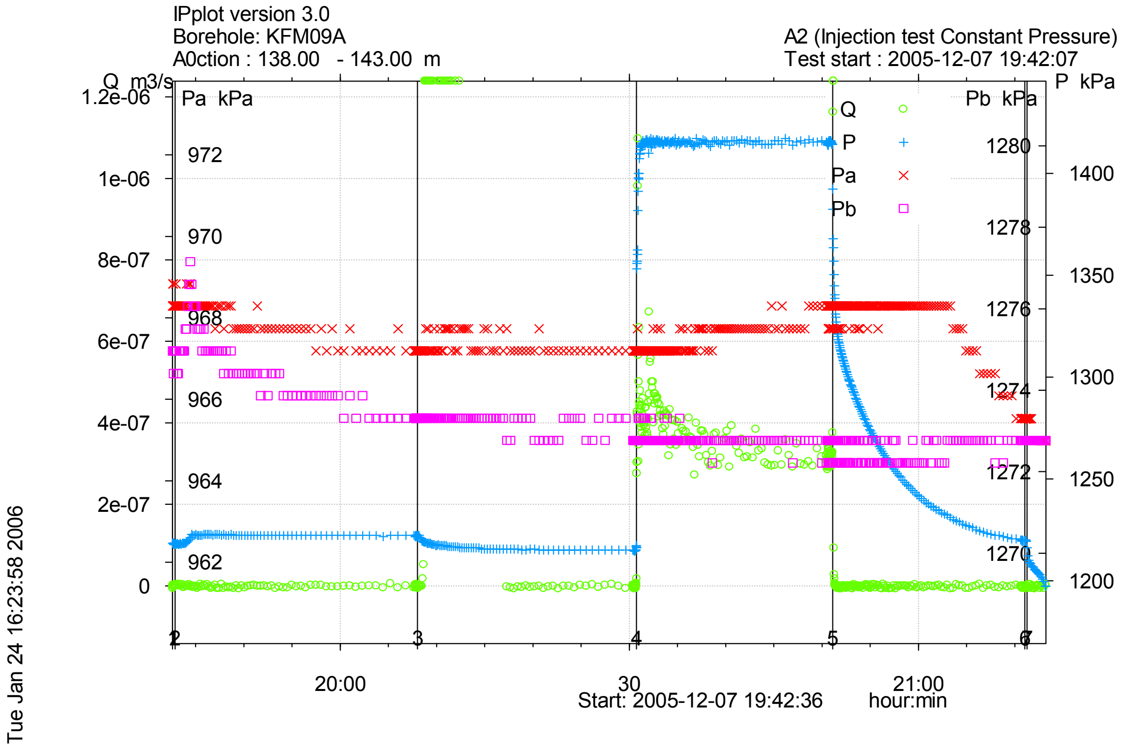


Figure A3-240. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 138.0-143.0 m in borehole KFM09A.*

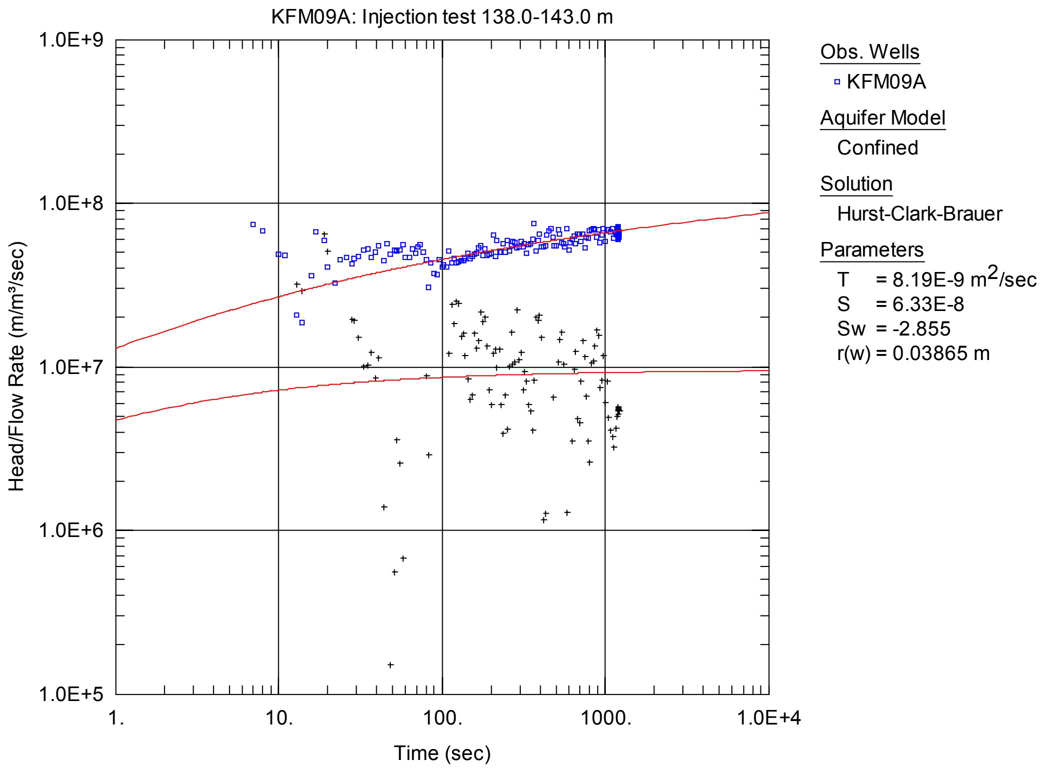


Figure A3-241. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 138.0-143.0 m in KFM09A.*

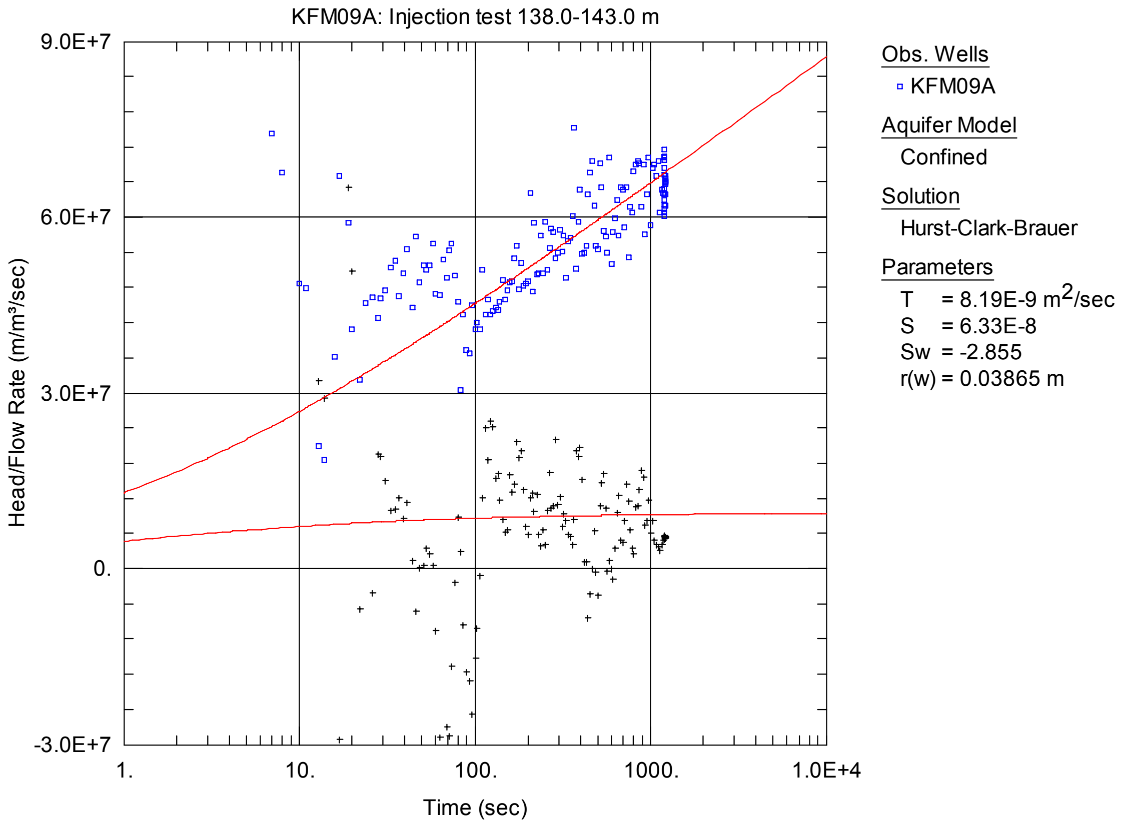


Figure A3-242. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 138.0-143.0 m in KFM09A.*

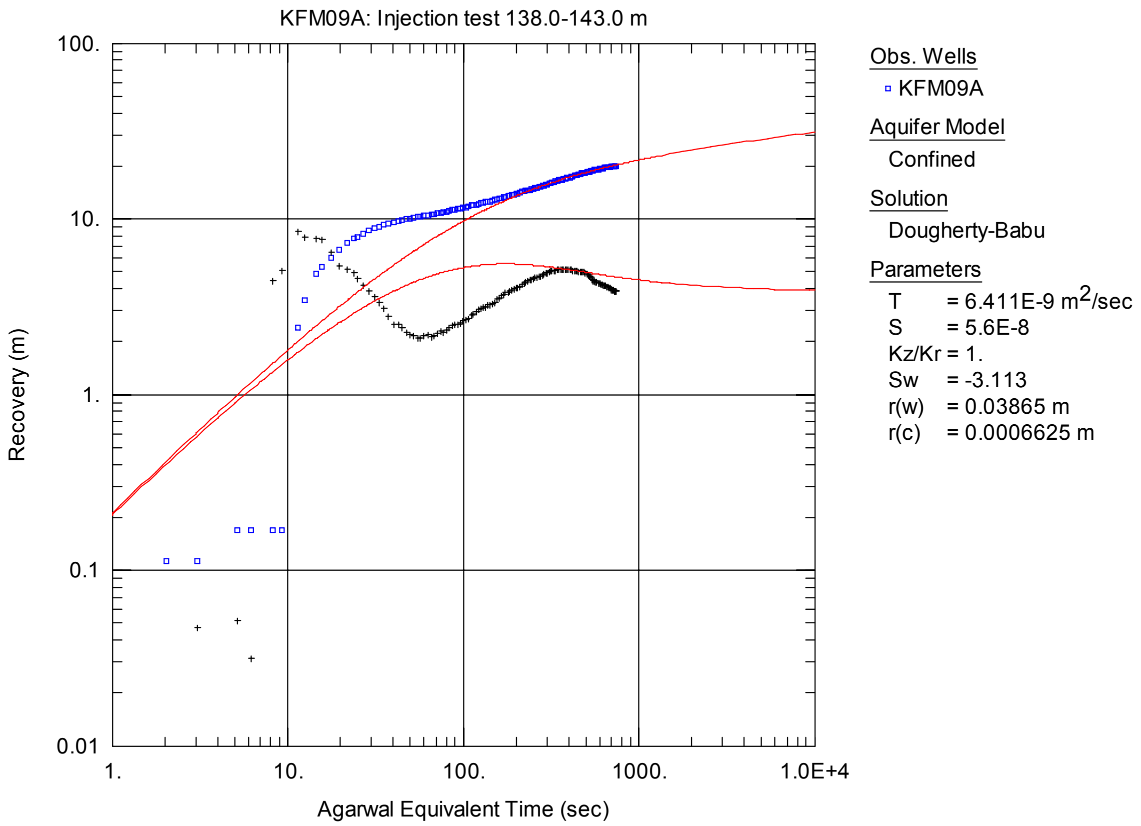


Figure A3-243. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 138.0-143.0 m in KFM09A.*

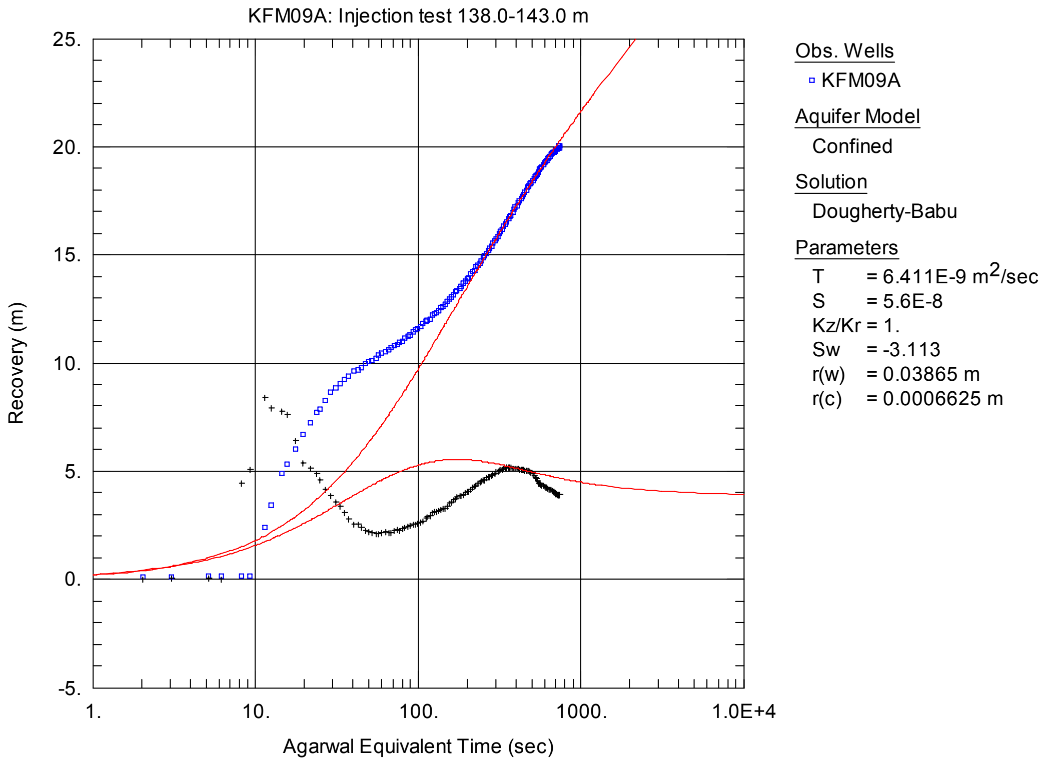


Figure A3-244. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 138.0-143.0 m in KFM09A.*

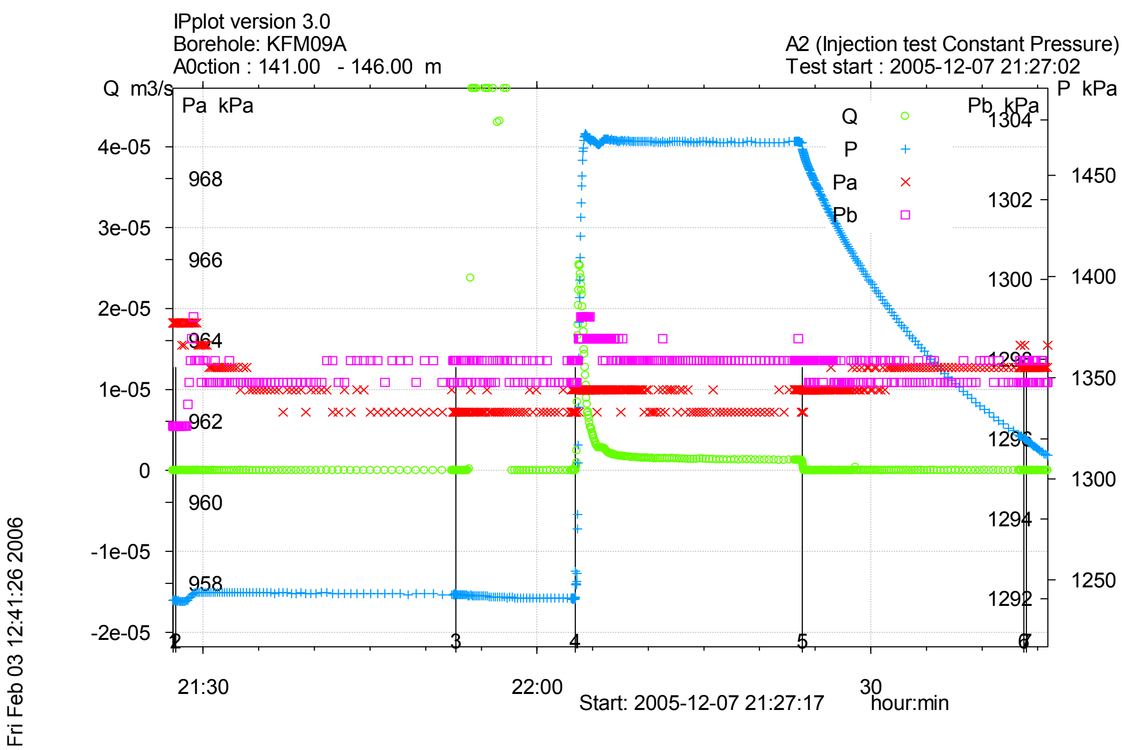


Figure A3-245. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 141.0-146.0 m in borehole KFM09A.*

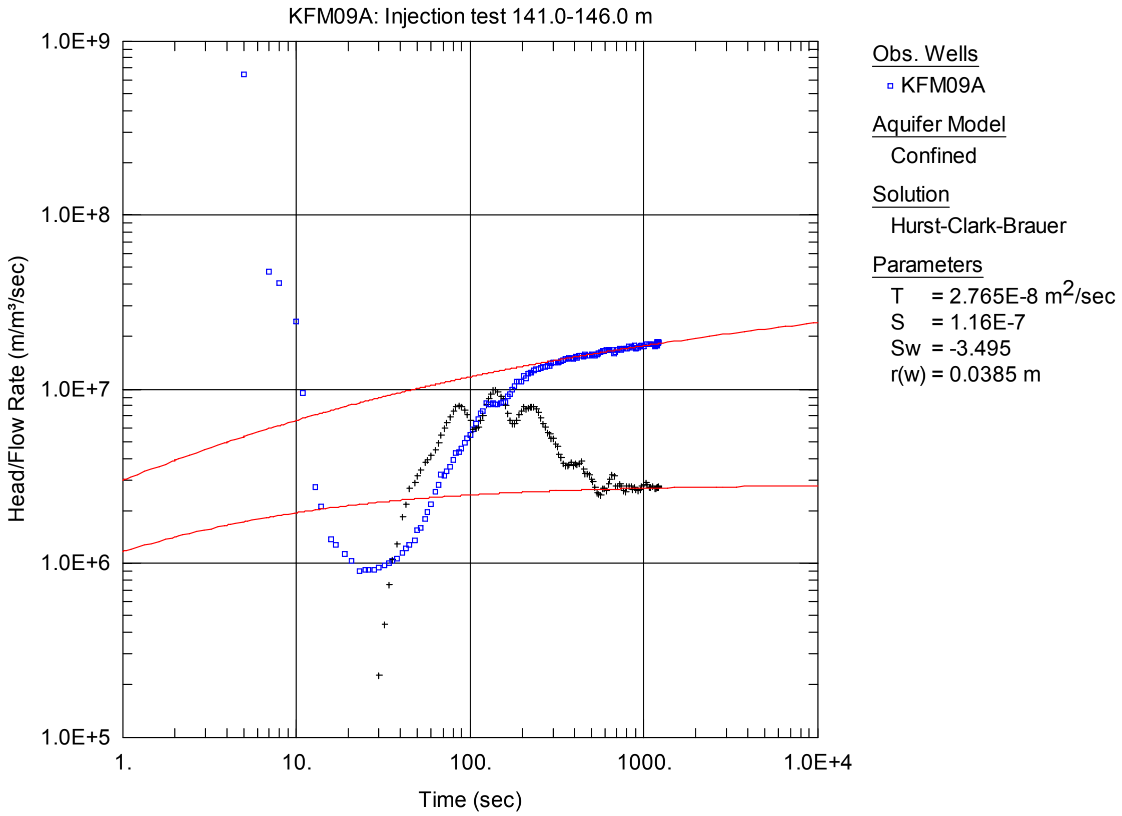


Figure A3-246. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 141.0-146.0 m in KFM09A.*

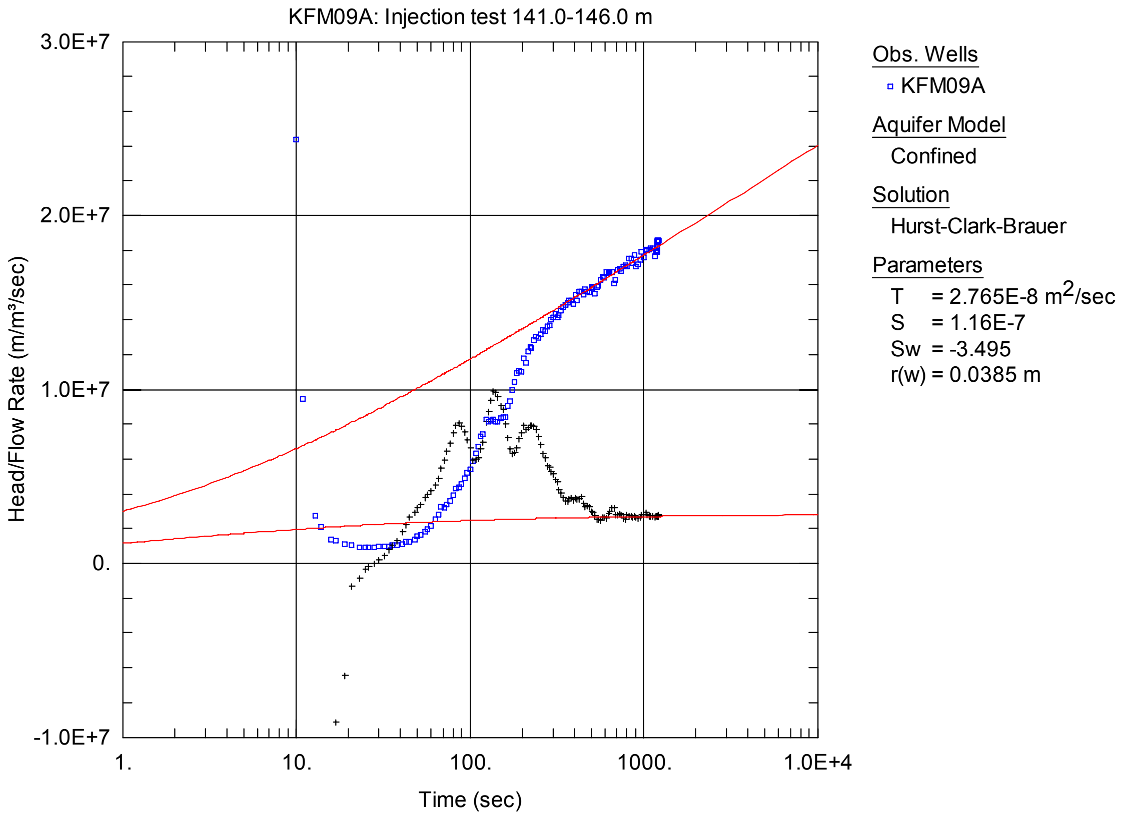


Figure A3-247. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 141.0-146.0 m in KFM09A.*

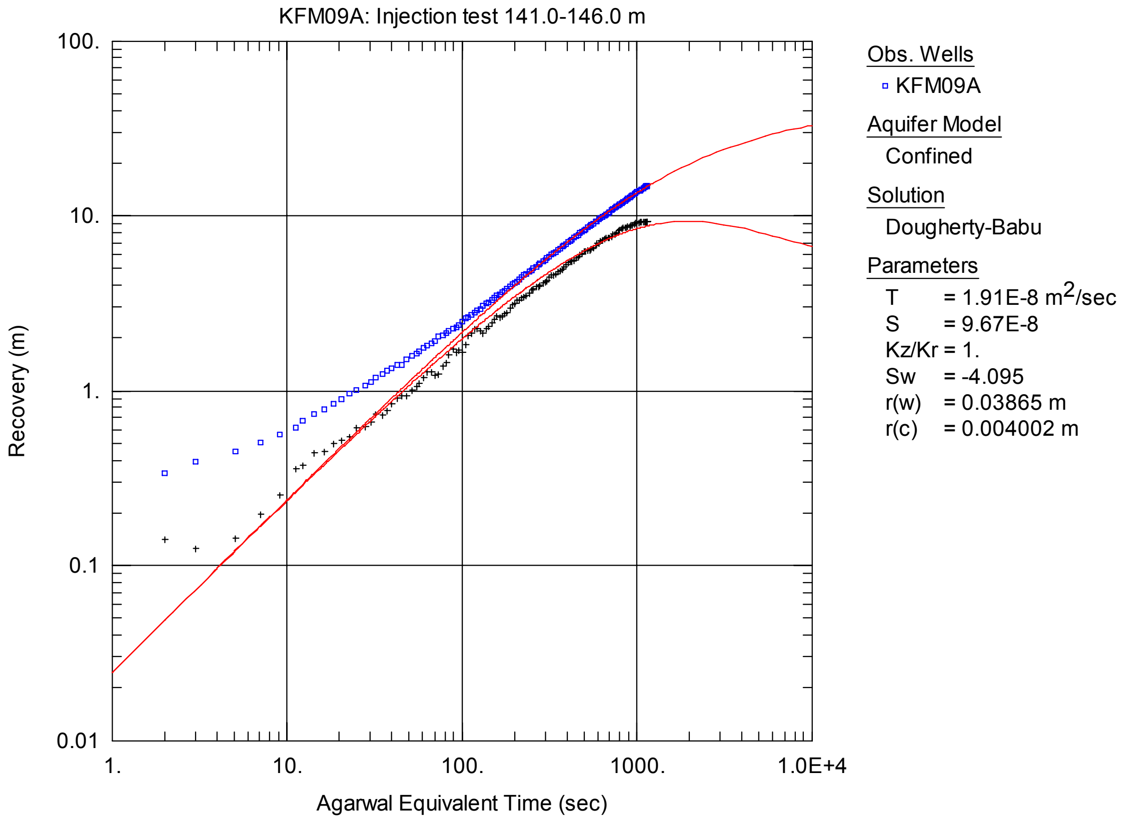


Figure A3-248. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 141.0-146.0 m in KFM09A.*

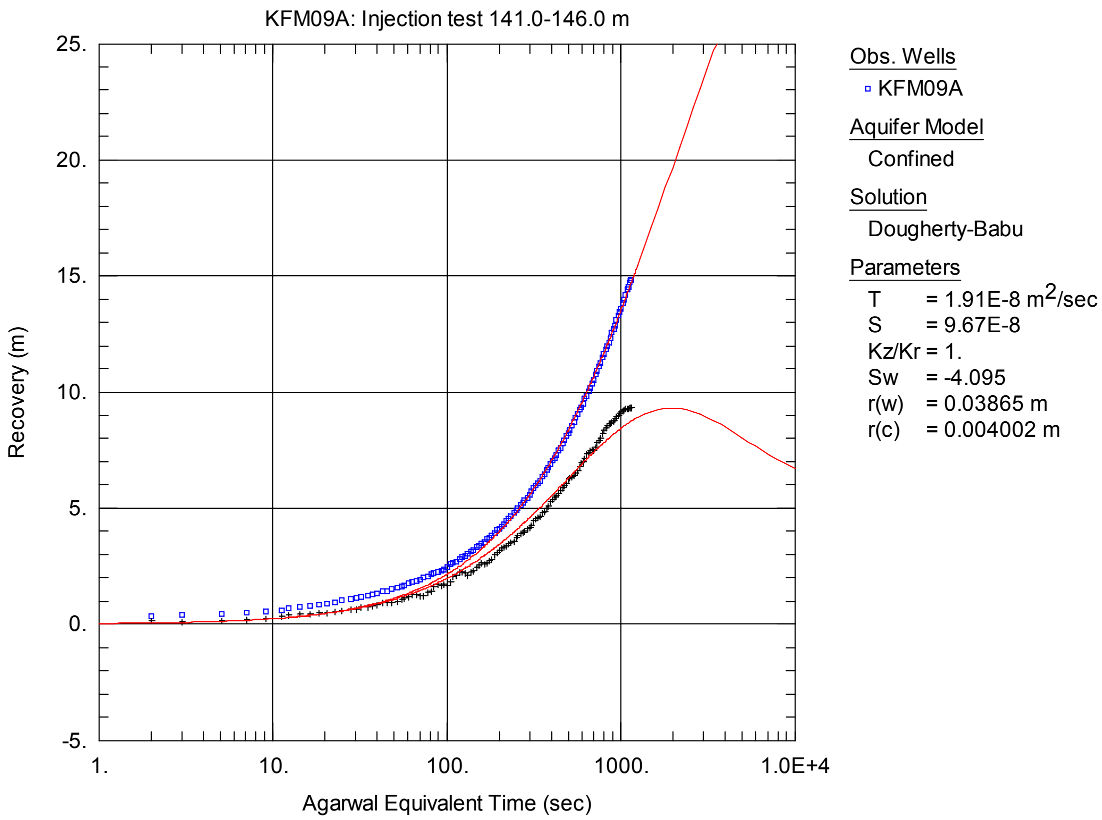


Figure A3-249. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 141.0-146.0 m in KFM09A.*

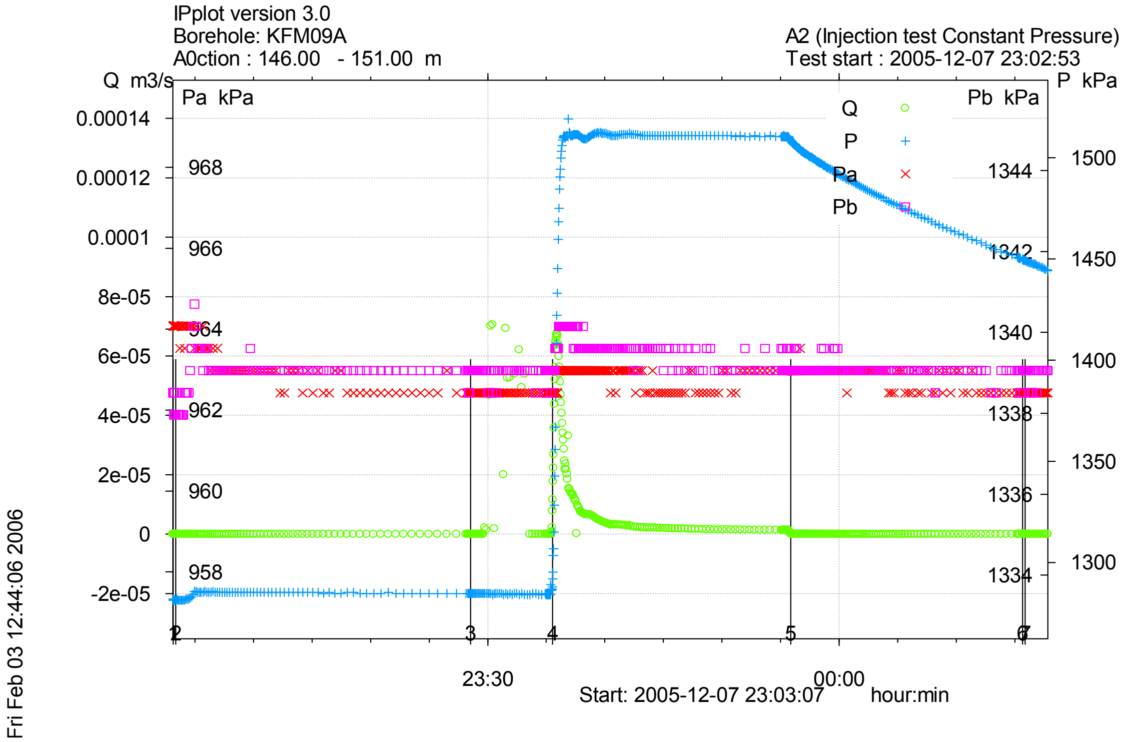


Figure A3-250. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 146.0-151.0 m in borehole KFM09A.*

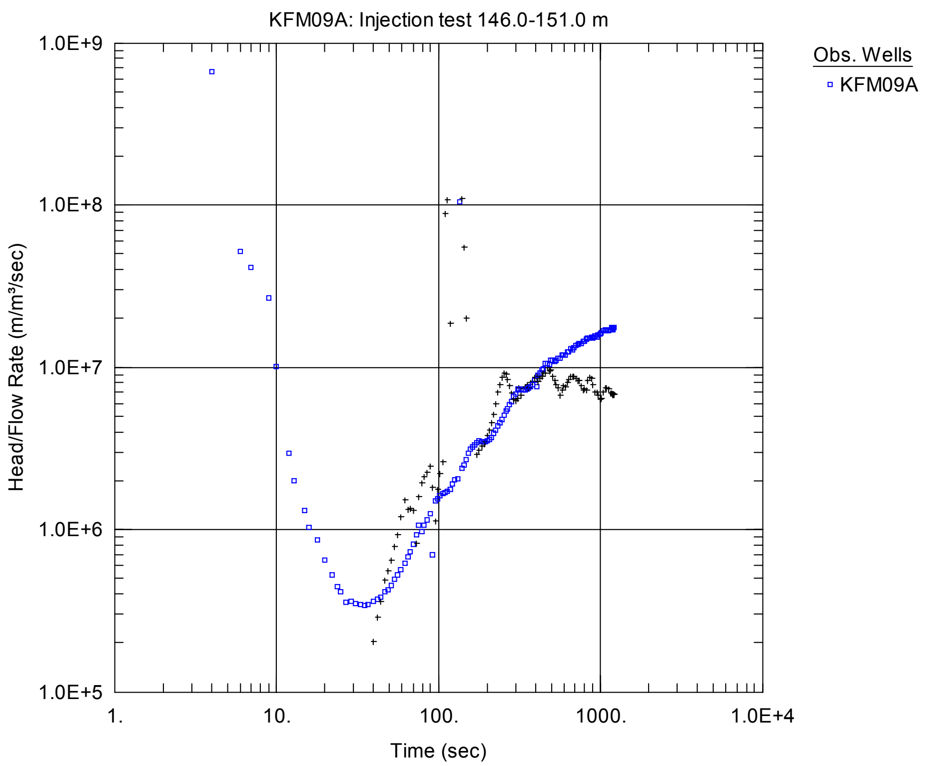


Figure A3-251. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 146.0-151.0 m in KFM09A.*

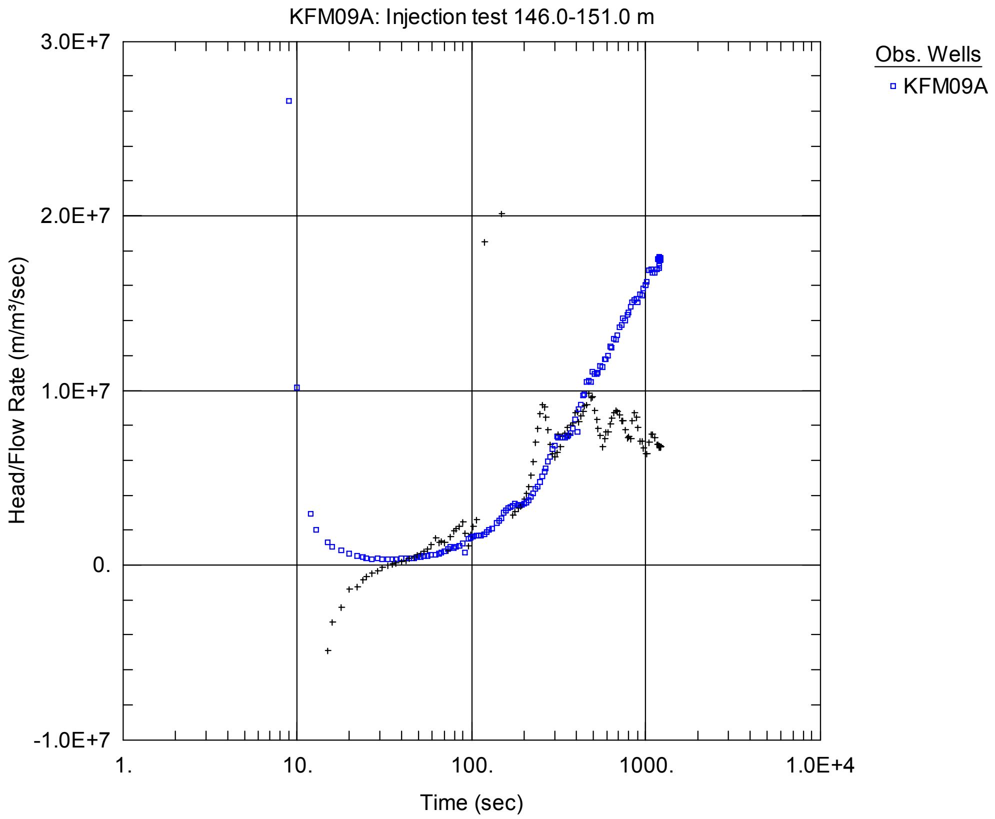


Figure A3-252. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 146.0-151.0 m in KFM09A.*

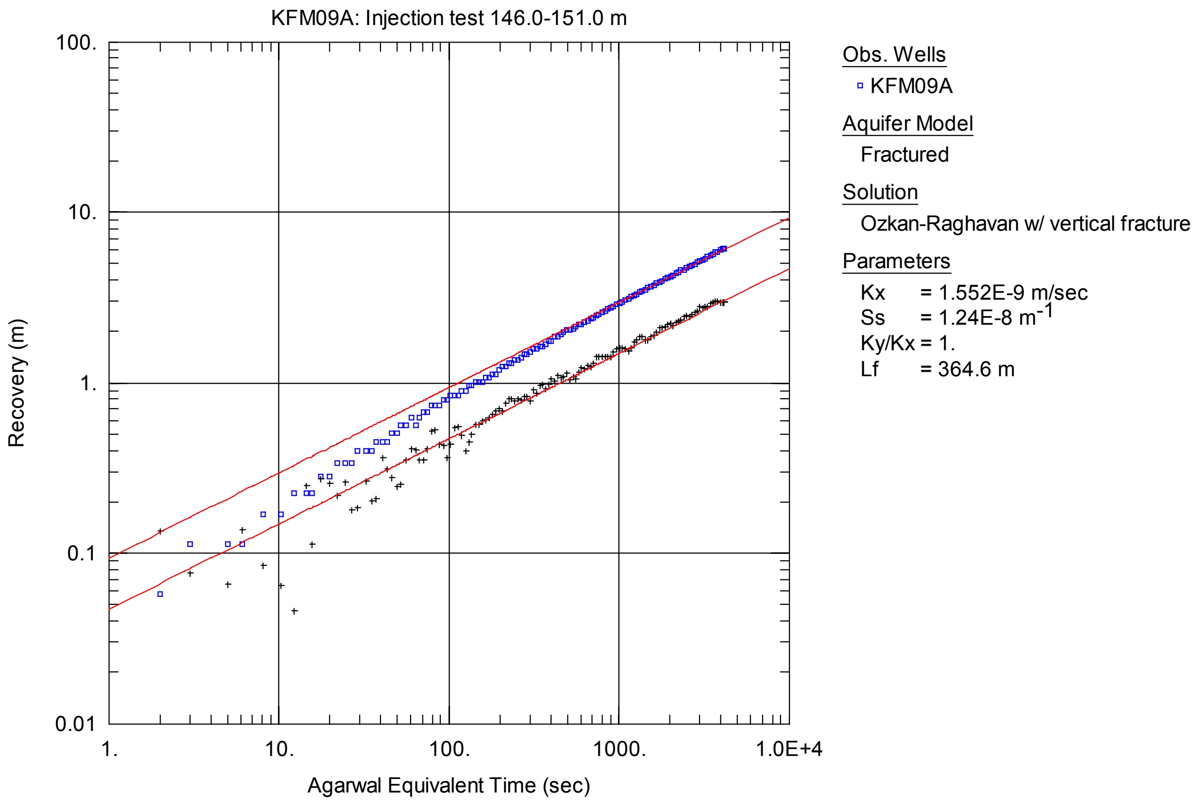


Figure A3-253. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 146.0-151.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

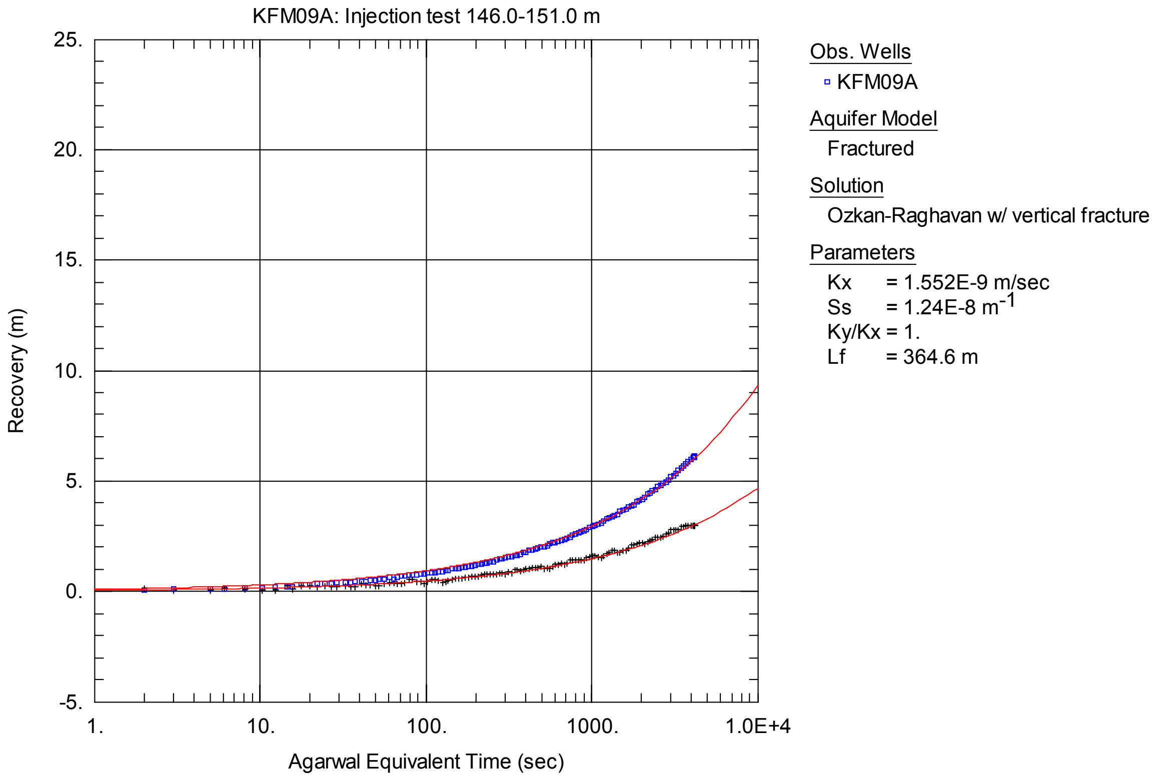


***Figure A3-254.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 146.0-151.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

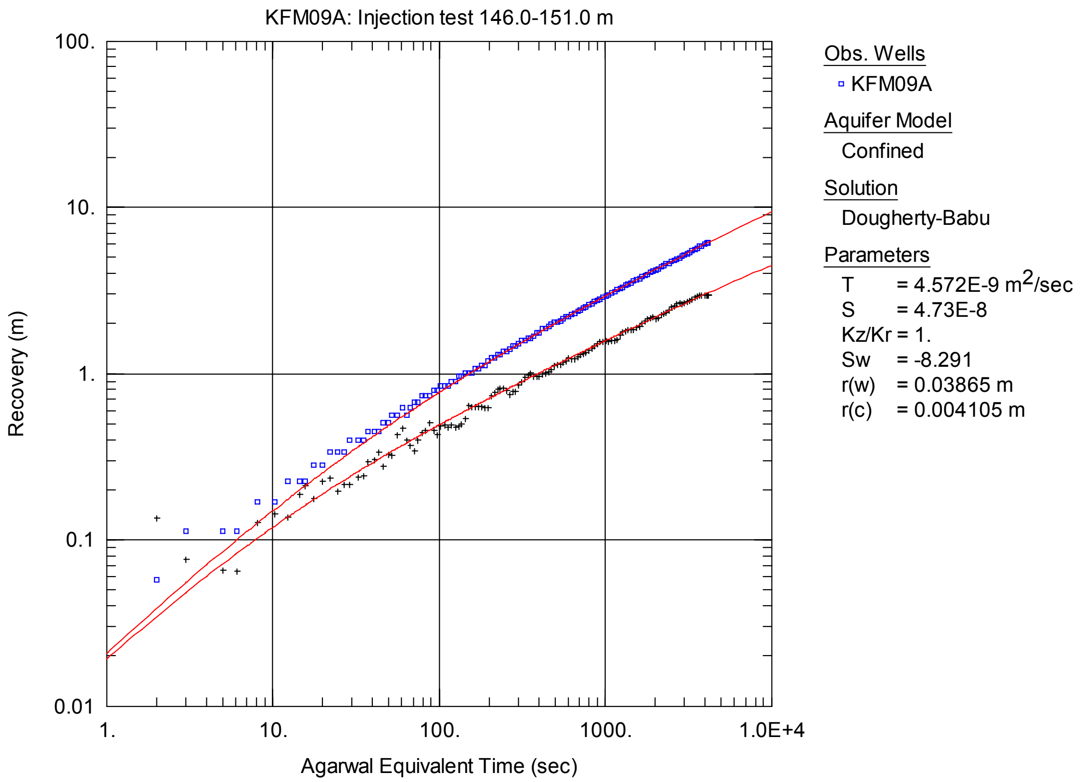


***Figure A3-255.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 146.0-151.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

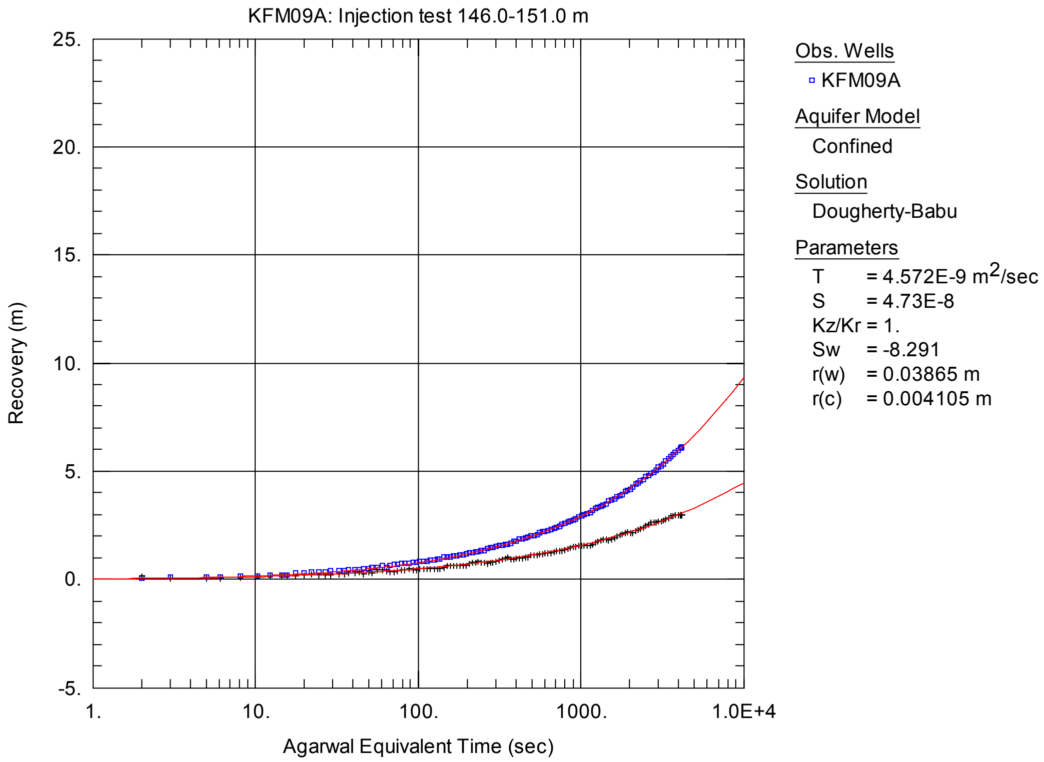


Figure A3-256. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 146.0-151.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

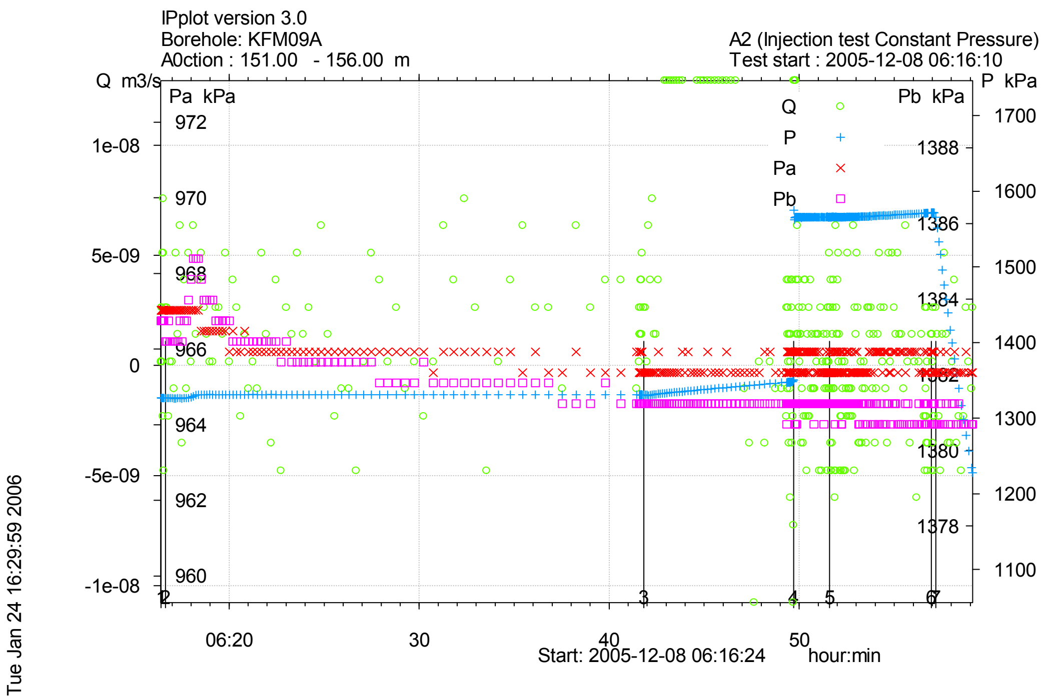


Figure A3-257. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 151.0-156.0 m in borehole KFM09A.*

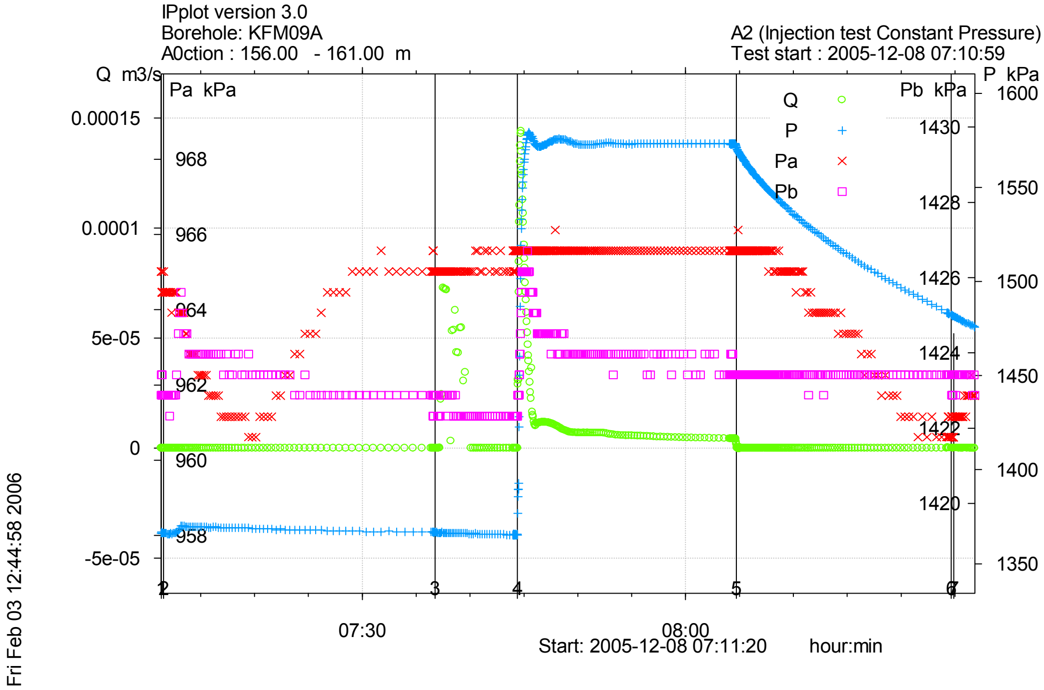


Figure A3-258. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 156.0-161.0 m in borehole KFM09A.*

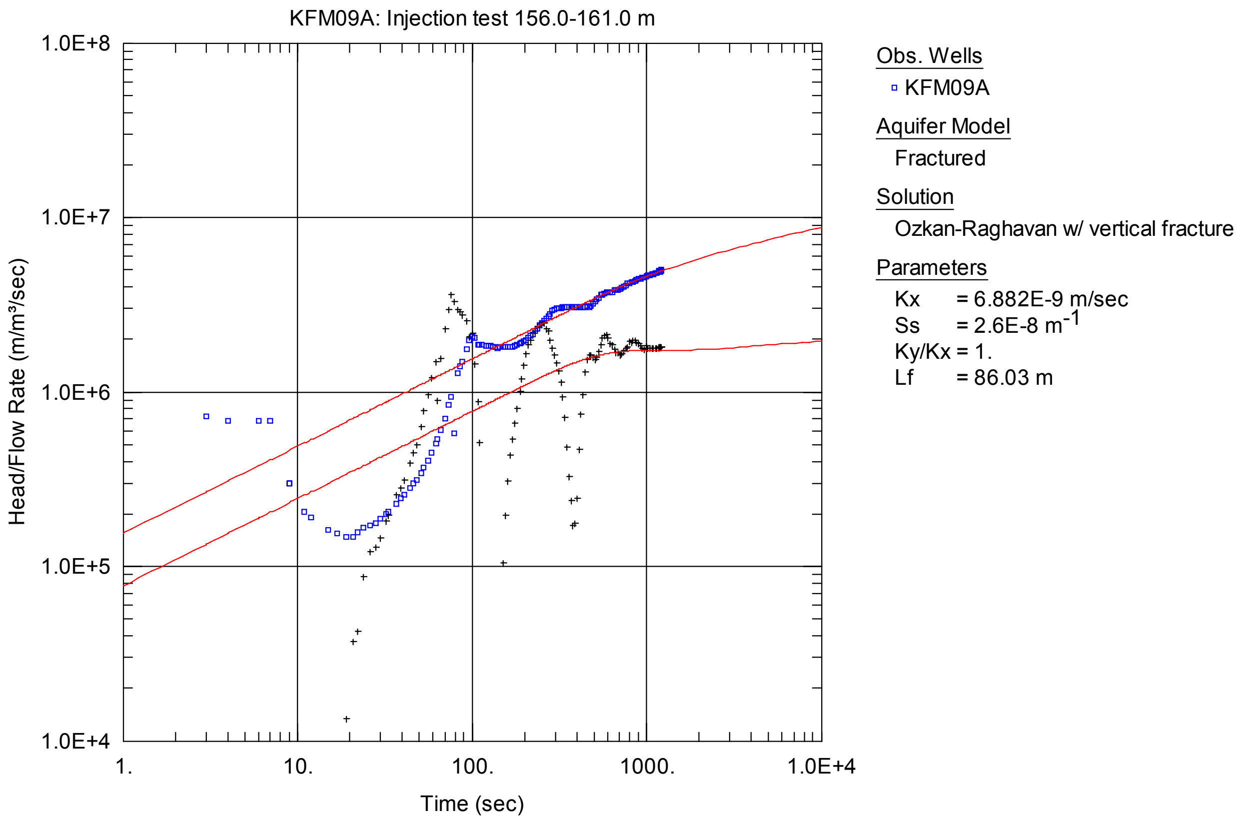


Figure A3-259. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 156.0-161.0 m in KFM09A.*

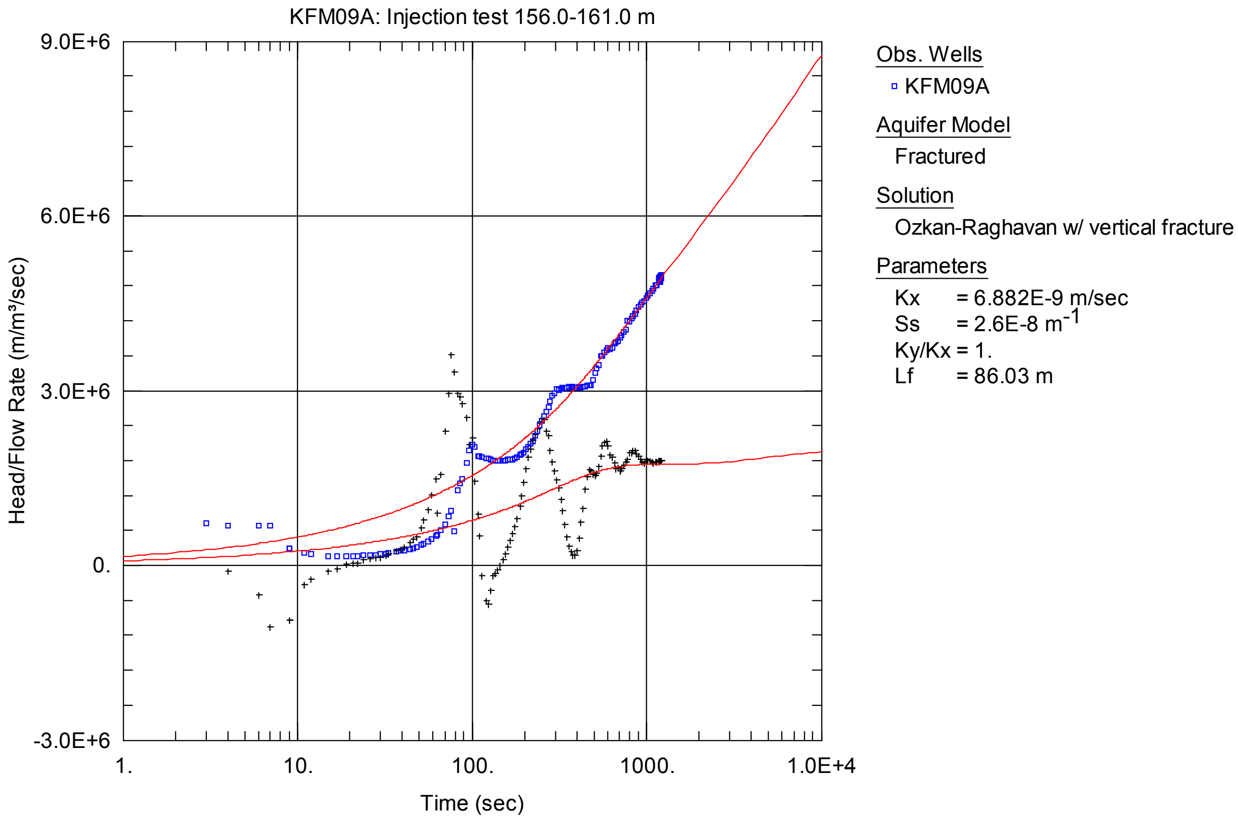


Figure A3-260. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 156.0-161.0 m in KFM09A.*

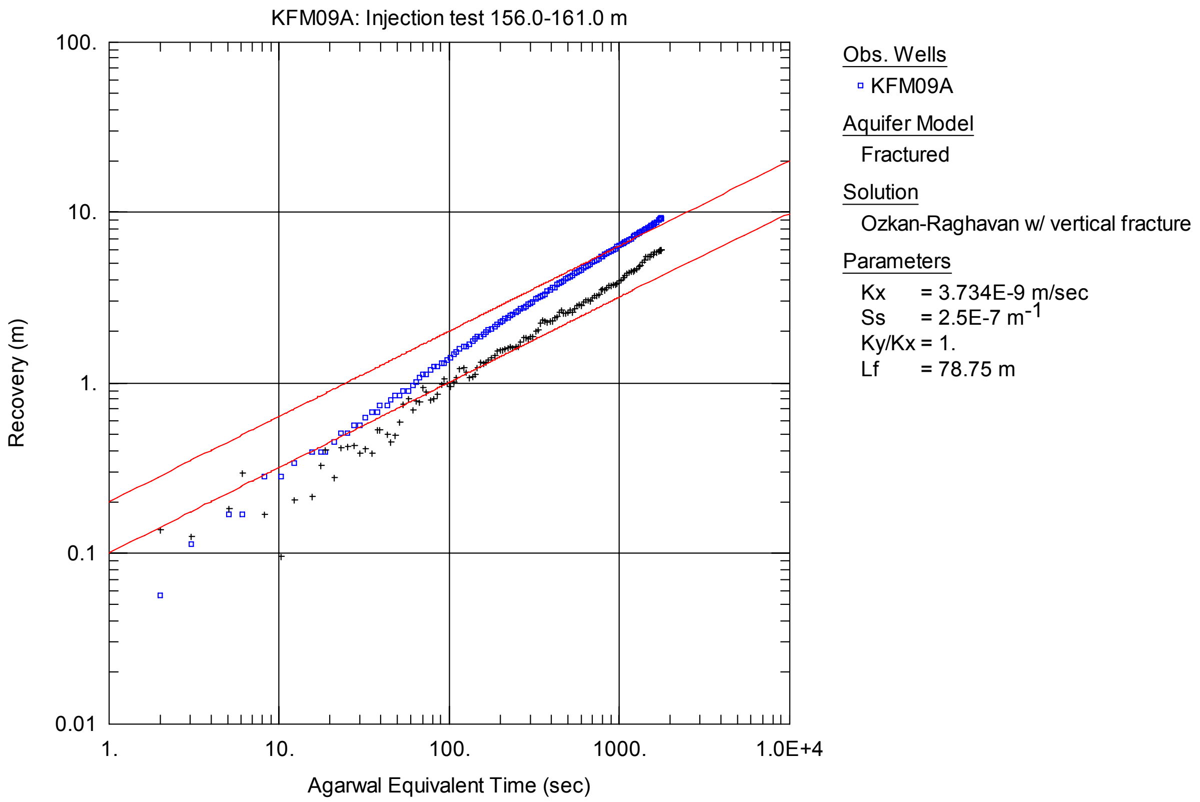


Figure A3-261. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 156.0-161.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.*

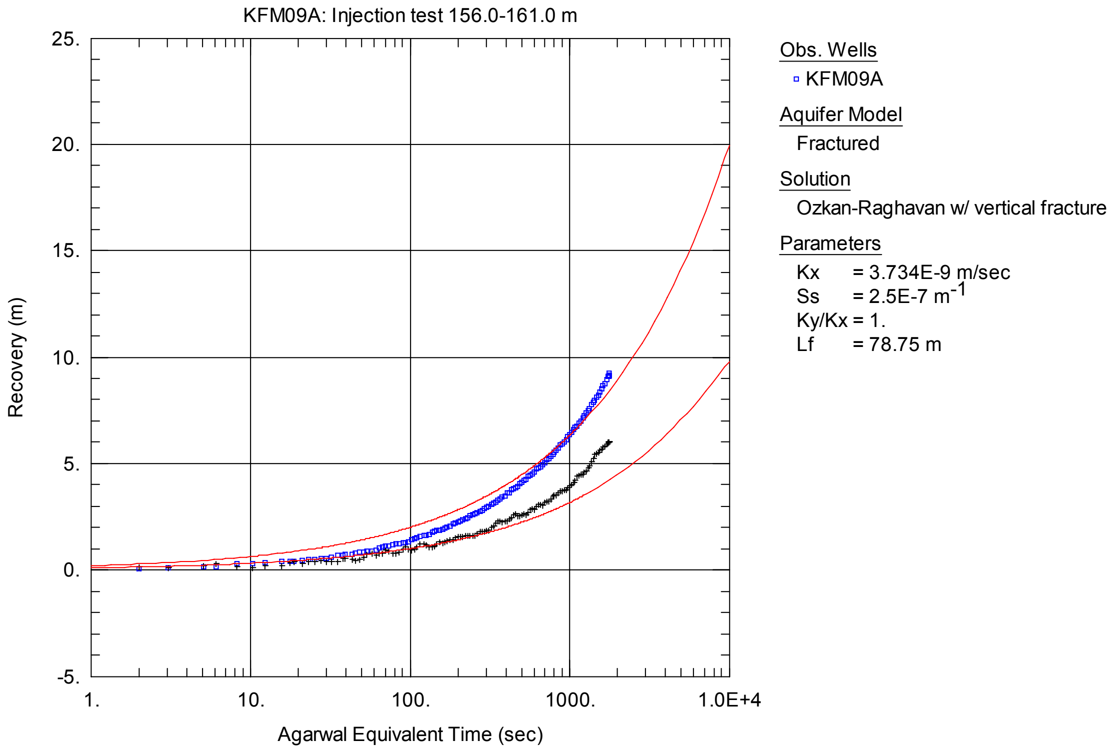


Figure A3-262. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 156.0-161.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.*

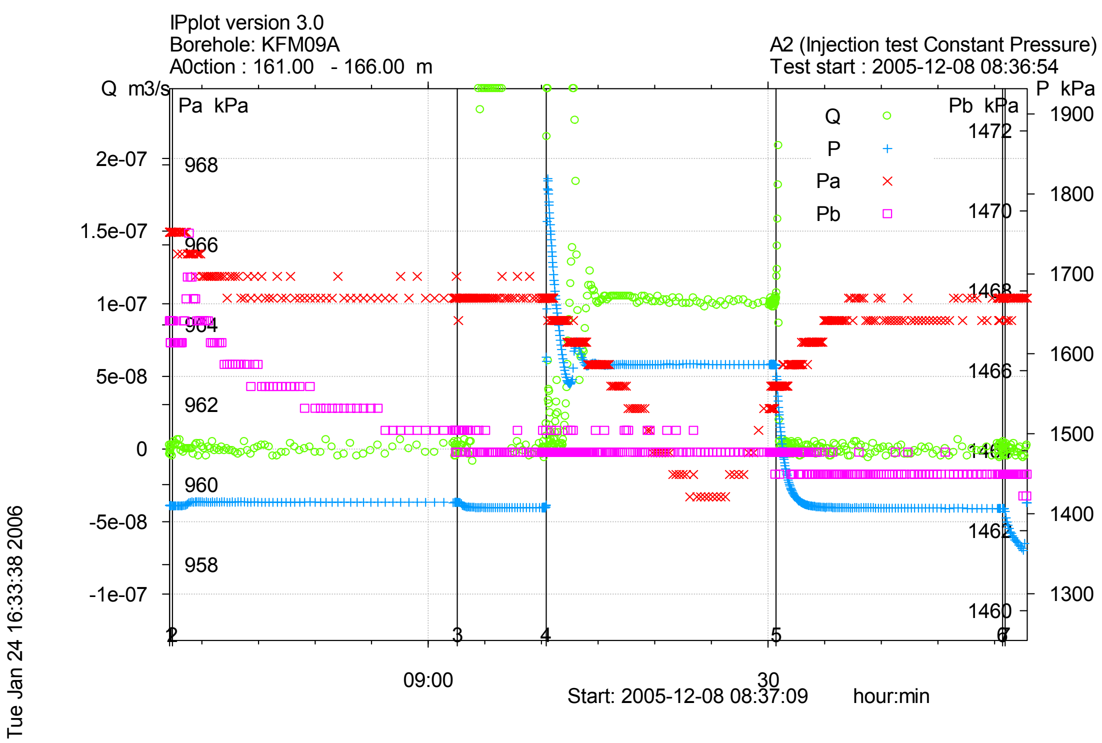


Figure A3-263. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 161.0-166.0 m in borehole KFM09A.*

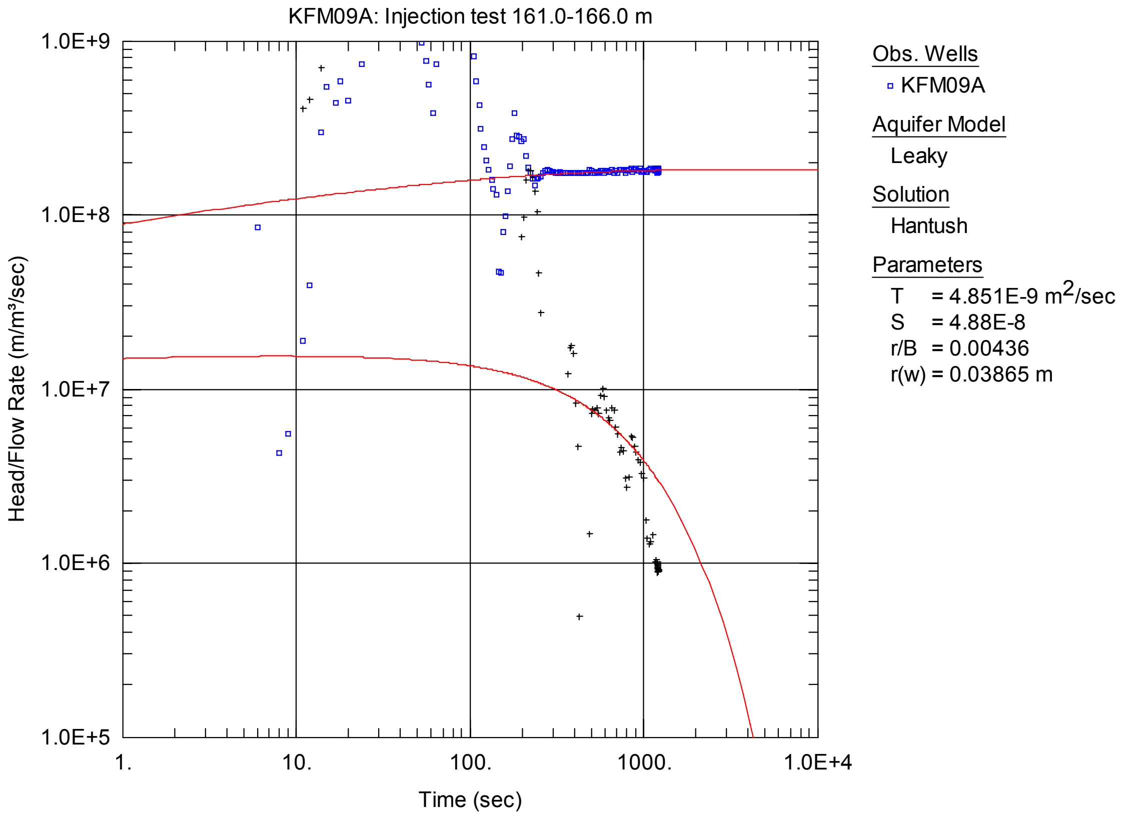


***Figure A3-264.** Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 161.0-166.0 m in KFM09A.*

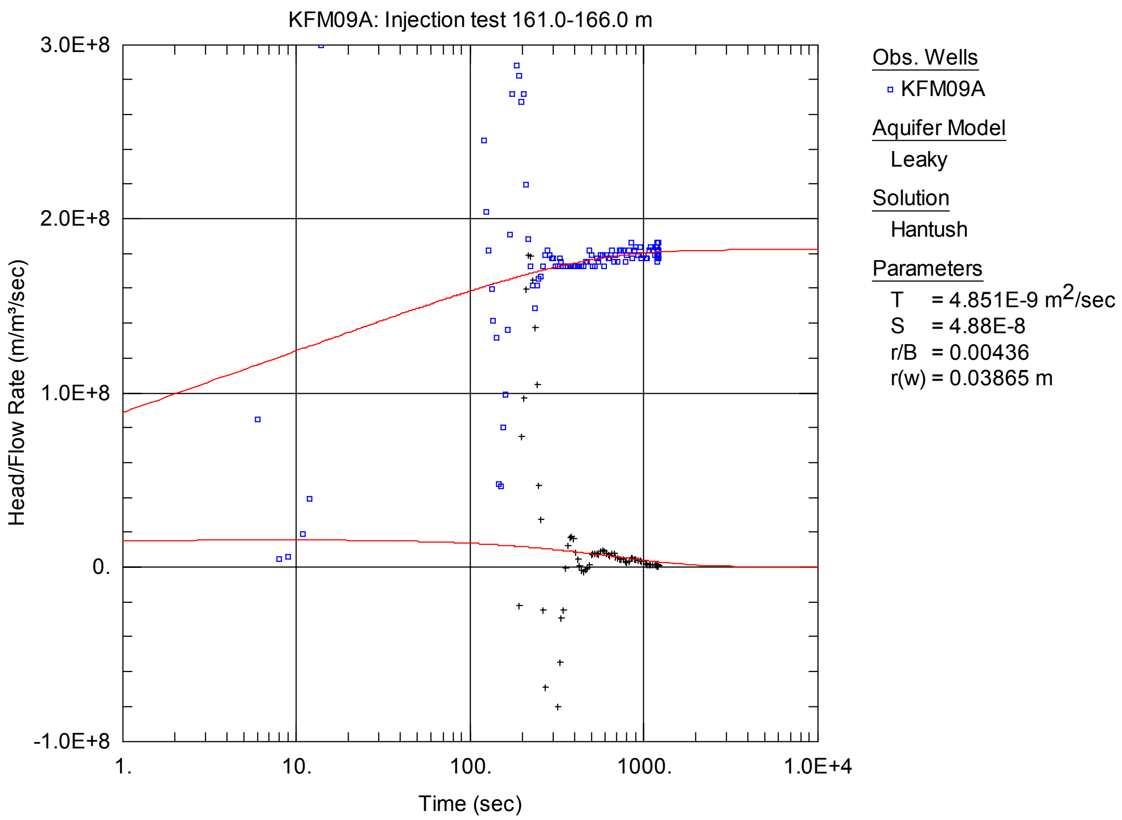


***Figure A3-265.** Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 161.0-166.0 m in KFM09A.*

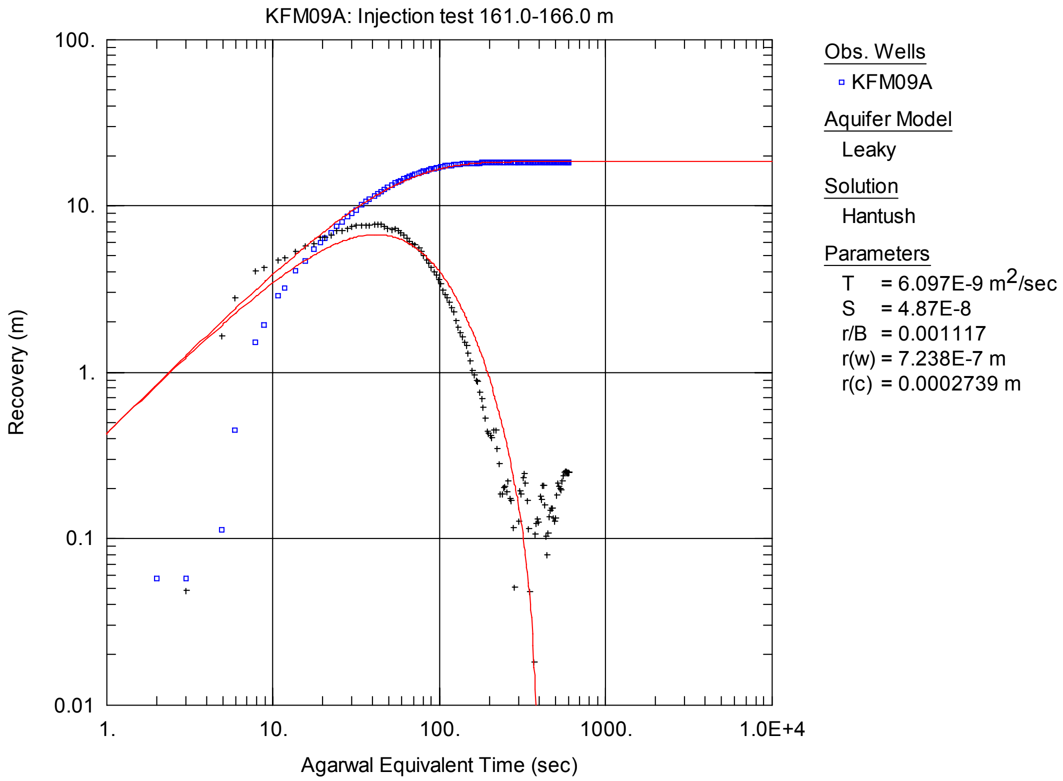


Figure A3-266. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 161.0-166.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.*

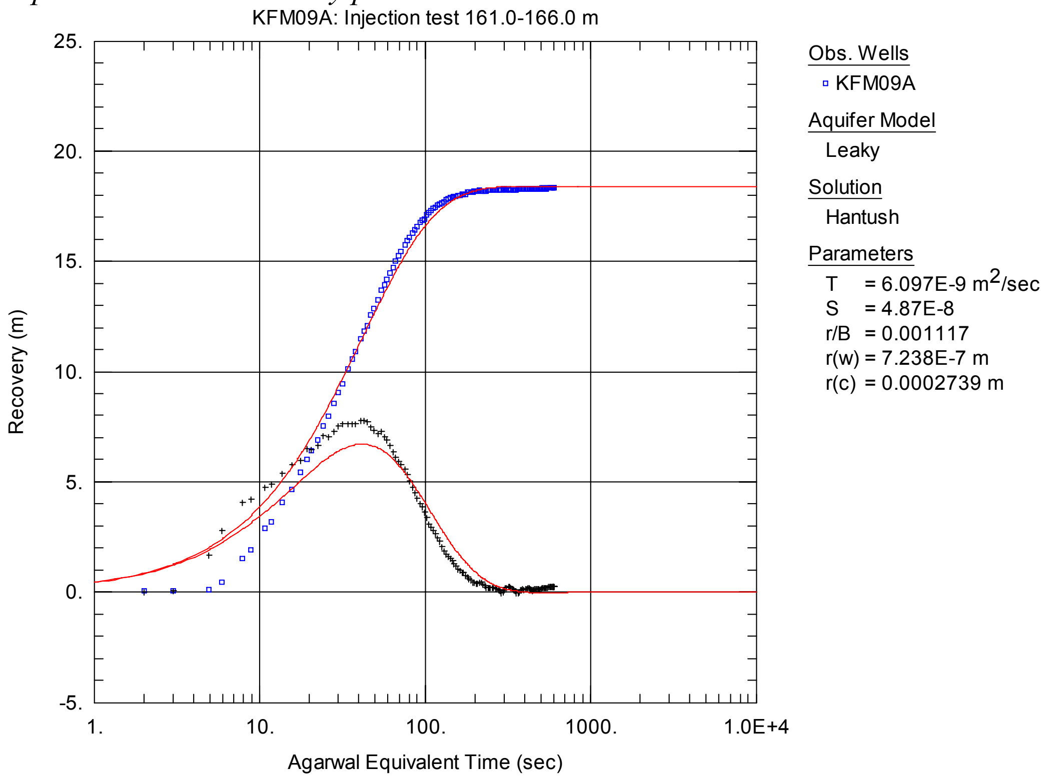


Figure A3-267. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 161.0-166.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.*

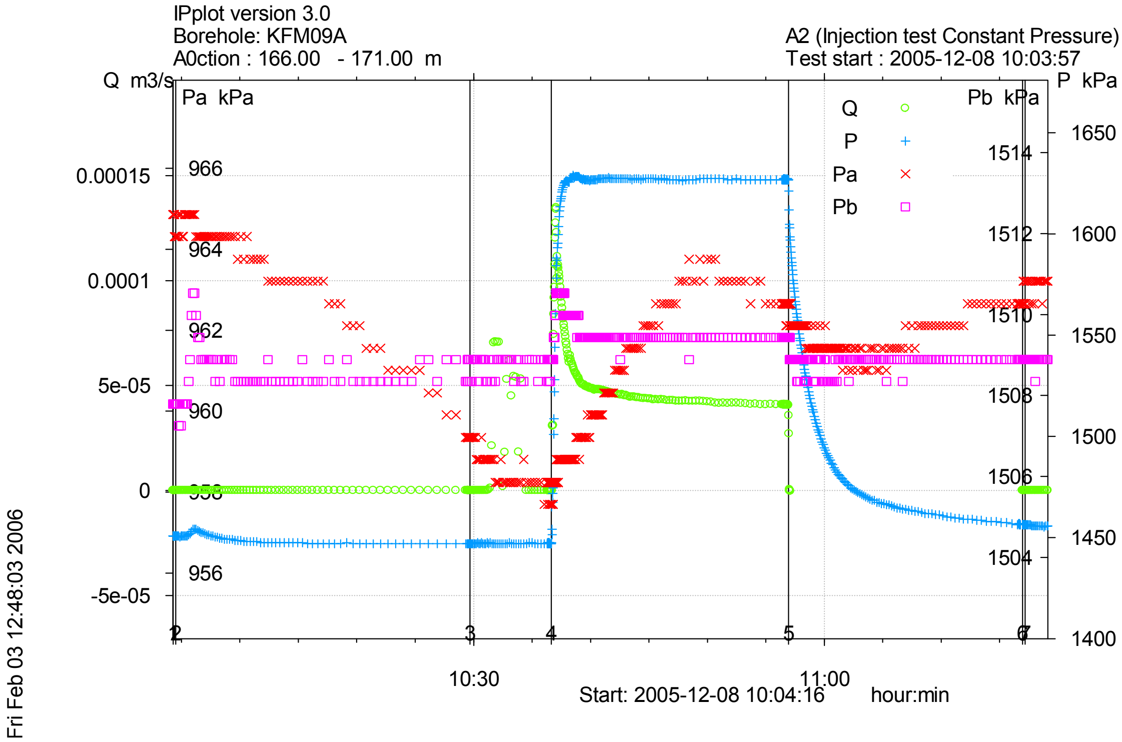


Figure A3-268. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 166.0-171.0 m in borehole KFM09A.

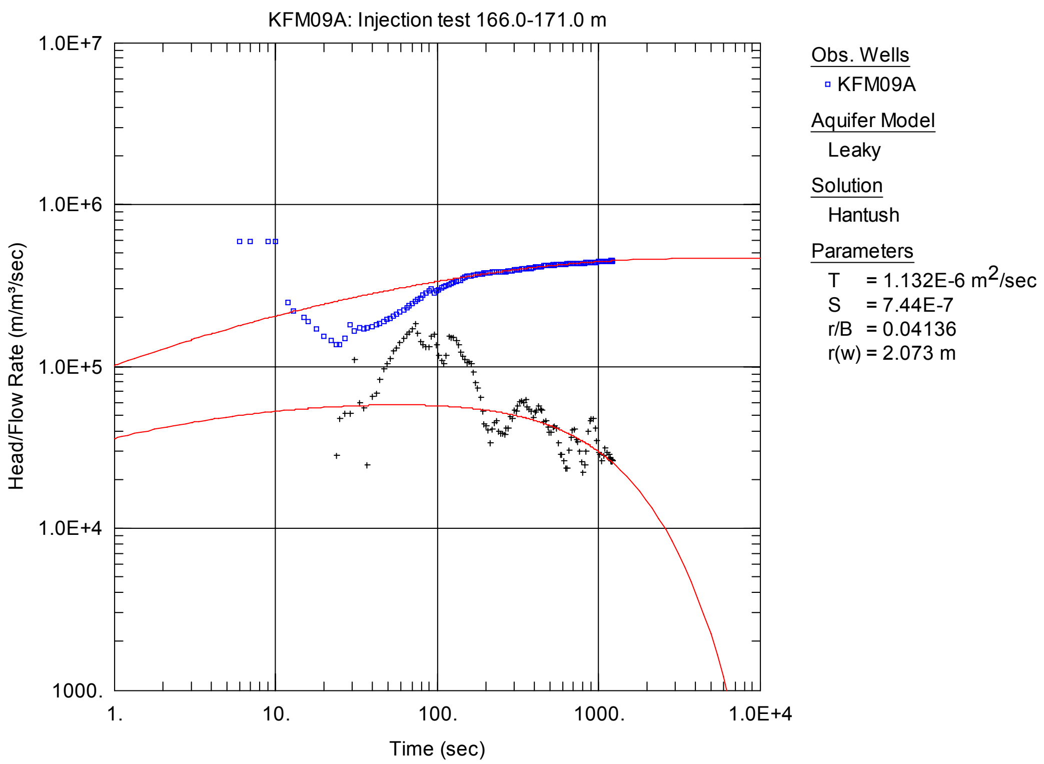


Figure A3-269. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 166.0-171.0 m in KFM09A.

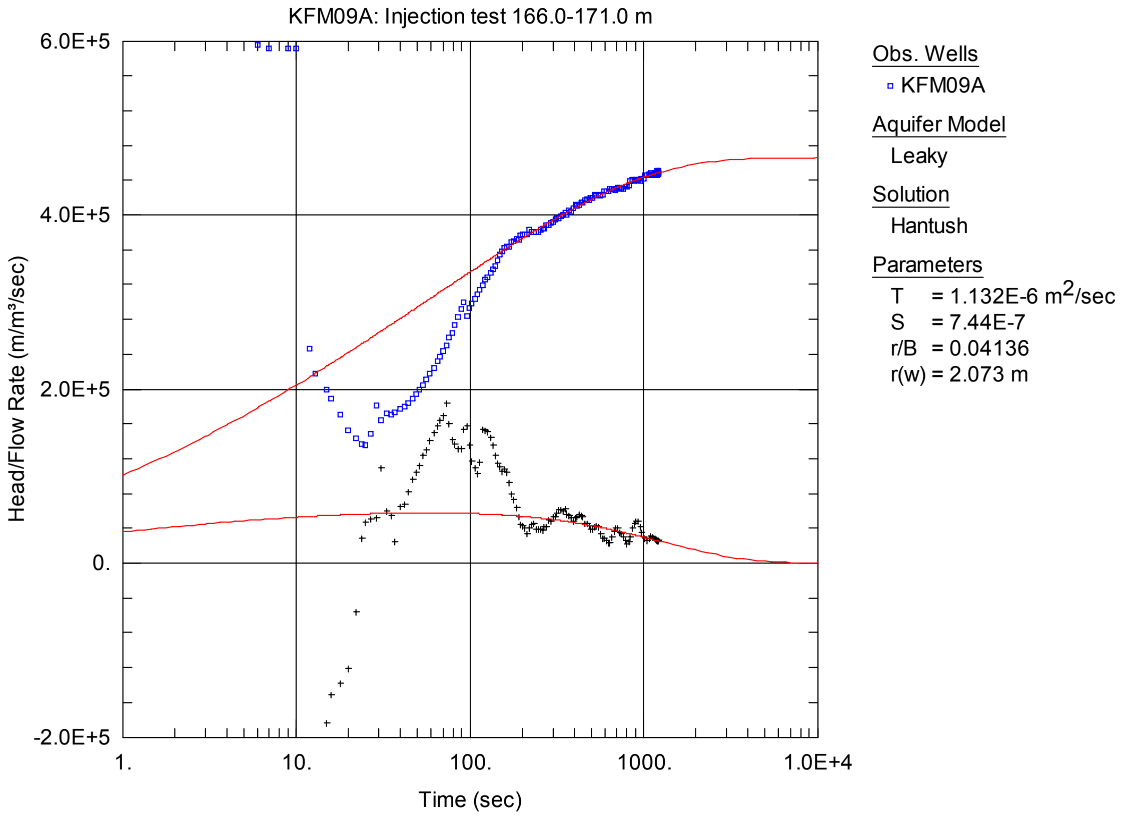


Figure A3-270. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 166.0-171.0 m in KFM09A.*

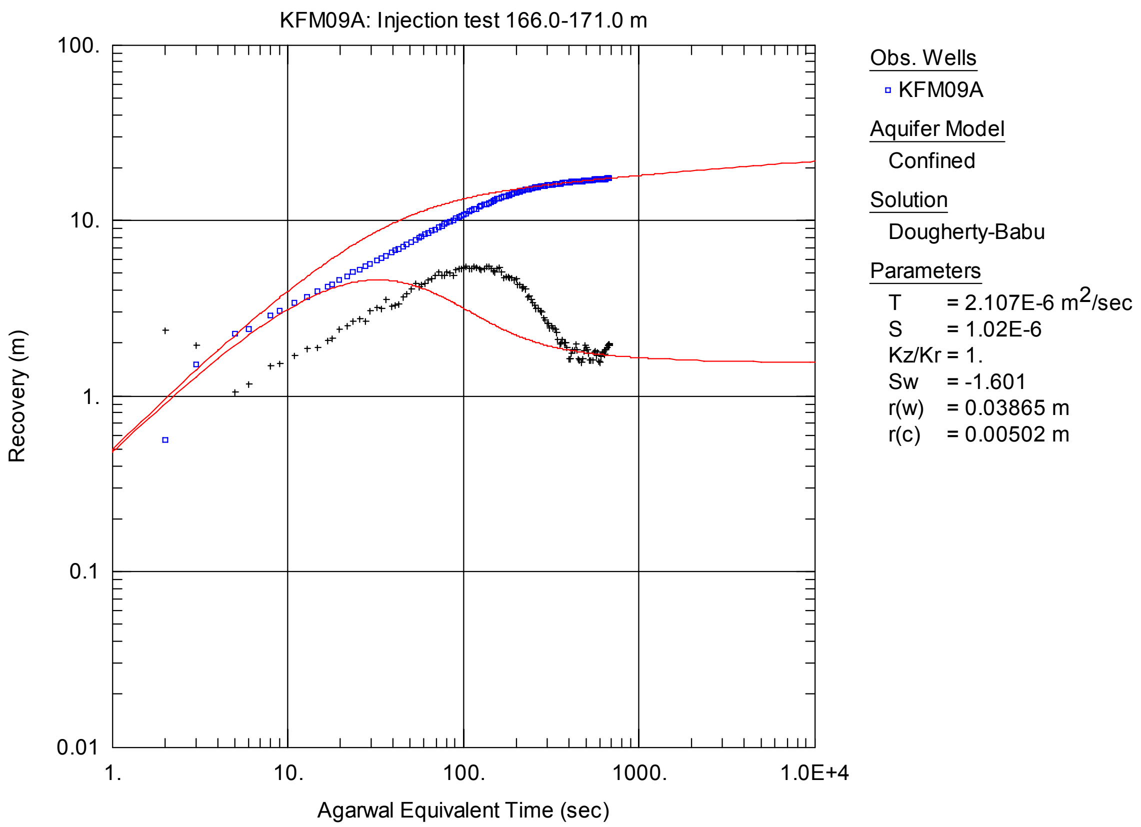


Figure A3-271. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 166.0-171.0 m in KFM09A.*

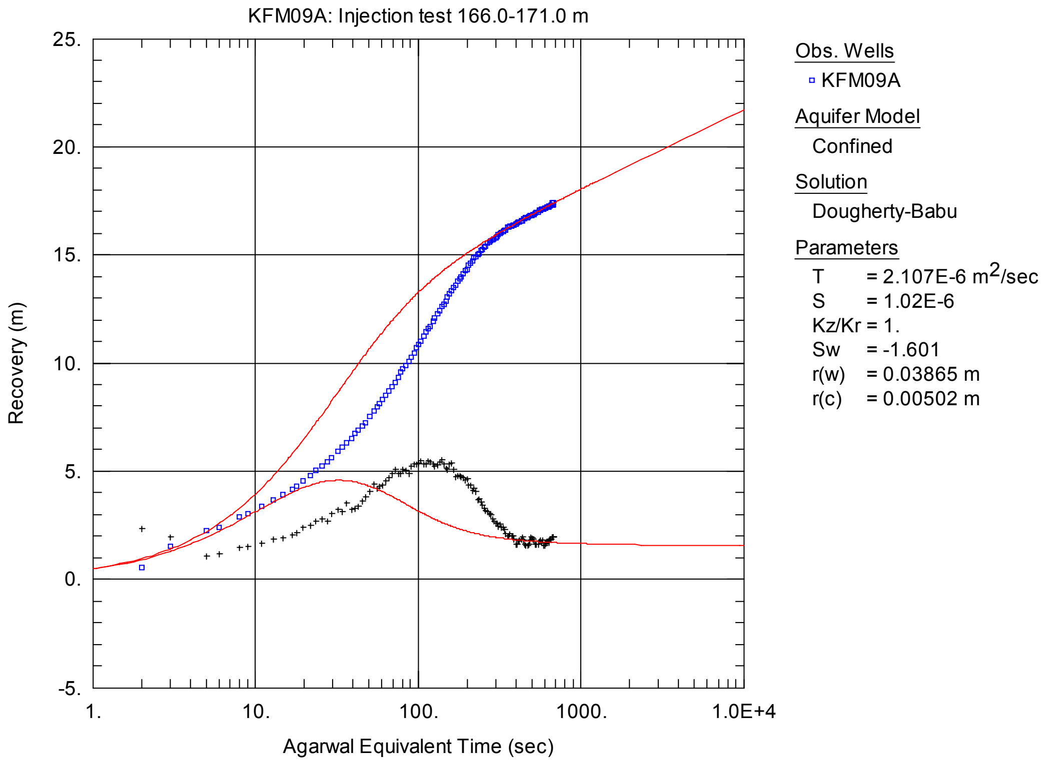


__Figure A3-272.__ Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 166.0-171.0 m in KFM09A.

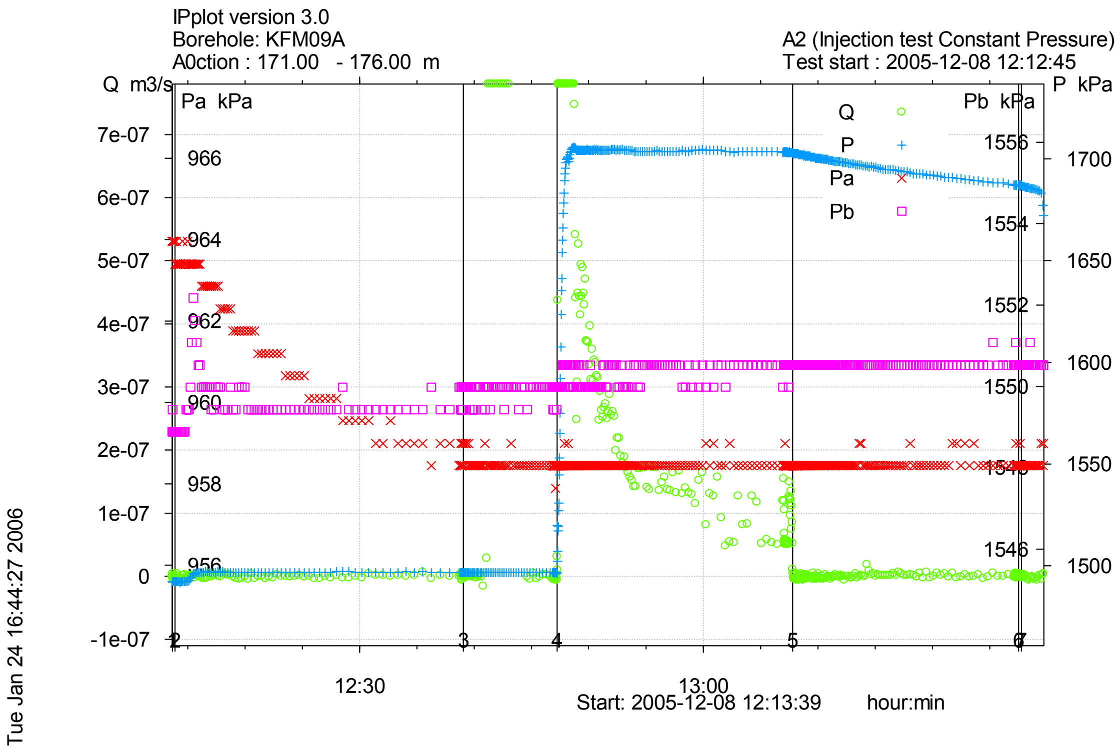


__Figure A3-273.__ Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 171.0-176.0 m in borehole KFM09A

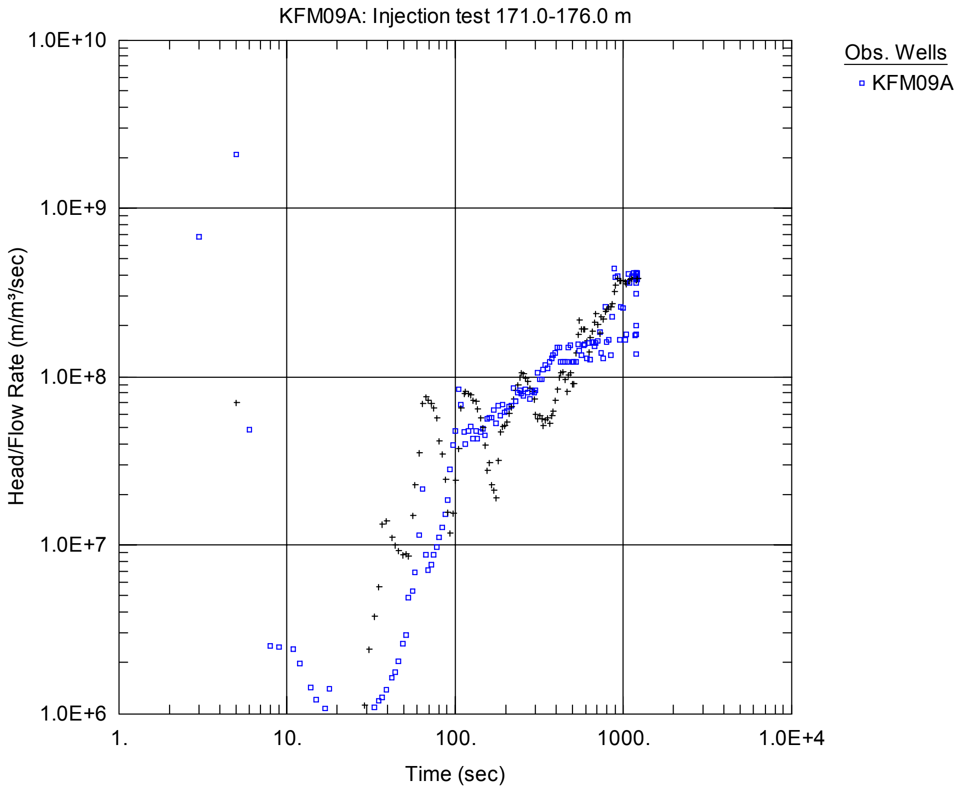


Figure A3-274. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 171.0-176.0 m in KFM09A.*

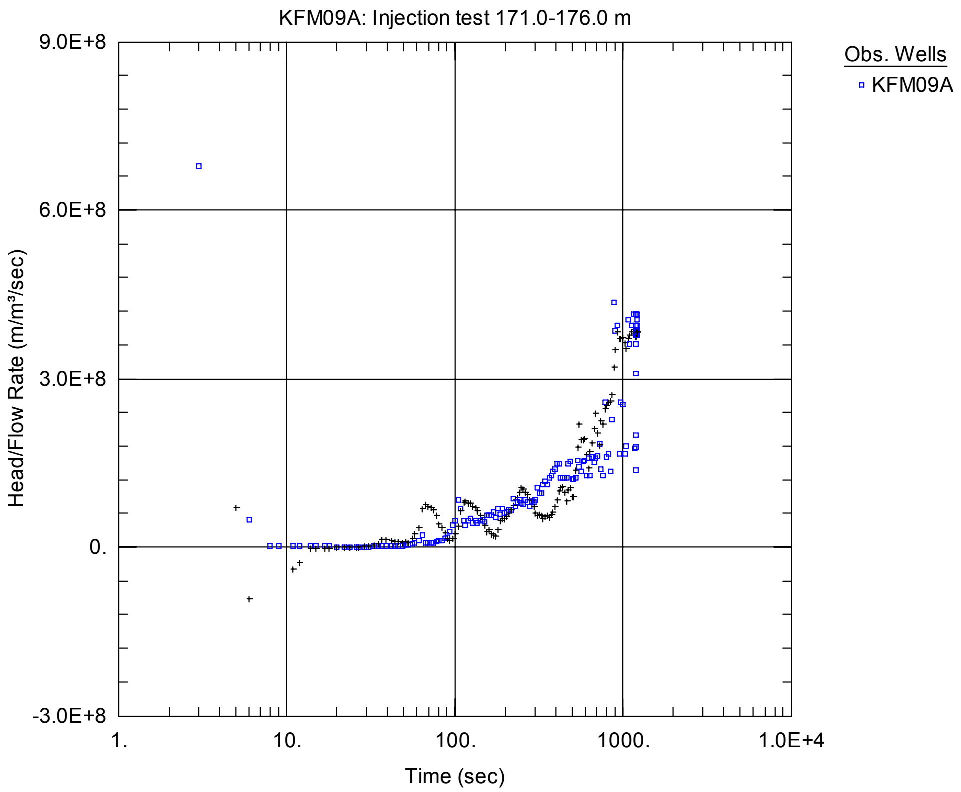


Figure A3-275. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 171.0-176.0 m in KFM09A.*

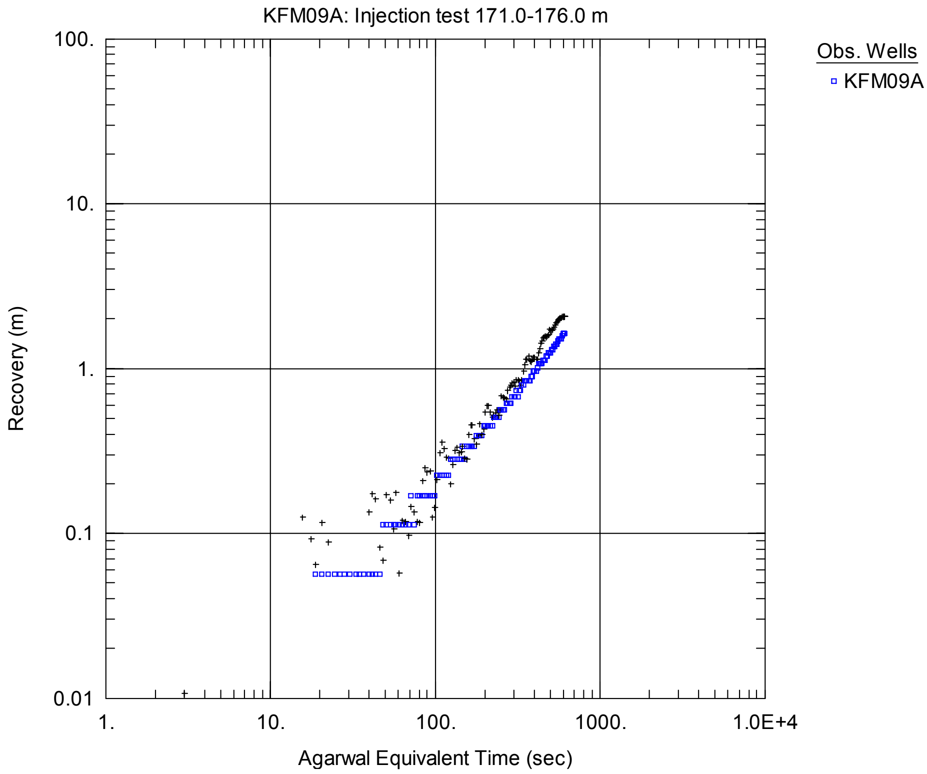


Figure A3-276. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 171.0-176.0 m in KFM09A.*

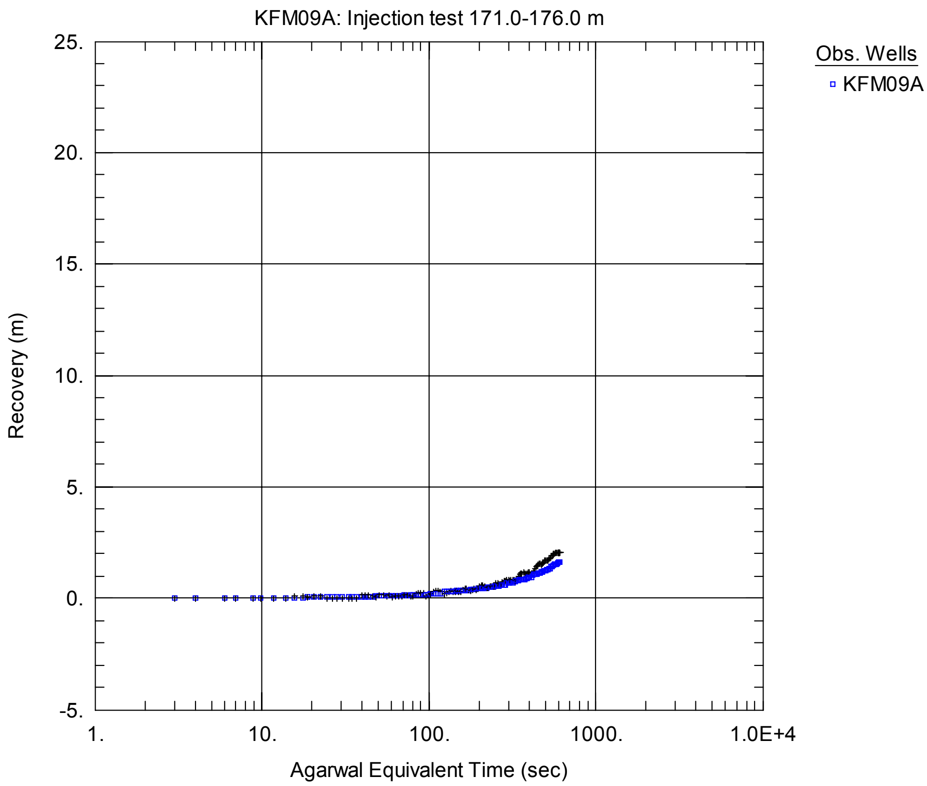


Figure A3-277. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 171.0-176.0 m in KFM09A.*

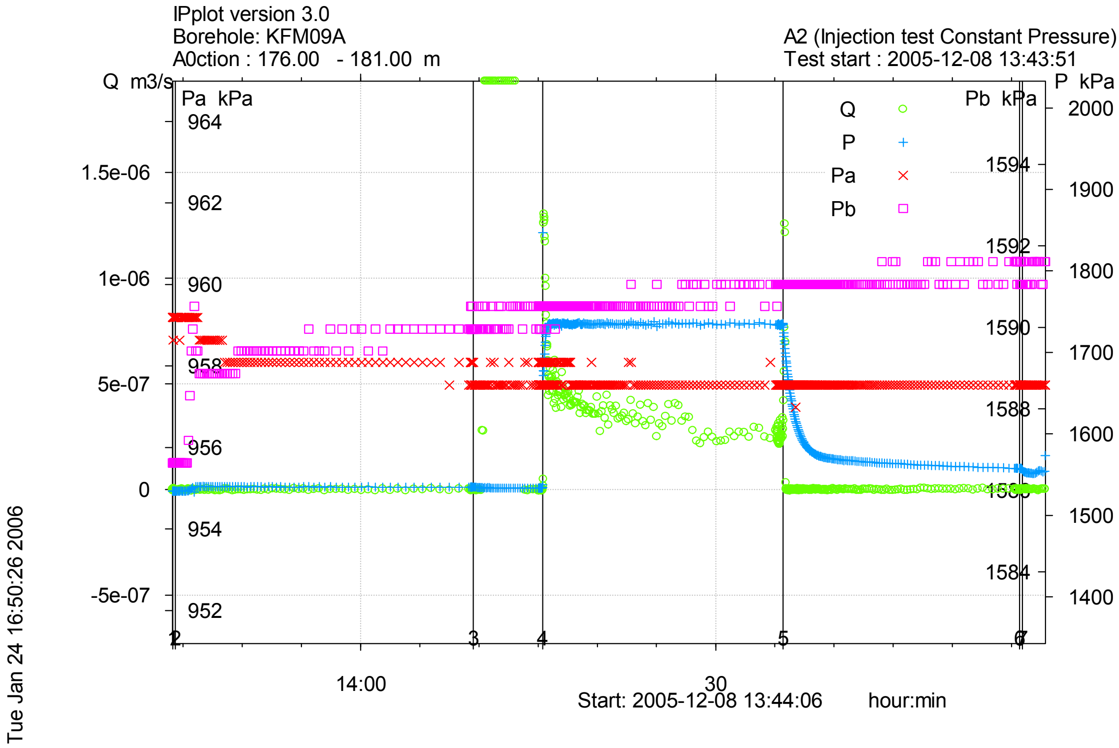


Figure A3-278. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 176.0-181.0 m in borehole KFM09A.*

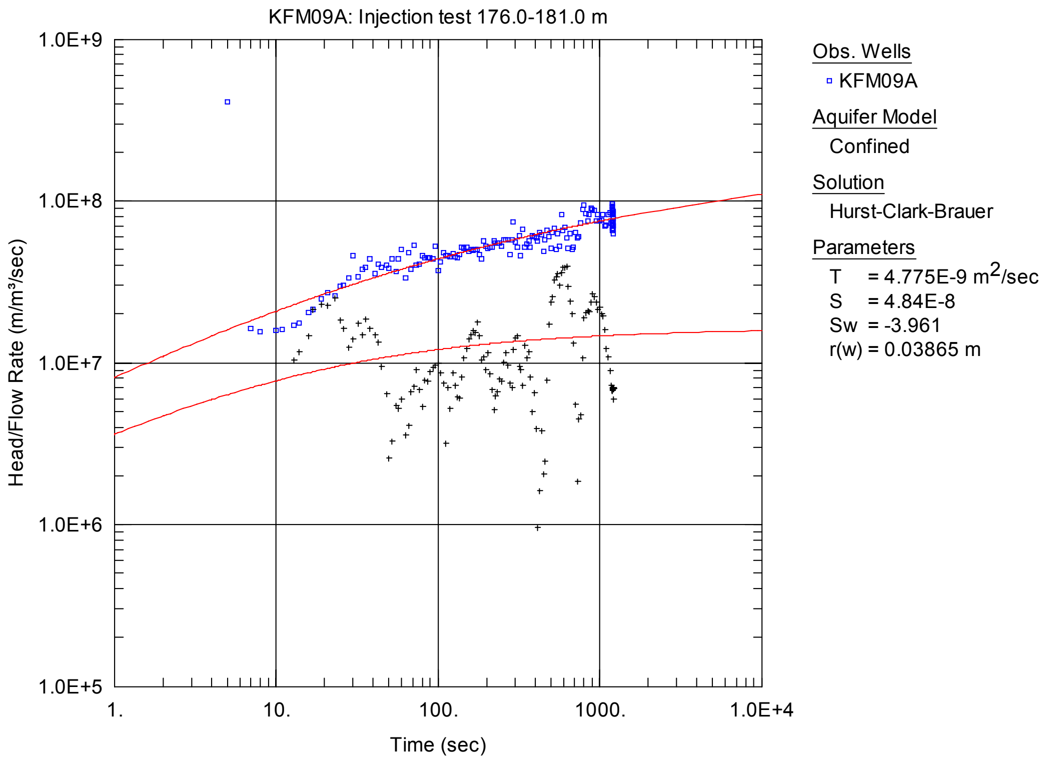


Figure A3-279. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 176.0-181.0 m in KFM09A.*

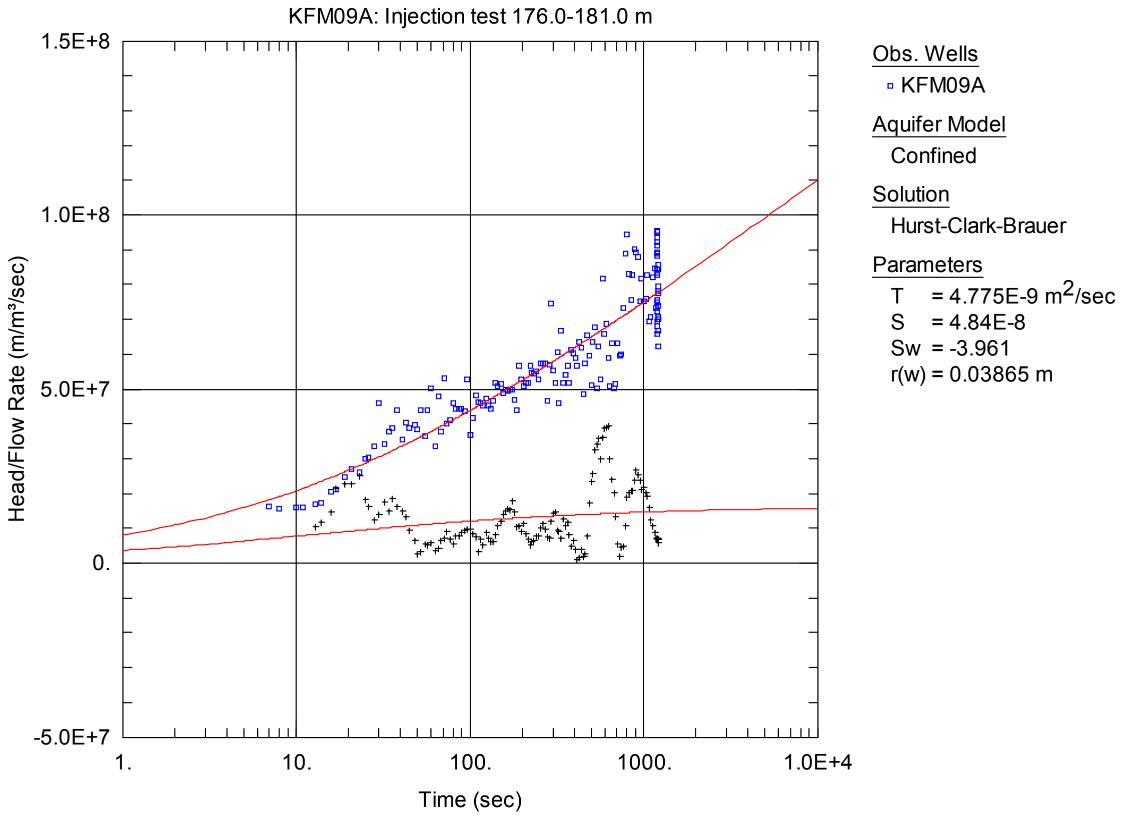


Figure A3-280. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 176.0-181.0 m in KFM09A.*

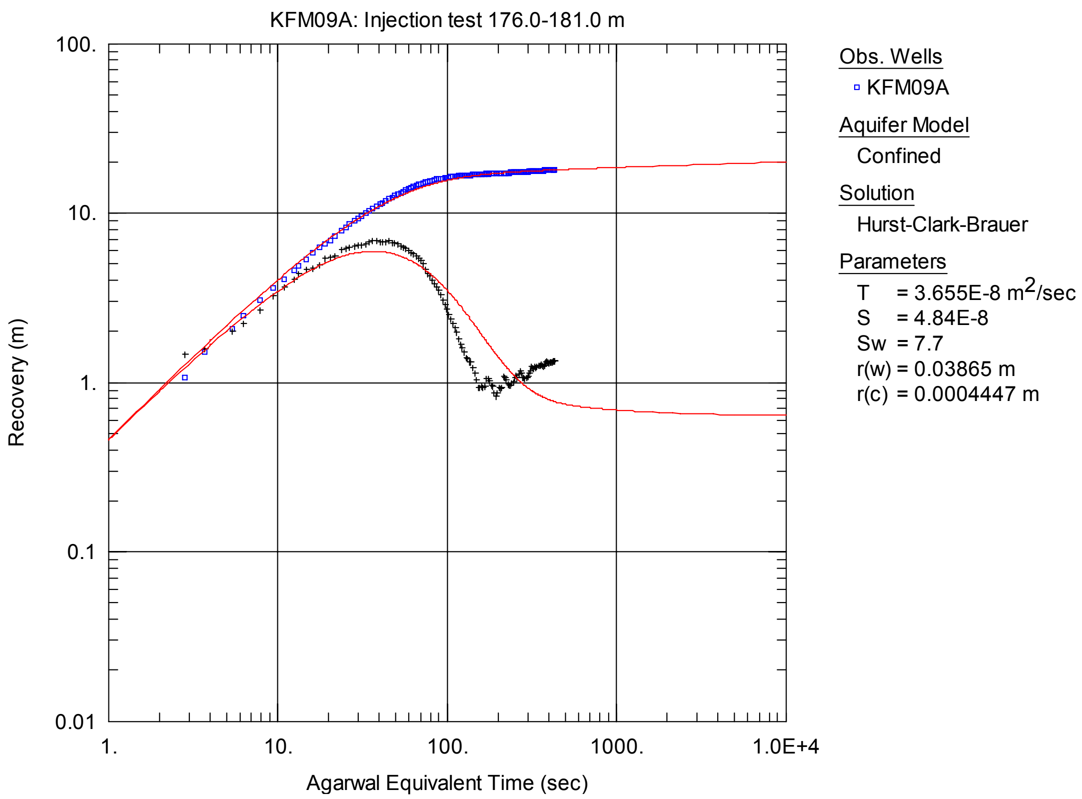


Figure A3-281. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 176.0-181.0 m in KFM09A No unambiguous transient evaluation is possible on the recovery period.*

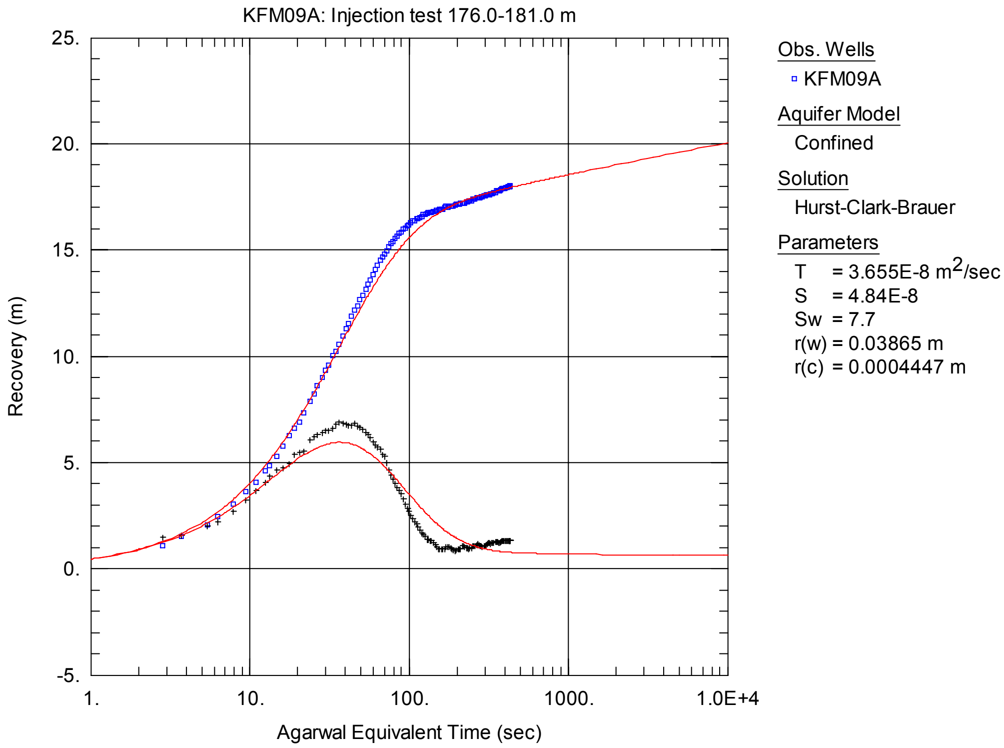


Figure A3-282. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 176.0-181.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.*

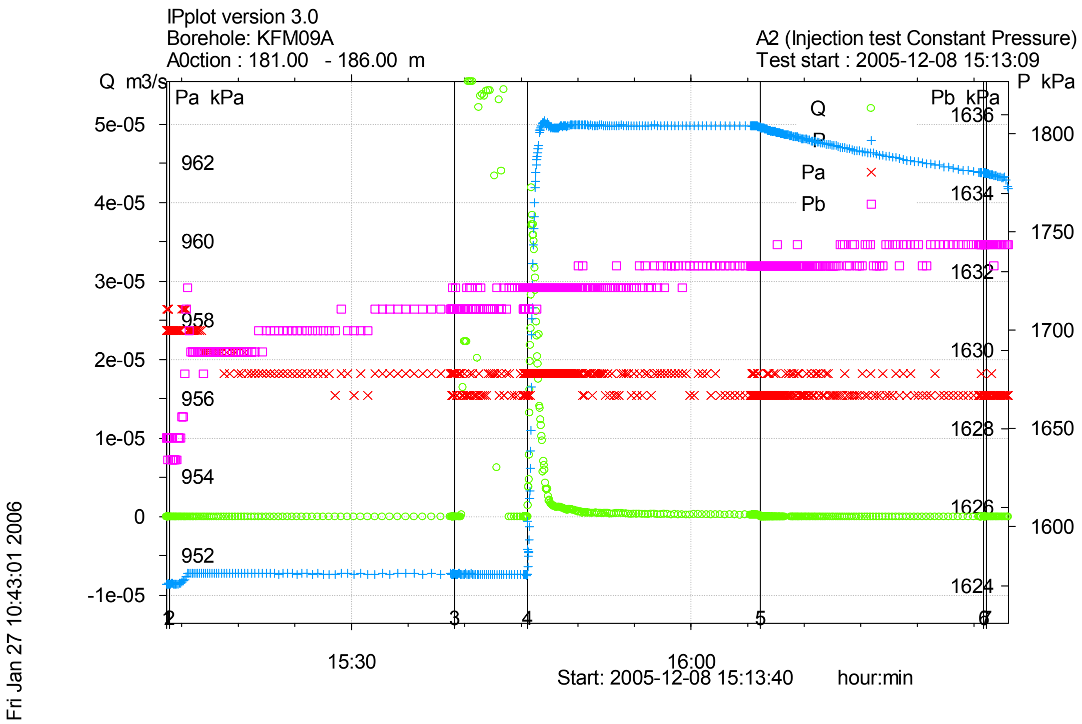


Figure A3-283. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 181.0-186.0 m in borehole KFM09A.*

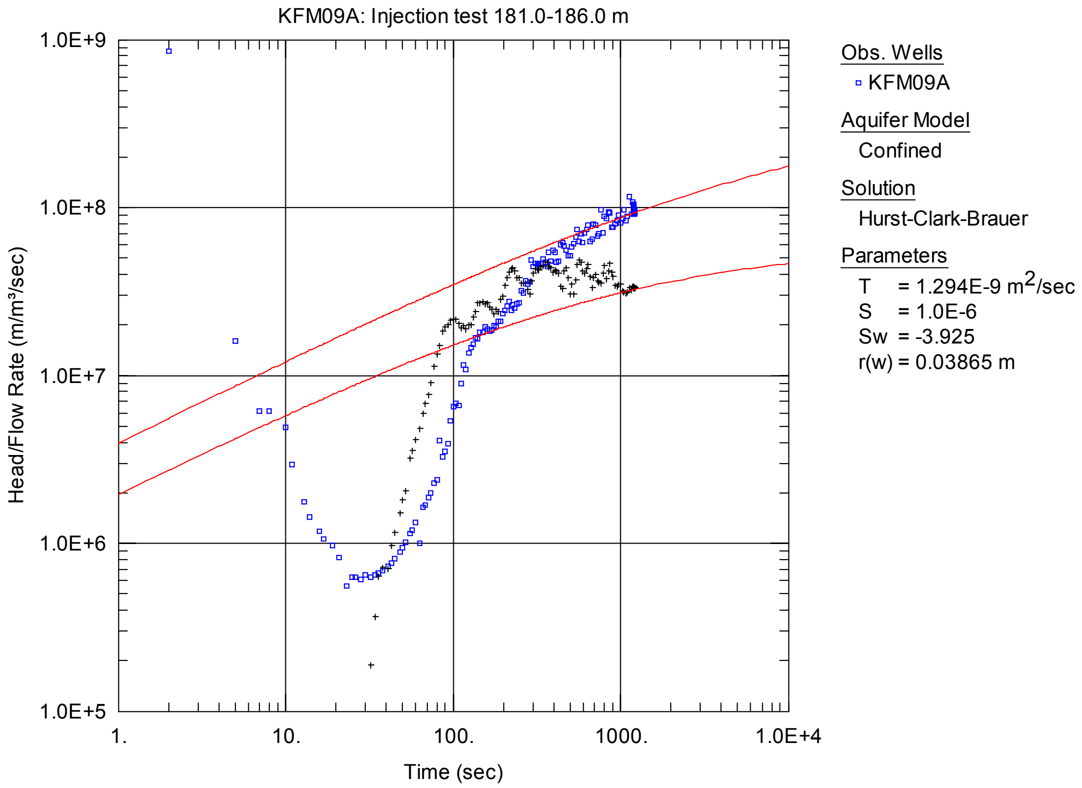


Figure A3-284. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 181.0-186.0 m in KFM09A. A fit with Hurst-Clark-Brauer is not possible and no transient evaluation is possible on the injection.*

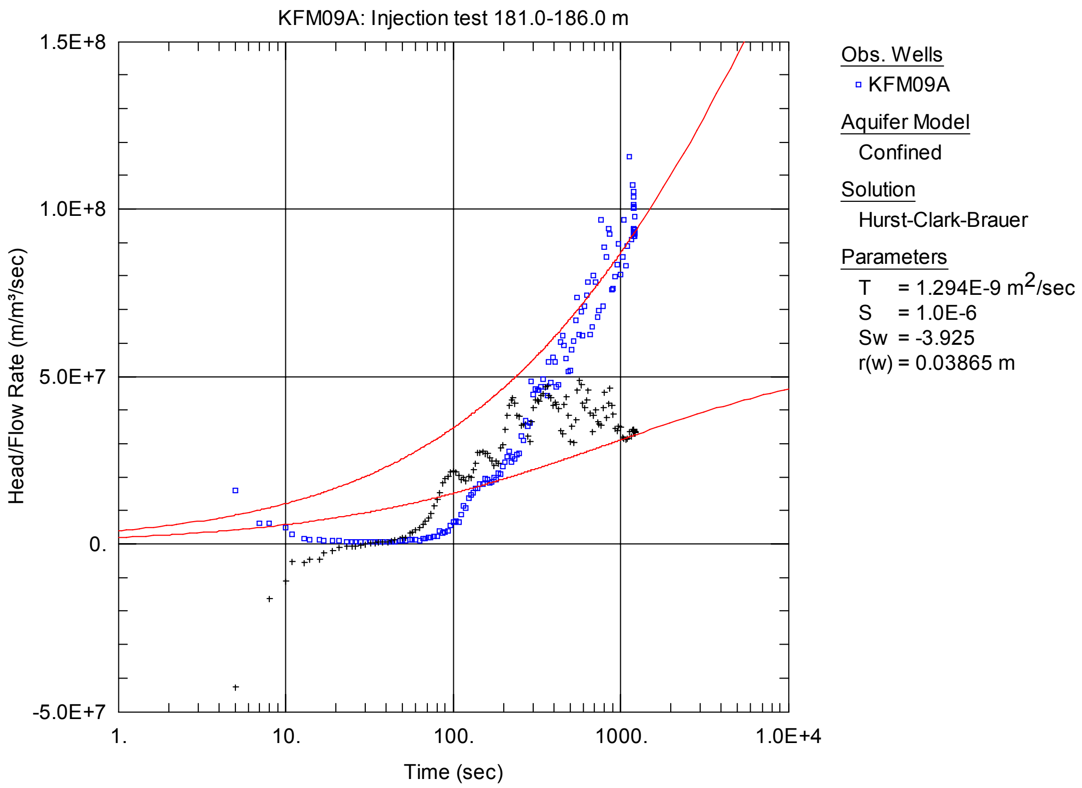


Figure A3-285. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 181.0-186.0 m in KFM09A. A fit with Hurst-Clark-Brauer is not possible and no transient evaluation is possible on the injection.*

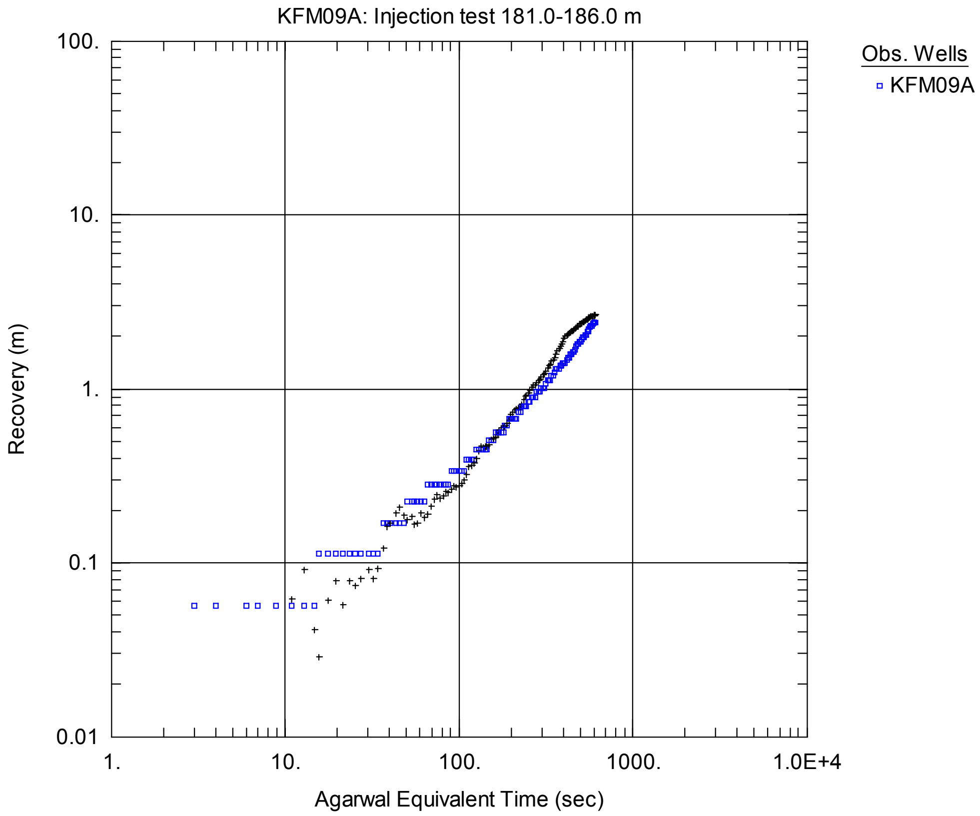


Figure A3-286. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 181.0-186.0 m in KFM09A.*

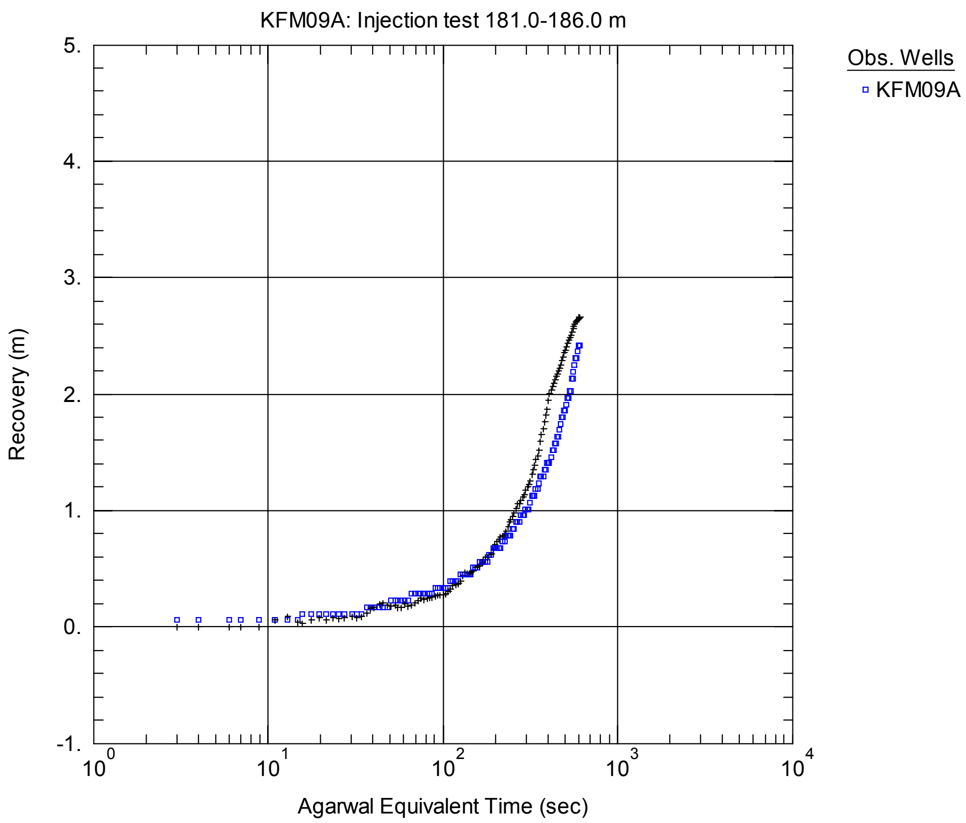


Figure A3-287. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 181.0-186.0 m in KFM09A.*

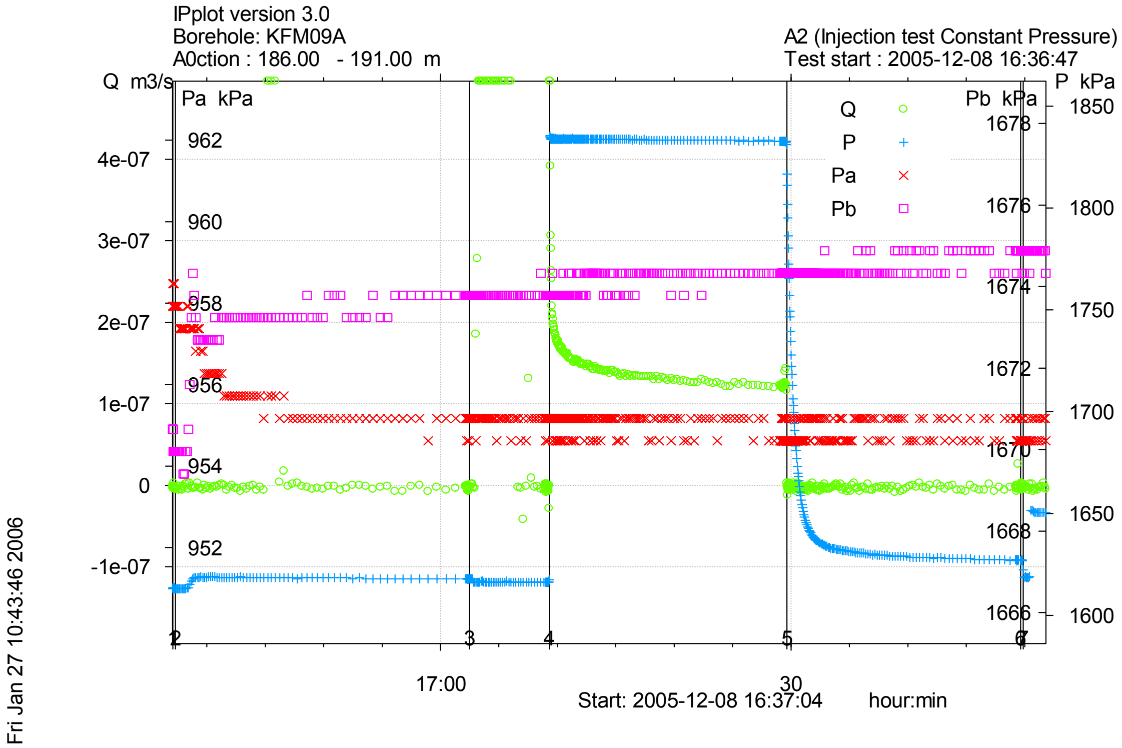


Figure A3-288. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 186.0-191.0 m in borehole KFM09A.*

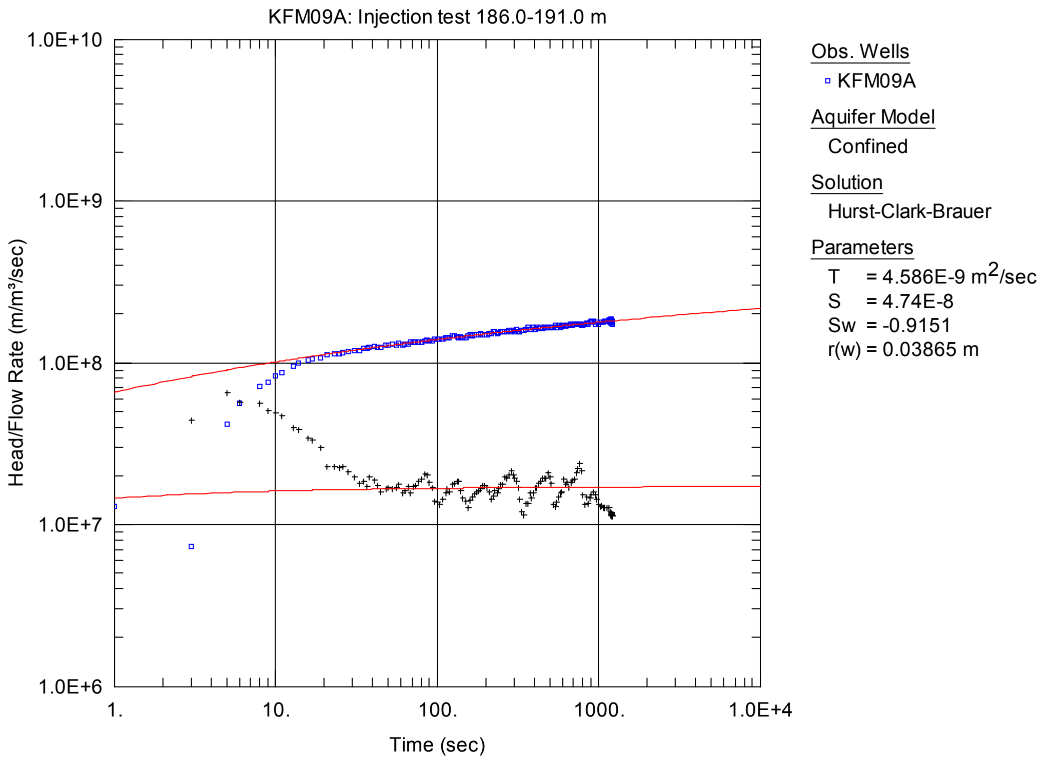


Figure A3-289. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 186.0-191.0 m in KFM09A.*

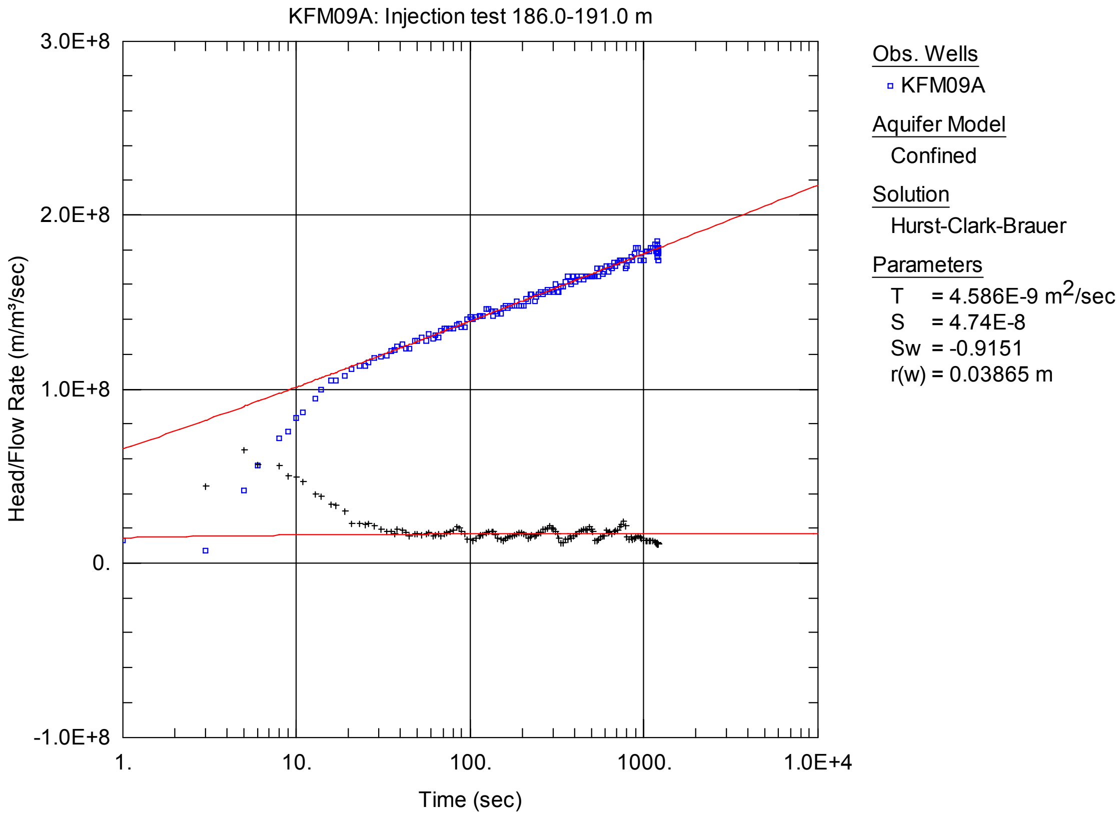


Figure A3-290. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 186.0-191.0 m in KFM09A.*

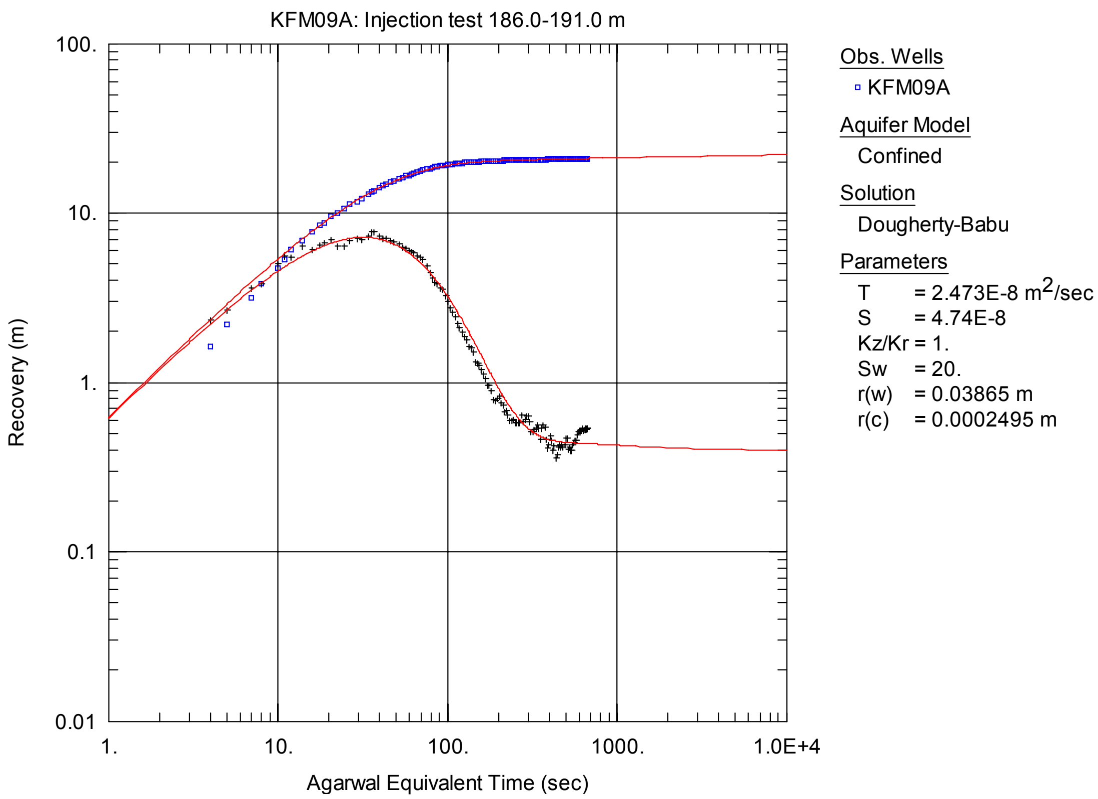


Figure A3-291. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 186.0-191.0 m in KFM09A. The transient evaluation on the recovery period is not regarded as representative.*

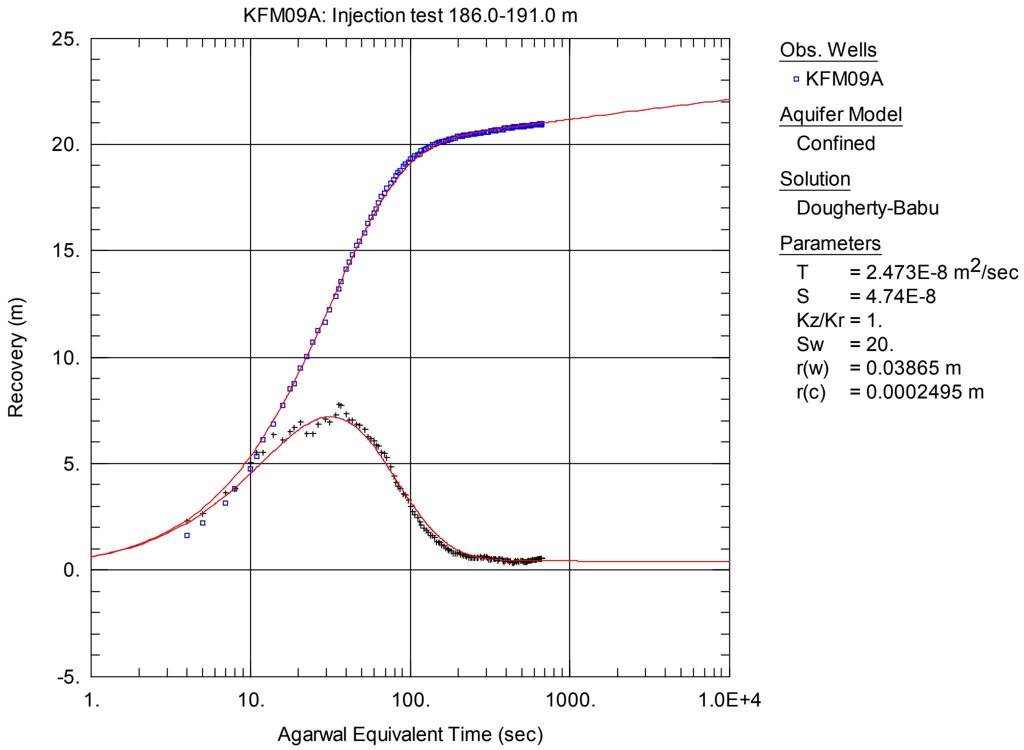


Figure A3-292. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 186.0-191.0 m in KFM09A. The transient evaluation on the recovery period is not regarded as representative.*

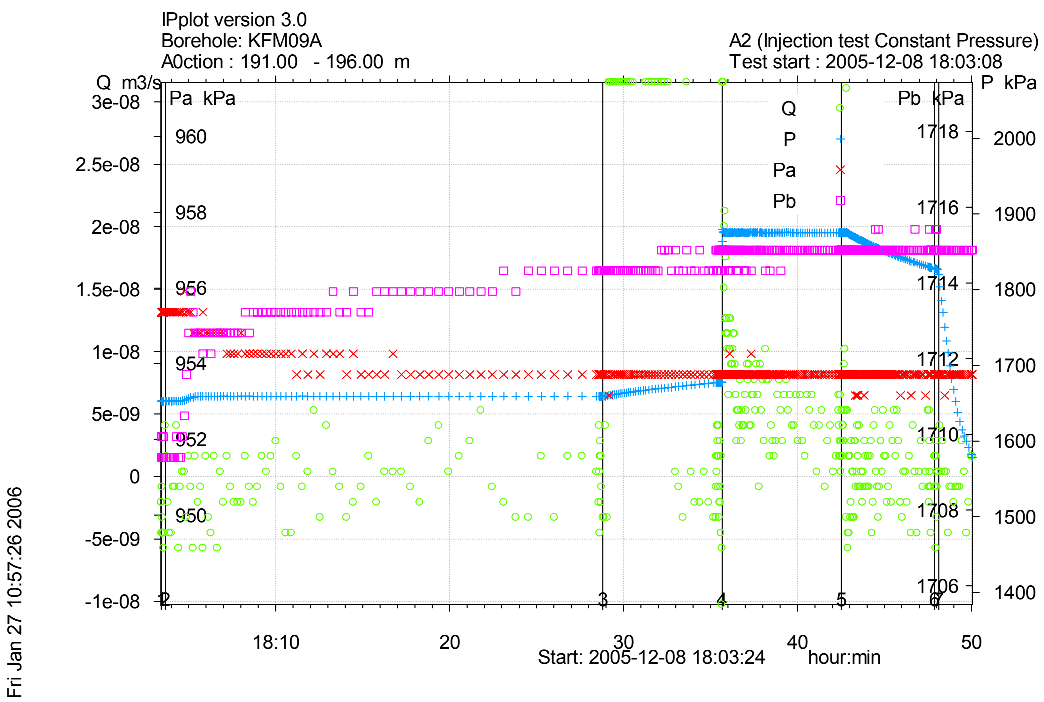


Figure A3-293. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 191.0-196.0 m in borehole KFM09A.*

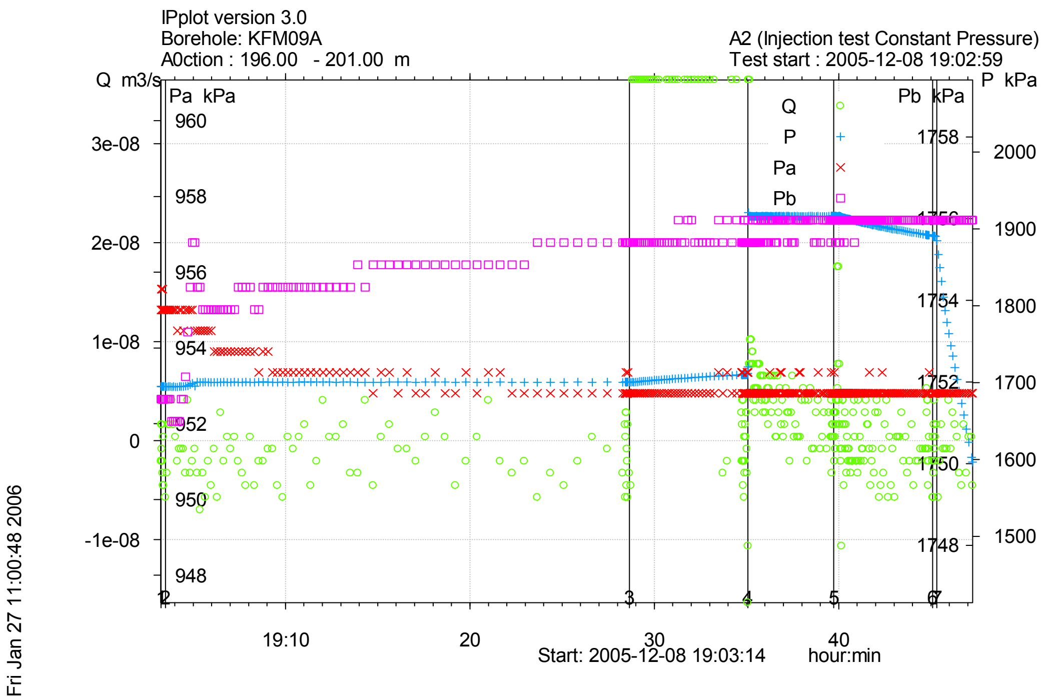


Figure A3-294. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 196.0-201.0 m in borehole KFM09A.*

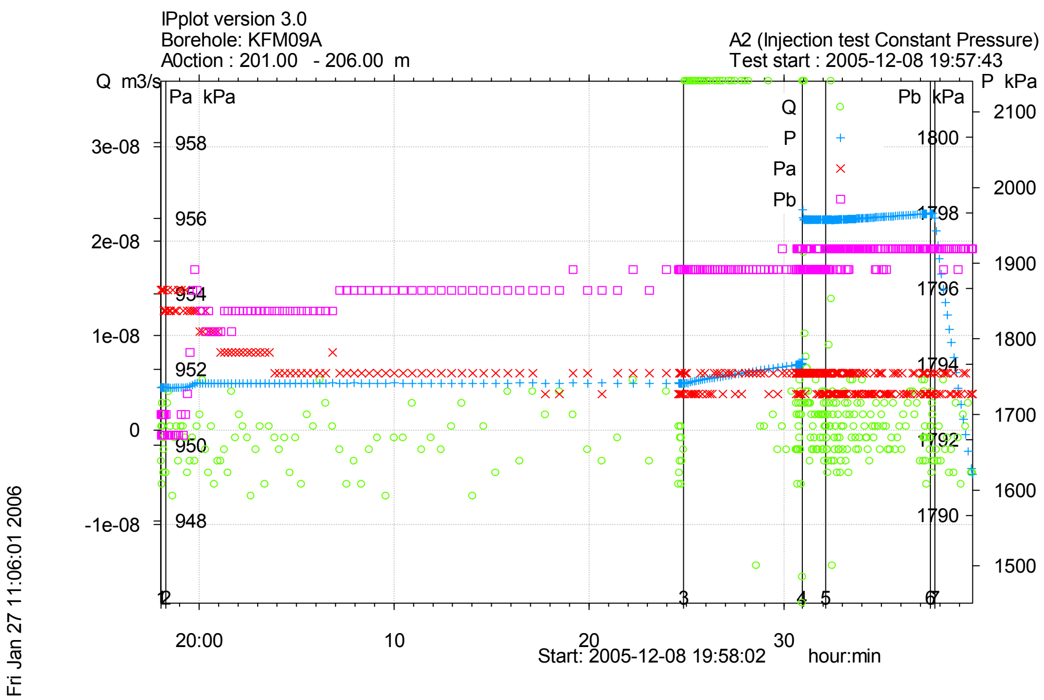


Figure A3-295. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 201.0-206.0 m in borehole KFM09A.*

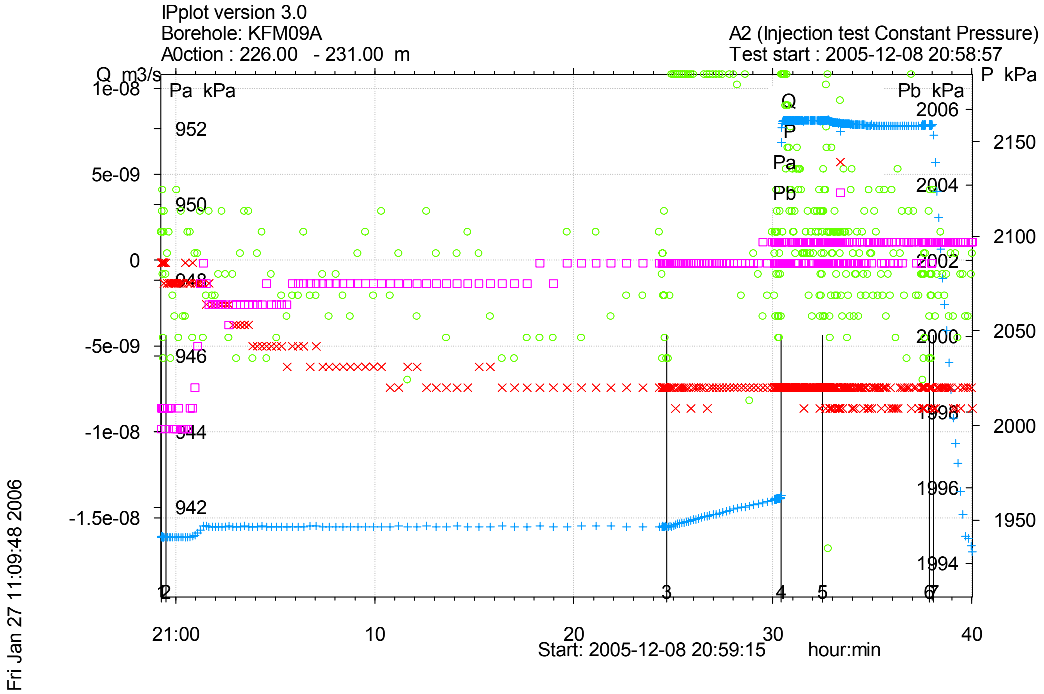


Figure A3-296. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 226.0-231.0 m in borehole KFM09A.*

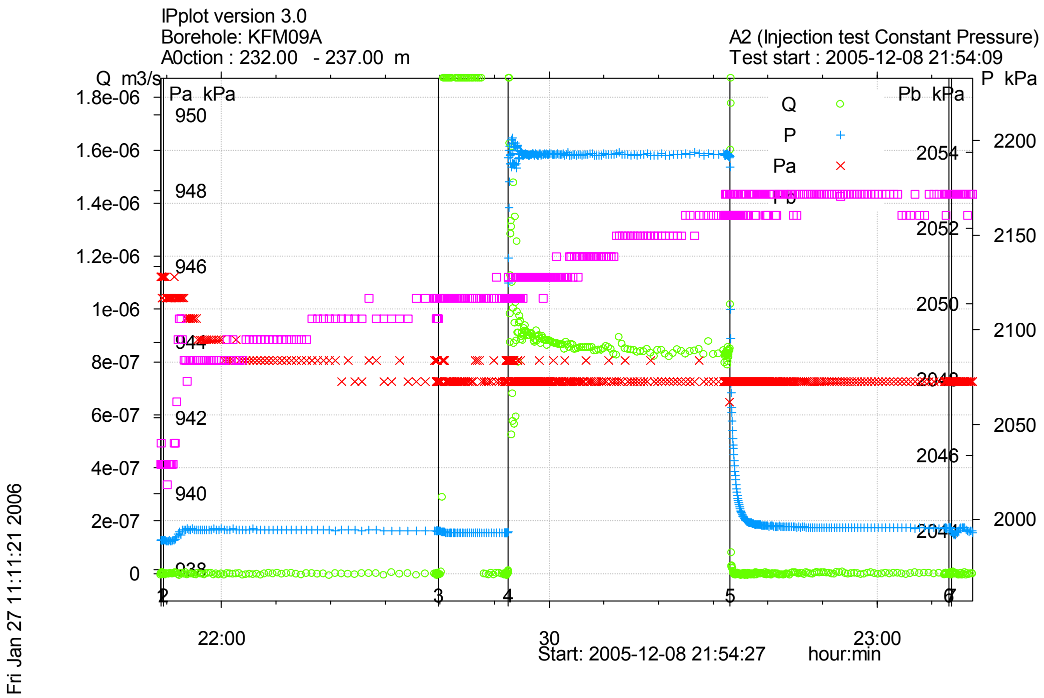


Figure A3-297. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 232.0-237.0 m in borehole KFM09A.*

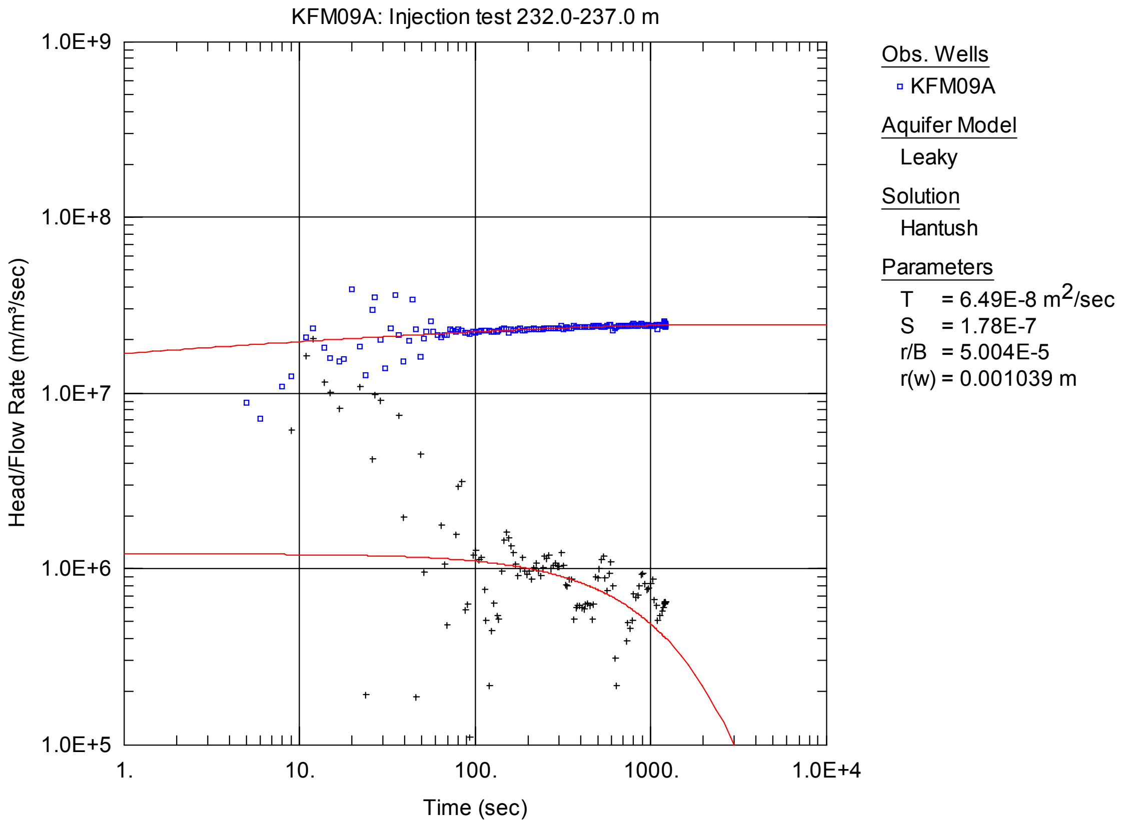


***Figure A3-298.** Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 232.0-237.0 m in KFM09A.*

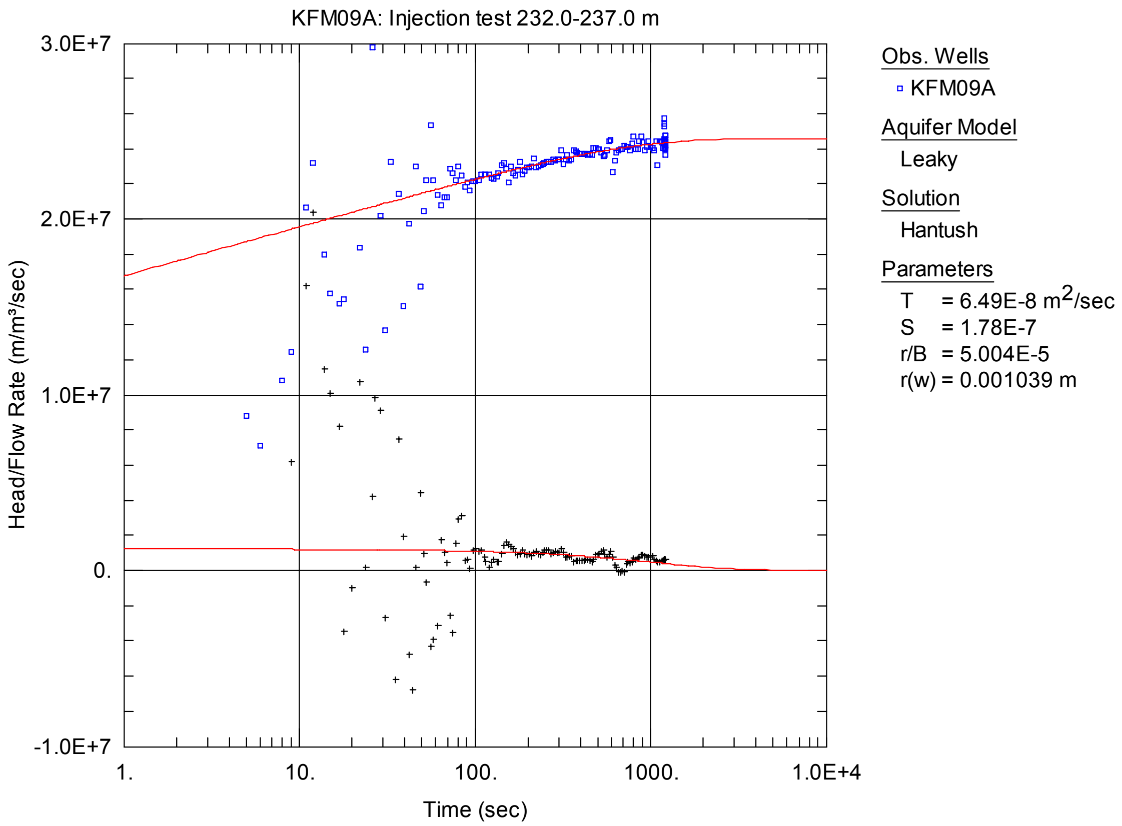


***Figure A3-299.** Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 232.0-237.0 m in KFM09A.*

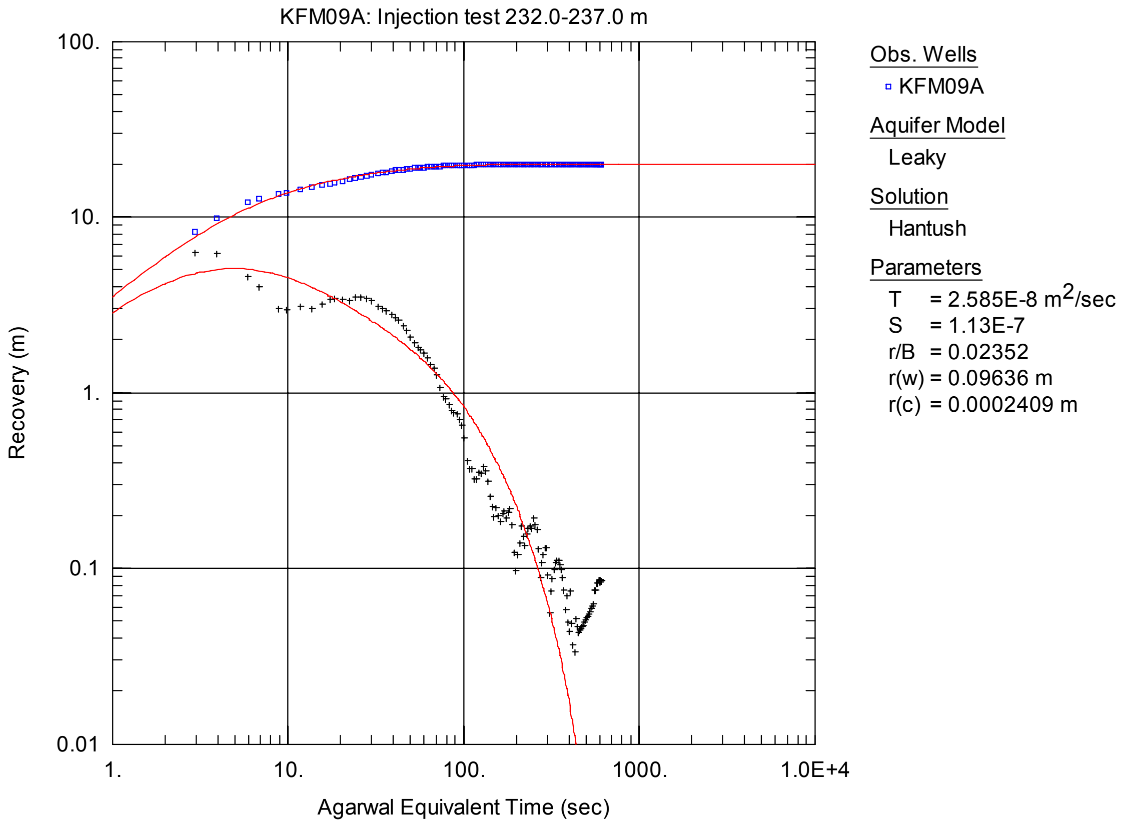


Figure A3-300. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 232.0-237.0 m in KFM09A.*

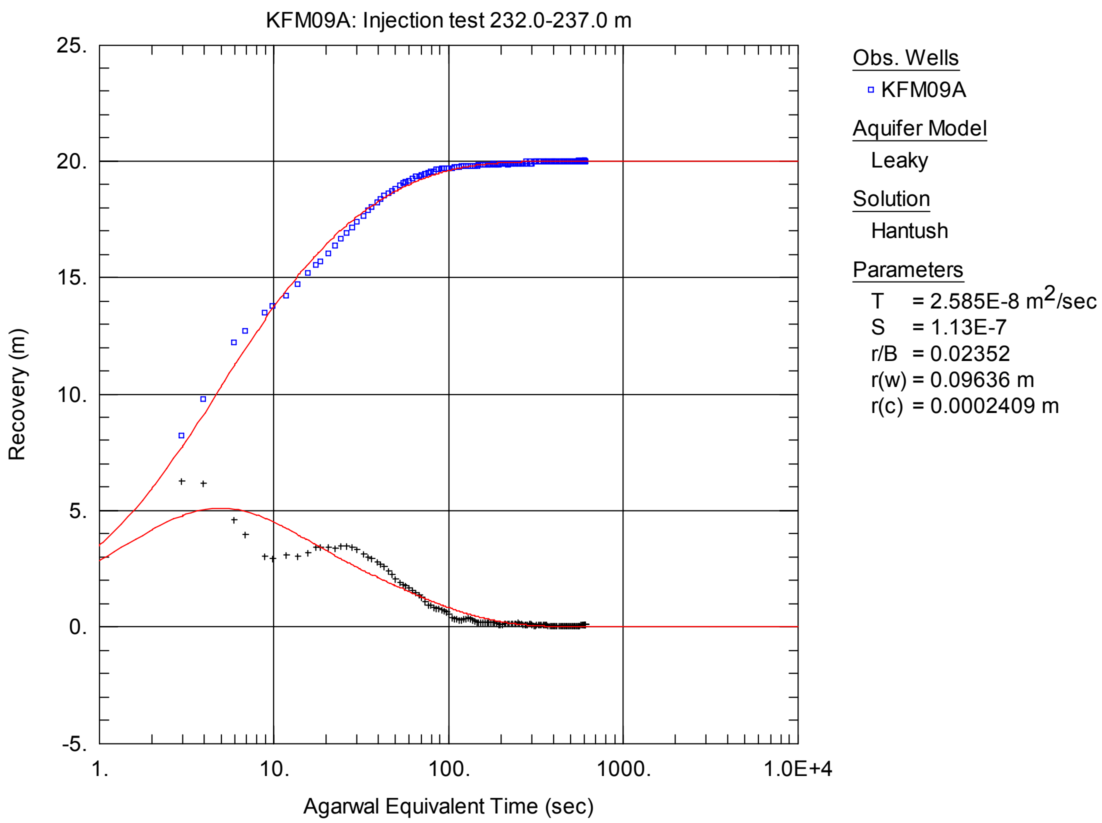


Figure A3-301. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 232.0-237.0 m in KFM09A.*

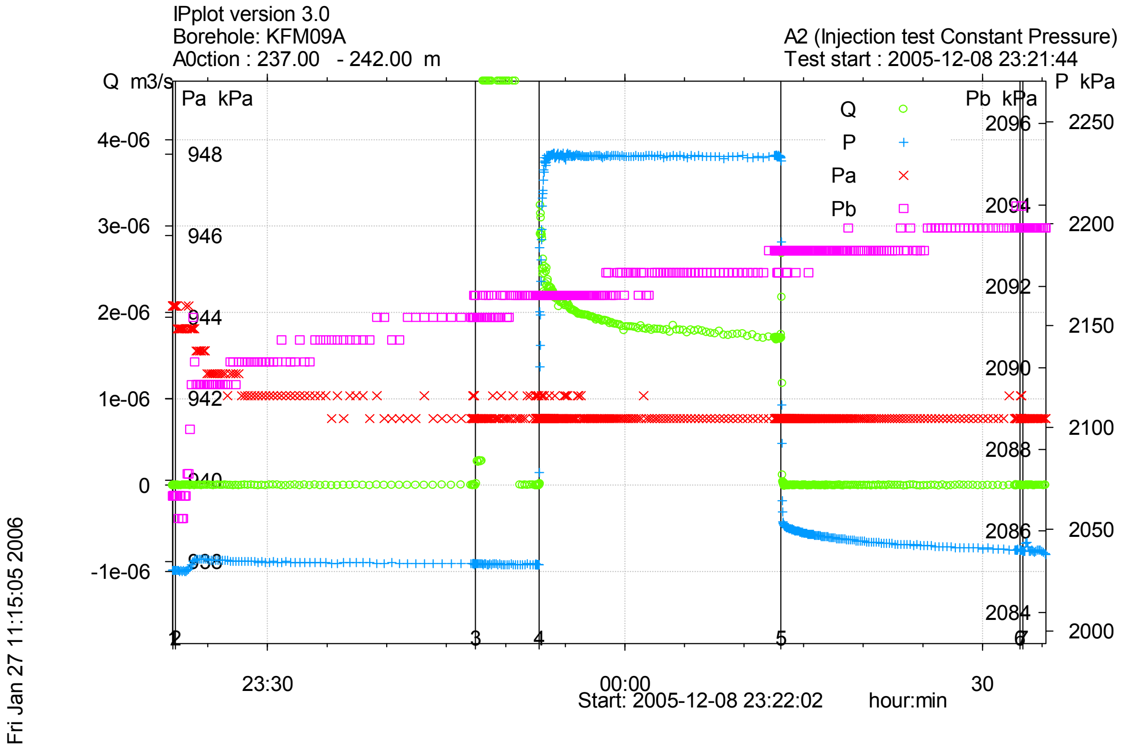


Figure A3-302. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 237.0-242.0 m in borehole KFM09A.*

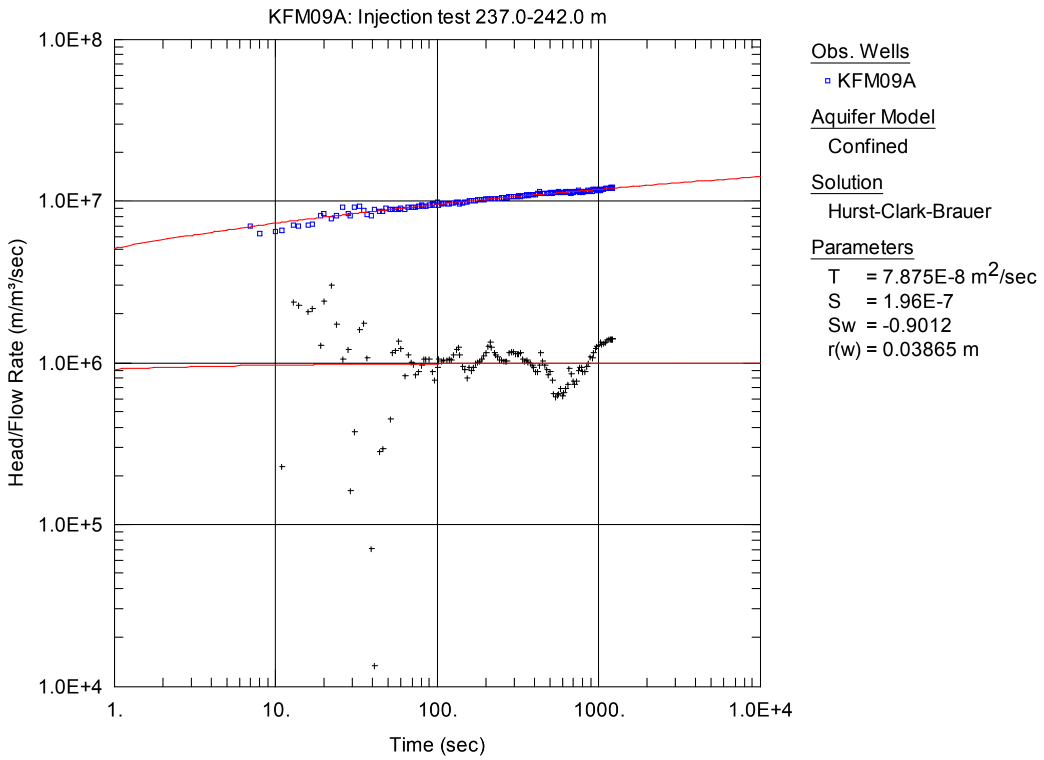


Figure A3-303. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 237.0-242.0 m in KFM09A.*

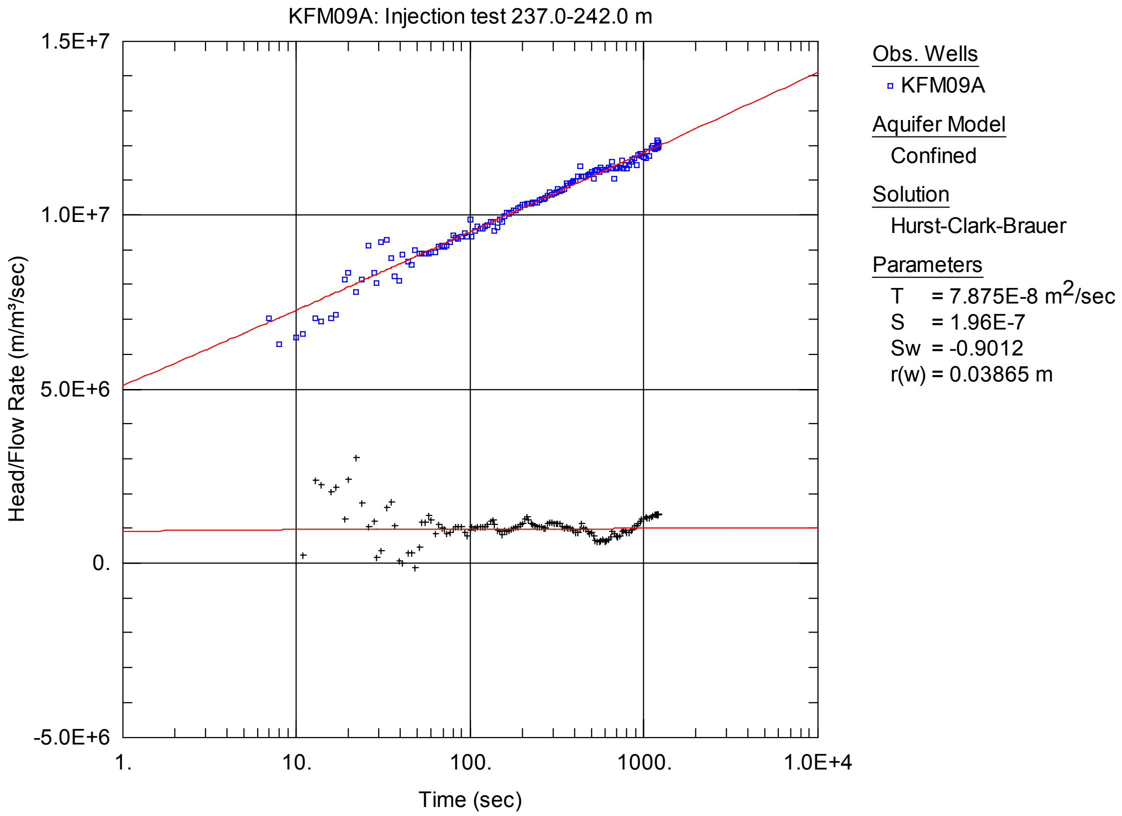


Figure A3-304. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 237.0-242.0 m in KFM09A.*

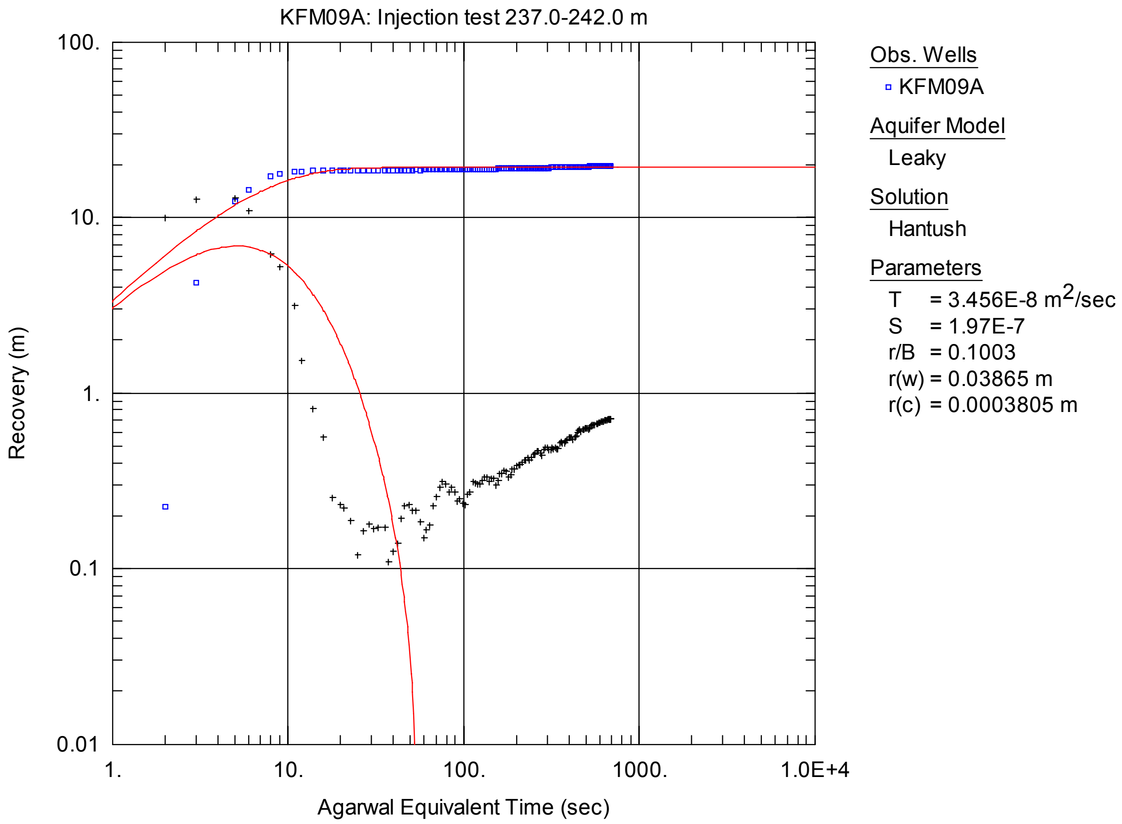


Figure A3-305. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 237.0-242.0 m in KFM09A.*

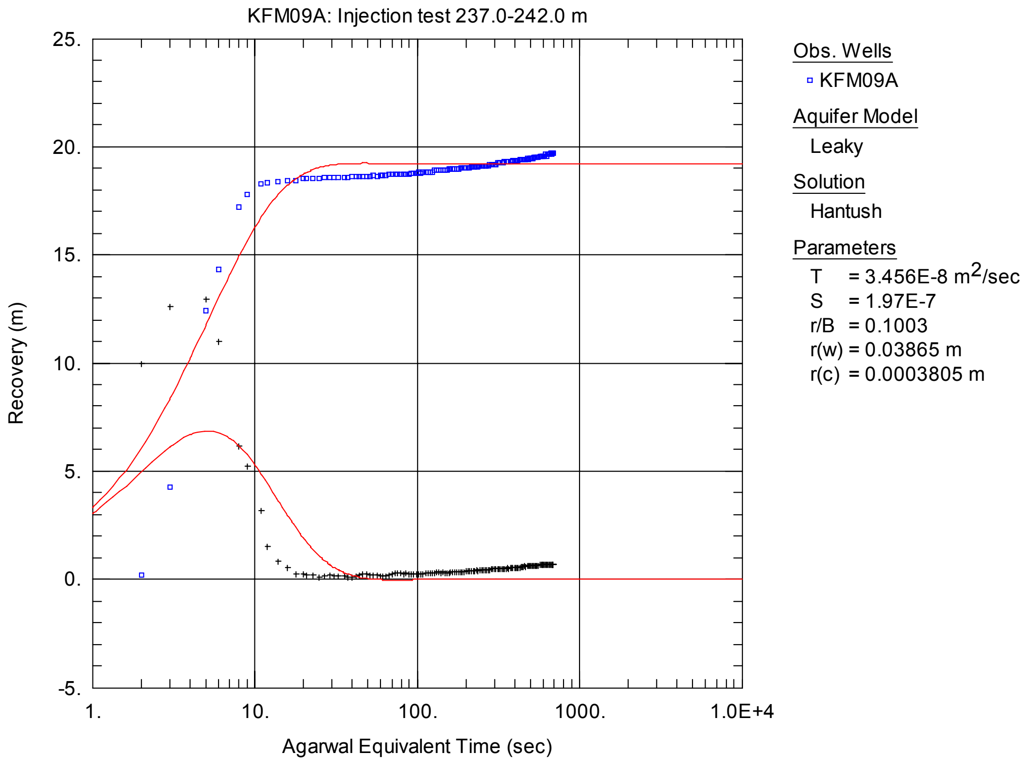


Figure A3-306. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 237.0-242.0 m in KFM09A.*

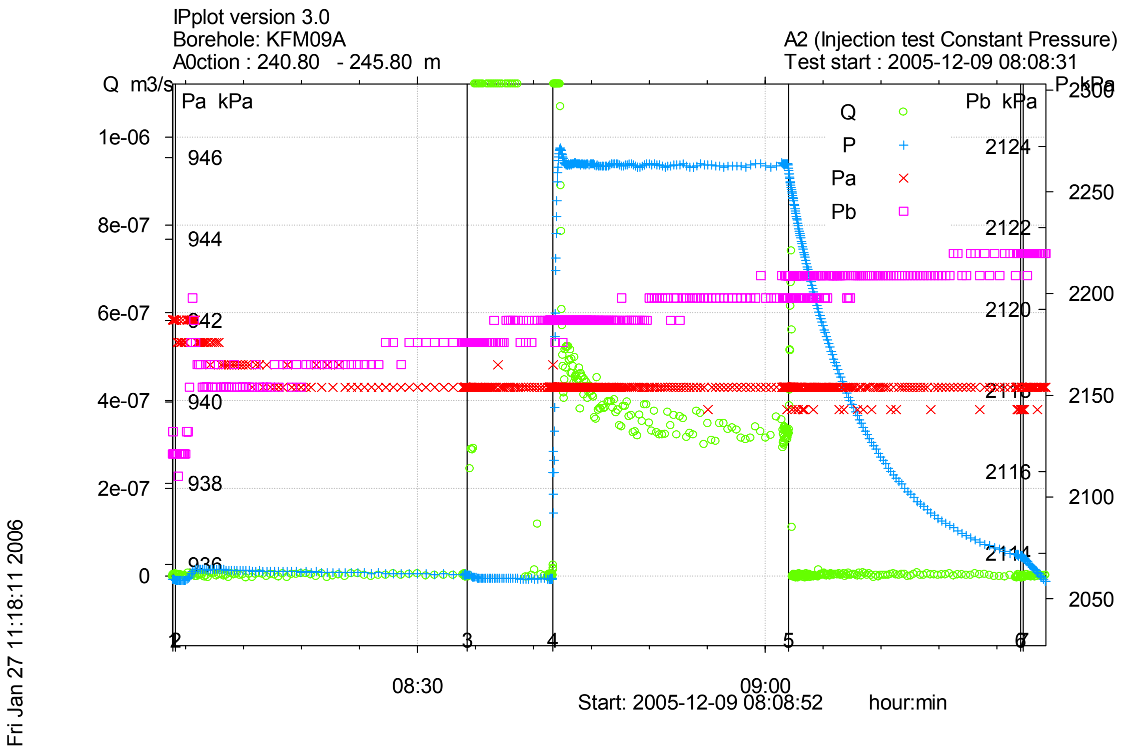


Figure A3-307. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 240.80-245.80 m in borehole KFM09A.*

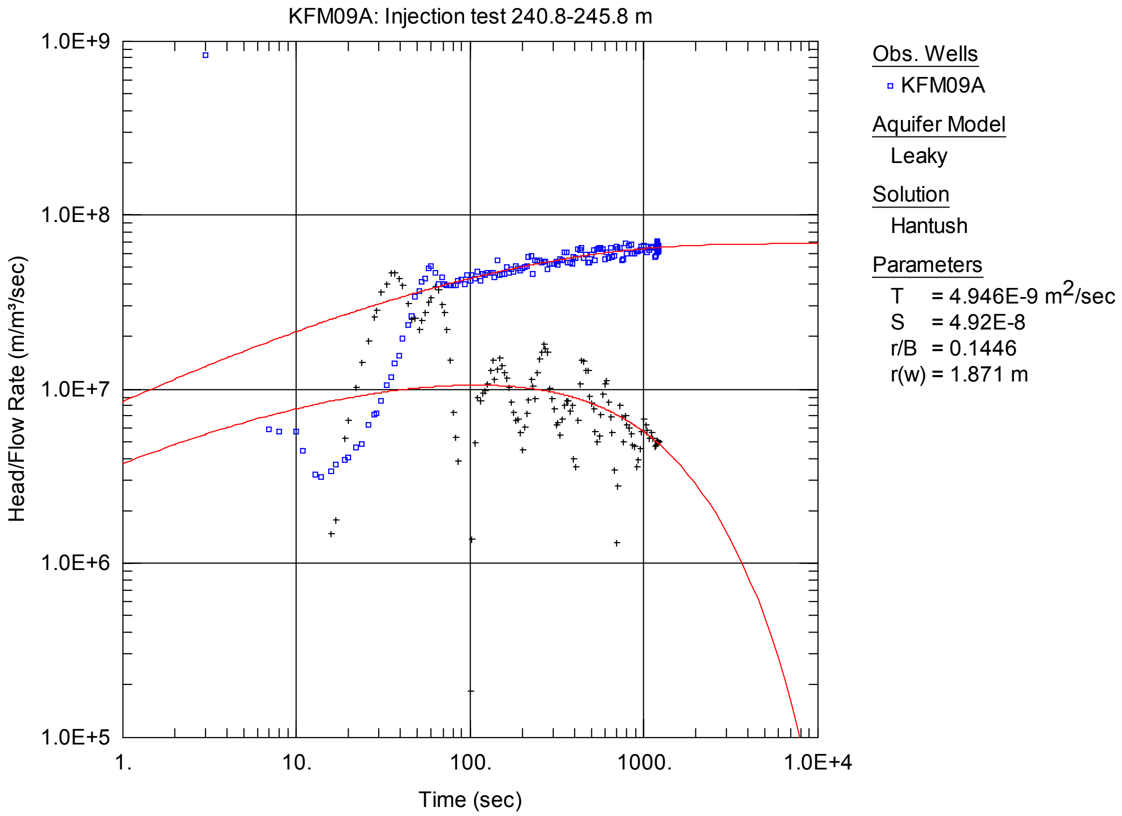


Figure A3-308. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 240.80-245.80 m in KFM09A.*

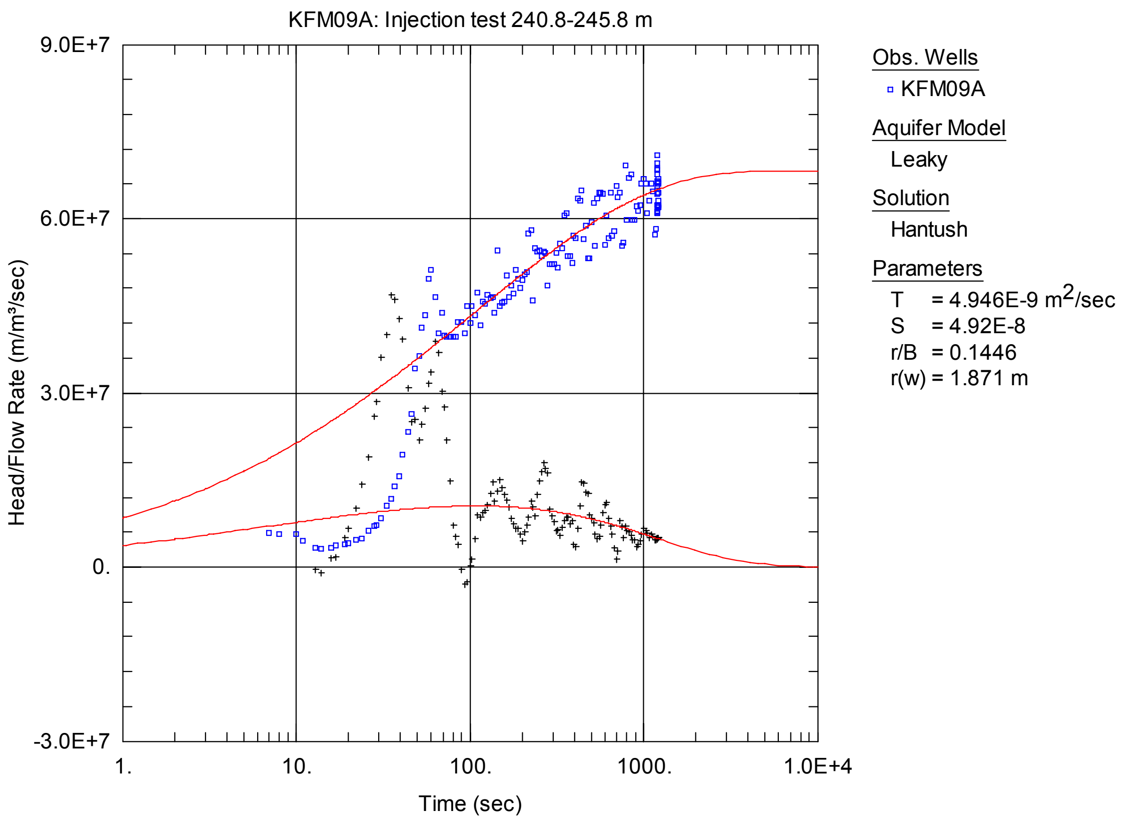


Figure A3-309. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 240.80-245.80 m in KFM09A.*

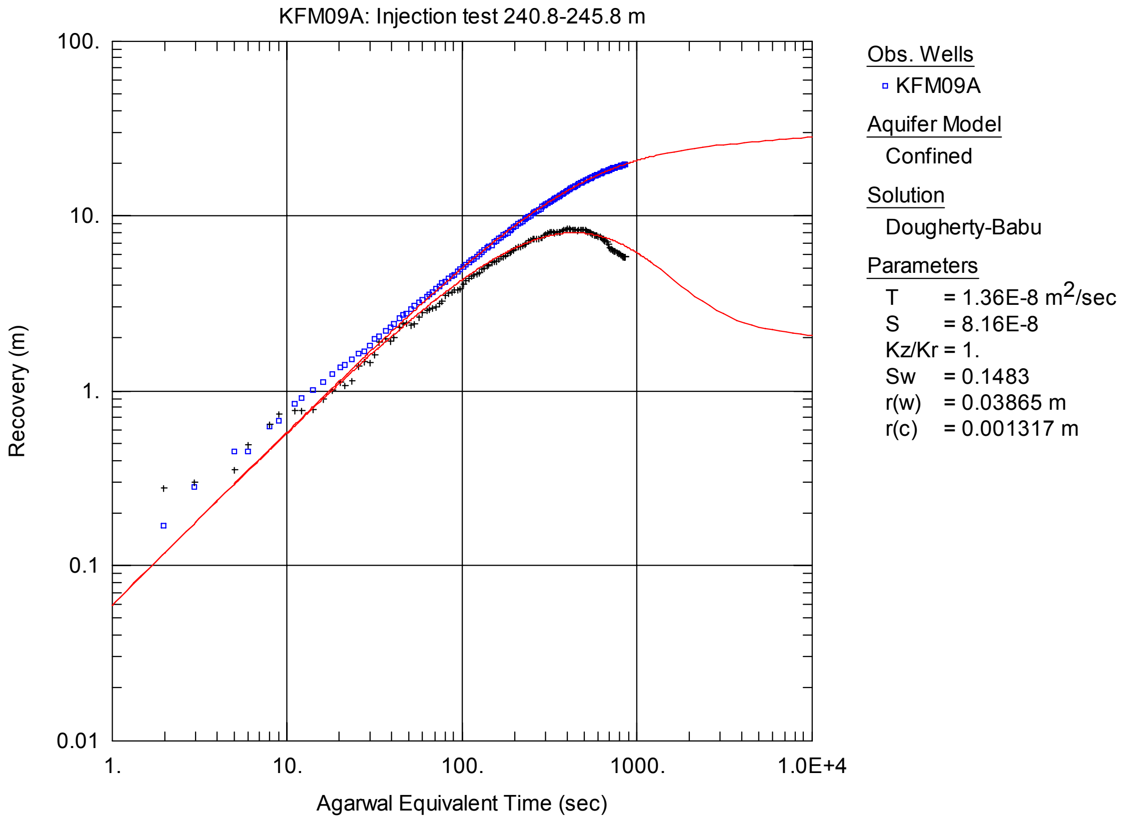


Figure A3-310. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 240.80-245.80 m in KFM09A.*

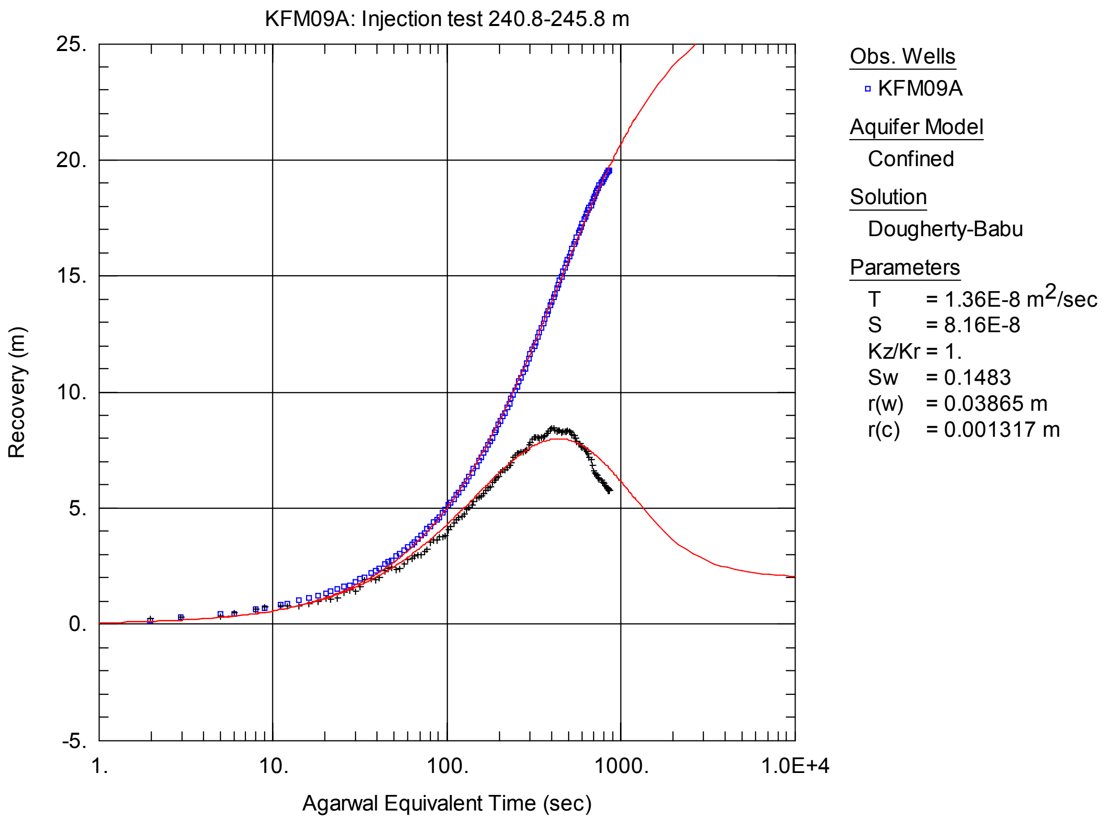


Figure A3-311. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 240.80-245.80 m in KFM09A.*

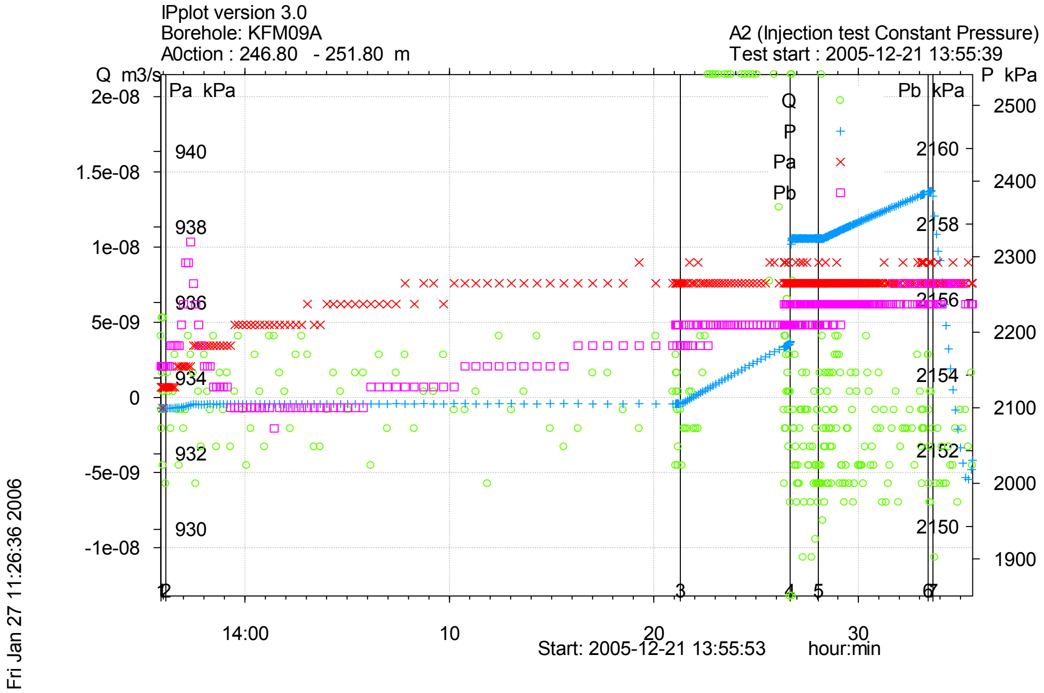


Figure A3-312. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 246.80-251.80 m in borehole KFM09A.*

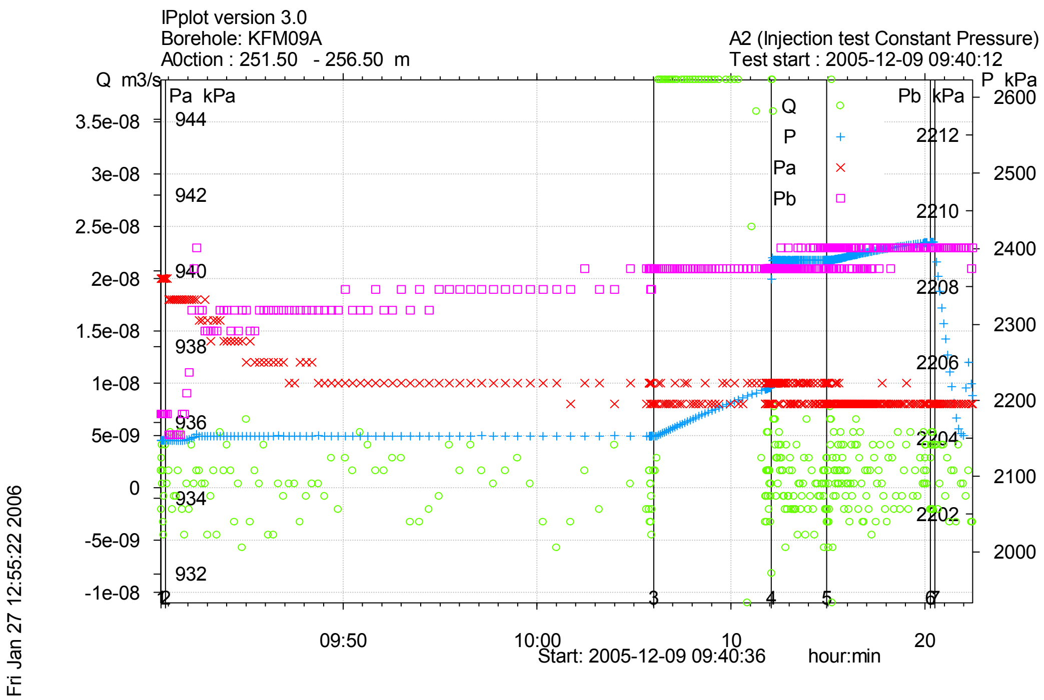


Figure A3-313. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 251.50-256.50 m in borehole KFM09A.*

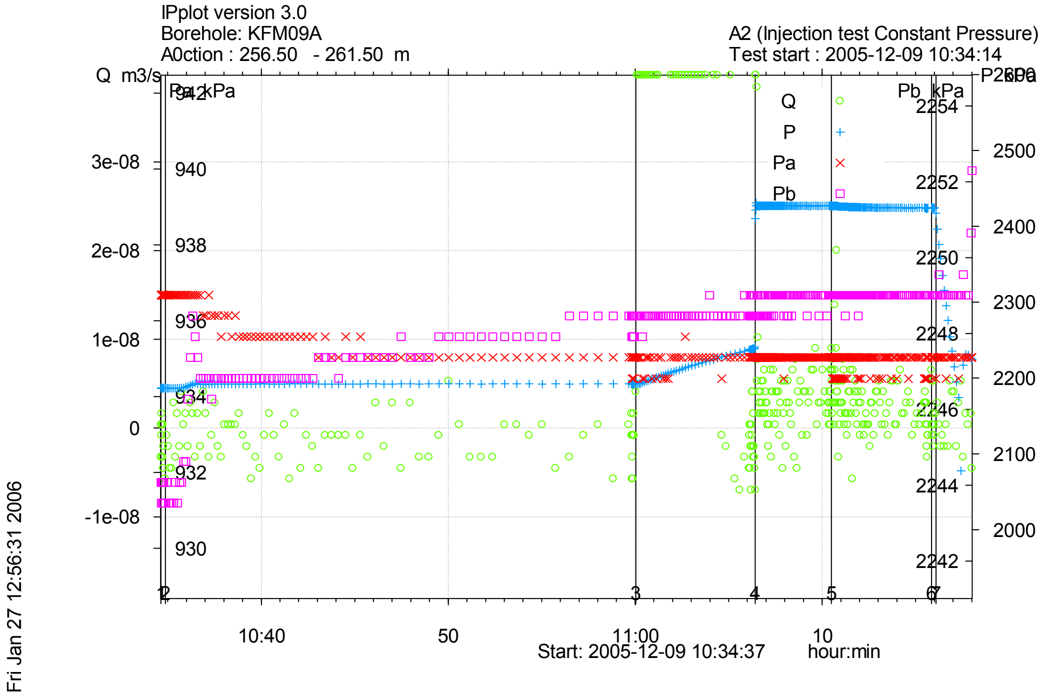


Figure A3-314. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 256.50-261.50 m in borehole KFM09A.*

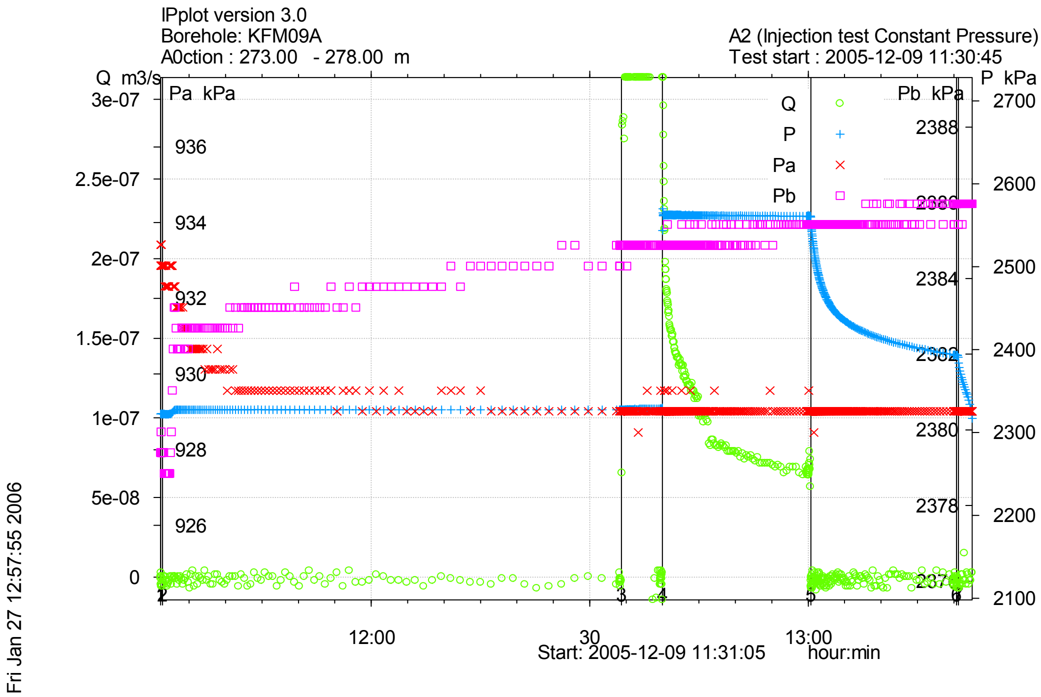


Figure A3-315. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 273.0-278.0 m in borehole KFM09A.*

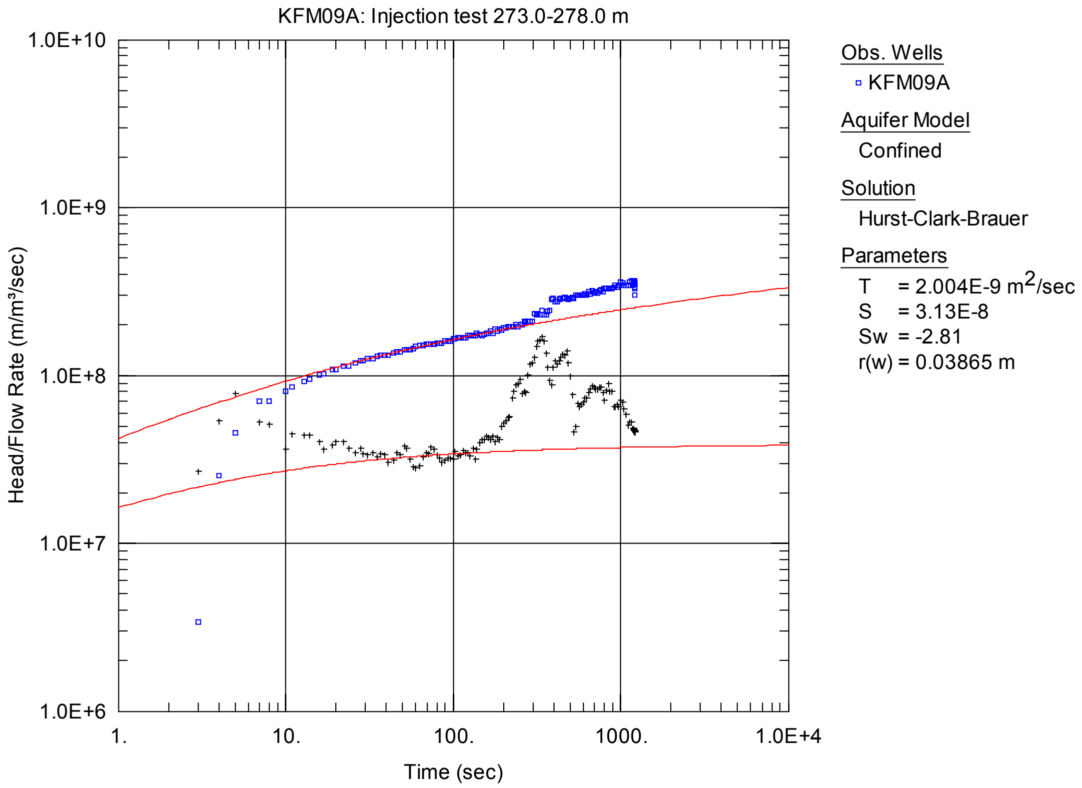


Figure A3-316. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 273.0-278.0 m in KFM09A. This plot shows a fit to the first of two different PRF:s during the injection period in this section.*

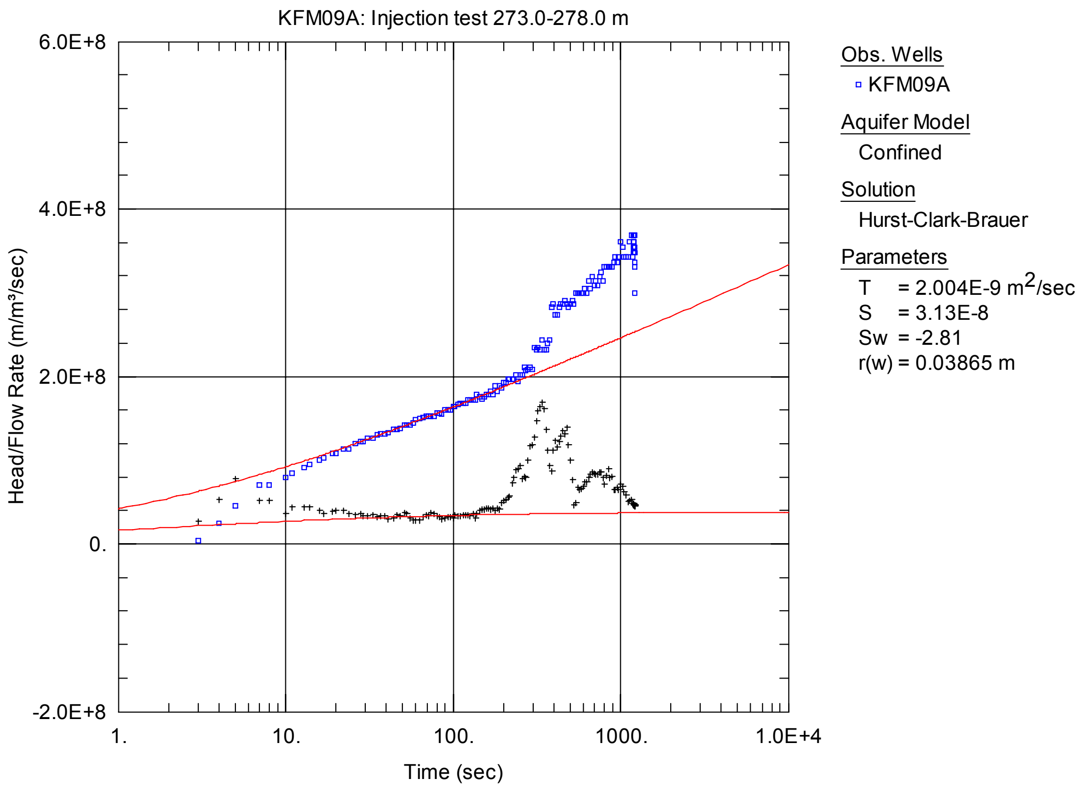


Figure A3-317. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 273.0-278.0 m in KFM09A. This plot shows a fit to the first of two different PRF:s during the injection period in this section.*

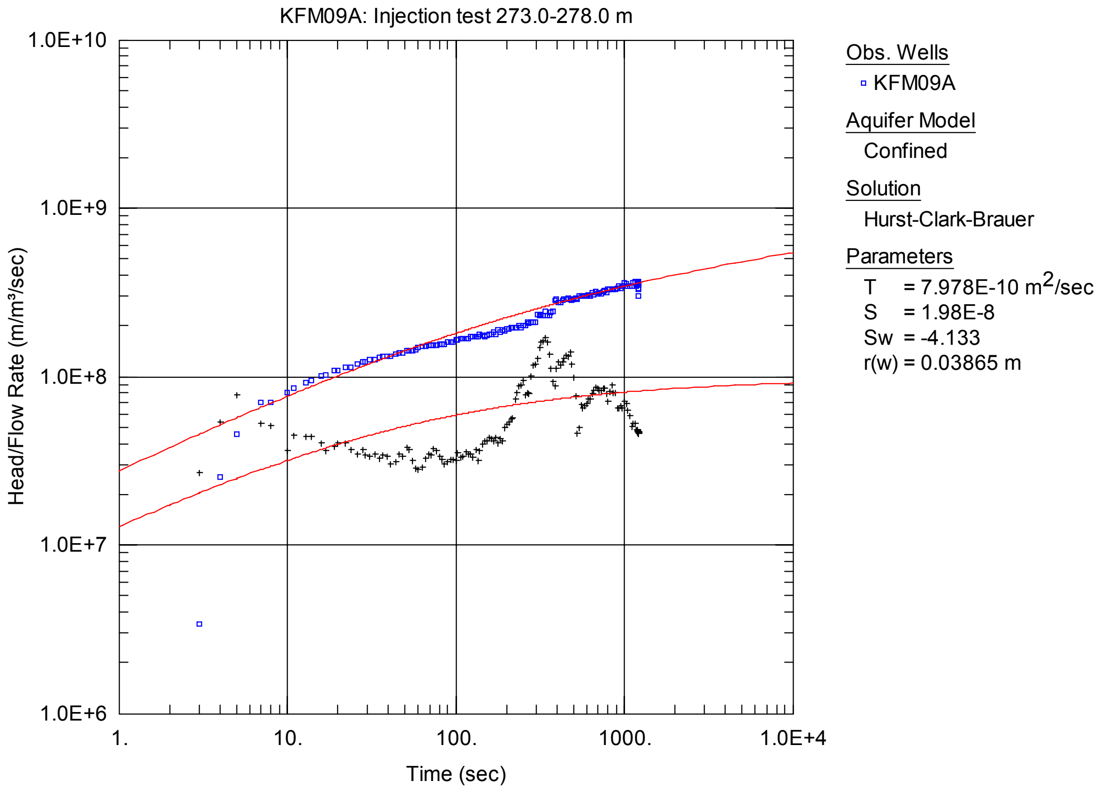


Figure A3-318. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 273.0-278.0 m in KFM09A. This plot shows a fit to the second of two different PRF:s during the injection period in this section.*

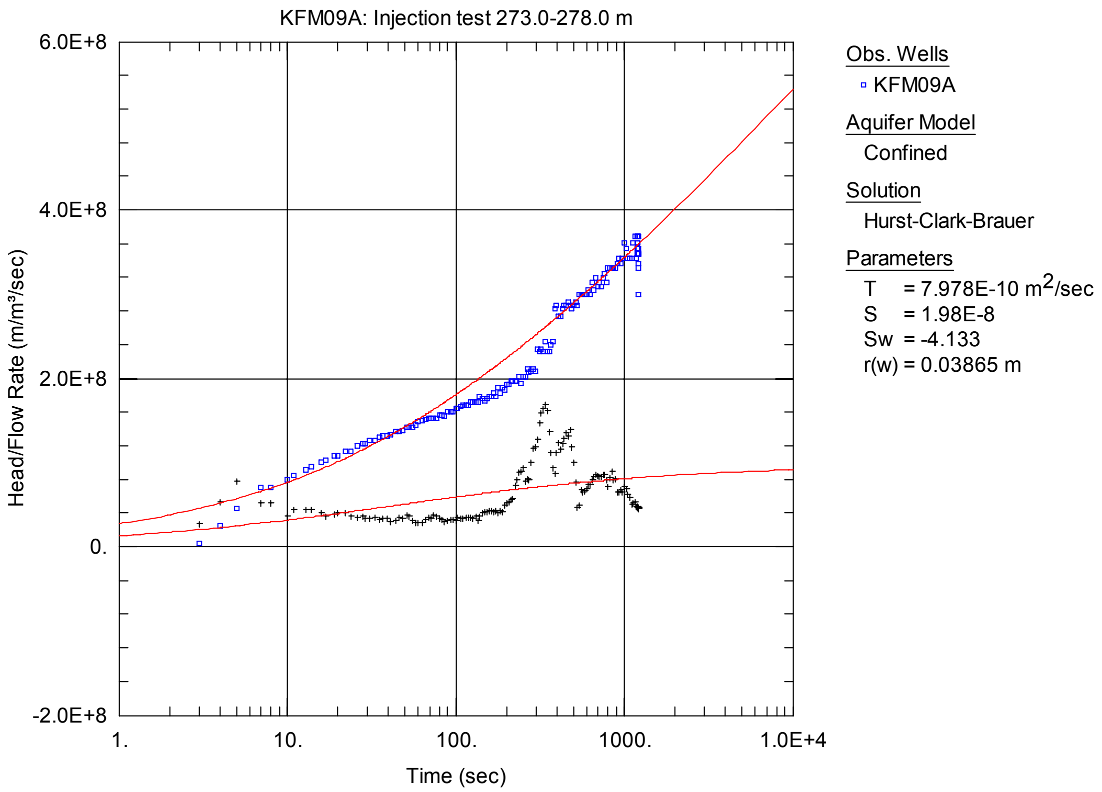


Figure A3-319. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 273.0-278.0 m in KFM09A. This plot shows a fit to the second of two different PRF:s during the injection period in this section.*

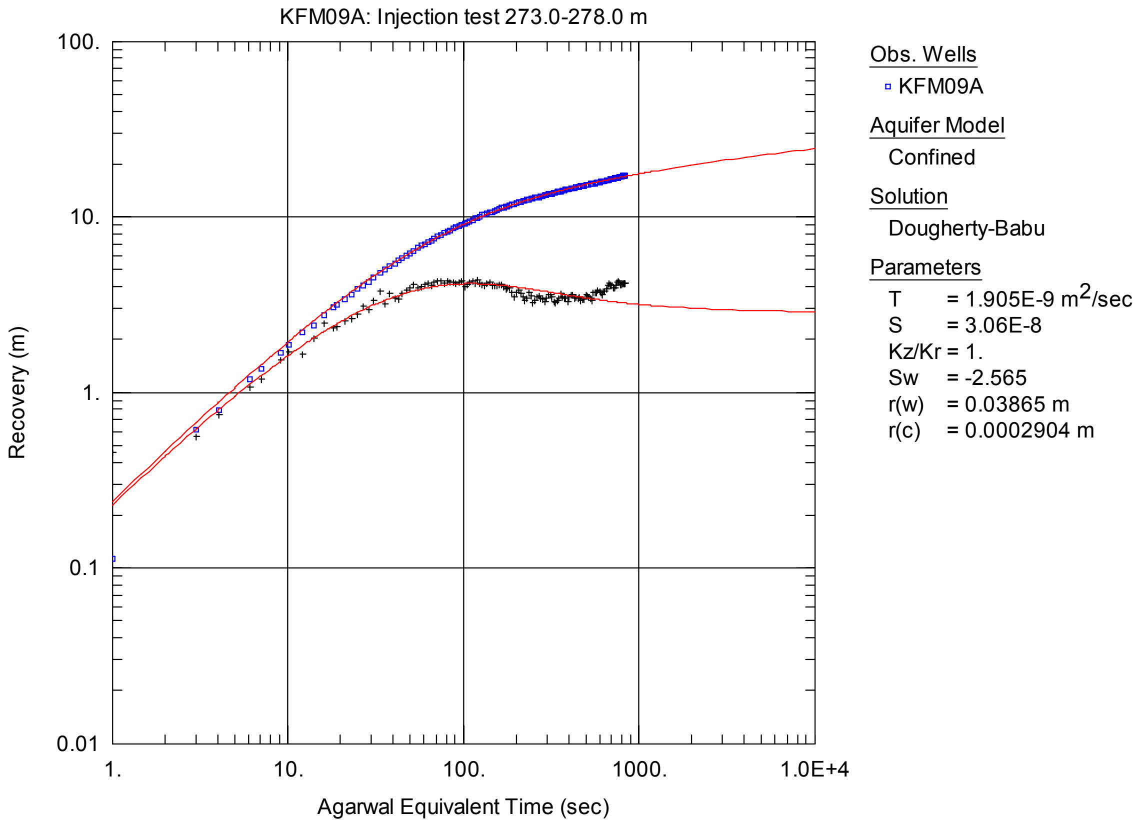


***Figure A3-320.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 273.0-278.0 m in KFM09A.*

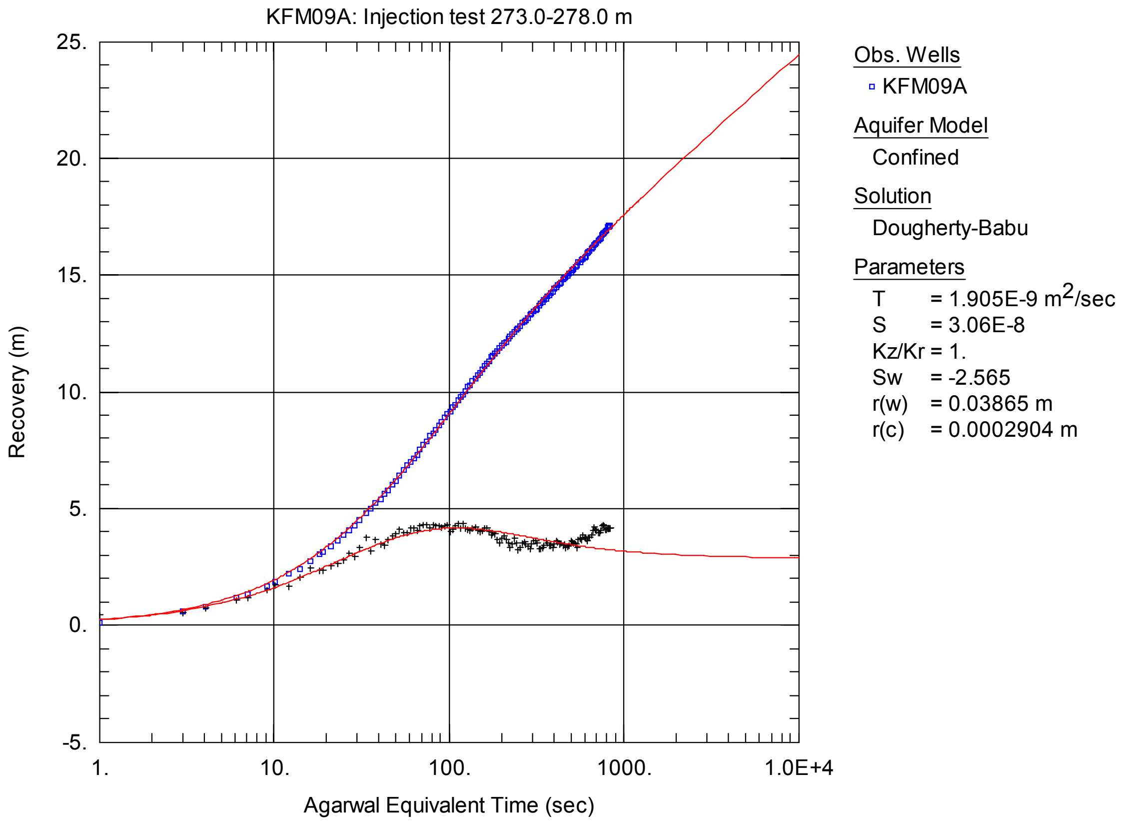


***Figure A3-321.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 273.0-278.0 m in KFM09A.*

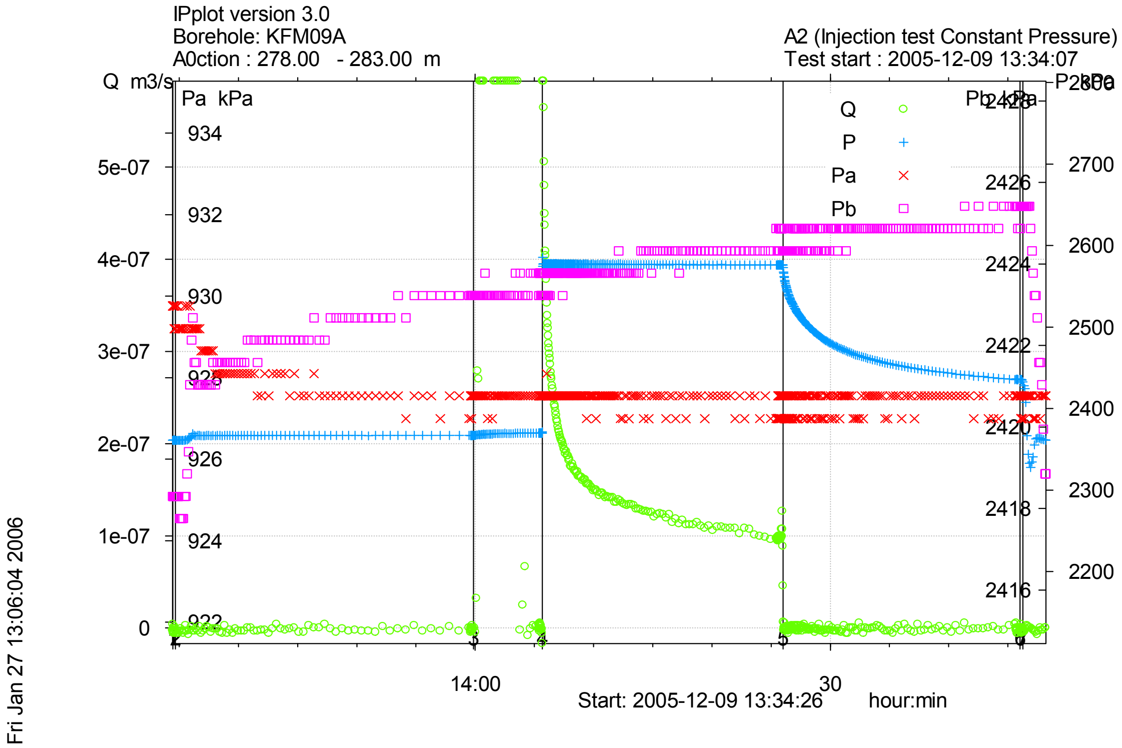


Figure A3-322. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in 278.0-283.0 m in borehole KFM09A.*

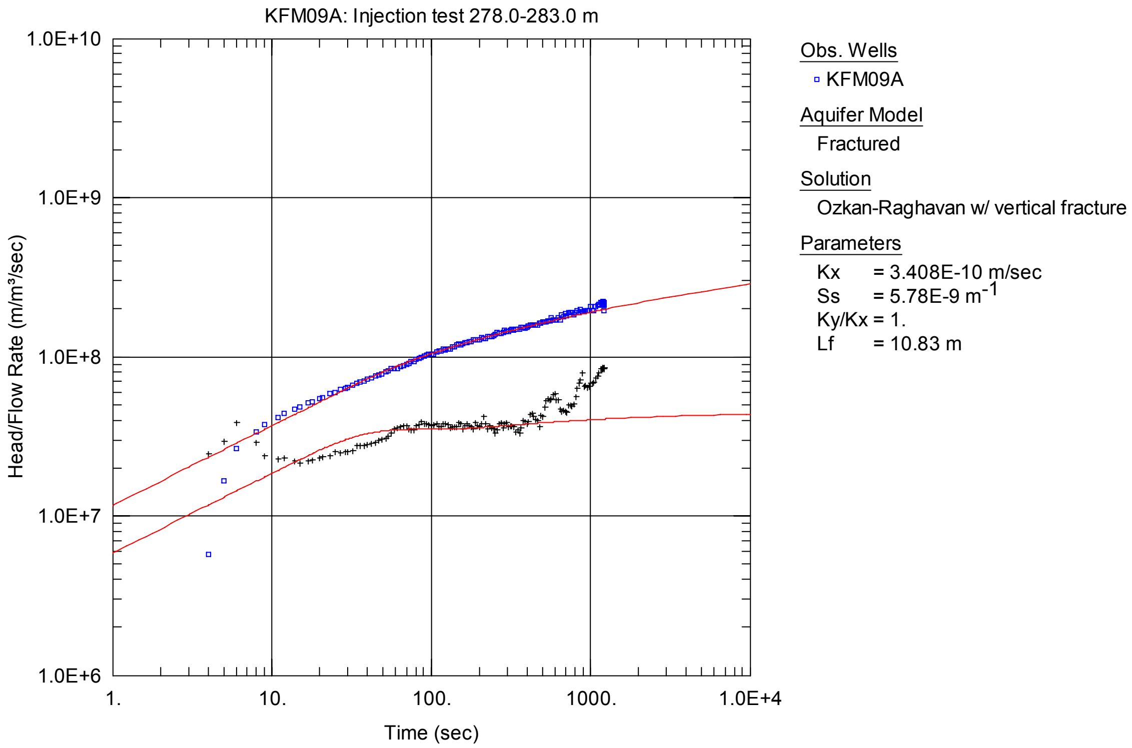


Figure A3-323. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 278.0-283.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

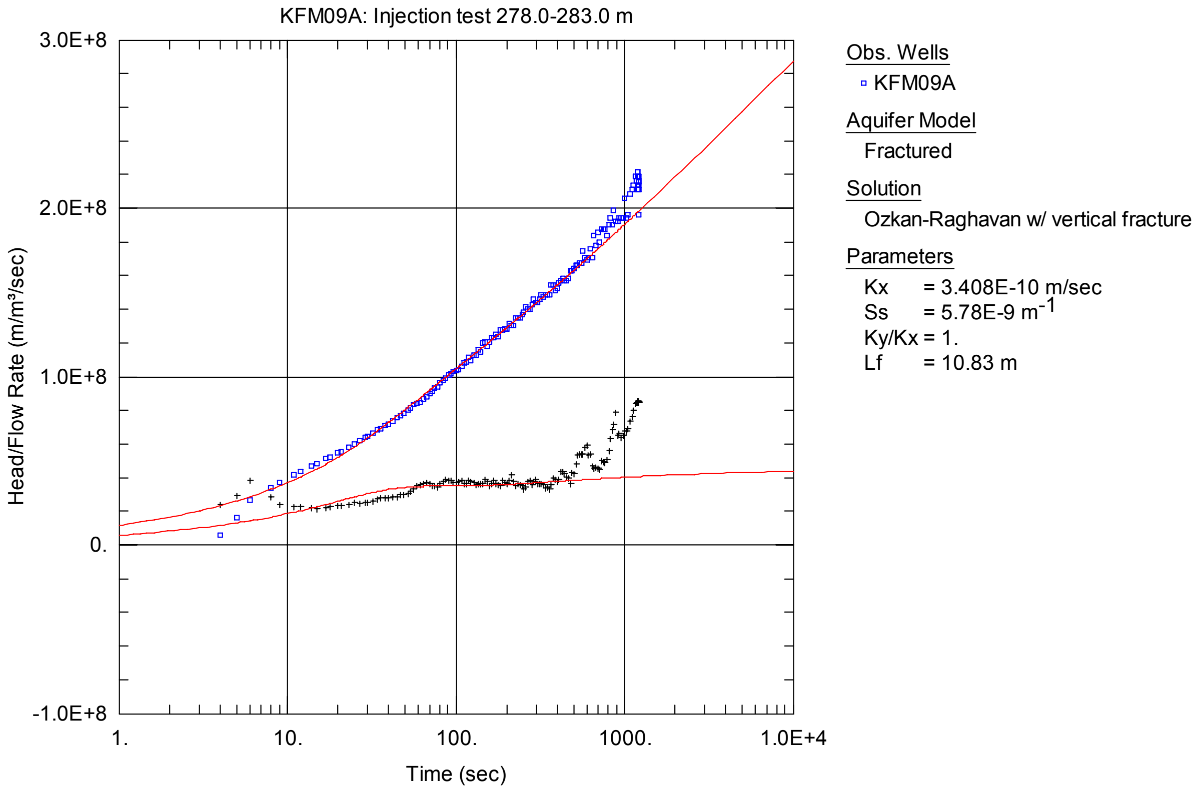


Figure A3-324. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 278.0-283.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

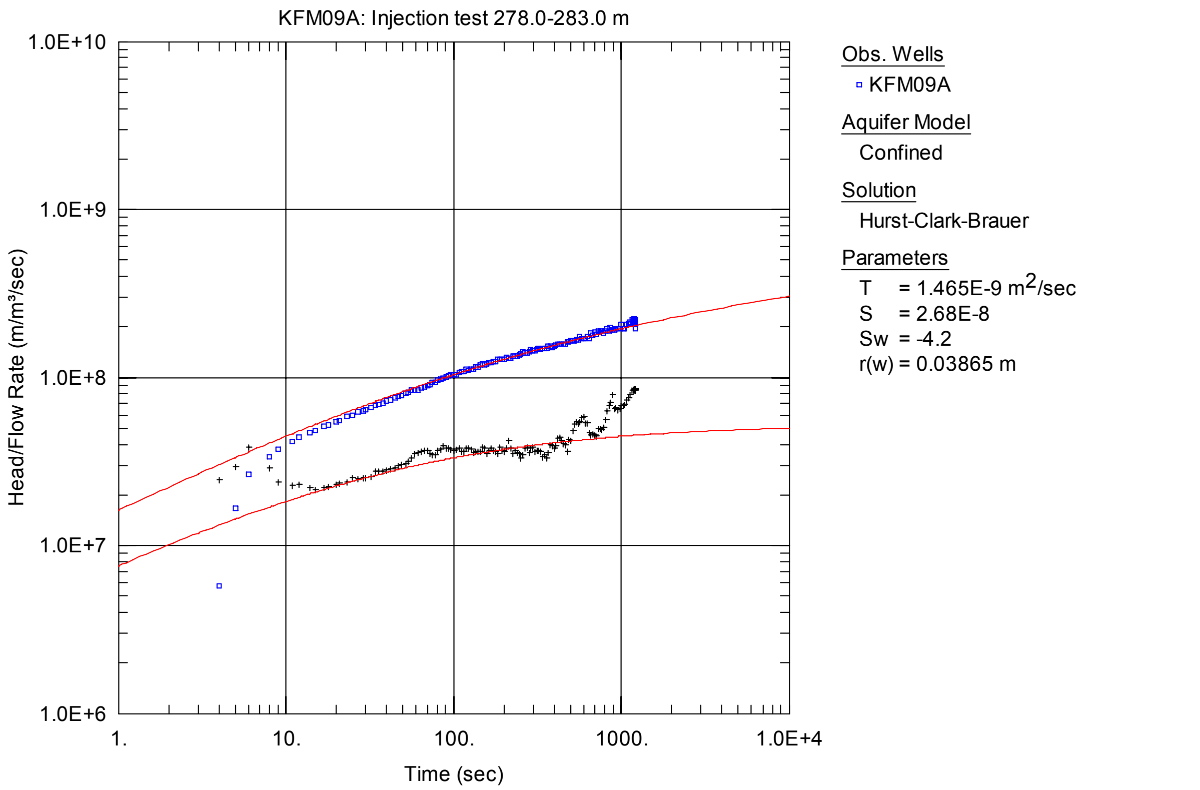


Figure A3-325. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 278.0-283.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for a pseudo-radial response.*

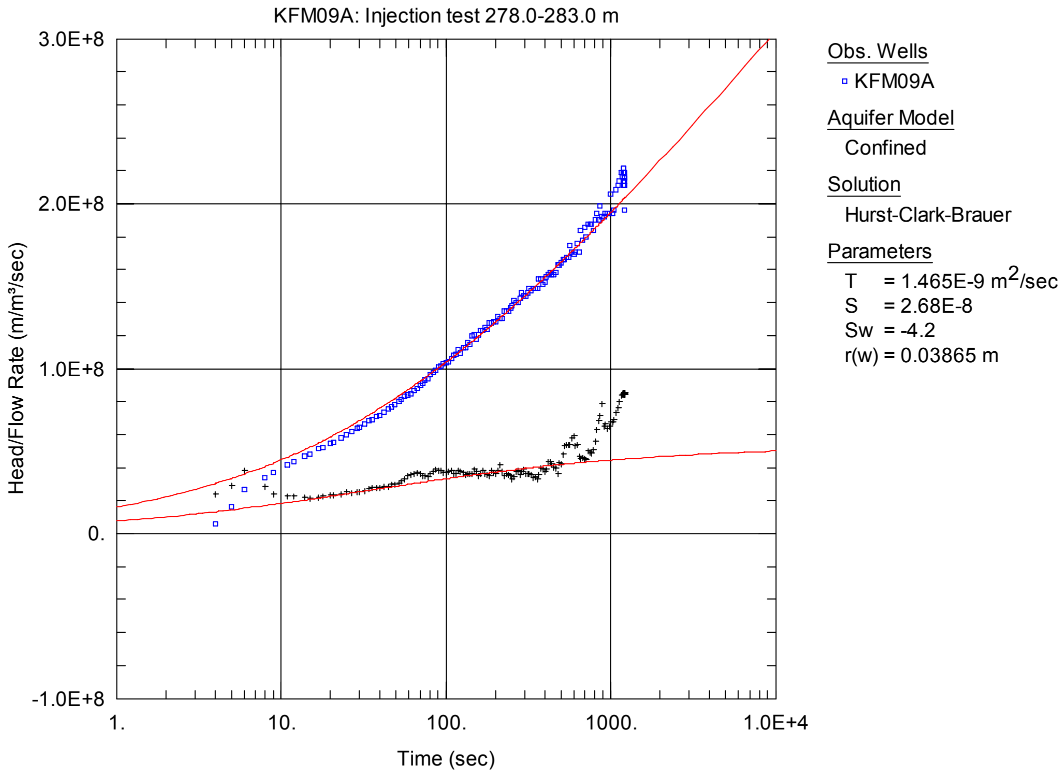


Figure A3-326. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 278.0-283.0 m in KFM09A This evaluation is made with the Hurst-Clark-Brauer model for a pseudo-radial response.*

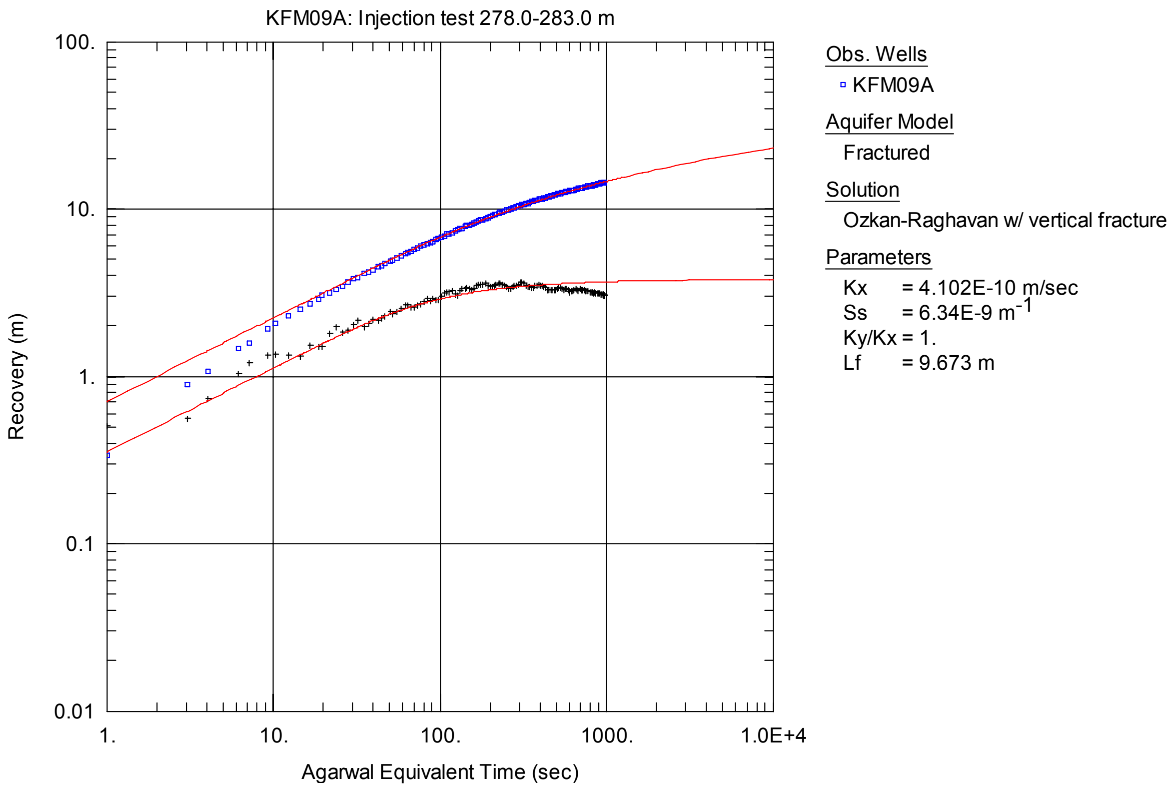


Figure A3-327. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 278.0-283.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

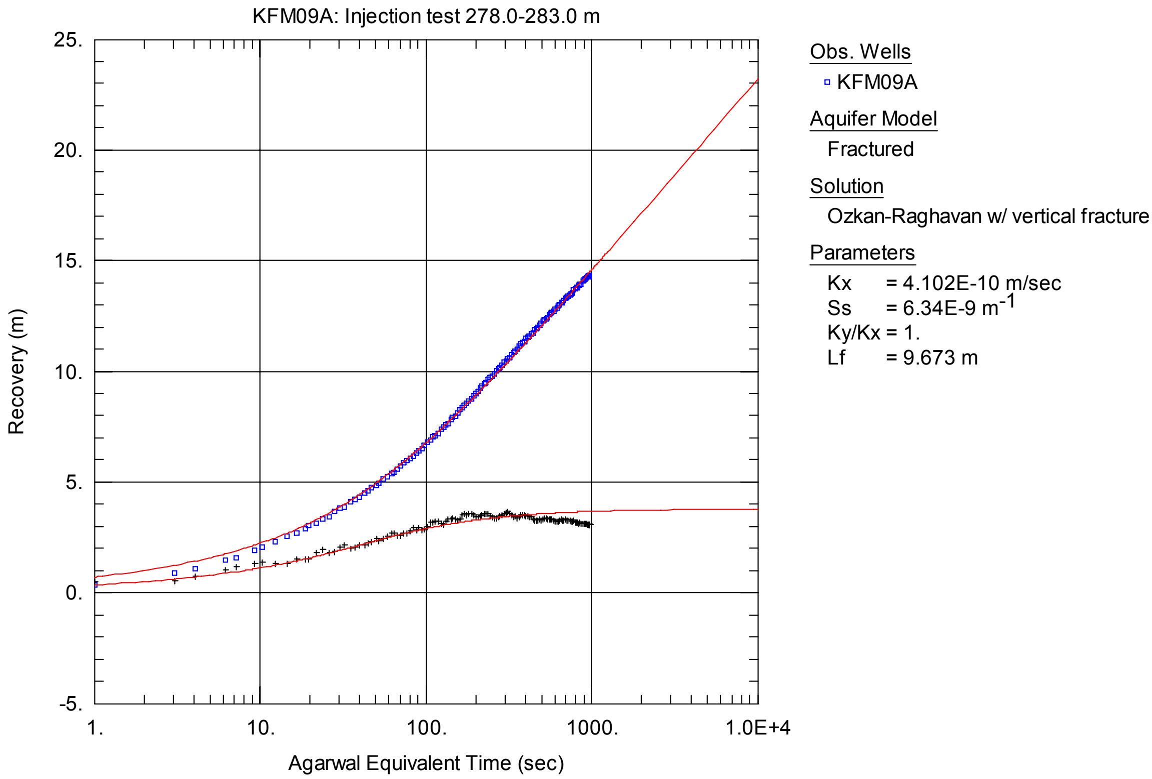


Figure A3-328. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 278.0-283.0 m in KFM09A This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

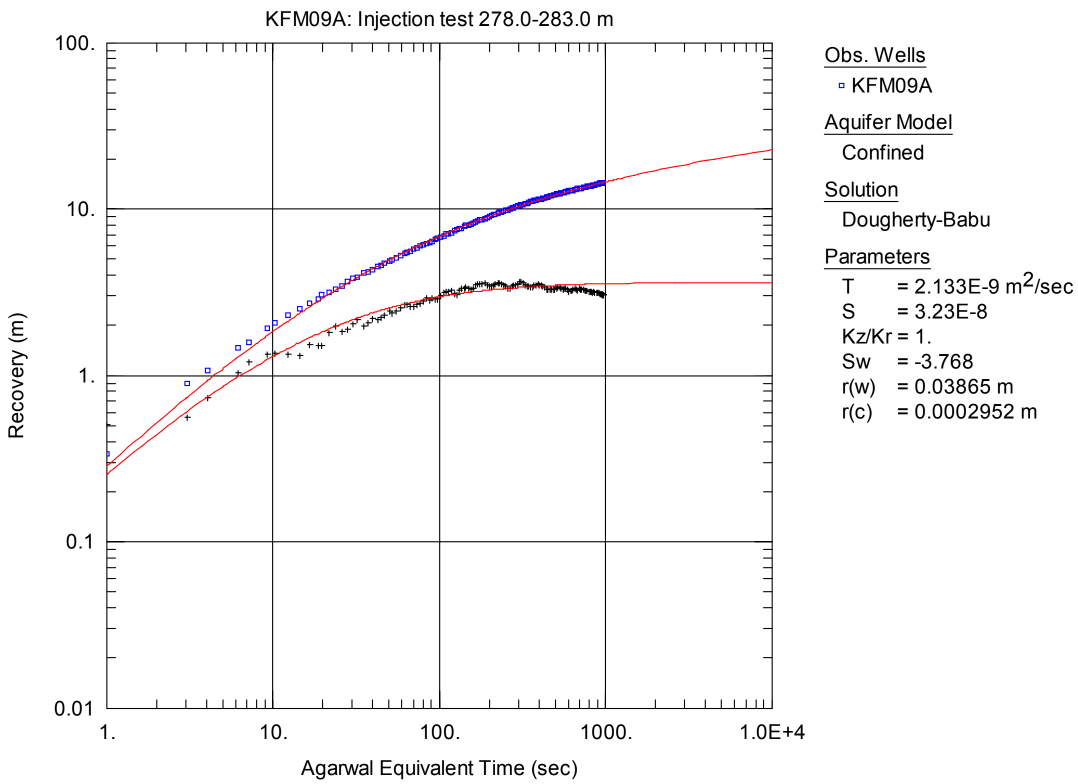


Figure A3-329. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 278.0-283.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for pseudo-radial response during recovery.*

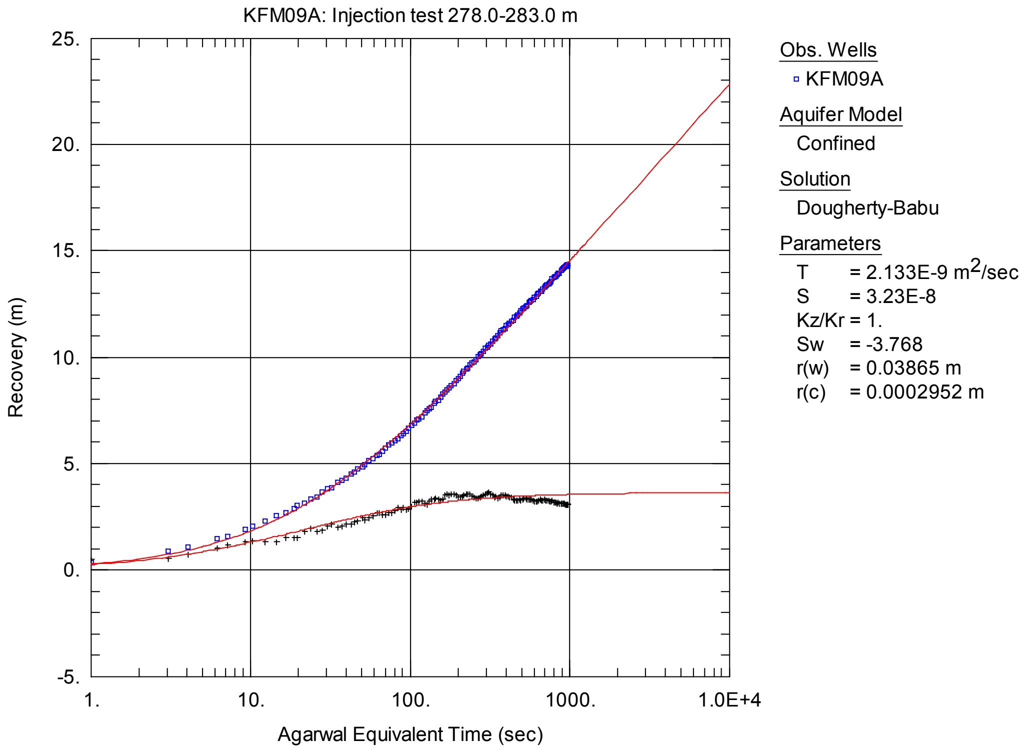


Figure A3-330. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 278.0-283.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for pseudo-radial response during recovery.*

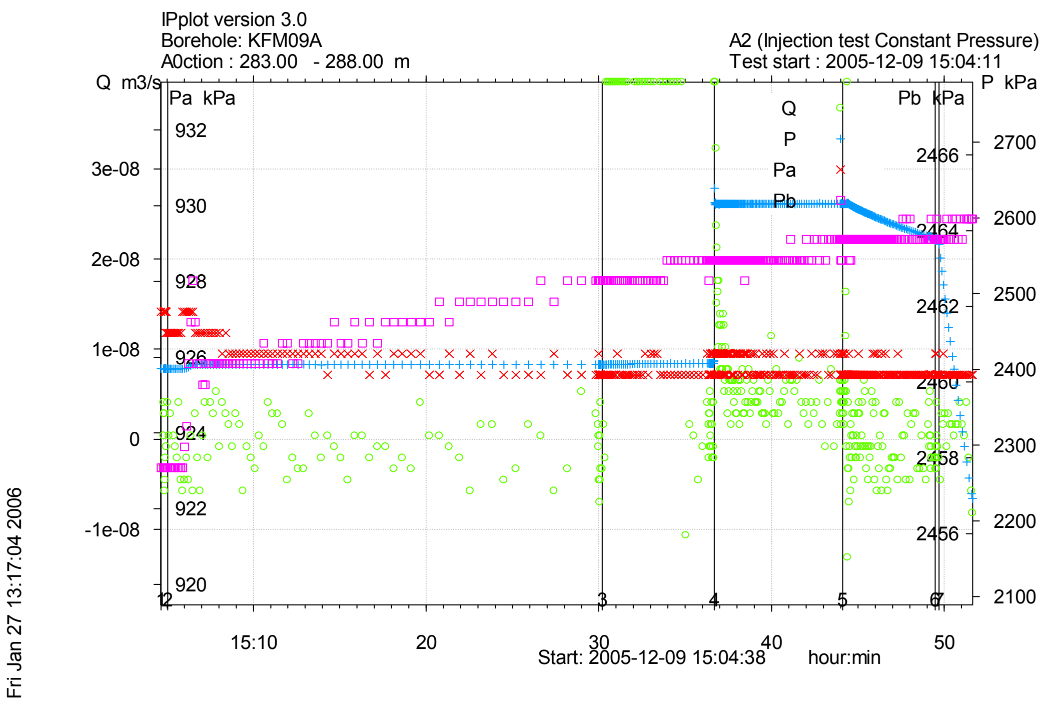


Figure A3-331. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 283.0-288.0 m in borehole KFM09A.*

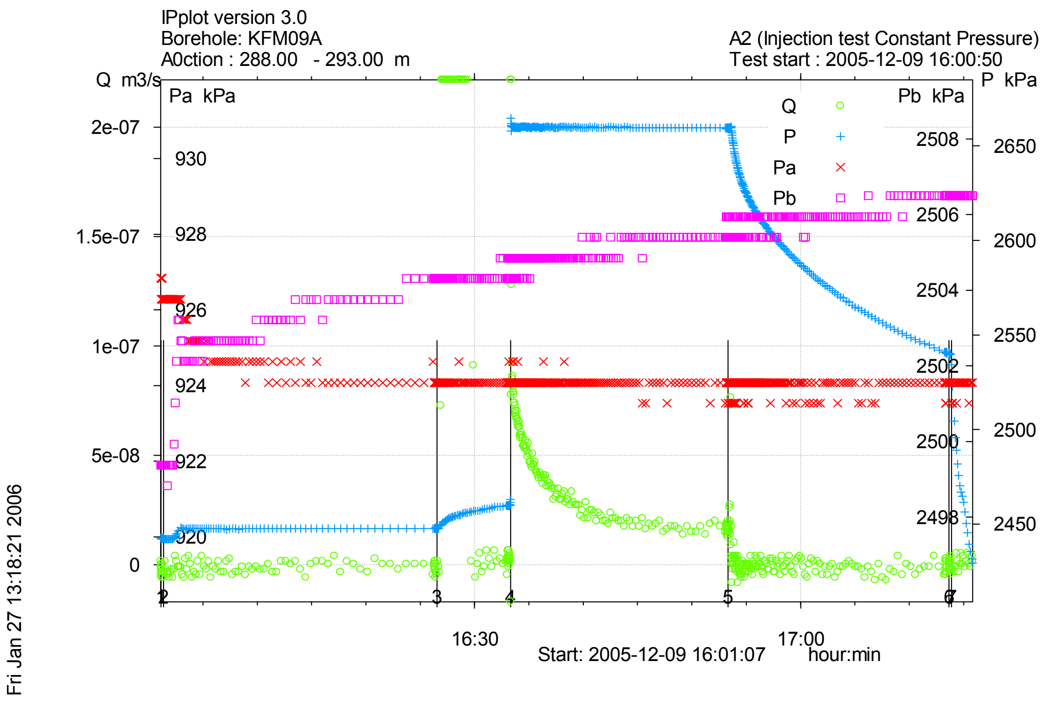


Figure A3-332. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 288.0-293.0 m in borehole KFM09A.

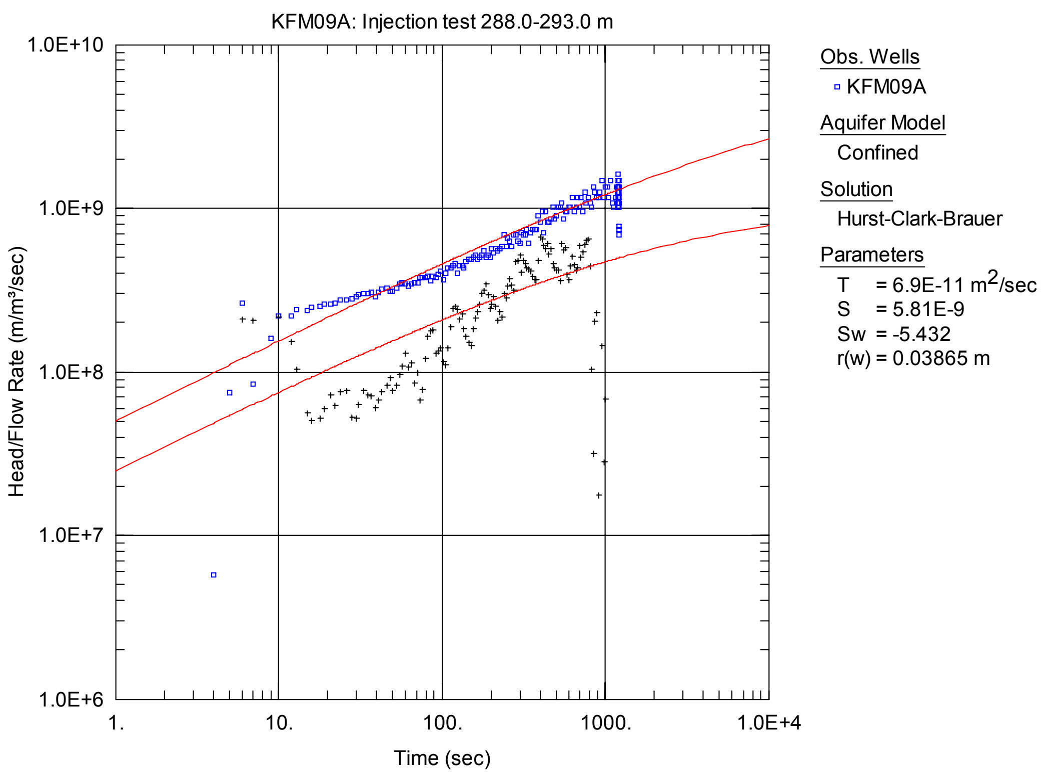


Figure A3-333. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 288.0-293.0 m in KFM09A.

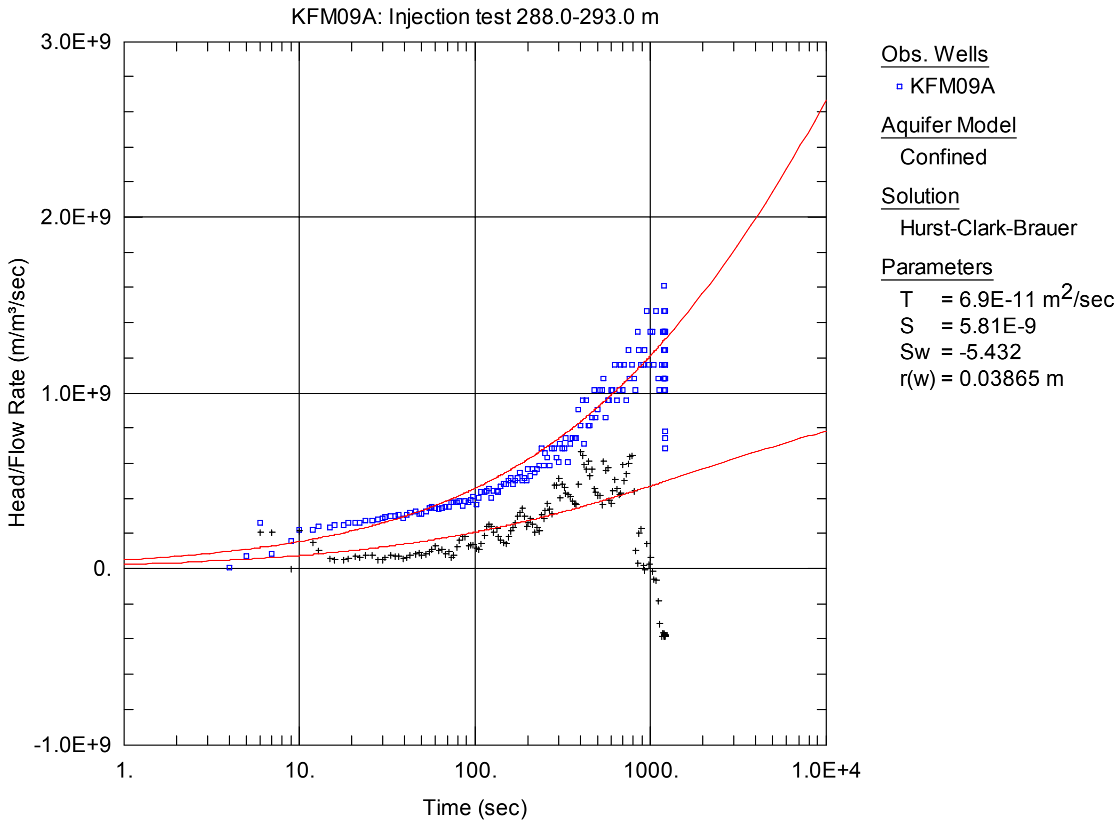


Figure A3-334. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 288.0-293.0 m in KFM09A.*

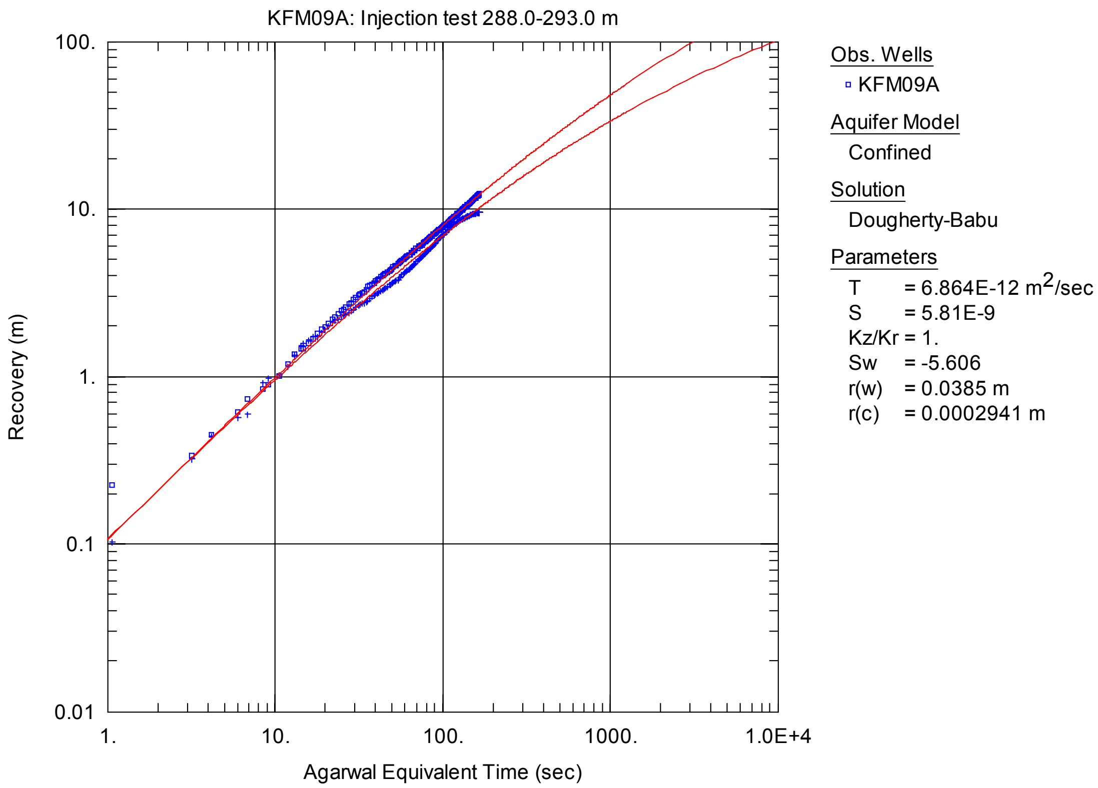


Figure A3-335. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 288.0-293.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.*

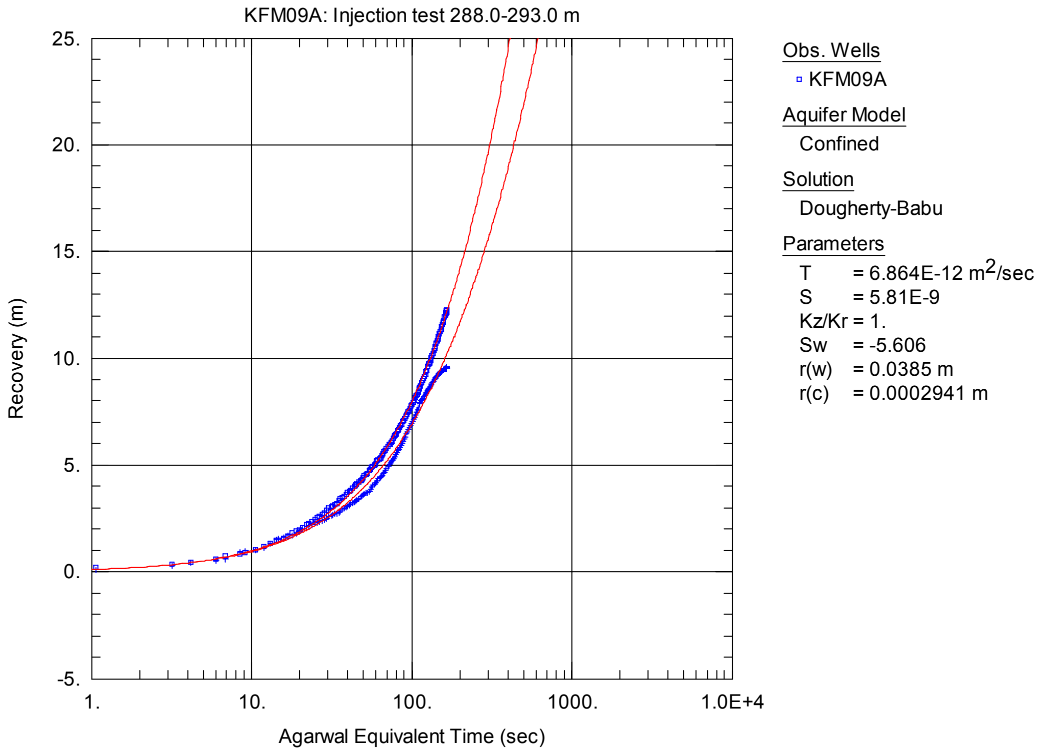


Figure A3-336. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 288.0-293.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.*

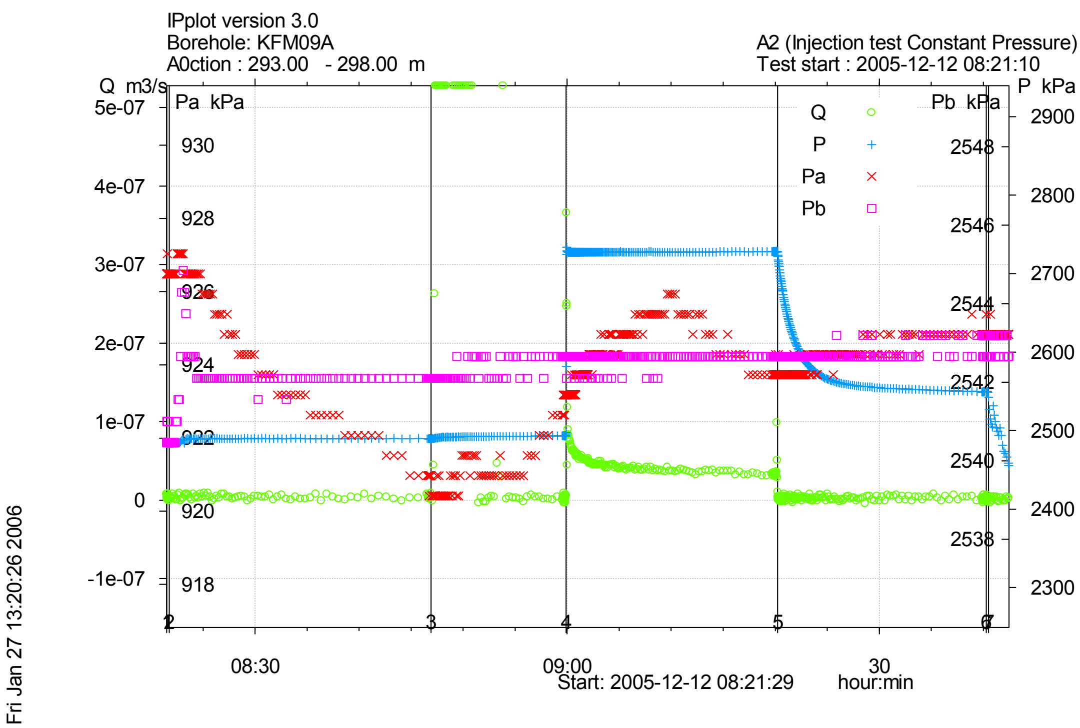


Figure A3-337. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 293.0-298.0 m in borehole KFM09A.*

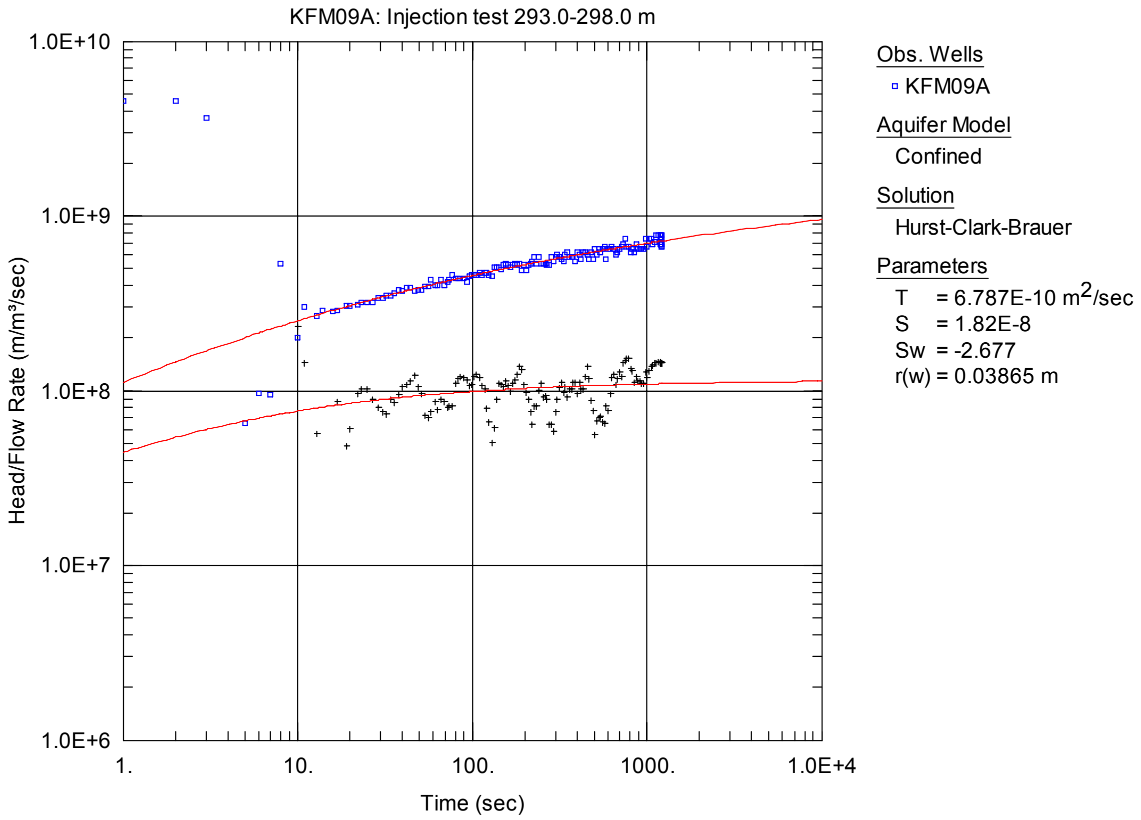


Figure A3-338. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 293.0-298.0 m in KFM09A.*

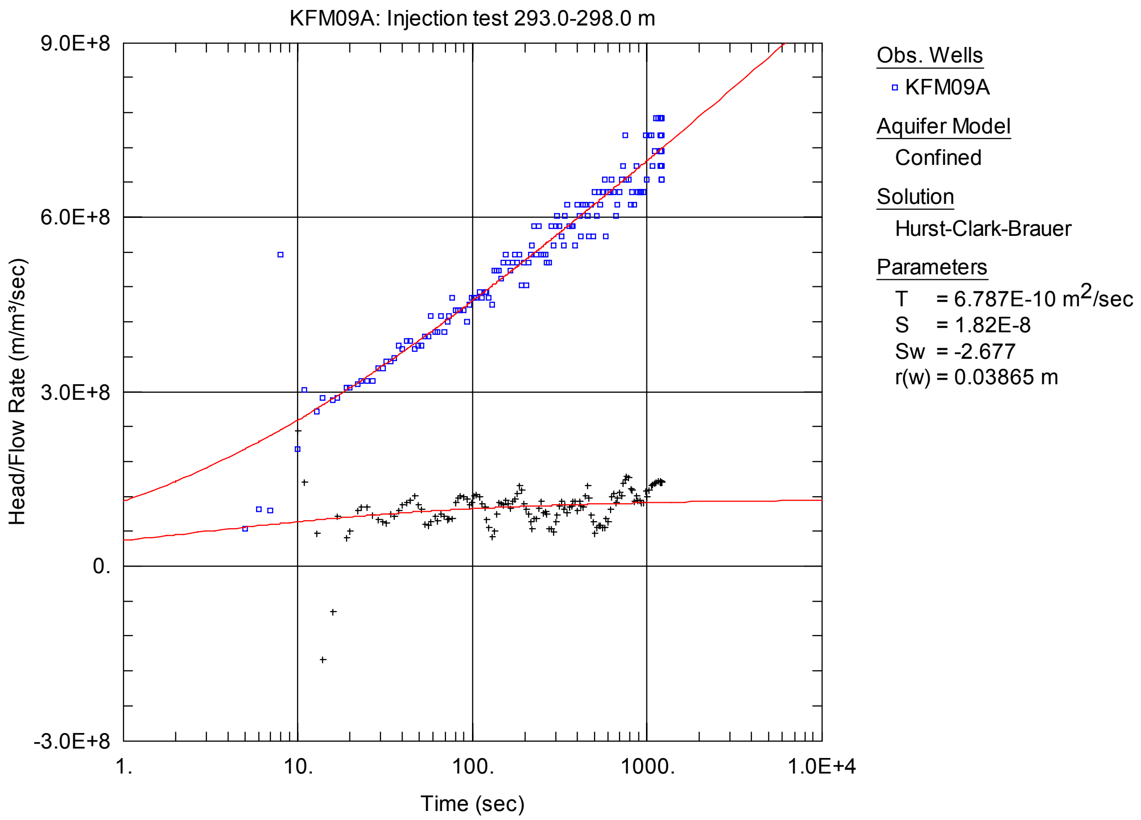


Figure A3-339. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 293.0-298.0 m in KFM09A.*

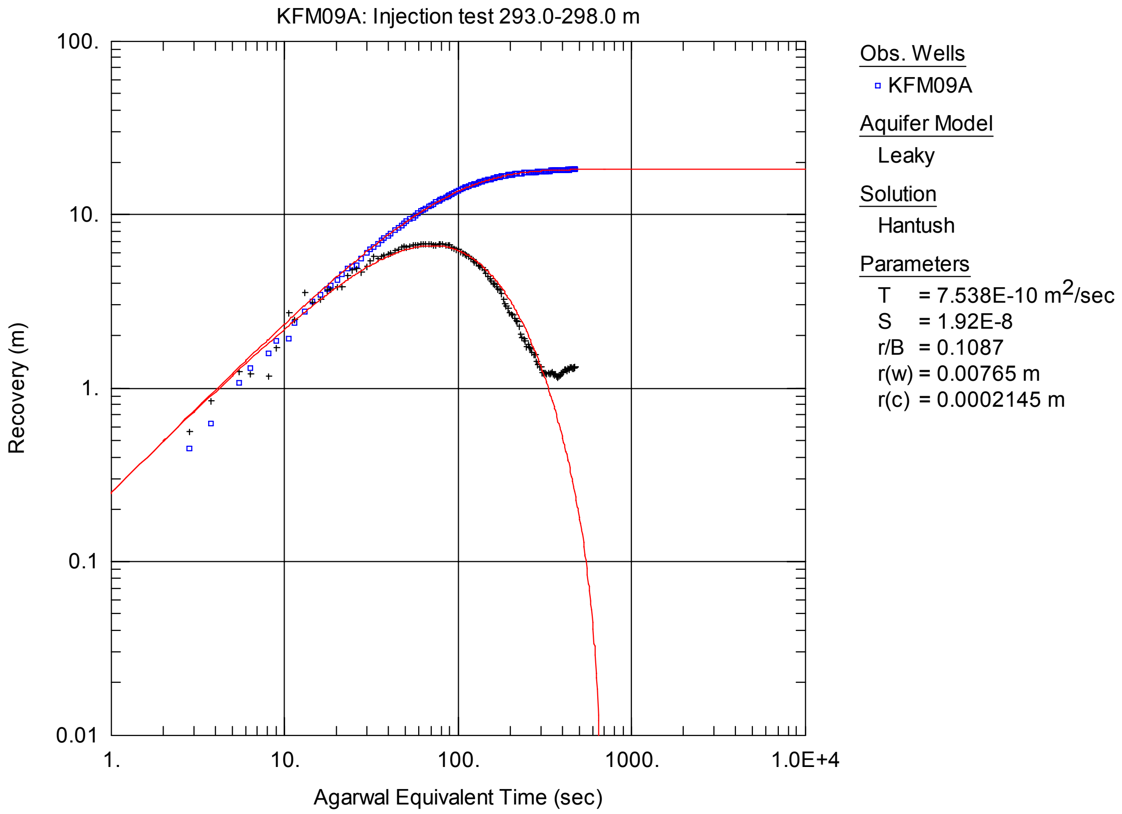


Figure A3-340. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 293.0-298.0 m in KFM09A.*

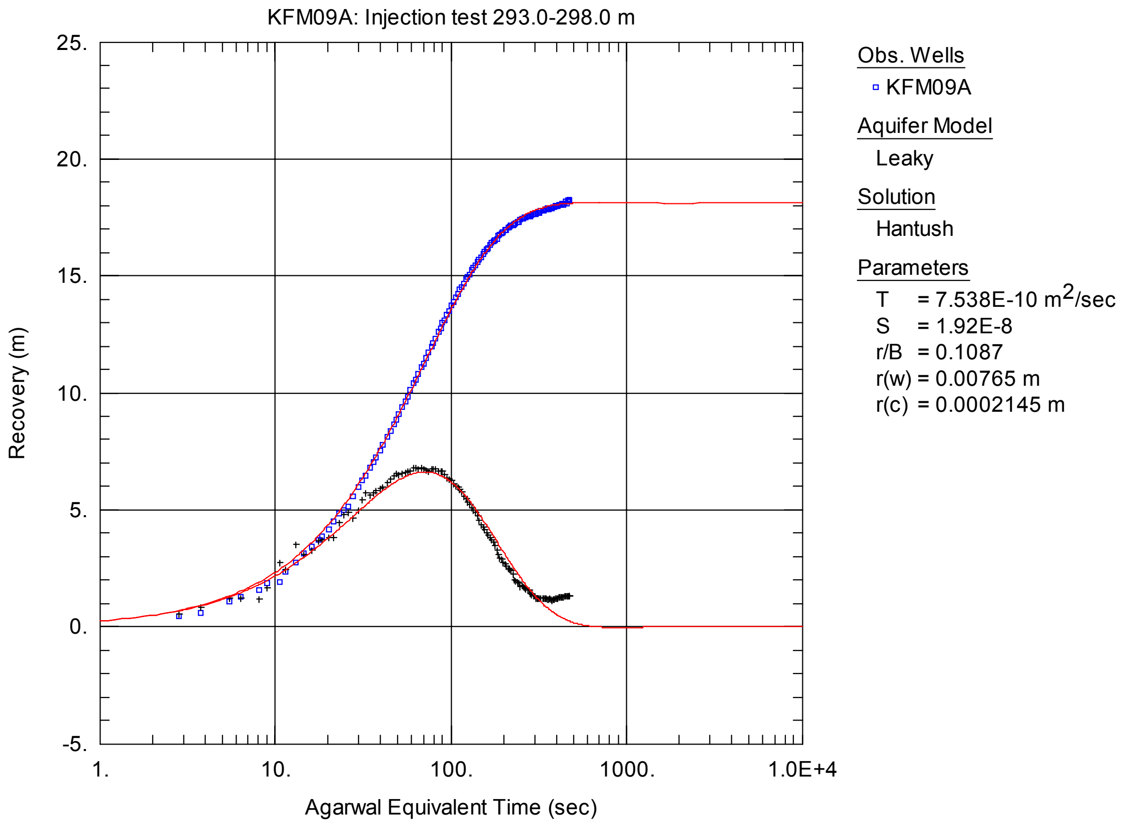


Figure A3-341. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 293.0-298.0 m in KFM09A.*

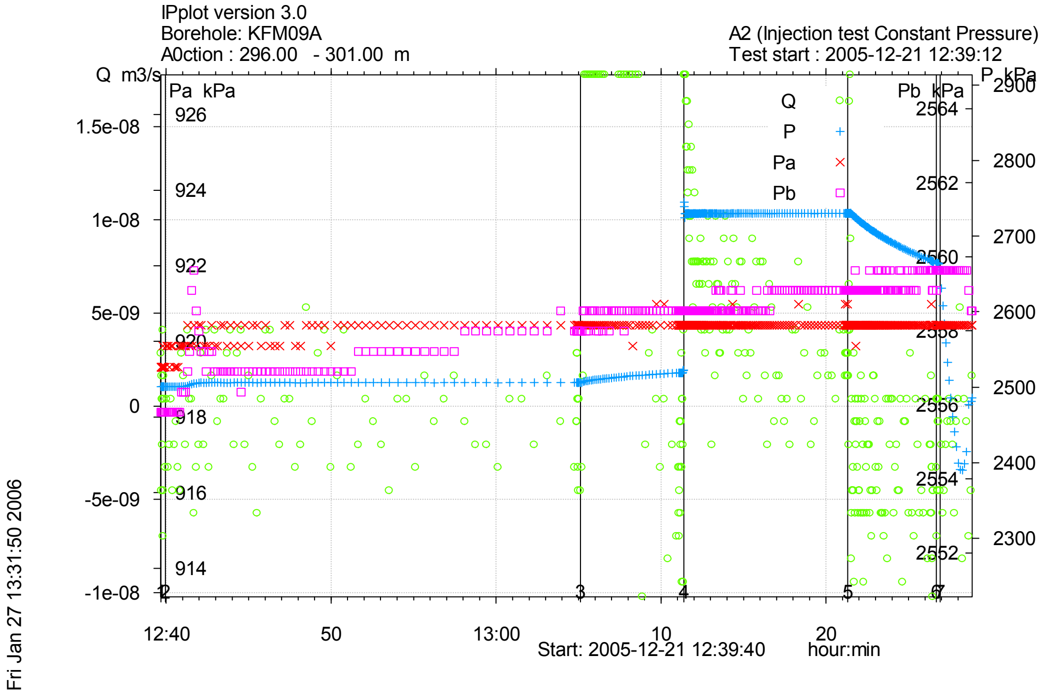


Figure A3-342. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 296.0-301.0 m in borehole KFM09A.*

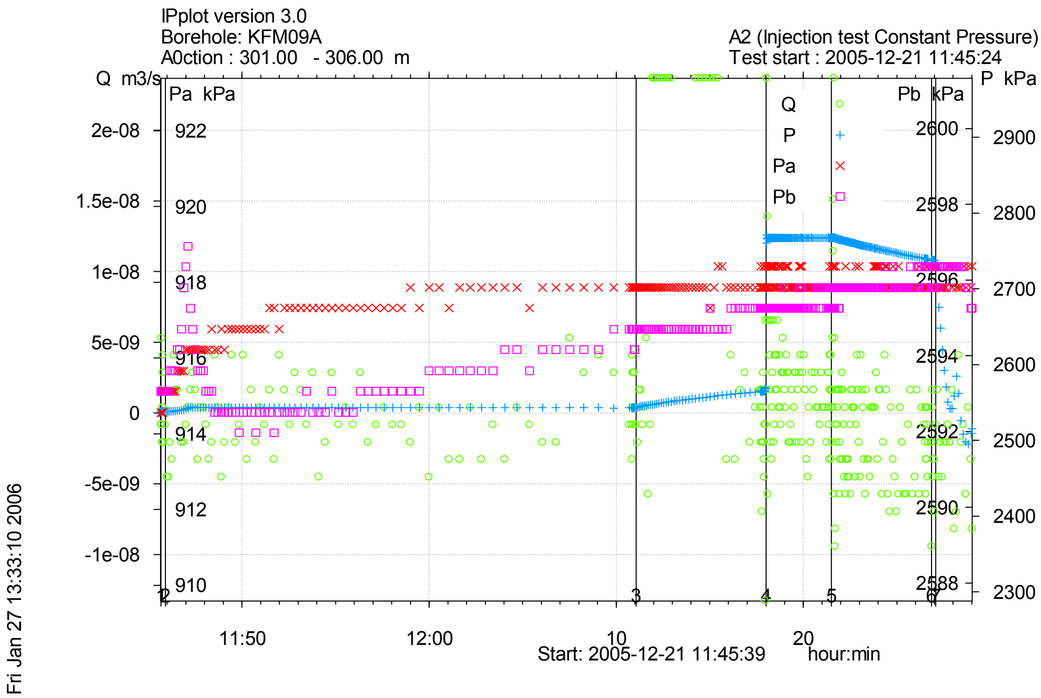


Figure A3-343. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 301.0-306.0 m in borehole KFM09A.*

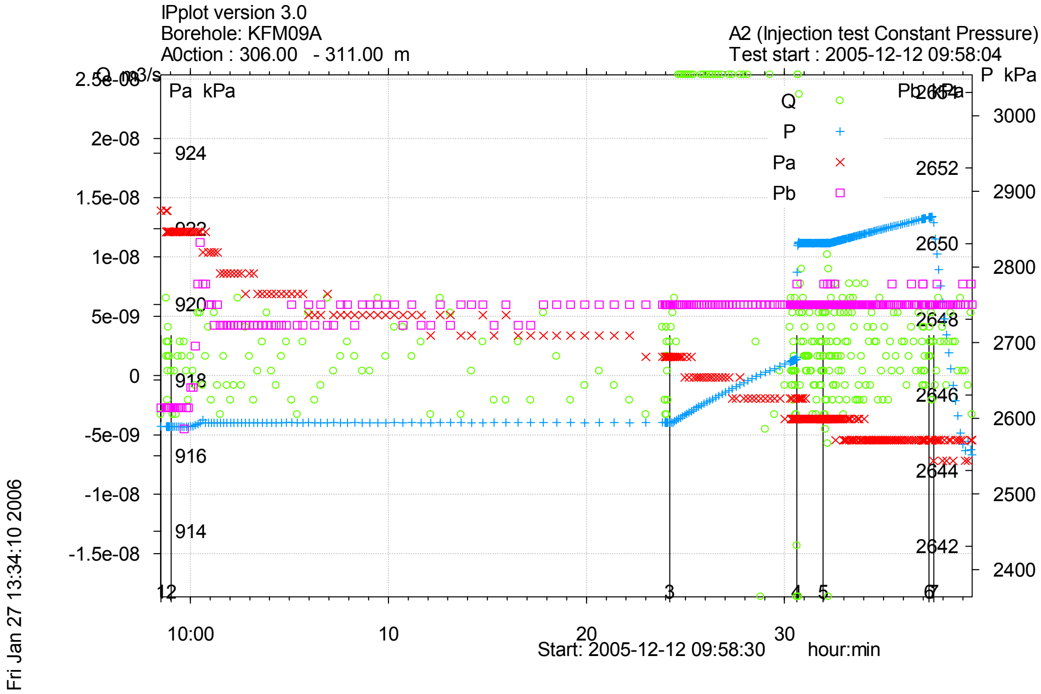


Figure A3-344. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 306.0-311.0 m in borehole KFM09A.

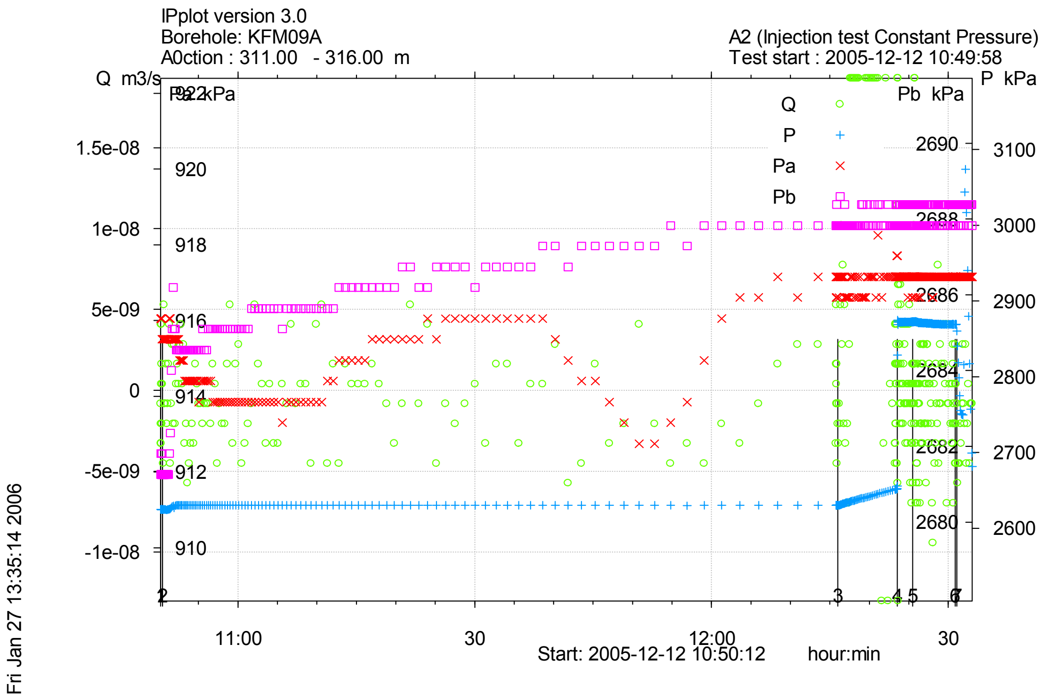


Figure A3-345. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 311.0-316.0 m in borehole KFM09A.

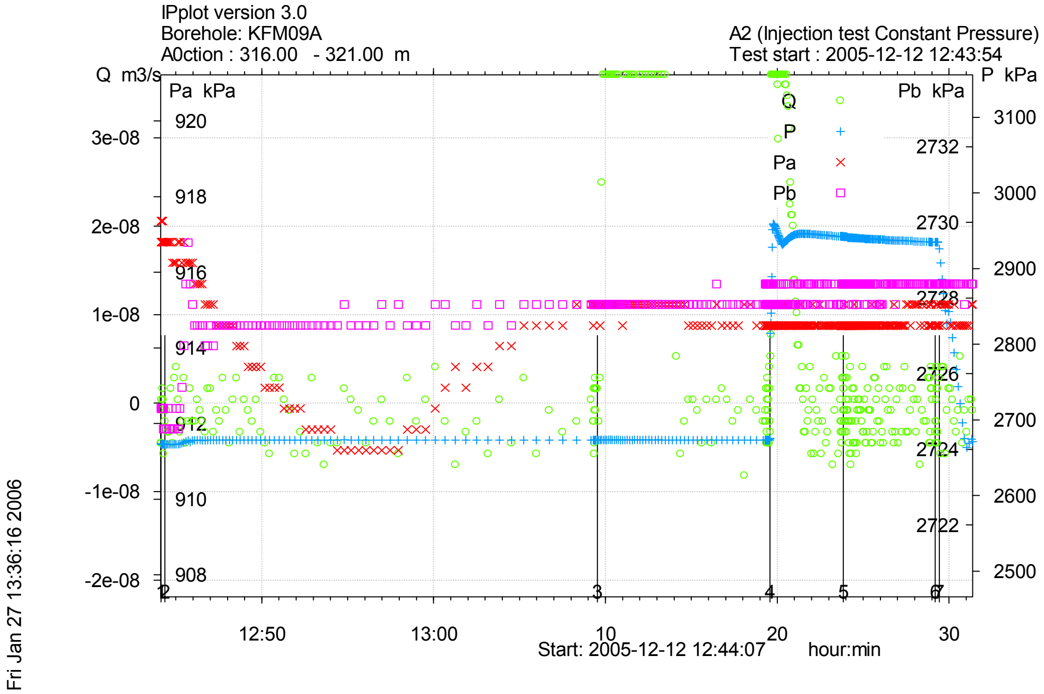


Figure A3-346. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 316.0-321.0 m in borehole KFM09A.

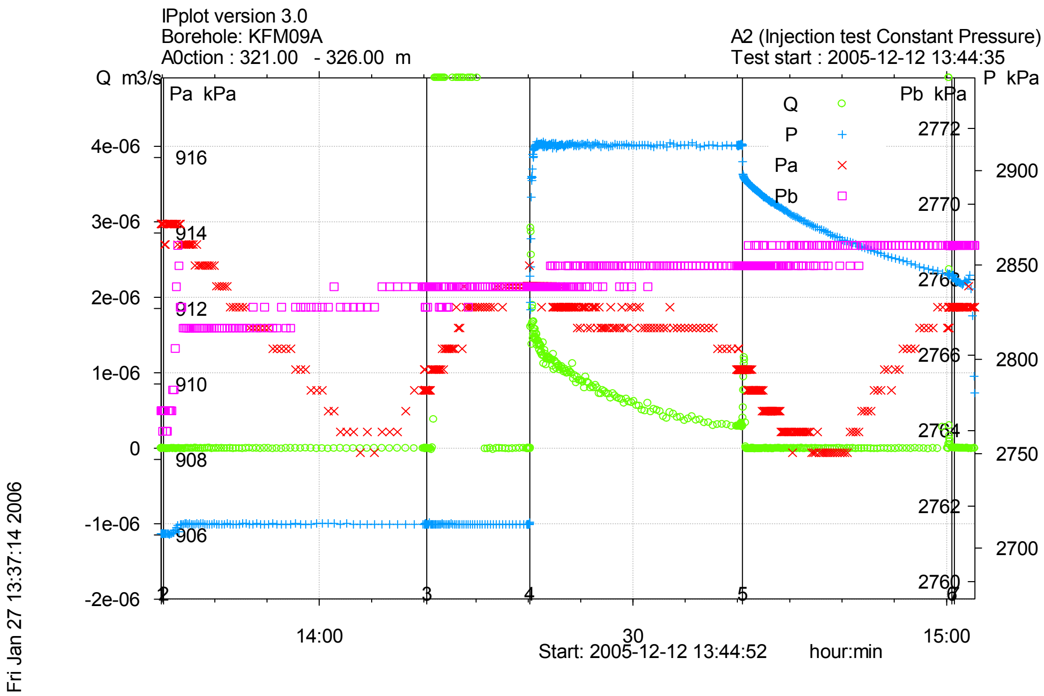


Figure A3-347. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 321.0-326.0 m in borehole KFM09A.

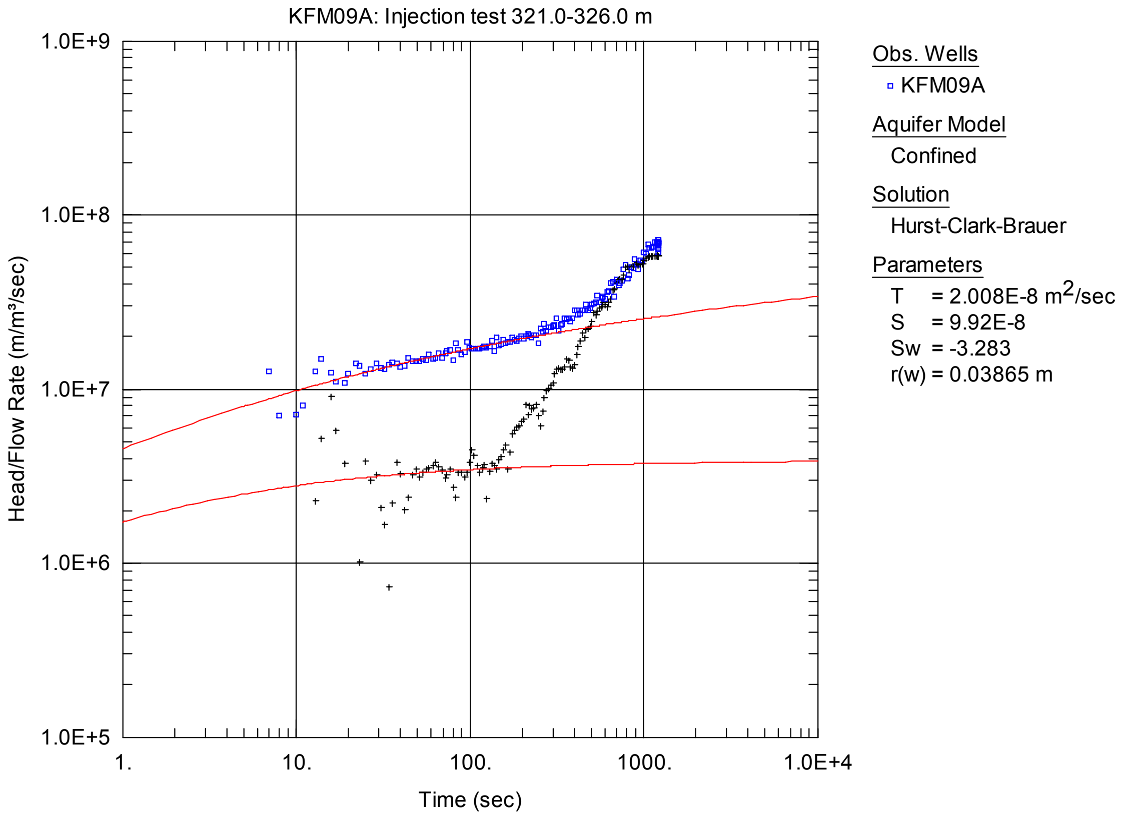


Figure A3-348. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 321.0-326.0 m in KFM09A.*

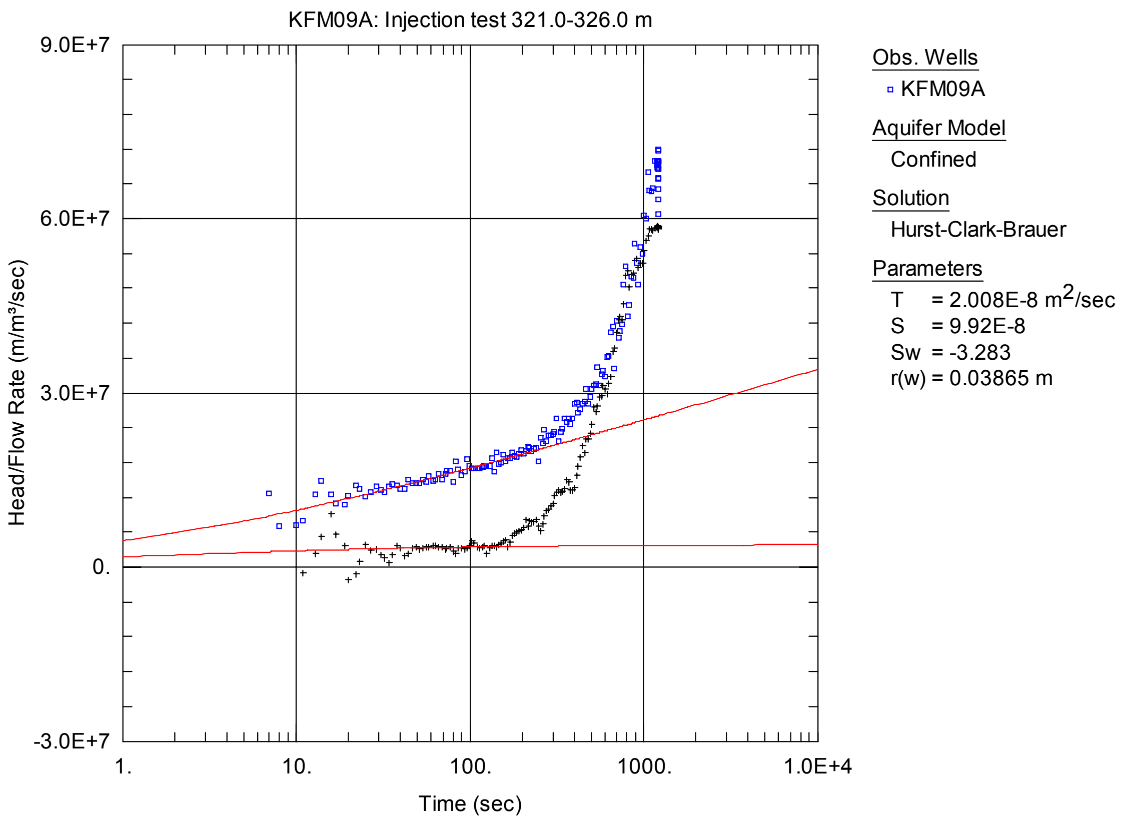


Figure A3-349. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 321.0-326.0 m in KFM09A.*

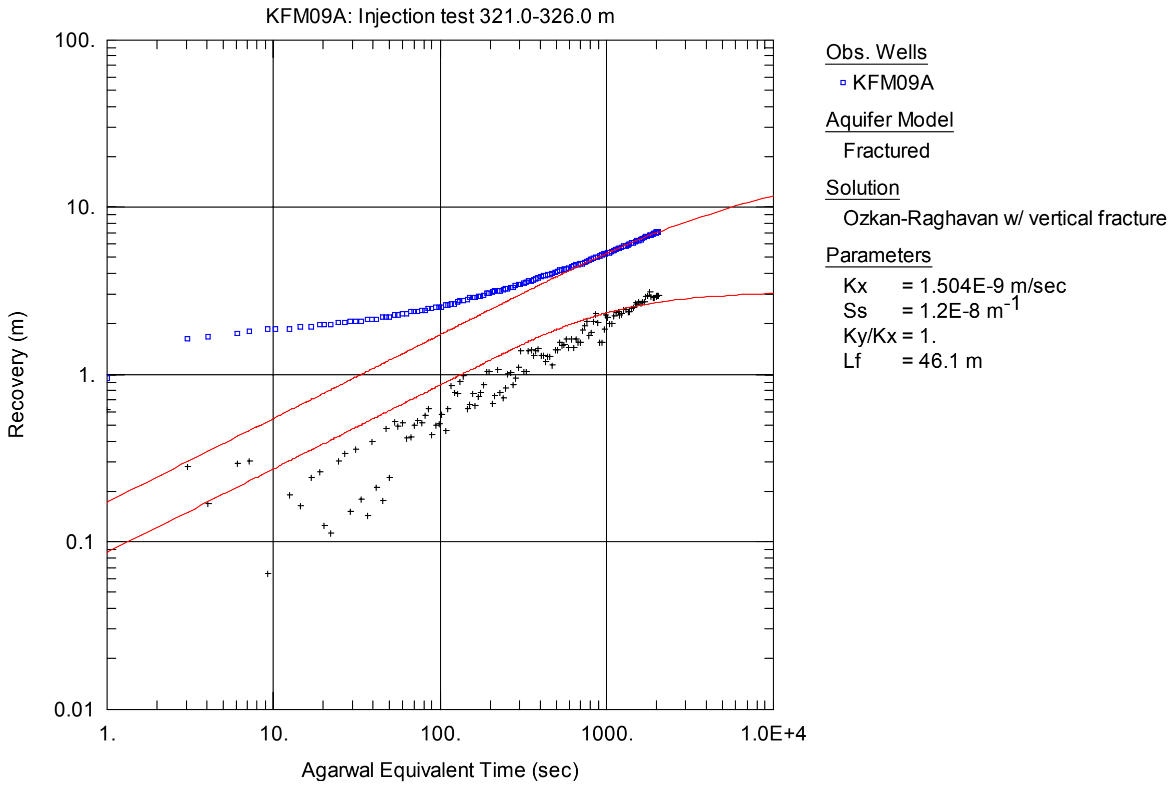


Figure A3-350. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 321.0-326.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.*

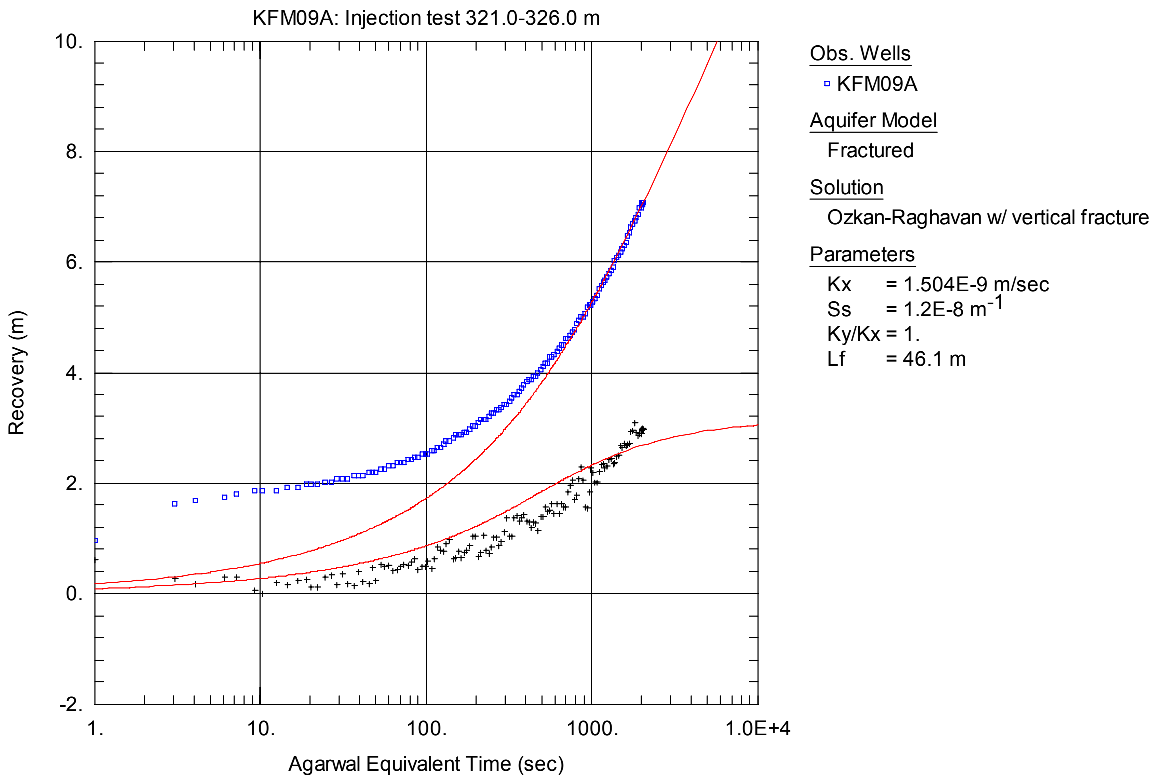


Figure A3-351. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 321.0-326.0 m in KFM09A No unambiguous transient evaluation is possible on the recovery period.*

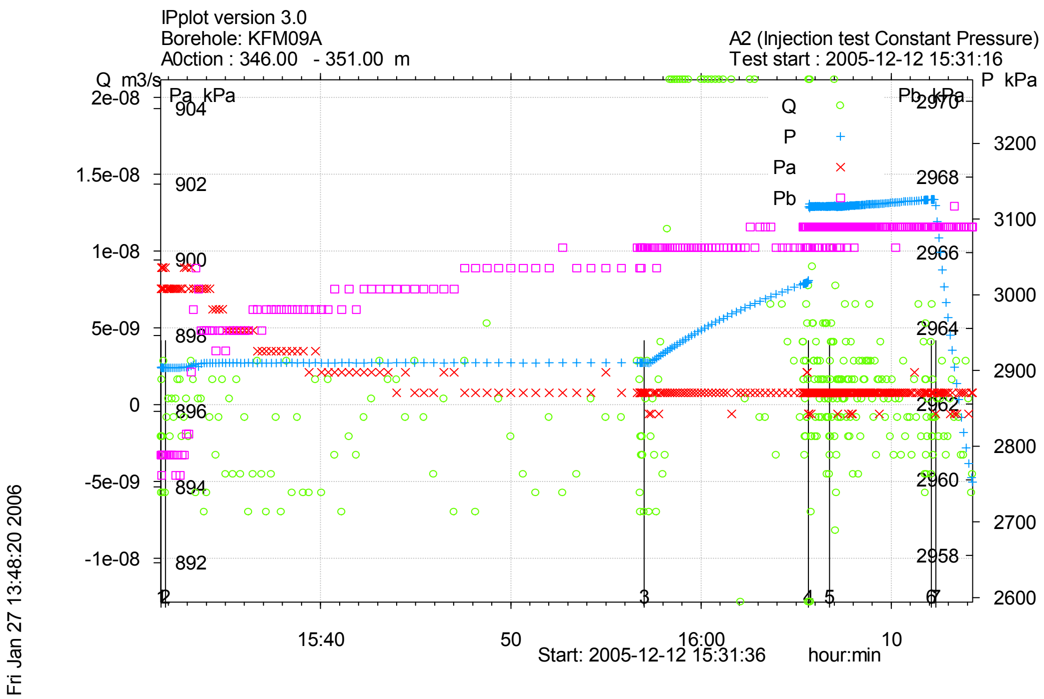


Figure A3-352. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 346.0-351.0 m in borehole KFM09A.*

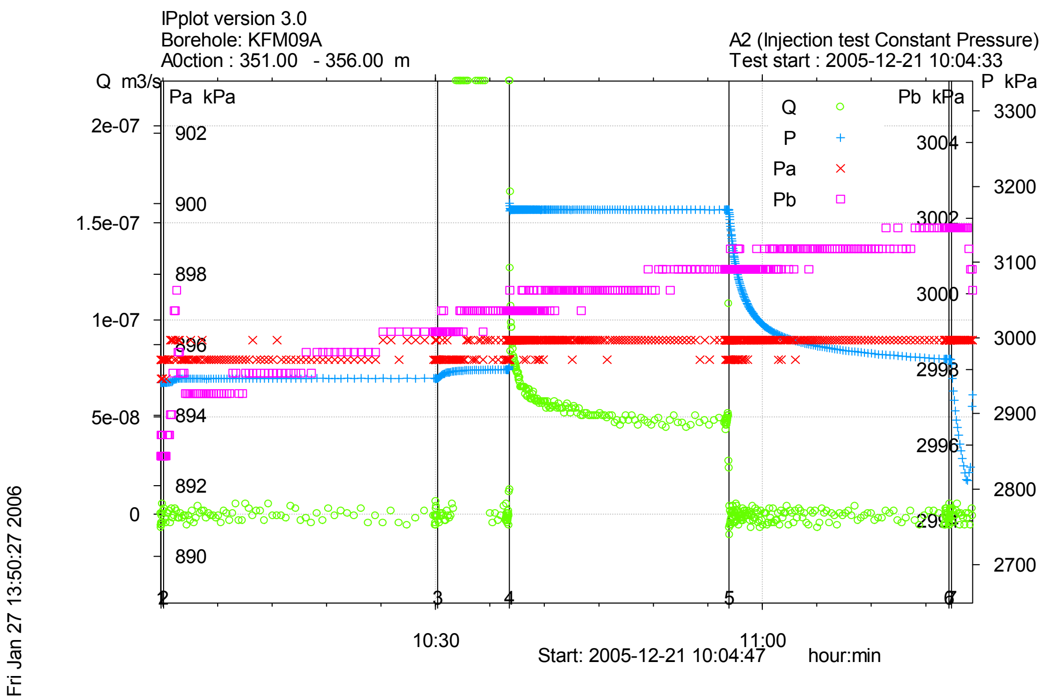


Figure A3-353. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 351.0-356.0 m in borehole KFM09A.*

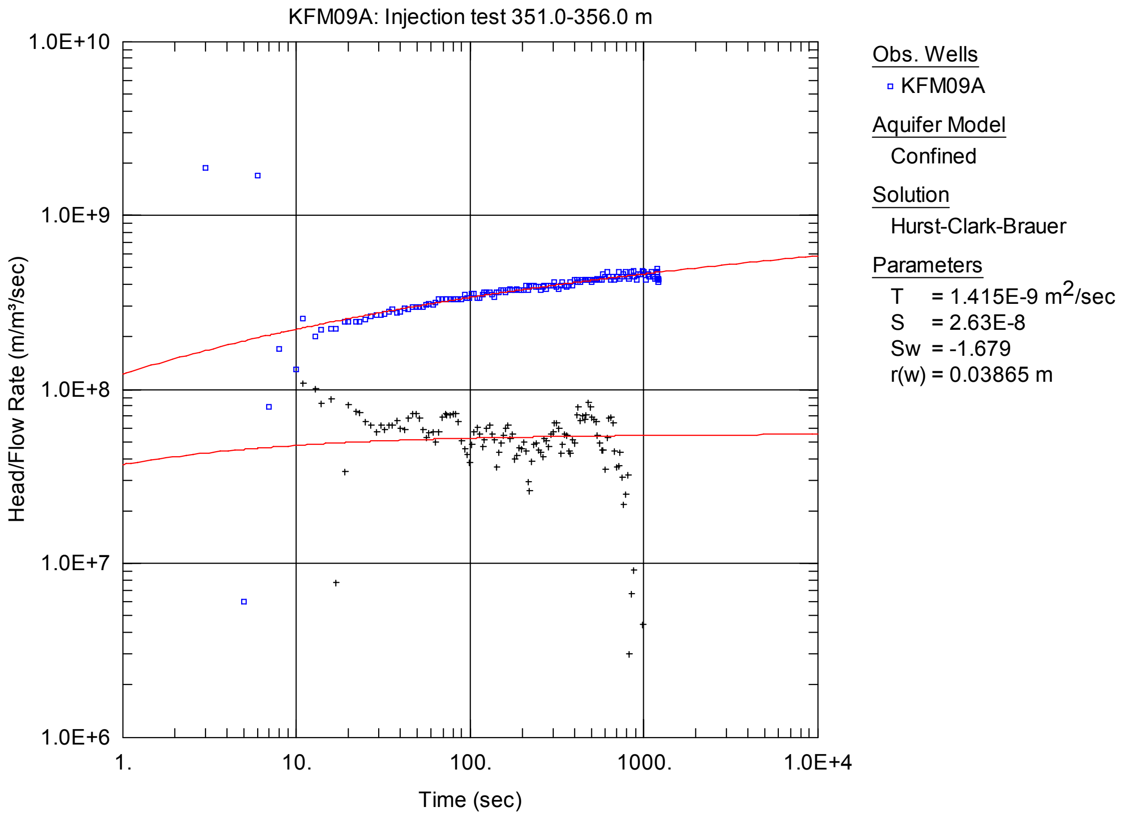


Figure A3-354. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 351.0-356.0 m in KFM09A.*

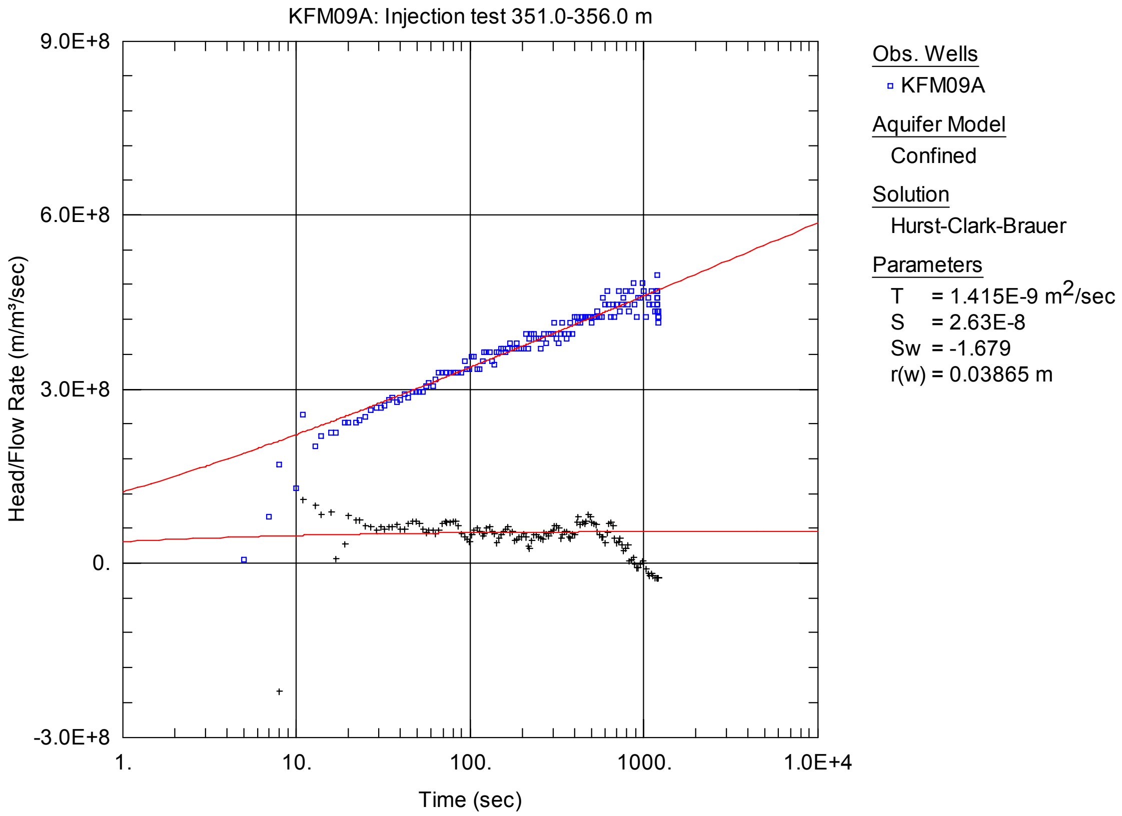


Figure A3-355. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 351.0-356.0 m in KFM09A.*

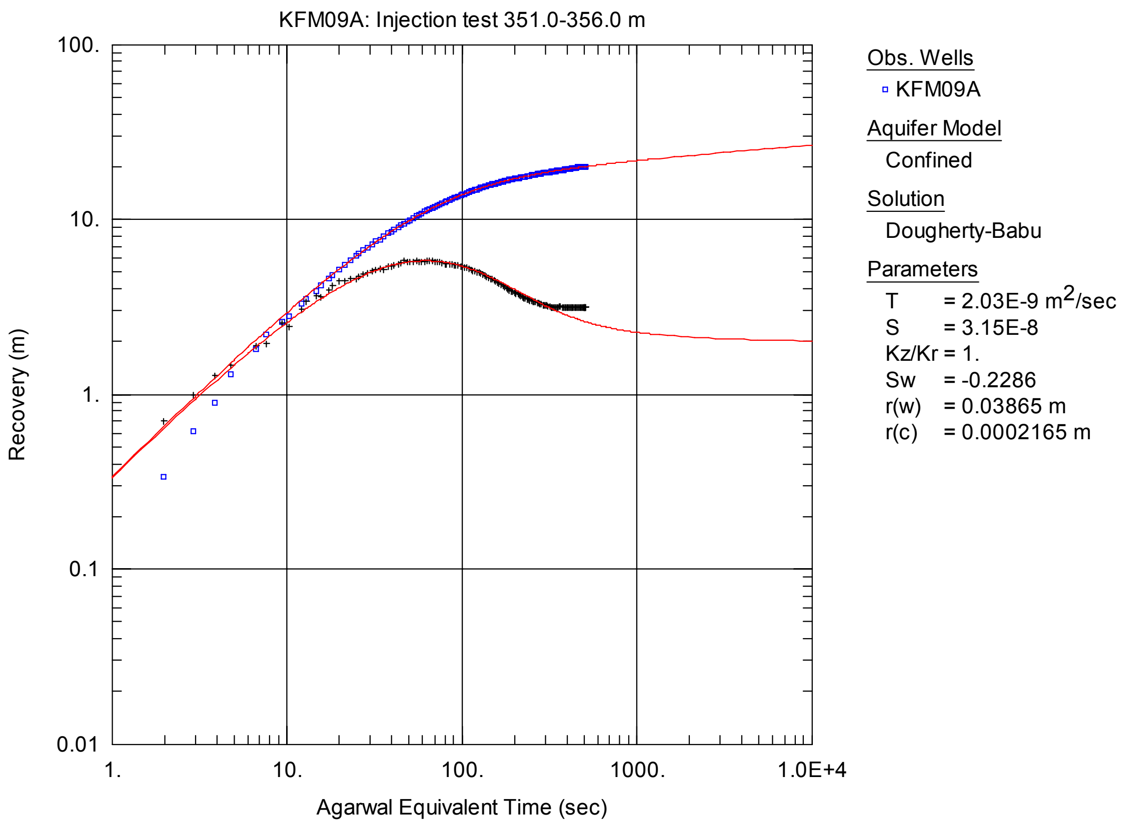


Figure A3-356. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 351.0-356.0 m in KFM09A.*

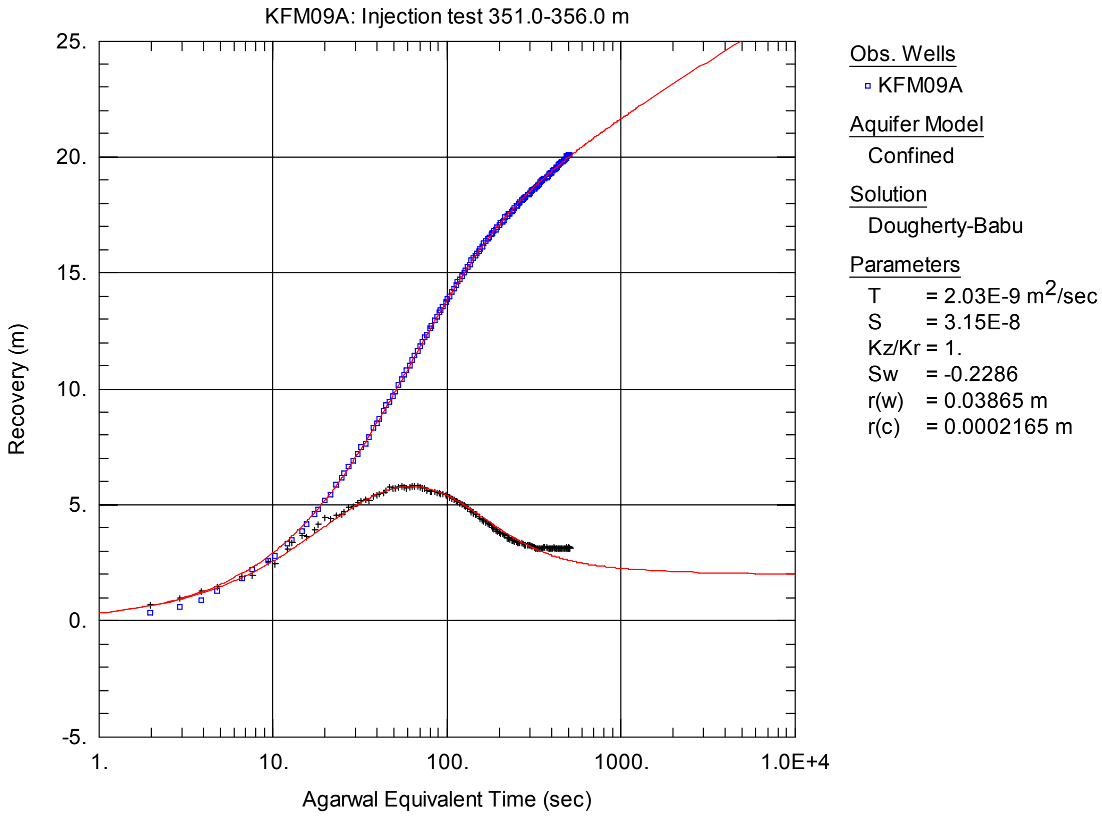


Figure A3-357. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 351.0-356.0 m in KFM09A.*

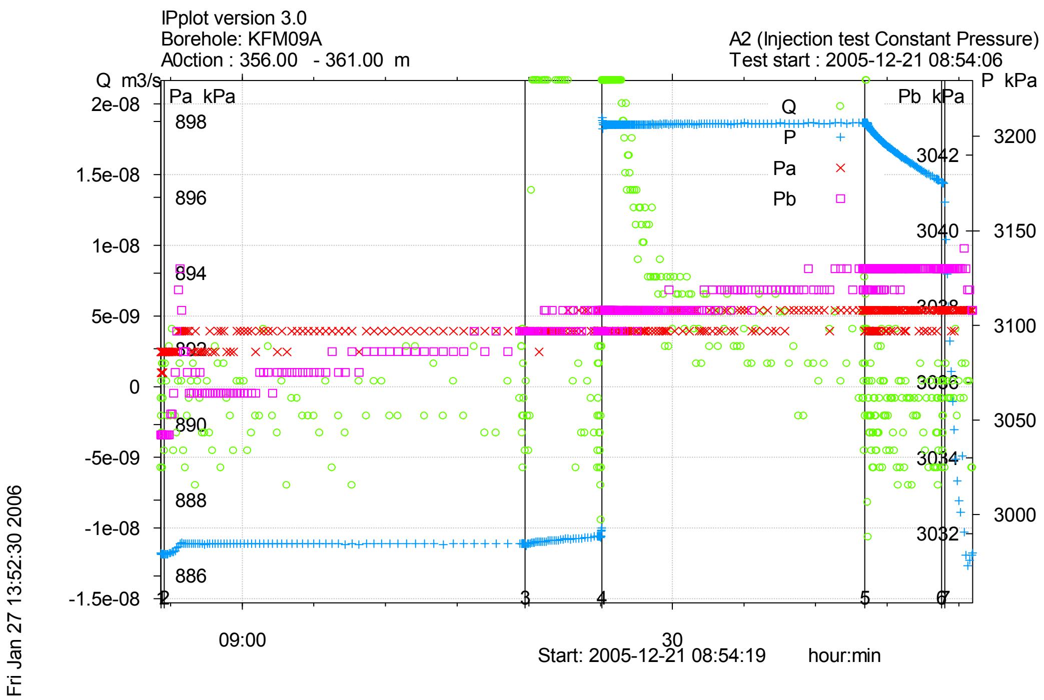


Figure A3-358. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 356.0-361.0 m in borehole KFM09A.*

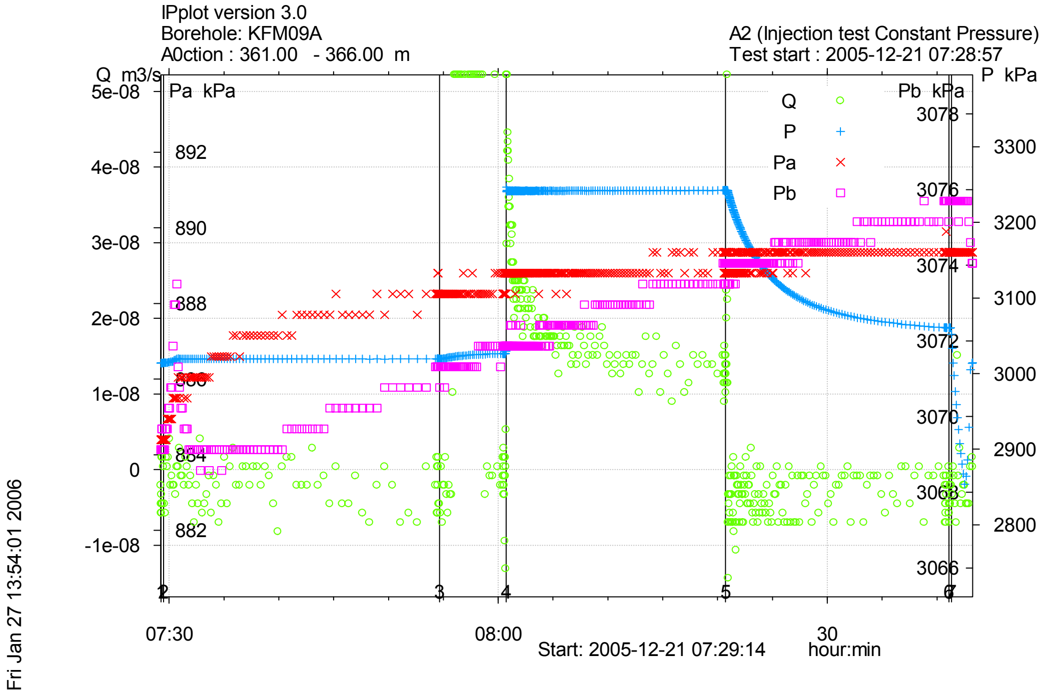


Figure A3-359. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 361.0-366.0 m in borehole KFM09A.*

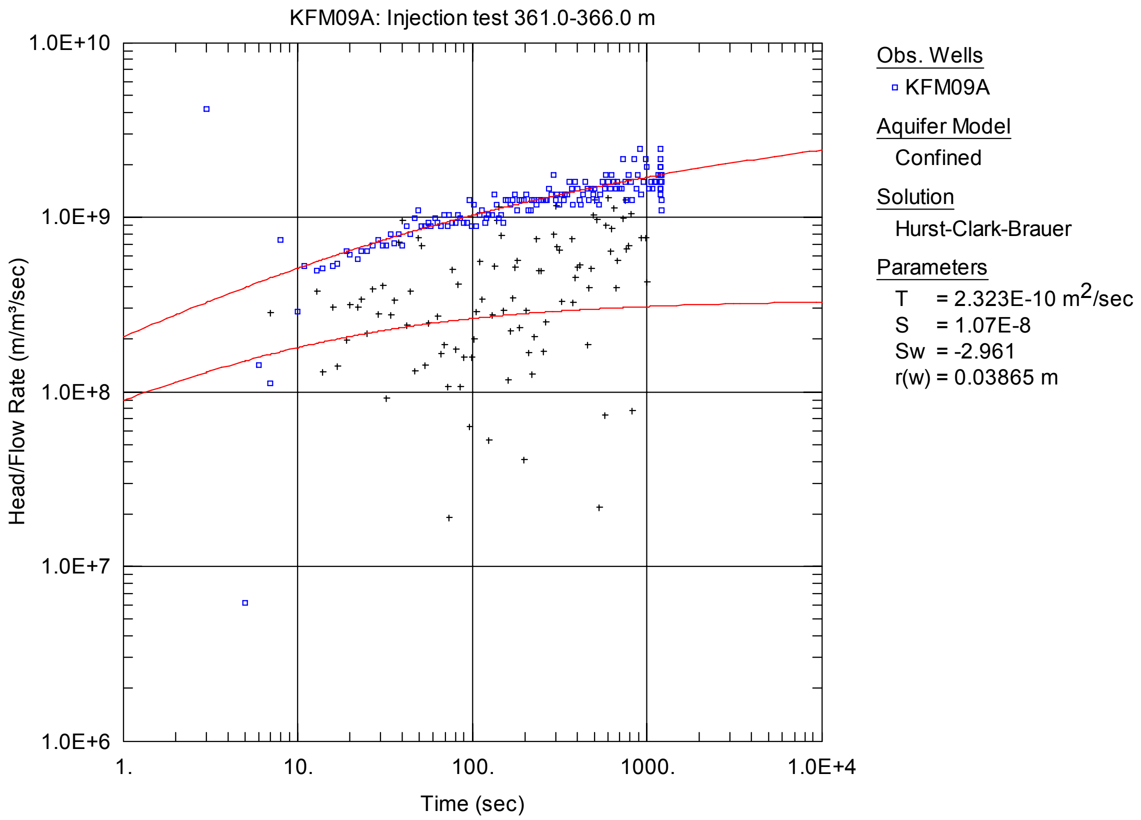


Figure A3-360. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 361.0-366.0 m in KFM09A.*

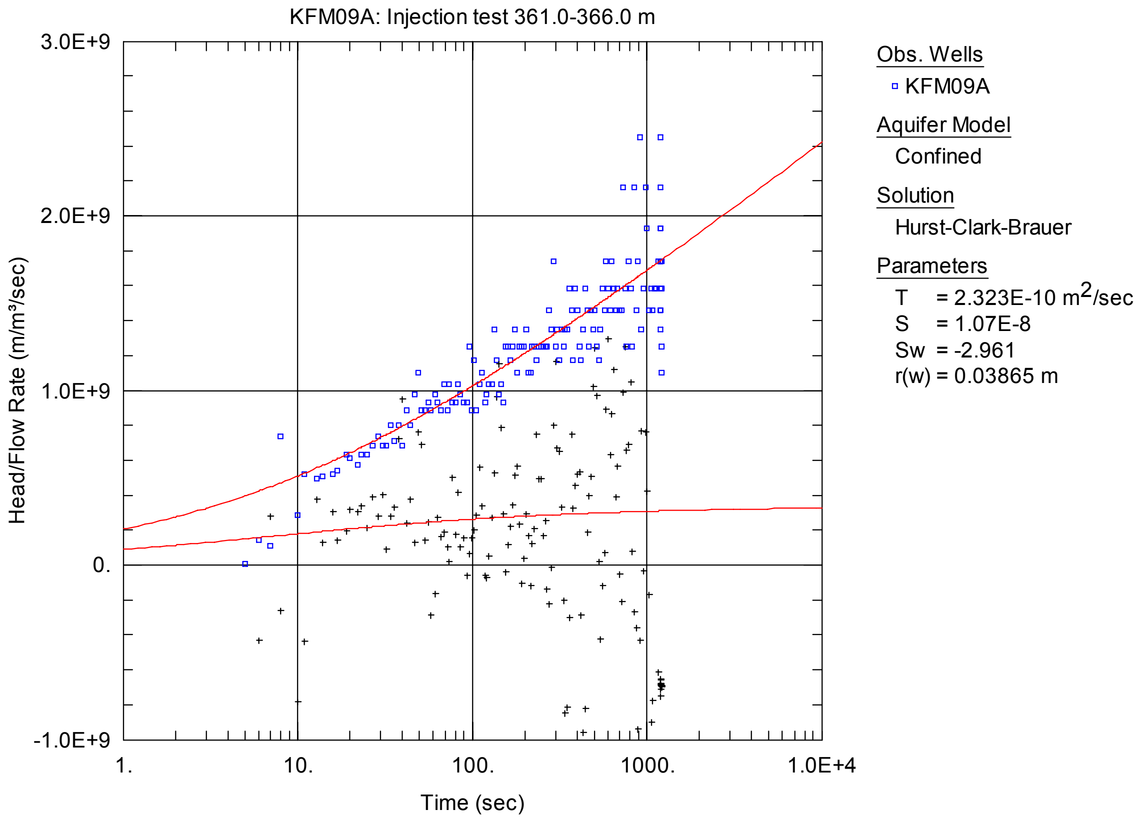


***Figure A3-361.** Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 361.0-366.0 m in KFM09A.*

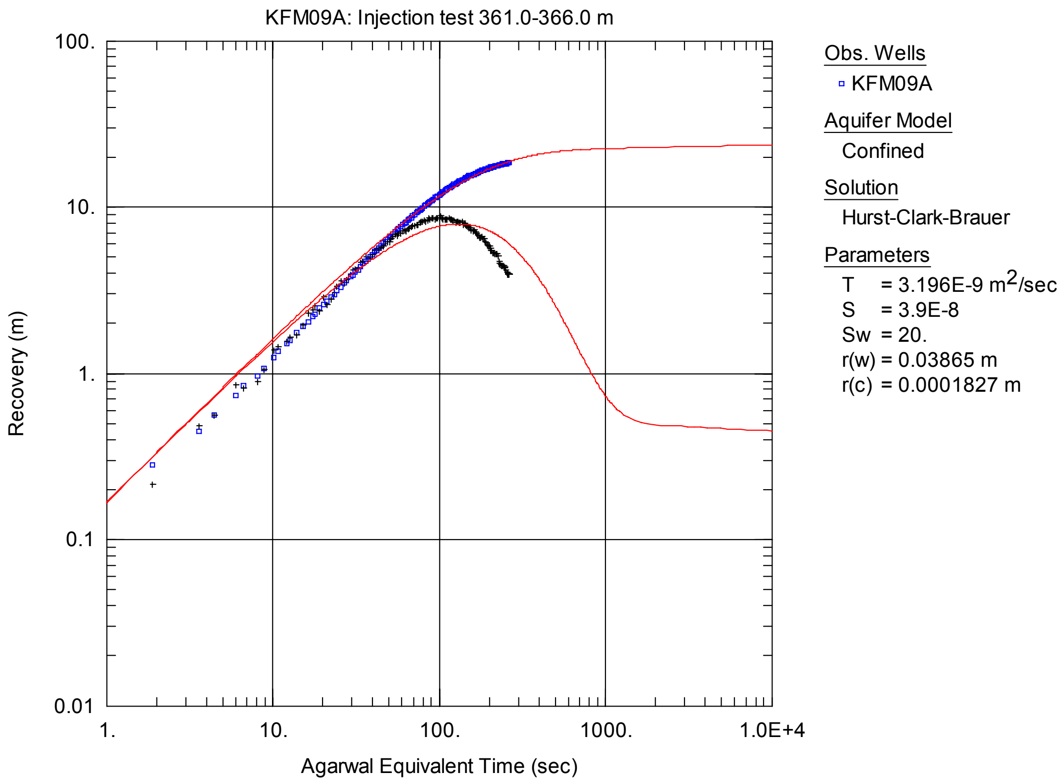


***Figure A3-362.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 361.0-366.0 m in KFM09A. No unambiguous transient evaluation could be made from the recovery period.*

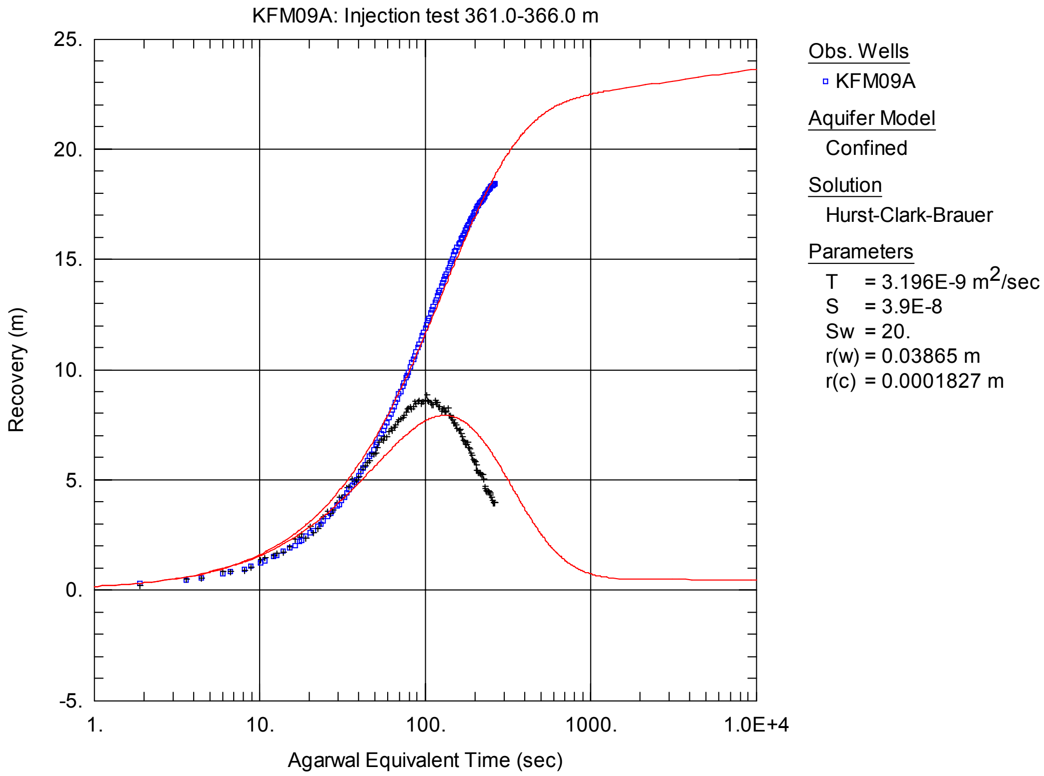


Figure A3-363. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 361.0-366.0 m in KFM09A. No unambiguous transient evaluation could be made from the recovery period.*

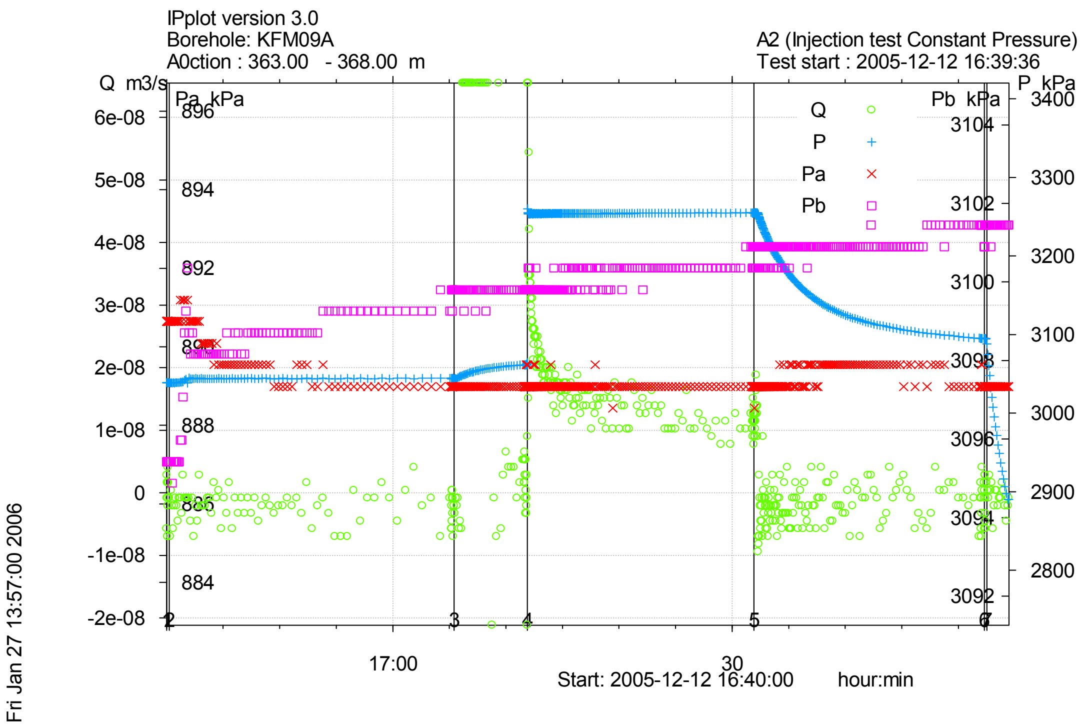


Figure A3-364. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 363.0-368.0 m in borehole KFM09A.*

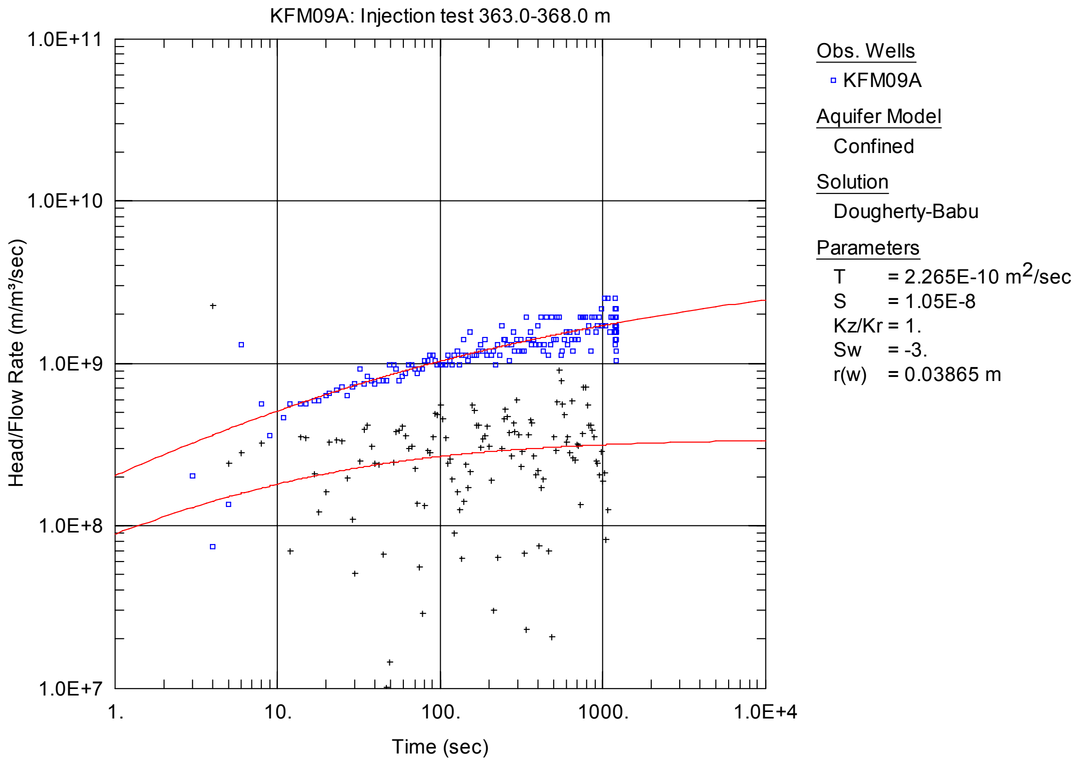


Figure A3-365. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 363.0-368.0 m in KFM09A.*

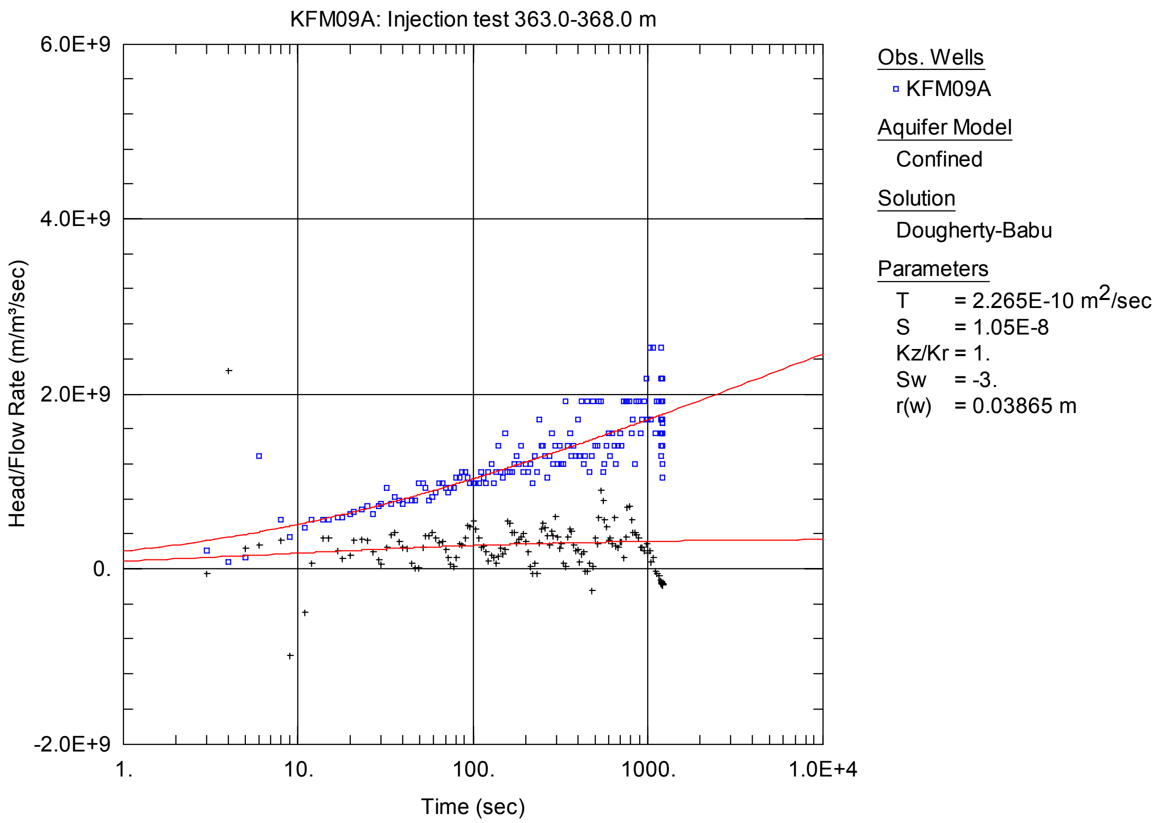


Figure A3-366. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 363.0-368.0 m in KFM09A.*

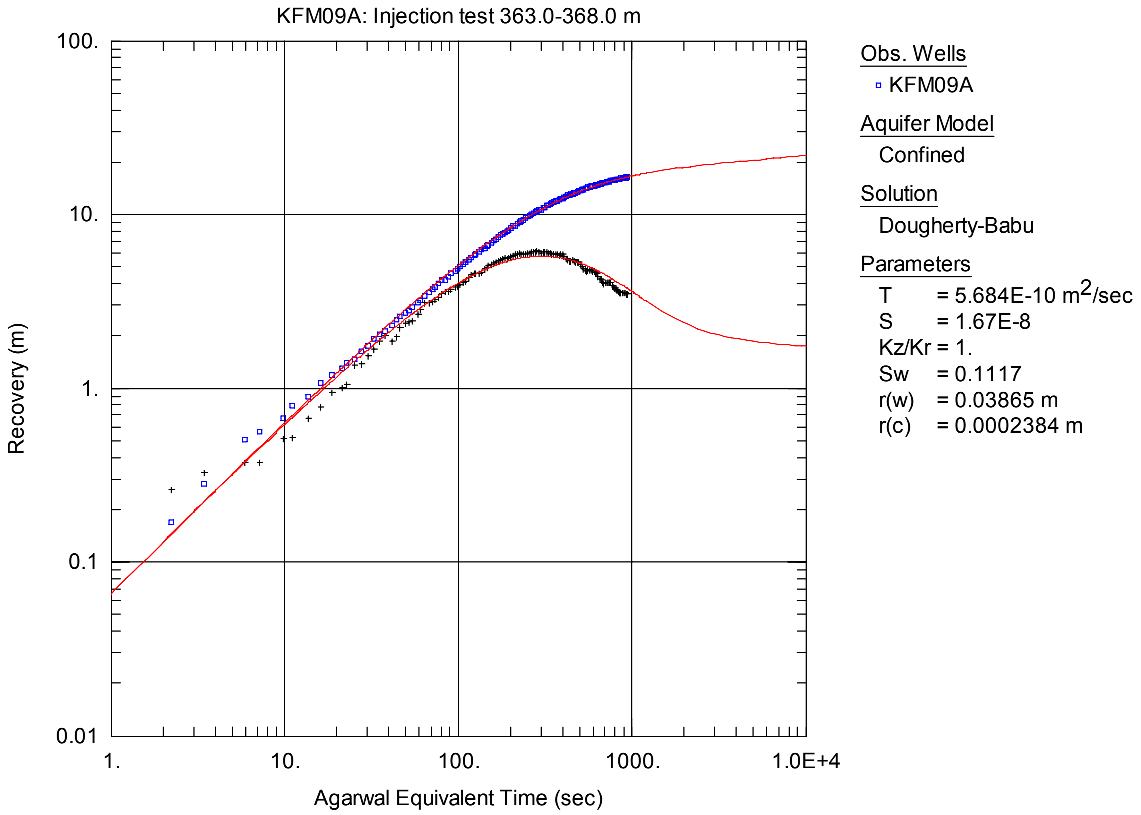


Figure A3-367. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 363.0-368.0 m in KFM09A.*

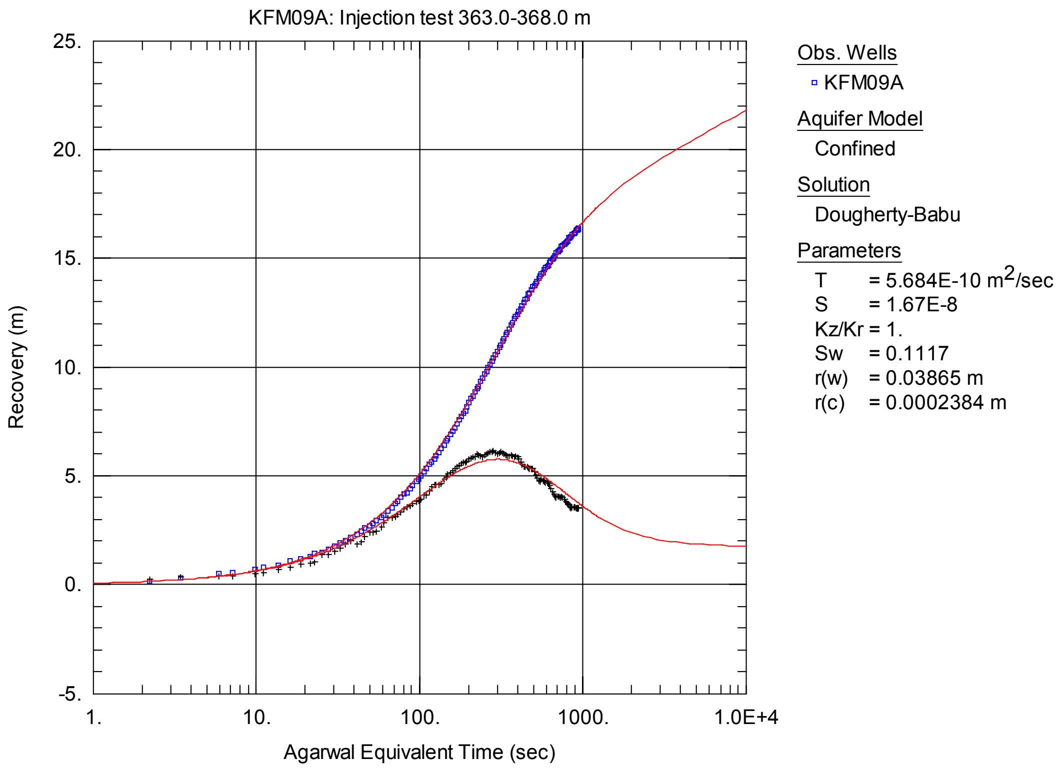


Figure A3-368. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 363.0-368.0 m in KFM09A.*

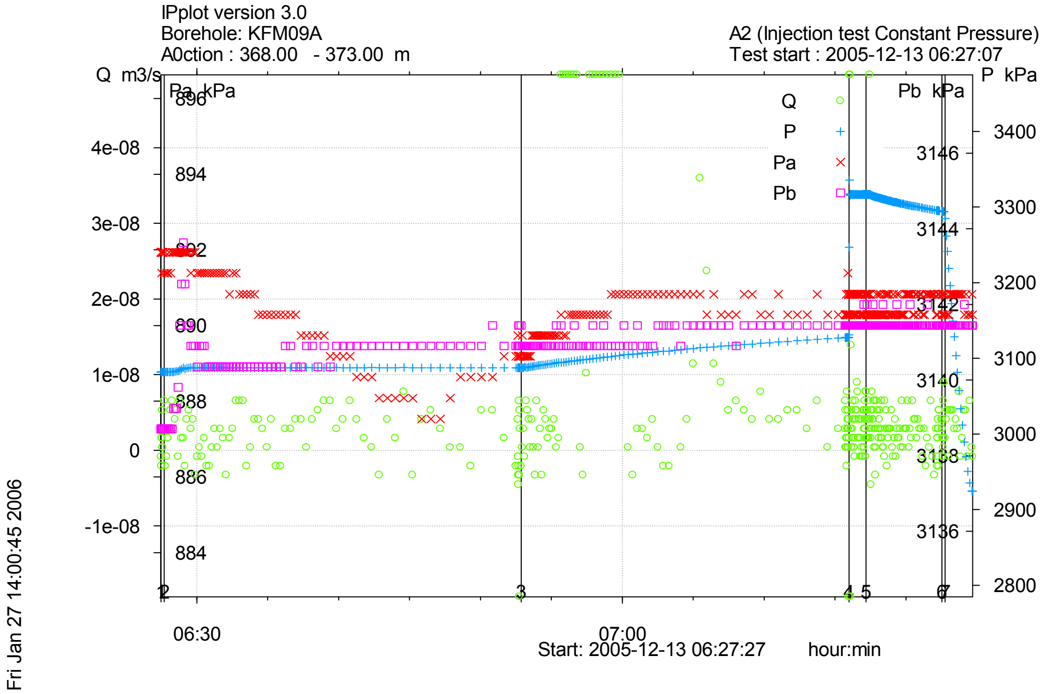


Figure A3-369. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 368.0-373.0 m in borehole KFM09A.*

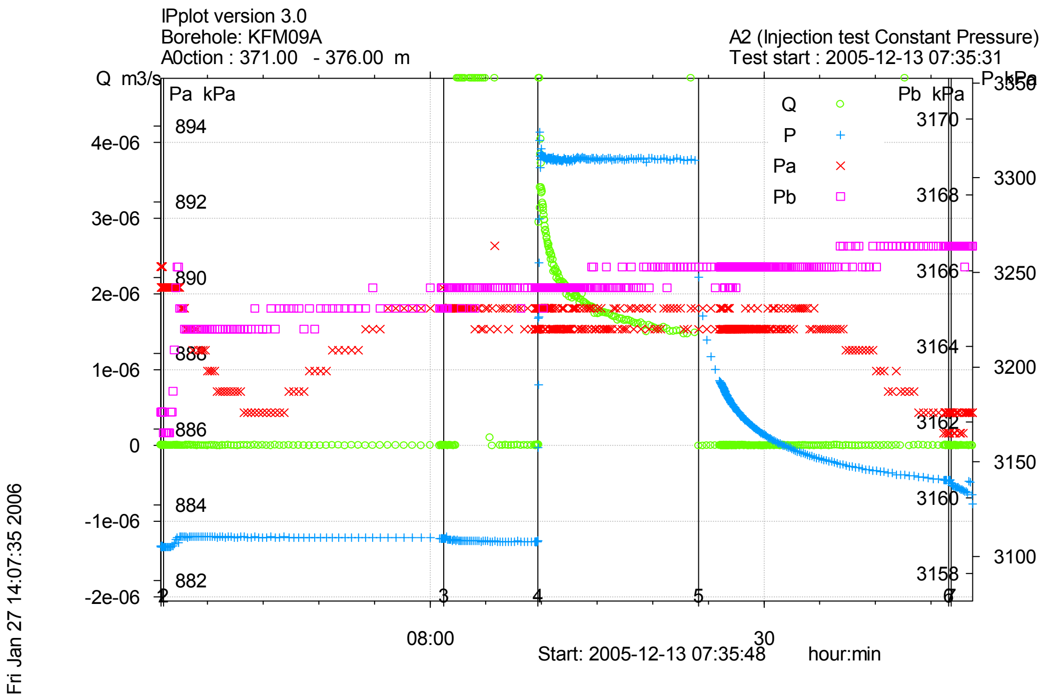


Figure A3-370. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 371.0-376.0 m in borehole KFM09A.*

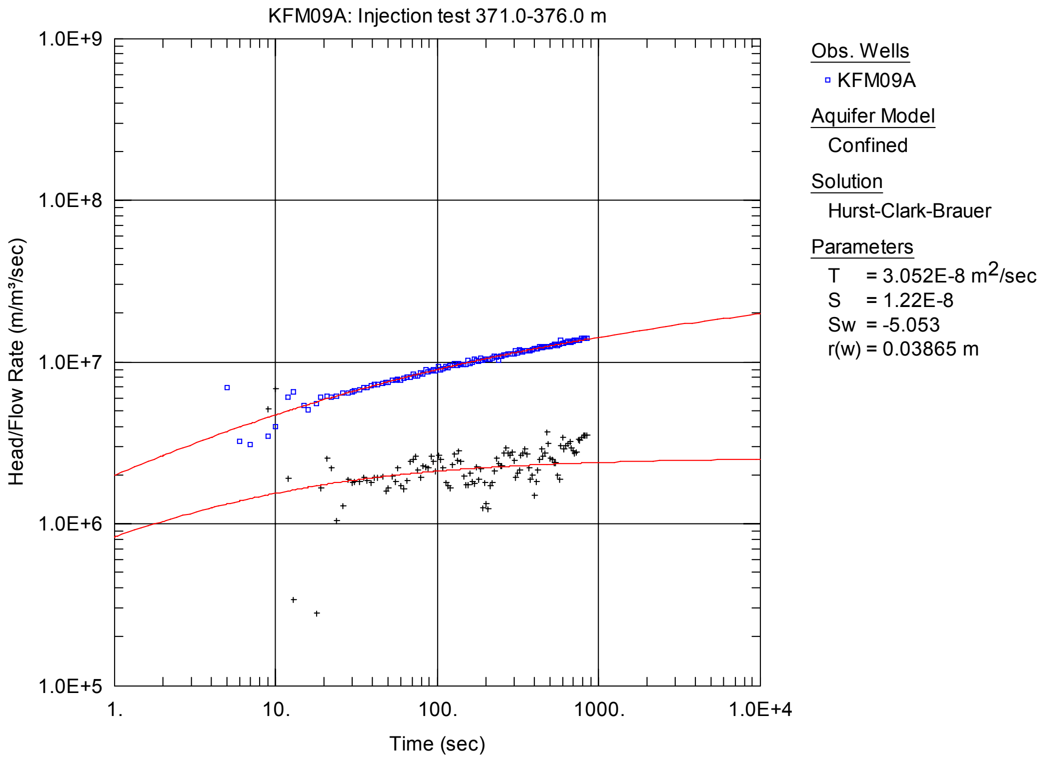


Figure A3-371. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 371.0-376.0 m in KFM09A.*

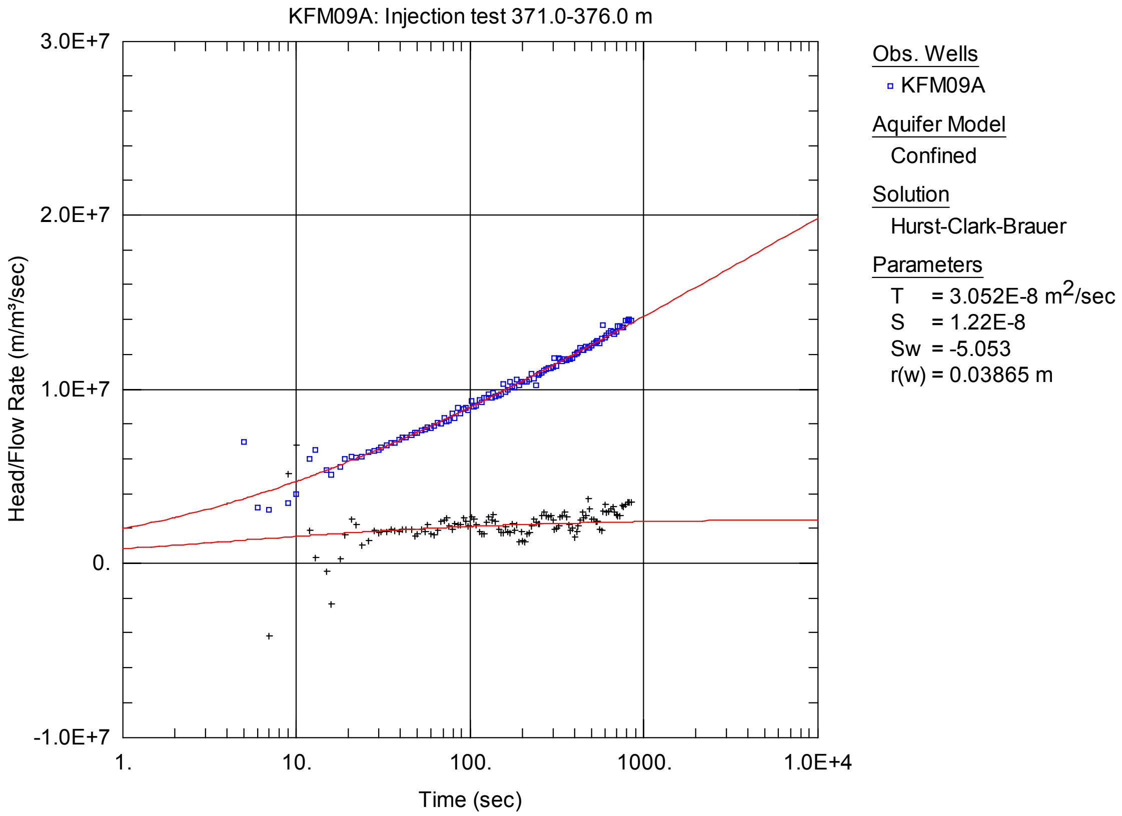


Figure A3-372. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 371.0-376.0 m in KFM09A.*

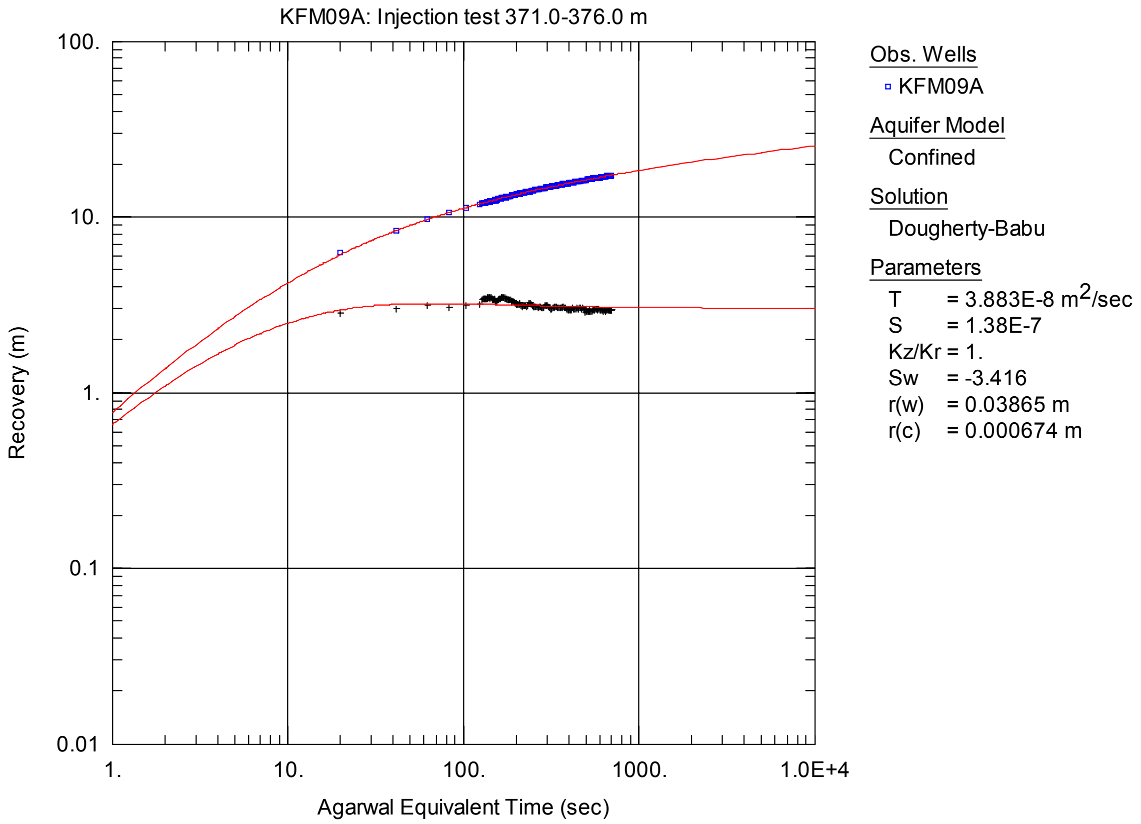


Figure A3-373. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 371.0-376.0 m in KFM09A.*

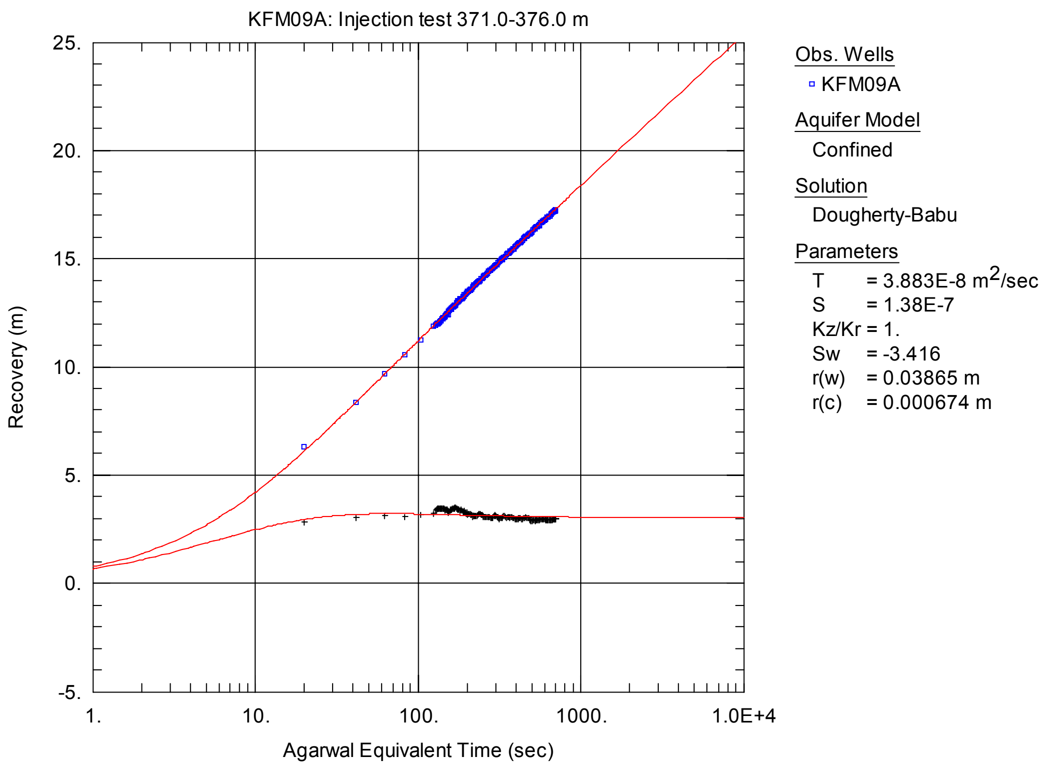


Figure A3-374. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 371.0-376.0 m in KFM09A.*

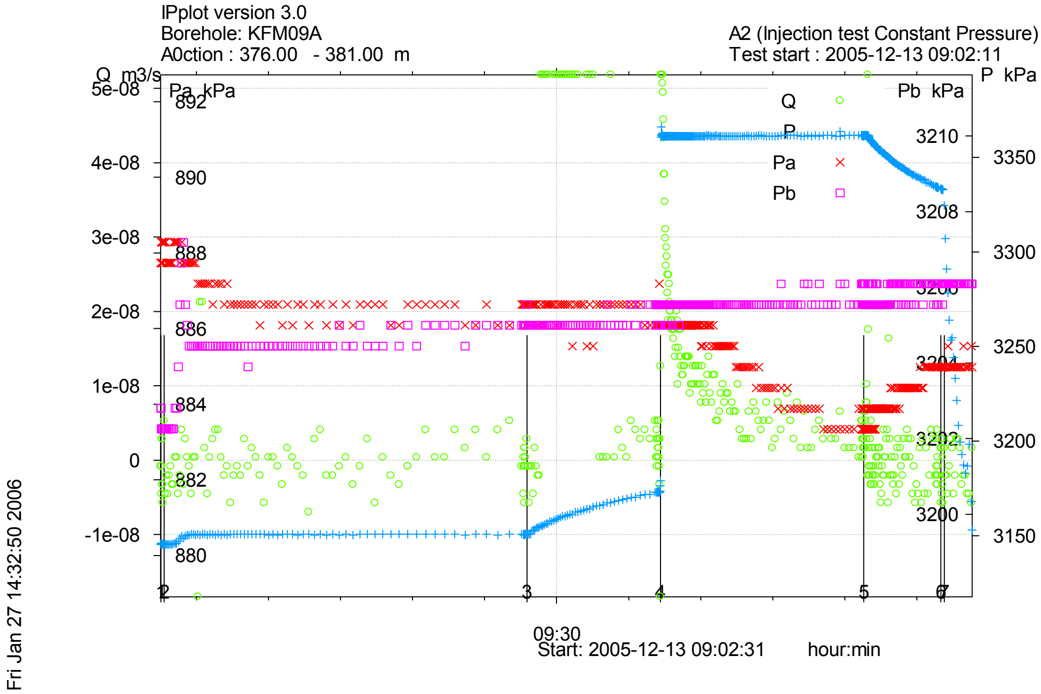


Figure A3-375. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 376.0-381.0 m in borehole KFM09A.

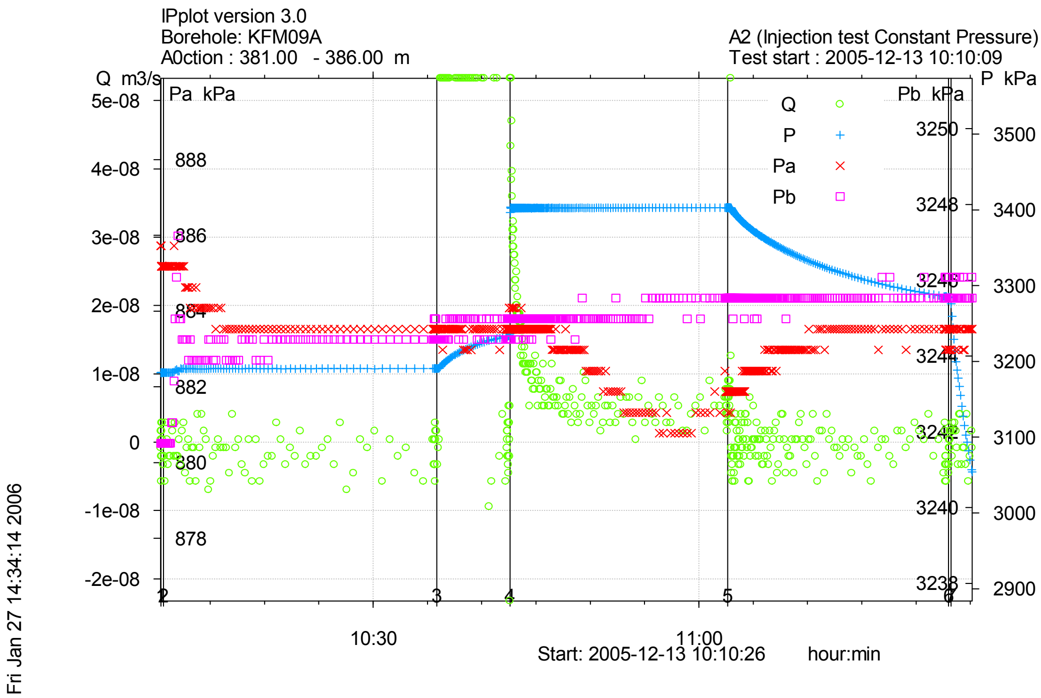


Figure A3-376. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 381.0-386.0 m in borehole KFM09A.

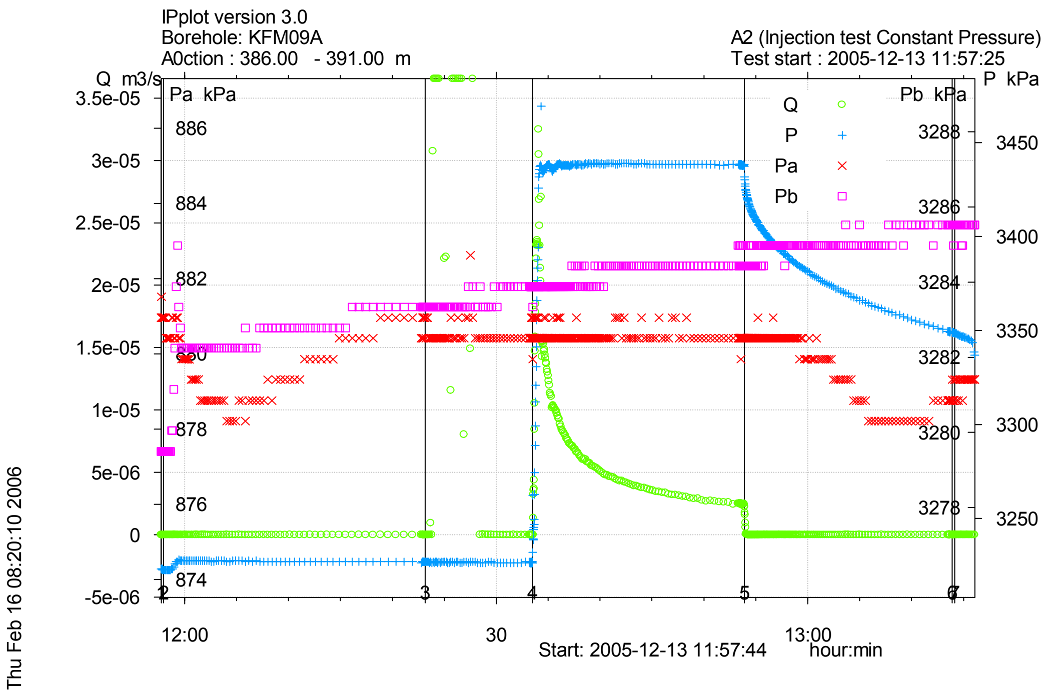


Figure A3-377. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 386.0-391.0 m in borehole KFM09A.*

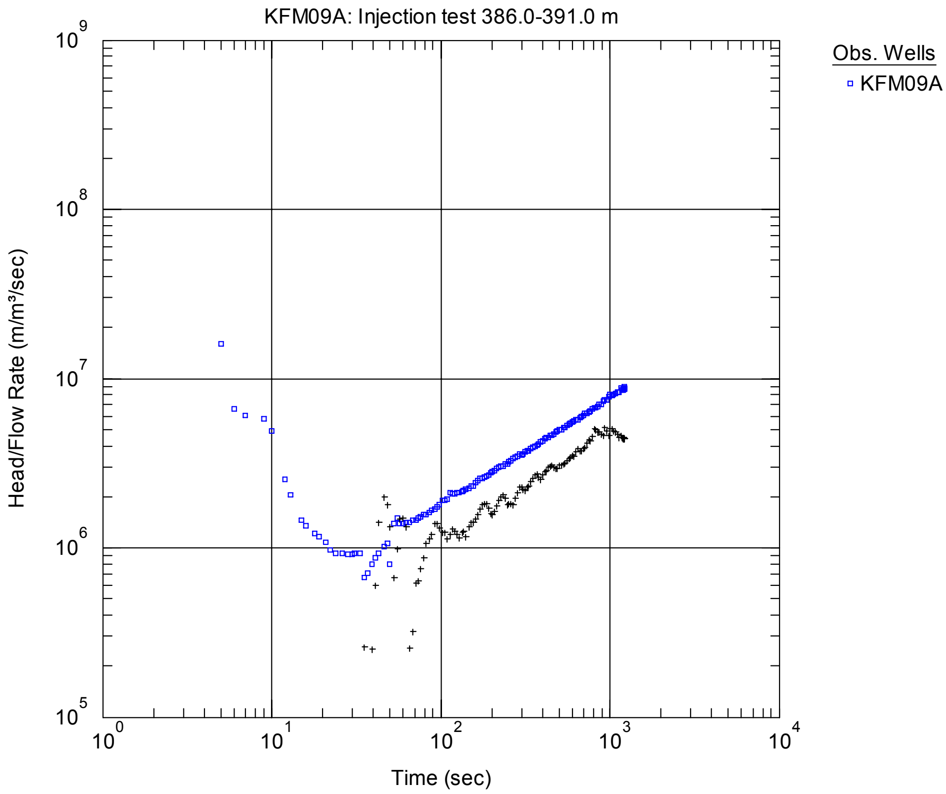


Figure A3-378. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 386.0-391.0 m in KFM09A*

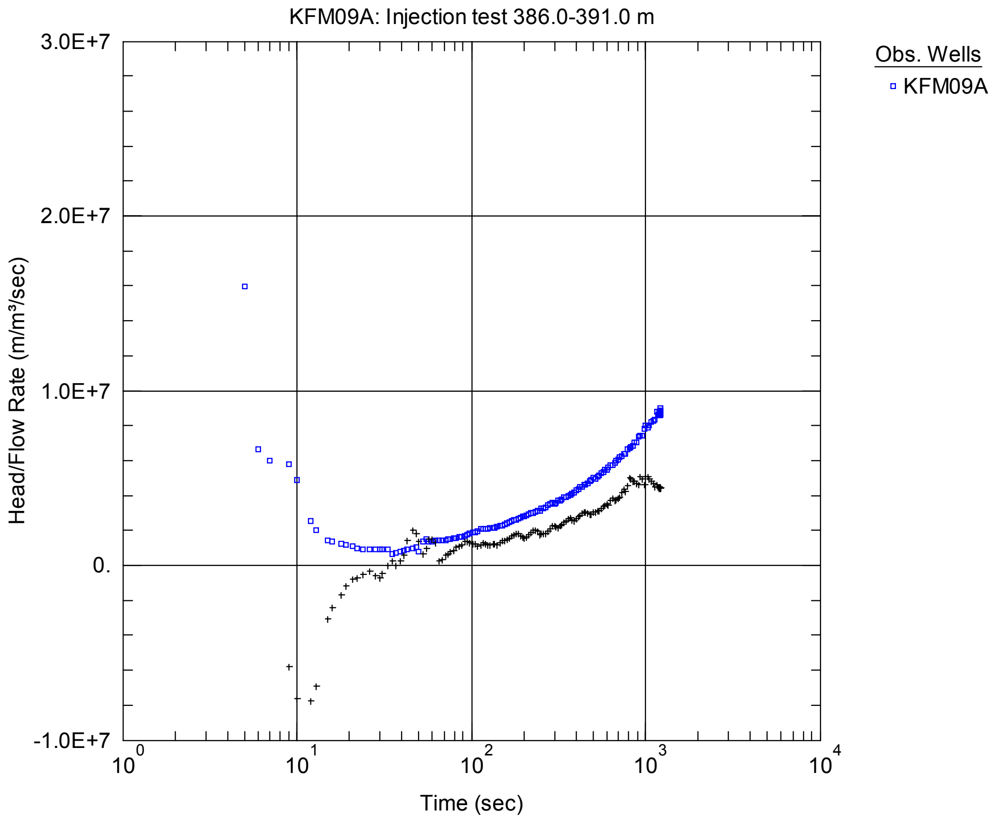


__Figure A3-379.__ Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 386.0-391.0 m in KFM09A.

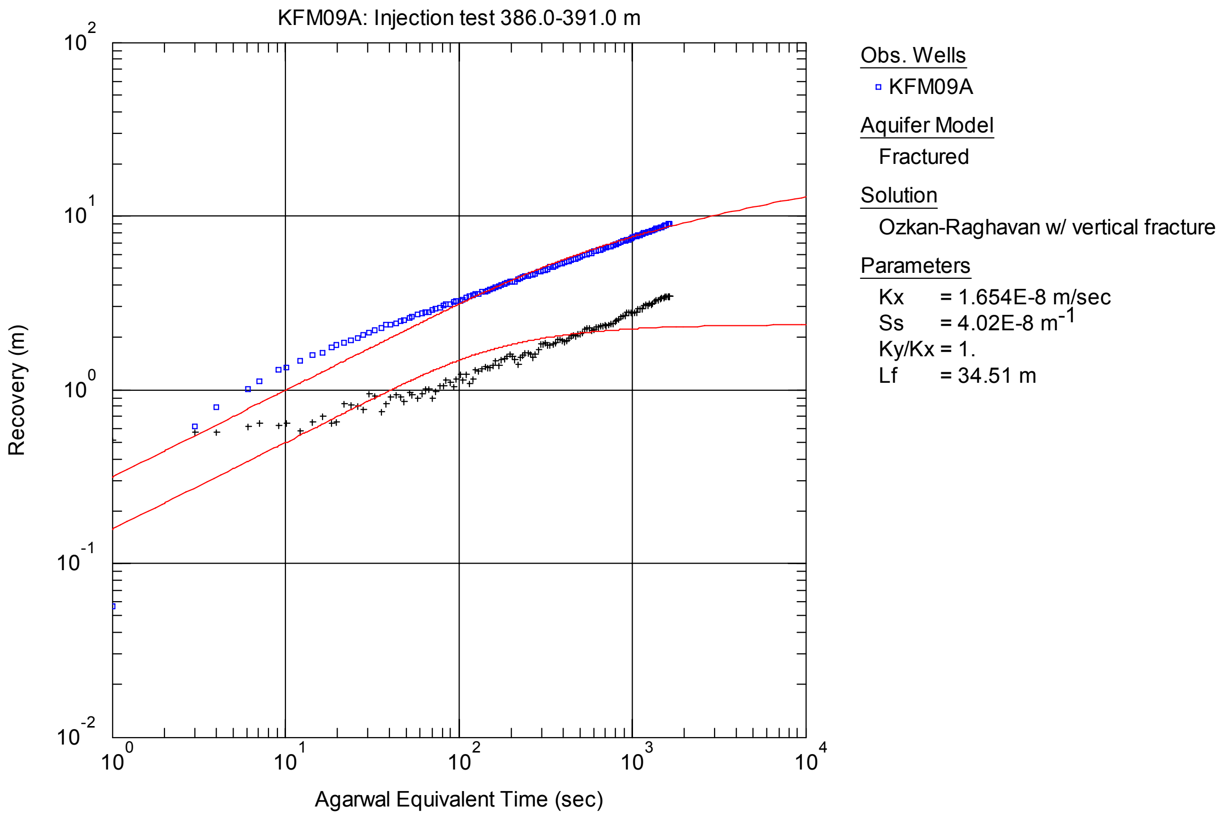


__Figure A3-380.__ Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 386.0-391.0 m in KFM09A.

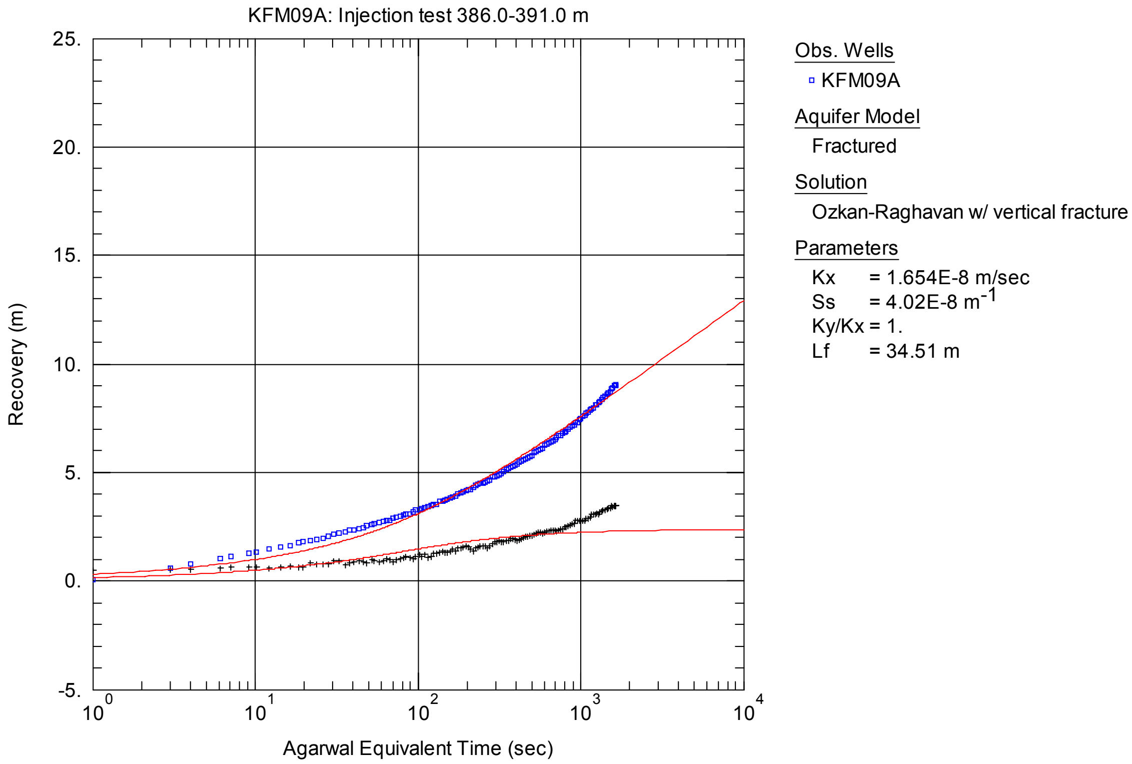


__Figure A3-381.__ Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 386.0-391.0 m in KFM09A.

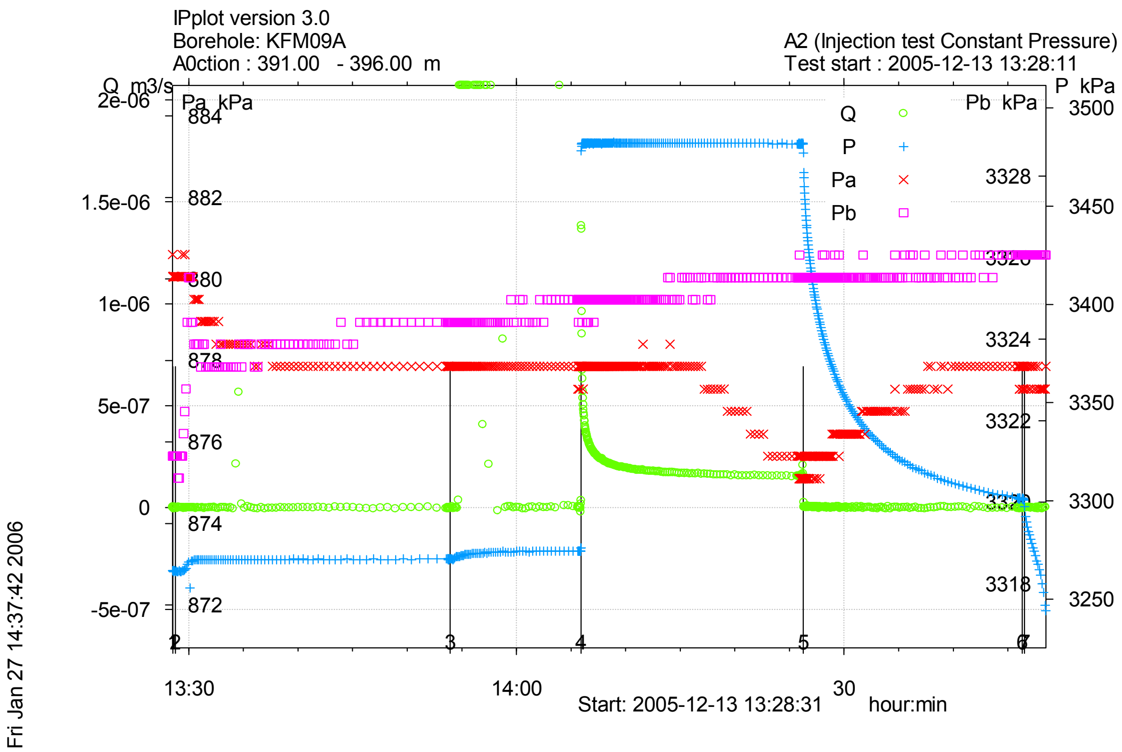


__Figure A3-382.__ Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 391.0-396.0 m in borehole KFM09A.

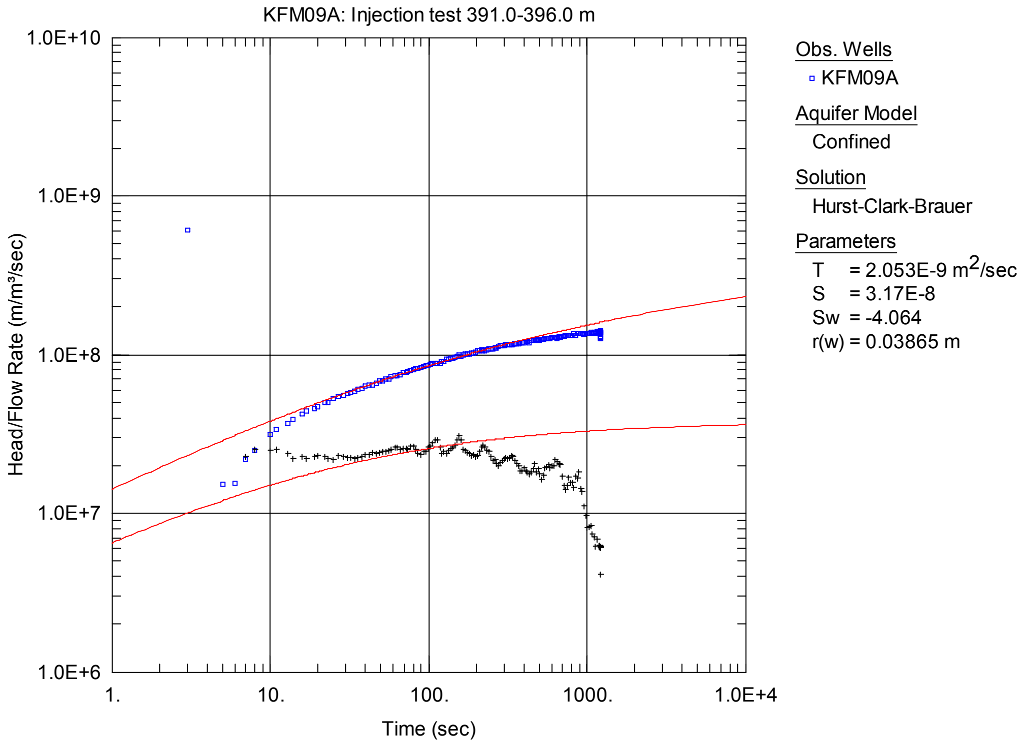


Figure A3-383. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 391.0-396.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for a pseudo-radial response.*

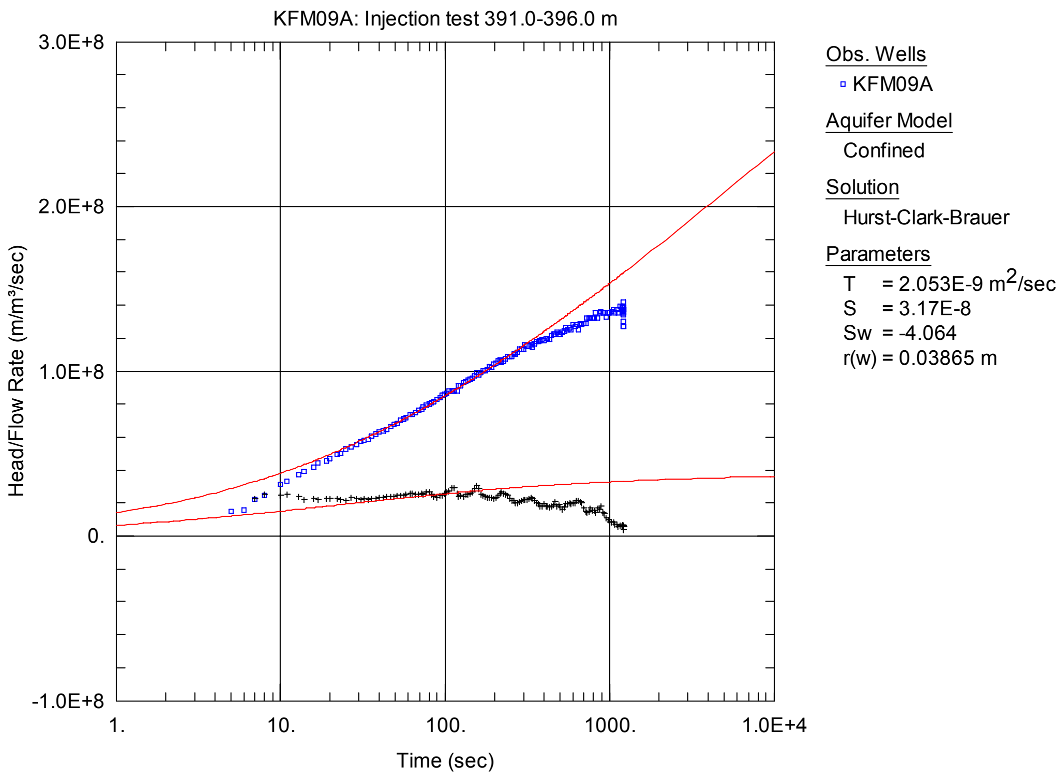


Figure A3-384. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 391.0-396.0 m in KFM09A This evaluation is made with the Hurst-Clark-Brauer model for a pseudo-radial response.*

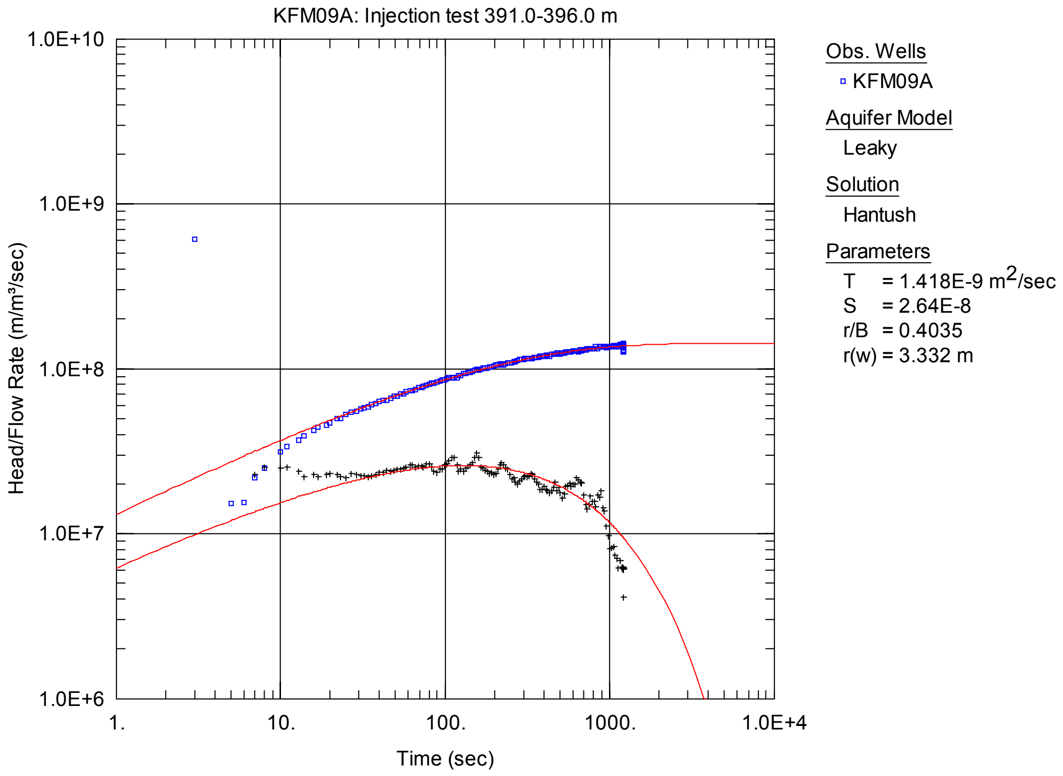


Figure A3-385. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 391.0-396.0 m in KFM09A This evaluation is made with the Hantush model for a pseudo-spherical response.*

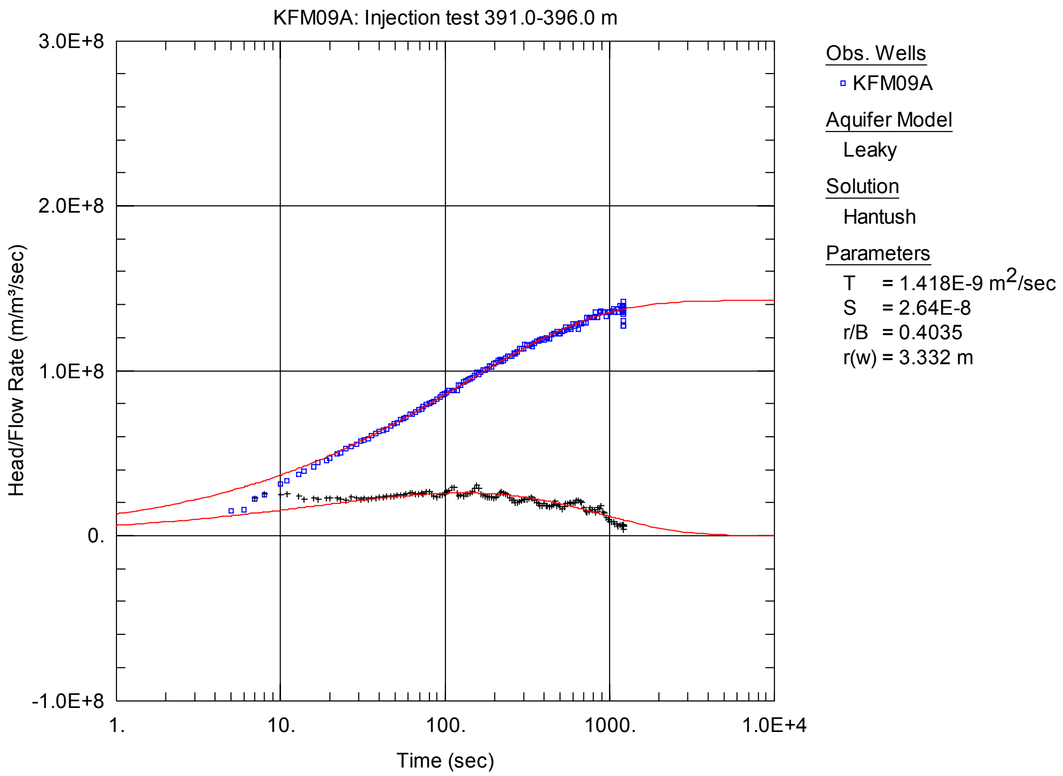


Figure A3-386. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 391.0-396.0 m in KFM09A This evaluation is made with the Hantush model for a pseudo-spherical response.*

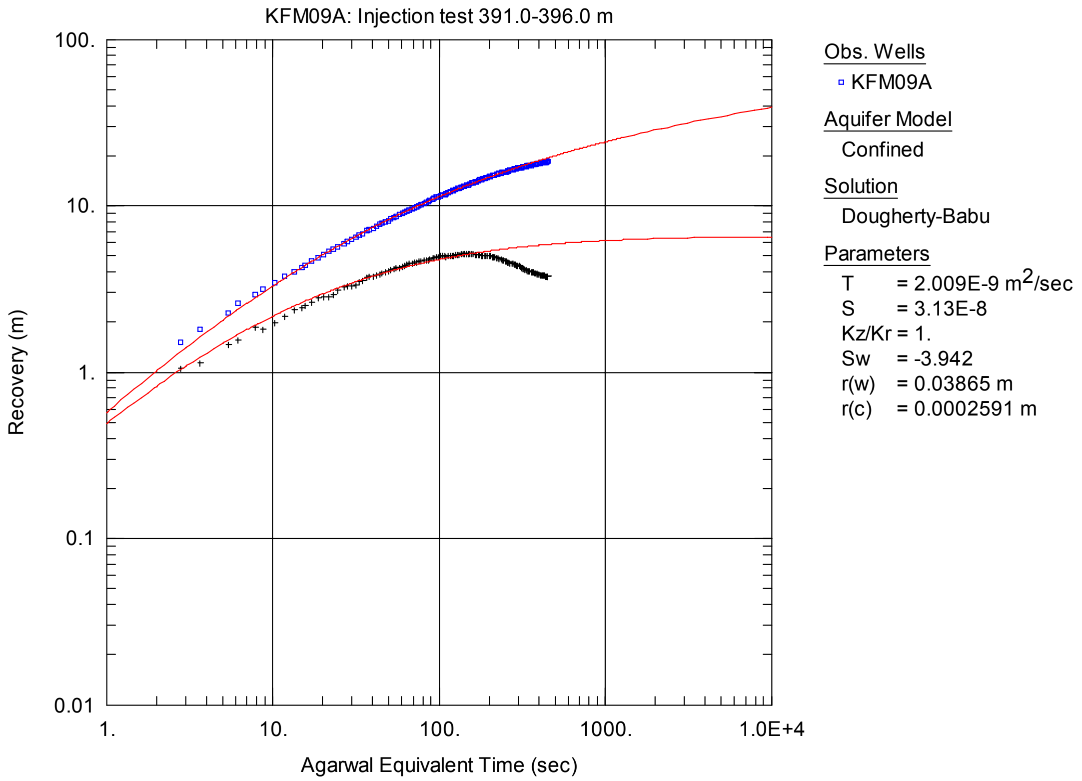


Figure A3-387. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 391.0-396.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

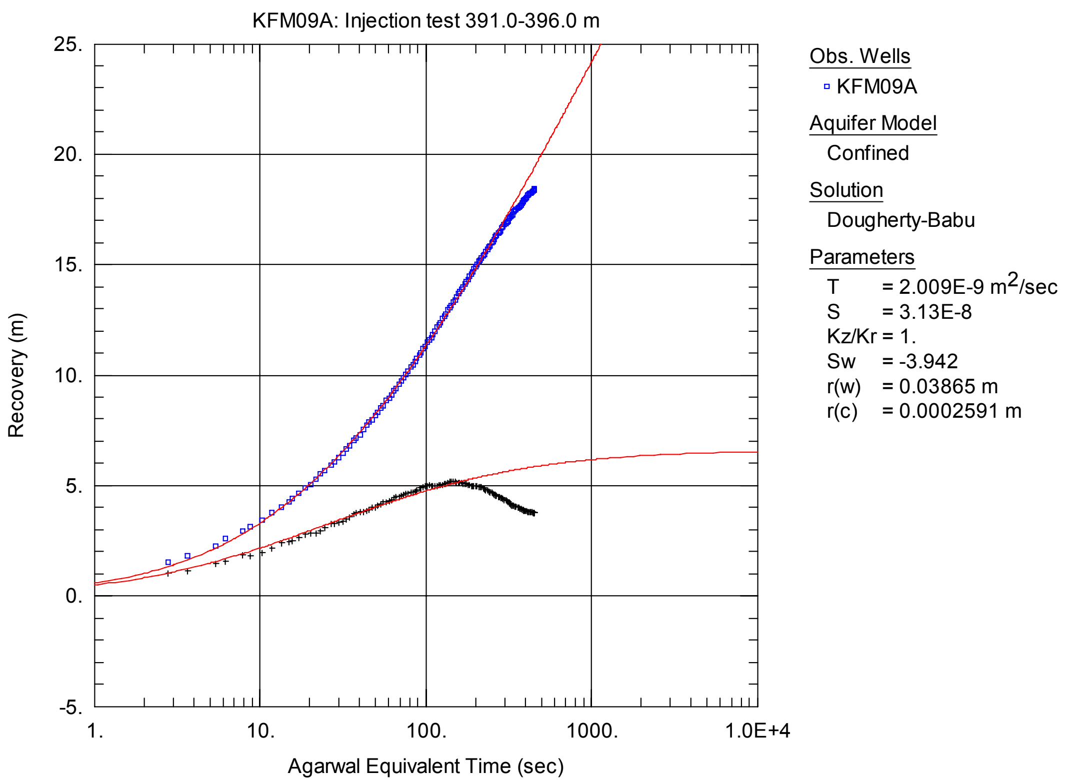


Figure A3-388. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 391.0-396.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

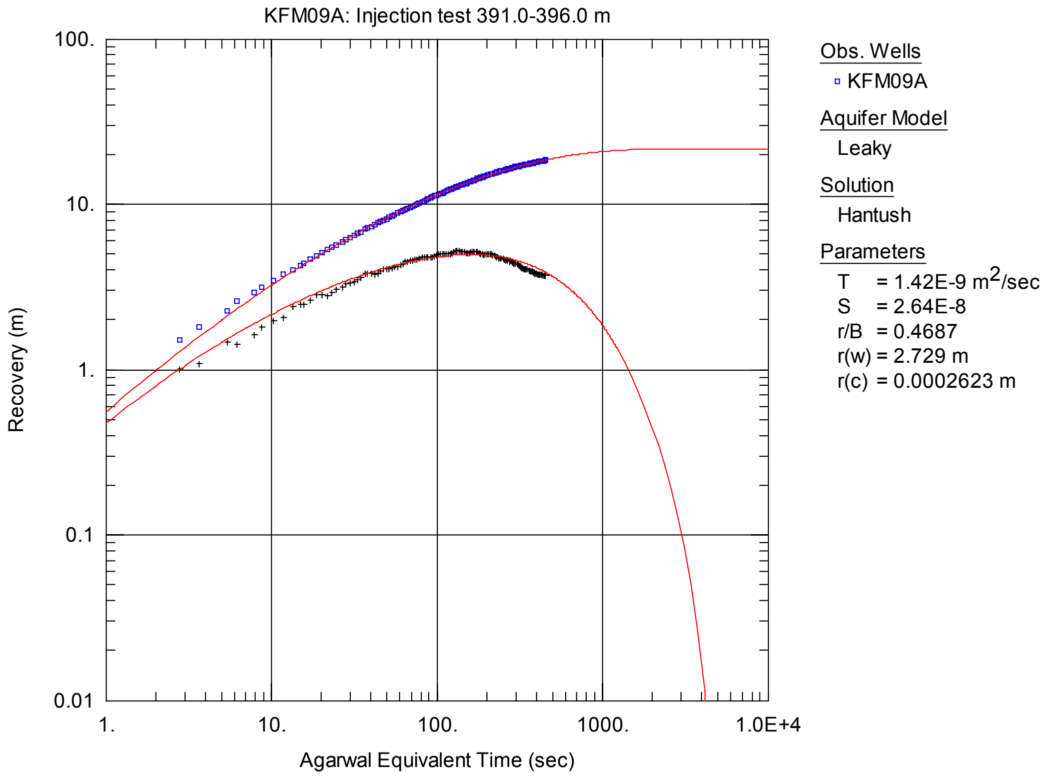


Figure A3-389. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 391.0-396.0 m in KFM09A. This evaluation is made with the Hantush model for a pseudo-spherical response.*

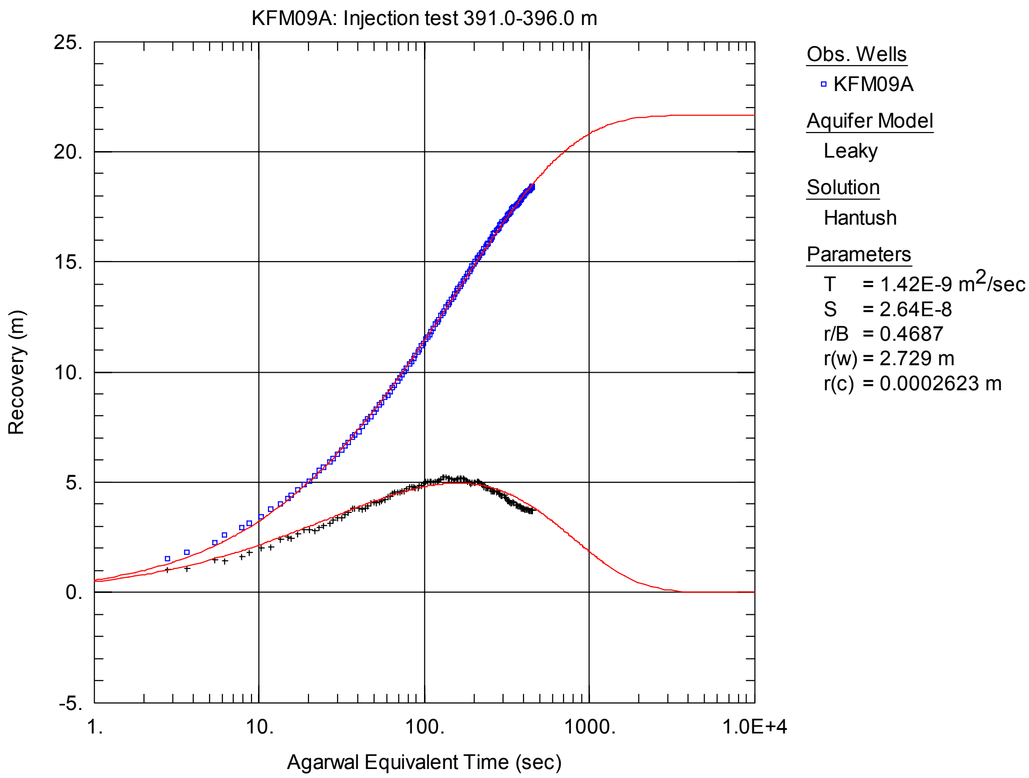


Figure A3-390. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 391.0-396.0 m in KFM09A. This evaluation is made with the Hantush model for a pseudo-spherical response.*

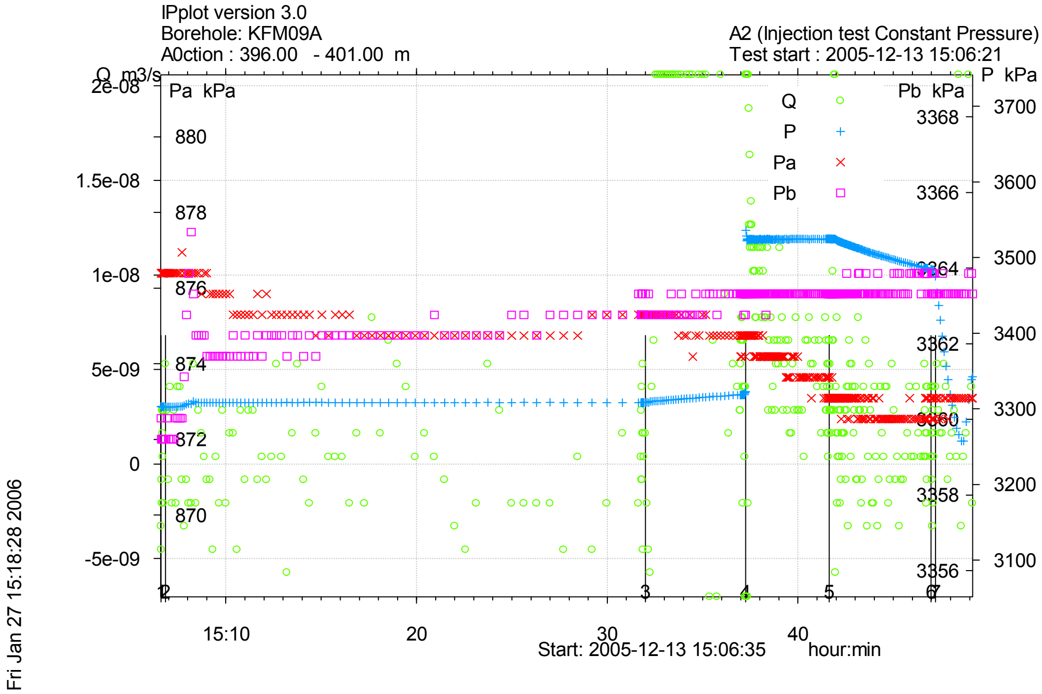


Figure A3-391. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 396.0-401.0 m in borehole KFM09A.

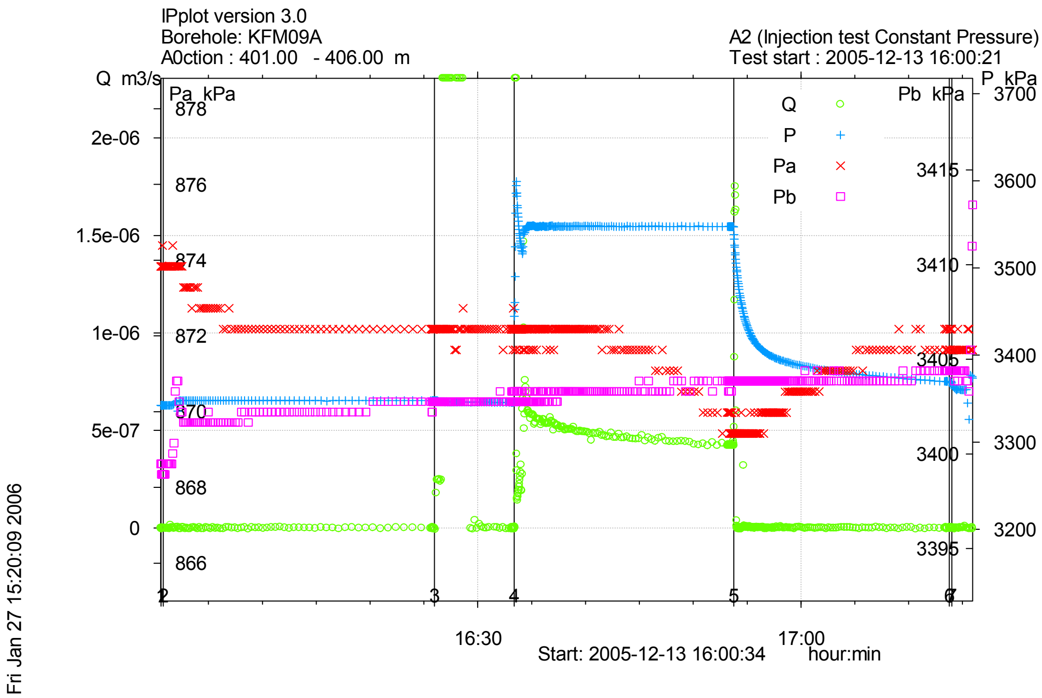


Figure A3-392. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 401.0-406.0 m in borehole KFM09A.

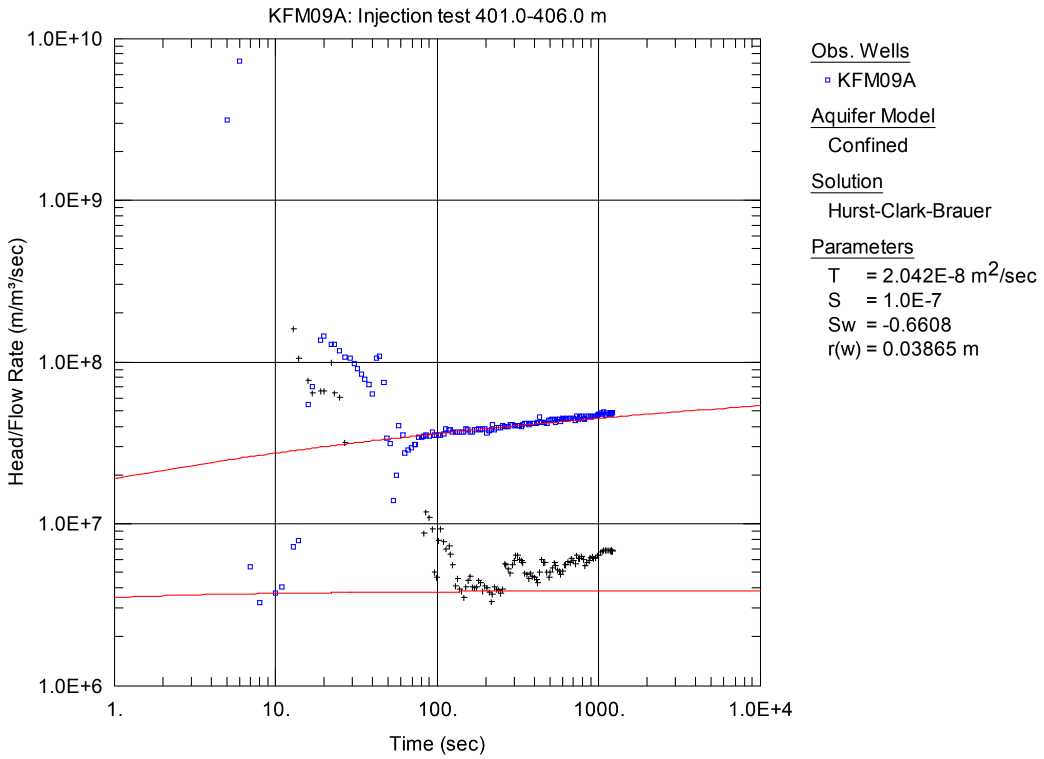


Figure A3-393. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 401.0-406.0 m in KFM09A.*

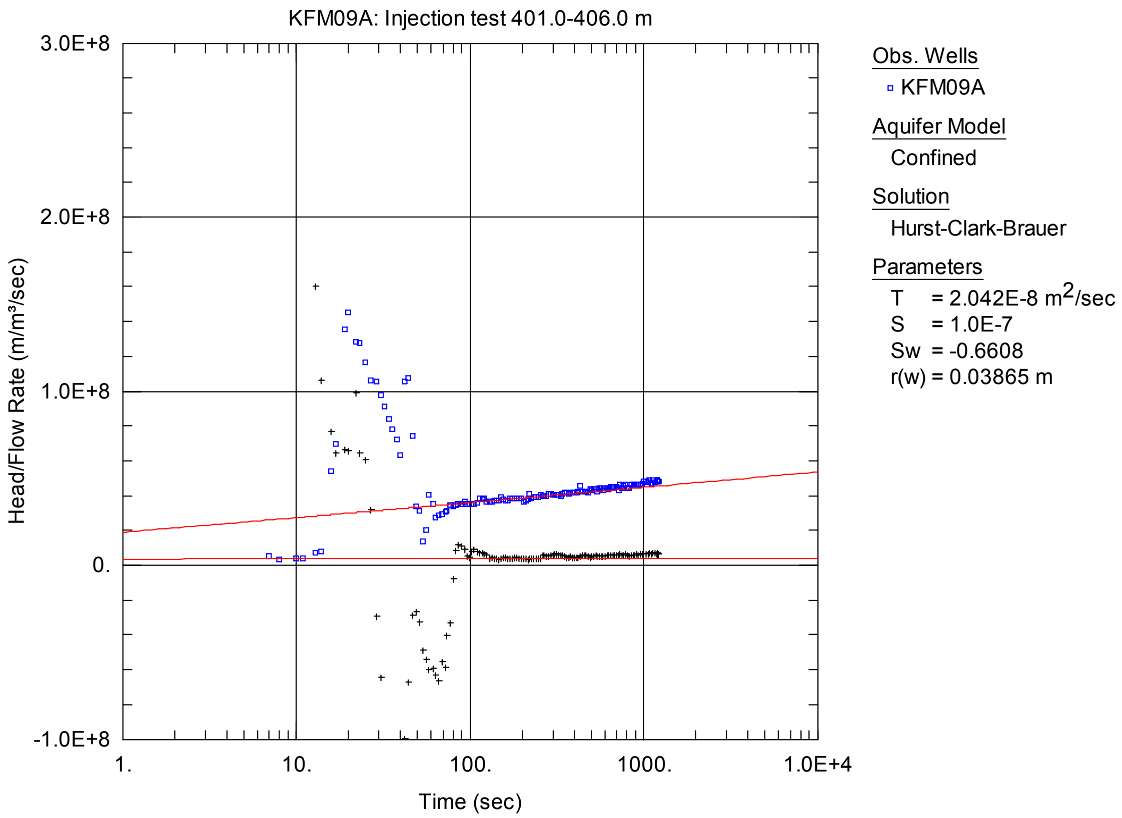


Figure A3-394. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 401.0-406.0 m in KFM09A.*

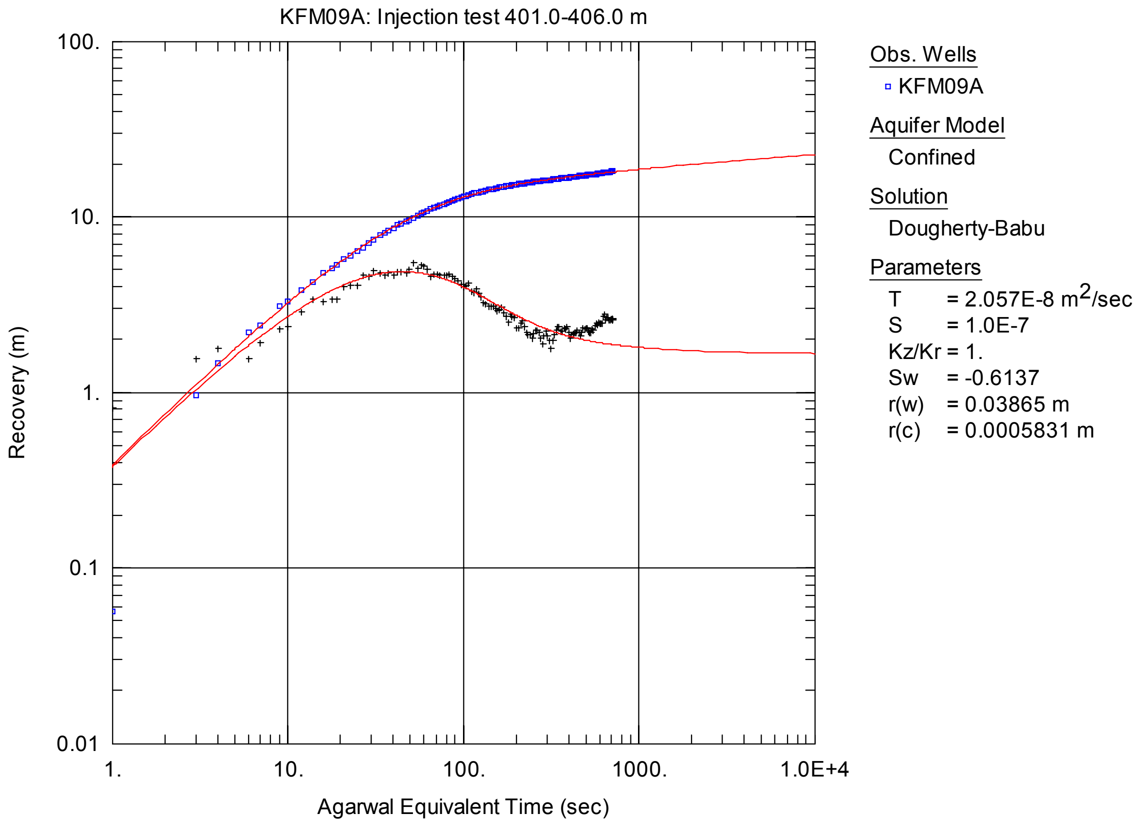


Figure A3-395. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 401.0-406.0 m in KFM09A.*

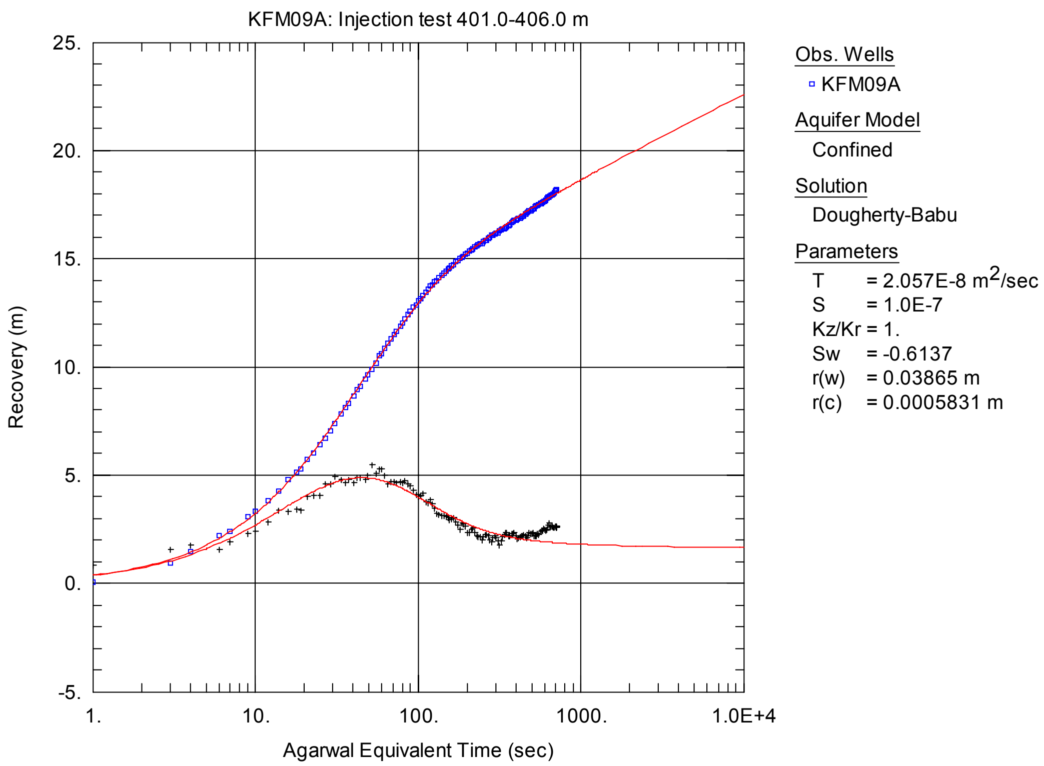


Figure A3-396. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 401.0-406.0 m in KFM09A.*

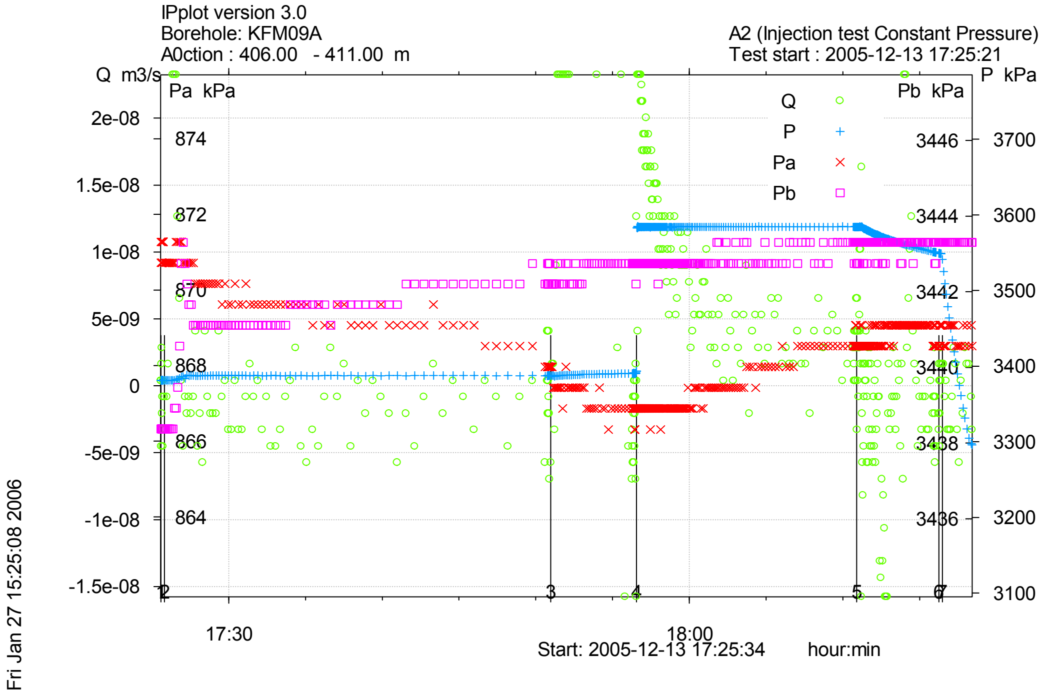


Figure A3-397. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 406.0-411.0 m in borehole KFM09A.*

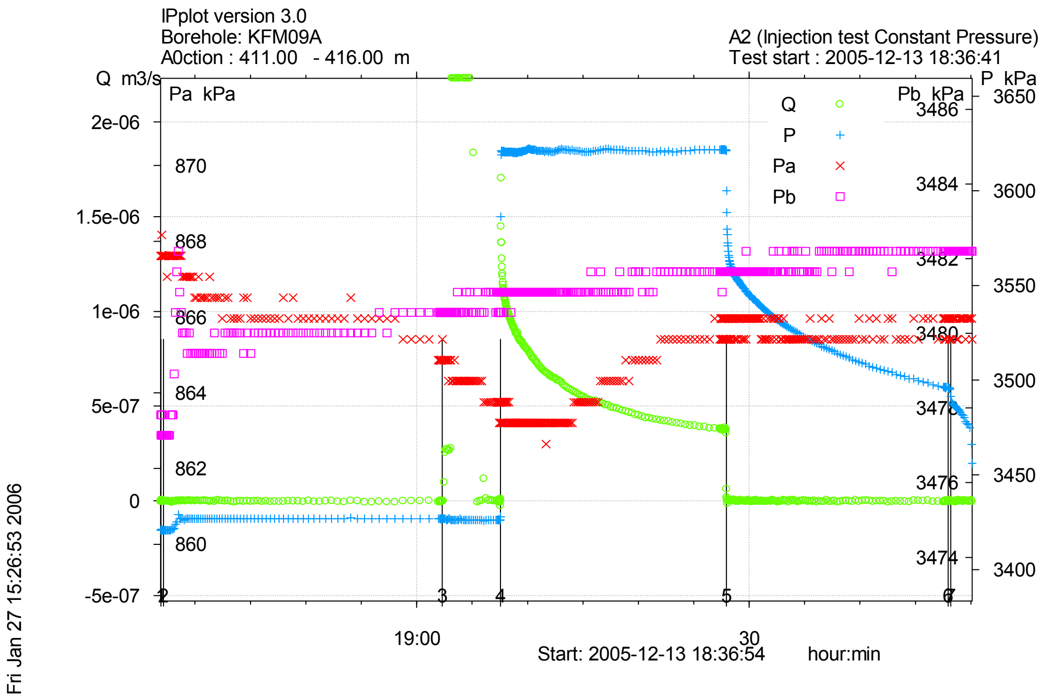


Figure A3-398. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 411.0-416.0 m in borehole KFM09A.*

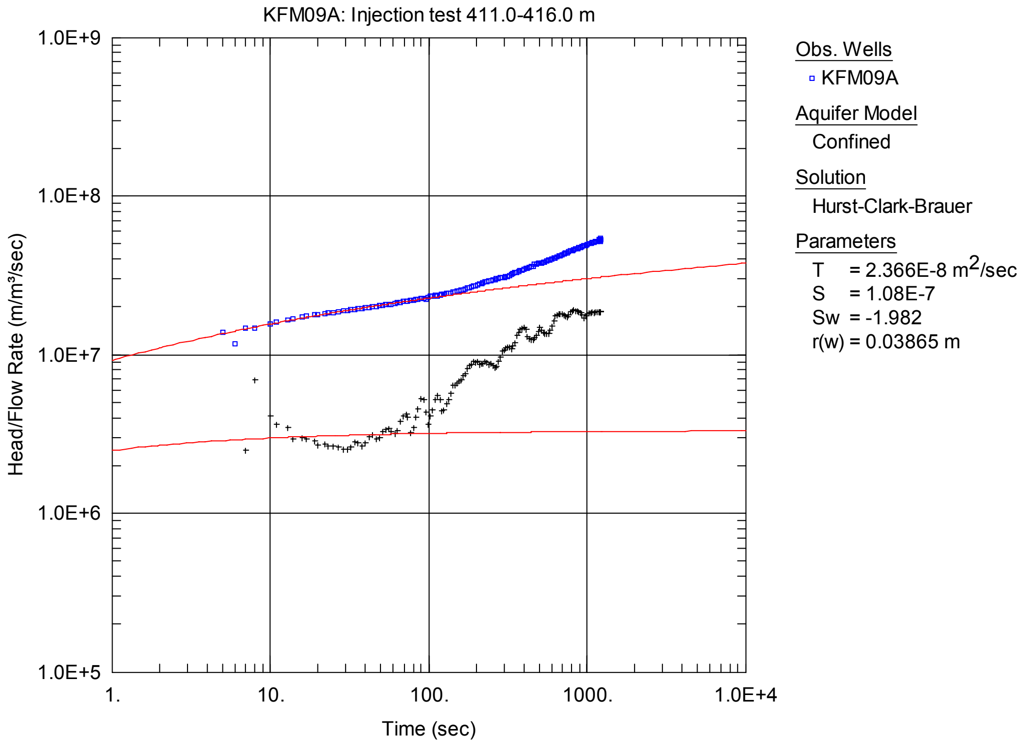


***Figure A3-399.** Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 411.0-416.0 m in KFM09A. This plot shows a fit to the first of two different PRF:s during the injection period in this section.*

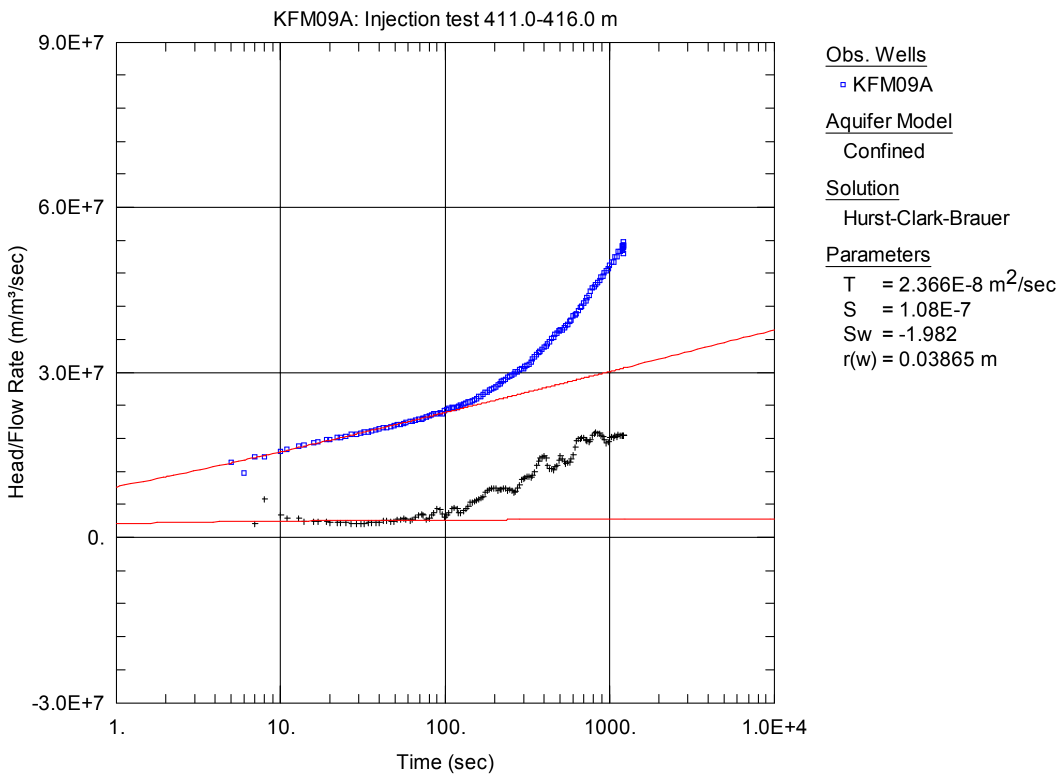


***Figure A3-400.** Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 411.0-416.0 m in KFM09A. This plot shows a fit to the first of two different PRF:s during the injection period in this section.*

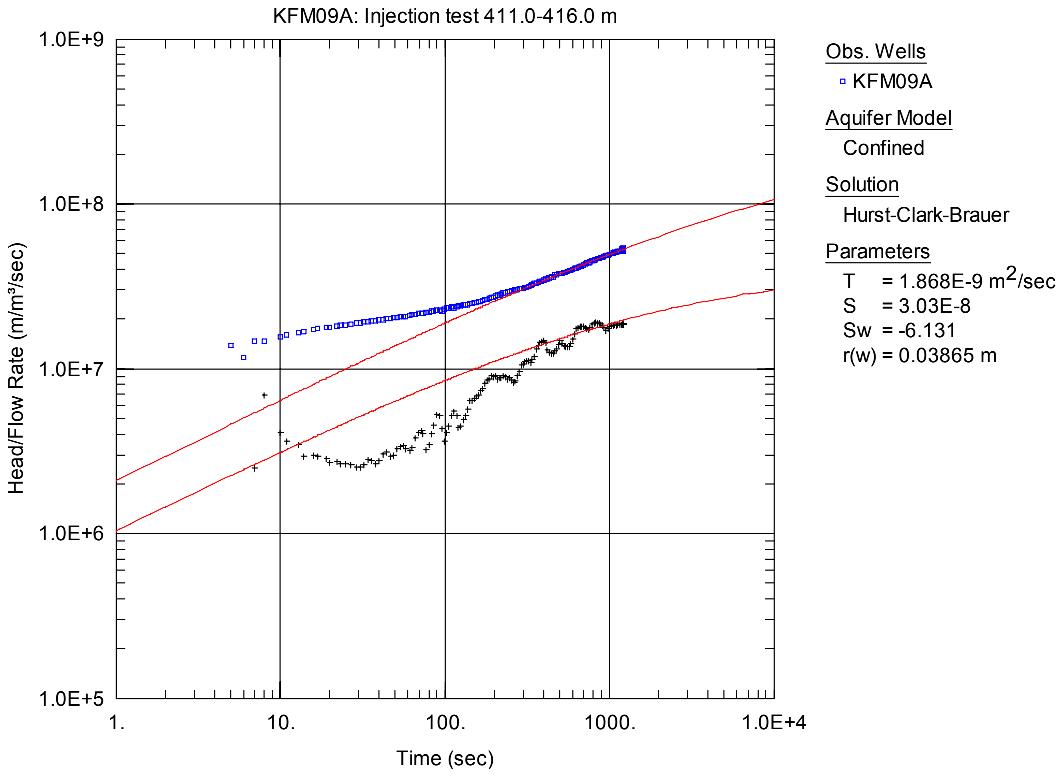


Figure A3-401. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 411.0-416.0 m in KFM09A. This plot shows a fit to the second of two different PRF:s during the injection period in this section.*

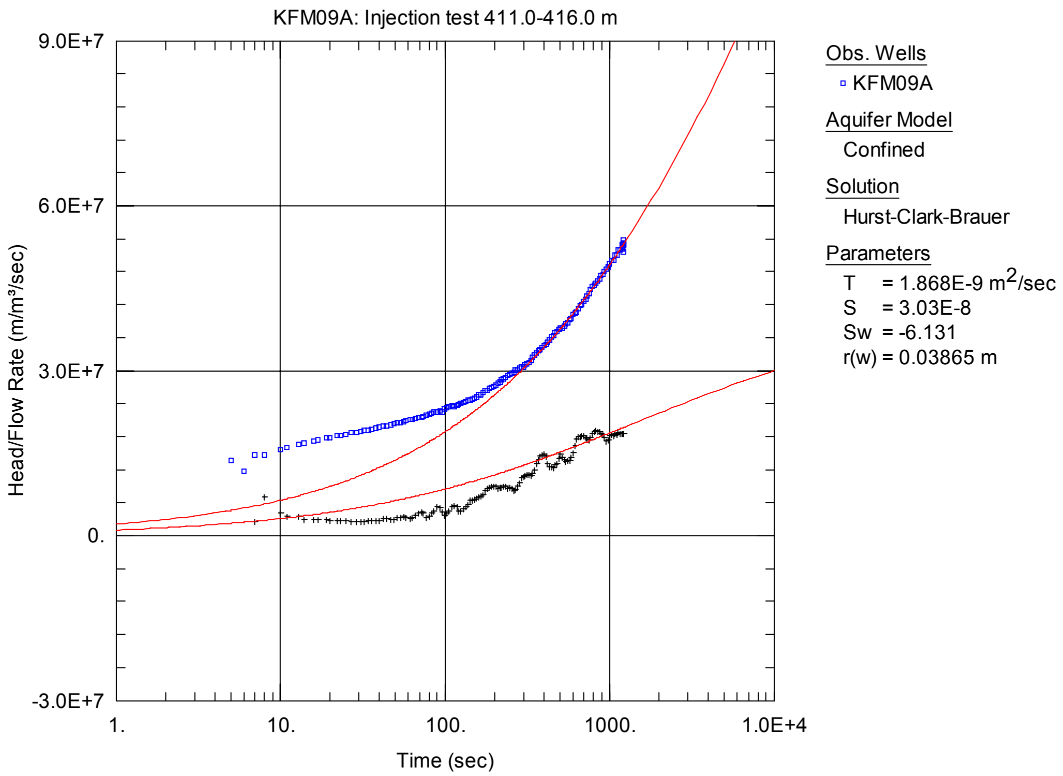


Figure A3-402. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 411.0-416.0 m in KFM09A. This plot shows a fit to the second of two different PRF:s during the injection period in this section.*

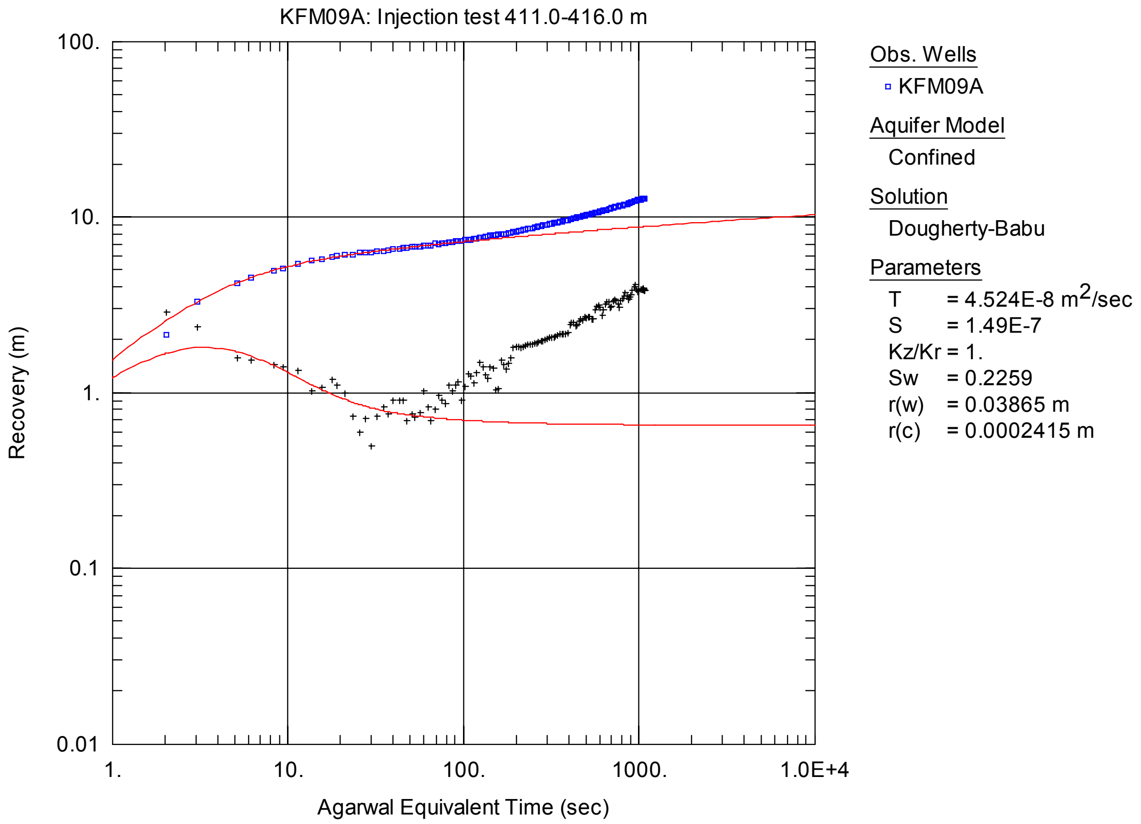


Figure A3-403. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 411.0-416.0 x m in KFM09A.*

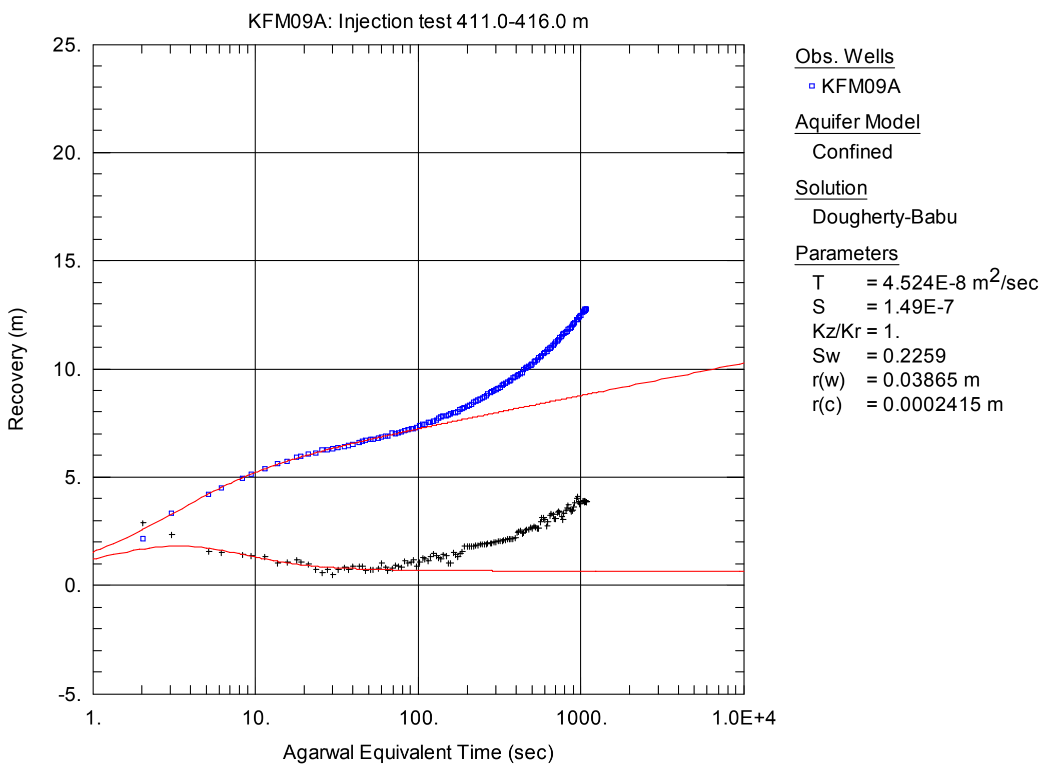


Figure A3-404. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 411.0-416.0 m in KFM09A.*

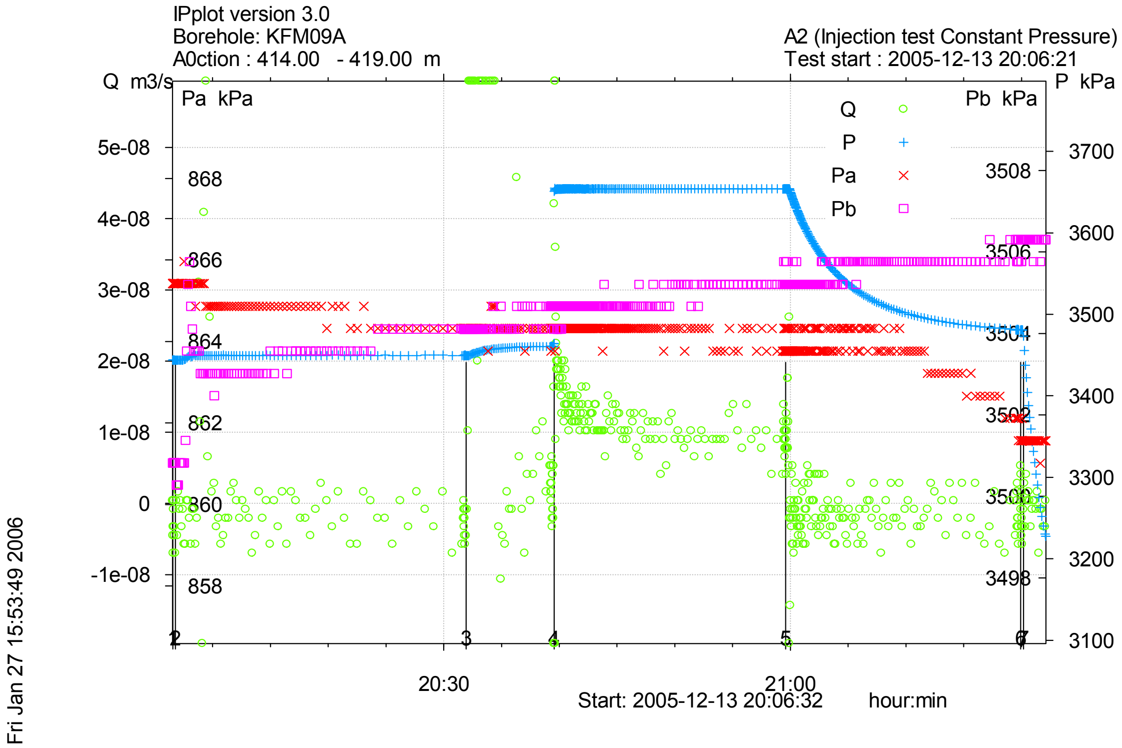


Figure A3-405. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 414.0-419.0 m in borehole KFM09A.

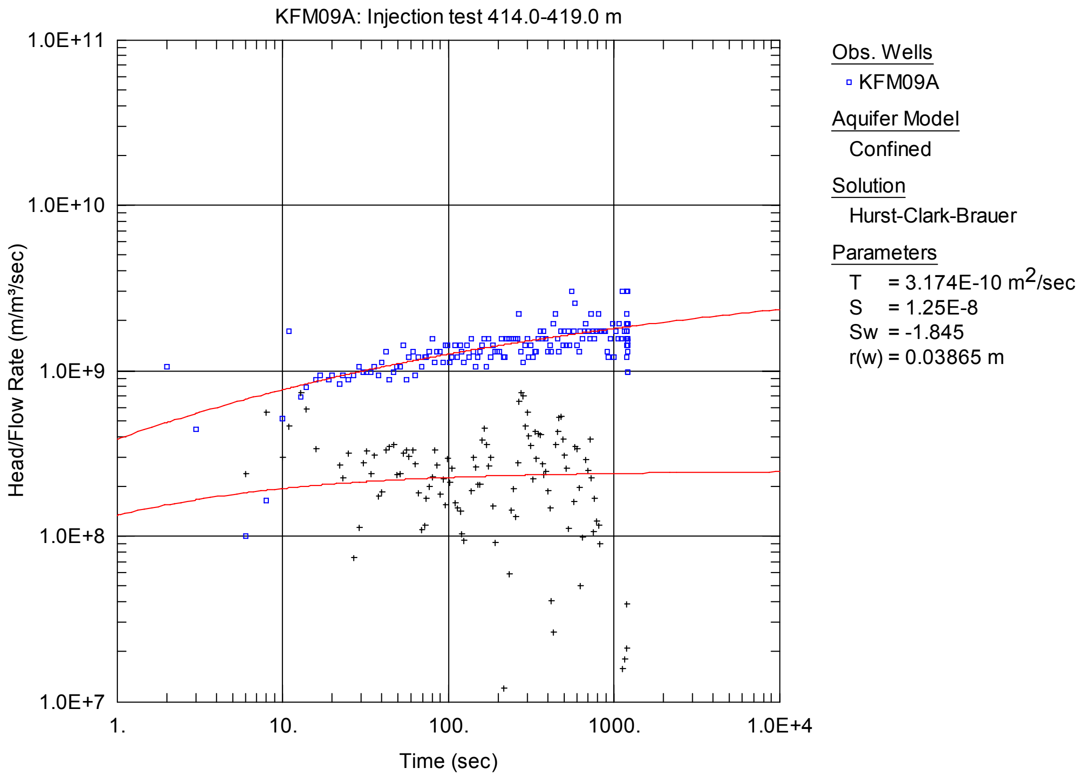


Figure A3-406. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 414.0-419.0 m in KFM09A.

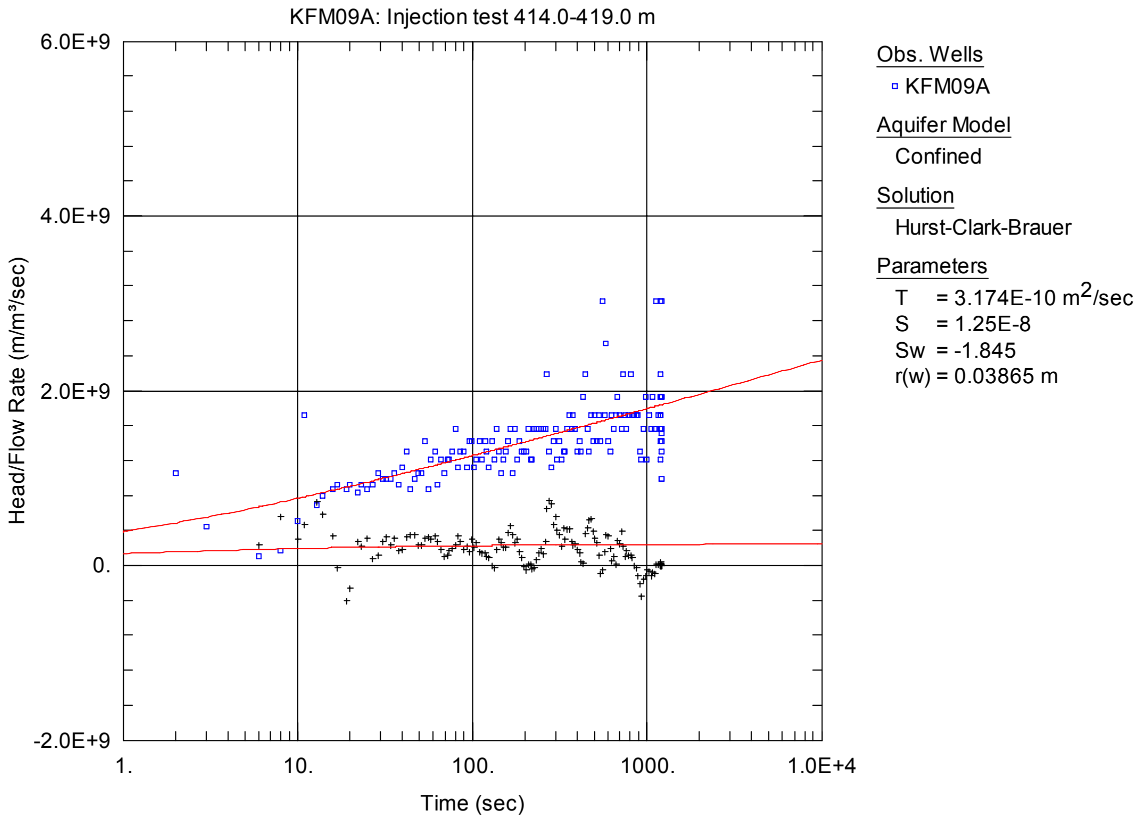


***Figure A3-407.** Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 414.0-419.0 m in KFM09A.*

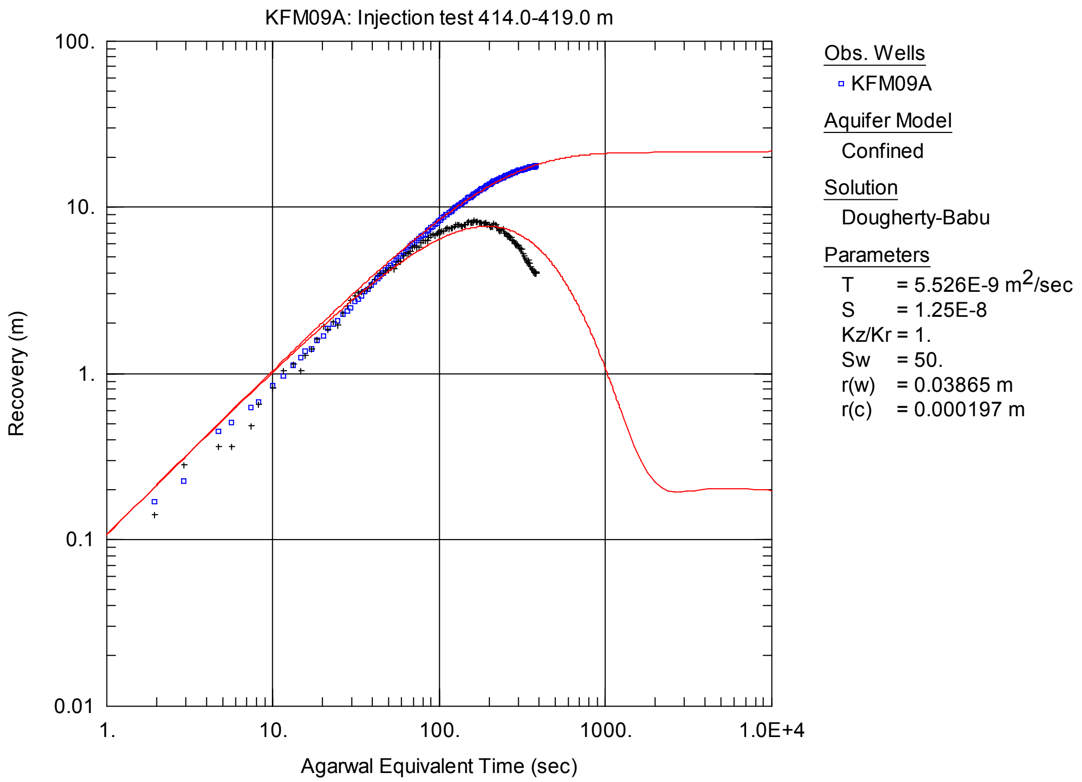


***Figure A3-408.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 414.0-419.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.*

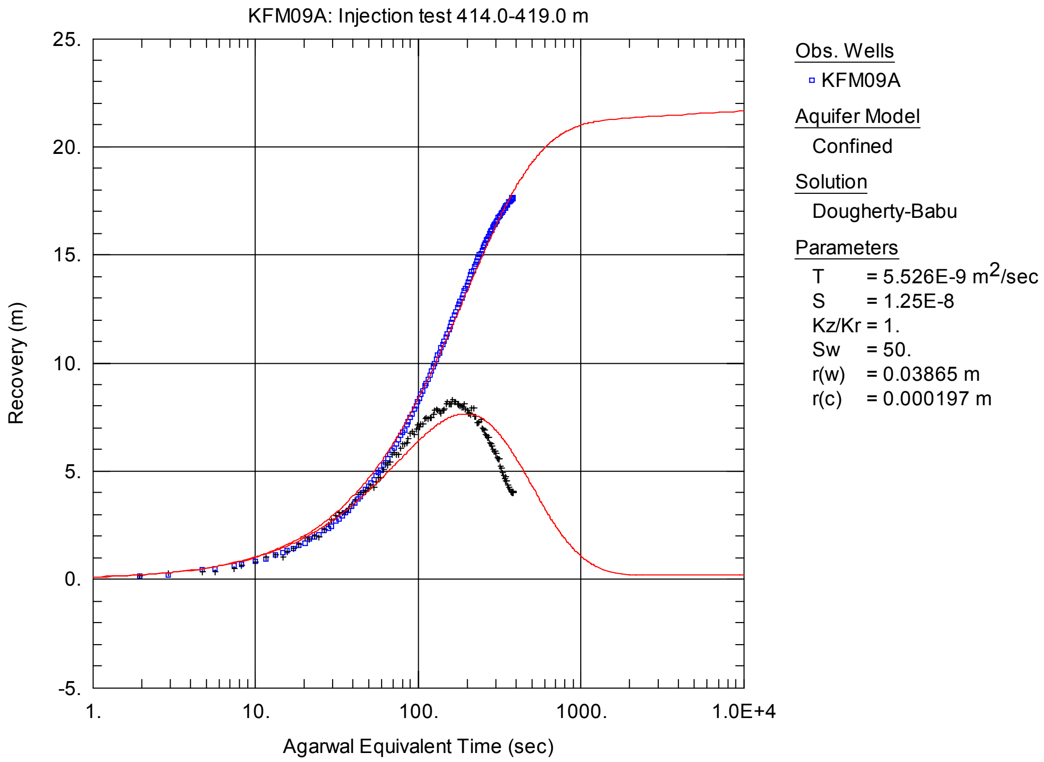


Figure A3-409. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 414.0-419.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.*

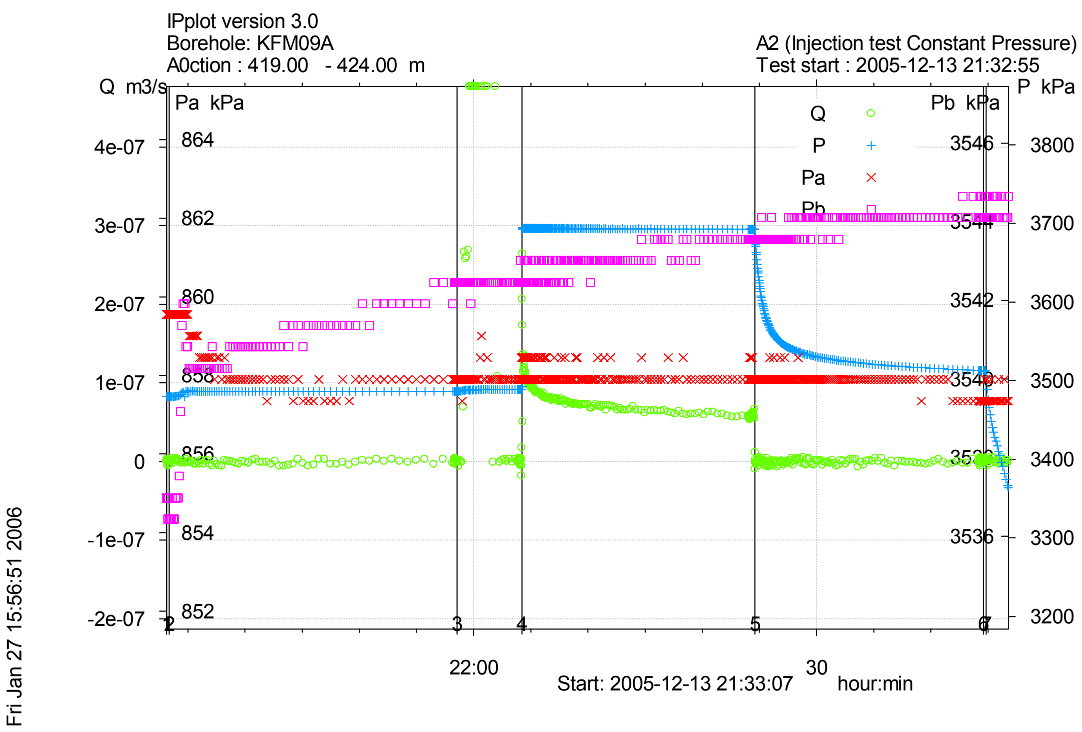


Figure A3-410. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 419.0-424.0 m in borehole KFM09A.*

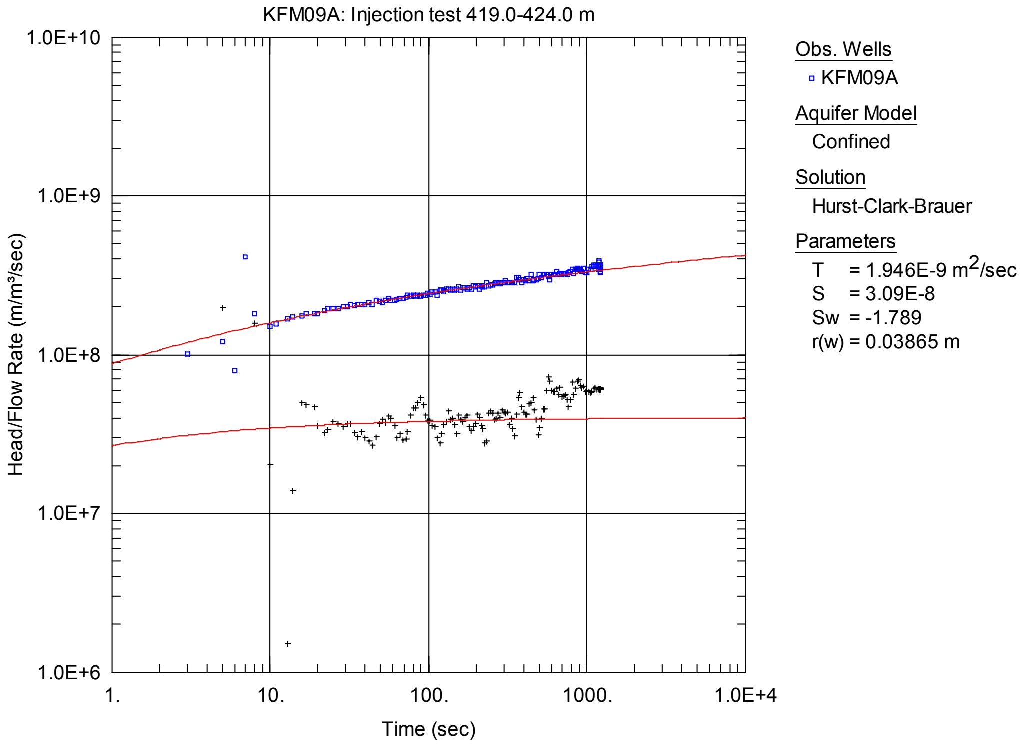


Figure A3-411. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 419.0-424.0 m in KFM09A. This plot shows a fit to the first of two different PRF:s during the injection period in this section.

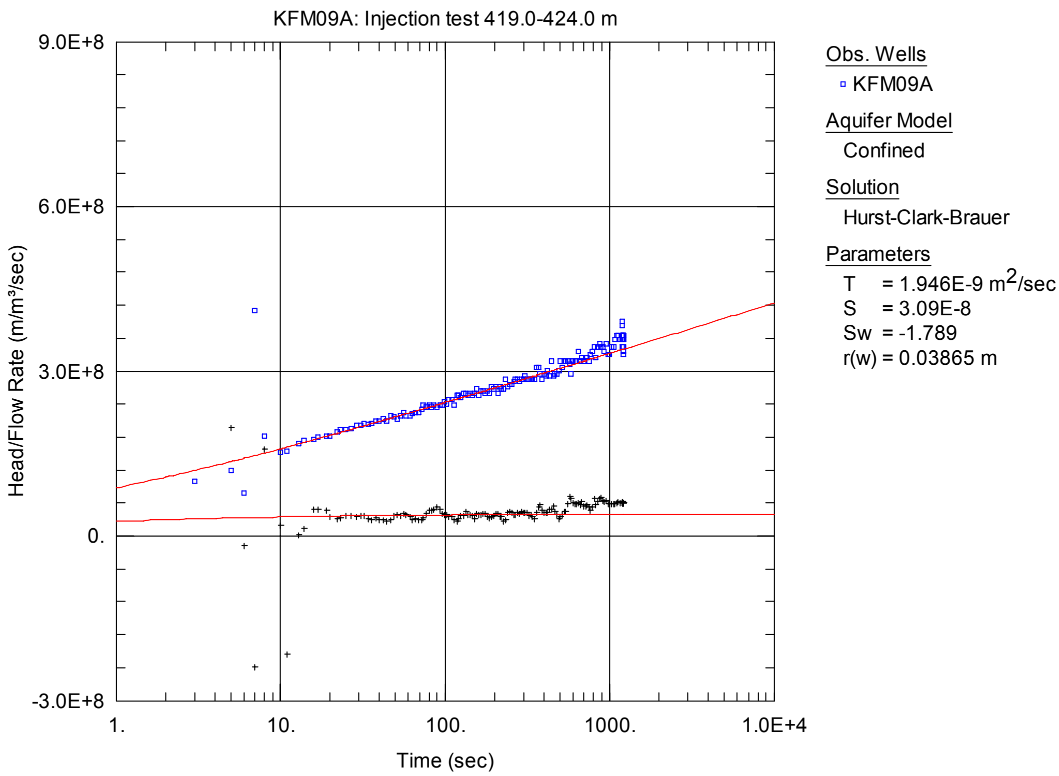


Figure A3-412. Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 419.0-424.0 m in KFM09A. This plot shows a fit to the first of two different PRF:s during the injection period in this section.

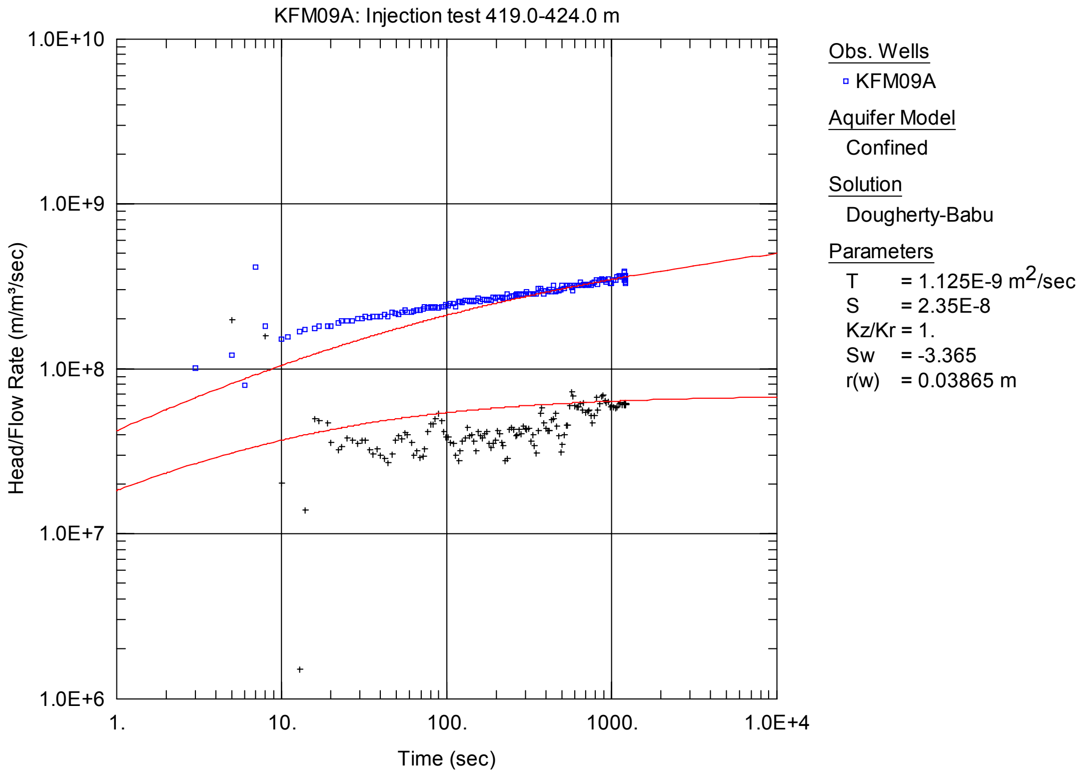


Figure A3-413. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 419.0-424.0 m in KFM09A. This plot shows a fit to the second of two different PRF:s during the injection period in this section.*

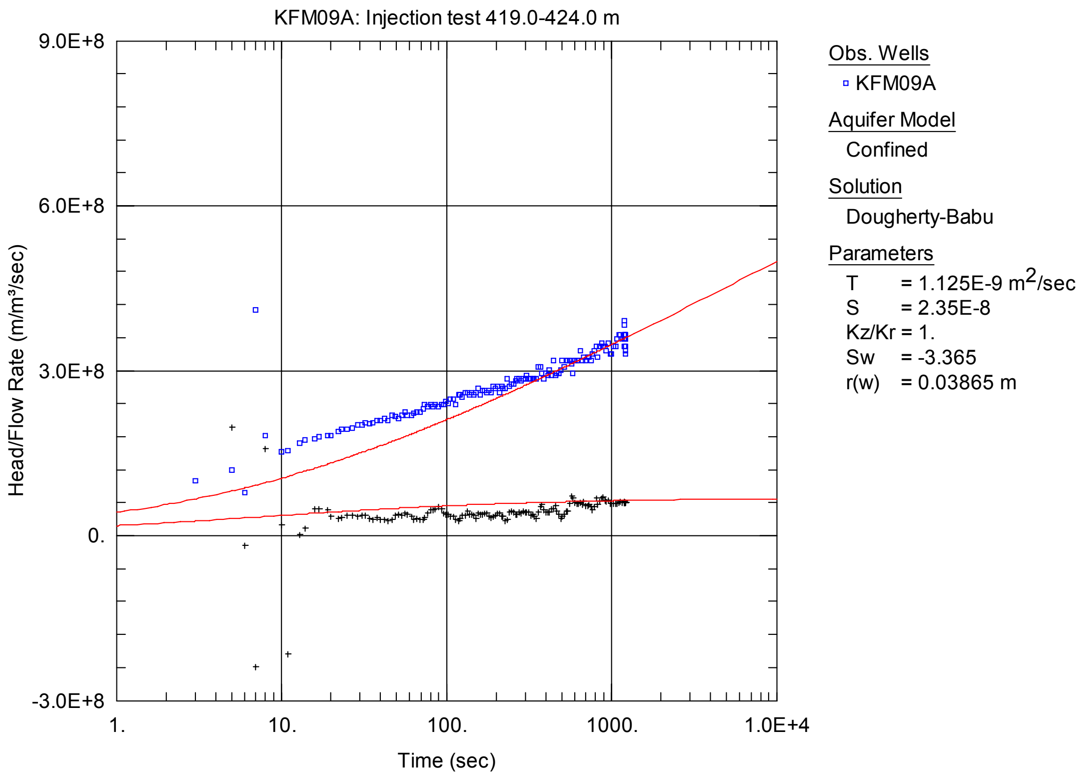


Figure A3-414. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 419.0-424.0 m in KFM09A. This plot shows a fit to the second of two different PRF:s during the injection period in this section.*

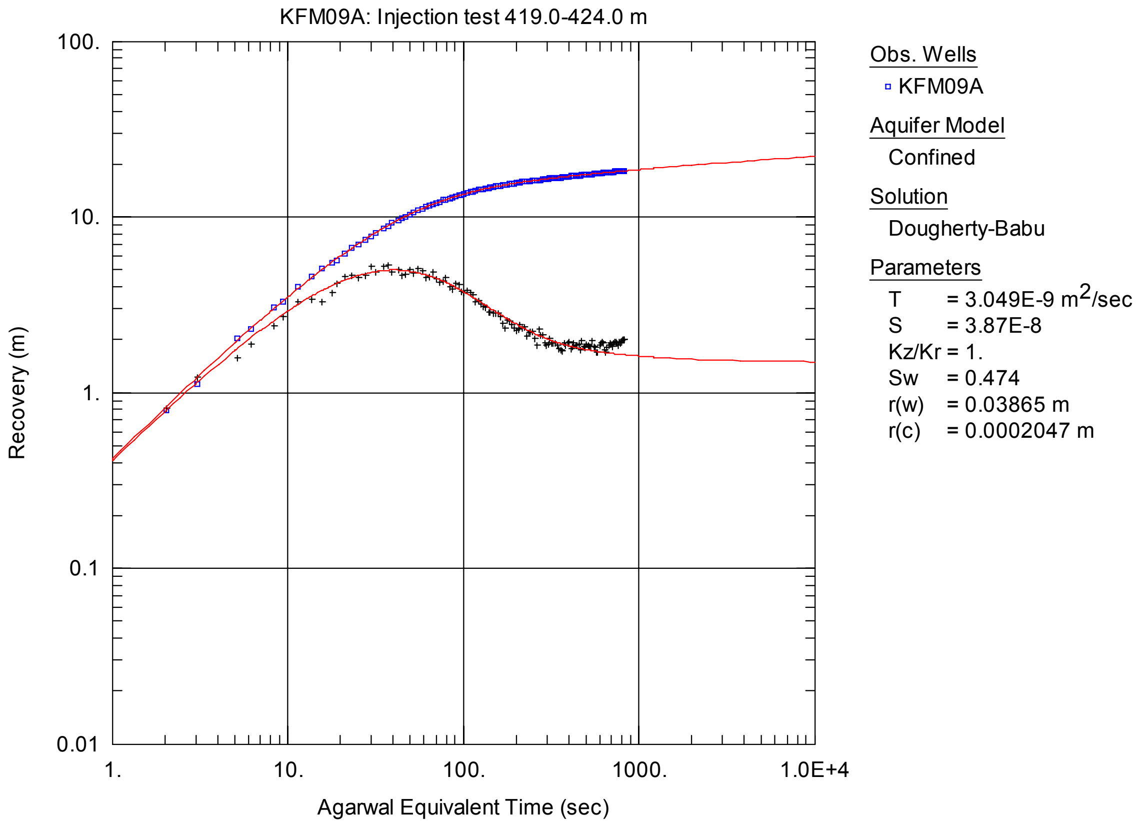


Figure A3-415. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 419.0-424.0 m in KFM09A.*

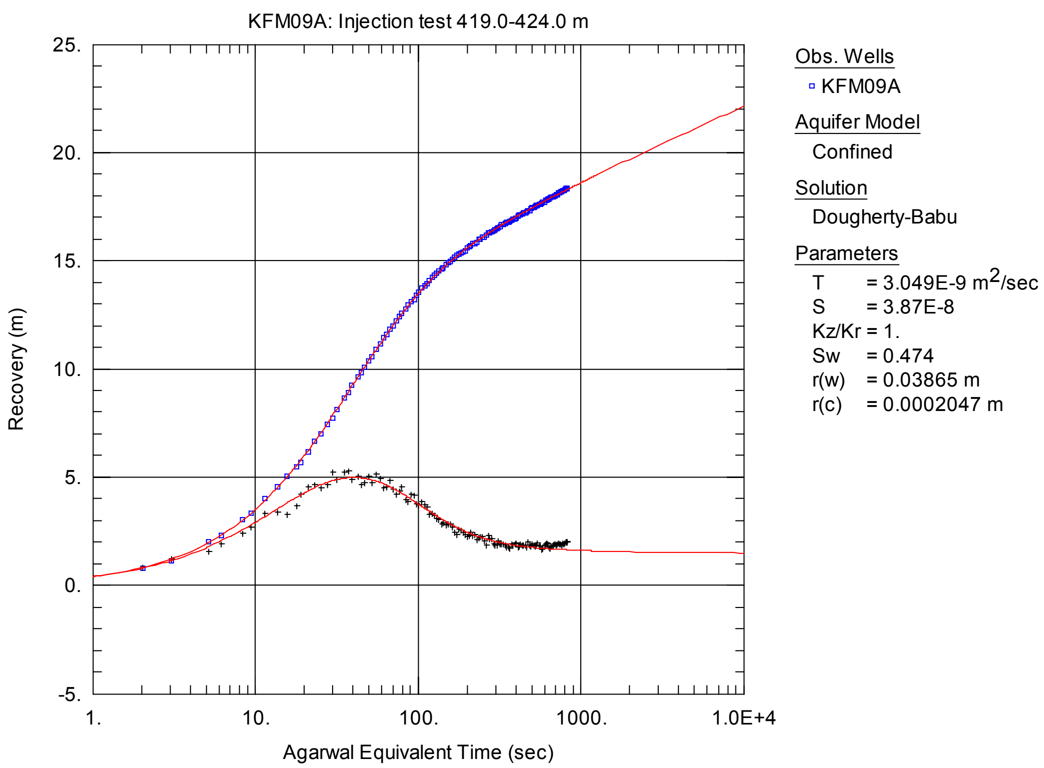


Figure A3-416. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 419.0-424.0 m in KFM09A.*

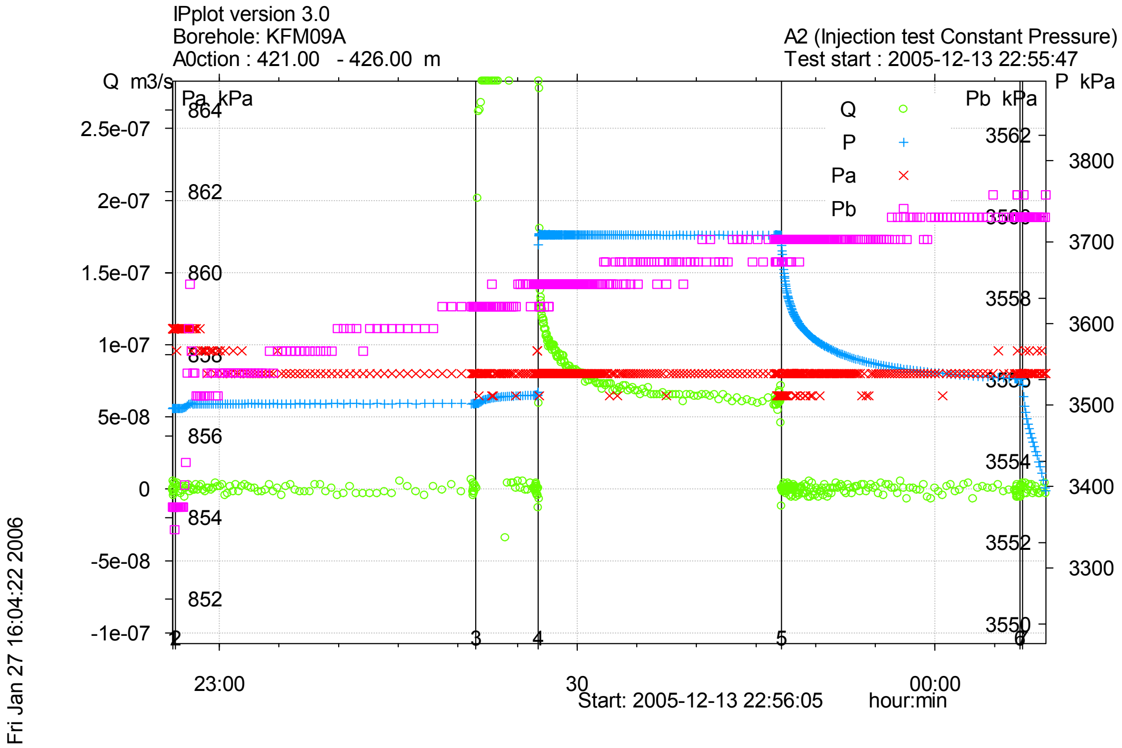


Figure A3-417. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 421.0-426.0 m in borehole KFM09A.*

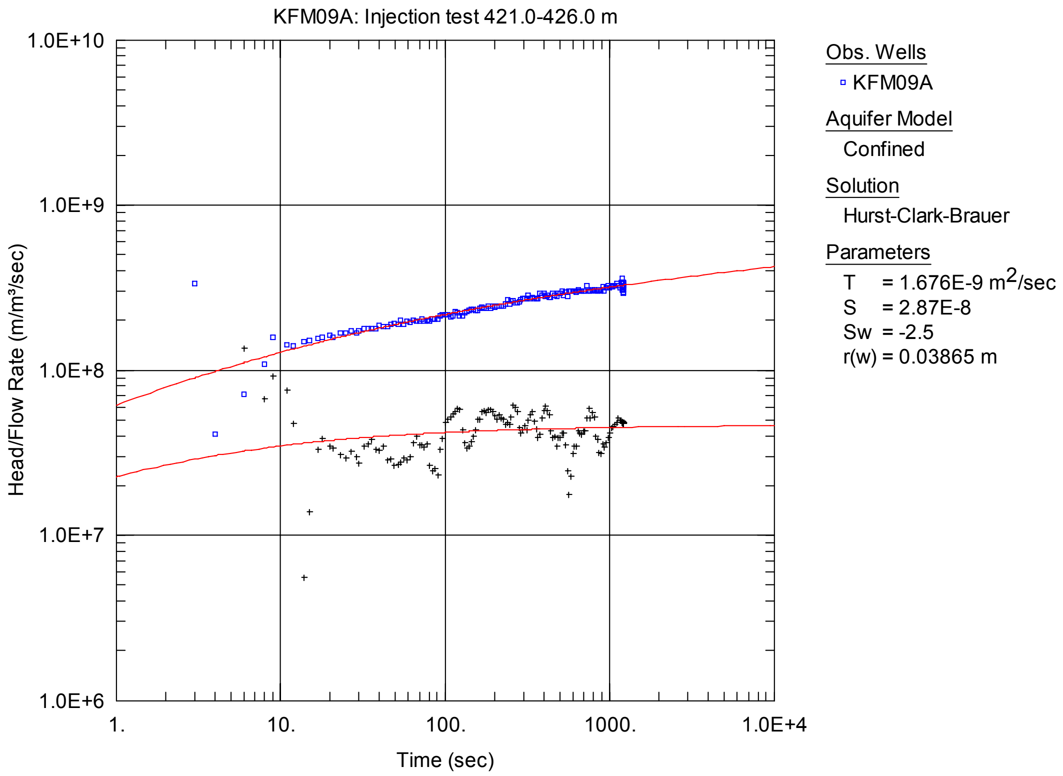


Figure A3-418. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 421.0-426.0 m in KFM09A.*

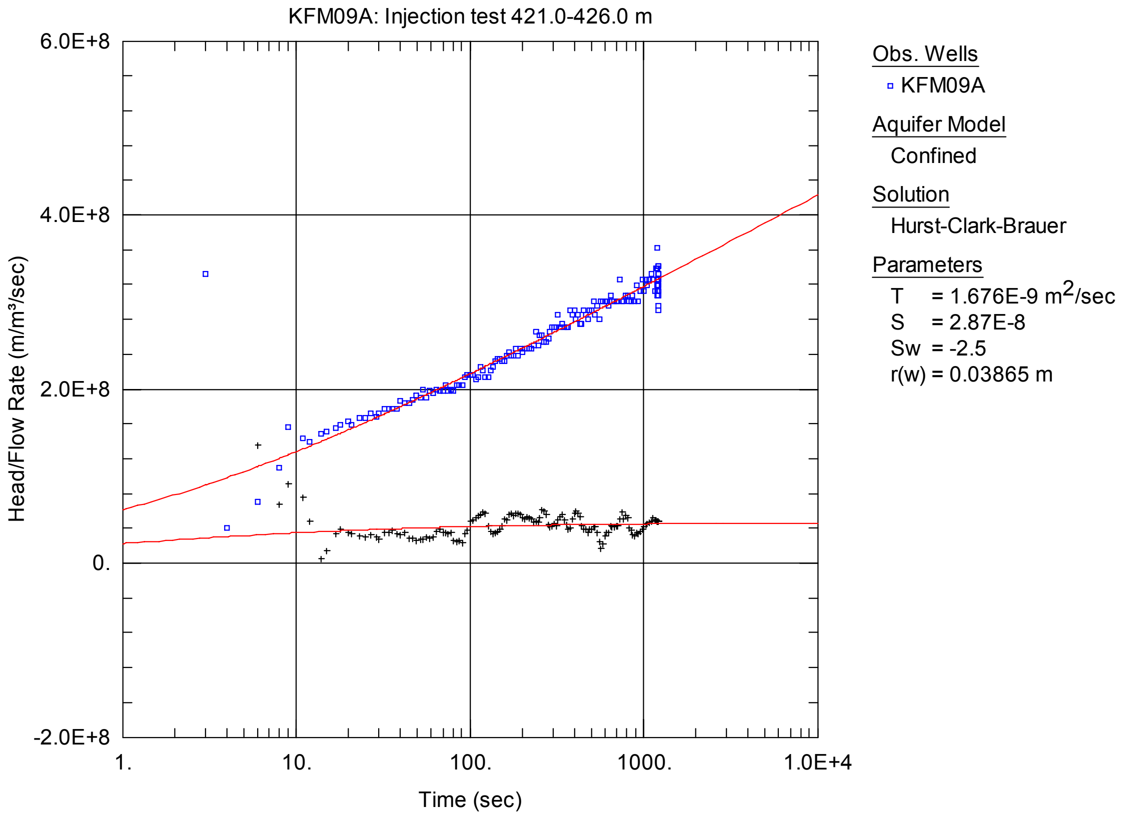


Figure A3-419. Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 421.0-426.0 m in KFM09A.

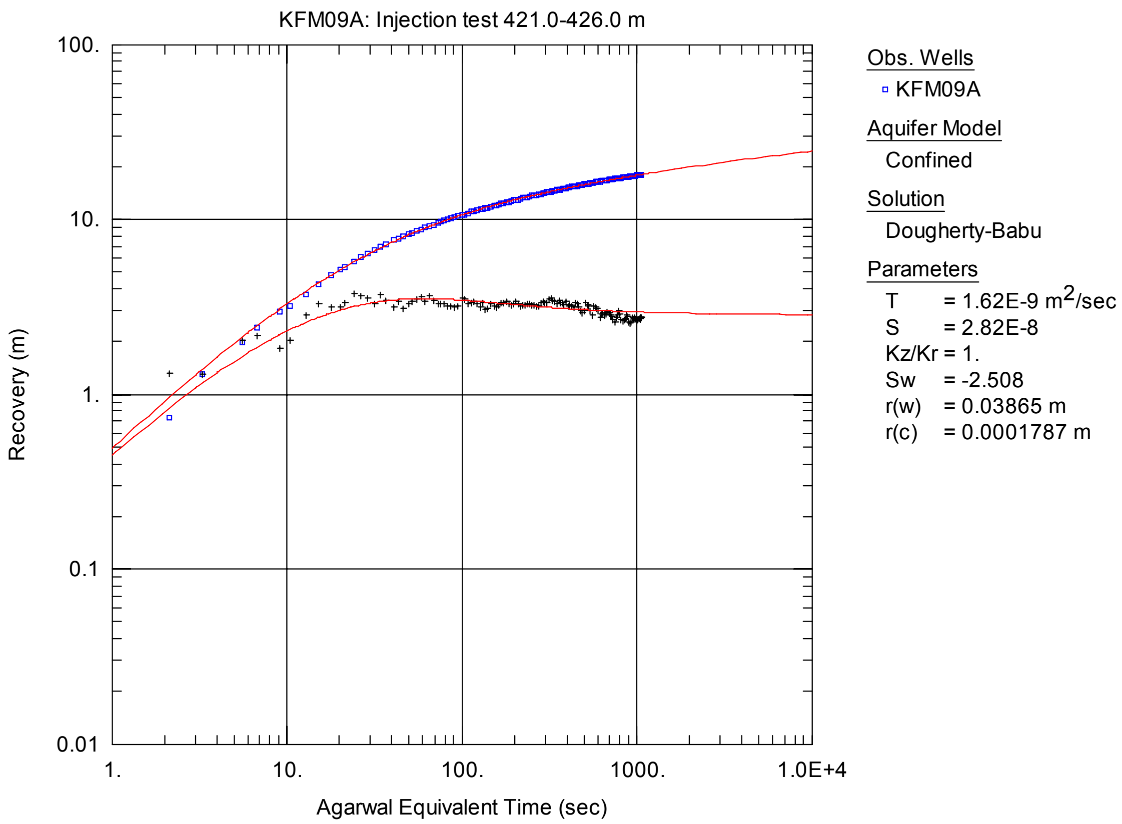


Figure A3-420. Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 421.0-426.0 m in KFM09A.

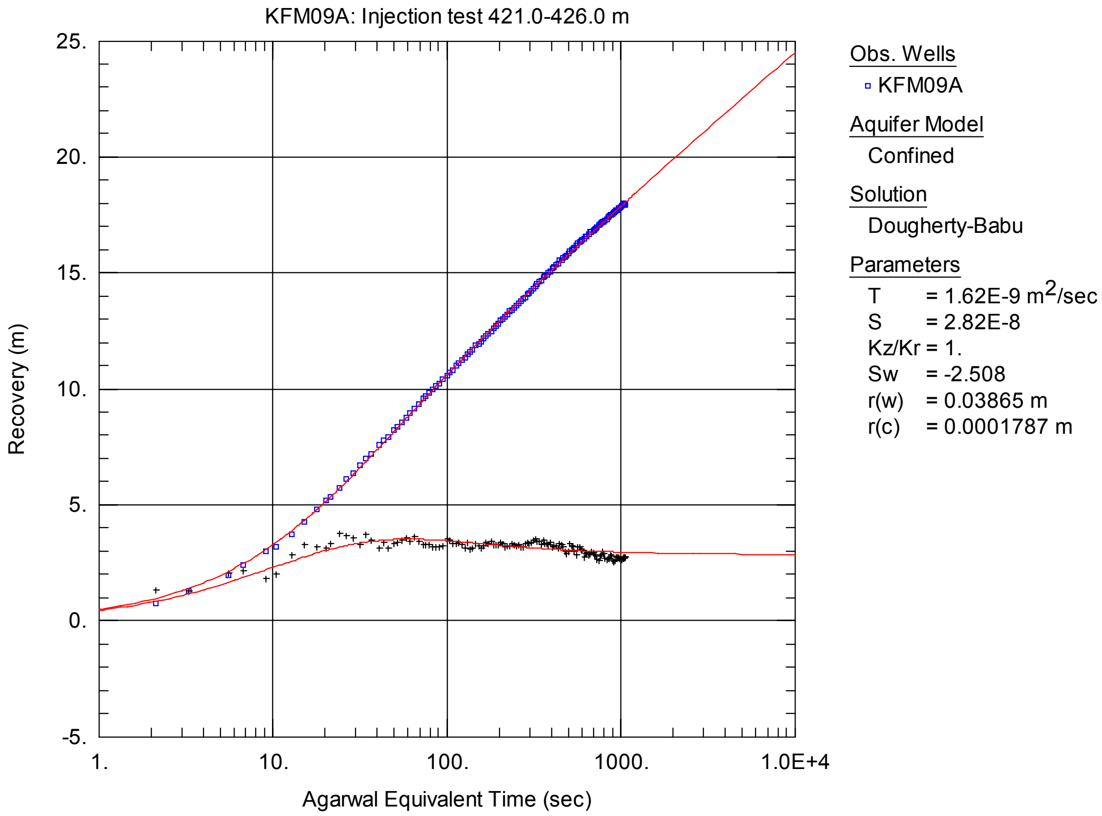


Figure A3-421. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 421.0-426.0 m in KFM09A.*

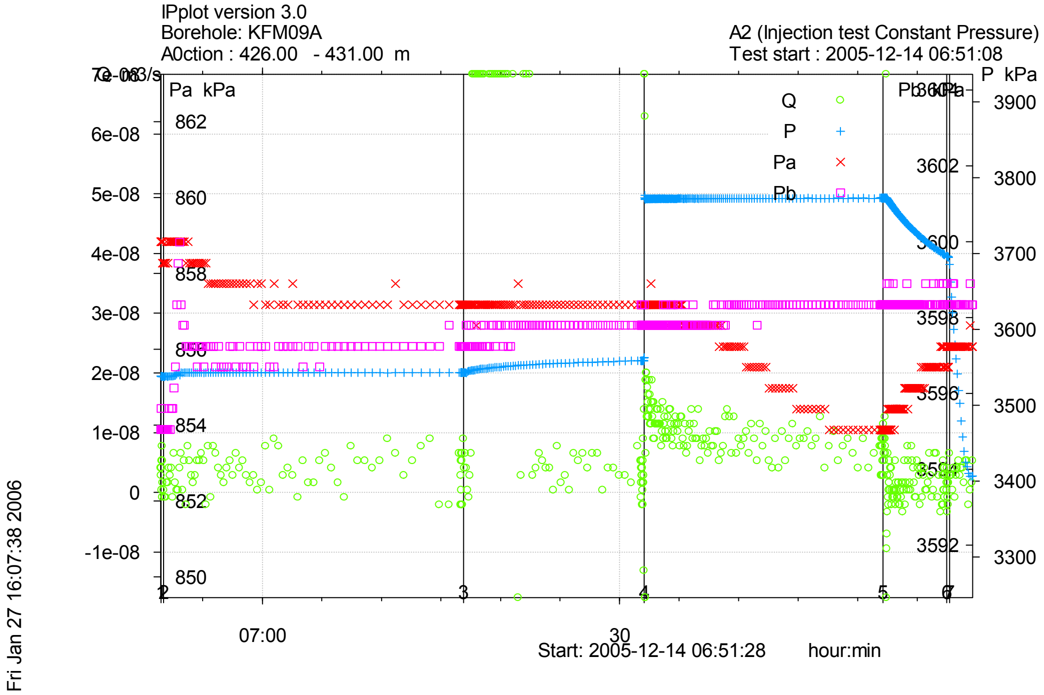


Figure A3-422. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 426.0-431.0 m in borehole KFM09A.*

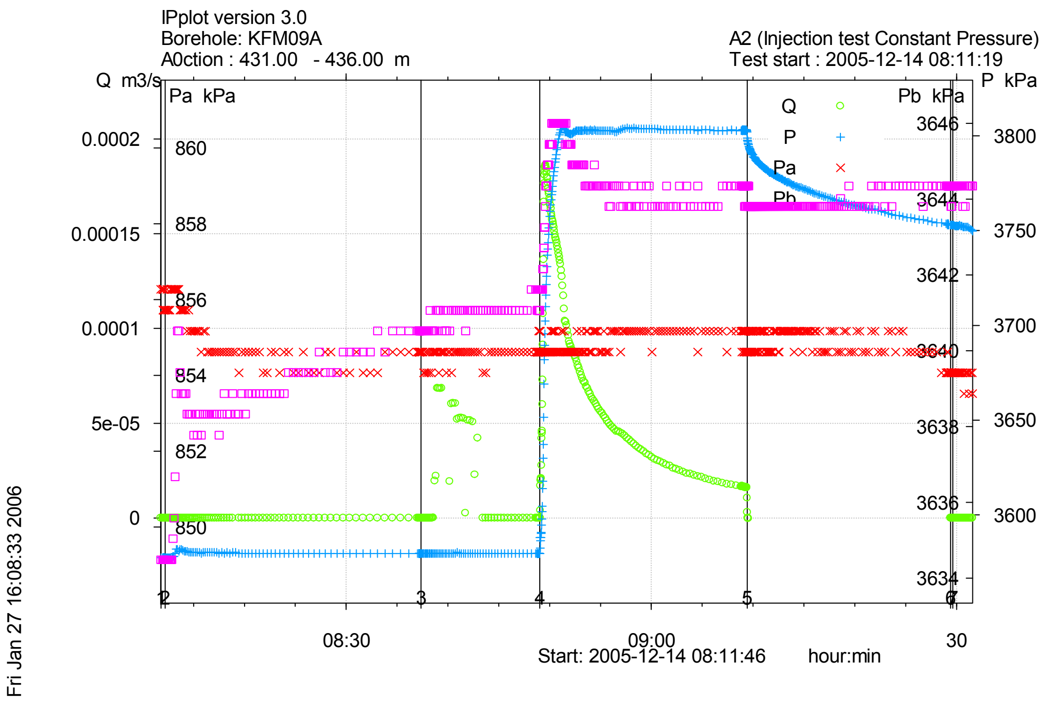


Figure A3-423. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 431.0-436.0 m in borehole KFM09A.

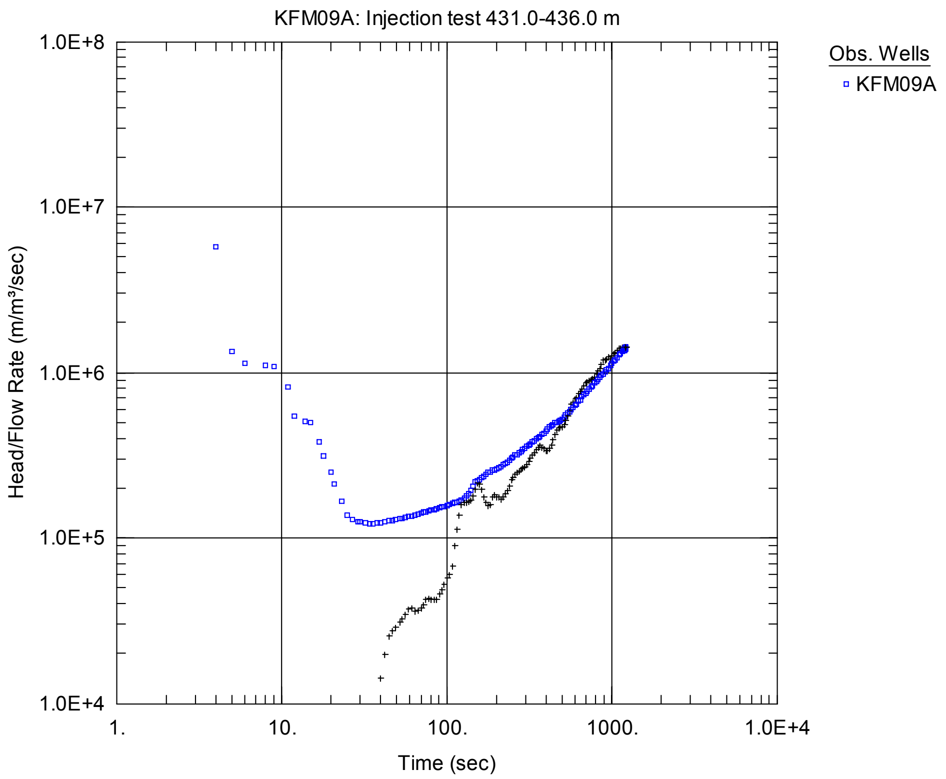


Figure A3-424. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 431.0-436.0 m in KFM09A.

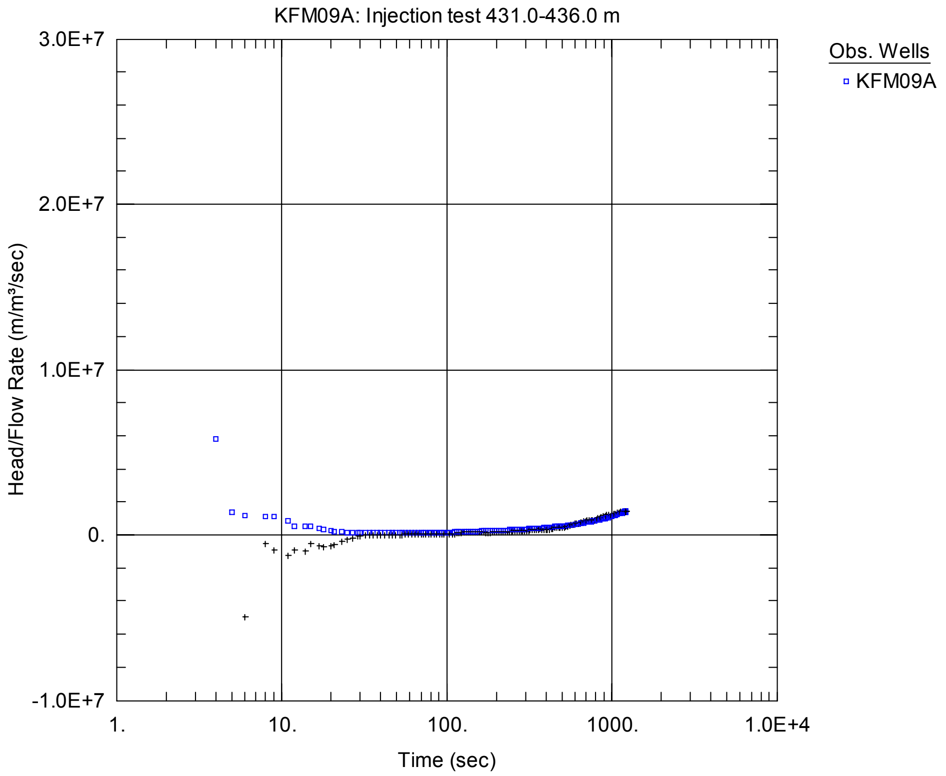


Figure A3-425. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 431.0-436.0 m in KFM09A.*

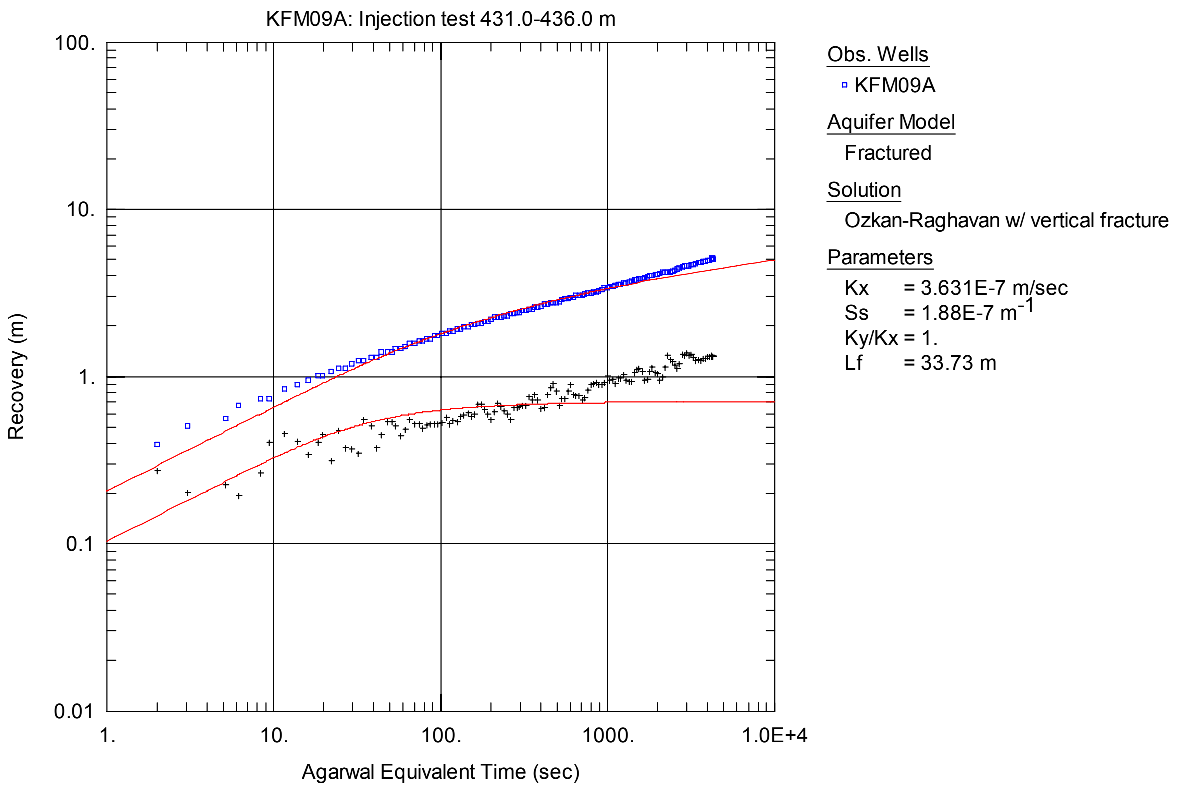


Figure A3-426. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 431.0-436.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

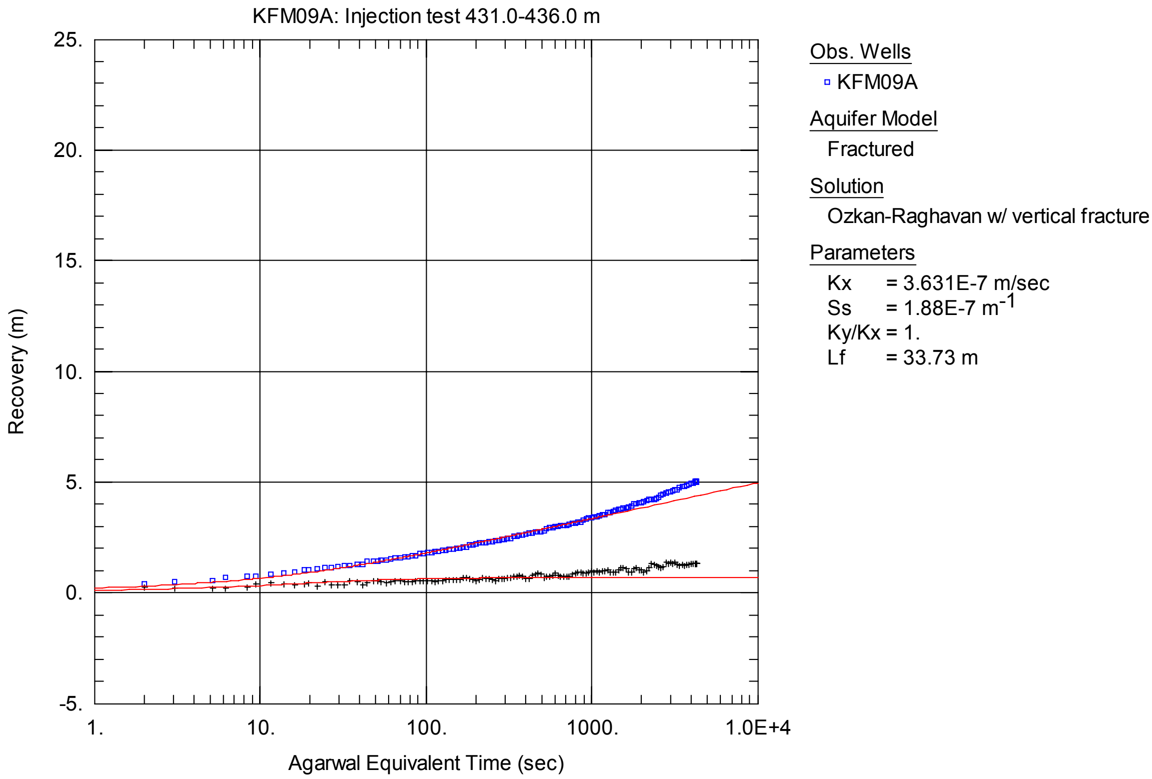


Figure A3-427. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 431.0-436.0 m in KFM09A.This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

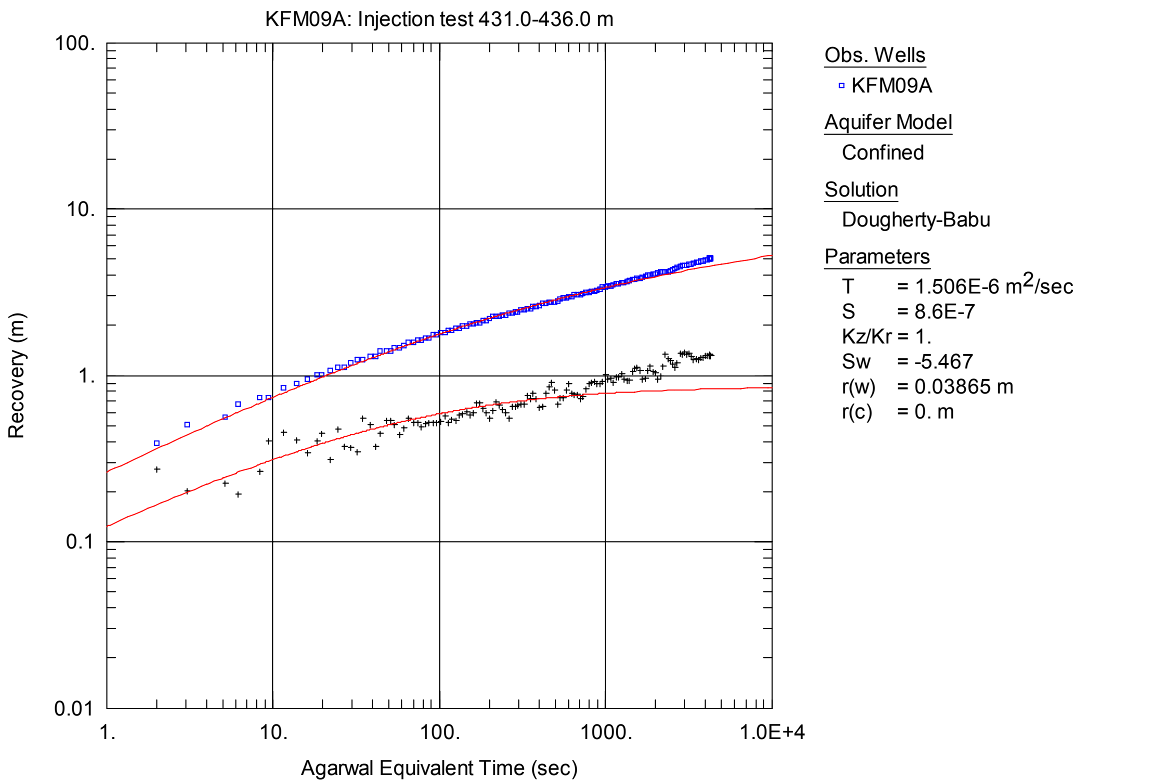


Figure A3-428. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 431.0-436.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

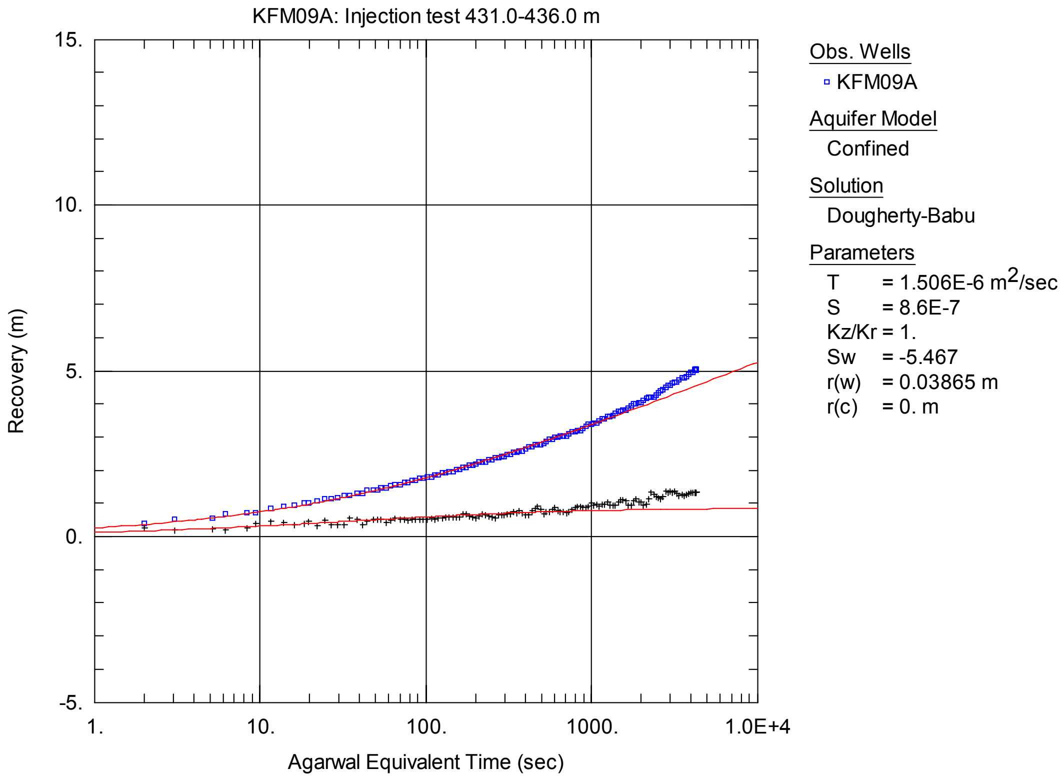


***Figure A3-429.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 431.0-436.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

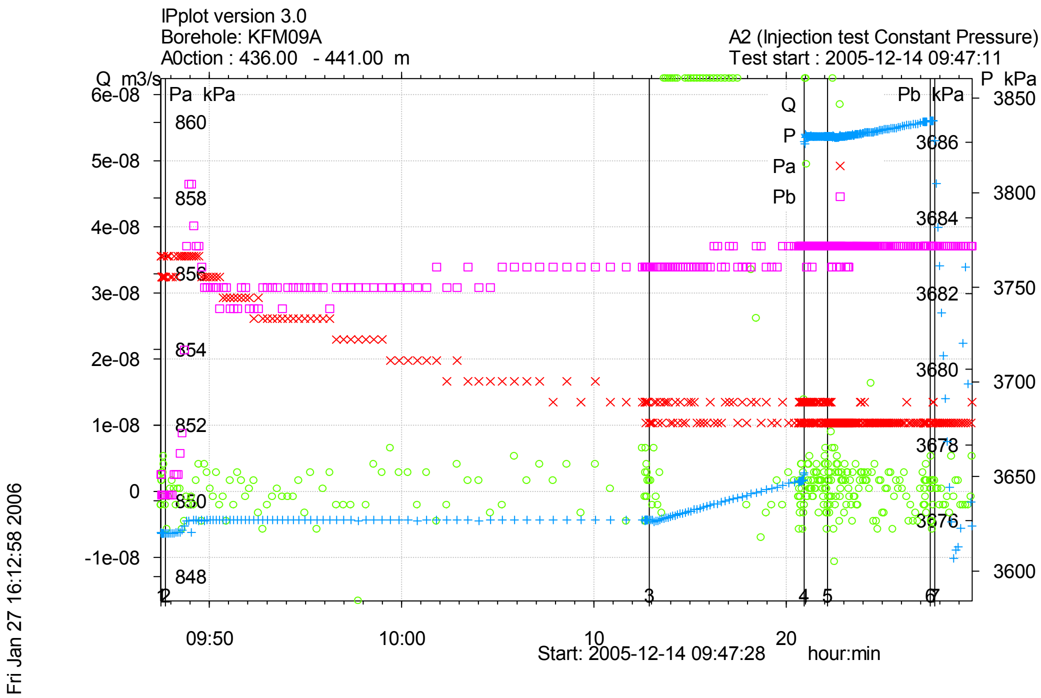


***Figure A3-430.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 436.0-441.0 m in borehole KFM09A.*

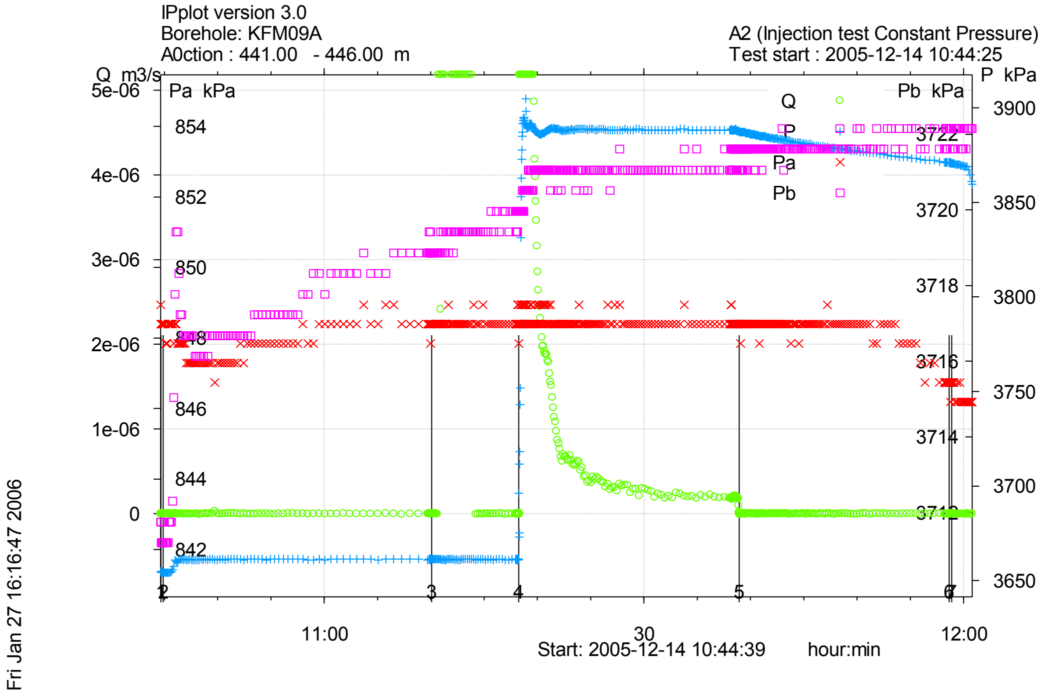


Figure A3-431. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in 441.0-446.0 m in borehole KFM09A.*

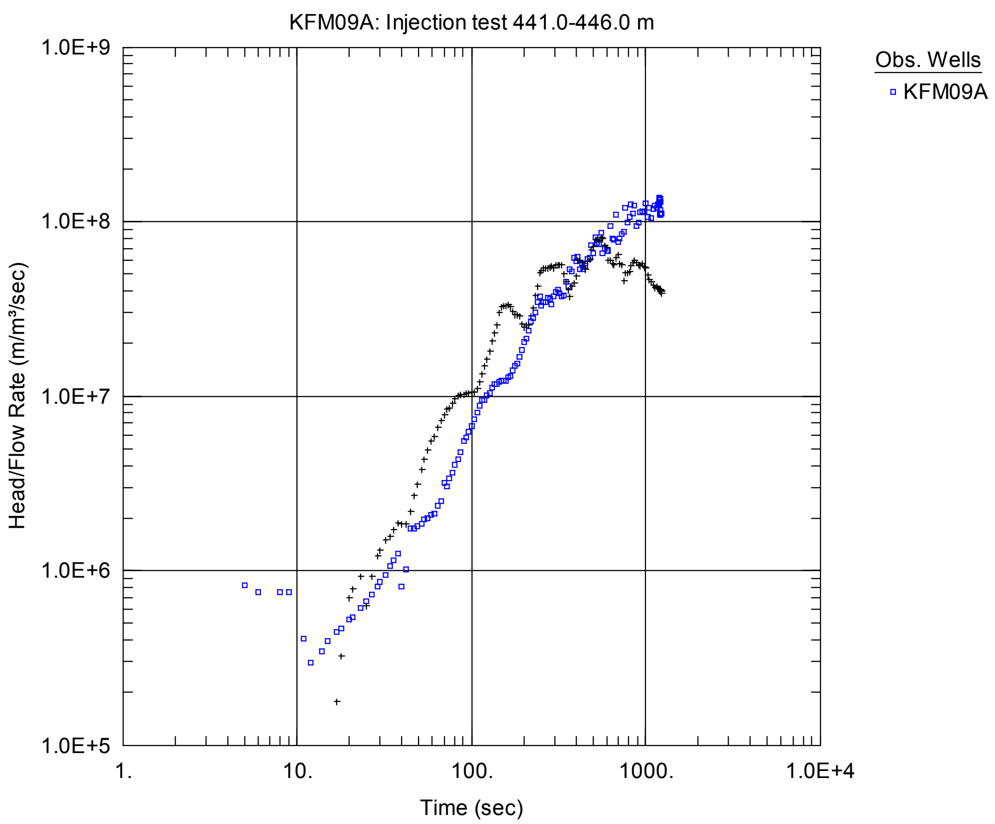


Figure A3-432. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 441.0-446.0 m in KFM09A.*

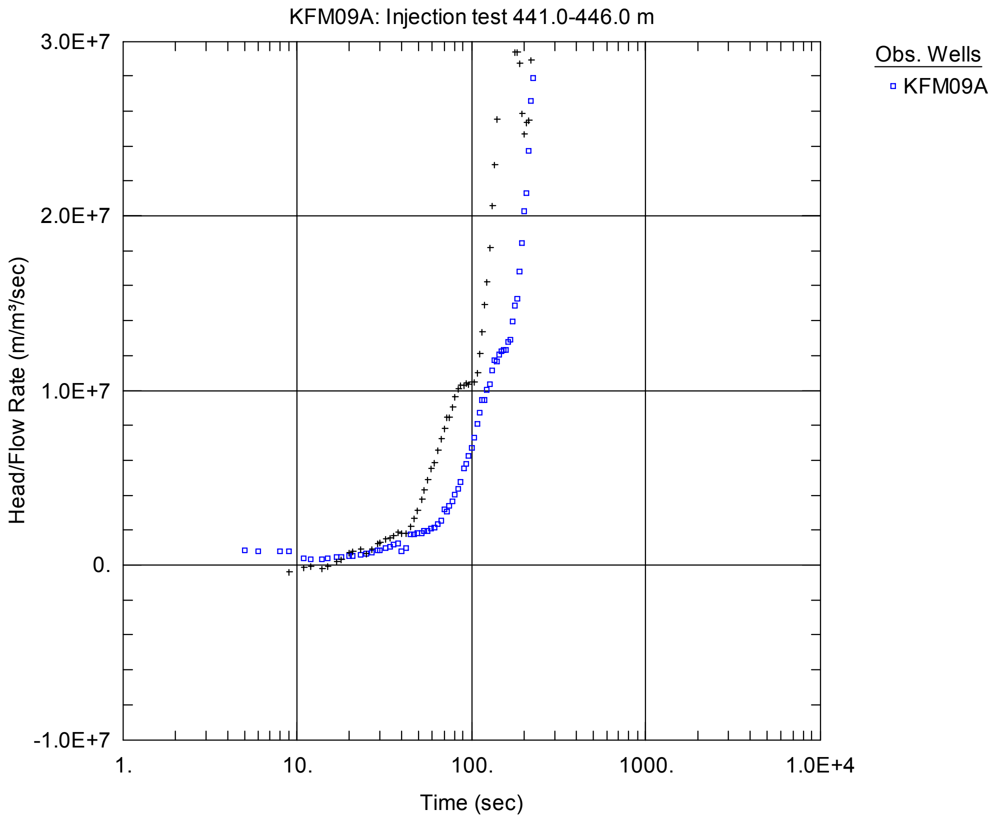


Figure A3-433. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 441.0-446.0 m in KFM09A.*

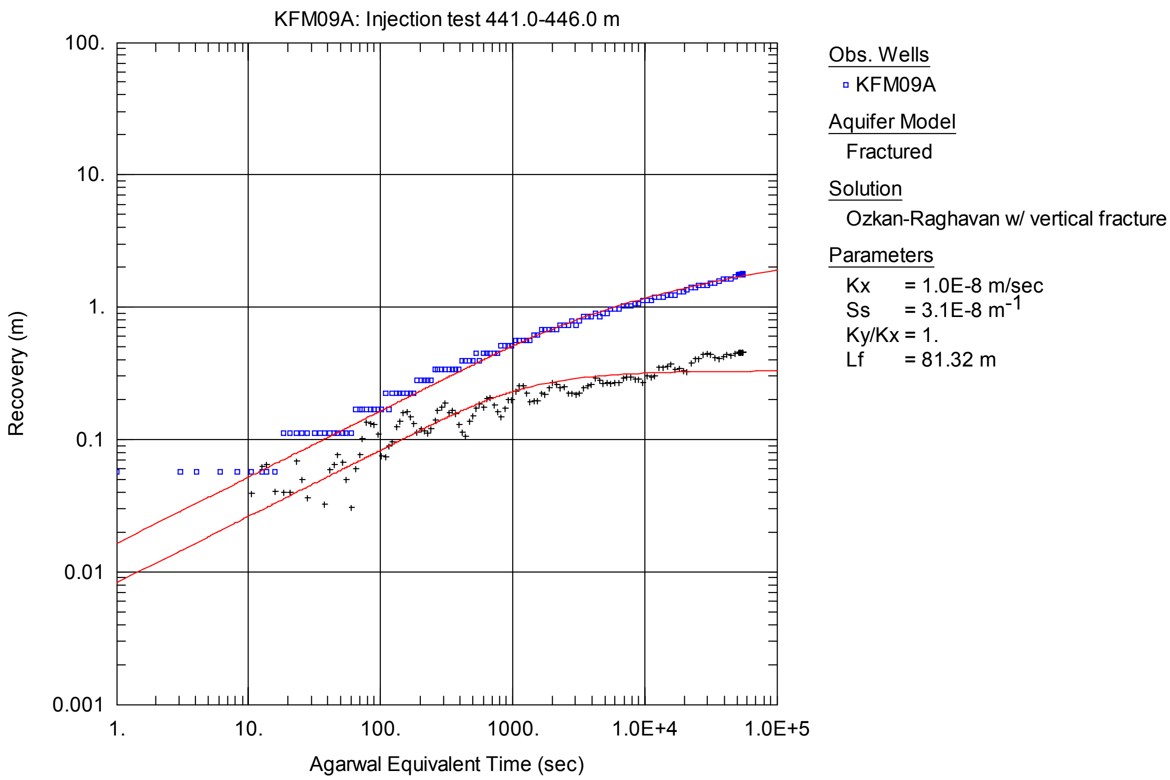


Figure A3-434. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 441.0-446.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

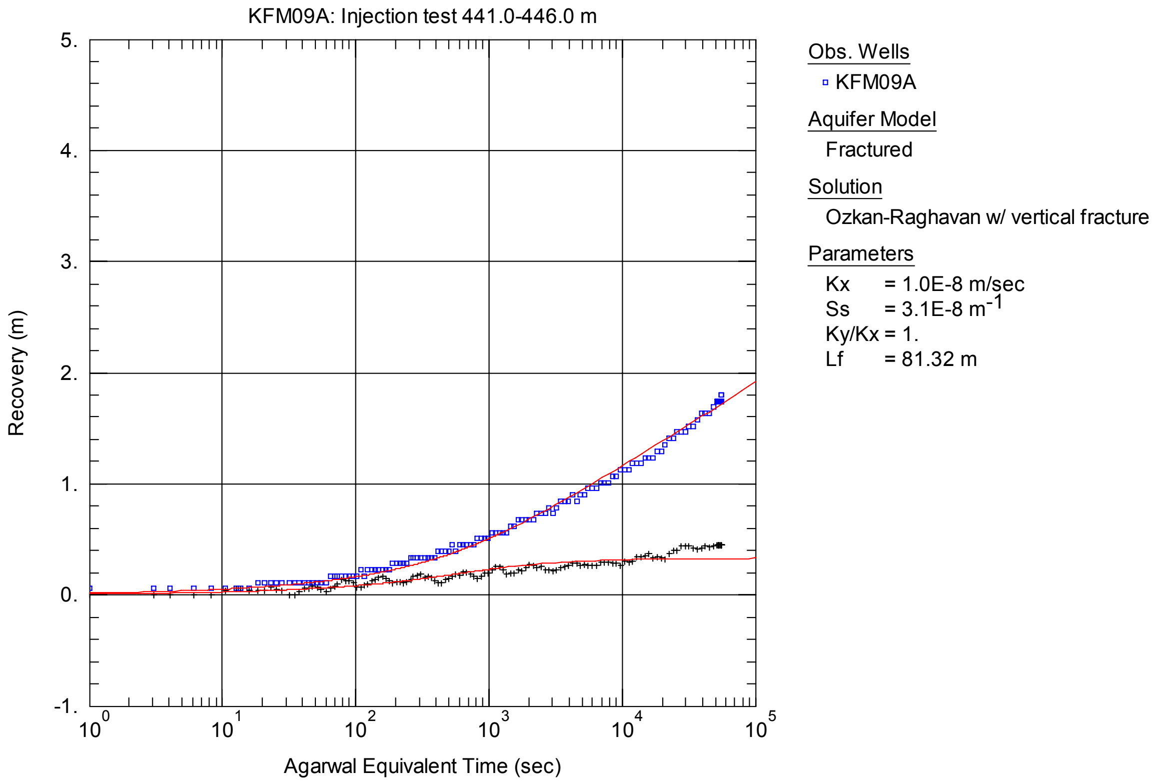


Figure A3-435. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 441.0-446.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

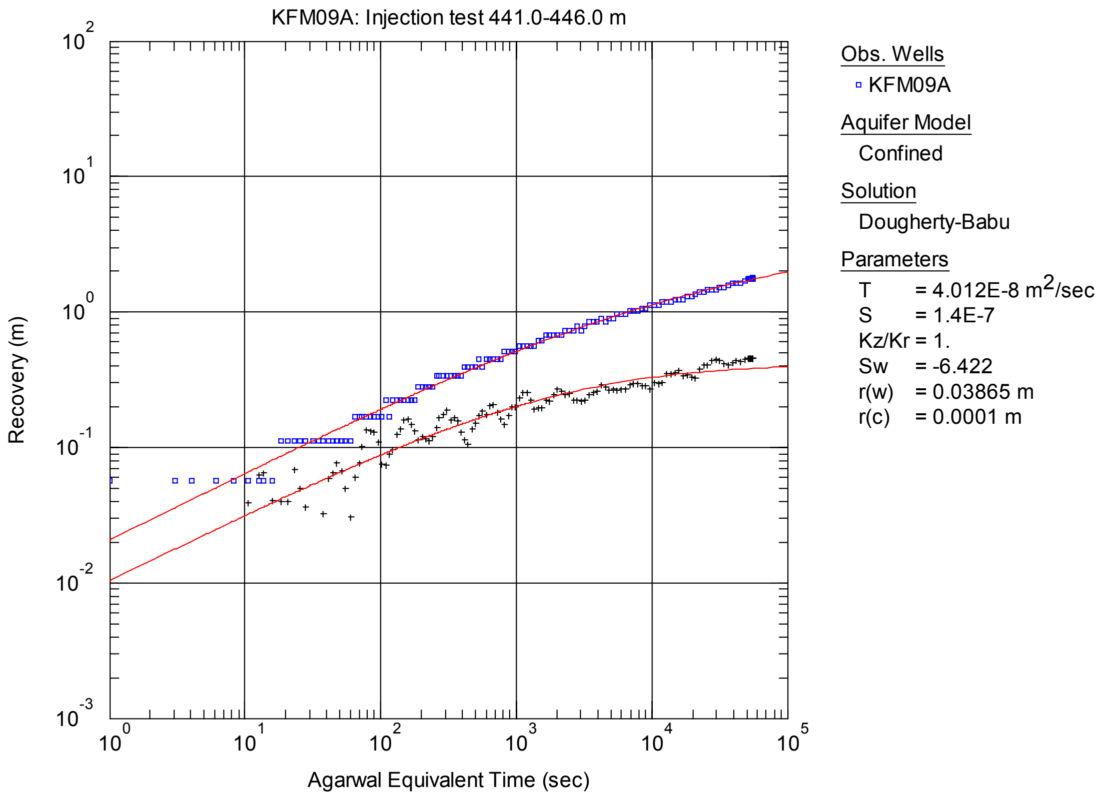


Figure A3-436. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 441.0-446.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

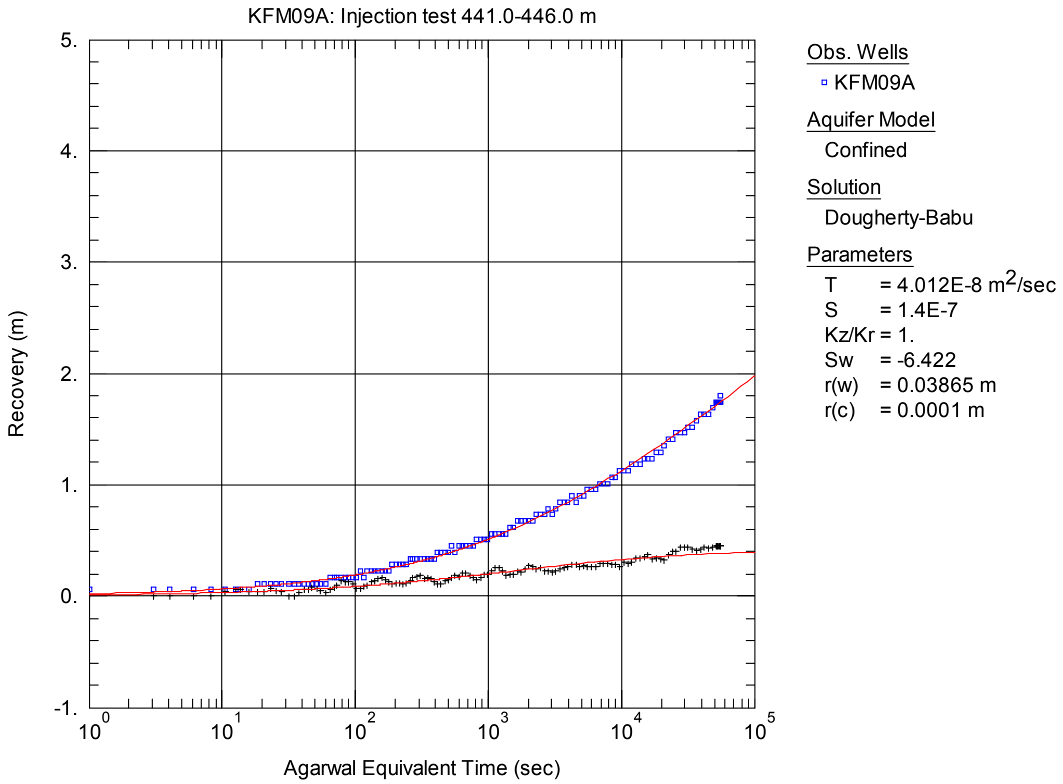


Figure A3-437. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 441.0-446.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

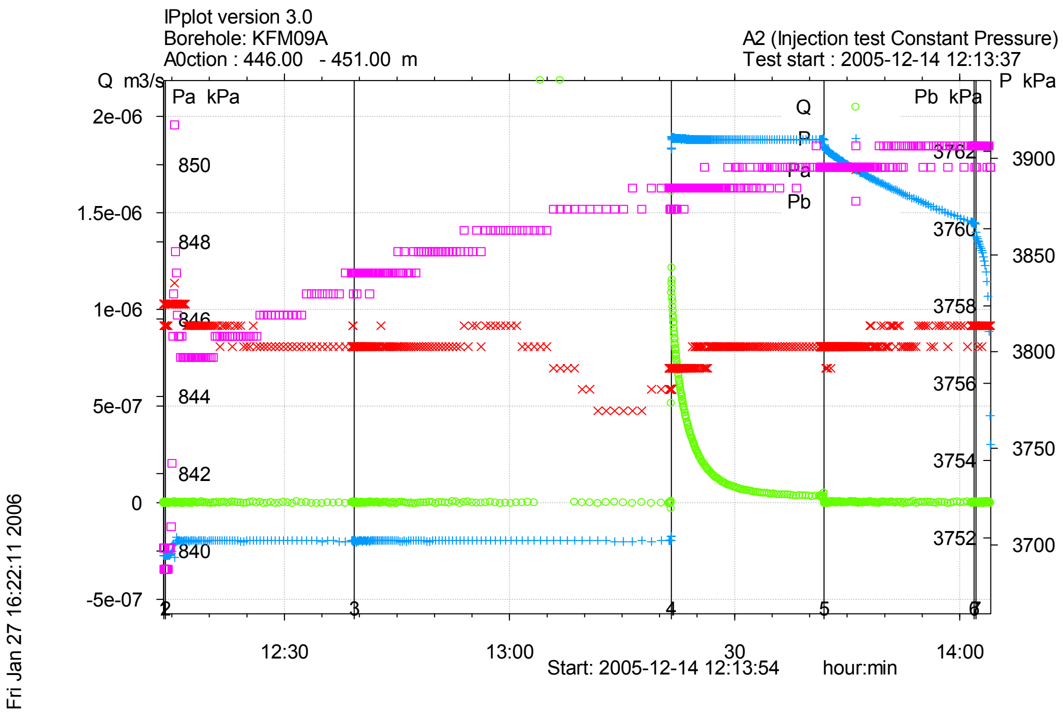


Figure A3-438. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 446.0-451.0 m in borehole KFM09A.*

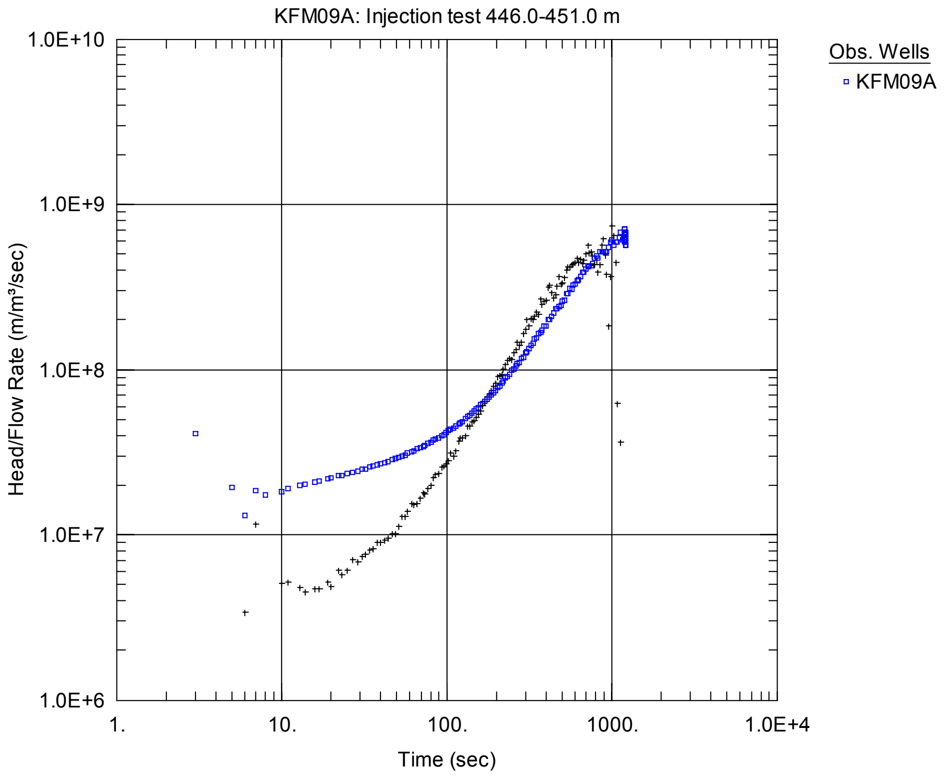


Figure A3-439. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 446.0-451.0 m in KFM09A.*

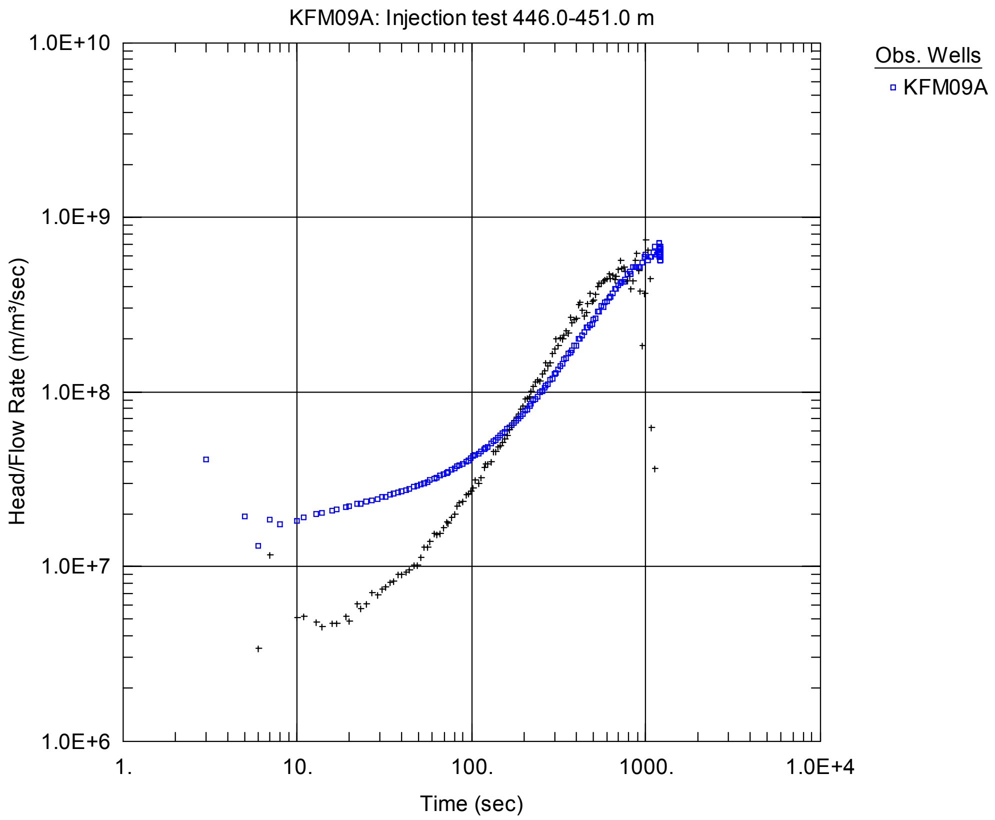


Figure A3-440. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 446.0-451.0 m in KFM09A.*

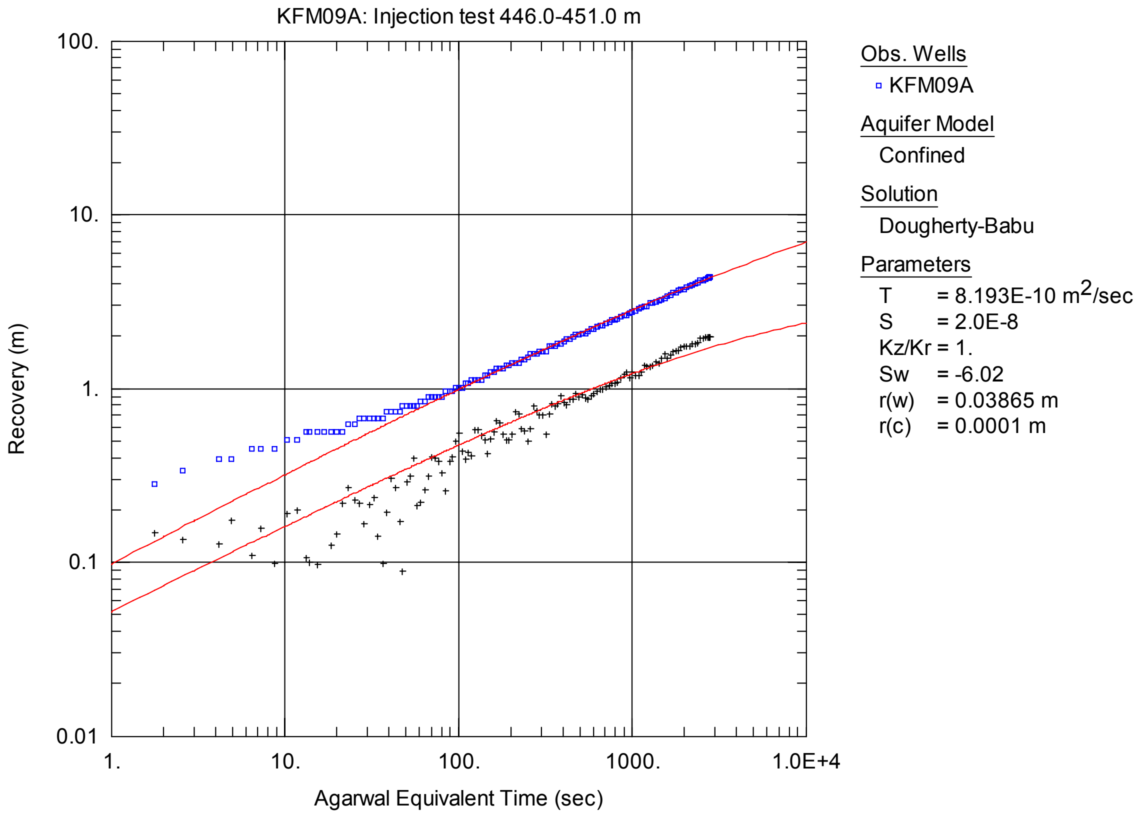


***Figure A3-441.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 446.0-451.0 m in KFM09A.*

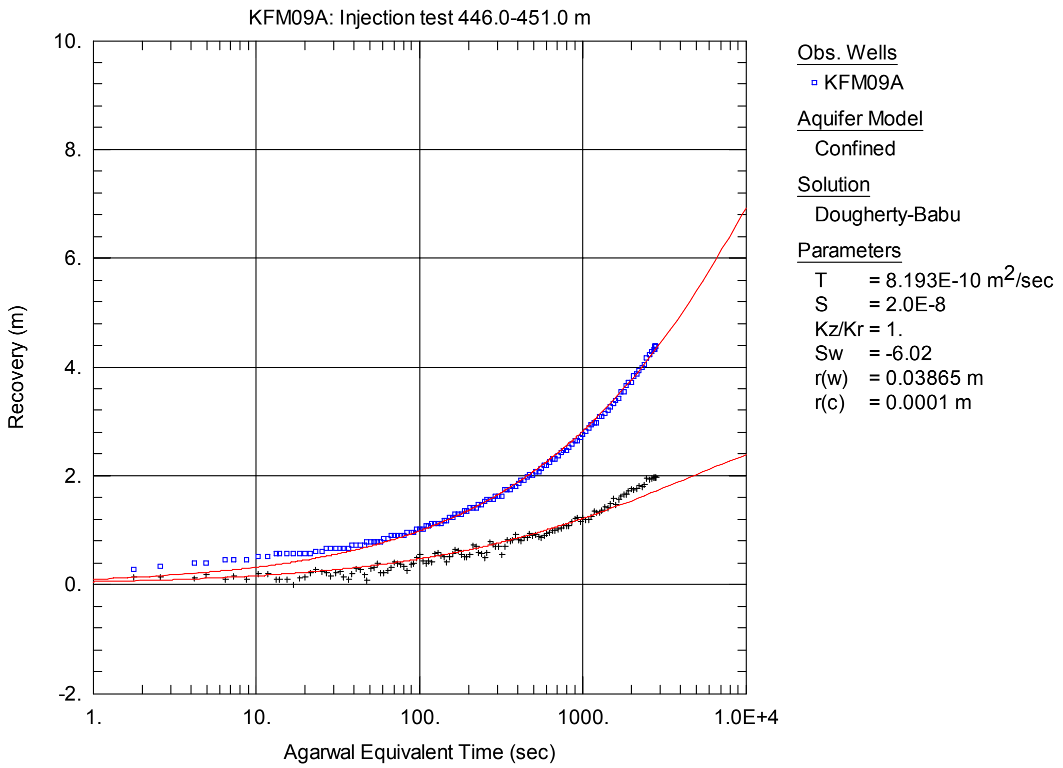


***Figure A3-442.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 446.0-451.0 m in KFM09A.*

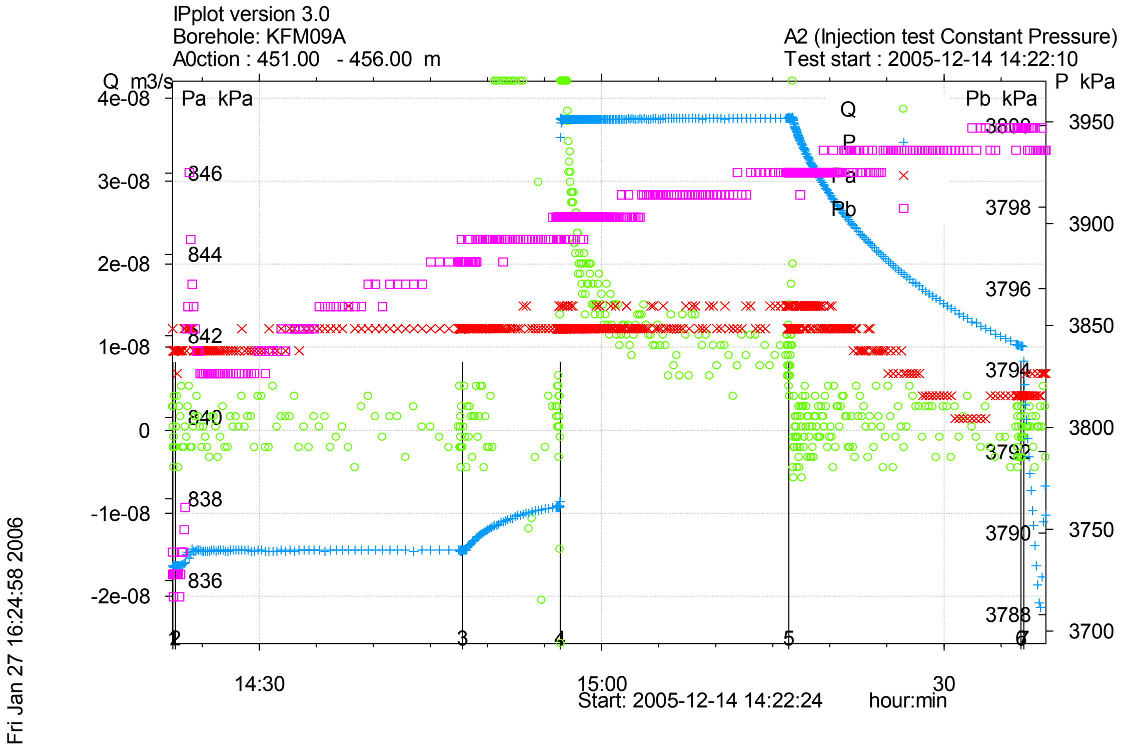


Figure A3-443. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 451.0-456.0 m in borehole KFM09A.

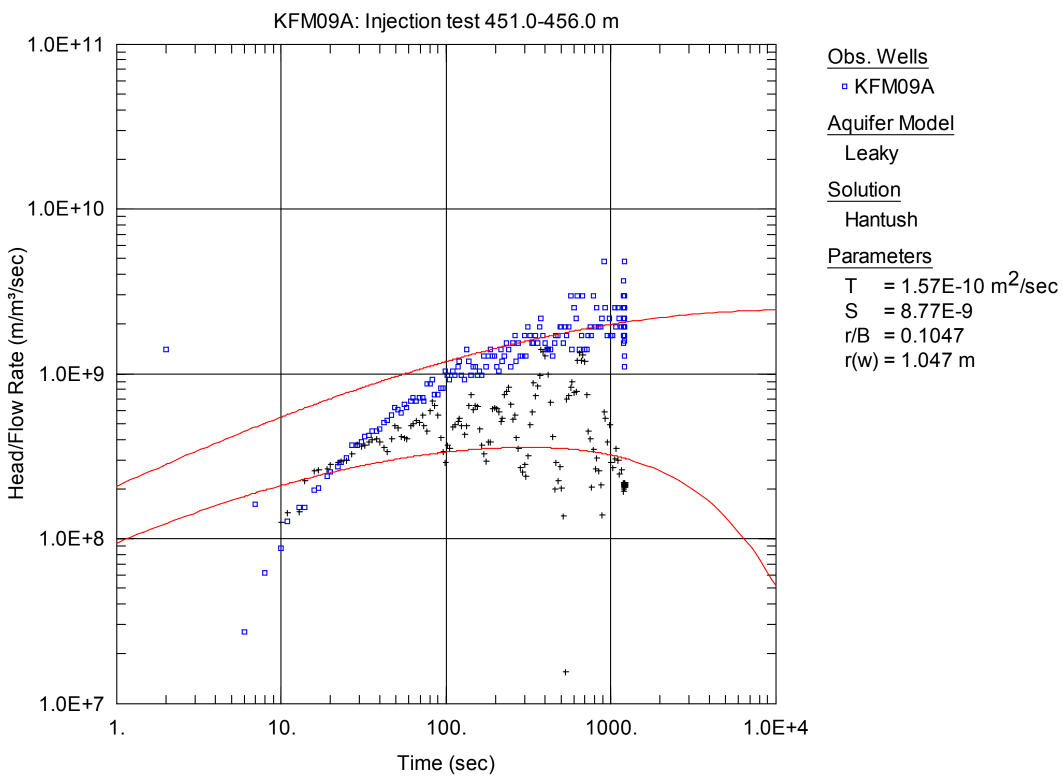


Figure A3-444. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 451.0-456.0 m in KFM09A.

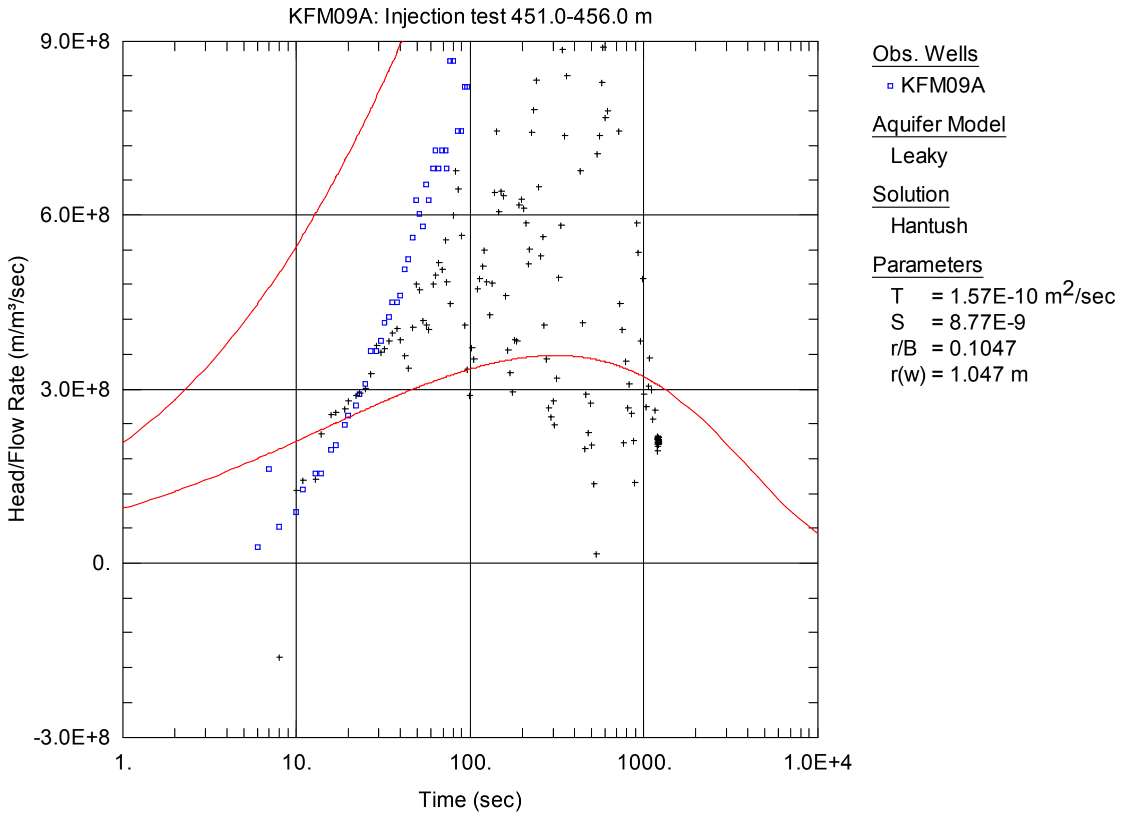


***Figure A3-445.** Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 451.0-456.0 m in KFM09A.*

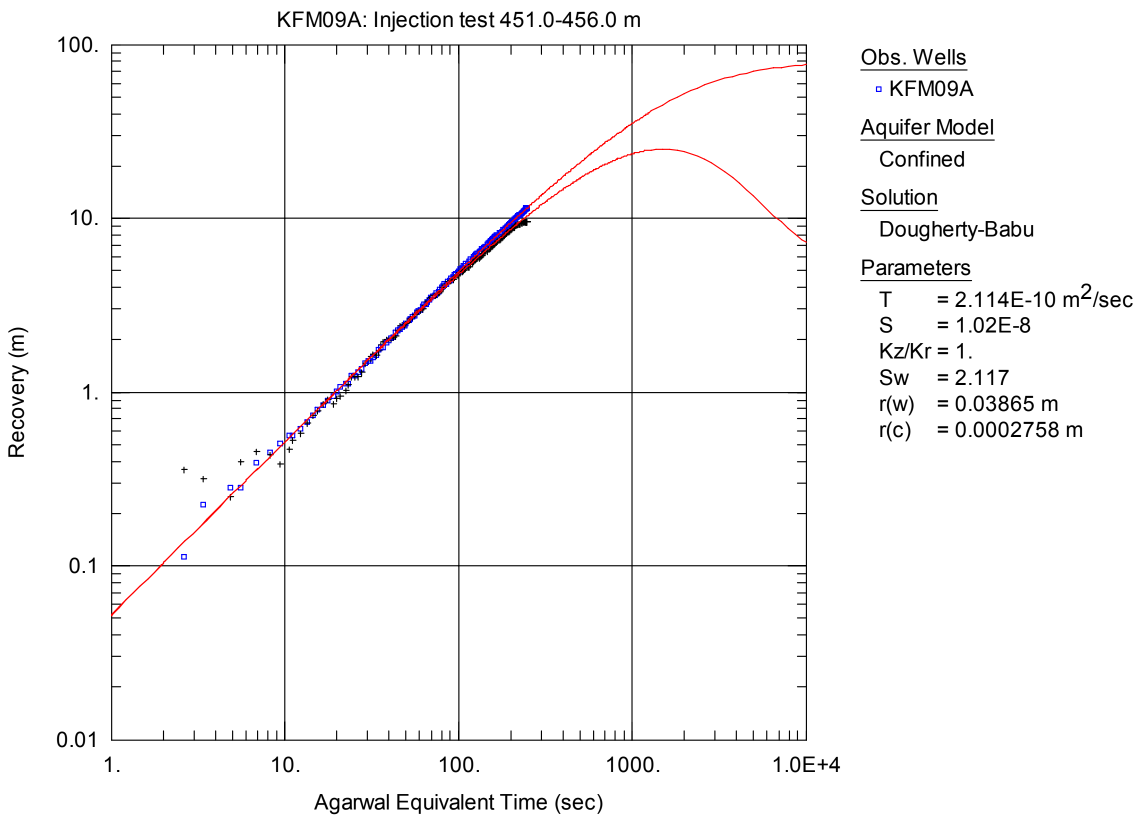


***Figure A3-446.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 451.0-456.0 m in KFM09A.*

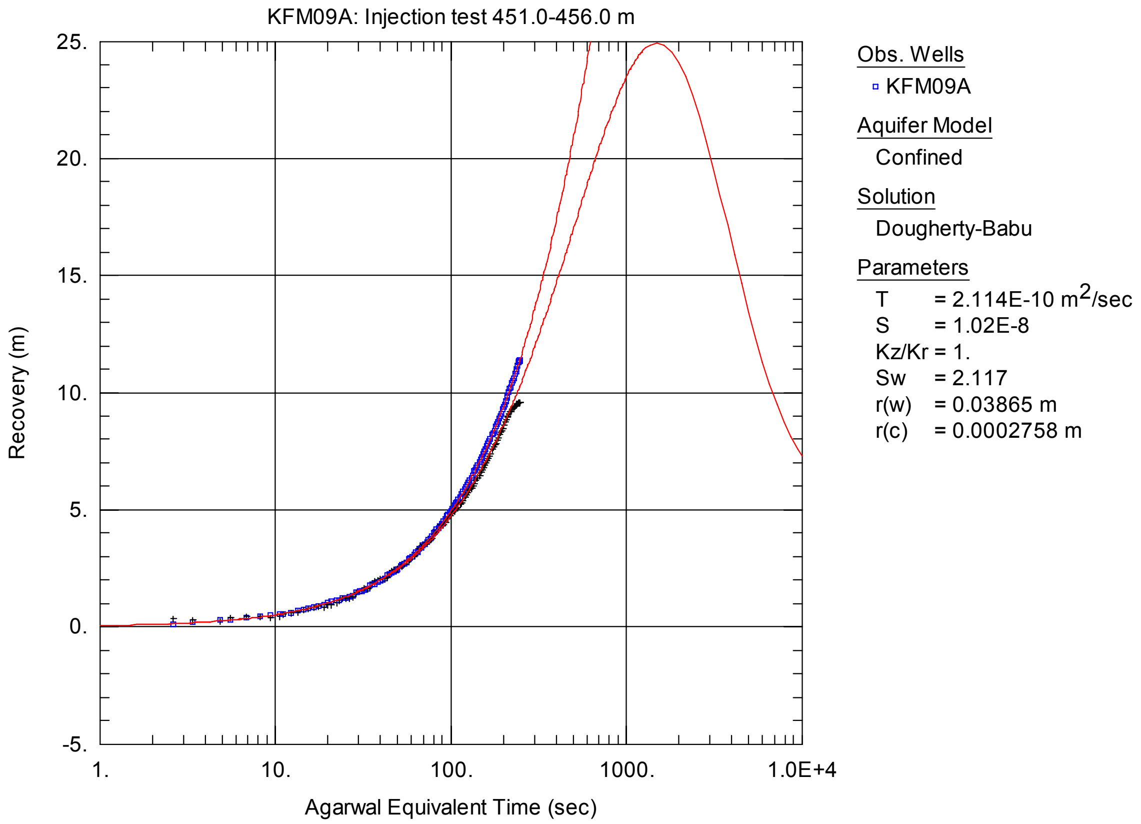


Figure A3-447. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 451.0-456.0 m in KFM09A.*

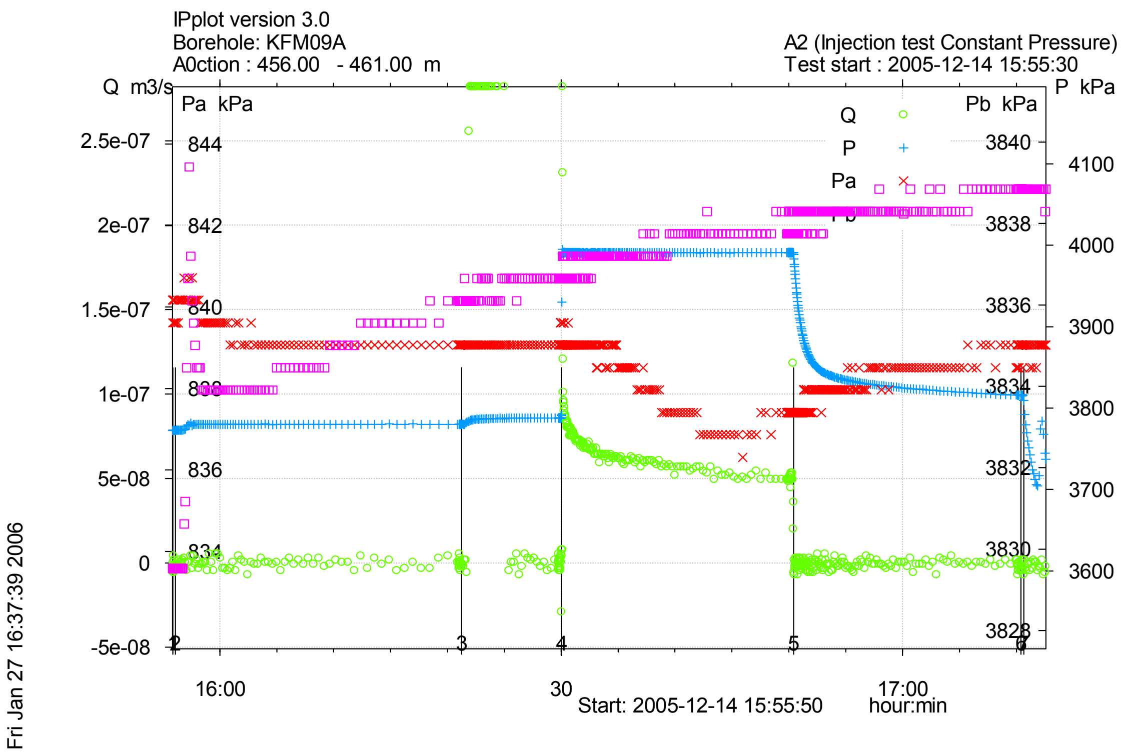


***Figure A3-448.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 456.0-461.0 m in borehole KFM09A.*

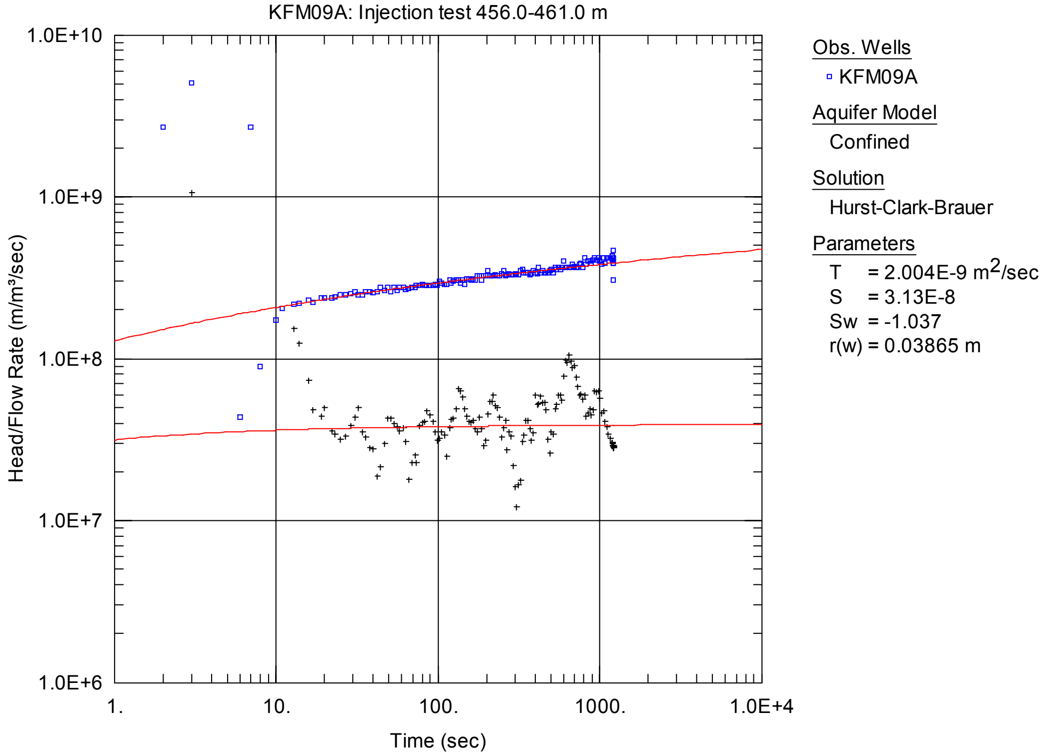


***Figure A3-449.** Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 456.0-461.0 m in KFM09A.*

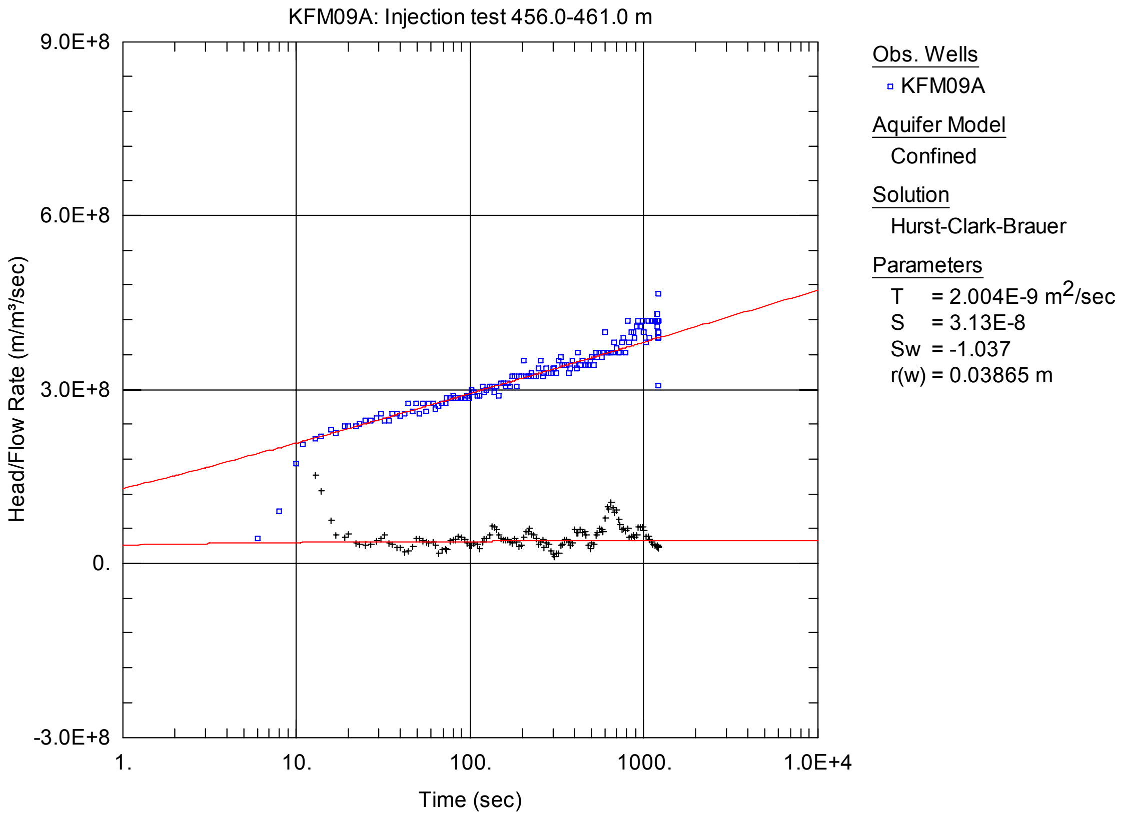


***Figure A3-450.** Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 456.0-461.0 m in KFM09A.*

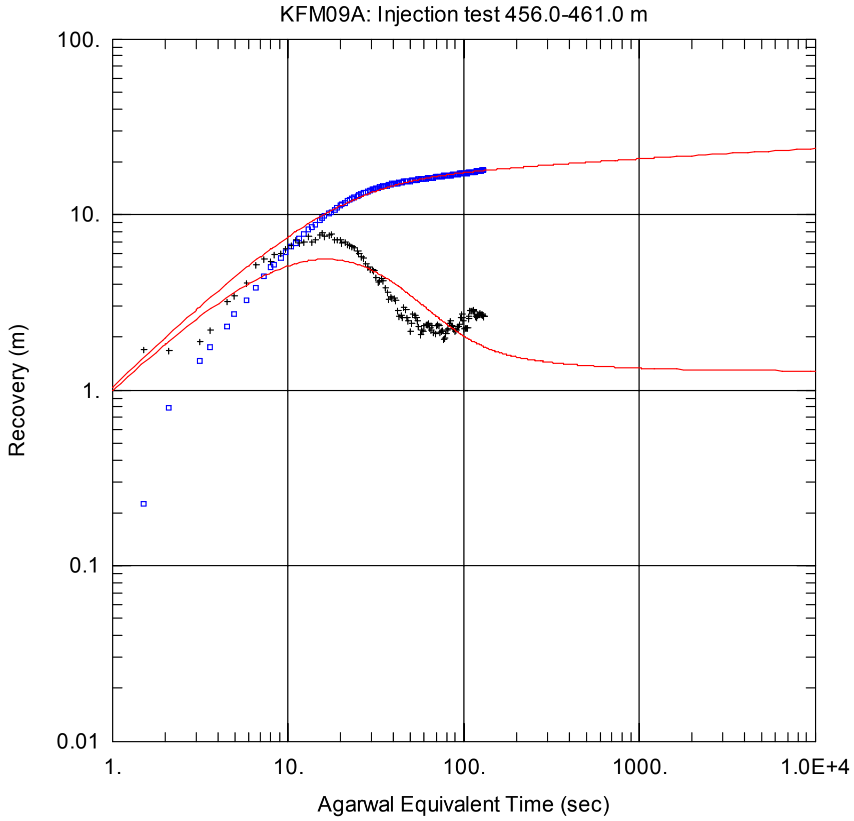


***Figure A3-451.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 456.0-461.0 m in KFM09A.*

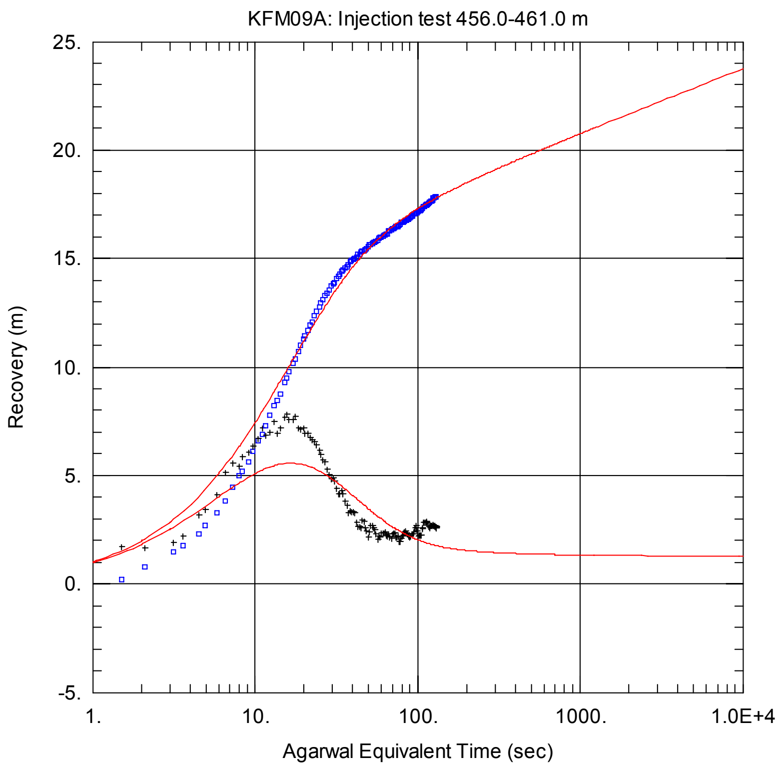


Figure A3-452. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 456.0-461.0 m in KFM09A.*

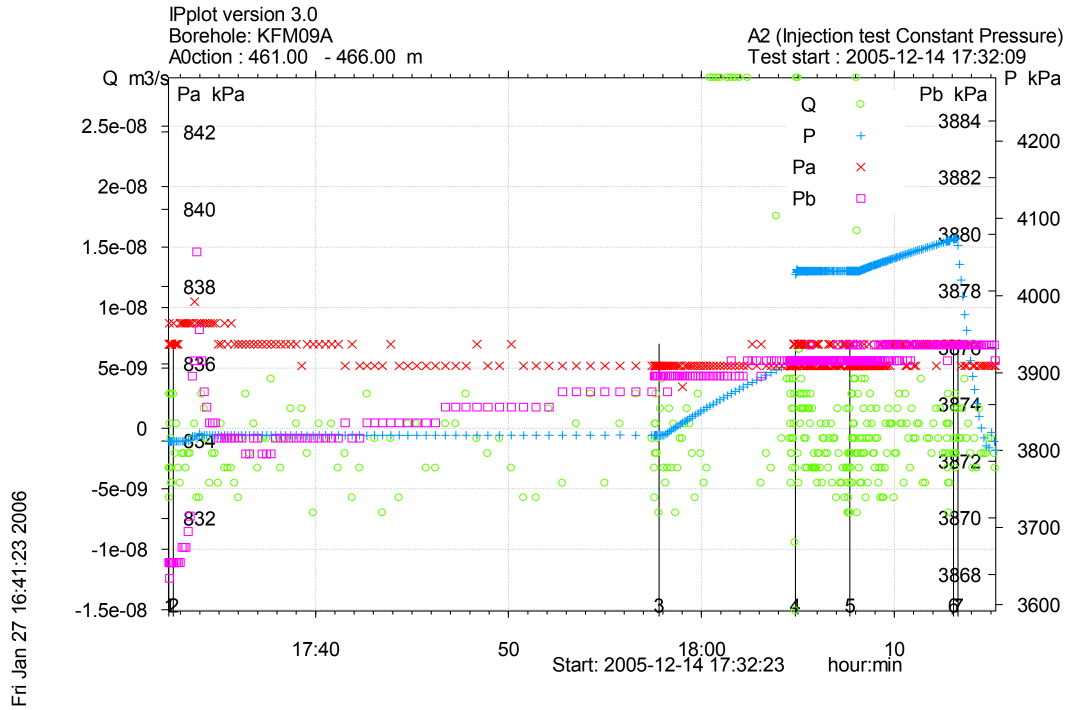


Figure A3-453. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 461.0-466.0 m in borehole KFM09A.*

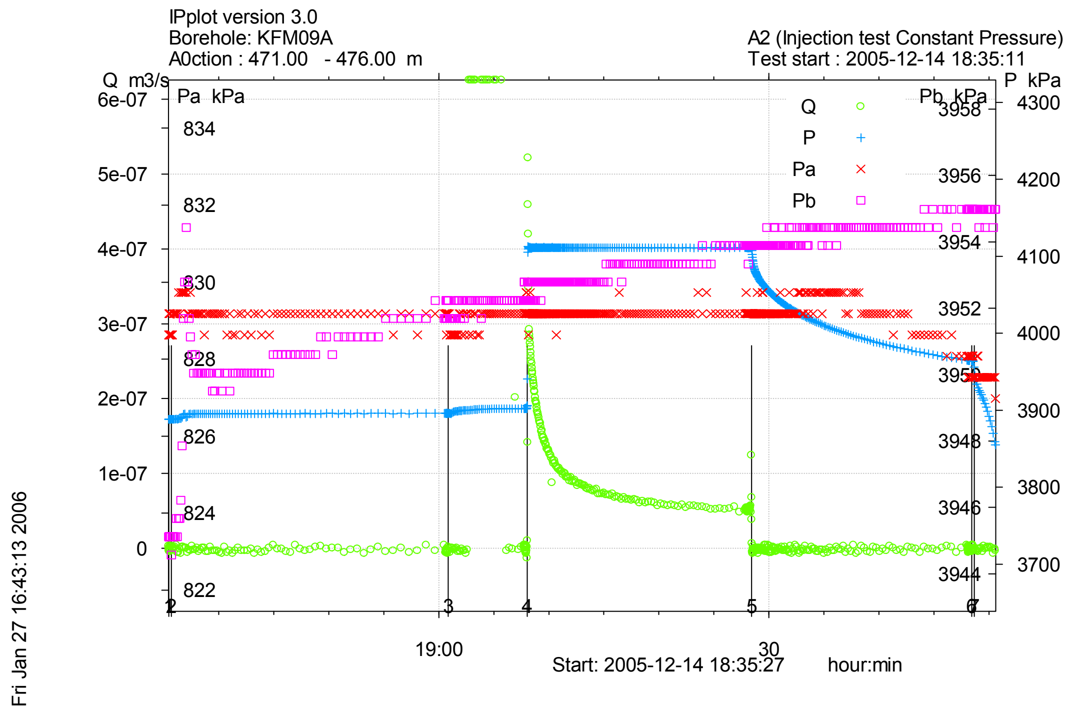


Figure A3-454. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 471.0-476.0 m in borehole KFM09A.

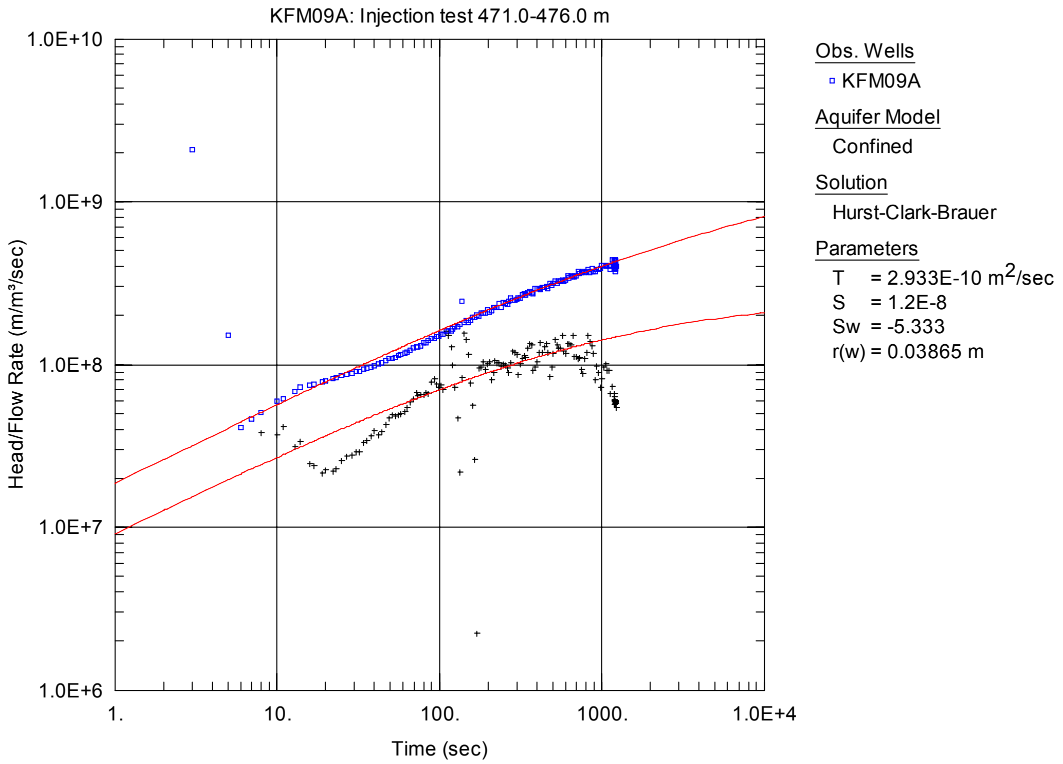


Figure A3-455. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 471.0-476.0 m in KFM09A.

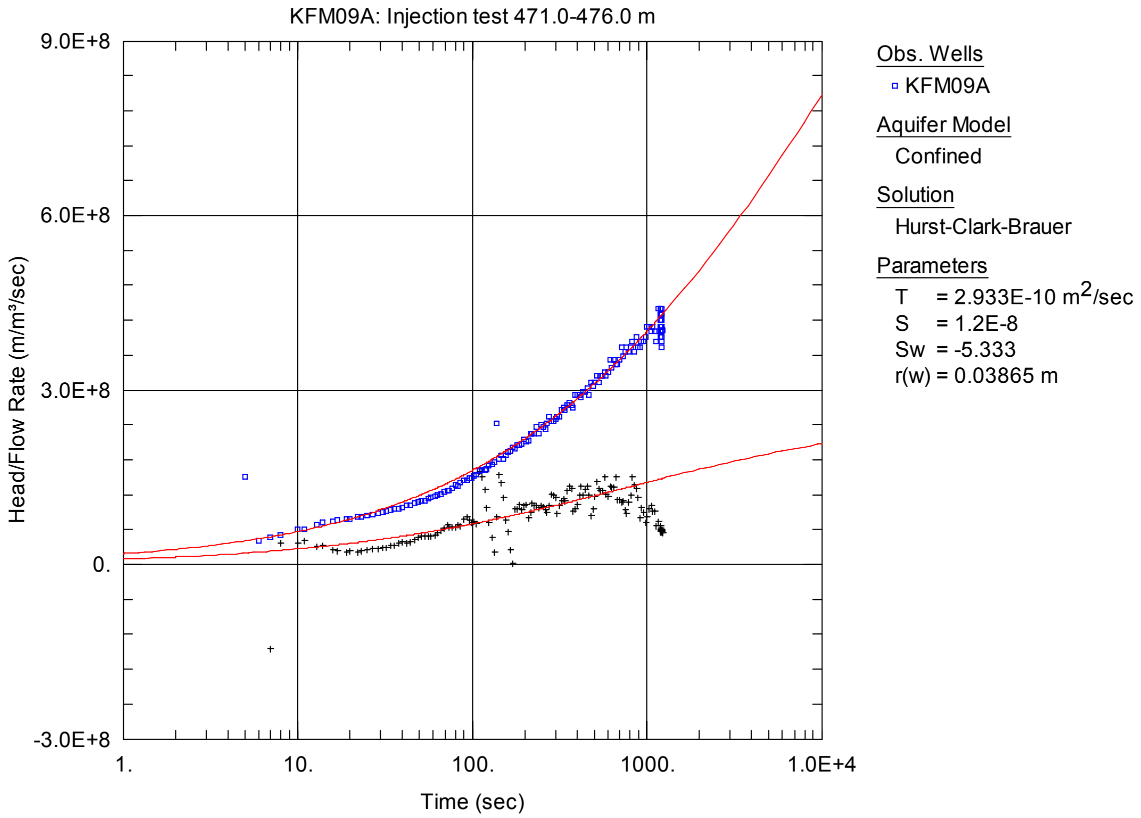


Figure A3-456. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 471.0-476.0 m in KFM09A.*

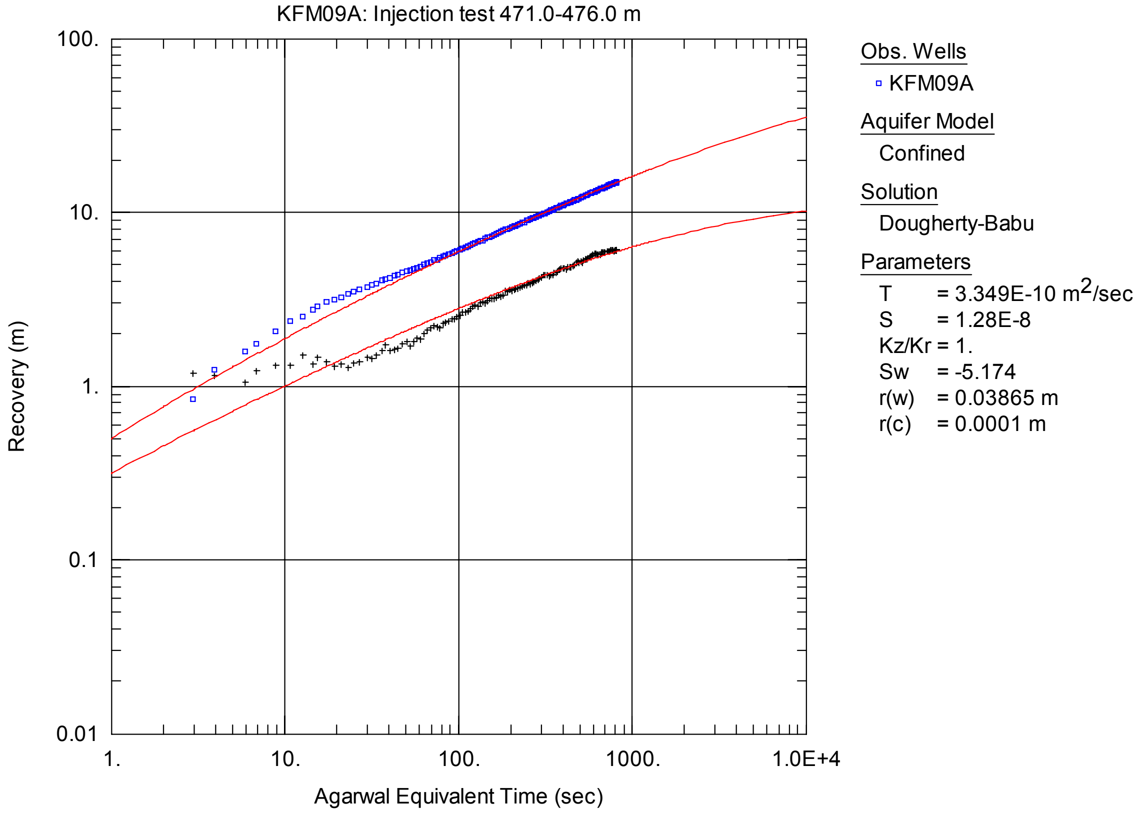


Figure A3-457. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 471.0-476.0 m in KFM09A.*

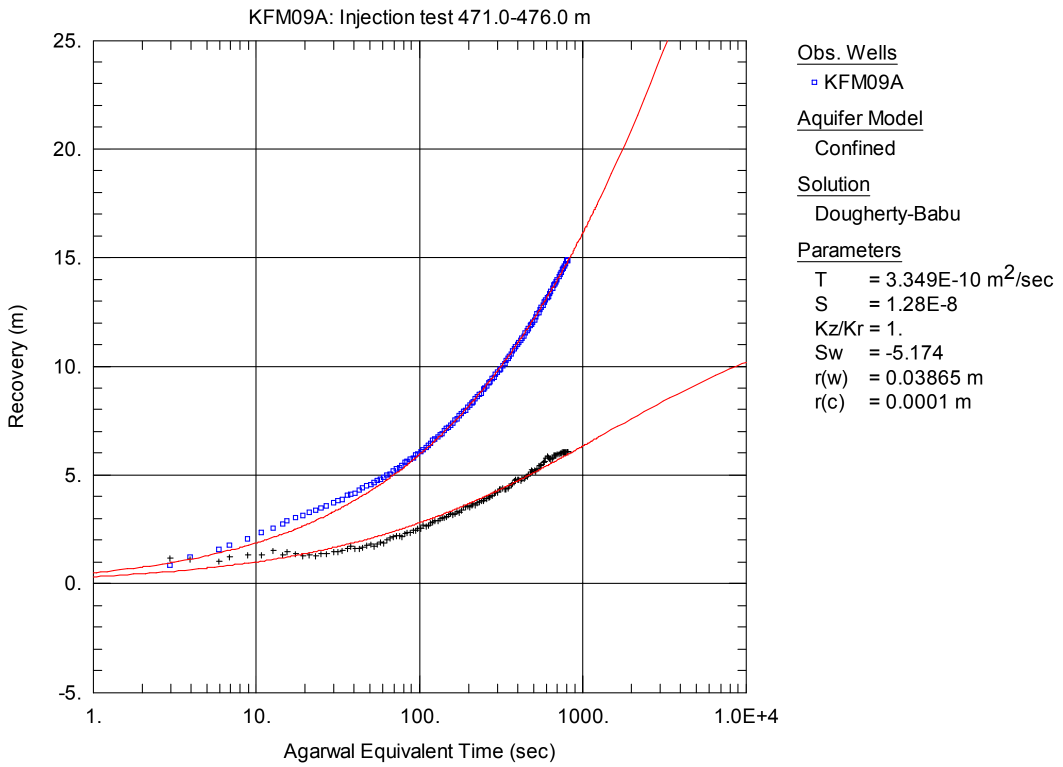


Figure A3-458. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 471.0-476.0 m in KFM09A.*

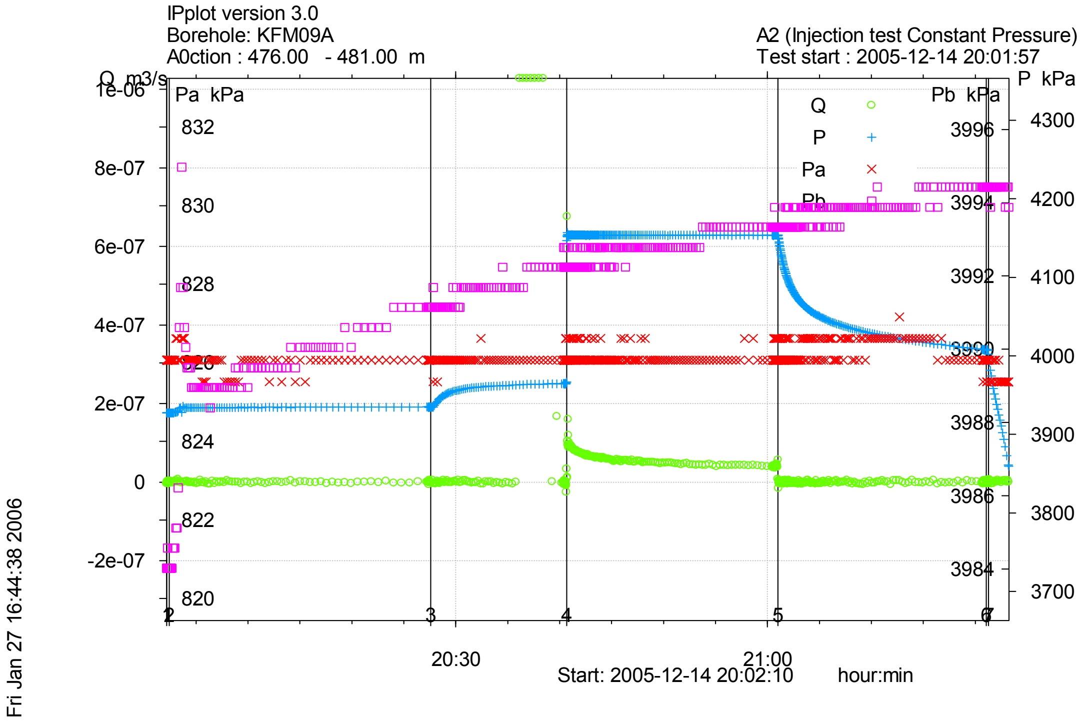


Figure A3-459. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 476.0-481.0 m in borehole KFM09A.*

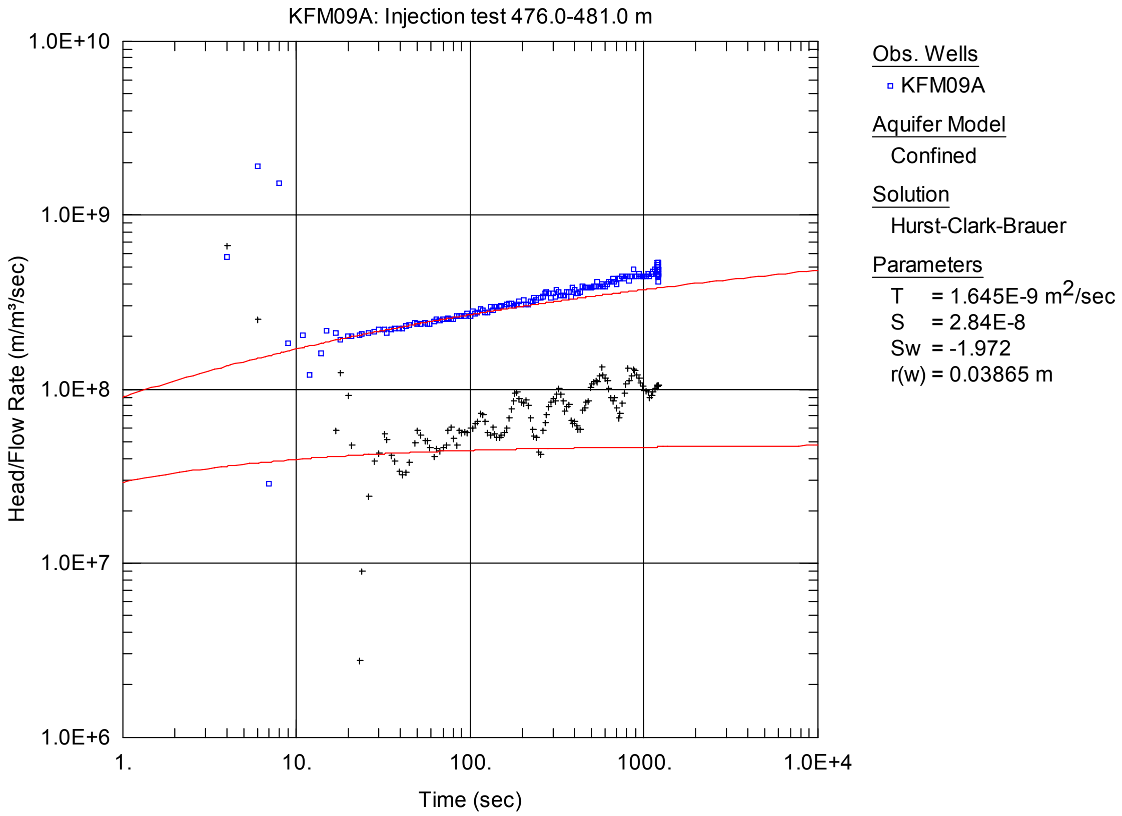


Figure A3-460. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 476.0-481.0 m in KFM09A.

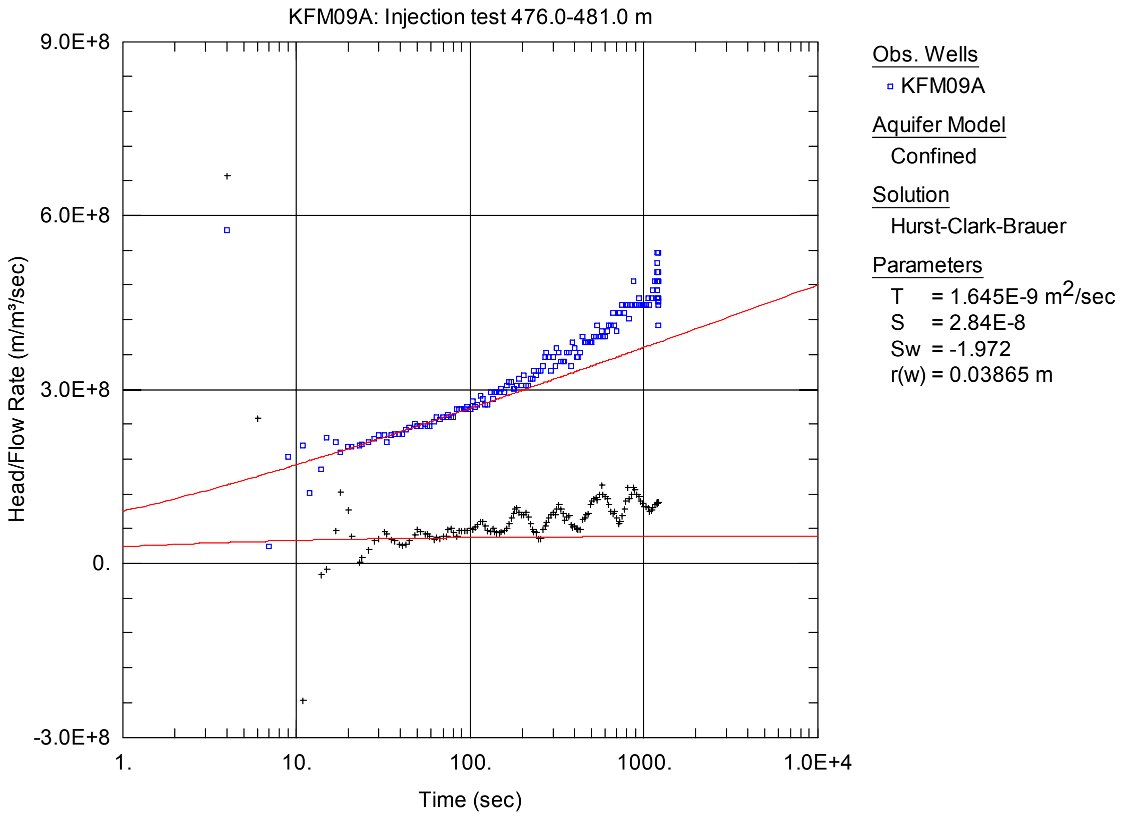


Figure A3-461. Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 476.0-481.0 m in KFM09A.

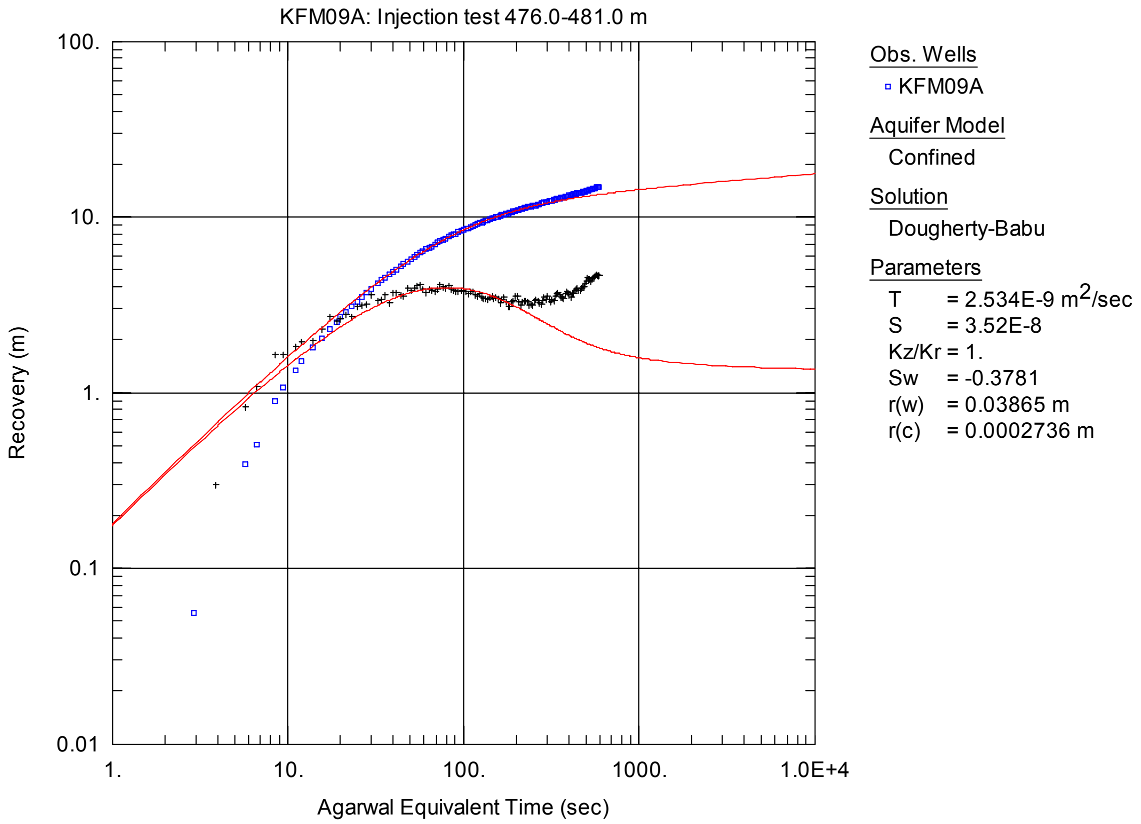


***Figure A3-462.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 476.0-481.0 m in KFM09A.*

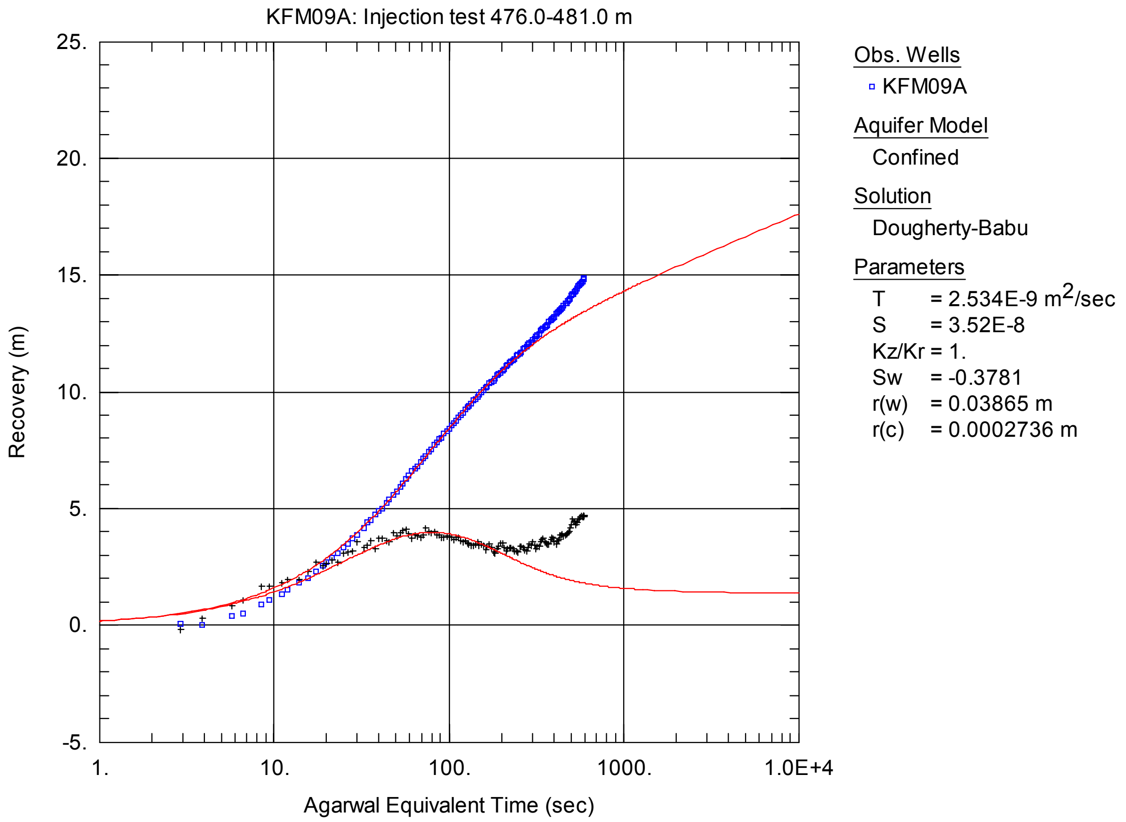


***Figure A3-463.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 476.0-481.0 m in KFM09A.*

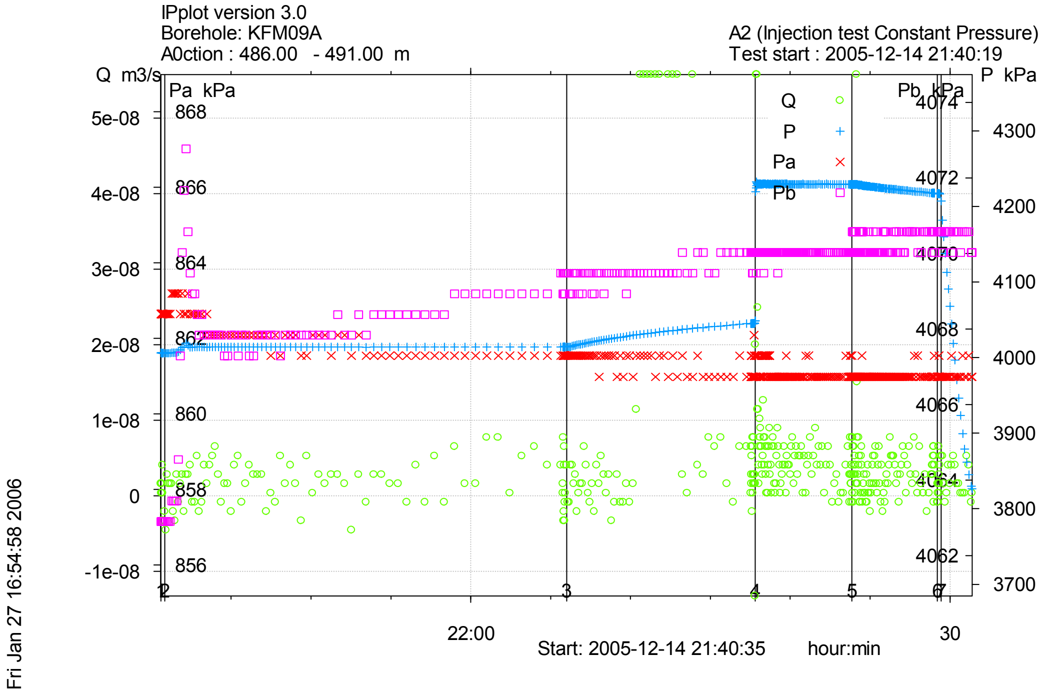


Figure A3-464. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 486.0-491.0 m in borehole KFM09A.*

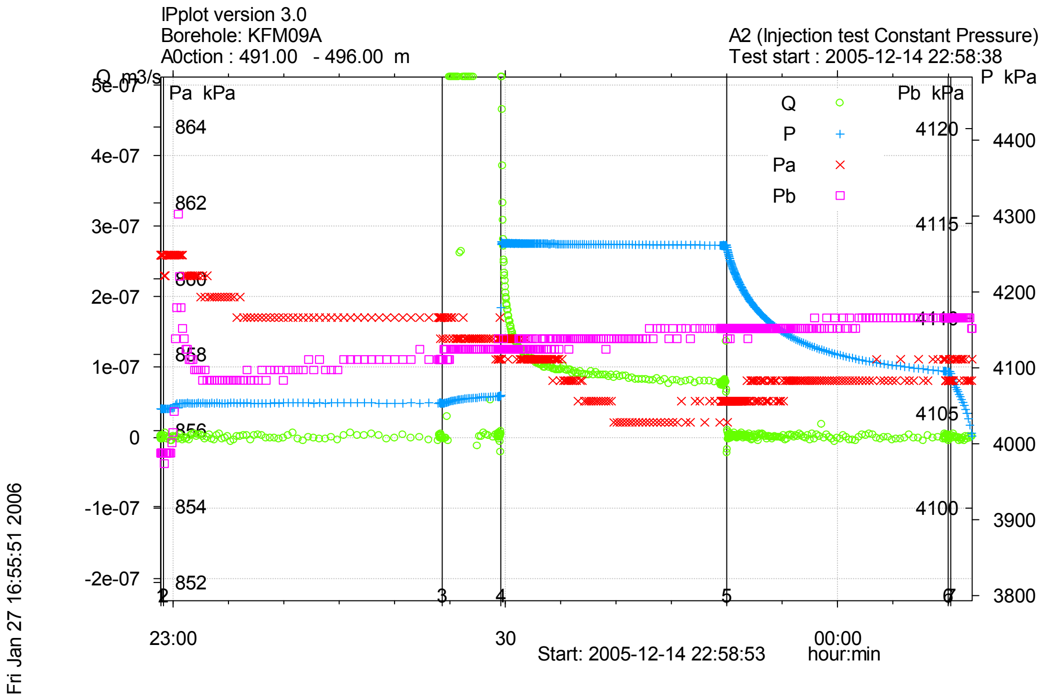


Figure A3-465. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 491.0-496.0 m in borehole KFM09A.*

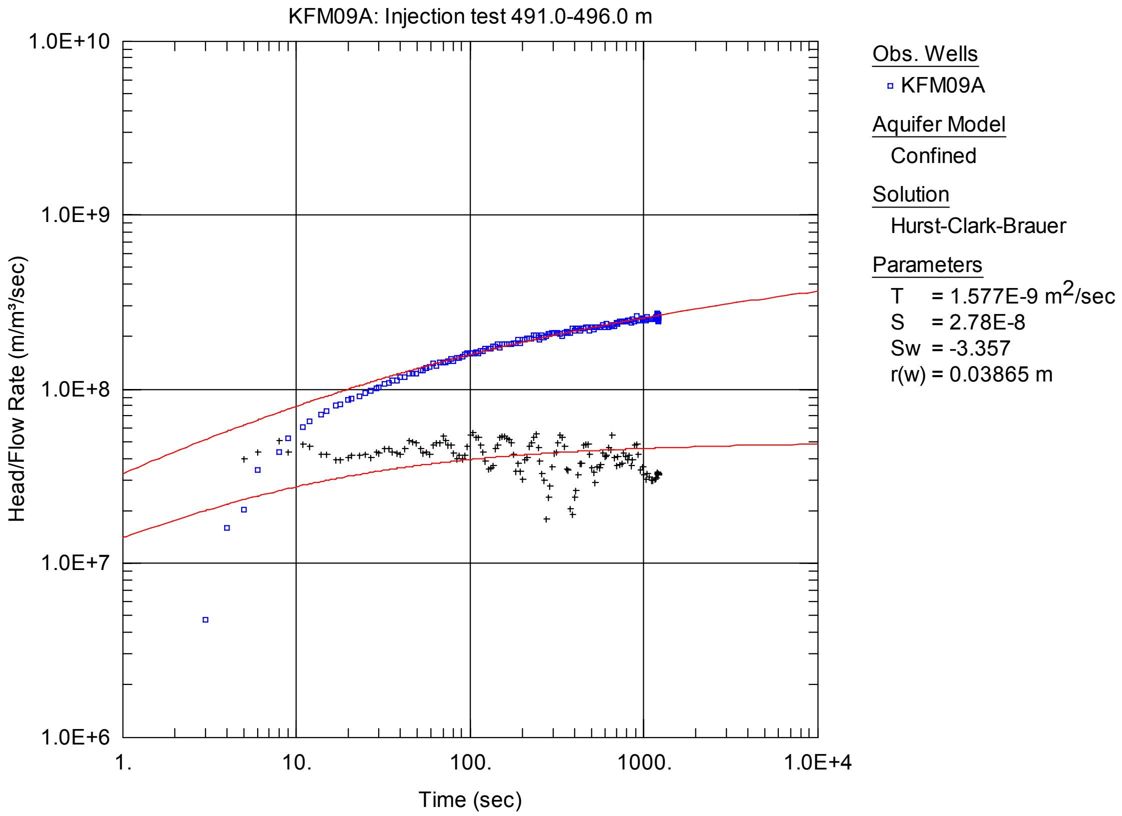


Figure A3-466. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 491.0-496.0 m in KFM09A.*

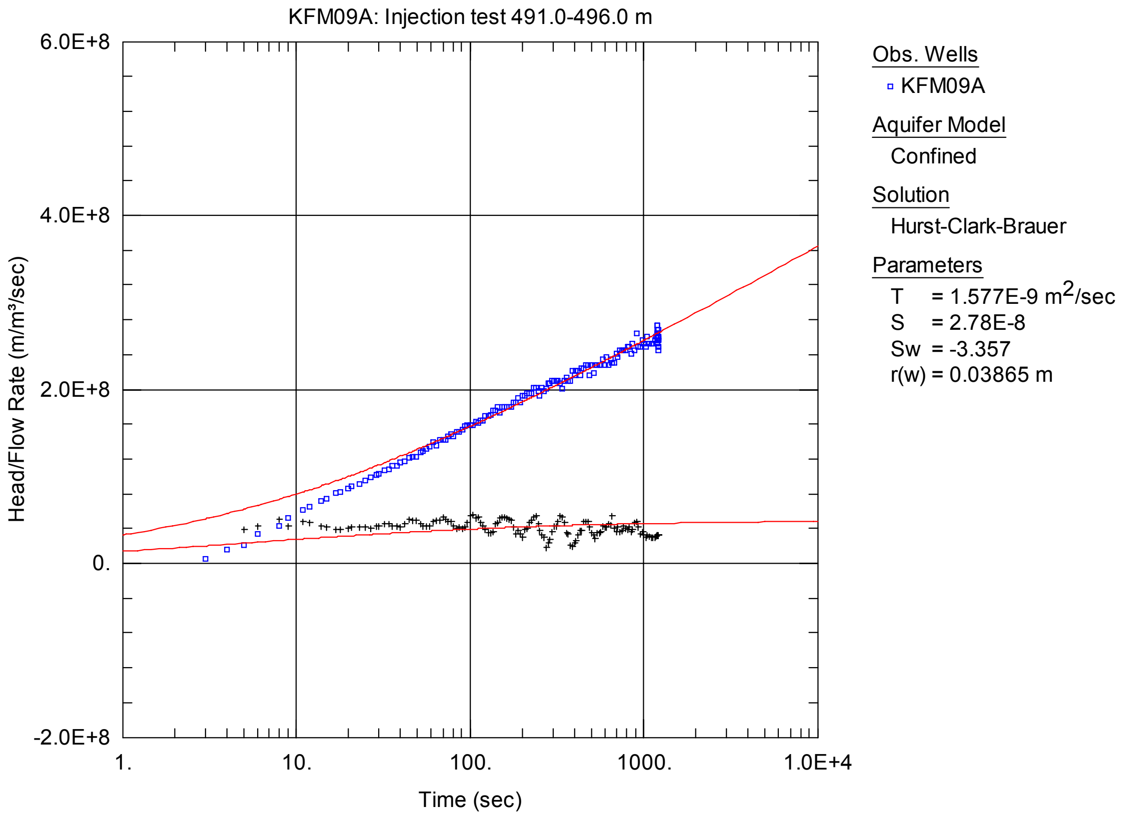


Figure A3-467. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 491.0-496.0 m in KFM09A.*

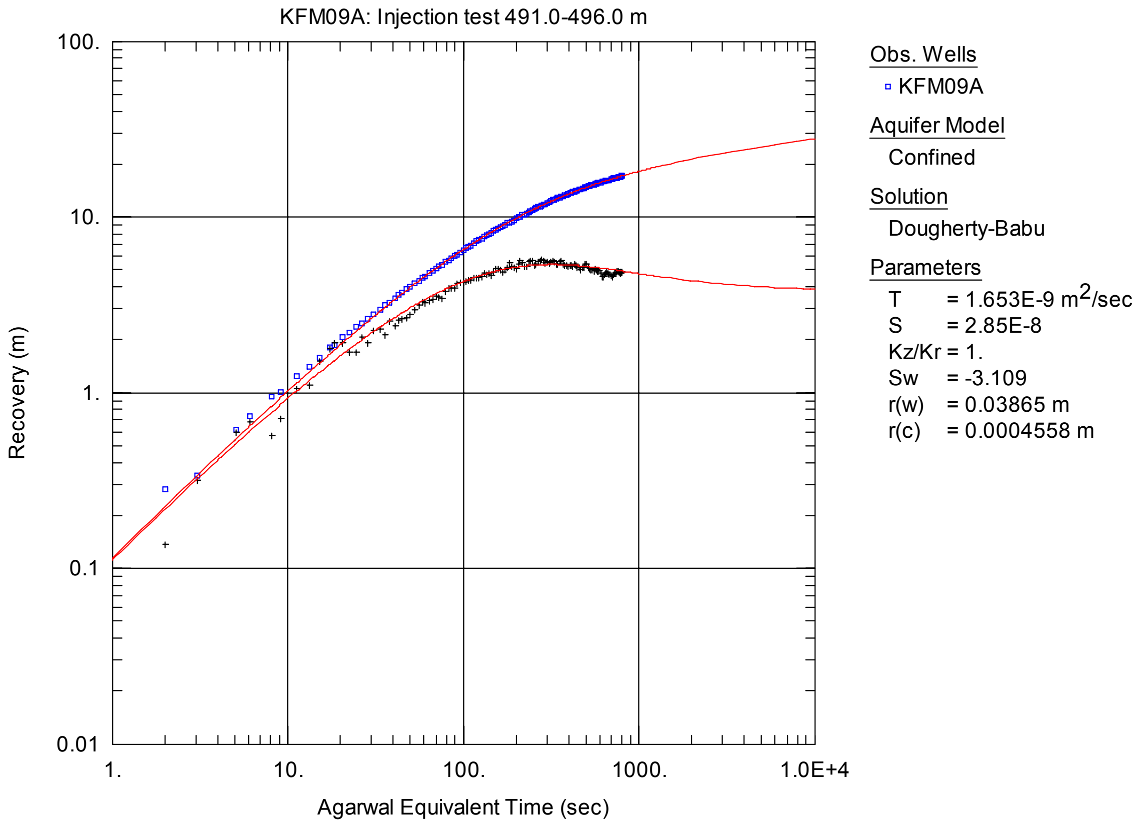


***Figure A3-468.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 491.0-496.0 m in KFM09A.*

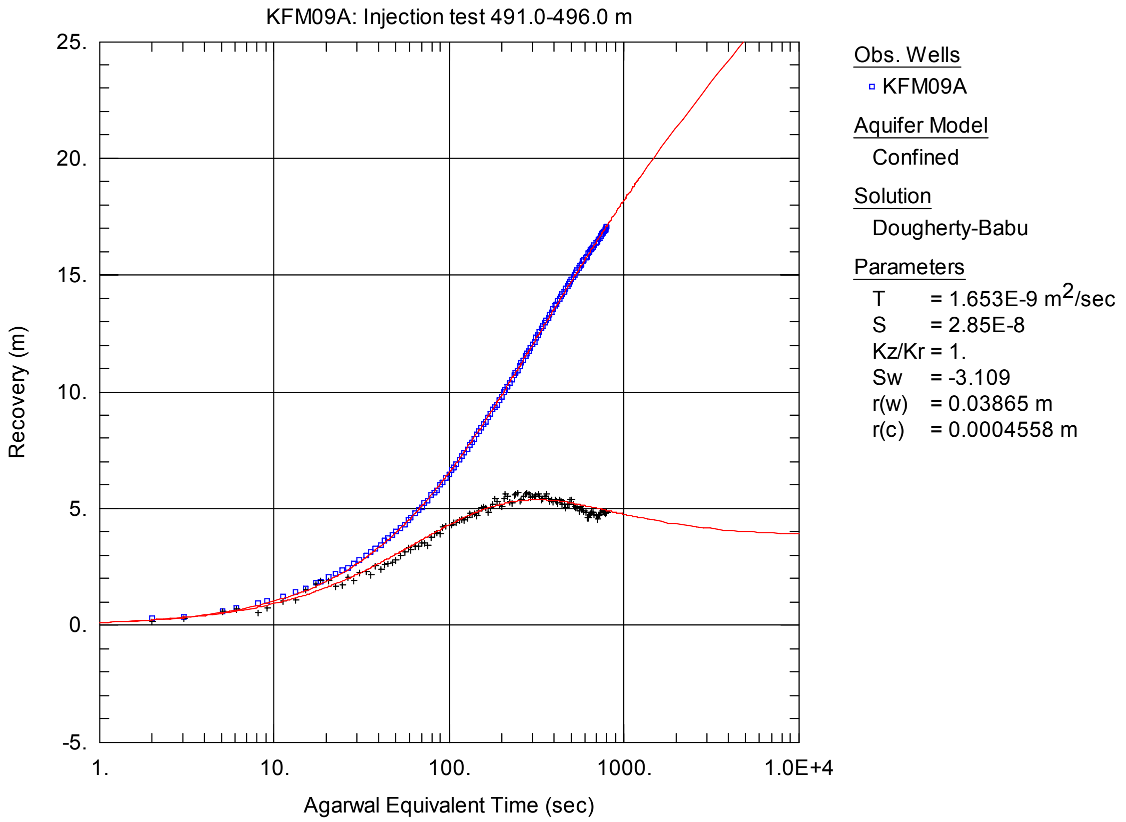


***Figure A3-469.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 491.0-496.0 m in KFM09A.*

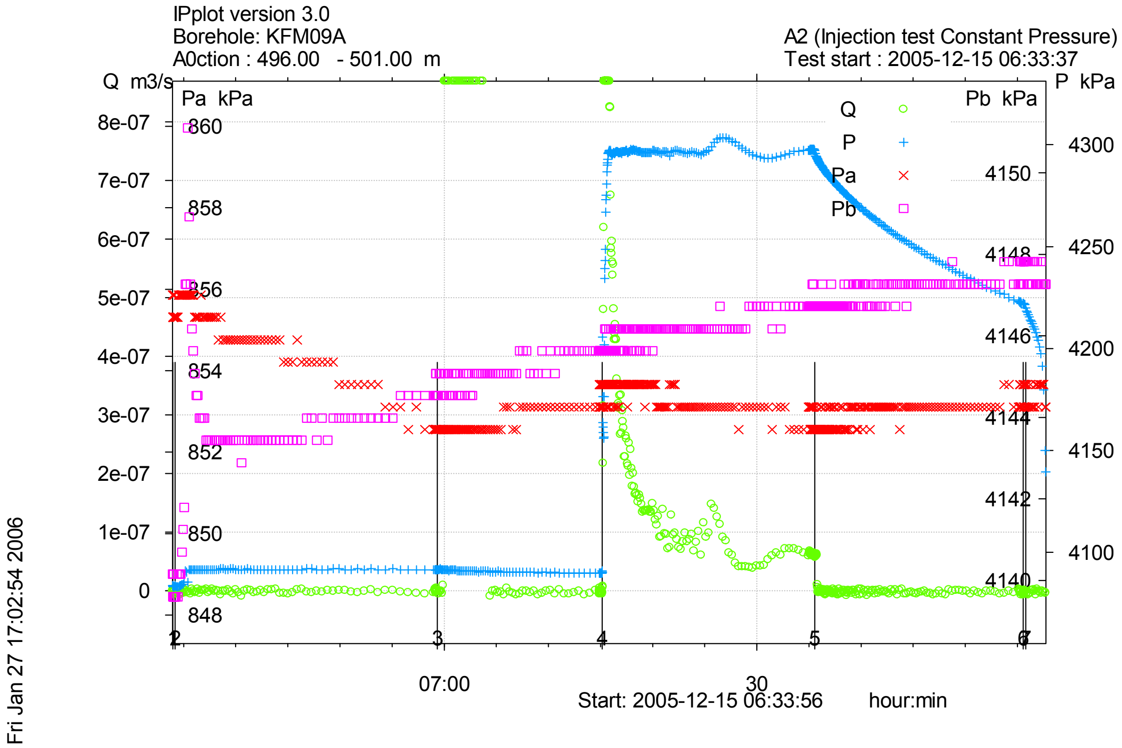


Figure A3-470. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 496.0-501.0 m in borehole KFM09A.*

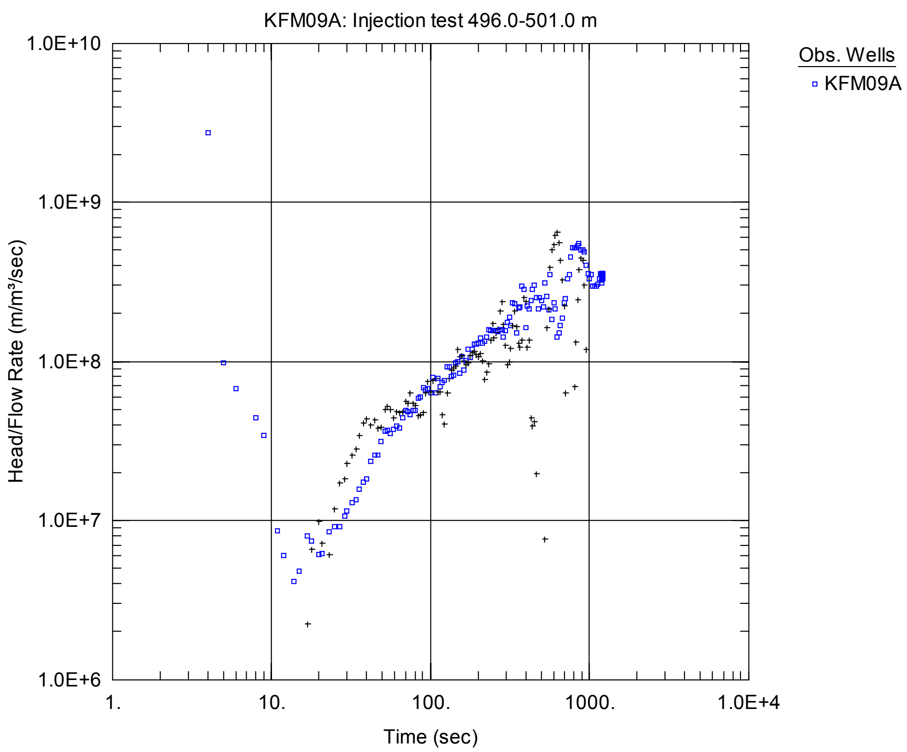


Figure A3-471. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 496.0-501.0 m in KFM09A.*

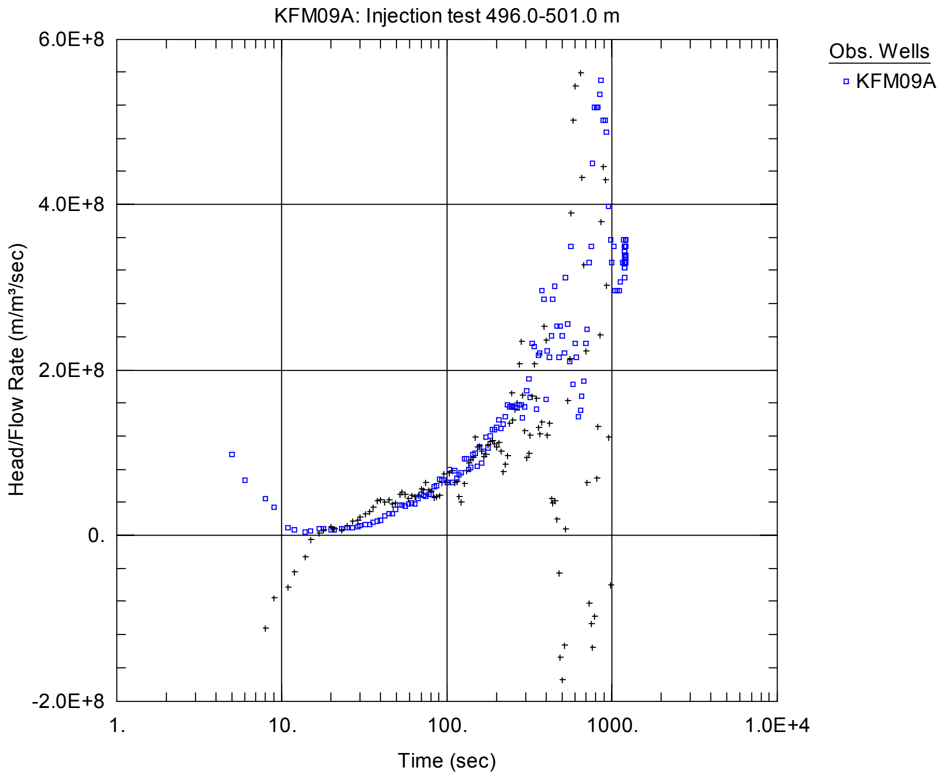


***Figure A3-472.** Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 496.0-501.0 m in KFM09A.*

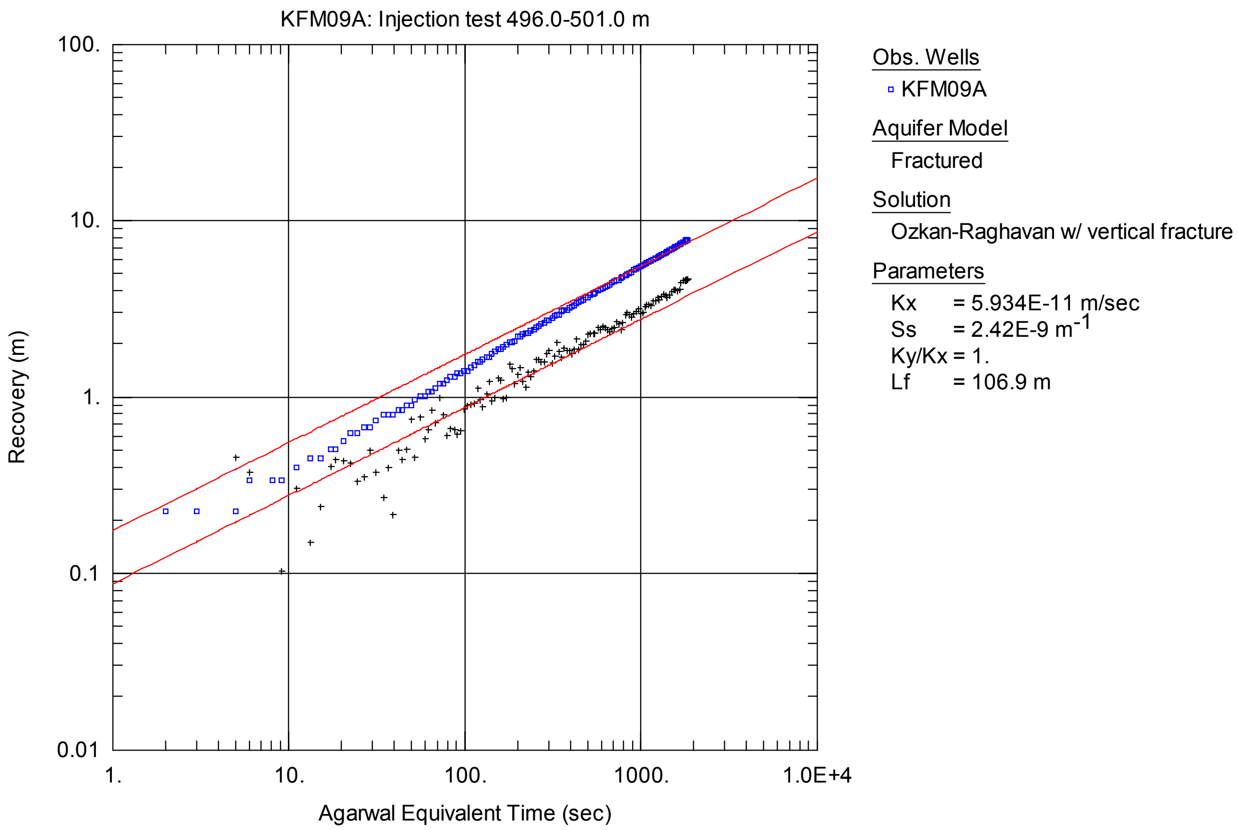


***Figure A3-473.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 496.0-501.0 m in KFM09A.*

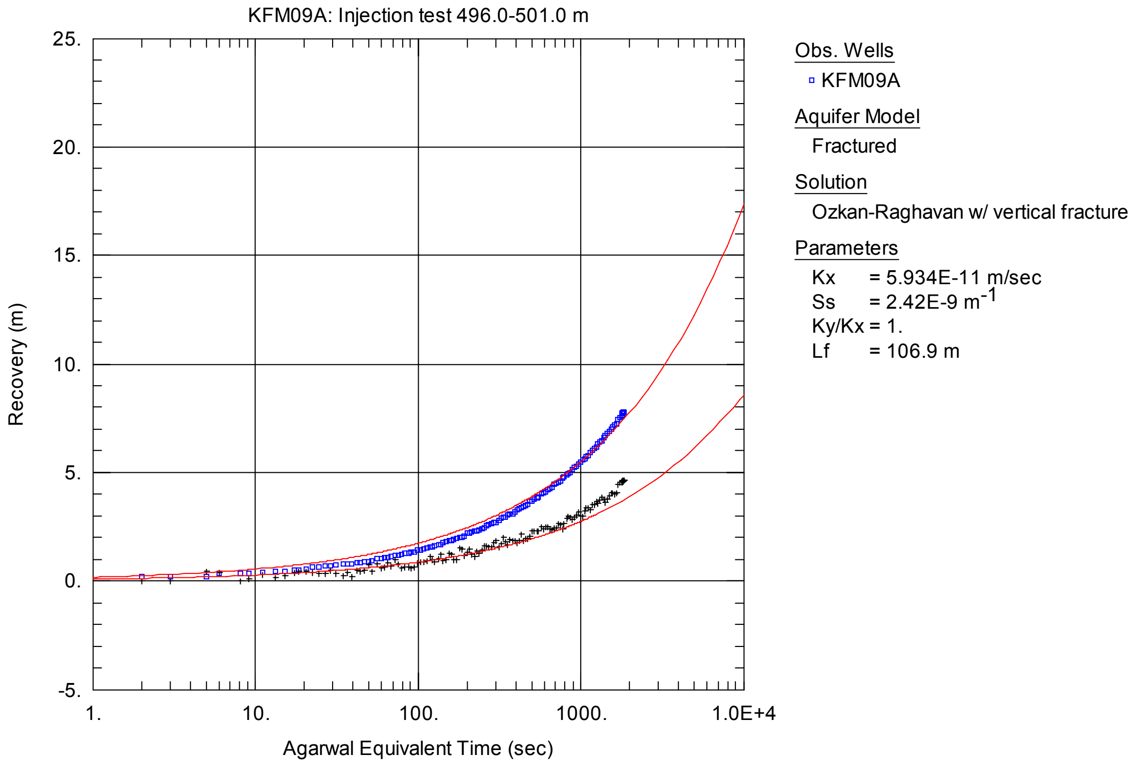


Figure A3-474. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 496.0-501.0 m in KFM09A.*

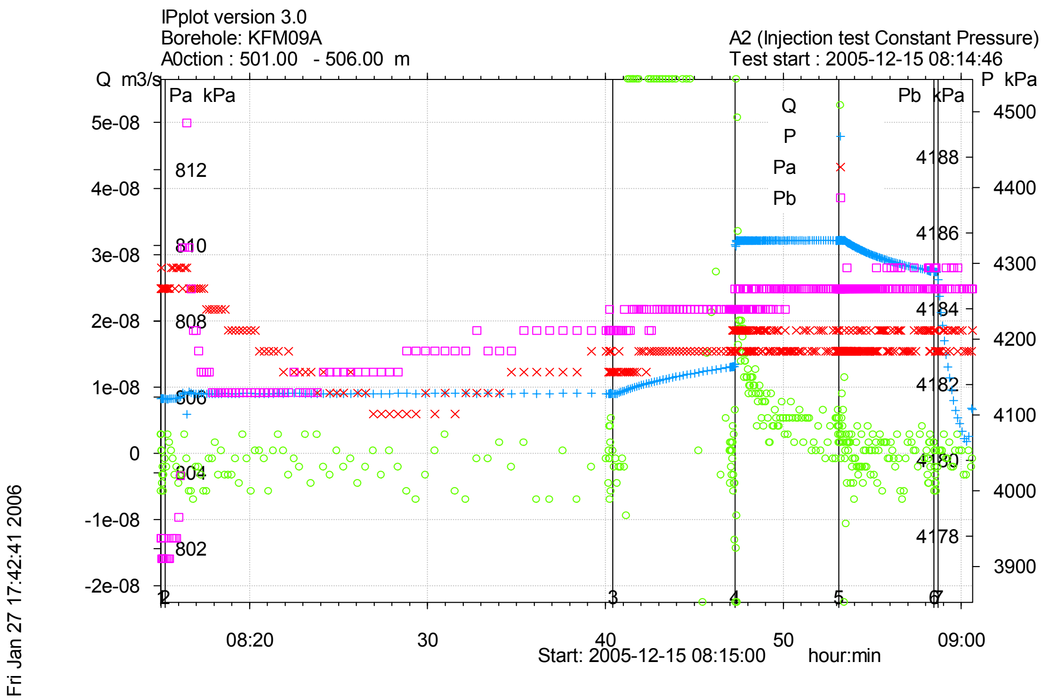


Figure A3-475. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 501.0-506.0 m in borehole KFM09A.*

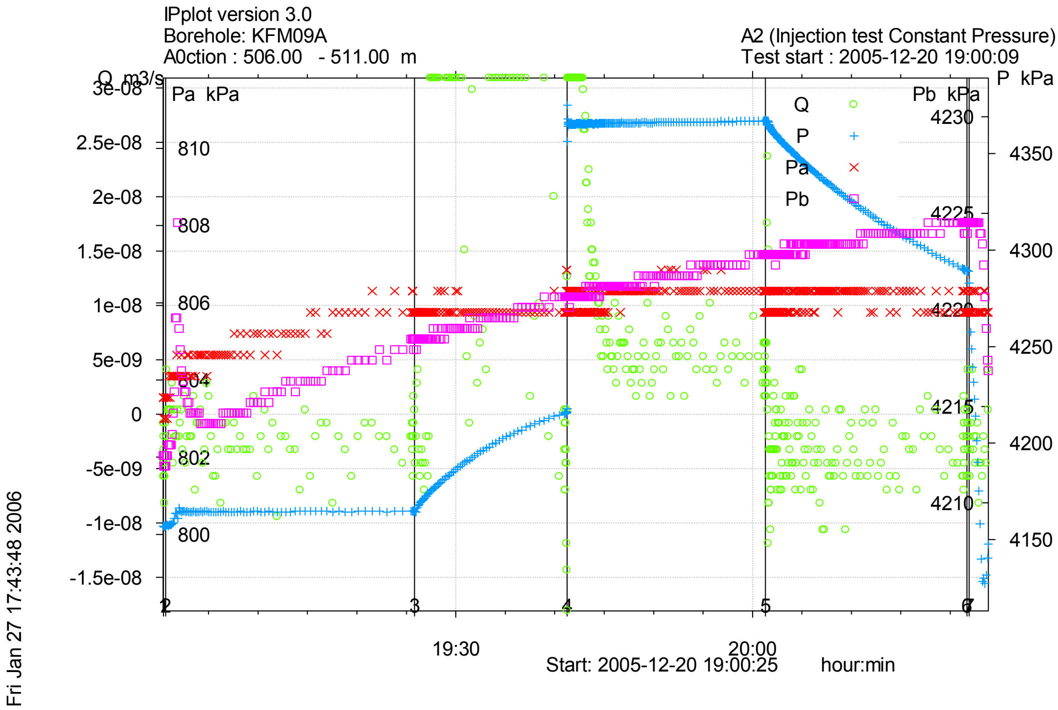


Figure A3-476. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 506.0-511.0 m in borehole KFM09A.

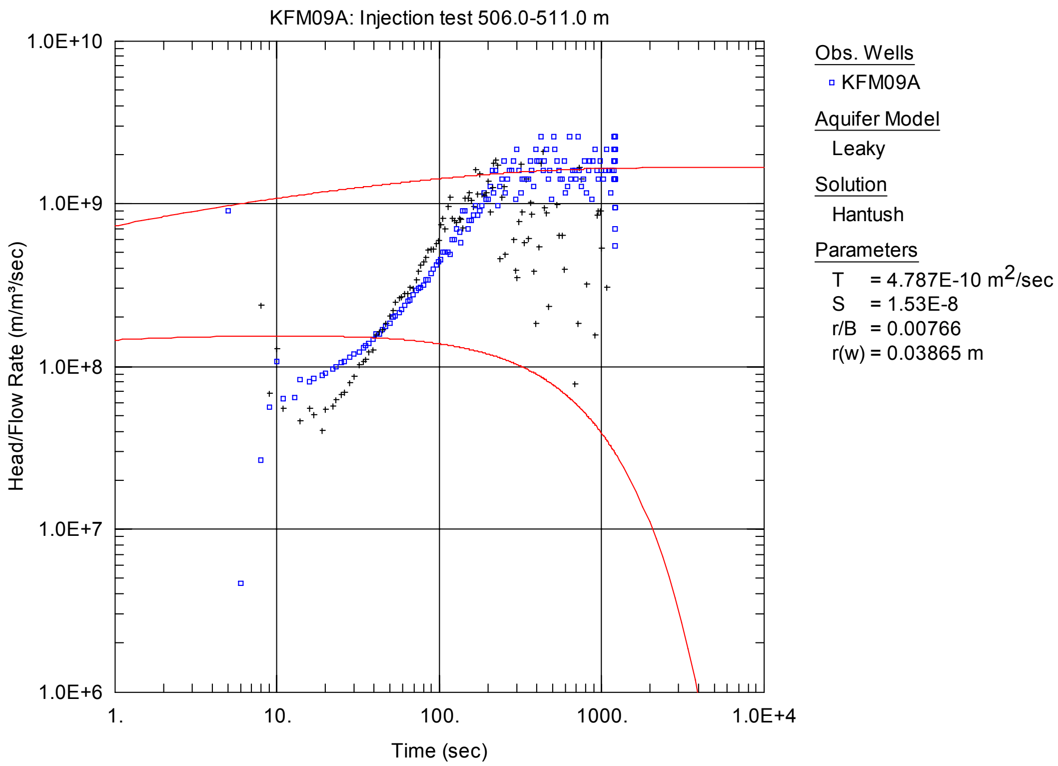


Figure A3-477. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 506.0-511.0 m in KFM09A.

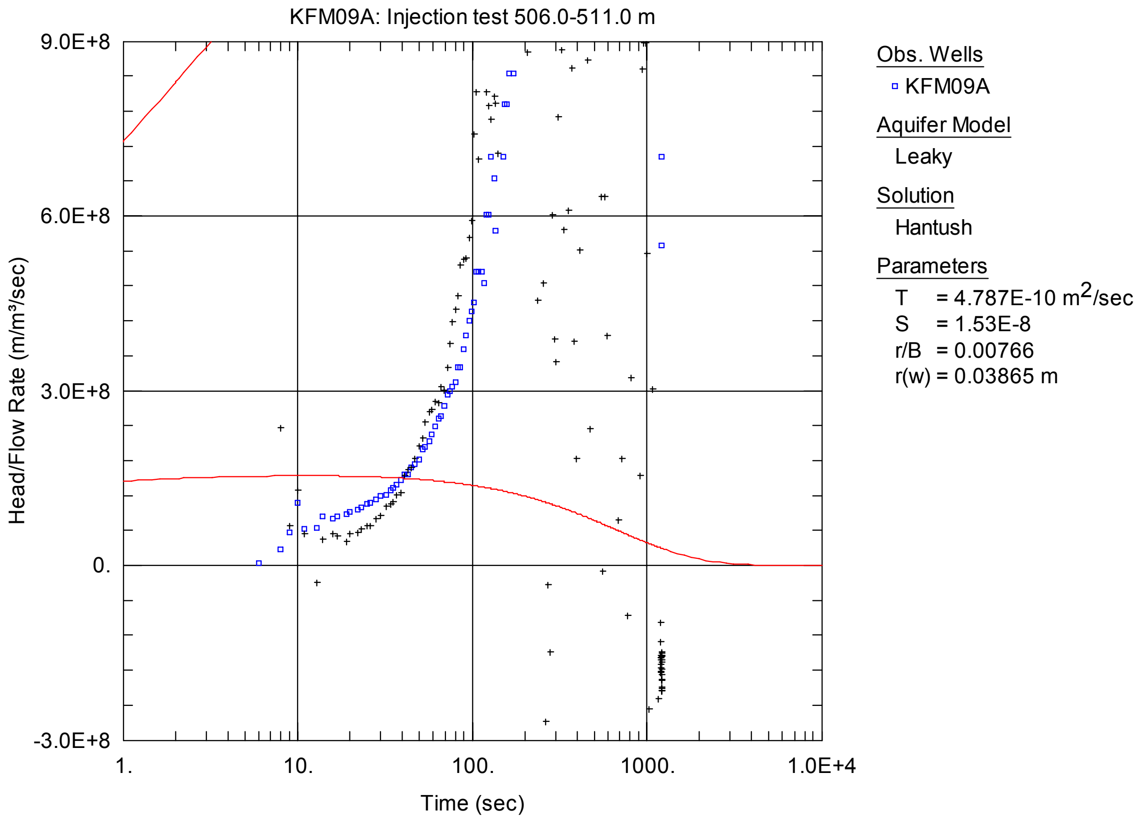


Figure A3-478. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 506.0-511.0 m in KFM09A.*

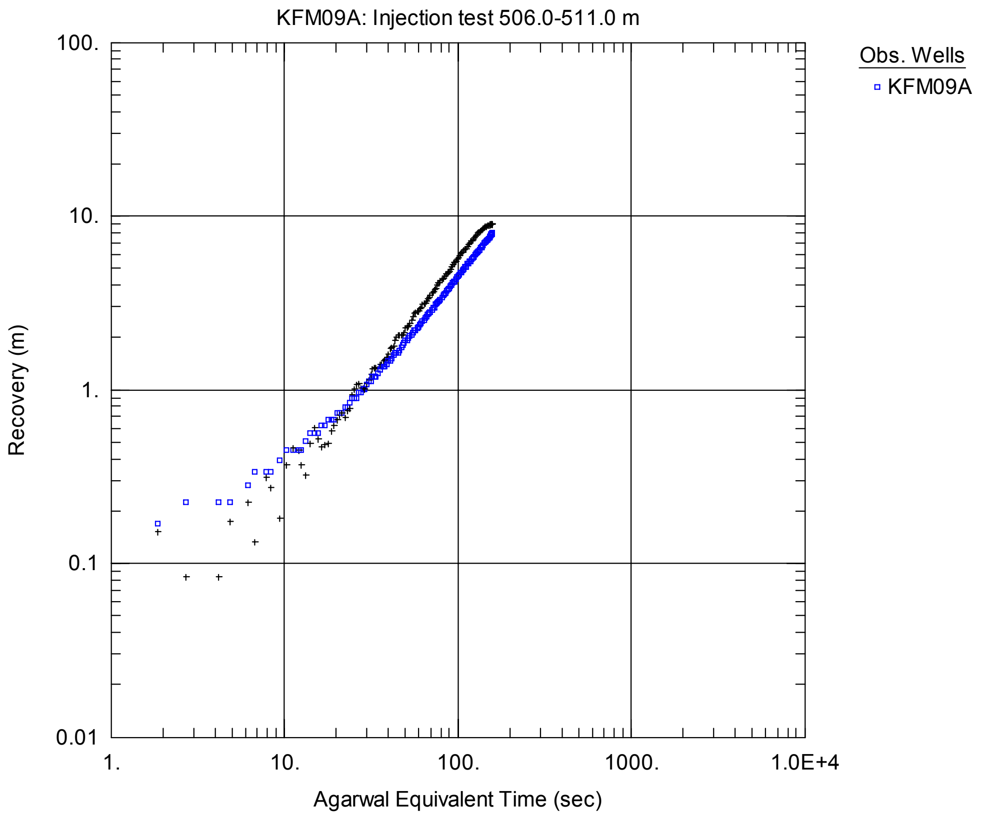


Figure A3-479. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 506.0-511.0 m in KFM09A.*

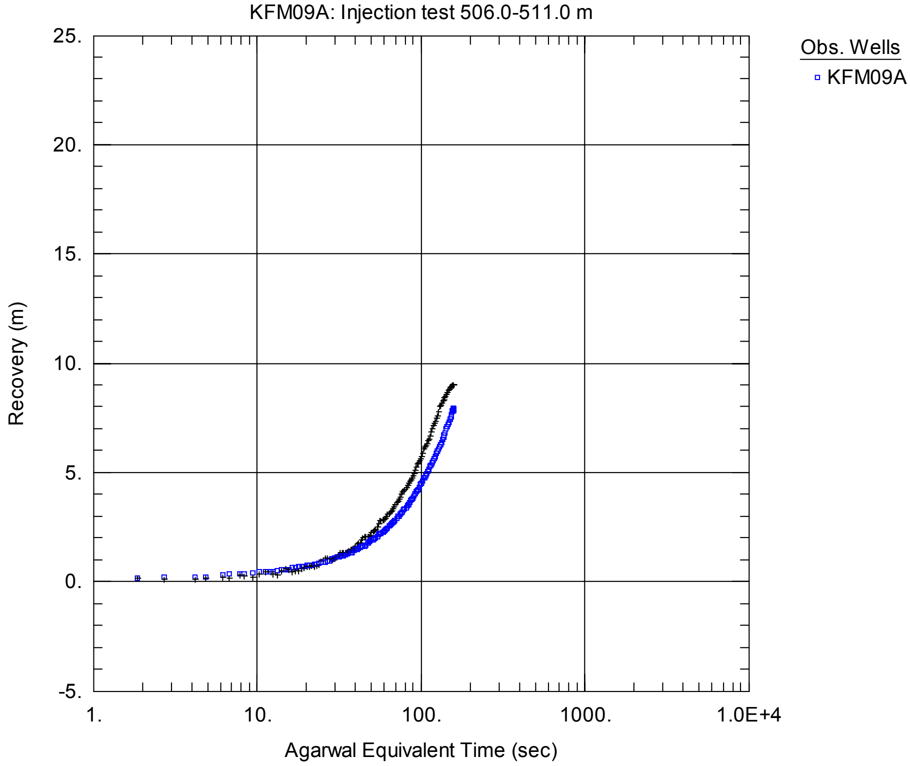


Figure A3-480. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 506.0-511.0 m in KFM09A.*

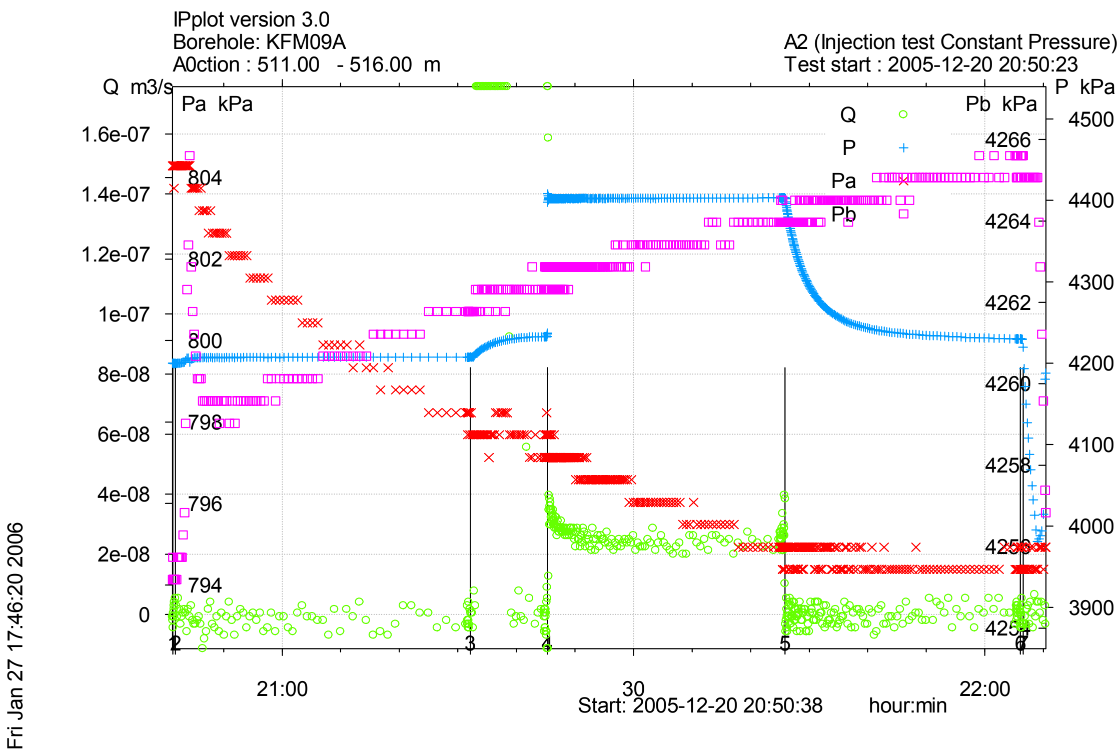


Figure A3-481. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 511.0-516.0 m in borehole KFM09A.*

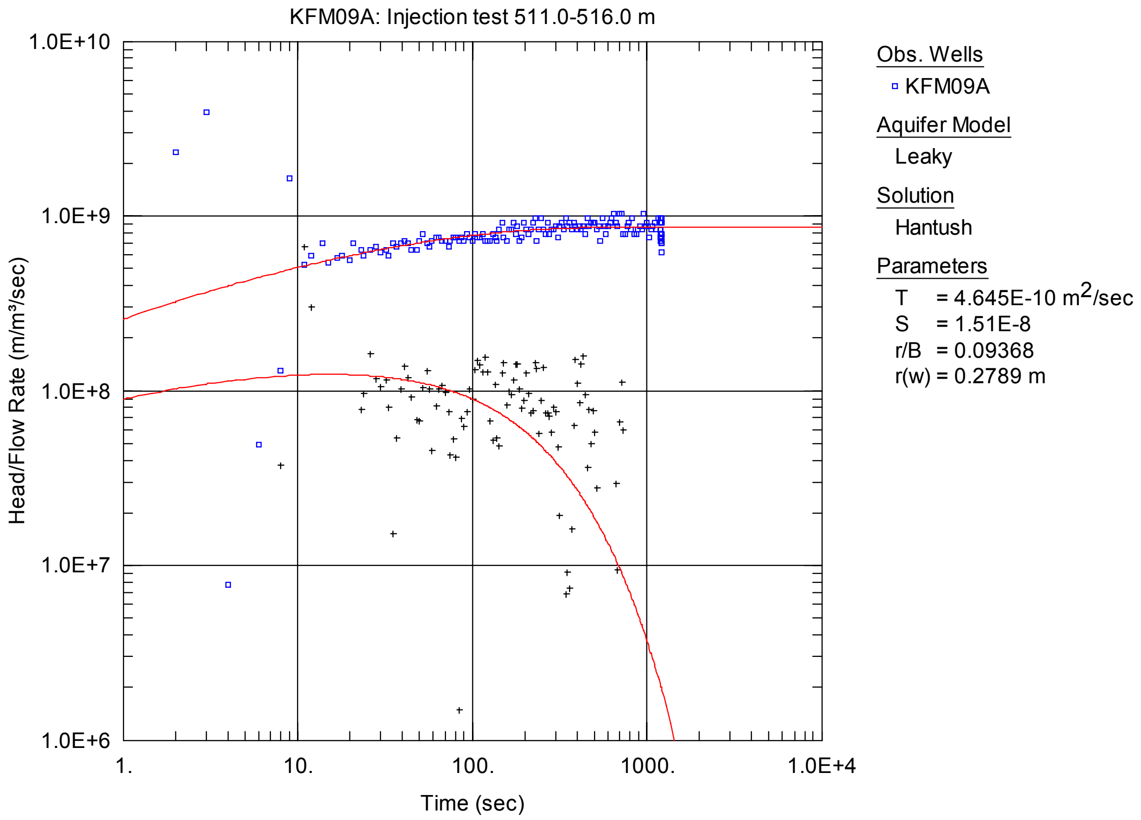


Figure A3-482. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 511.0-516.0 m in KFM09A.*

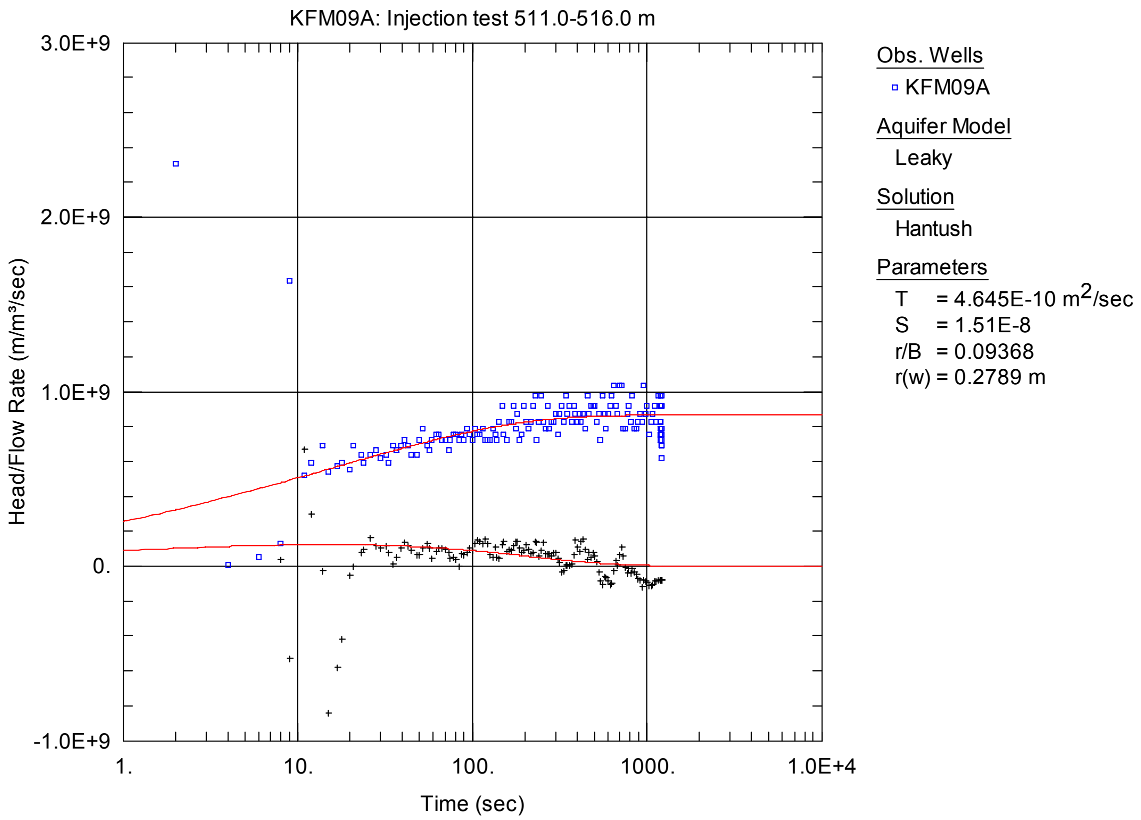


Figure A3-483. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 511.0-516.0 m in KFM09A.*

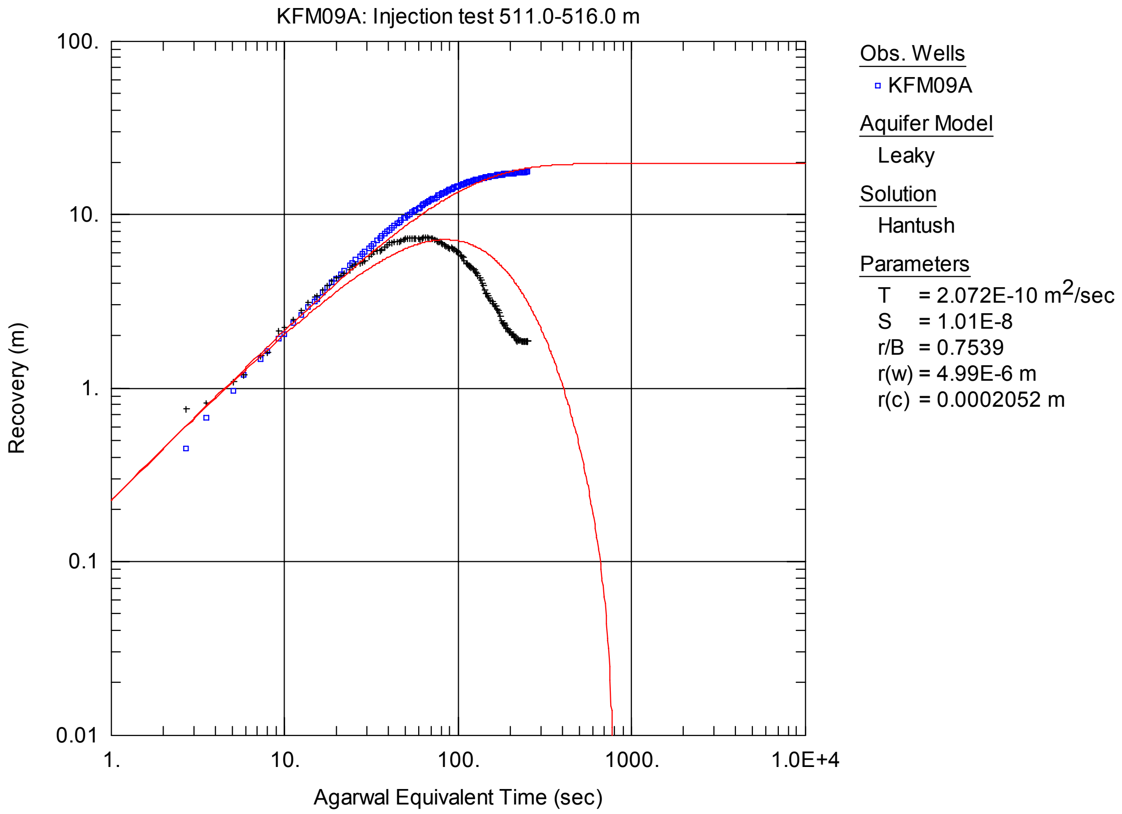


***Figure A3-484.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 511.0-516.0 m in KFM09A.*

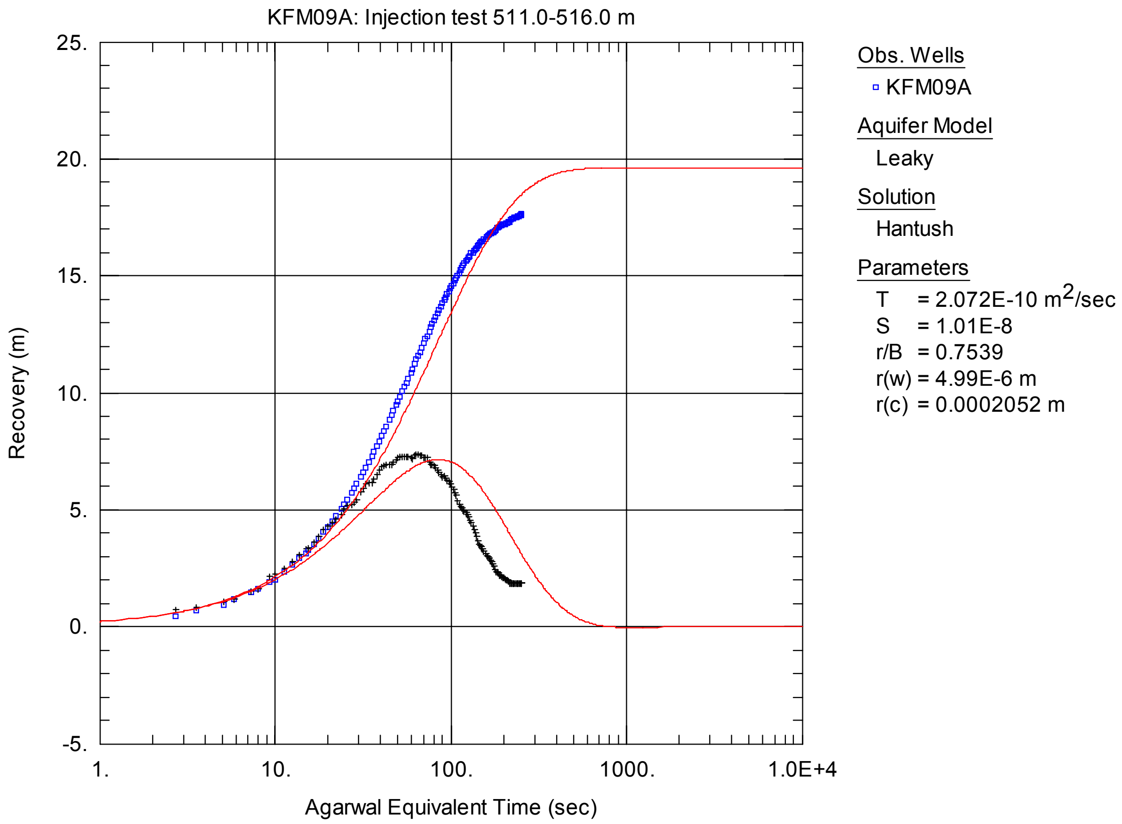


***Figure A3-485.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 511.0-516.0 m in KFM09A.*

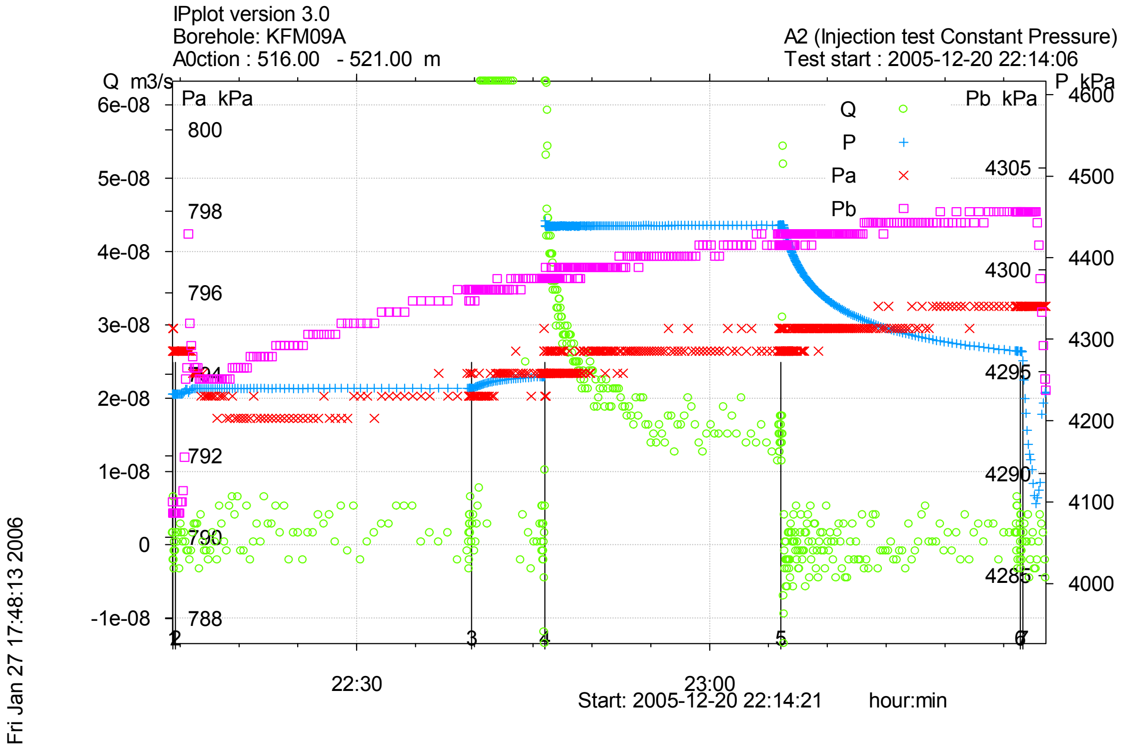


***Figure A3-486.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 516.0-521.0 m in borehole KFM09A.*

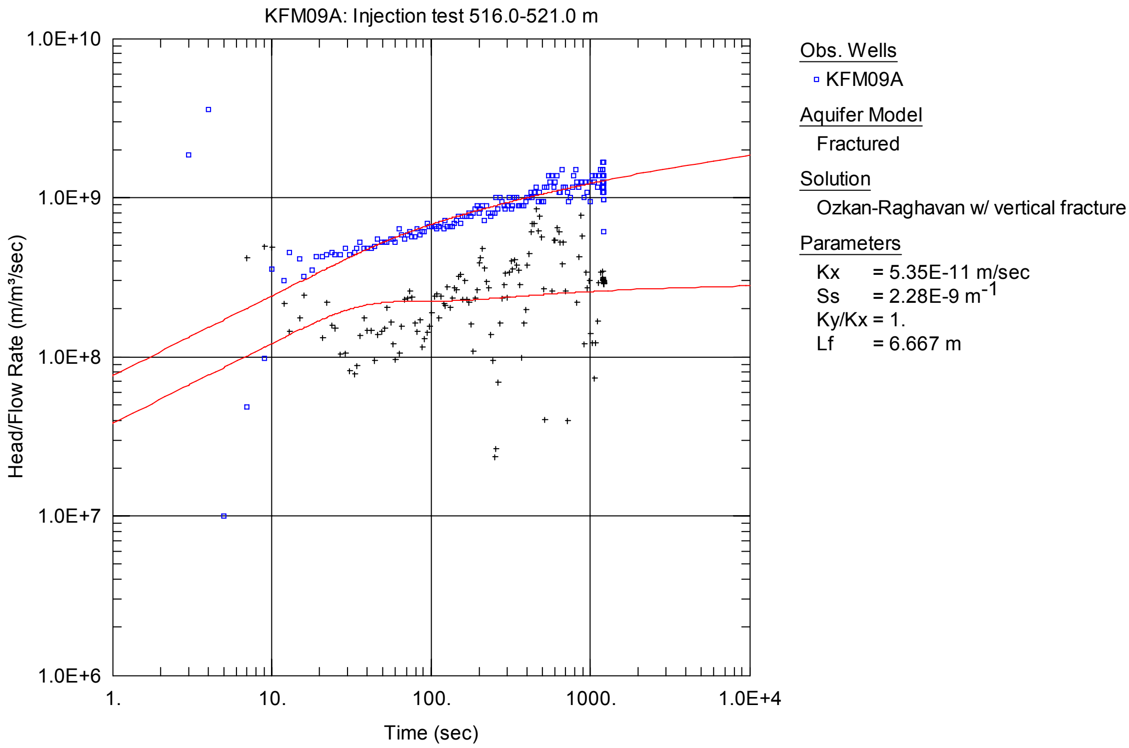


***Figure A3-487.** Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 516.0-521.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

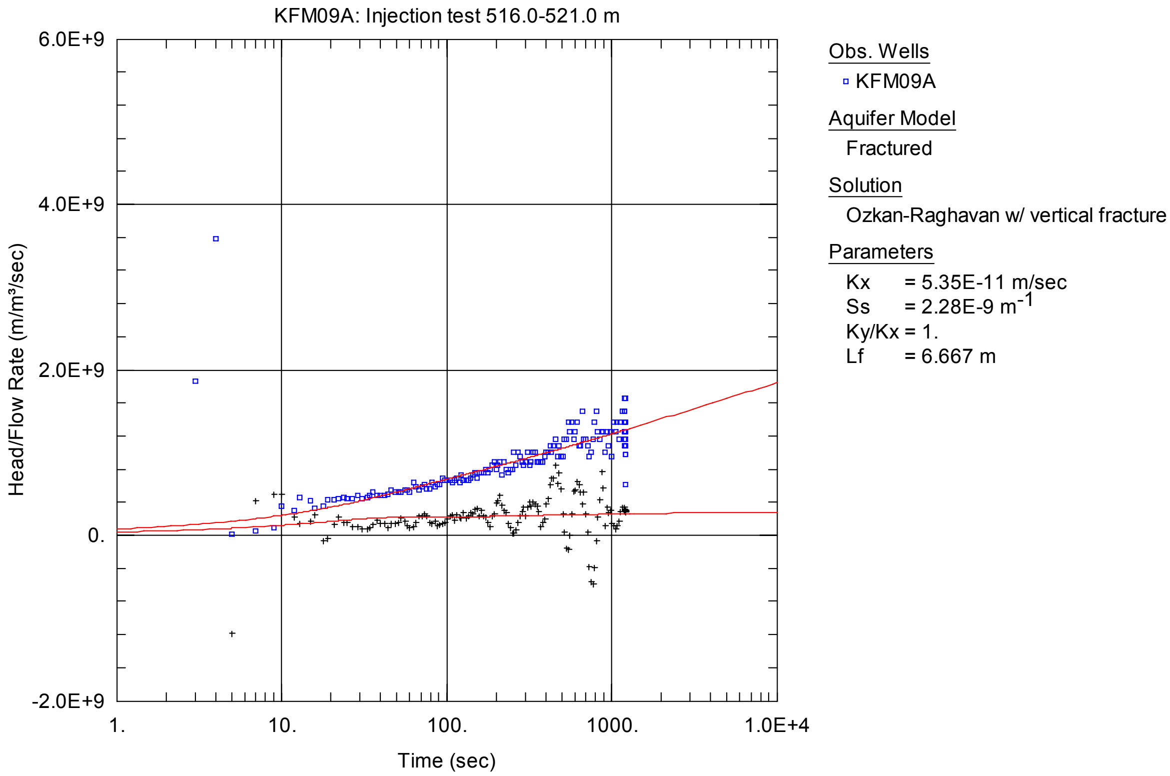


Figure A3-488. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 516.0-521.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

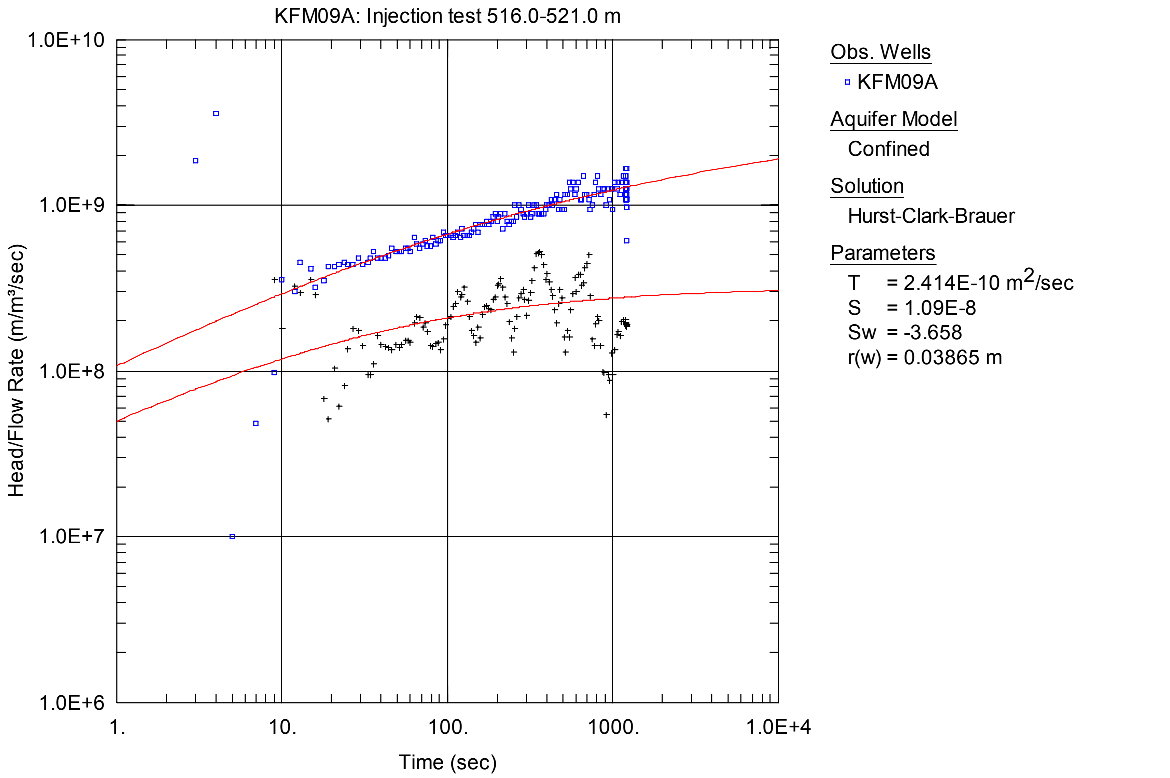


Figure A3-489. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 516.0-521.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for a pseudo-radial response.*

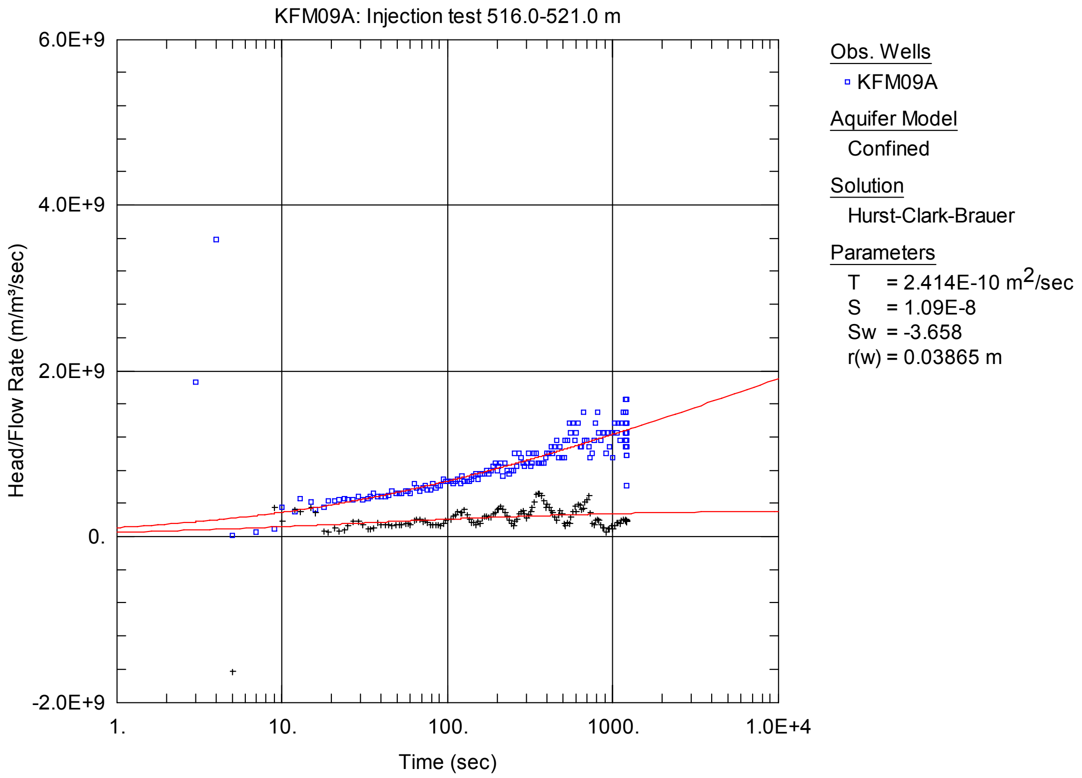


Figure A3-490. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 516.0-521.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for a pseudo-radial response.*

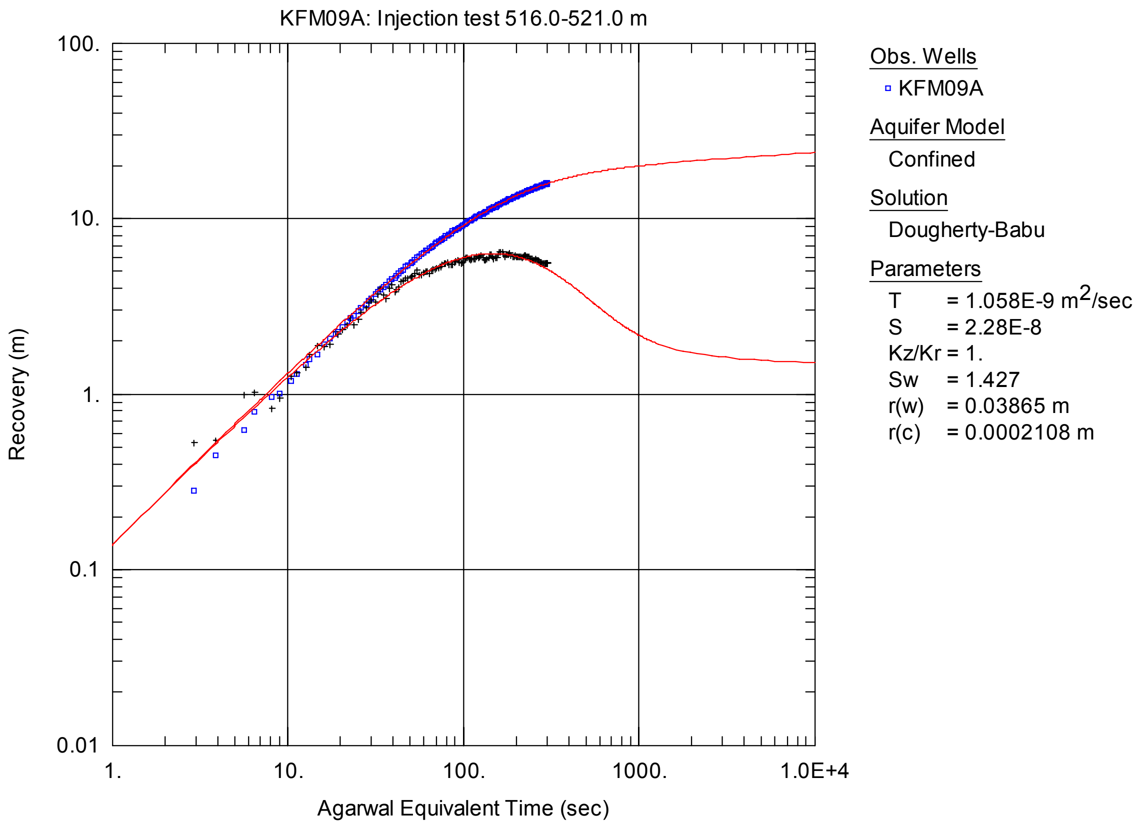


Figure A3-491. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 516.0-521.0 m in KFM09A.*

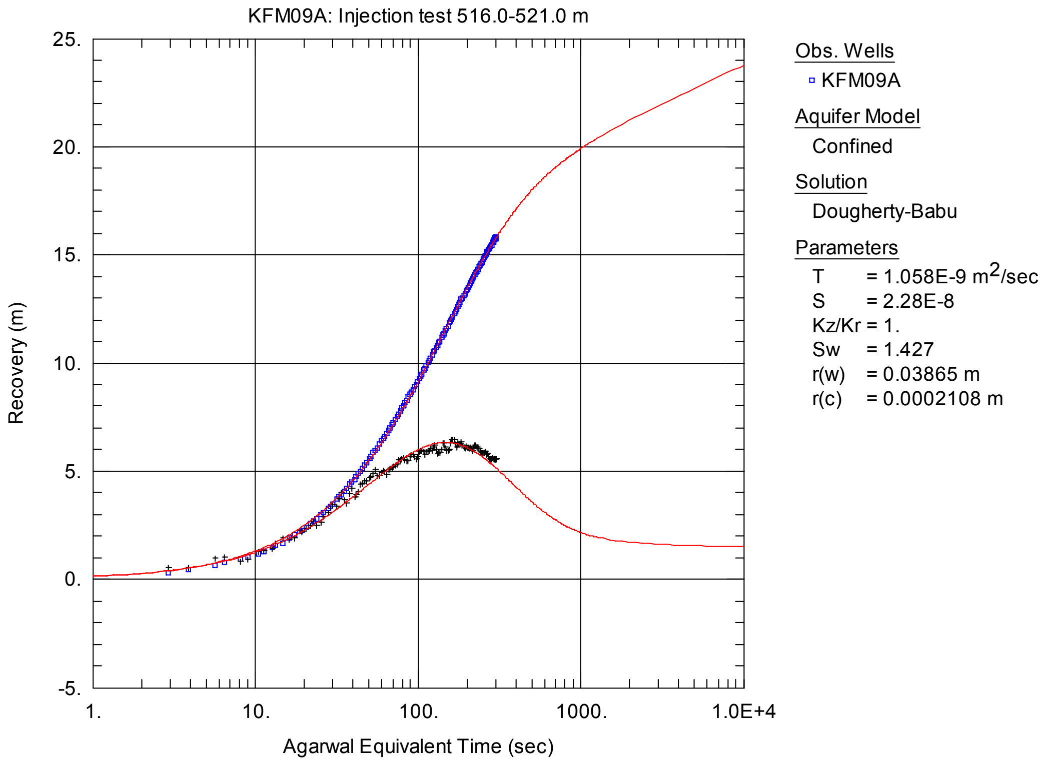


Figure A3-492. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 516.0-521.0 m in KFM09A.*

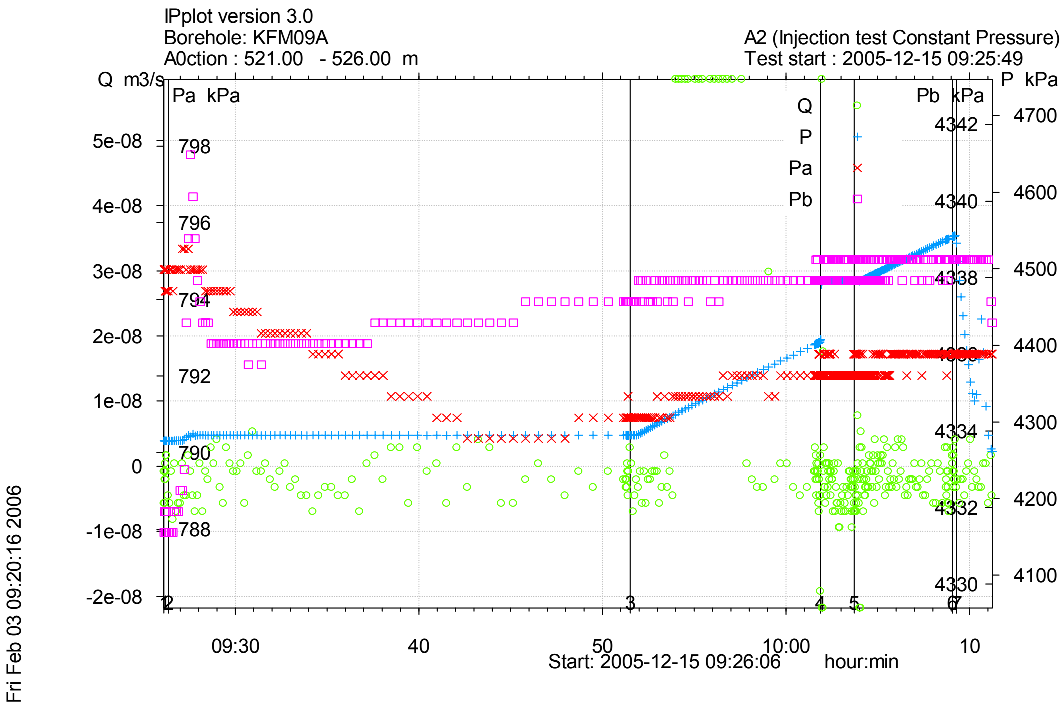


Figure A3-493. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 521.0-526.0 m in borehole KFM09A.*

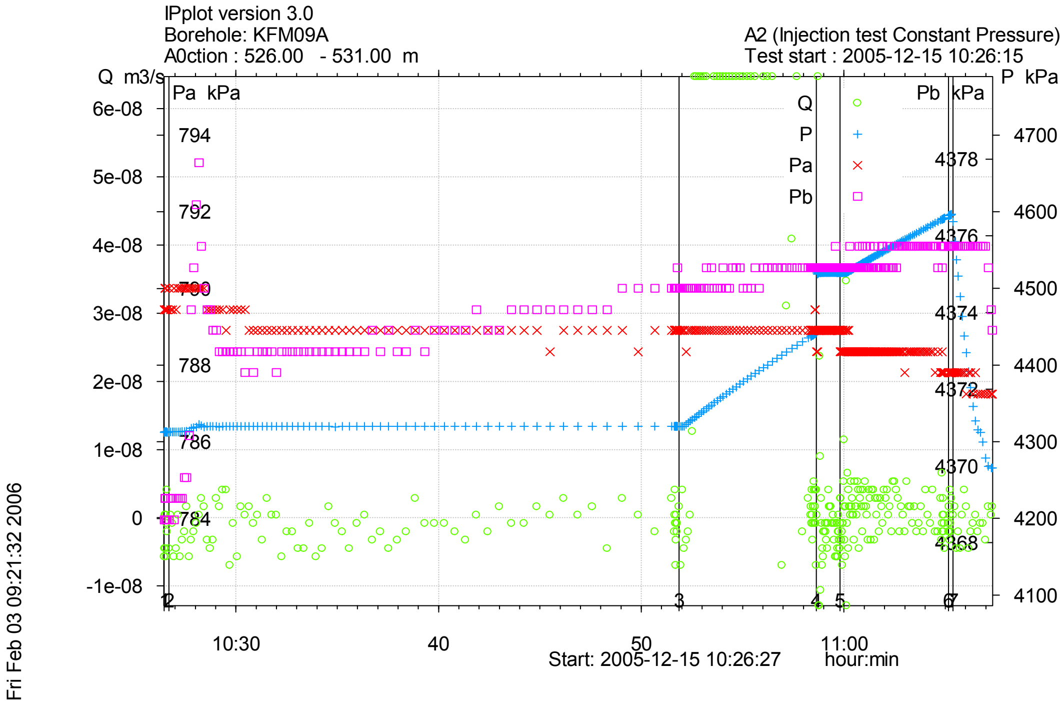


Figure A3-494. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 526.0-531.0 m in borehole KFM09A.*

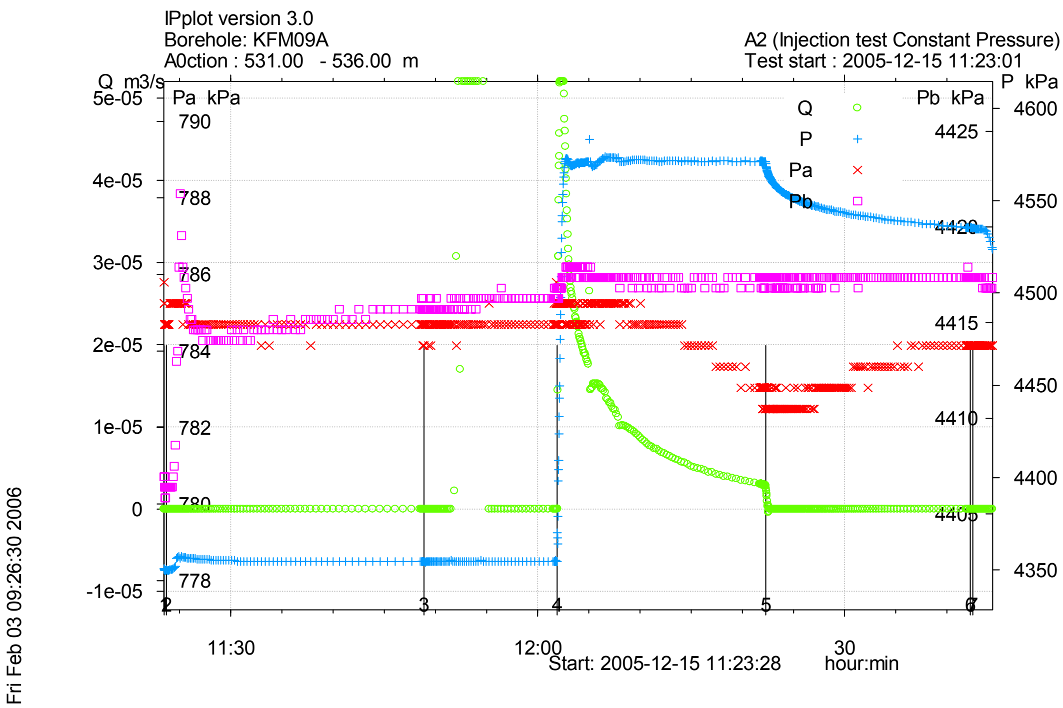


Figure A3-495. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 531.0-536.0 m in borehole KFM09A.*

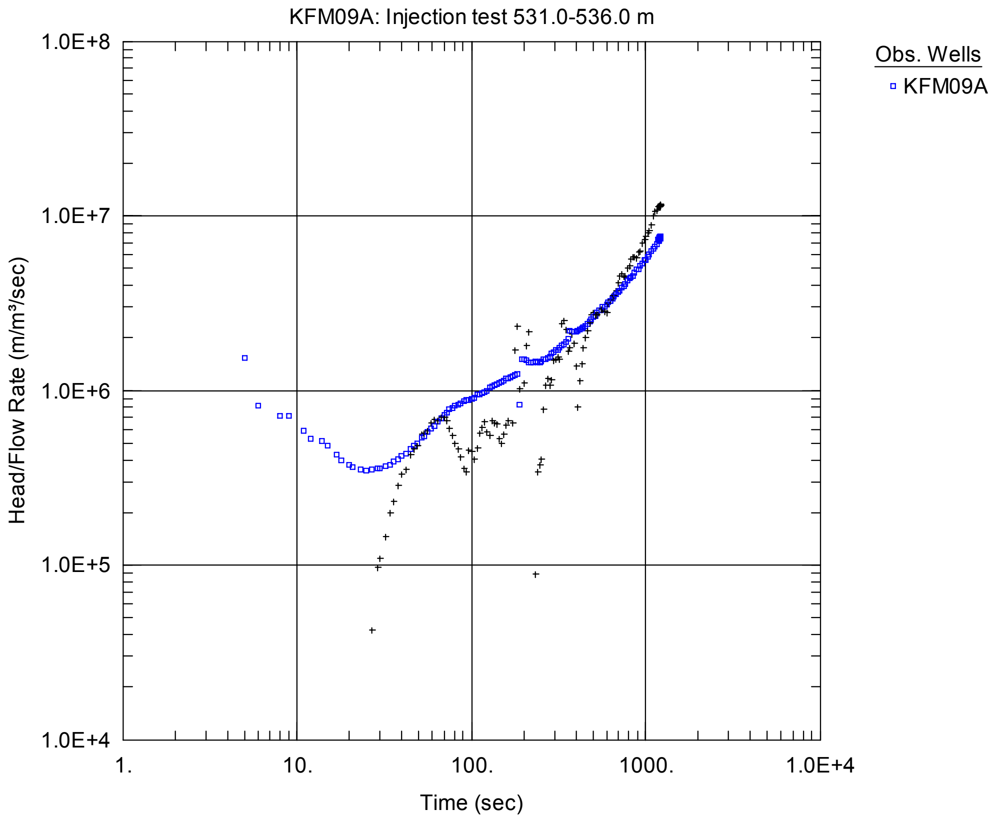


__Figure A3-496.__ Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 531.0-536.0 m in KFM09A.

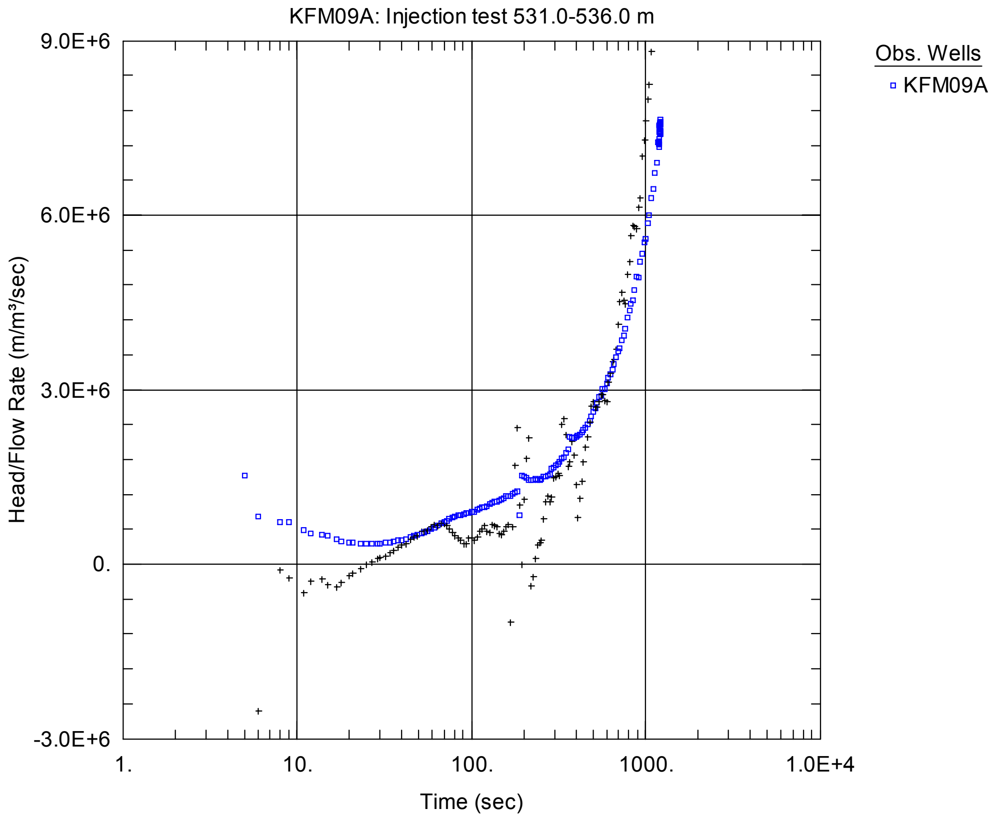


__Figure A3-497.__ Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 531.0-536.0 m in KFM09A.

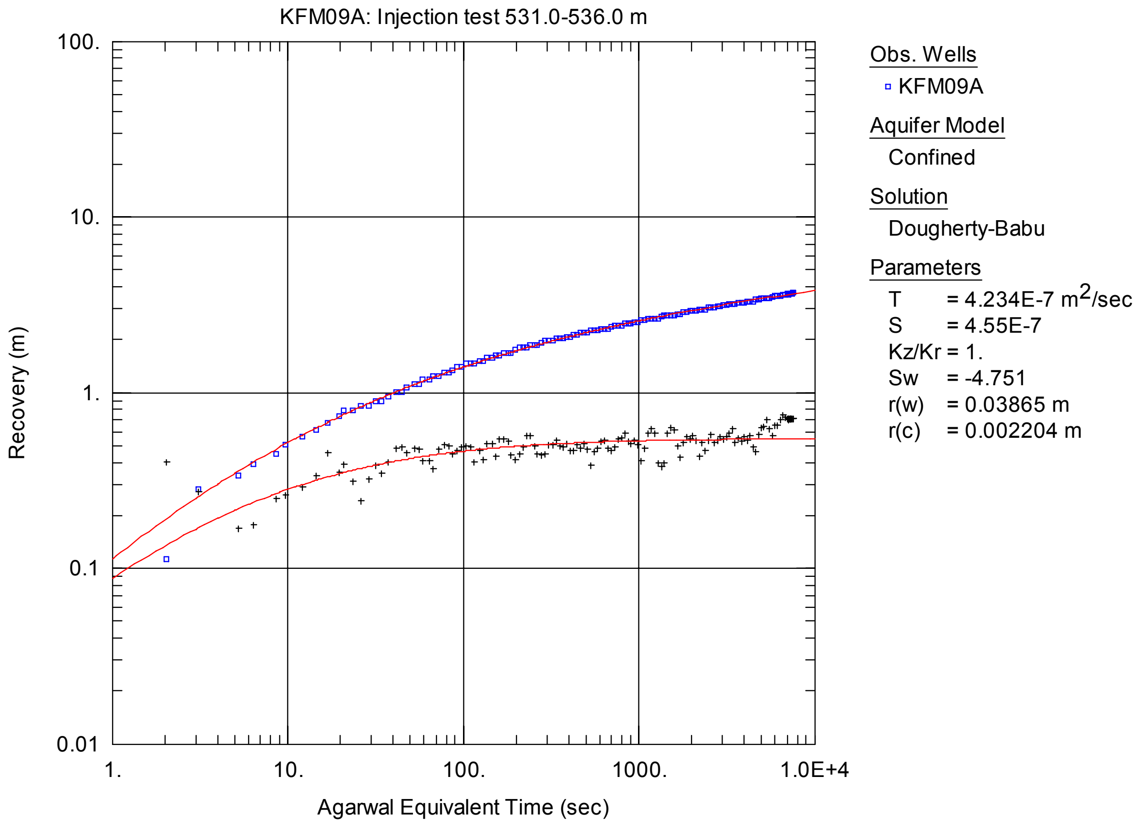


Figure A3-498. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 531.0-536.0 m in KFM09A.*

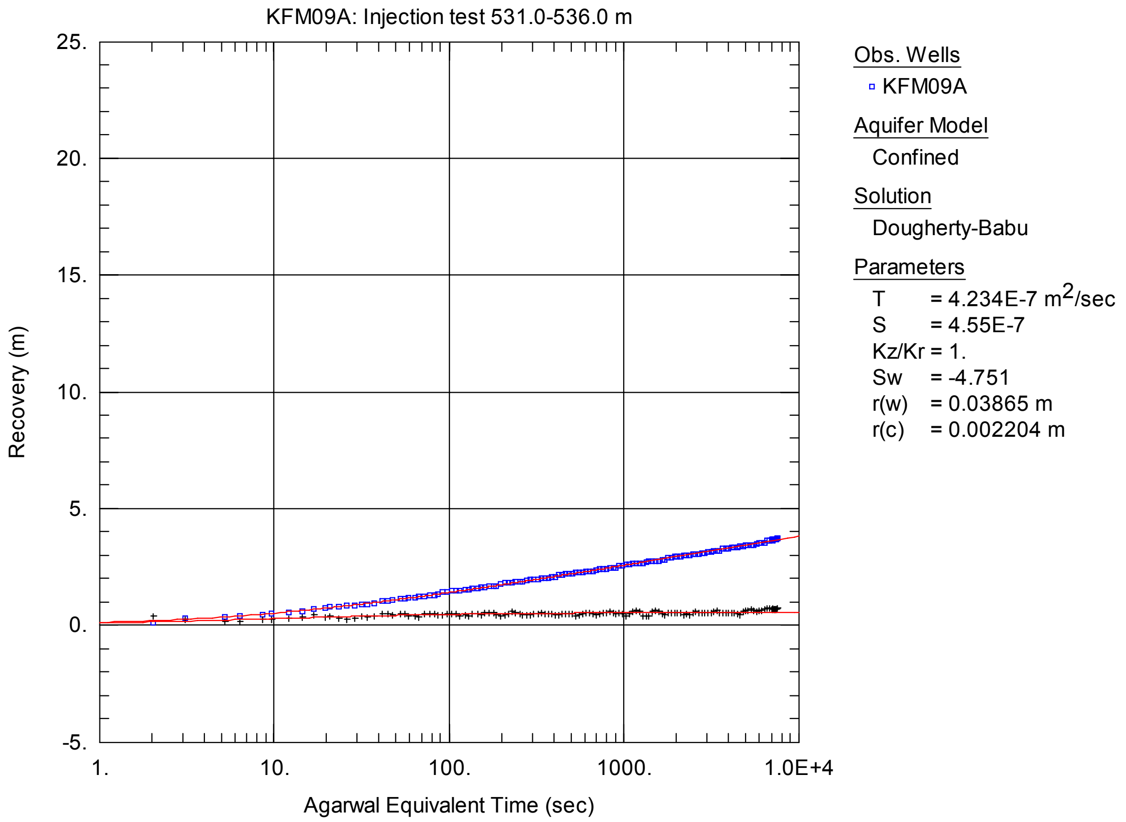


Figure A3-499. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 531.0-536.0 m in KFM09A.*

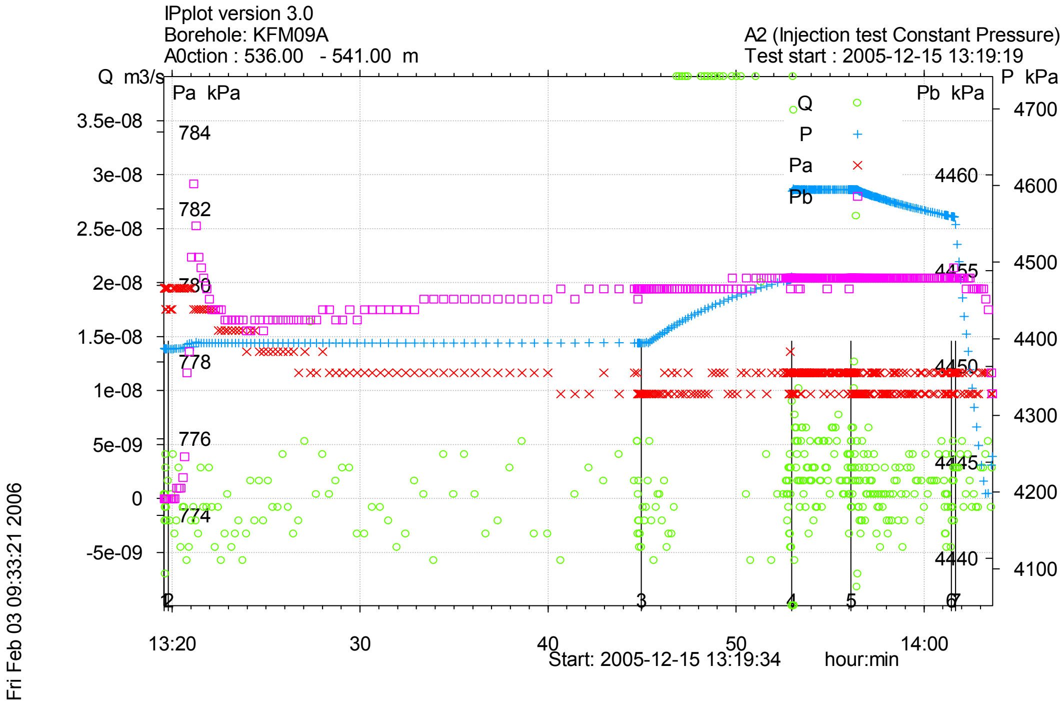


Figure A3-500. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 536.0-541.0 m in borehole KFM09A.*

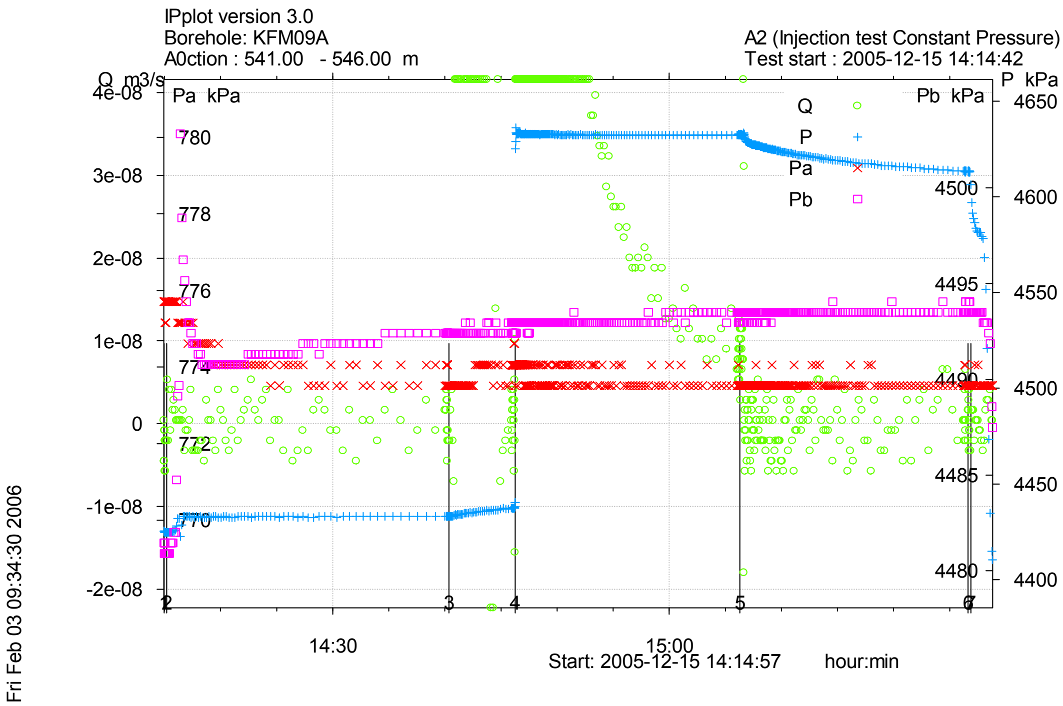


Figure A3-501. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 541.0-546.0 m in borehole KFM09A.*

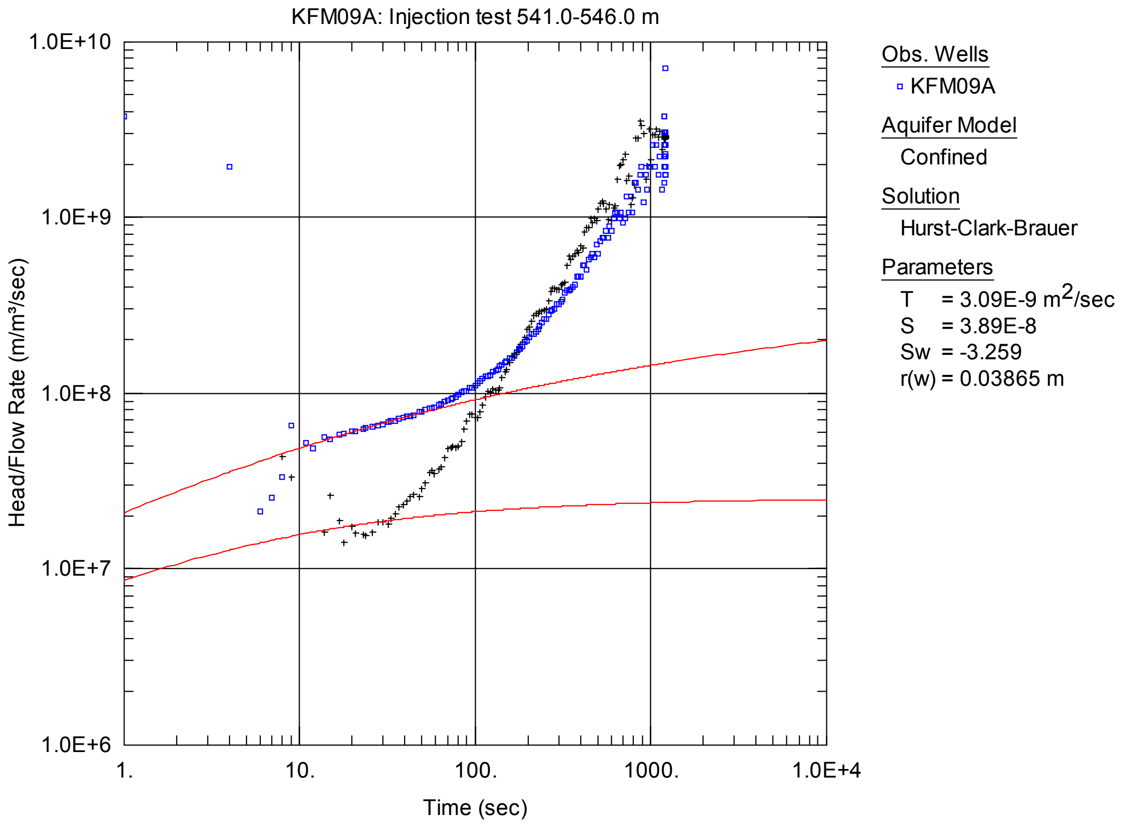


Figure A3-502. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 541.0-546.0 m in KFM09A.*

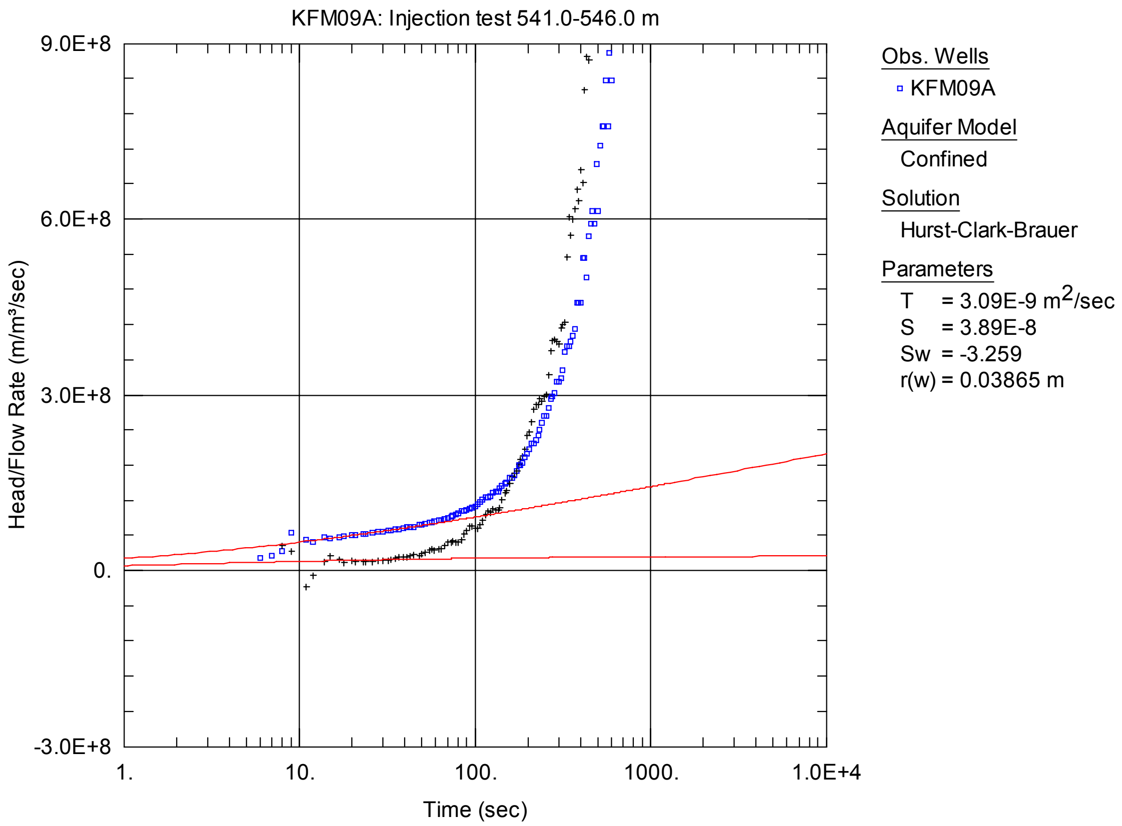


Figure A3-503. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 541.0-546.0 m in KFM09A.*

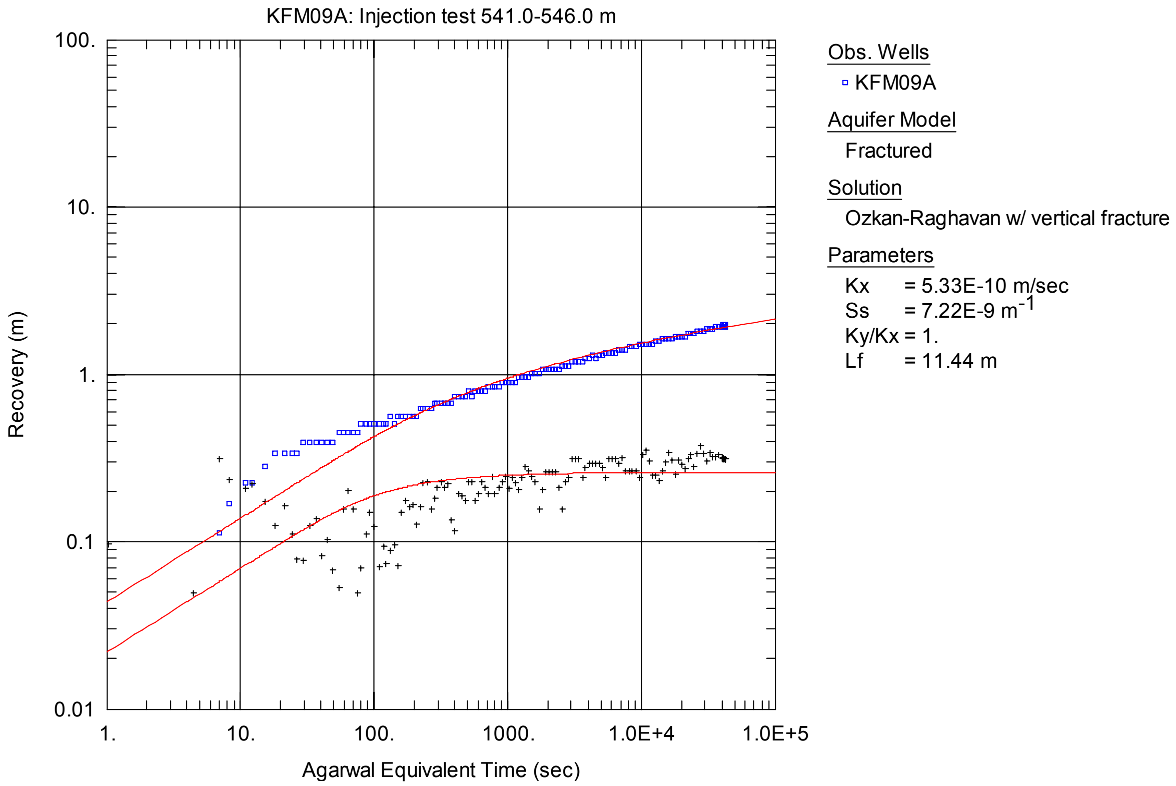


Figure A3-504. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 541.0-546.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

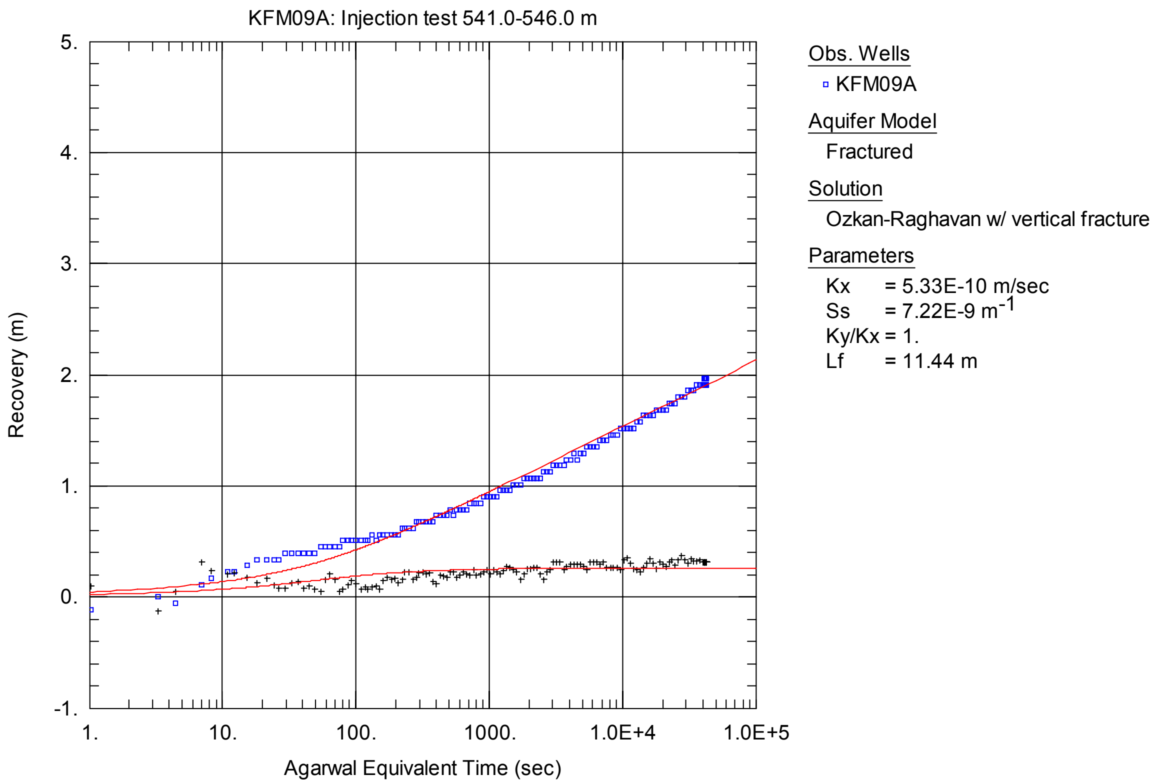


Figure A3-505. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 541.0-546.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

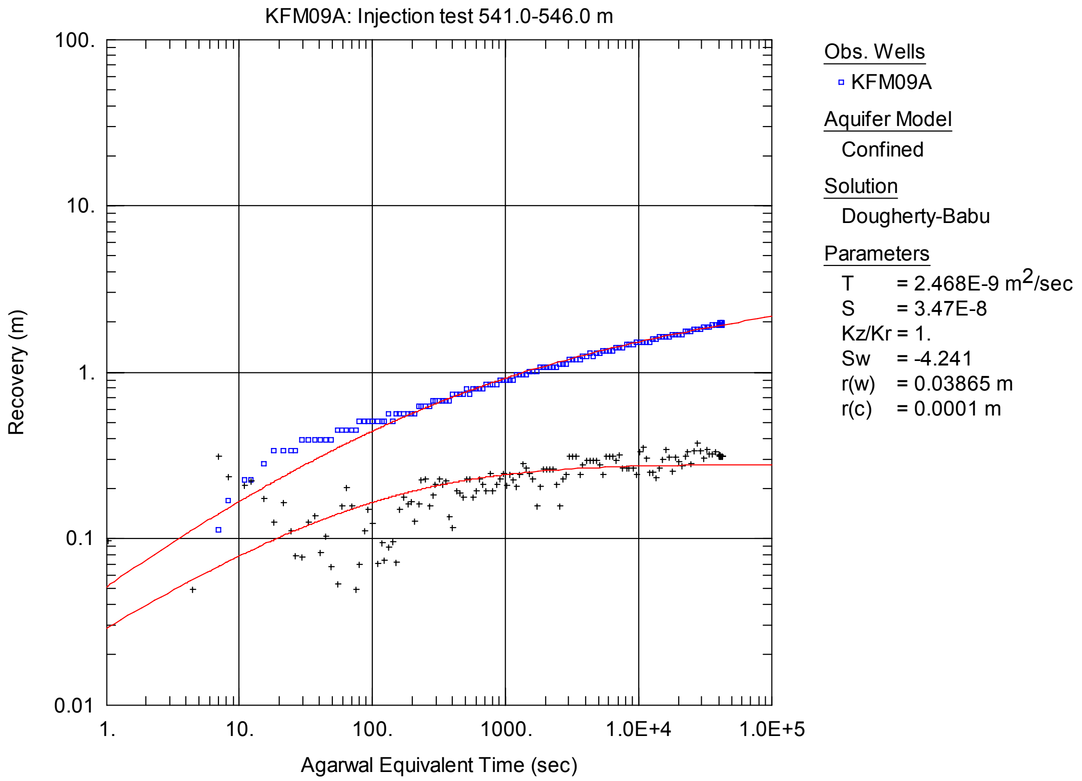


Figure A3-506. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 541.0-546.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

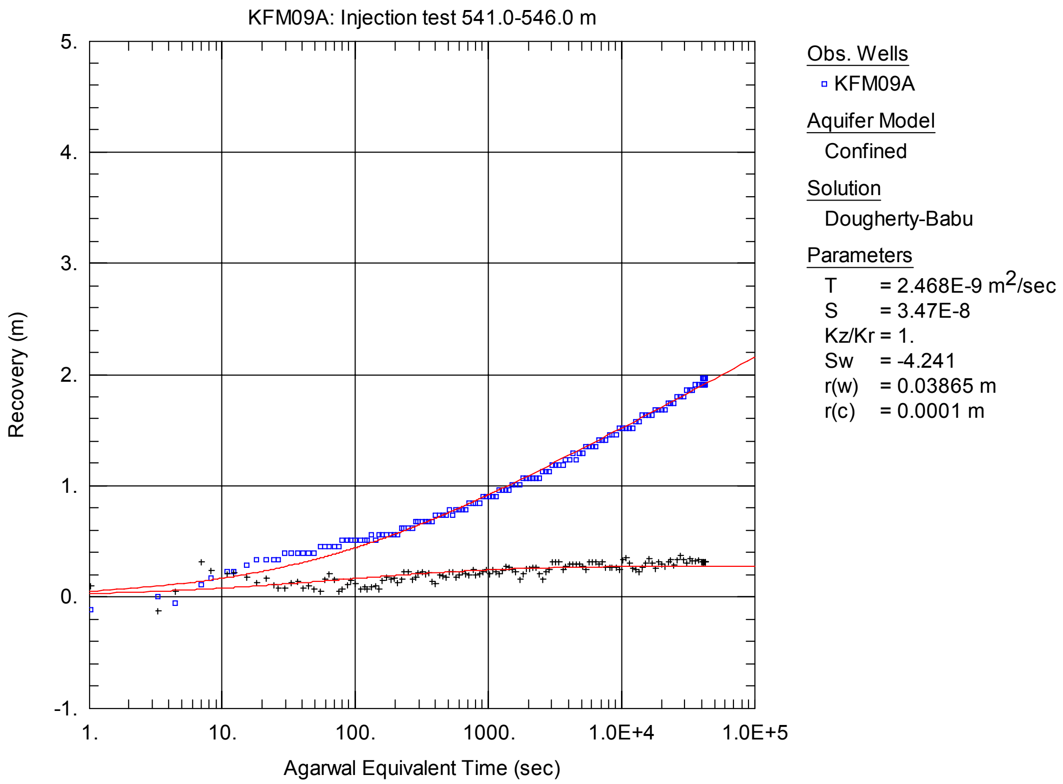


Figure A3-507. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 541.0-546.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

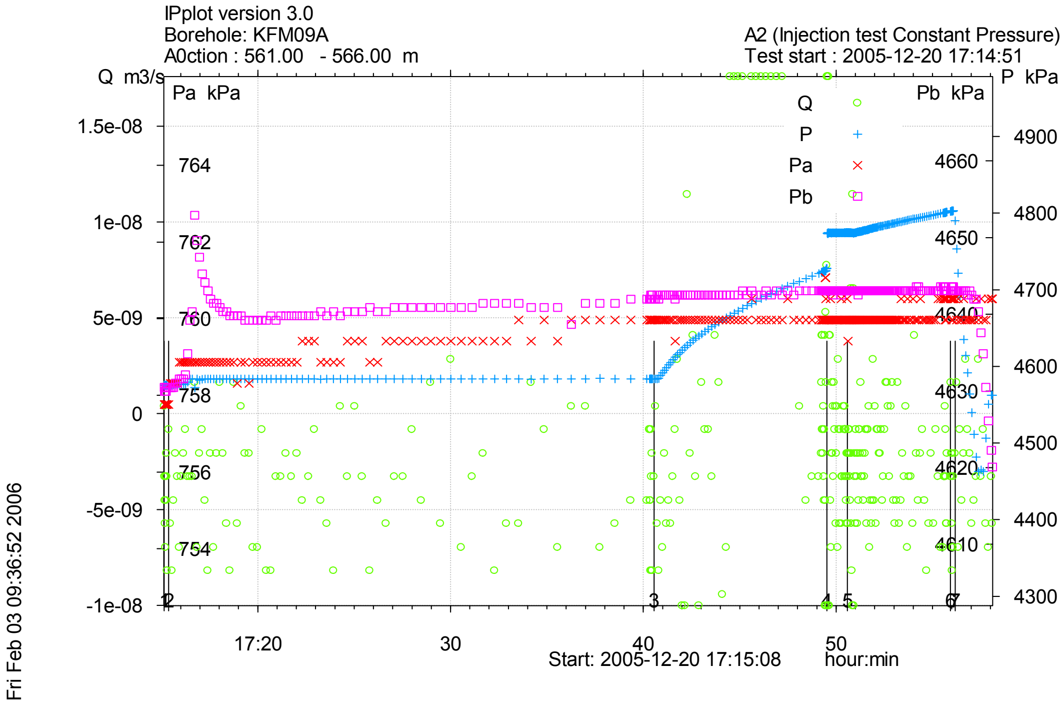


Figure A3-508. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 561.0-566.0 m in borehole KFM09A.

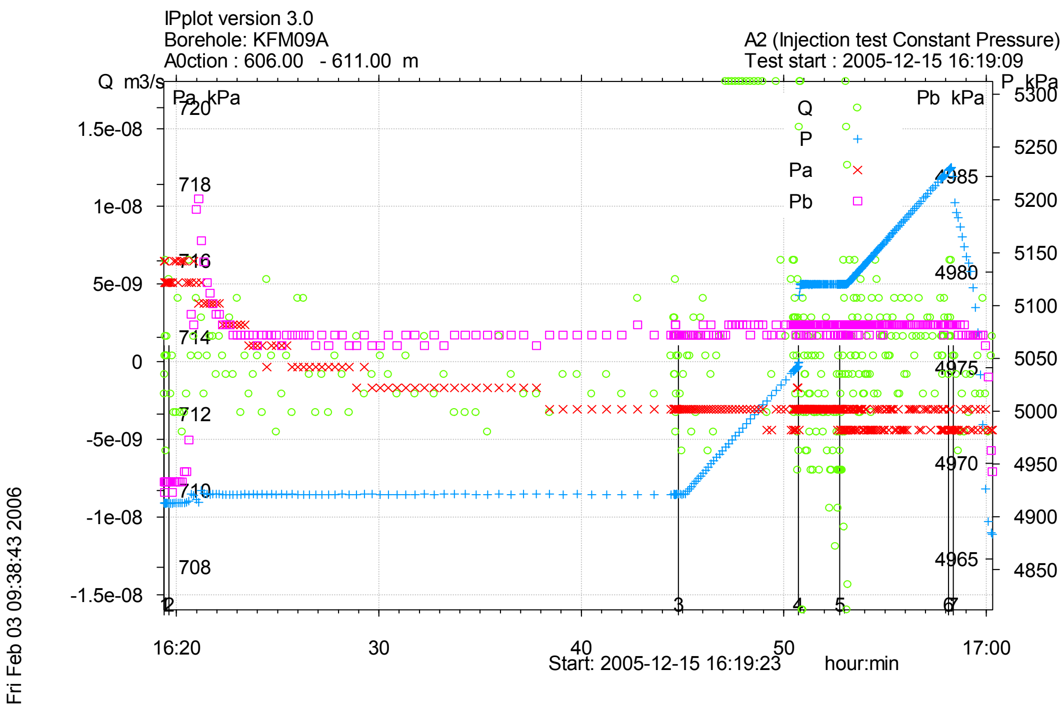


Figure A3-509. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 606.0-611.0 m in borehole KFM09A.

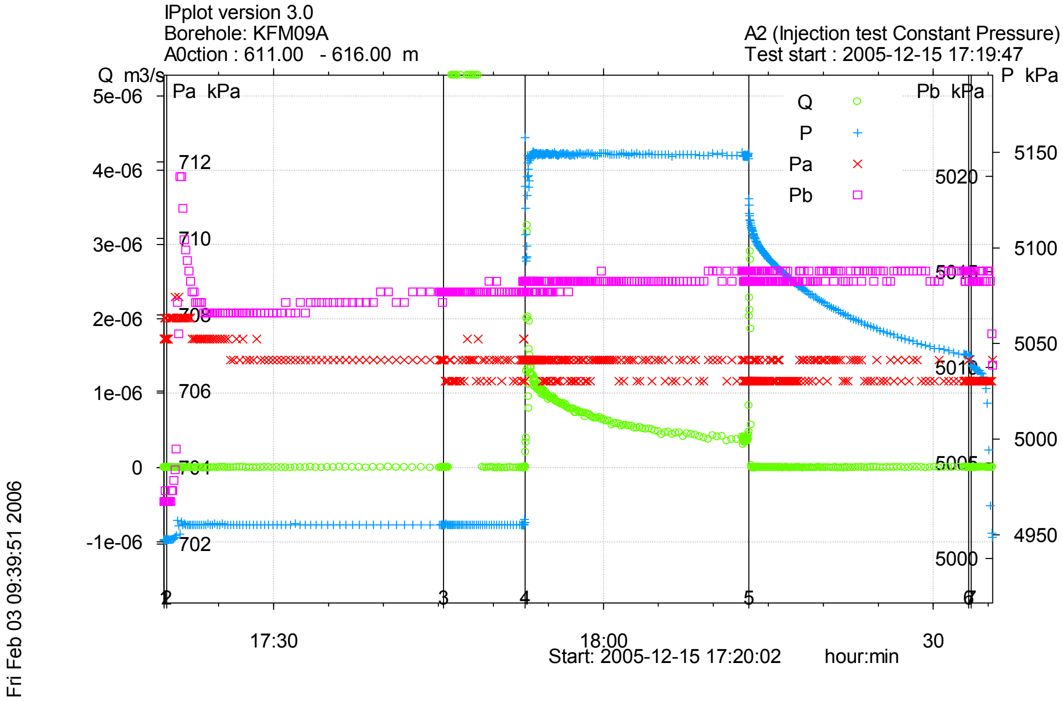


***Figure A3-510.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 611.0-616.0 m in borehole KFM09A.*

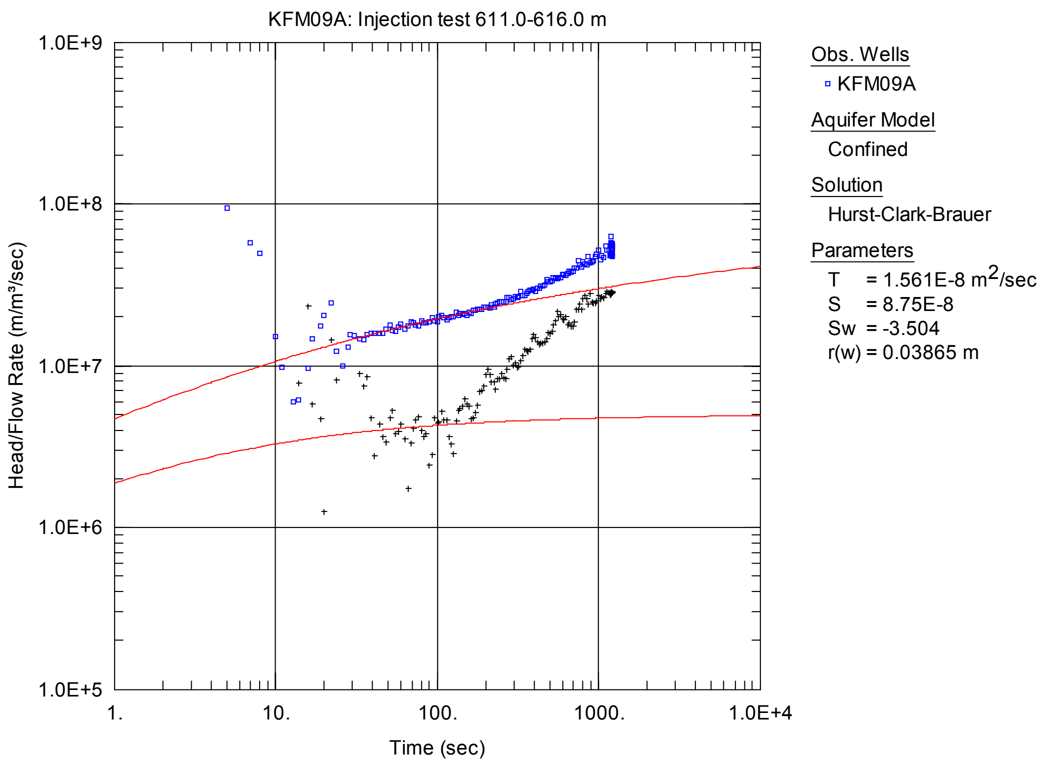


***Figure A3-511.** Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 611.0-616.0 m in KFM09A.*

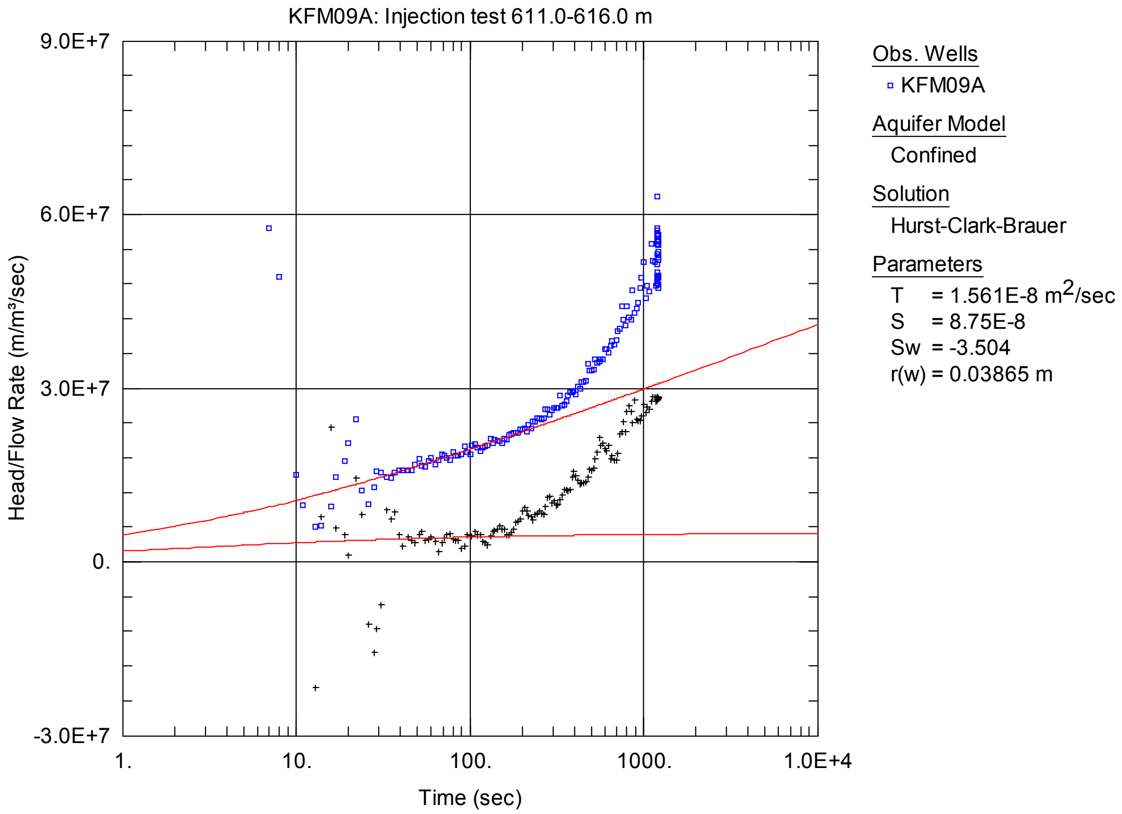


Figure A3-512. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 611.0-616.0 m in KFM09A.*

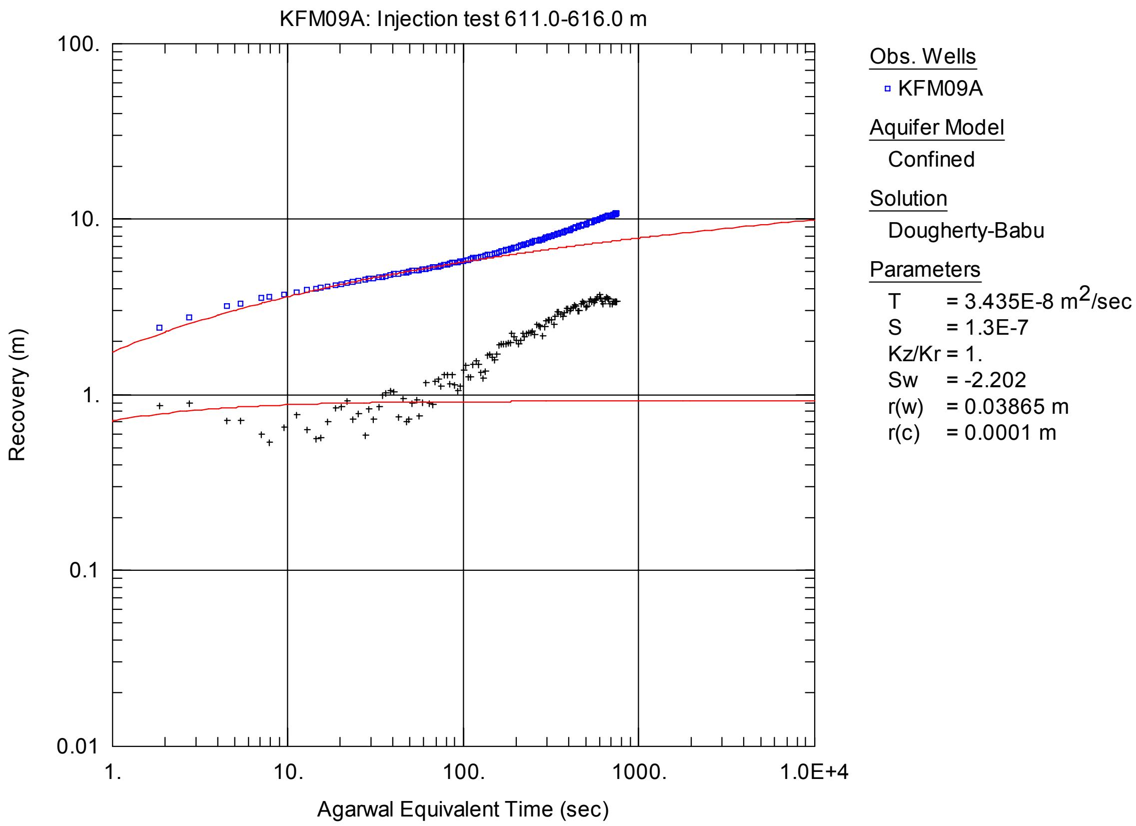


Figure A3-513. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 611.0-616.0 m in KFM09A.*

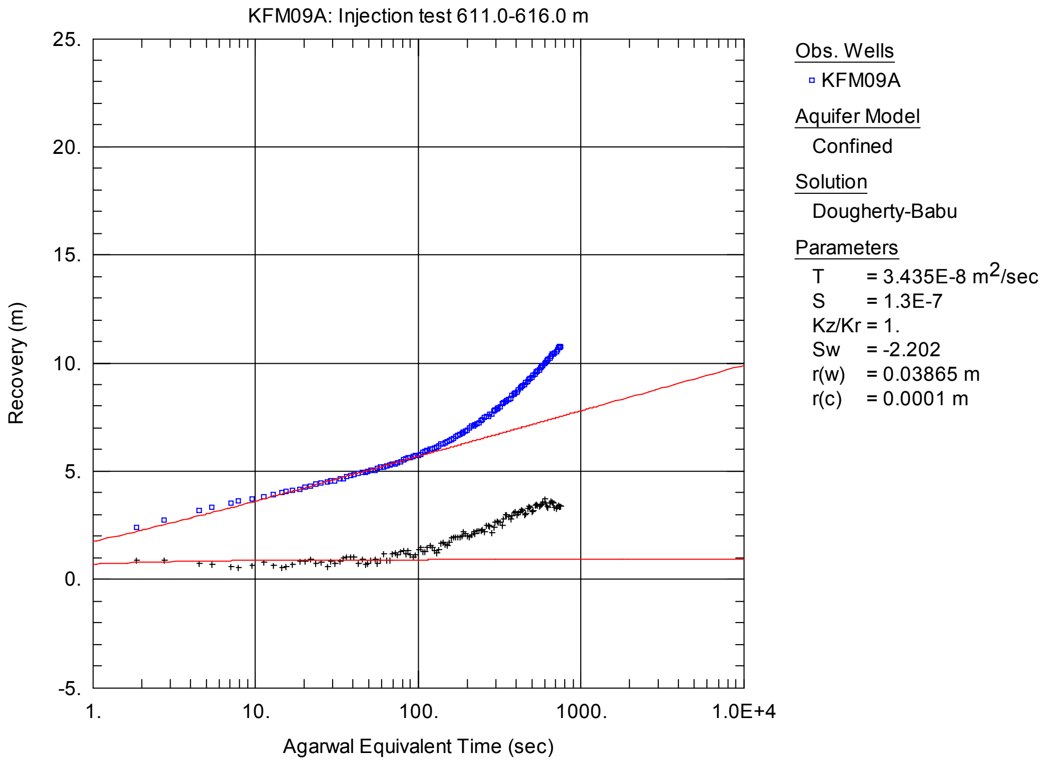


Figure A3-514. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 611.0-616.0 m in KFM09A.*

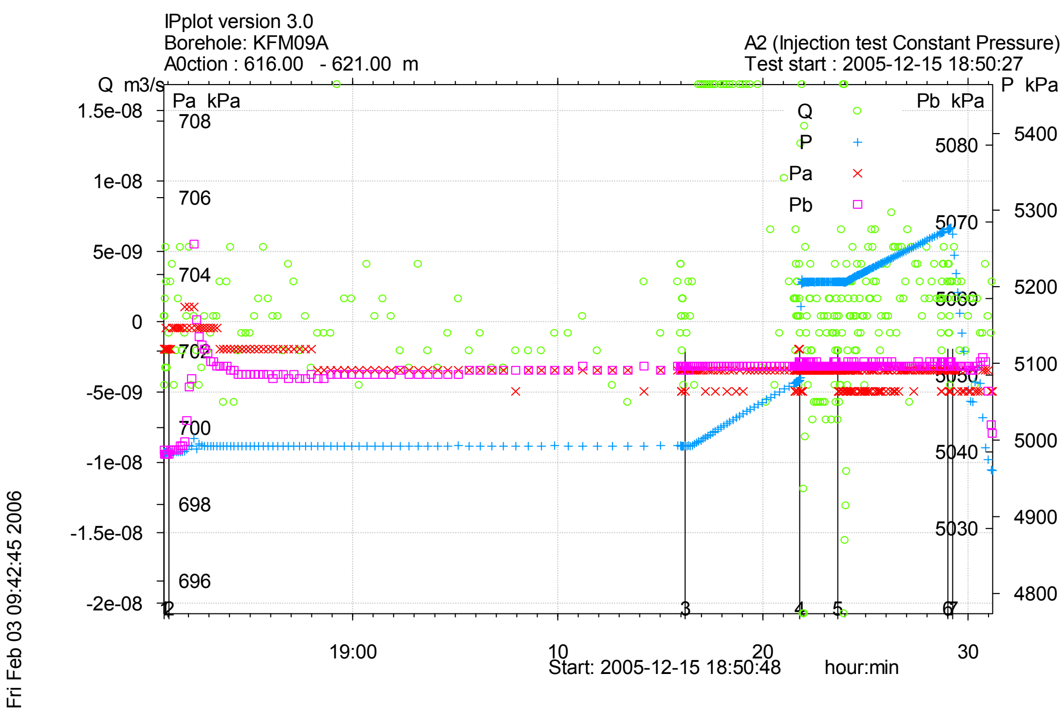


Figure A3-515. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 616.0-621.0 m in borehole KFM09A.*

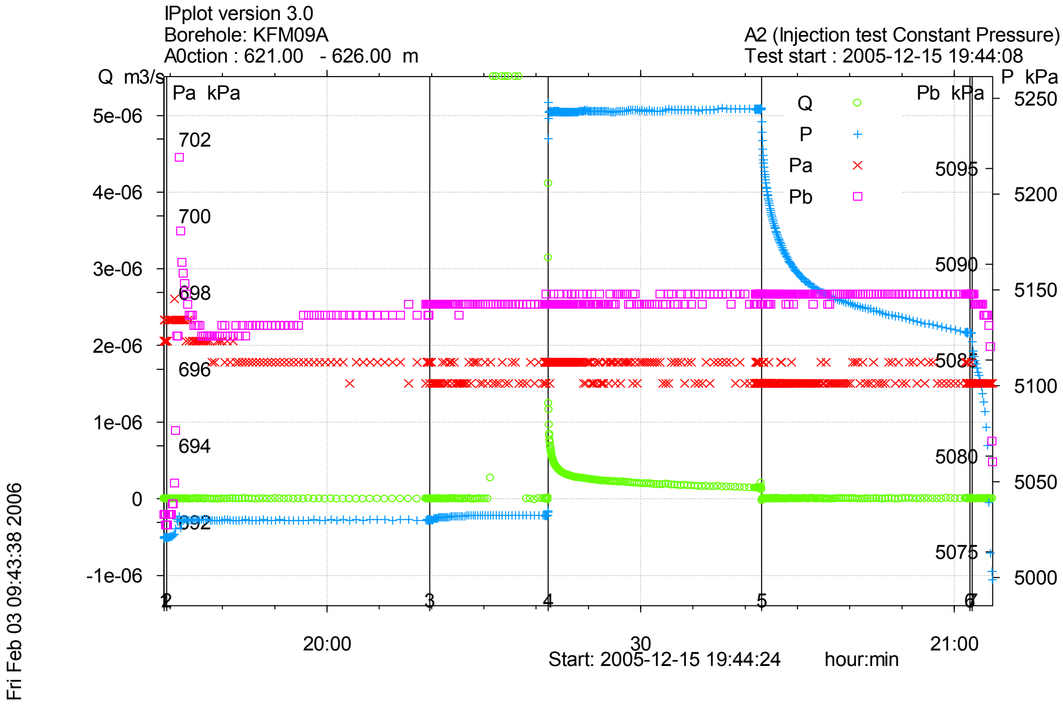


__Figure A3-516.__ Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 621.0-626.0 m in borehole KFM09A.

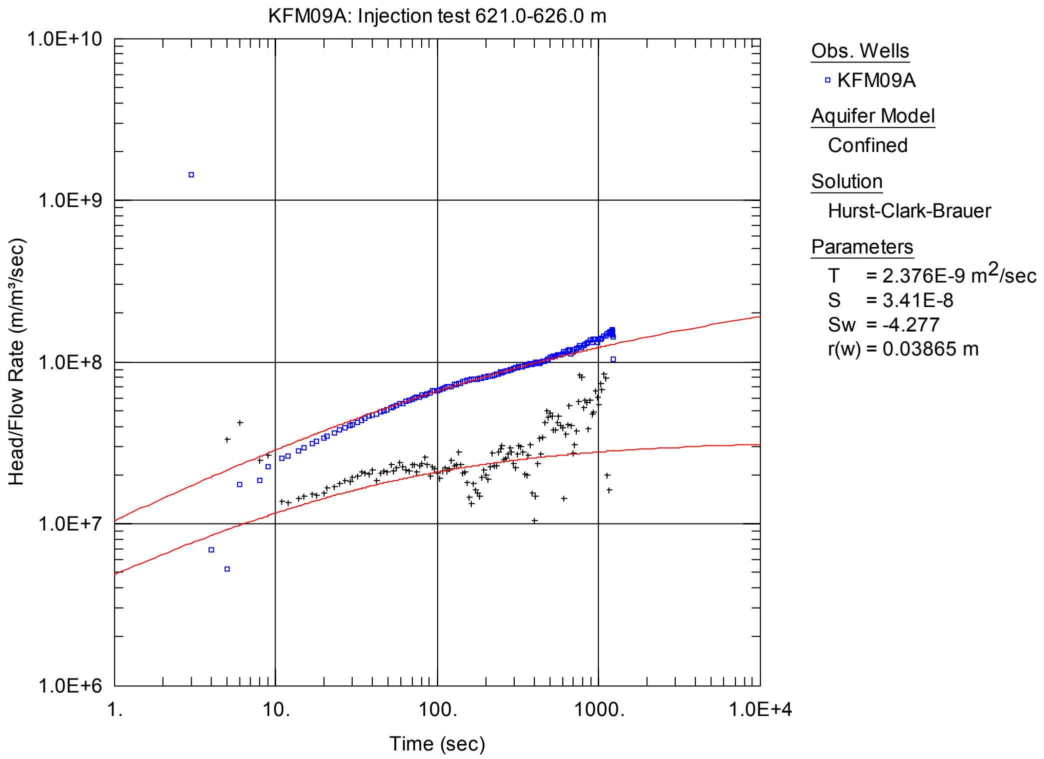


__Figure A3-517.__ Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 621.0-626.0 m in KFM09A.

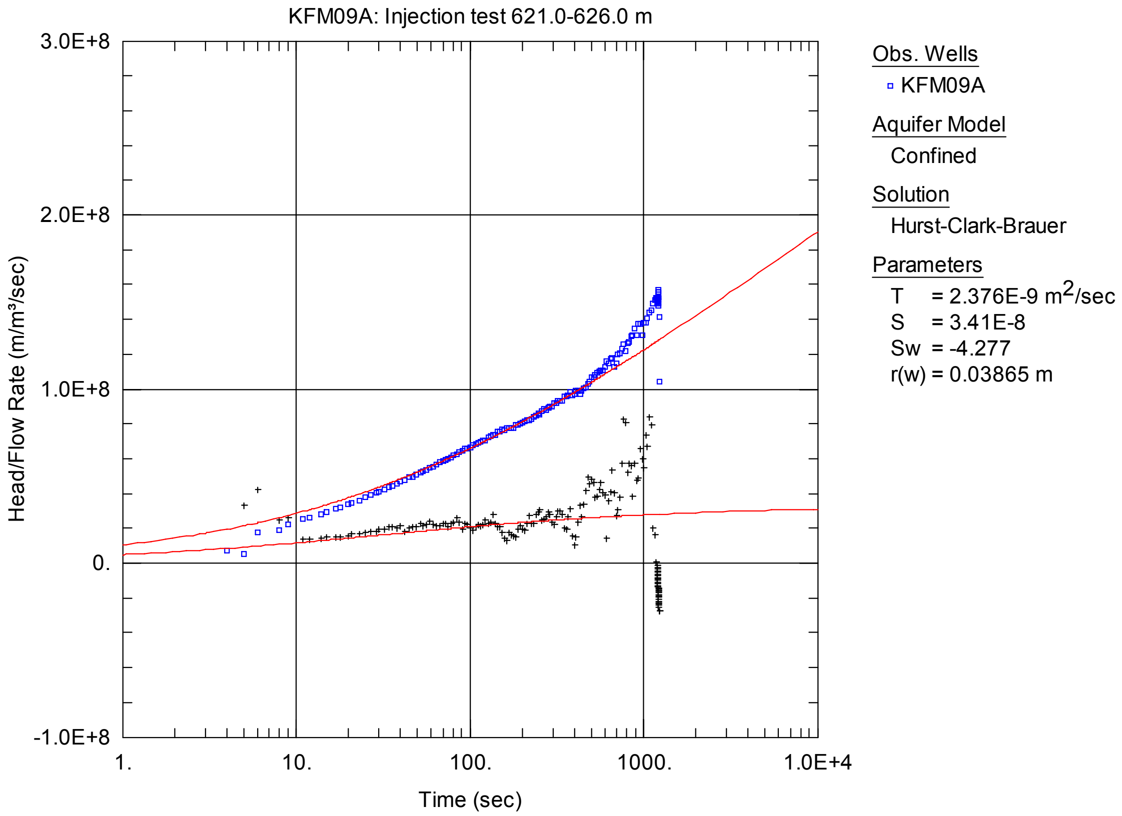


Figure A3-518. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 621.0-626.0 m in KFM09A.*

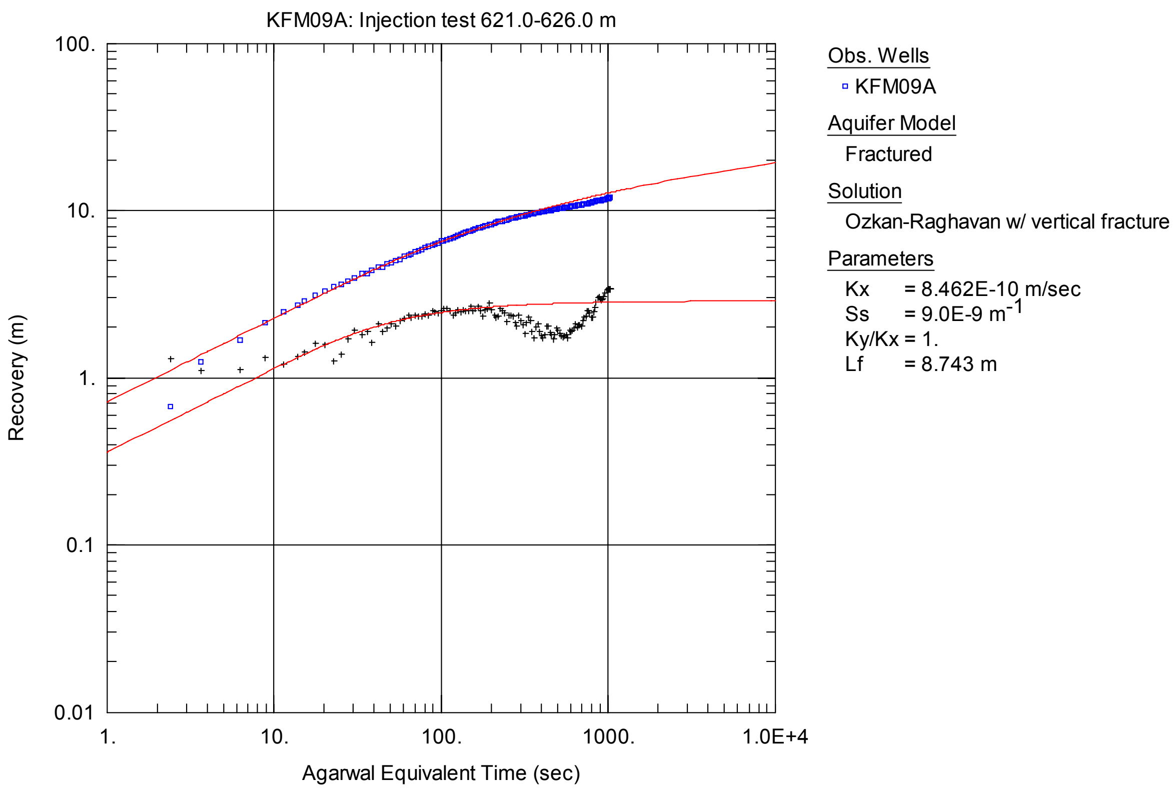


Figure A3-519. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 621.0-626.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

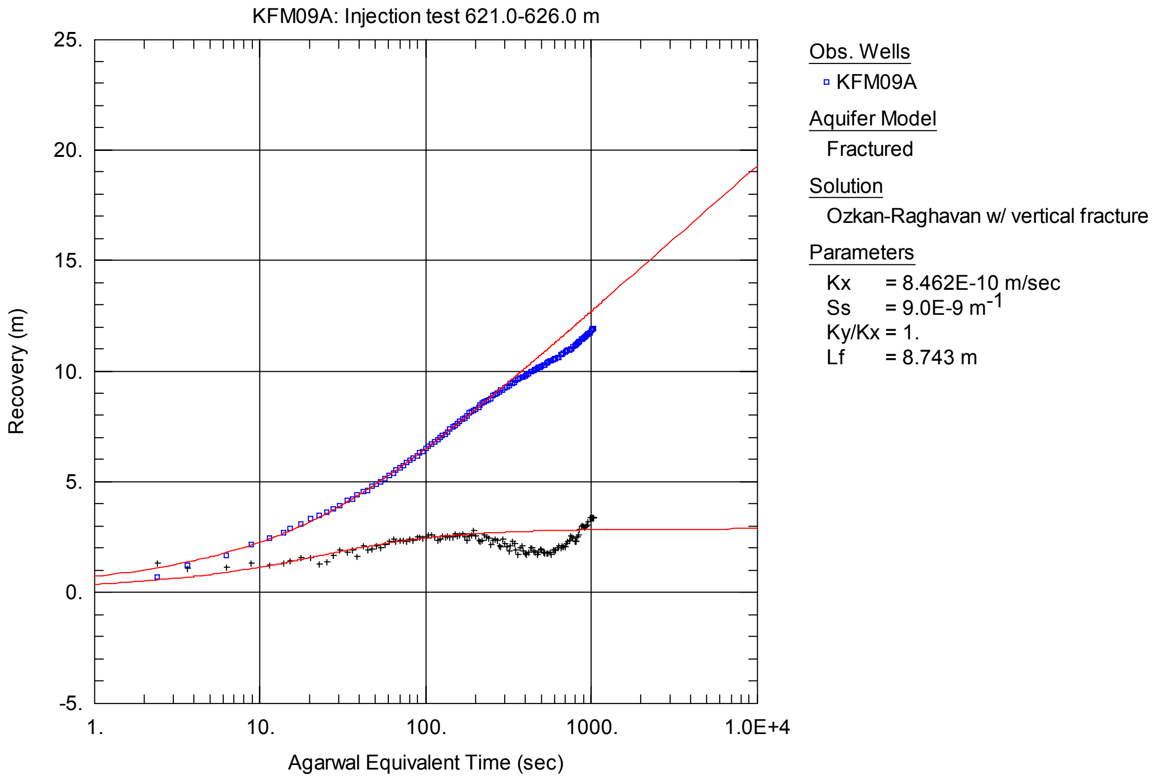


Figure A3-520. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 621.0-626.0 m in KFM09A.This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

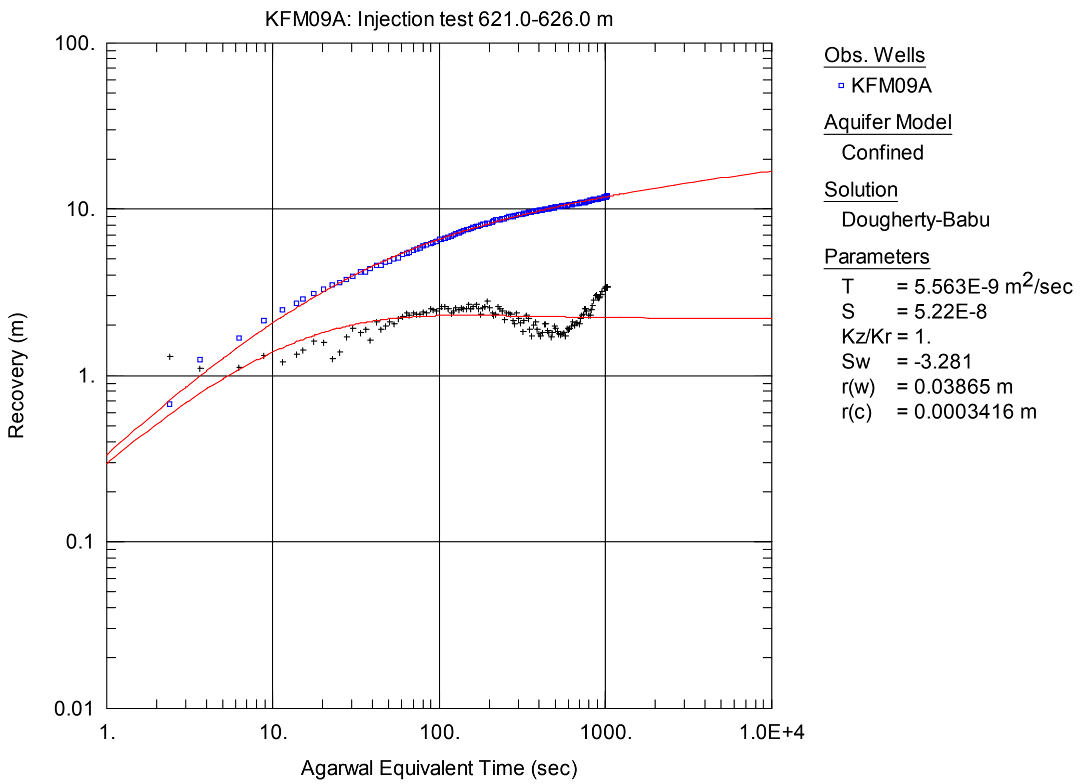


Figure A3-521. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 621.0-626.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

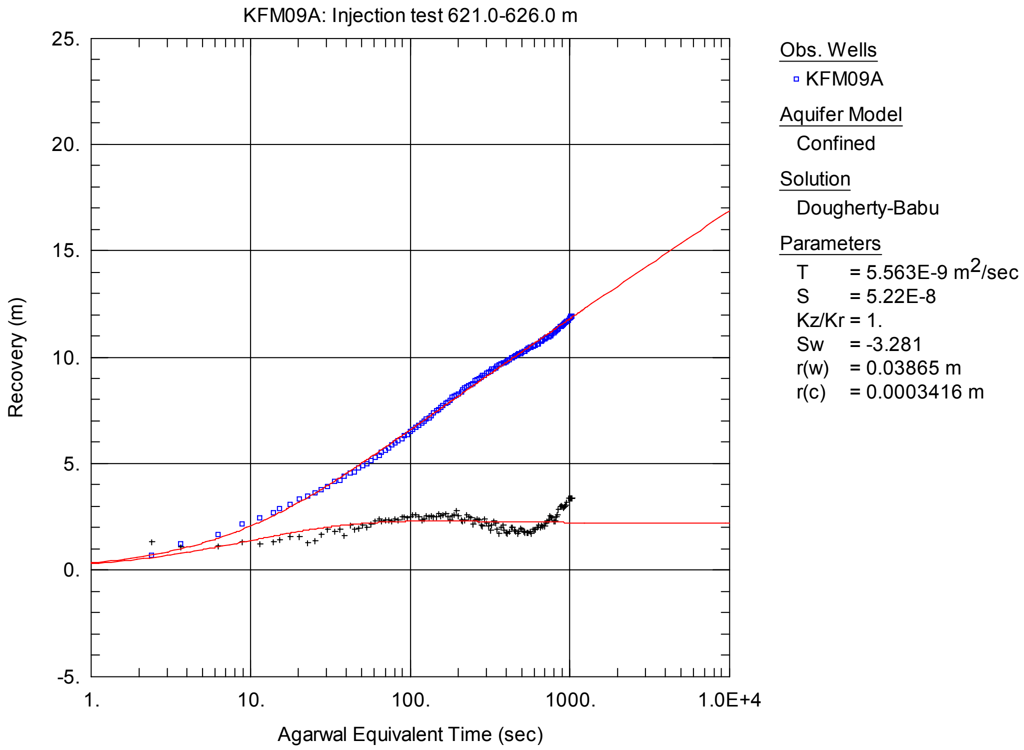


Figure A3-522. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 621.0-626.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

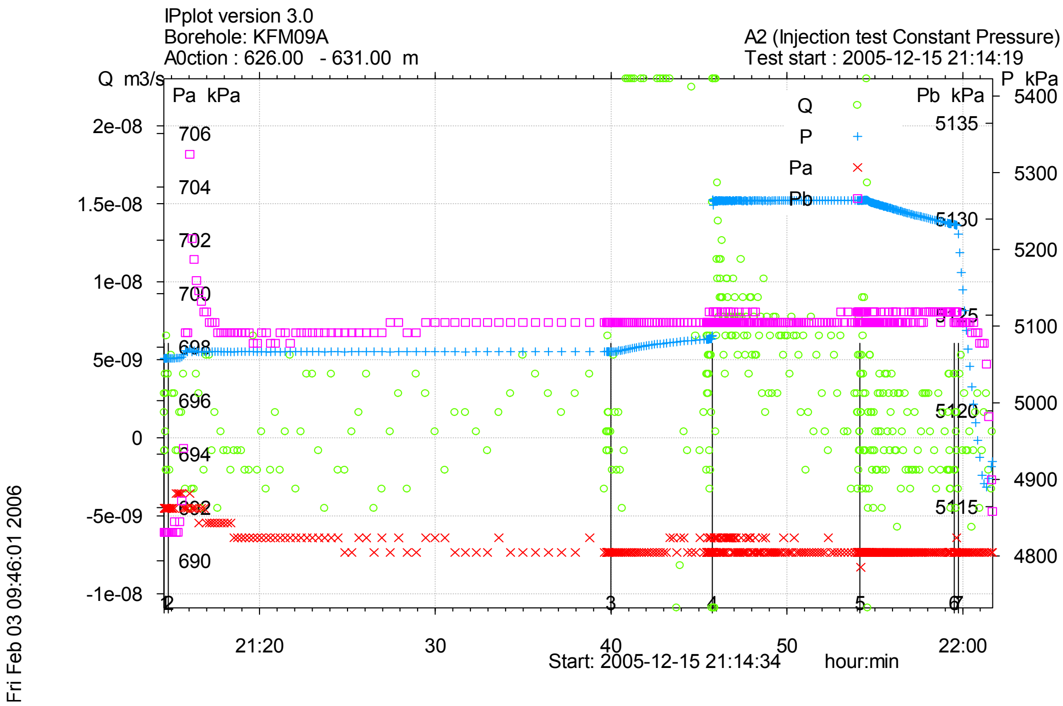


Figure A3-523. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 626.0-631.0 m in borehole KFM09A.*

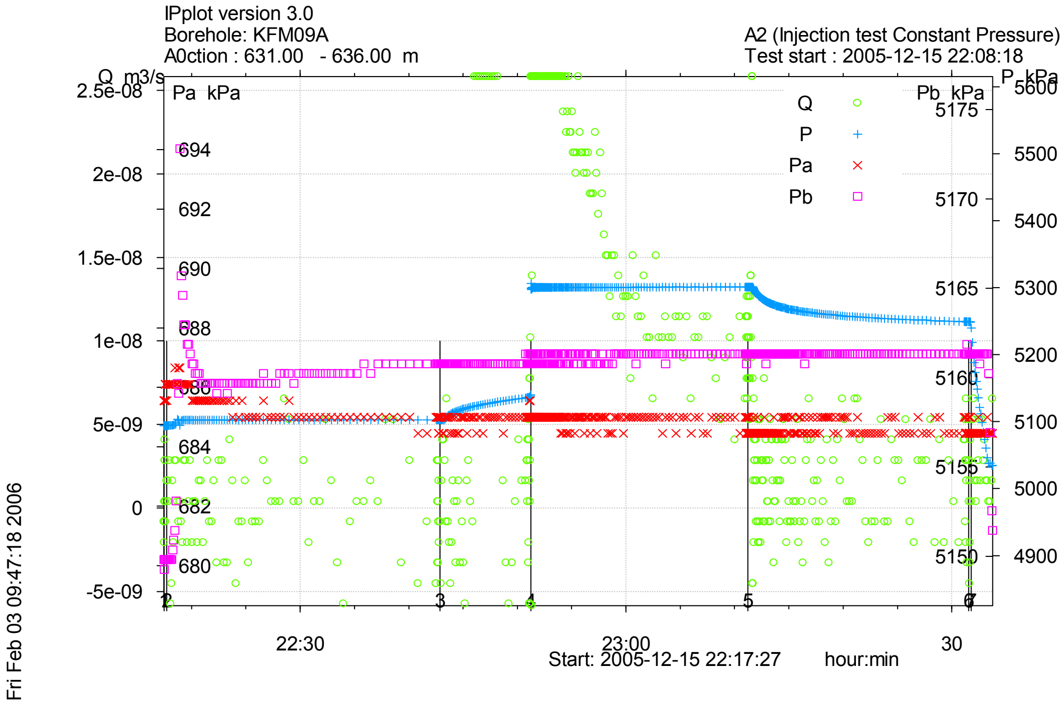


Figure A3-524. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 631.0-636.0 m in borehole KFM09A.

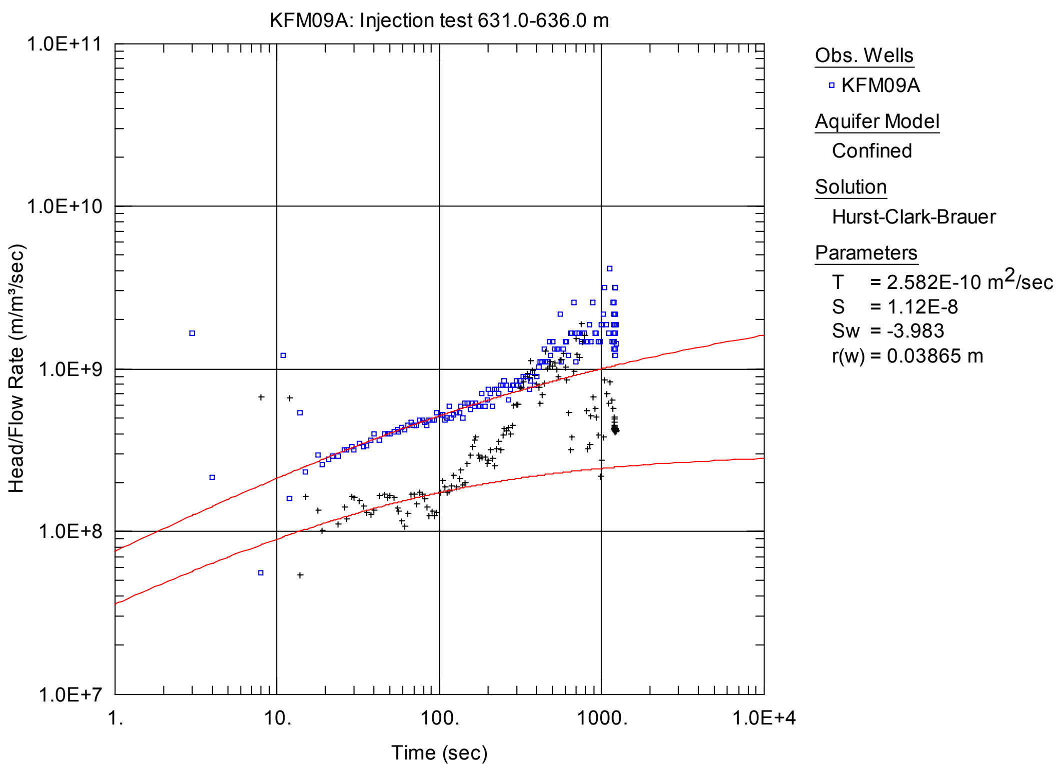


Figure A3-525. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 631.0-636.0 m in KFM09A.

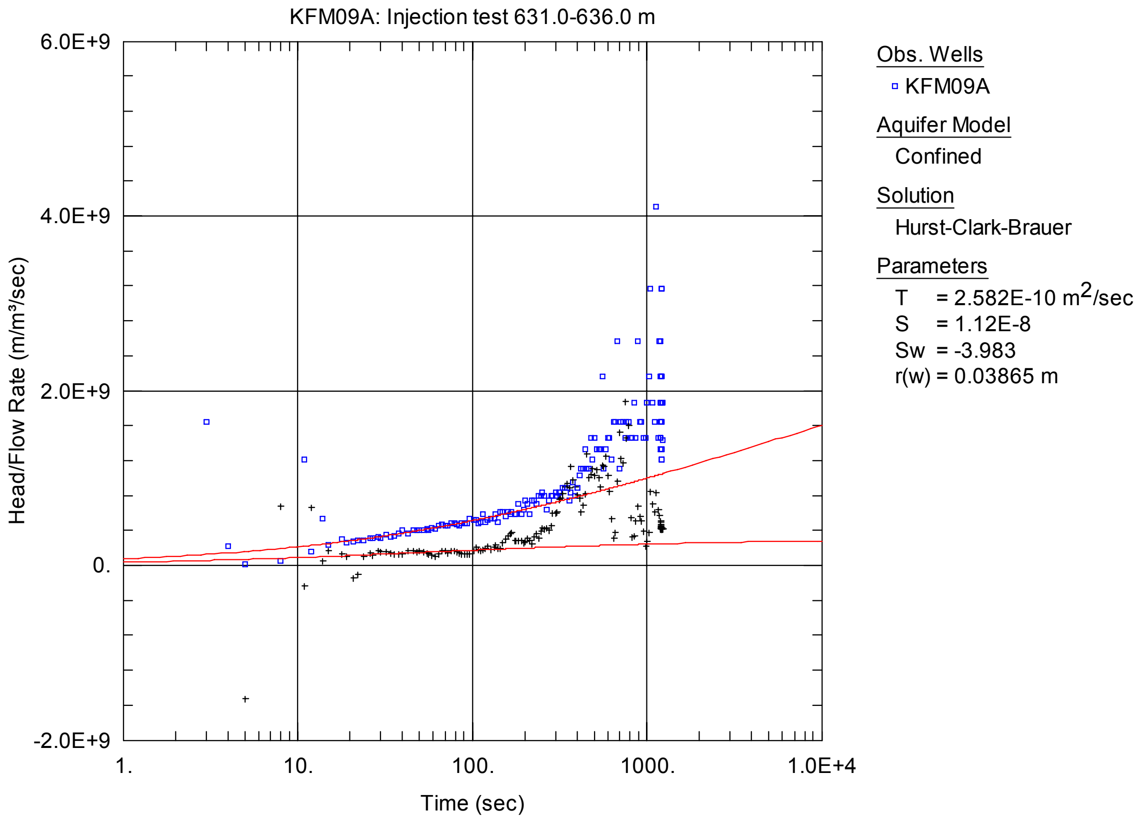


Figure A3-526. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 631.0-636.0 m in KFM09A.*

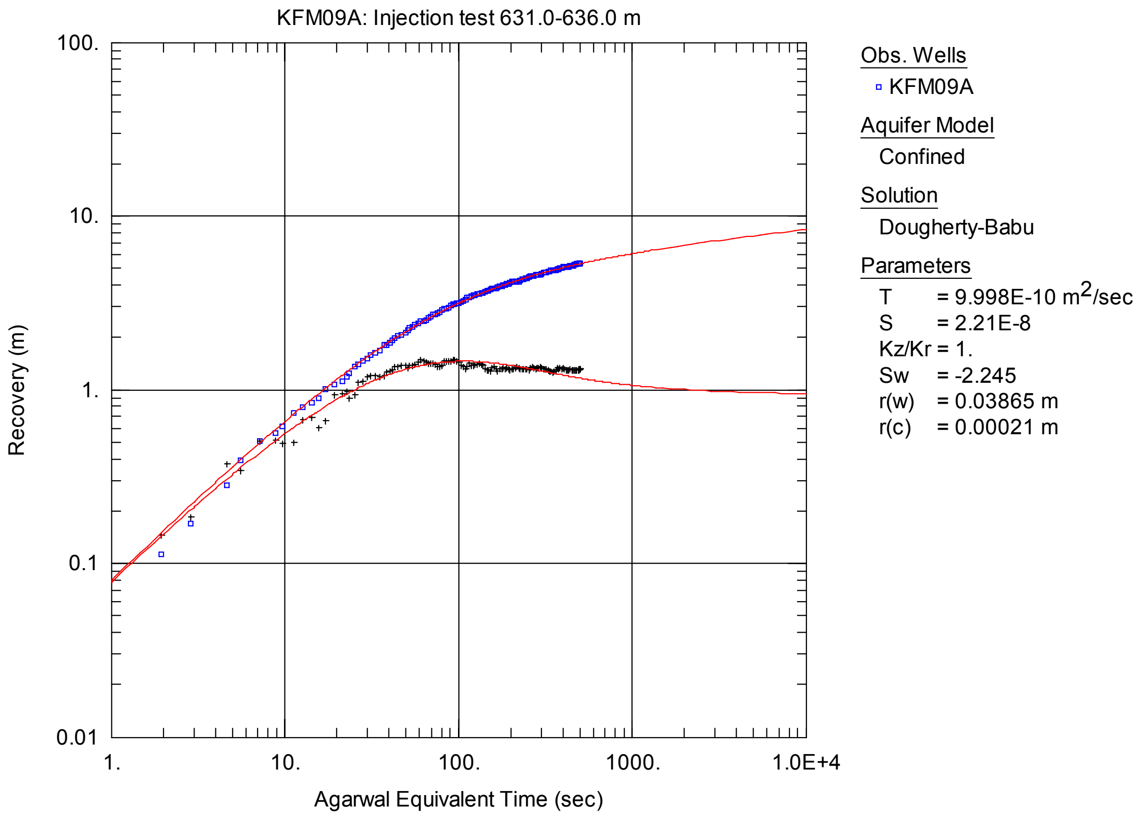


Figure A3-527. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 631.0-636.0 m in KFM09A.*

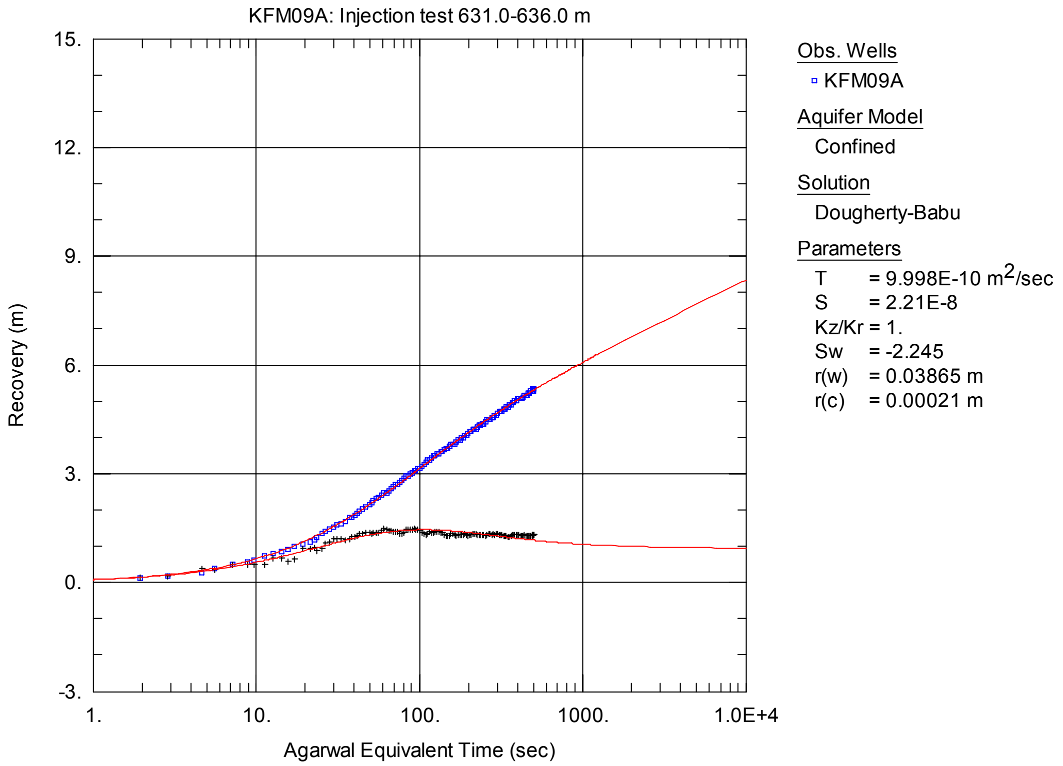


__Figure A3-528.__ Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 631.0-636.0 m in KFM09A.

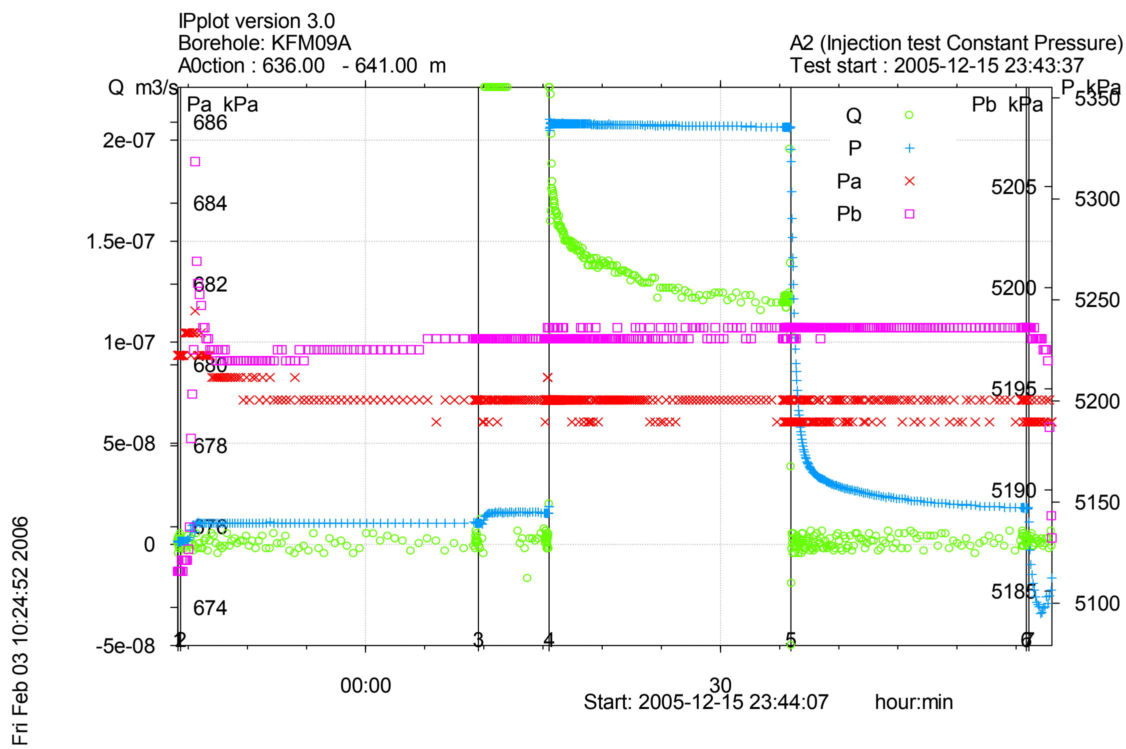


__Figure A3-529.__ Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 636.0-641.0 m in borehole KFM09A.

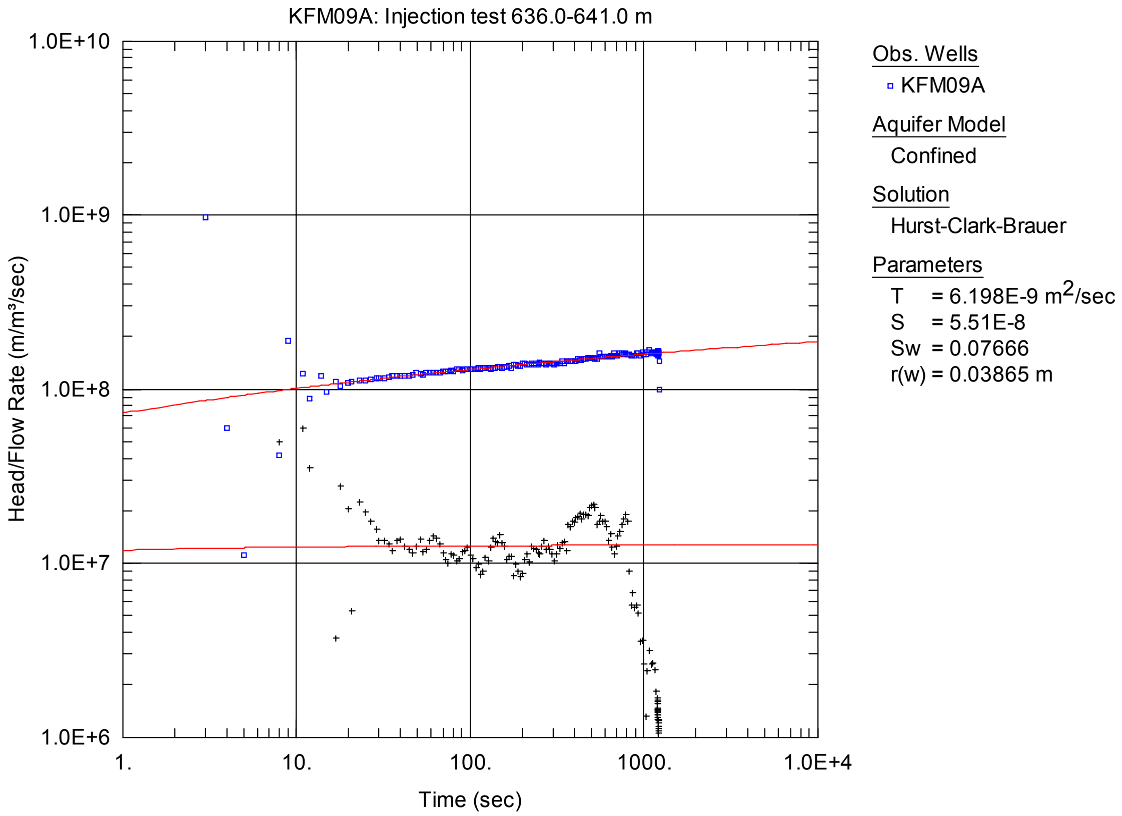


Figure A3-530. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 636.0-641.0 m in KFM09A.*

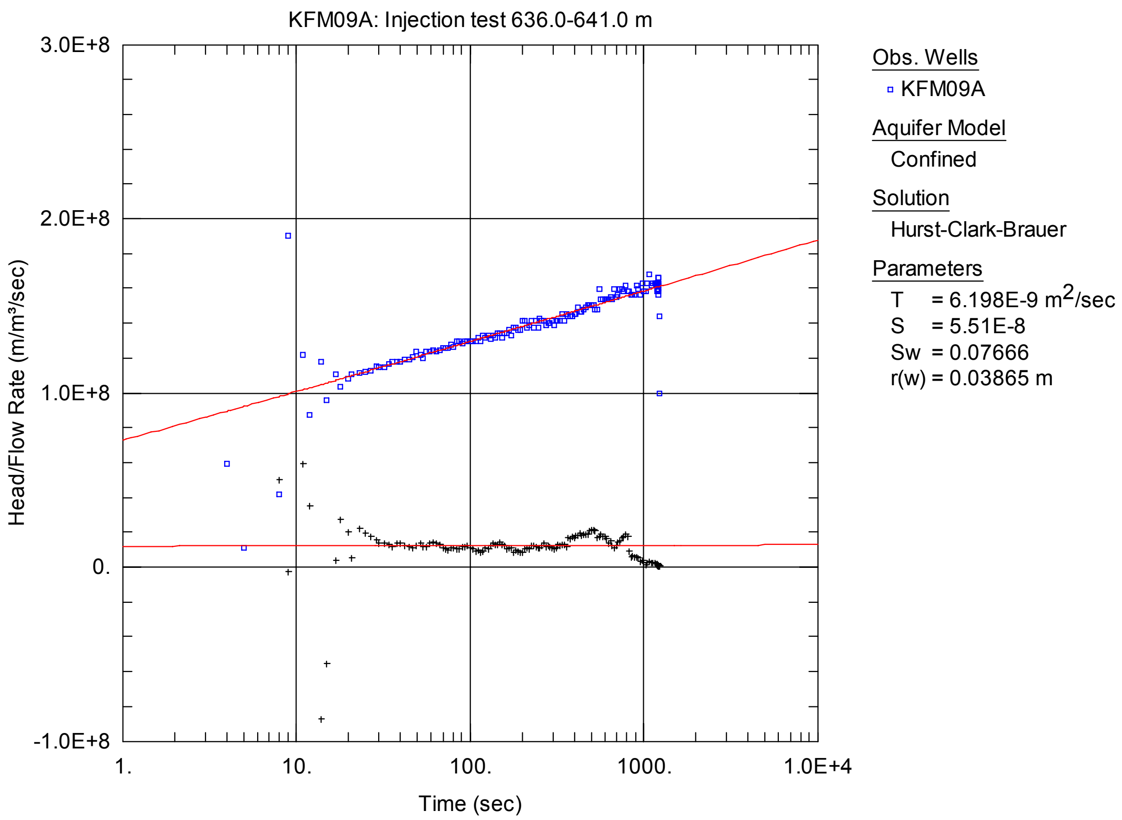


Figure A3-531. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 636.0-641.0 m in KFM09A.*

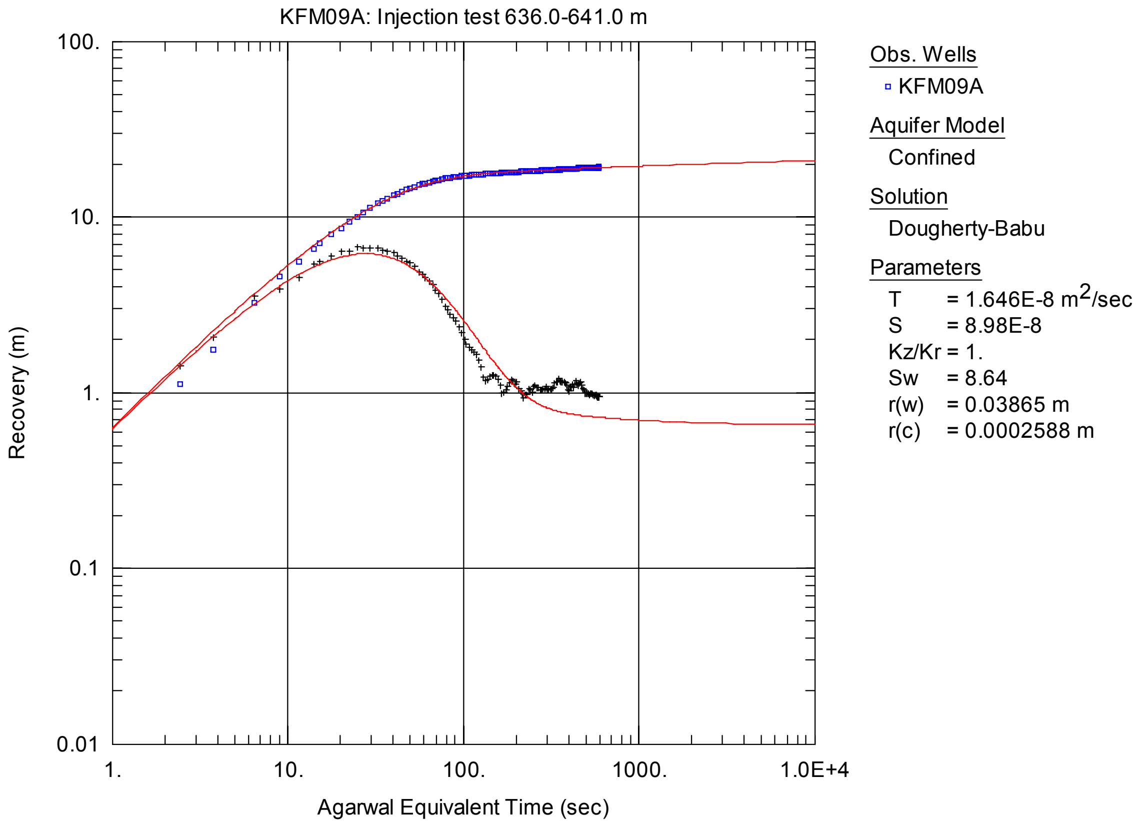


Figure A3-532. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 636.0-641.0 m in KFM09A.*

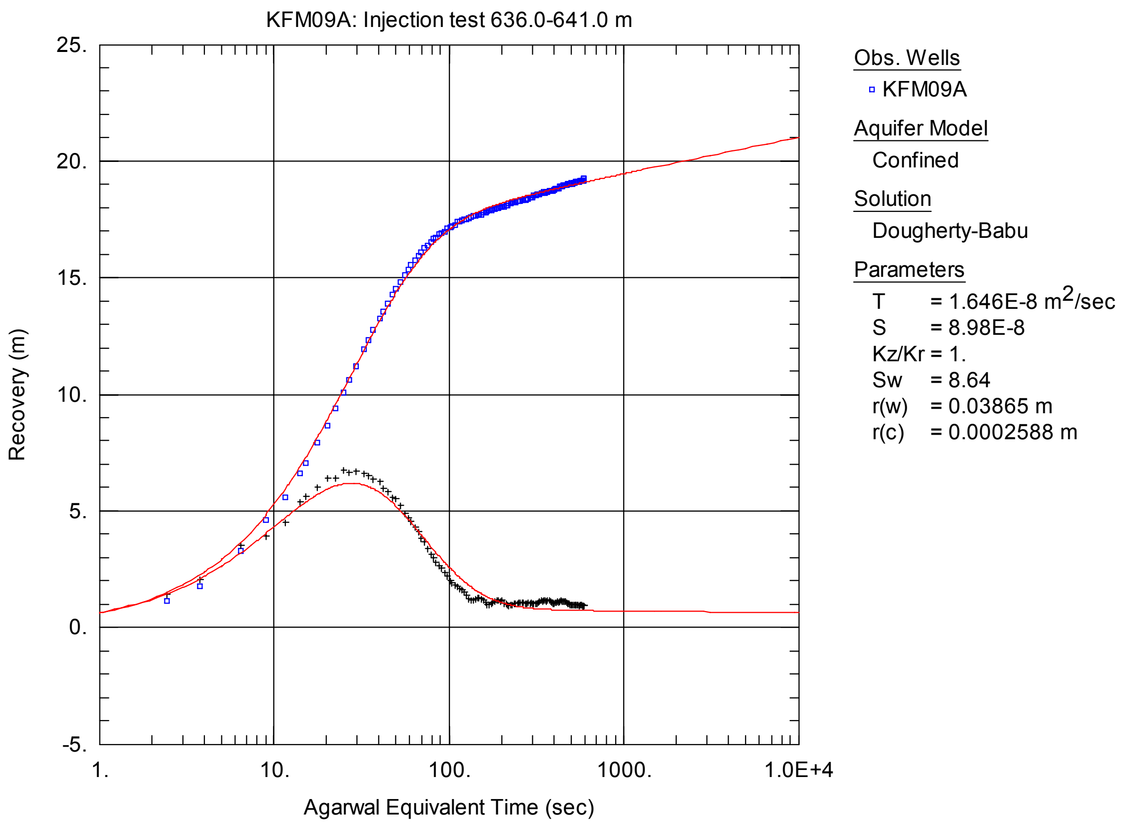


Figure A3-533. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 636.0-641.0 m in KFM09A.*

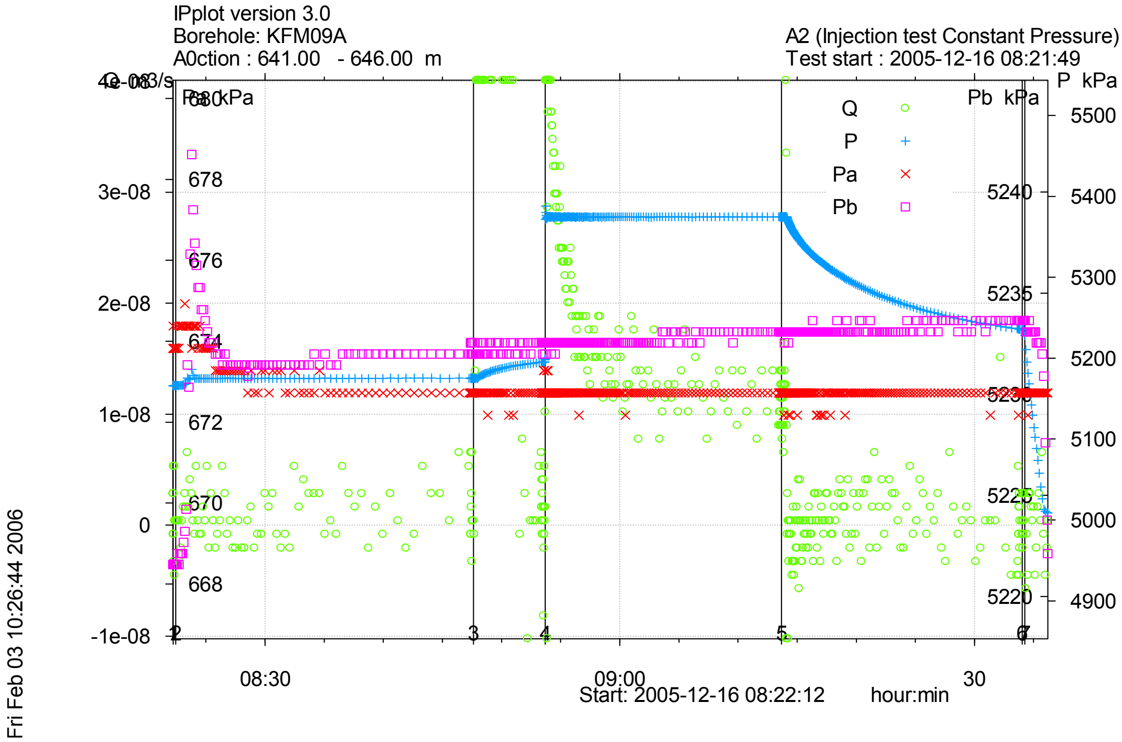


Figure A3-534. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 641.0-646.0 m in borehole KFM09A.

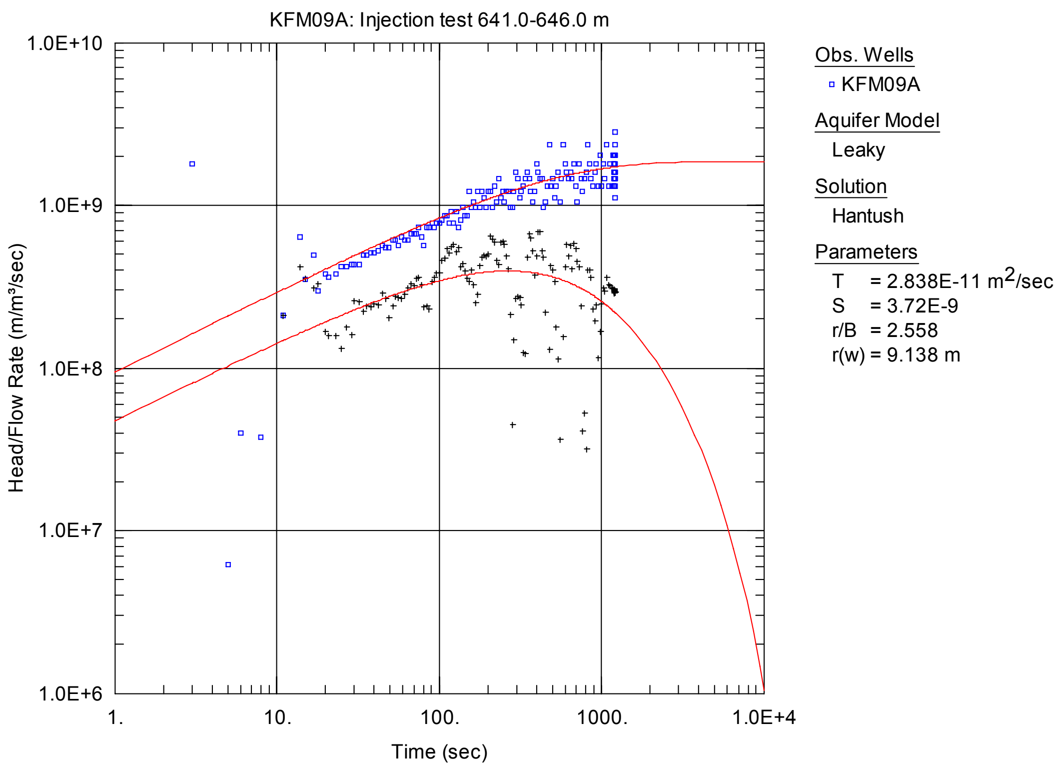


Figure A3-535. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 641.0-646.0 m in KFM09A.

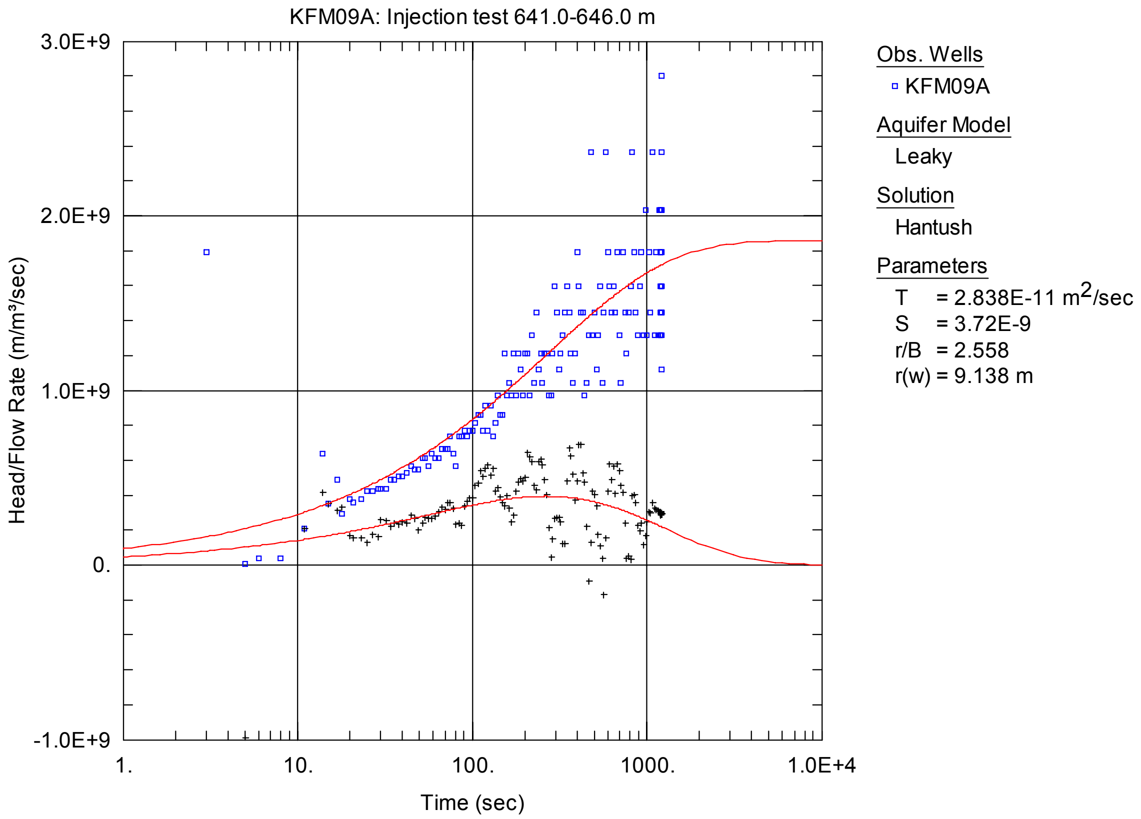


Figure A3-536. Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 641.0-646.0 m in KFM09A.

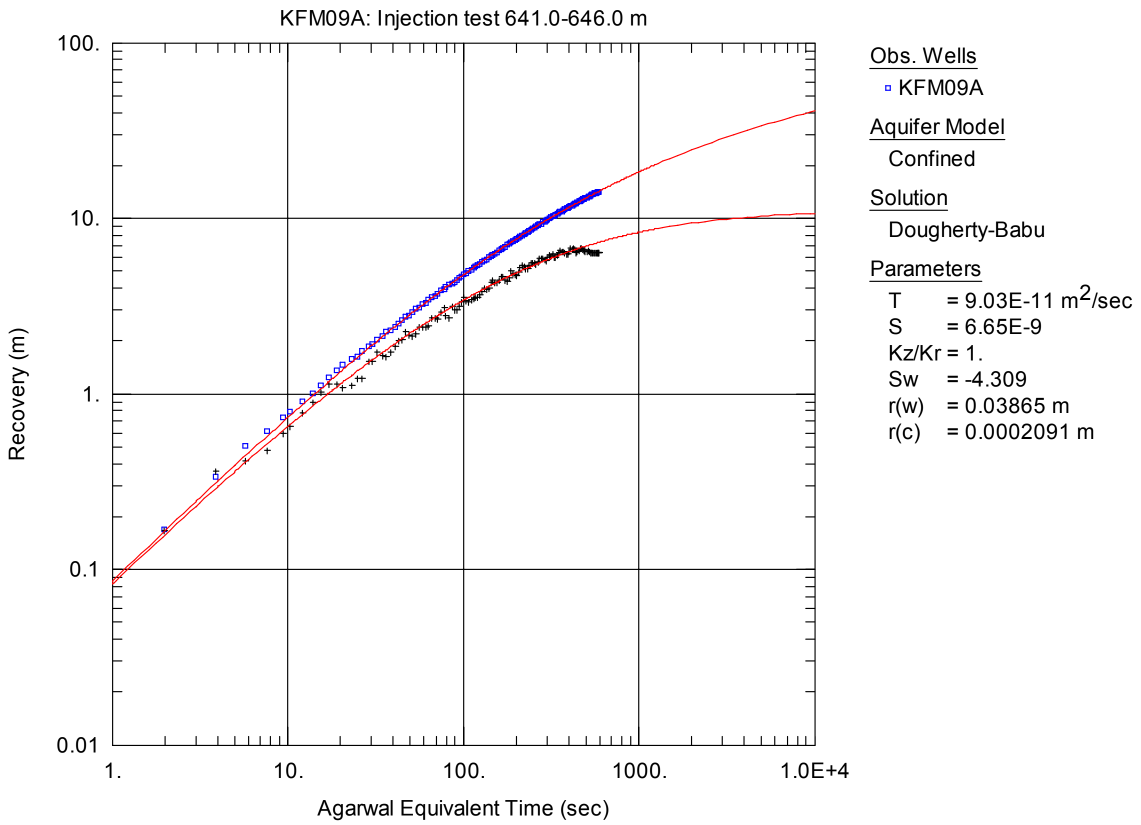


Figure A3-537. Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 641.0-646.0 m in KFM09A.

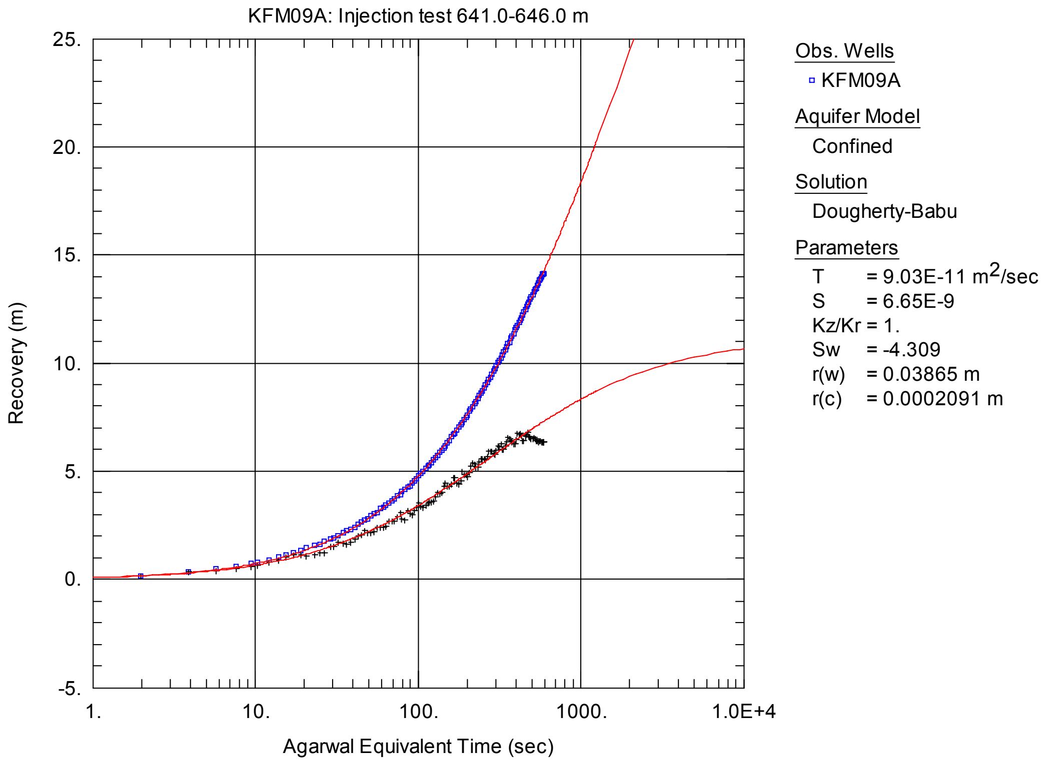


Figure A3-538. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 641.0-646.0 m in KFM09A.*

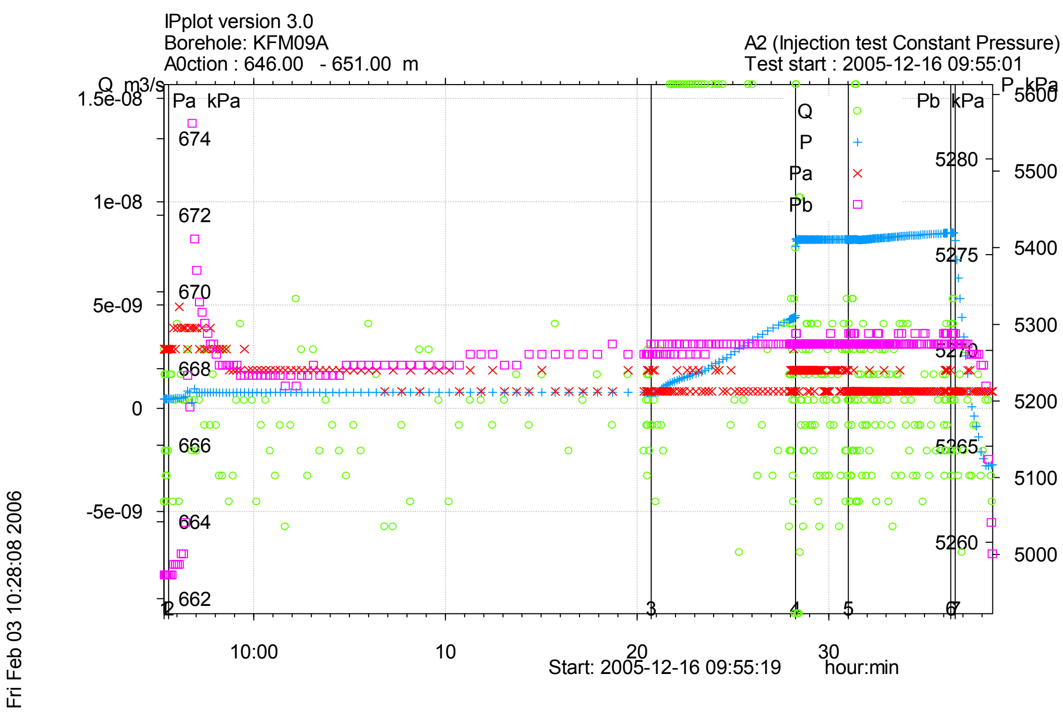


Figure A3-539. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 646.0-651.0 m in borehole KFM09A.*

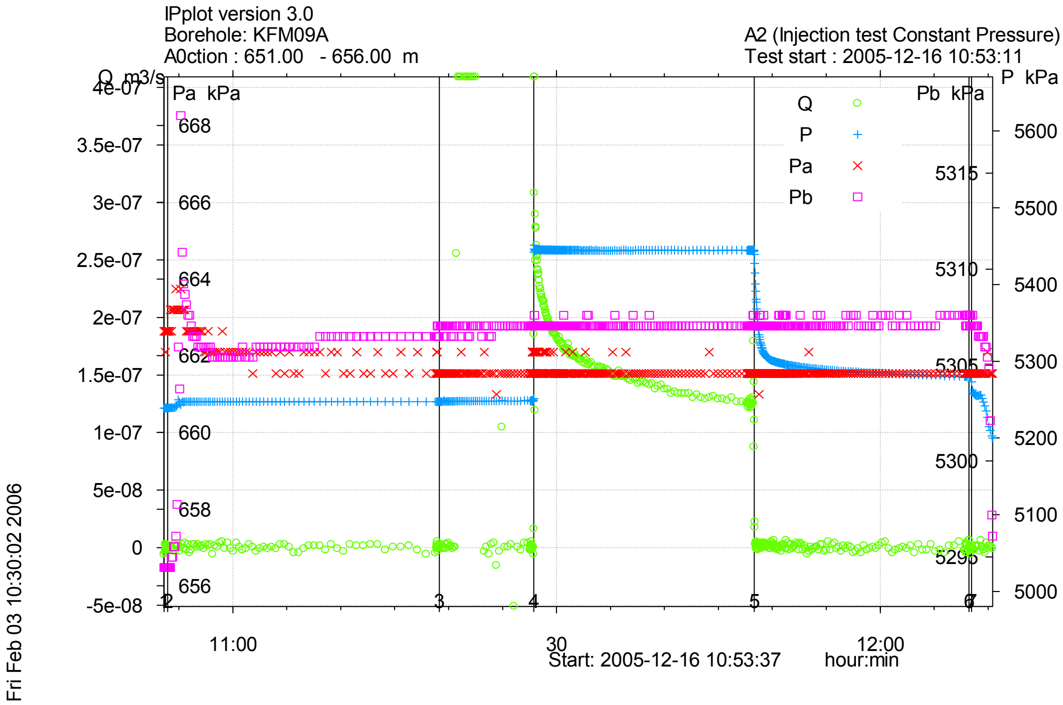


Figure A3-540. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 651.0-656.0 m in borehole KFM09A.*

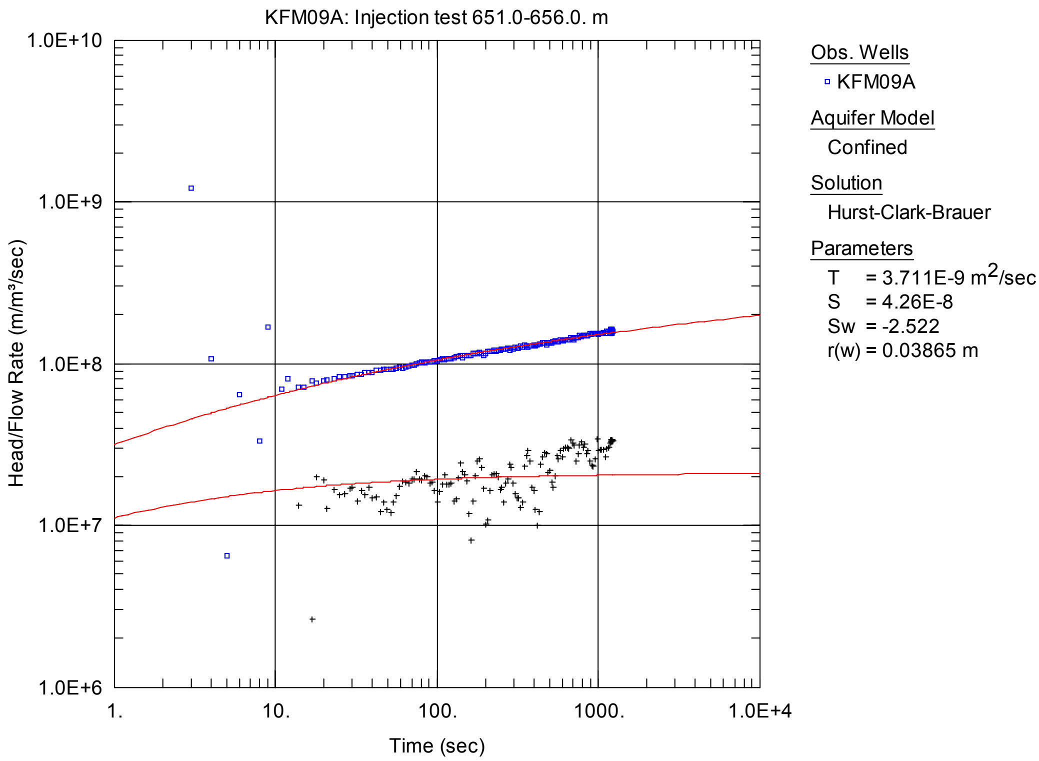


Figure A3-541. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 651.0-656.0 m in KFM09A.*

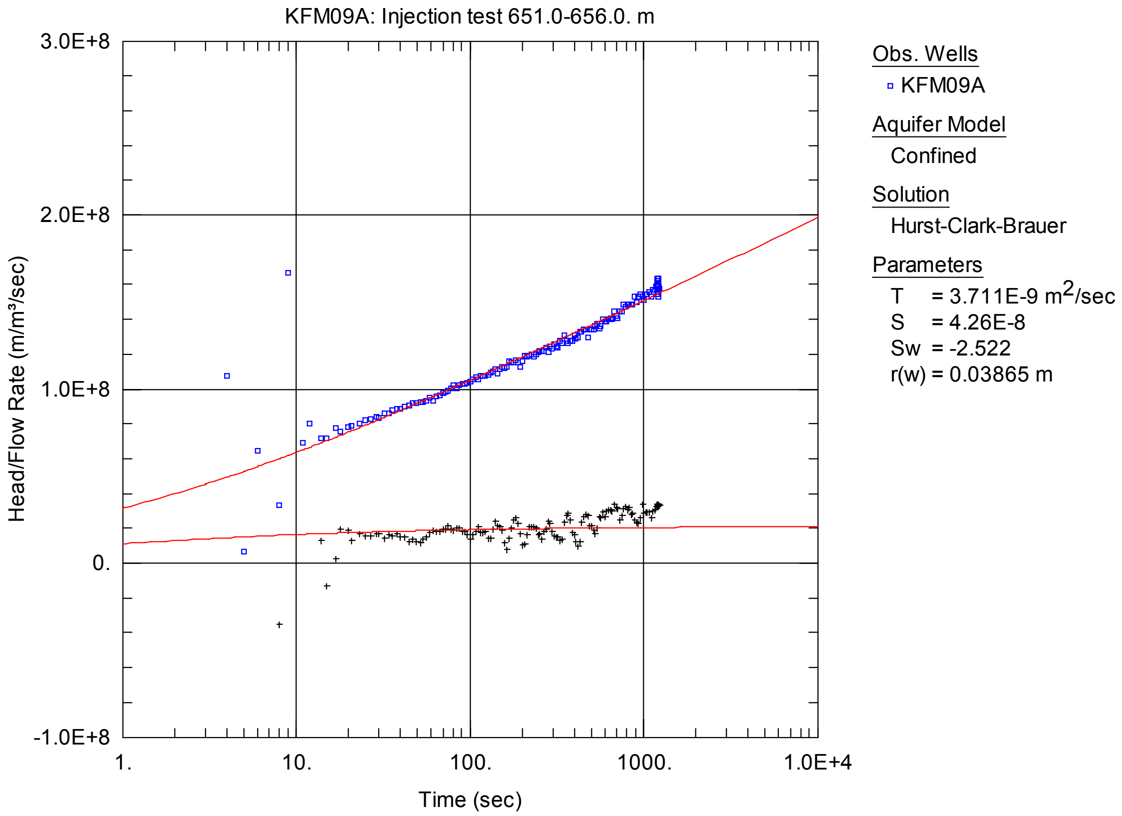


***Figure A3-542.** Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 651.0-656.0 m in KFM09A.*

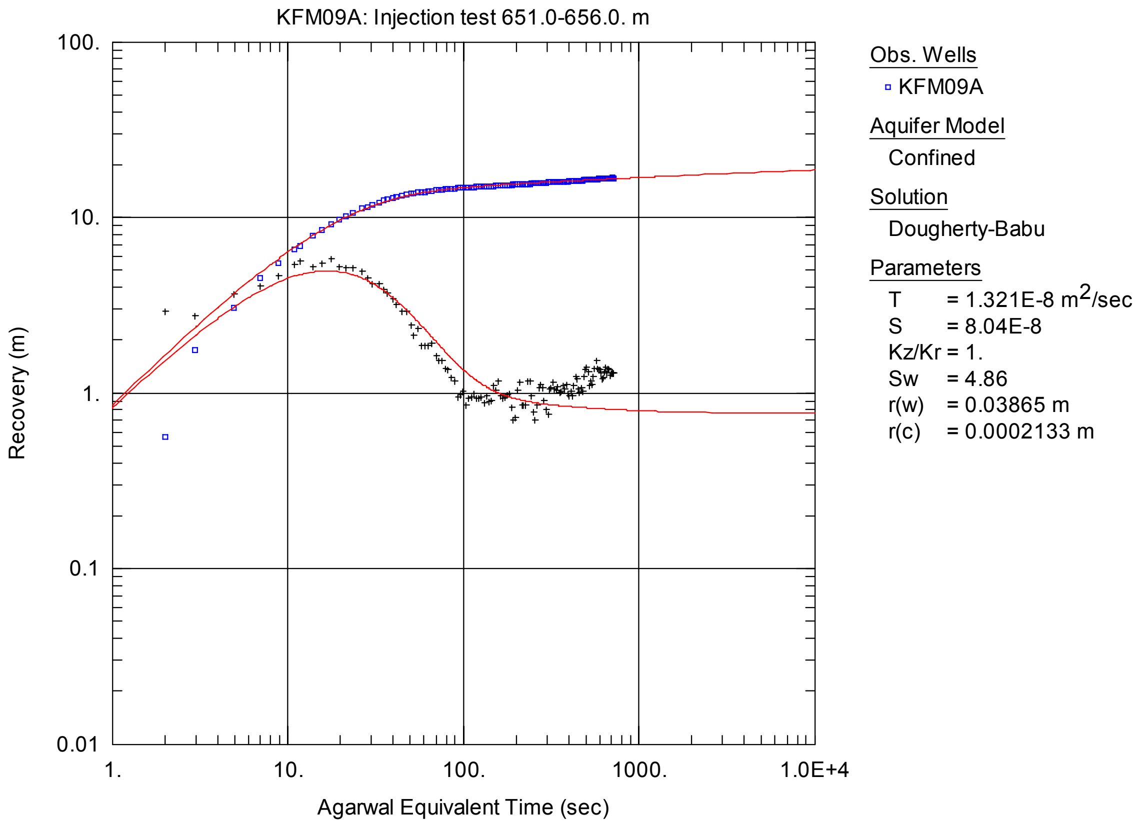


***Figure A3-543.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 651.0-656.0 m in KFM09A.*

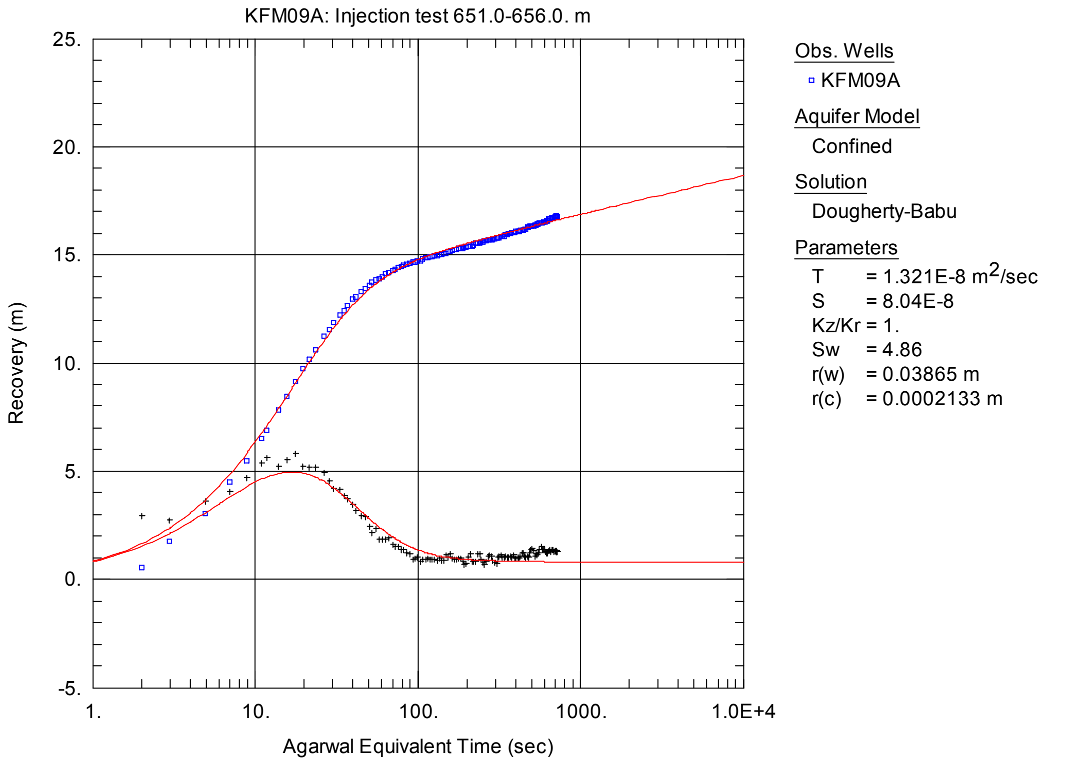


Figure A3-544. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 651.0-656.0 m in KFM09A.*

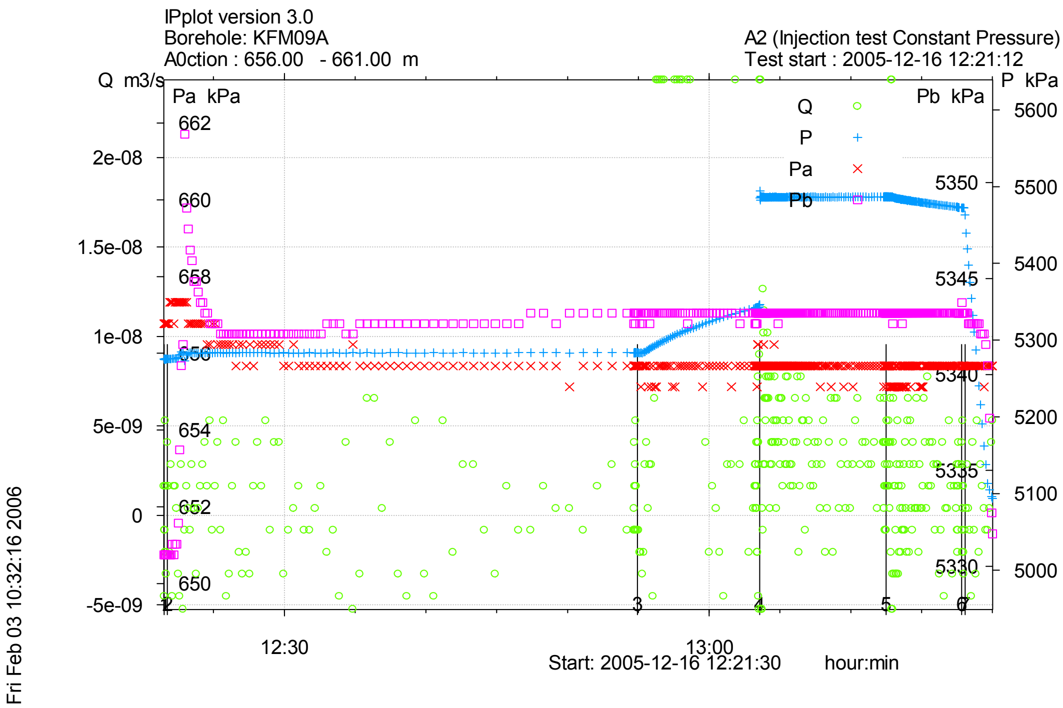


Figure A3-545. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 656.0-661.0 m in borehole KFM09A.*

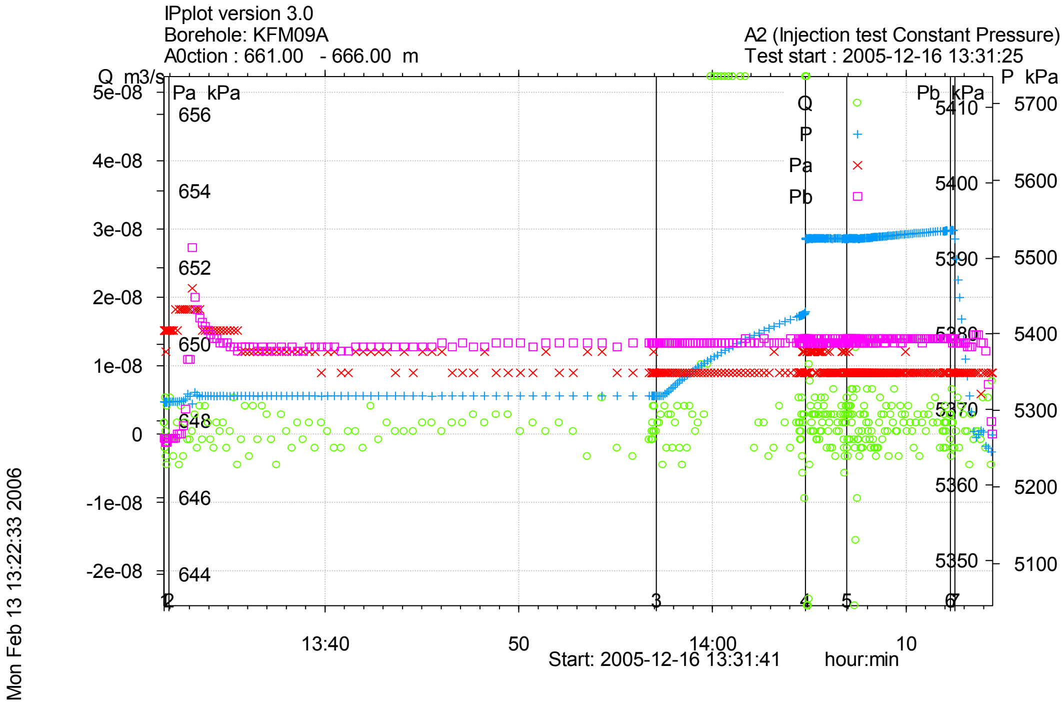


Figure A3-546. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 661.0-666.0 m in borehole KFM09A.*

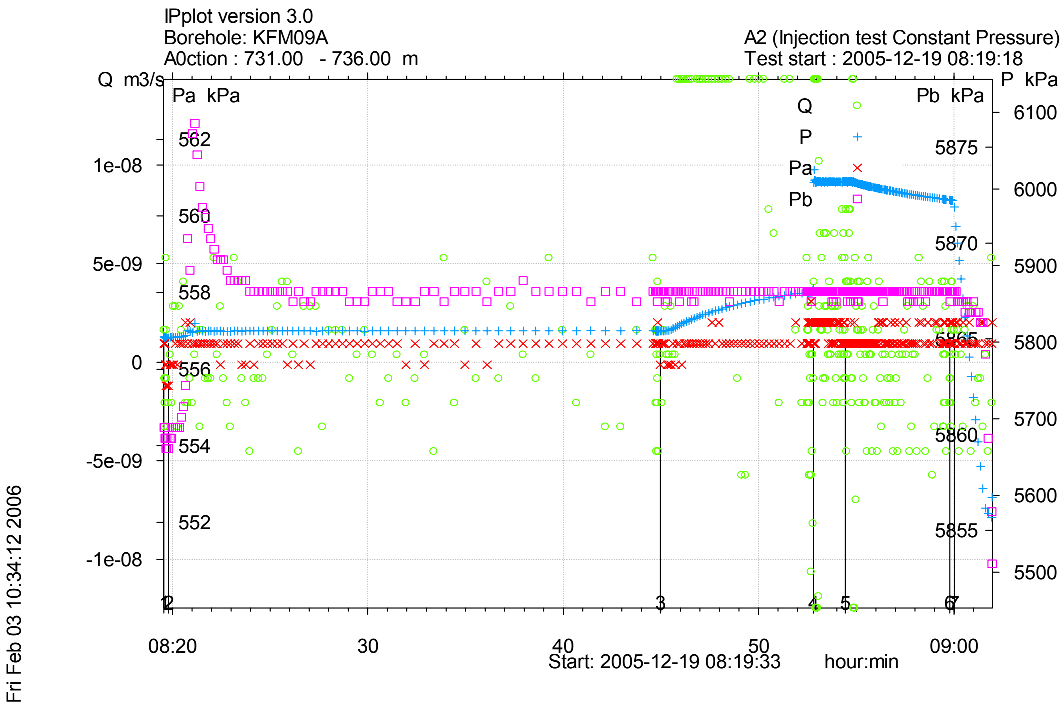


Figure A3-547. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 731.0-736.0 m in borehole KFM09A.*

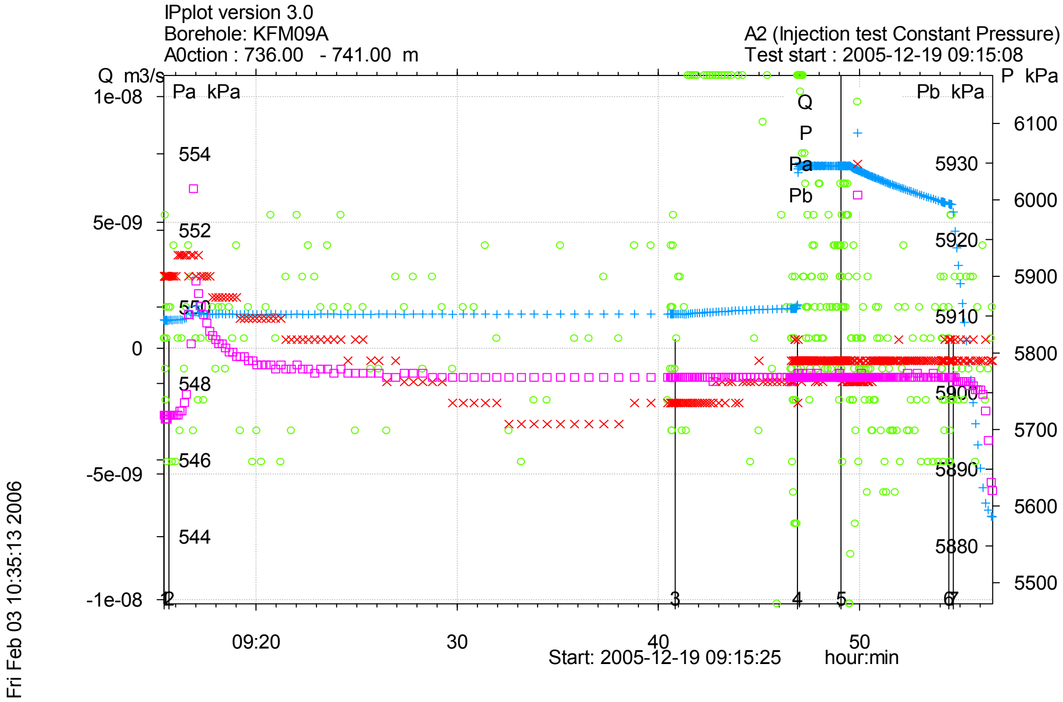


Figure A3-548. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 736.0-741.0 m in borehole KFM09A.*

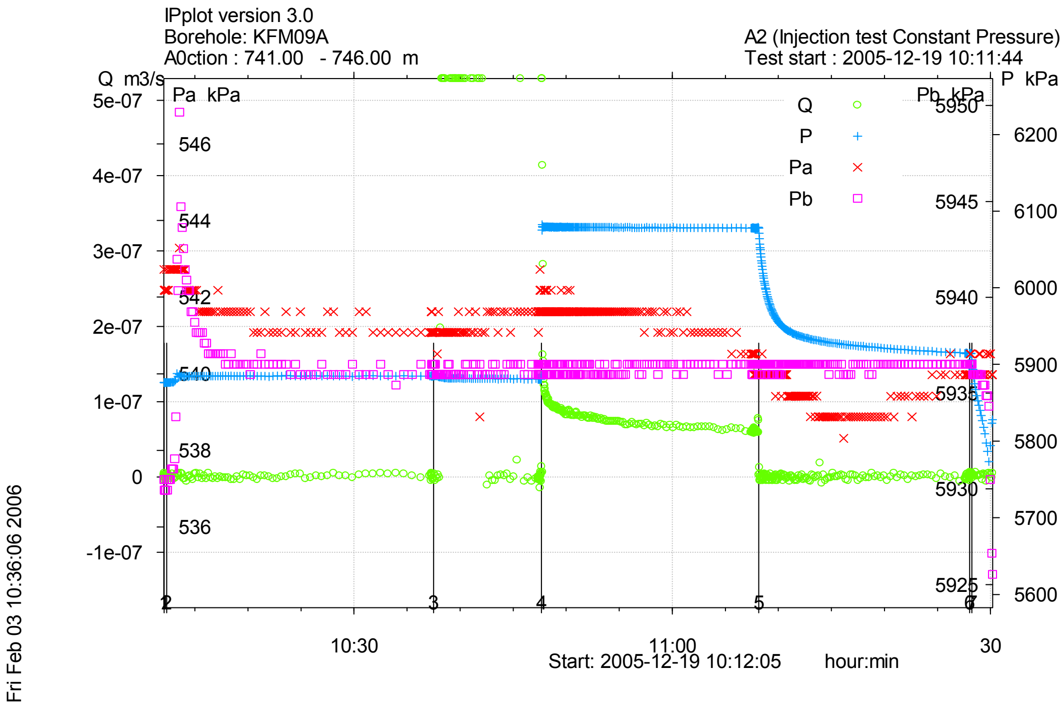


Figure A3-549. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 741.0-746.0 m in borehole KFM09A.*

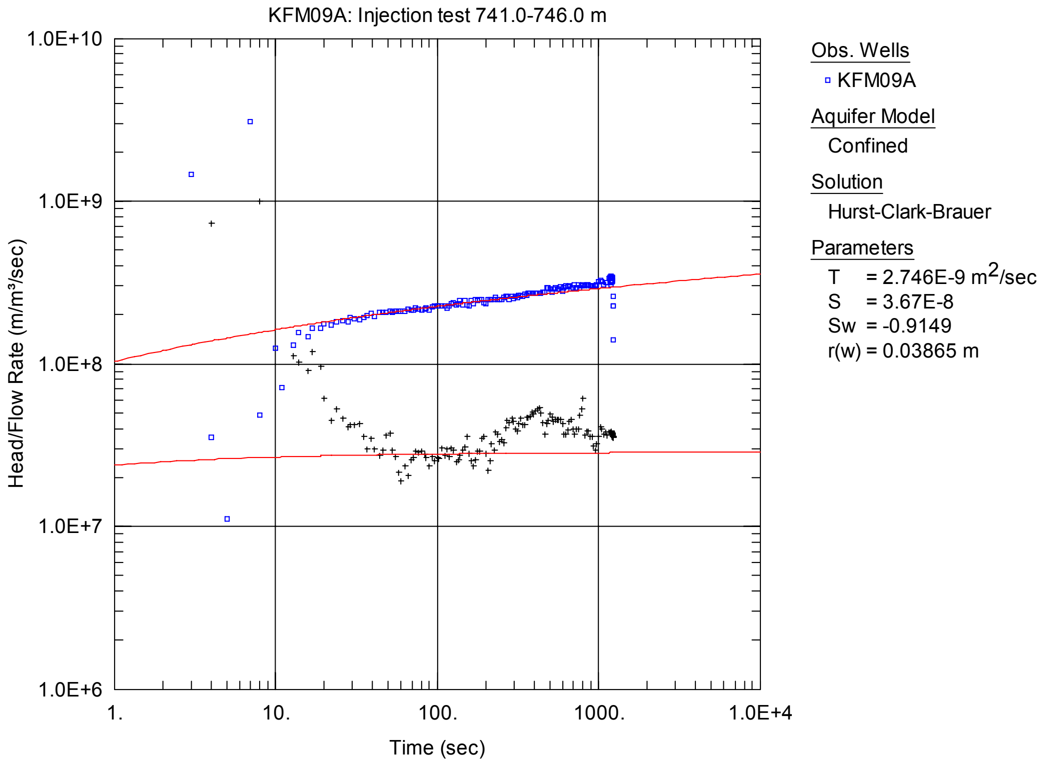


Figure A3-550. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 741.0-746.0 m in KFM09A. This plot shows a fit to the first of two different PRF:s during the injection period in this section.*

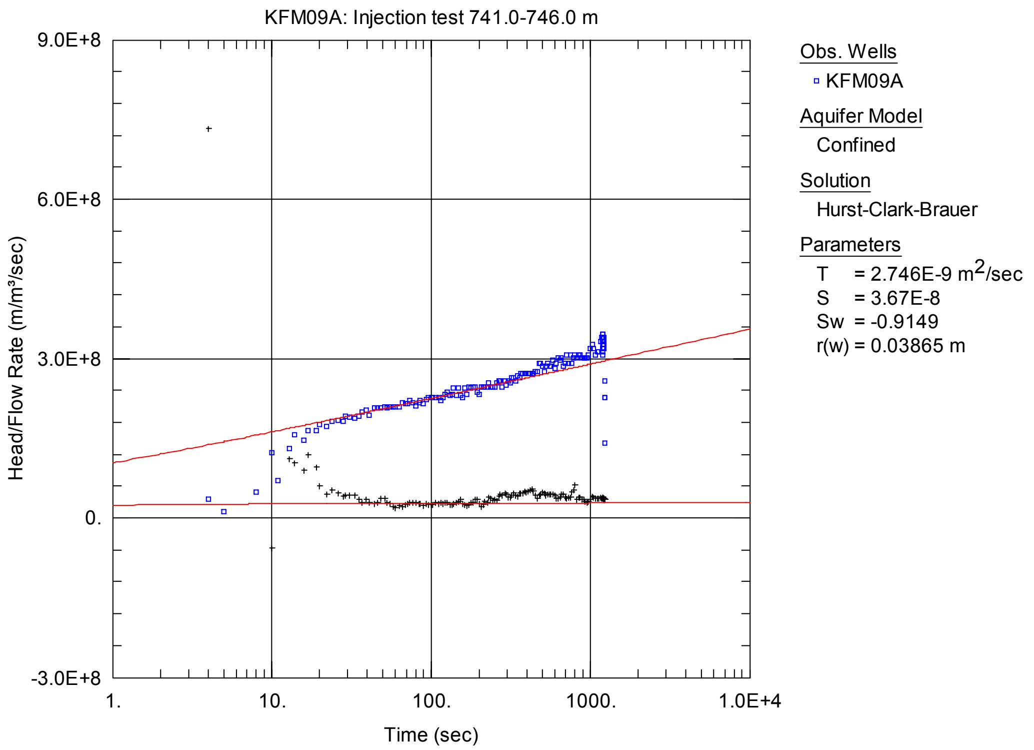


Figure A3-551. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 741.0-746.0 m in KFM09A. This plot shows a fit to the first of two different PRF:s during the injection period in this section.*

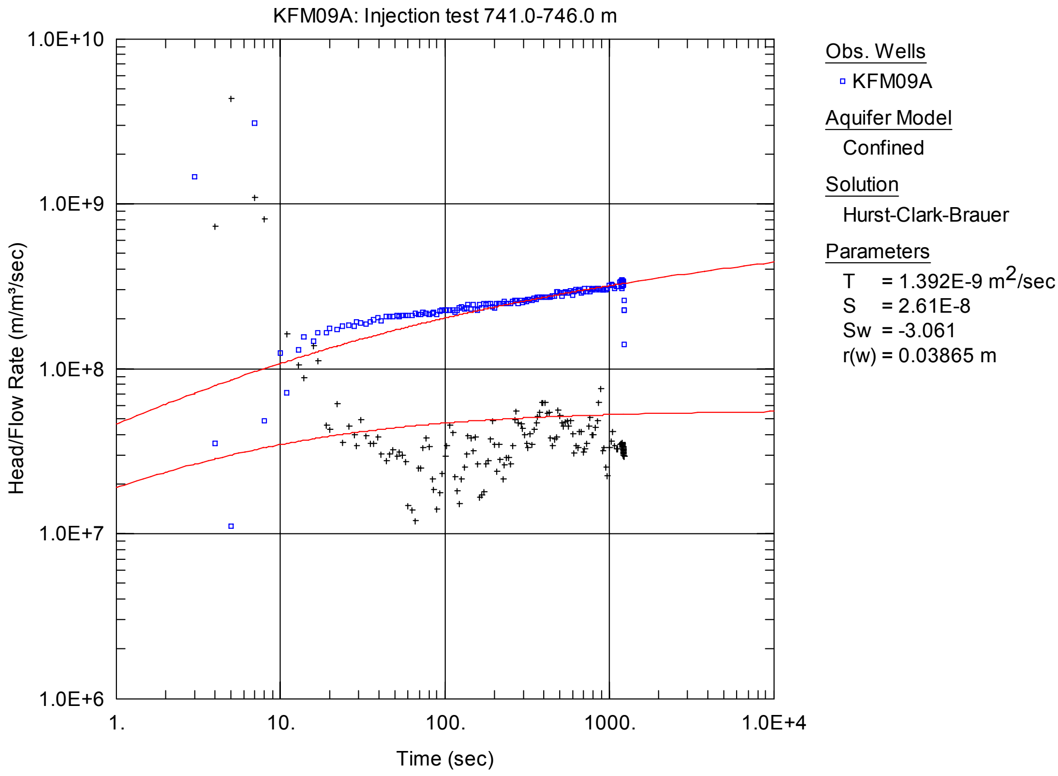


Figure A3-552. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 741.0-746.0 m in KFM09A. This plot shows a fit to the second of two different PRF:s during the injection period in this section.*

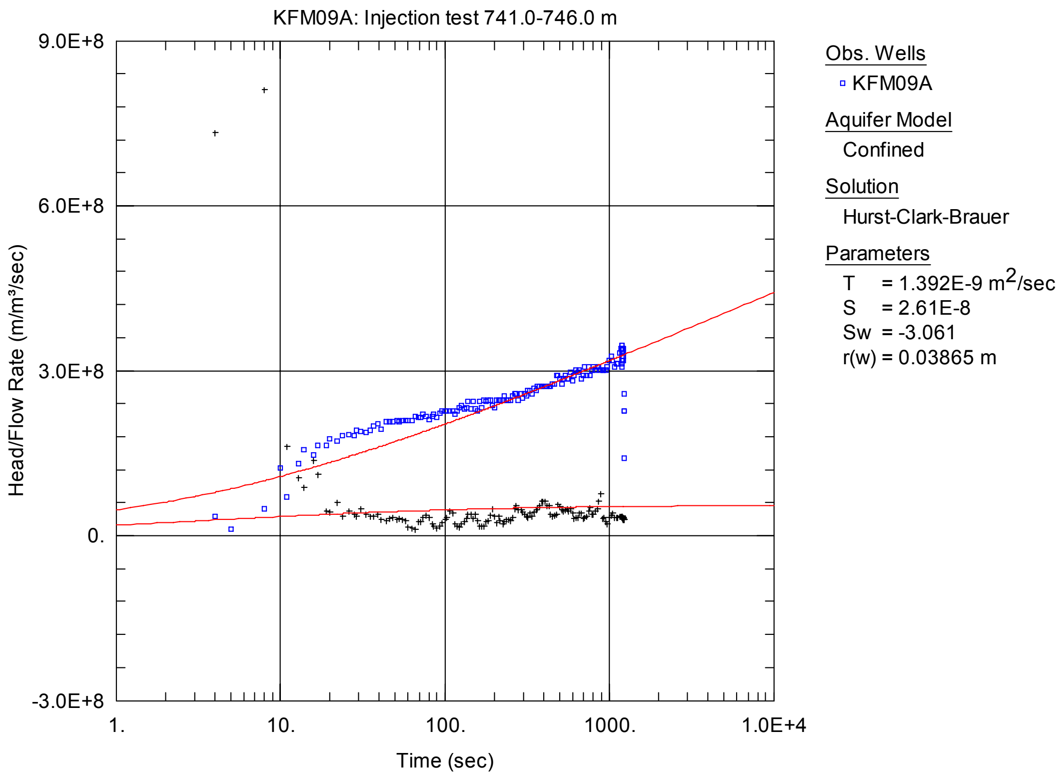


Figure A3-553. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 741.0-746.0 m in KFM09A. This plot shows a fit to the second of two different PRF:s during the injection period in this section.*

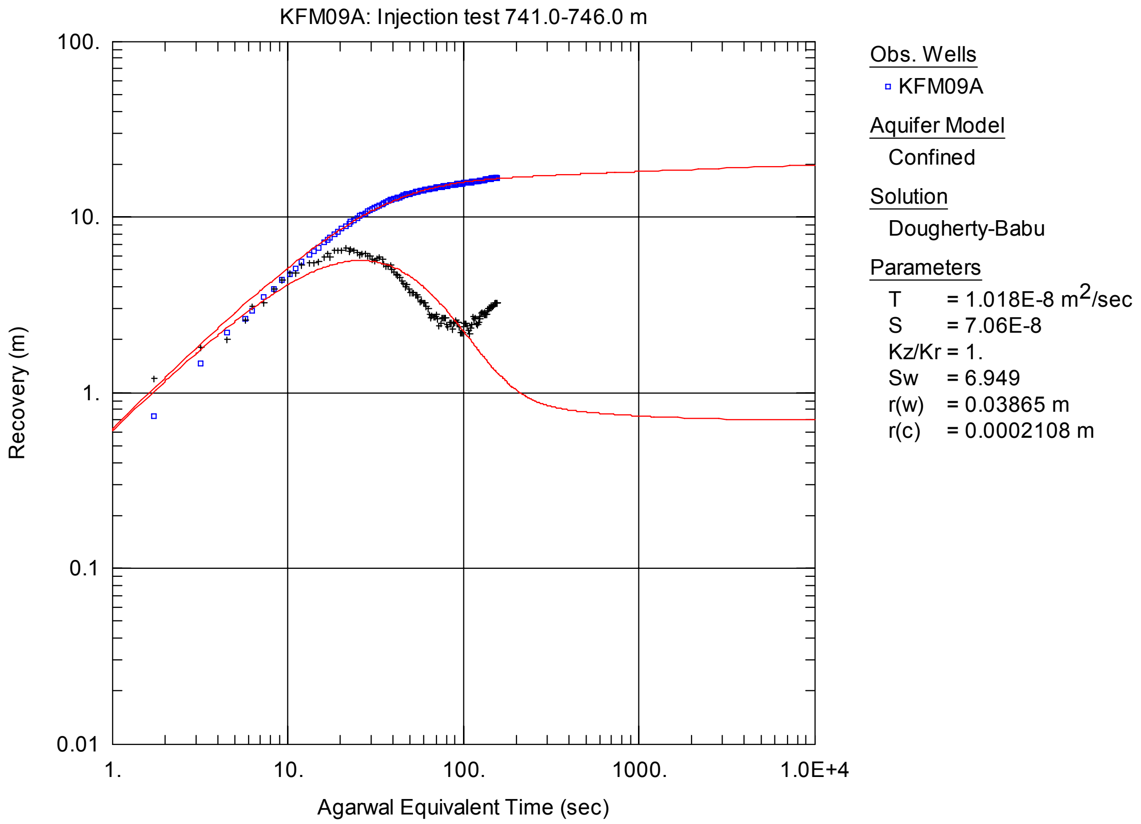


Figure A3-554. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 741.0-746.0 m in KFM09A.*

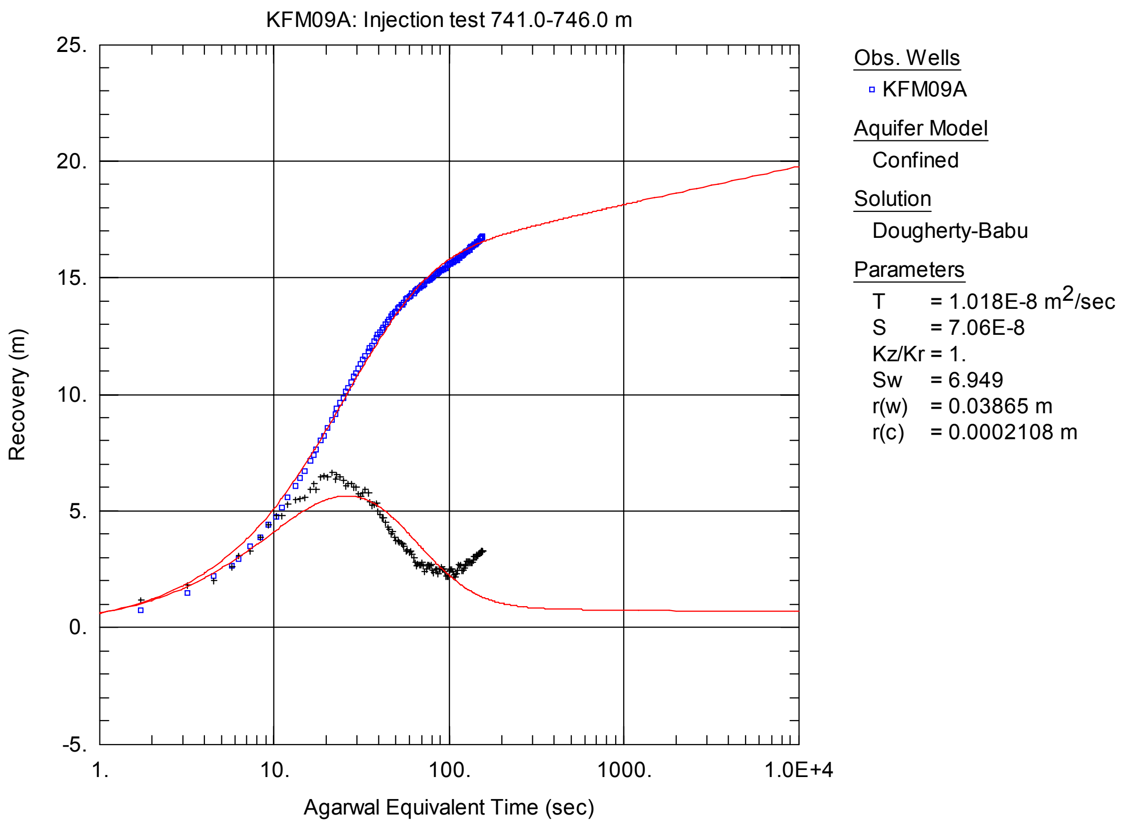


Figure A3-555. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 741.0-746.0 m in KFM09A.*

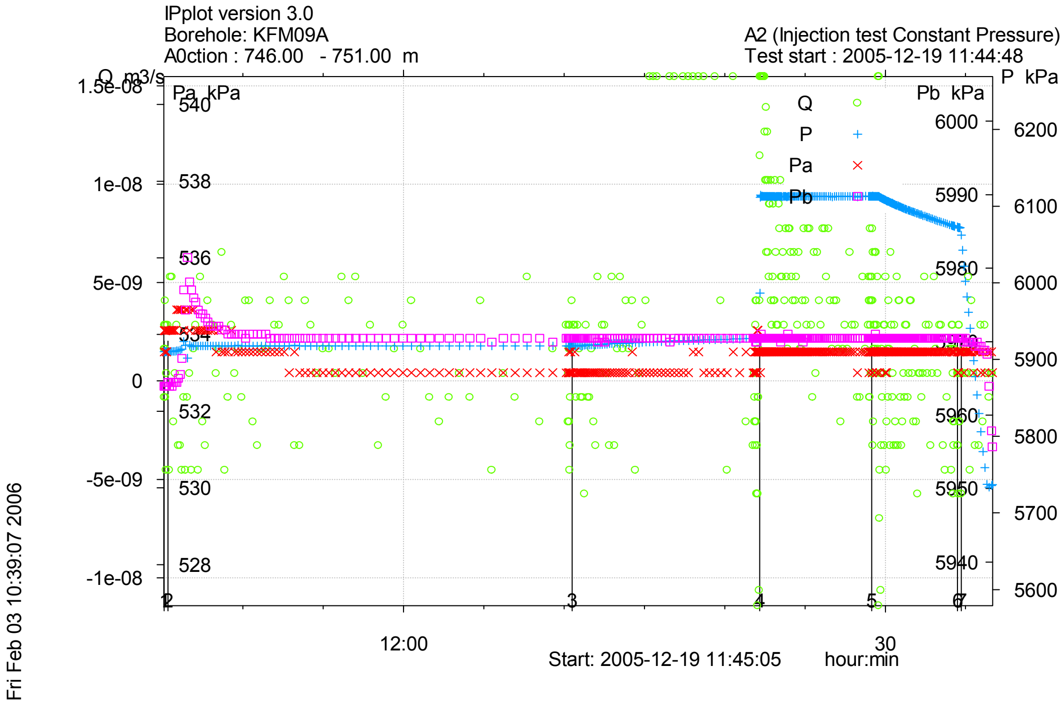


Figure A3-556. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 746.0-751.0 m in borehole KFM09A.*

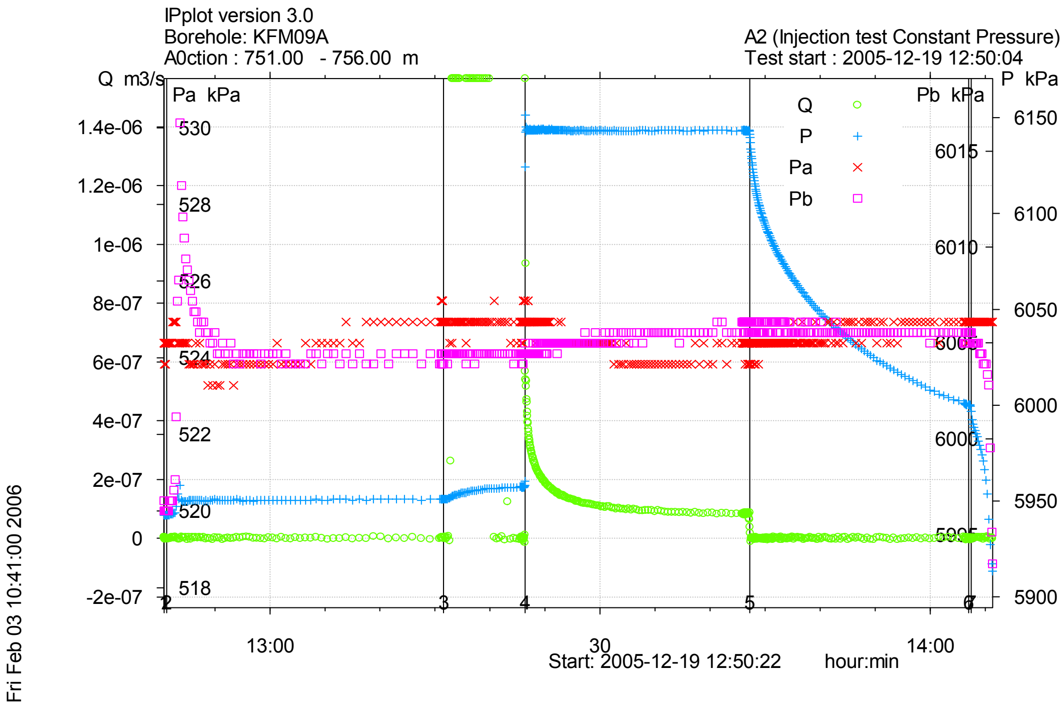


Figure A3-557. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 751.0-756.0 m in borehole KFM09A.*

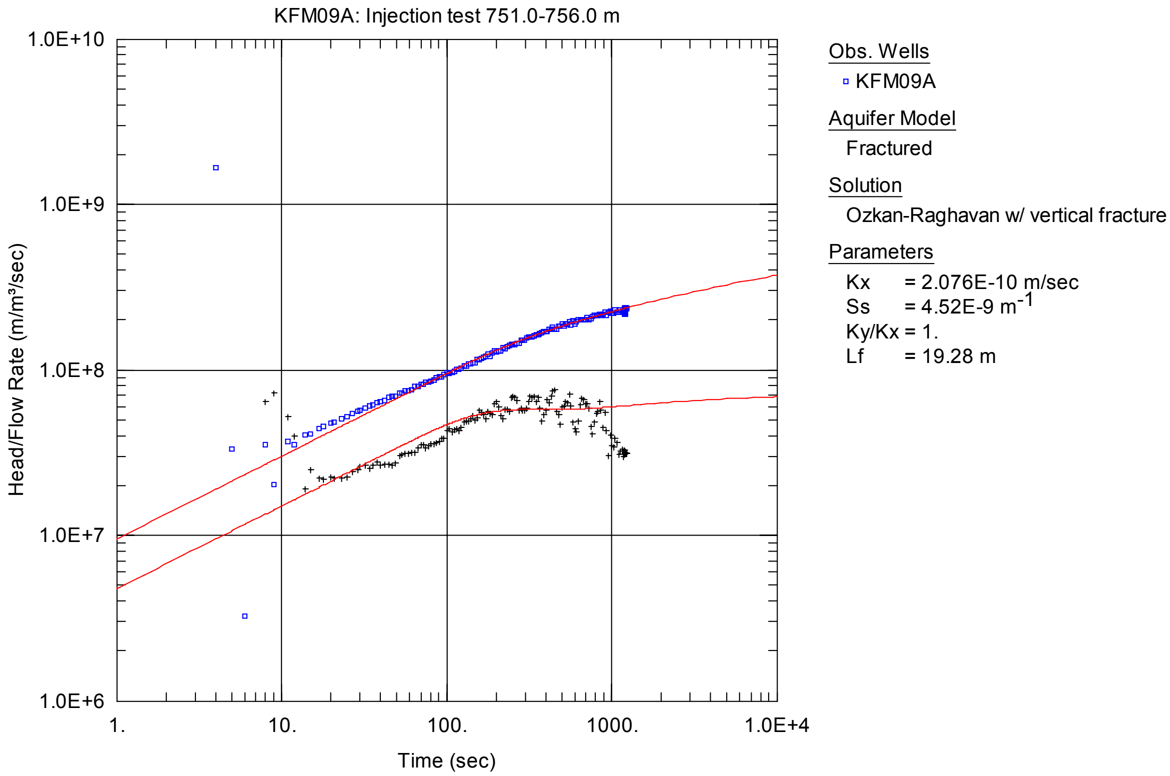


Figure A3-558. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 751.0-756.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

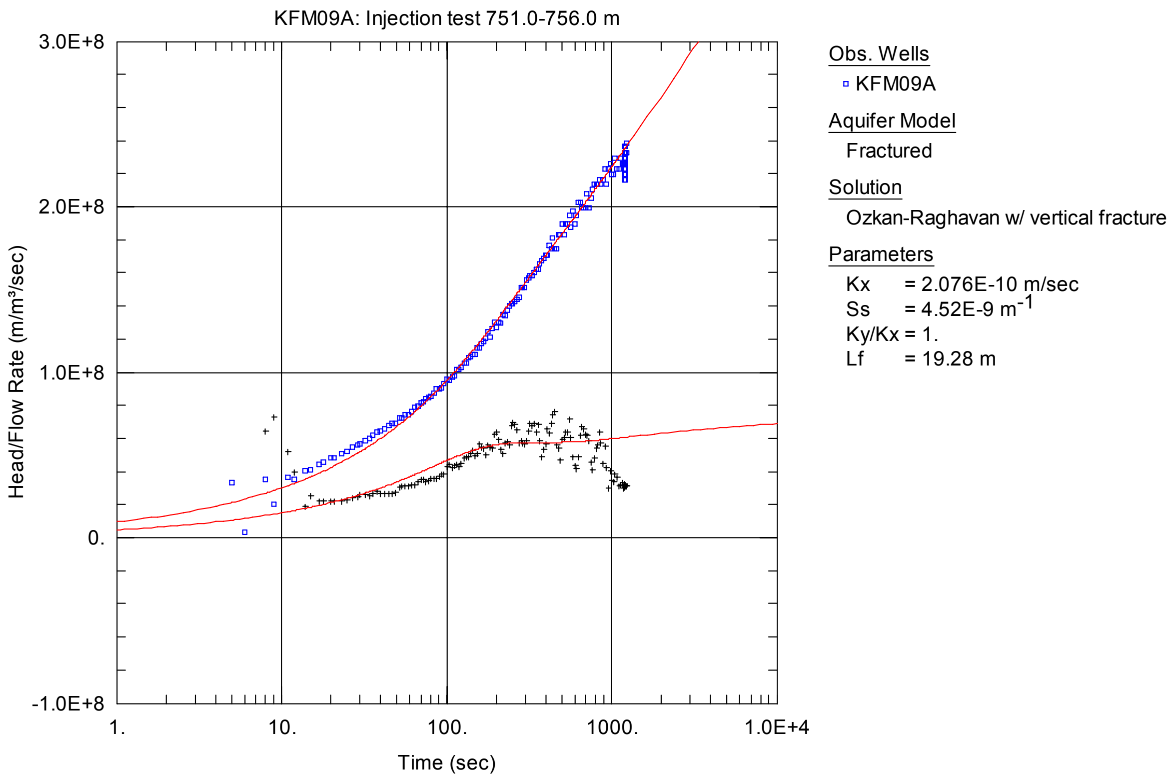


Figure A3-559. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 751.0-756.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

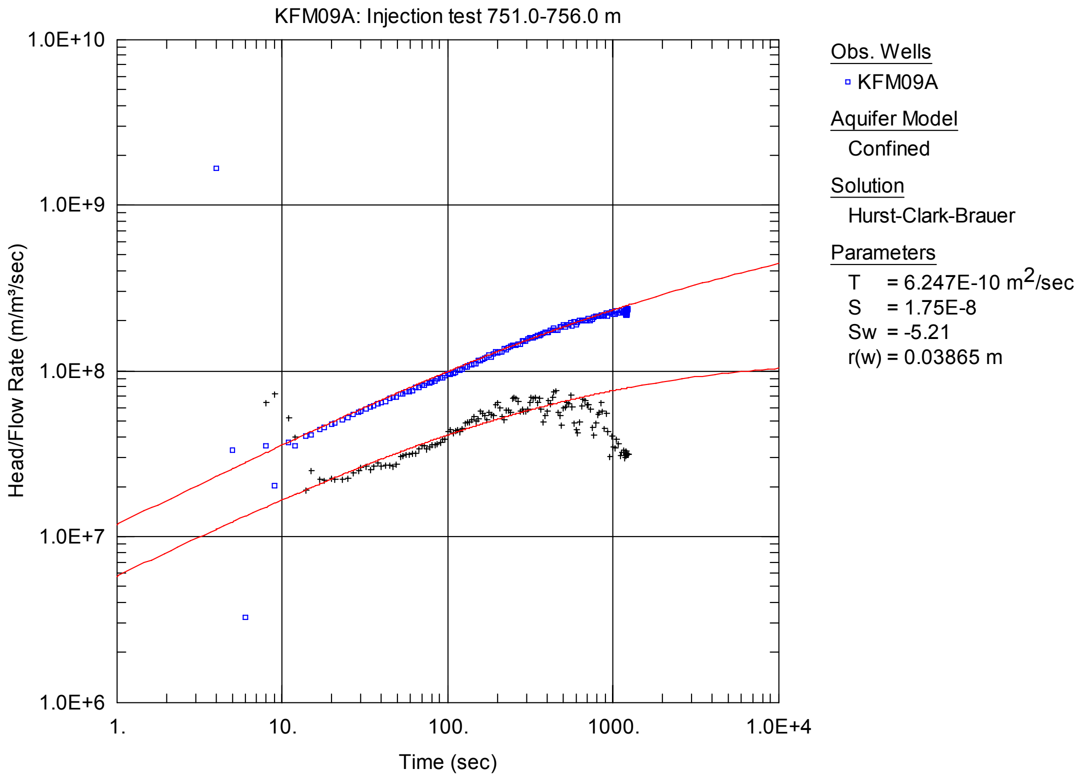


Figure A3-560. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 751.0-756.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for a pseudo-radial response.*

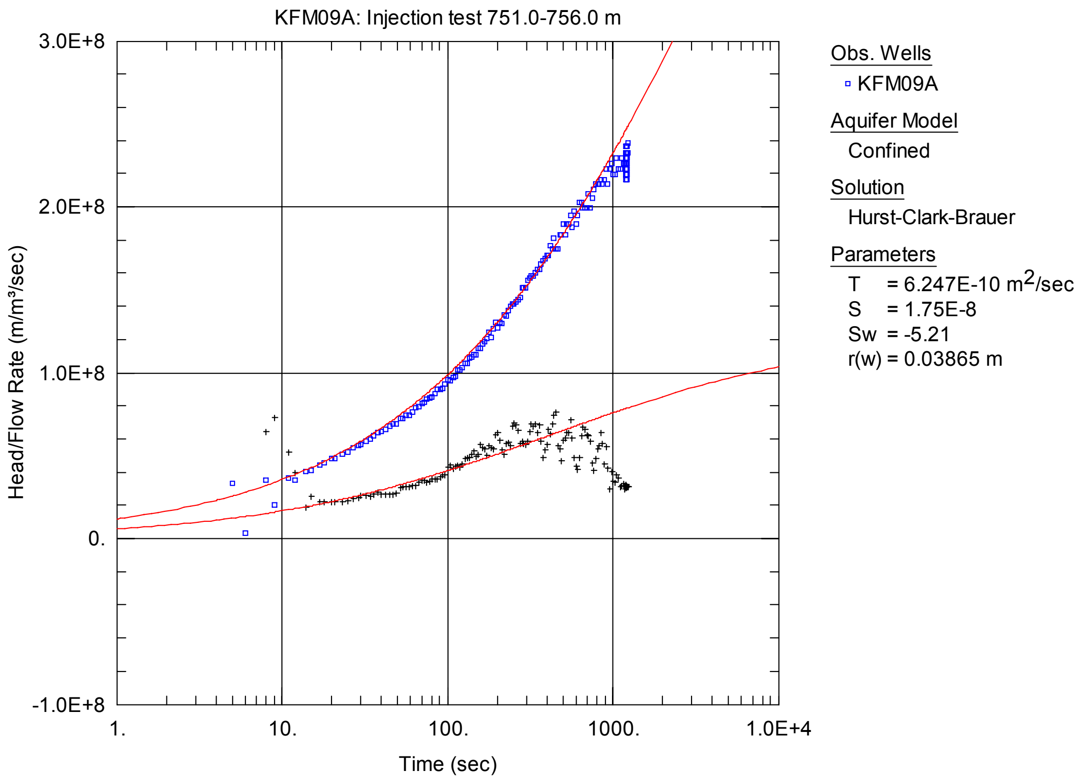


Figure A3-561. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 751.0-756.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for a pseudo-radial response.*

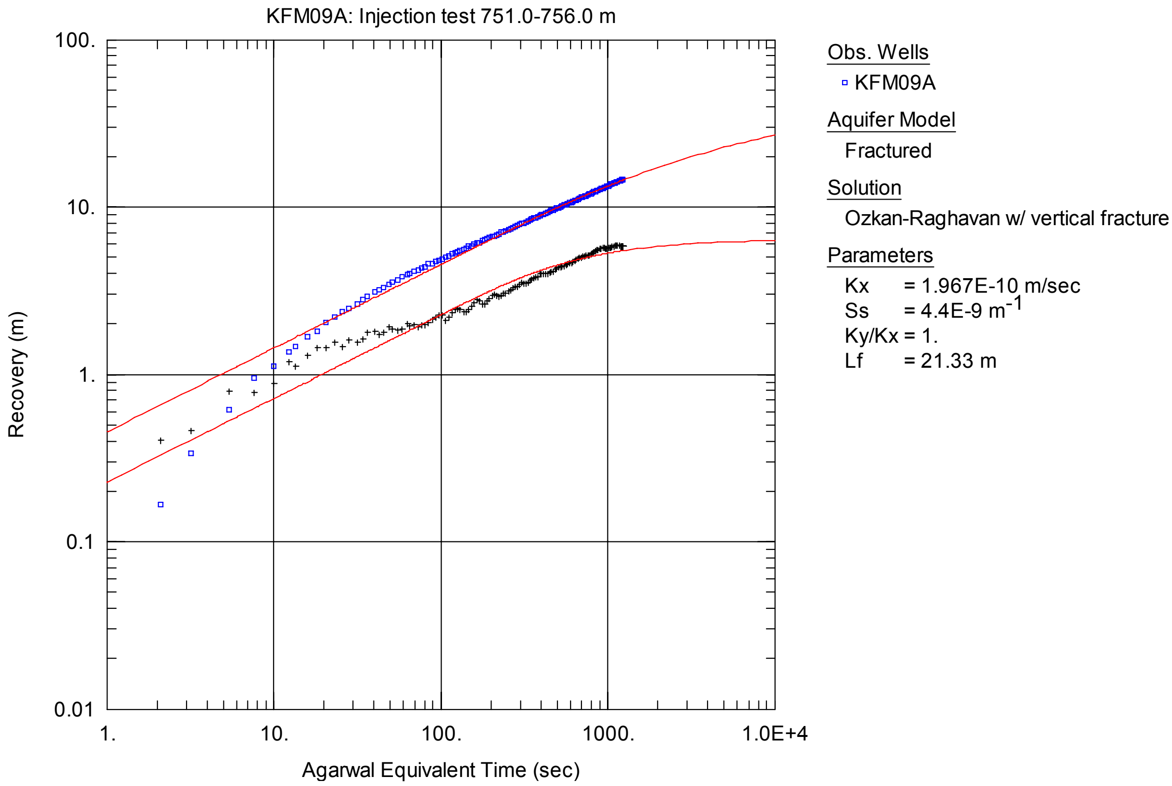


Figure A3-562. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 751.0-756.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

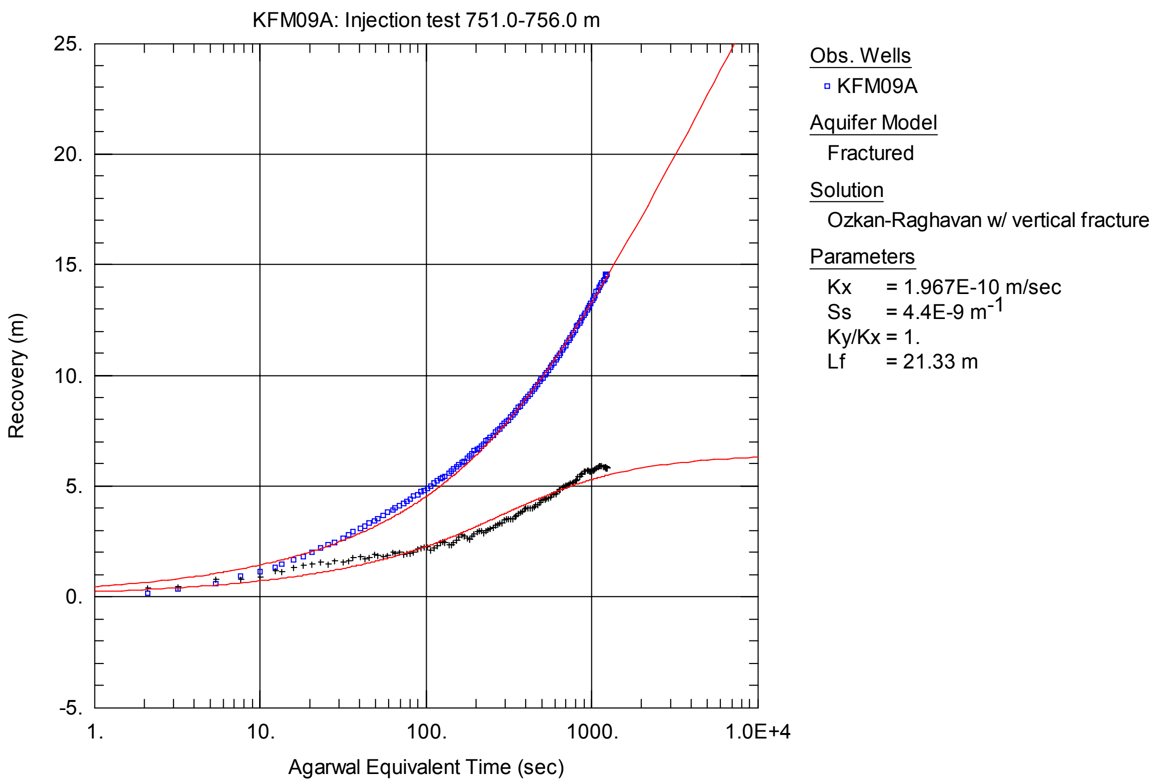


Figure A3-563. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 751.0-756.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

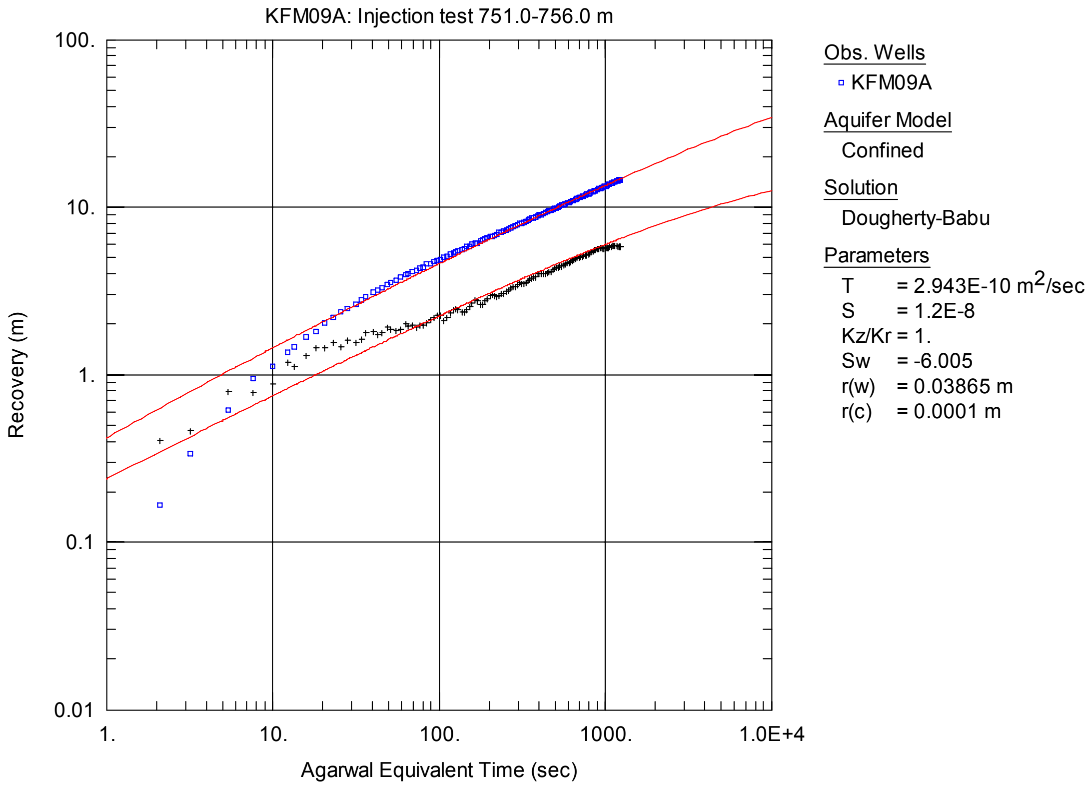


Figure A3-564. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 751.0-756.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

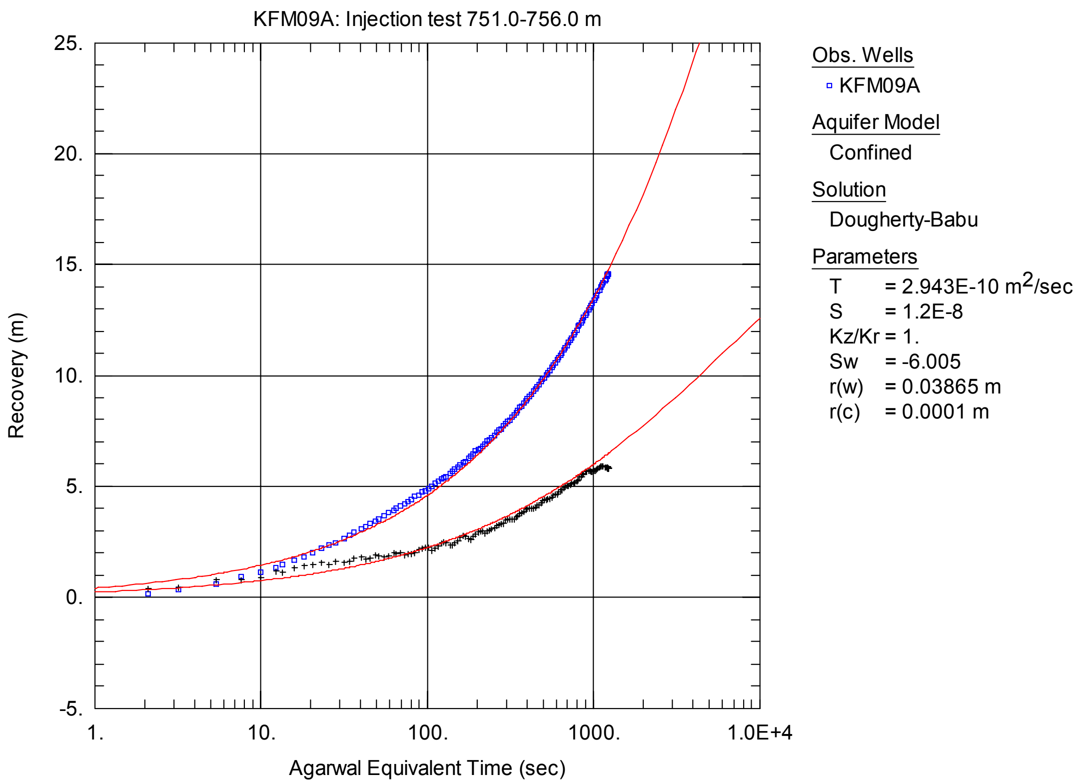


Figure A3-565. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 751.0-756.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

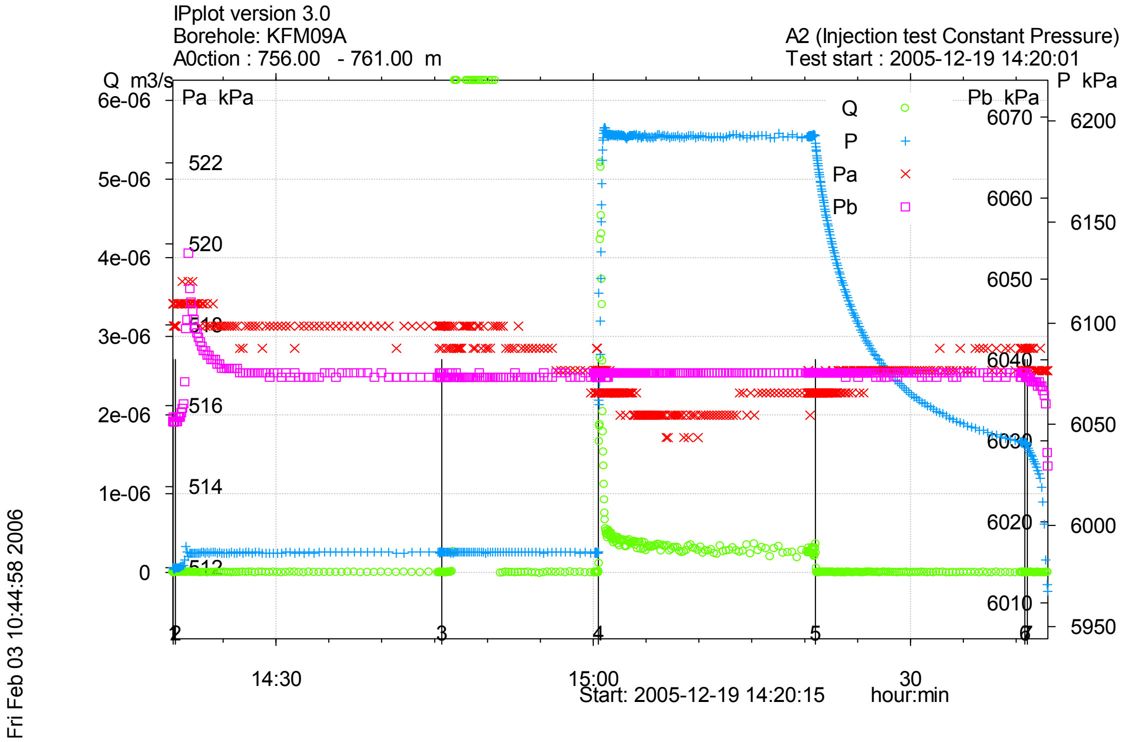


***Figure A3-566.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 756.0-761.0 m in borehole KFM09A.*

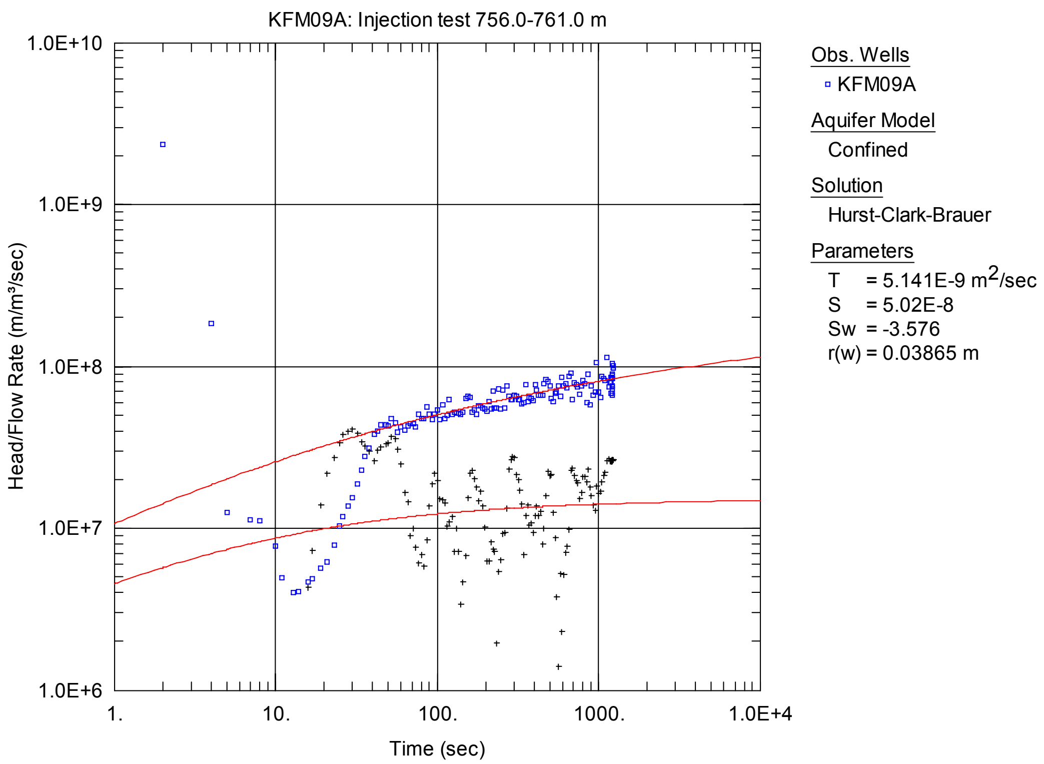


***Figure A3-567.** Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 756.0-761.0 m in KFM09A.*

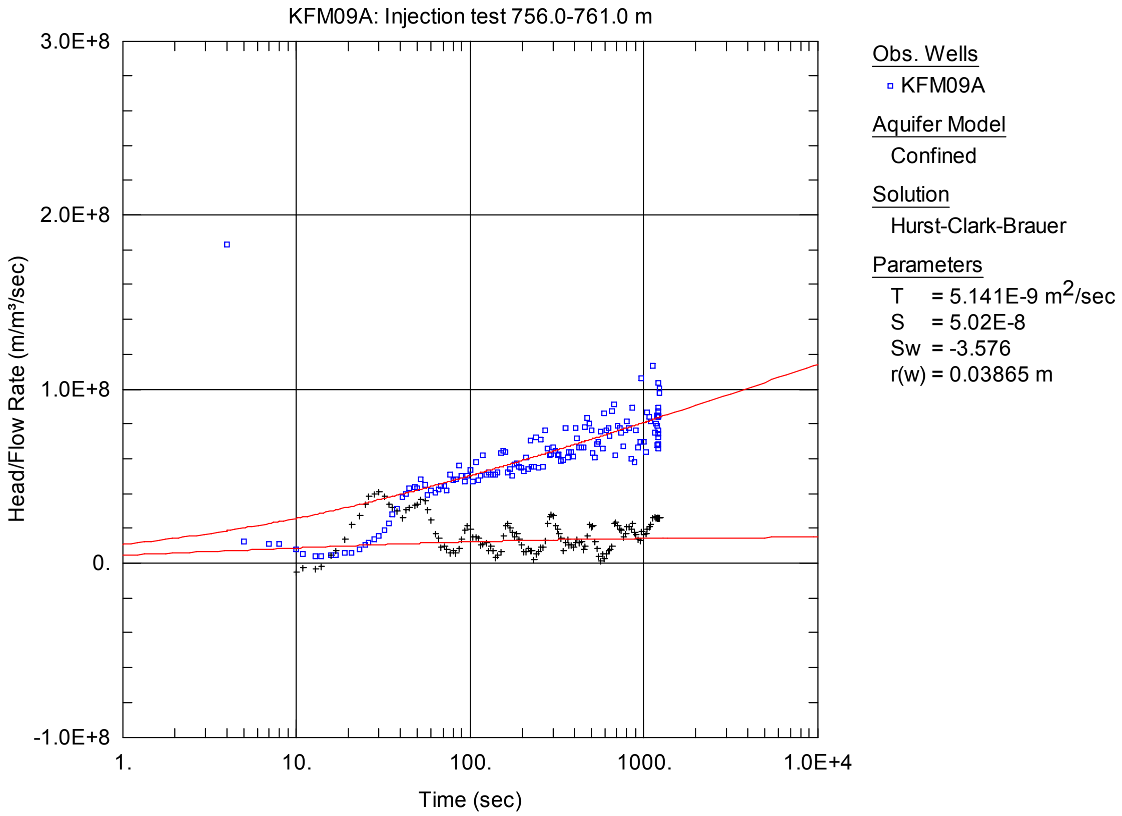


Figure A3-568. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 756.0-761.0 m in KFM09A.*

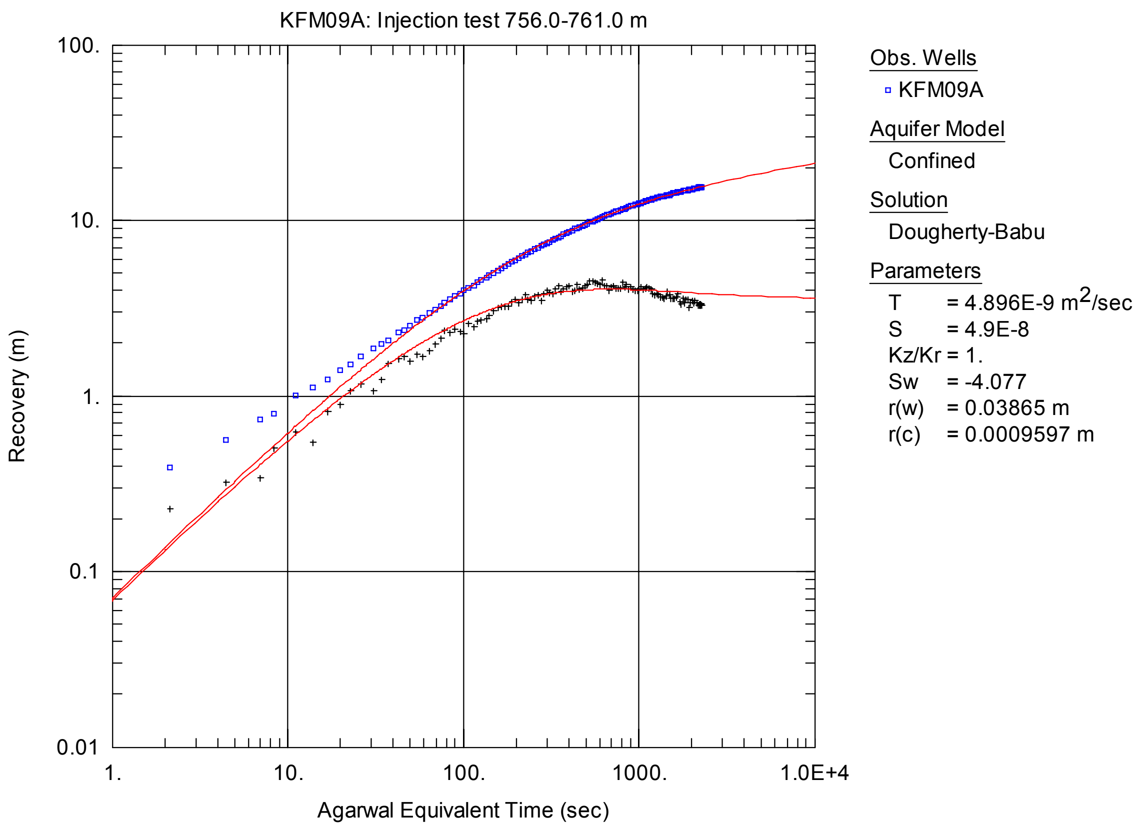


Figure A3-569. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 756.0-761.0 m in KFM09A.*

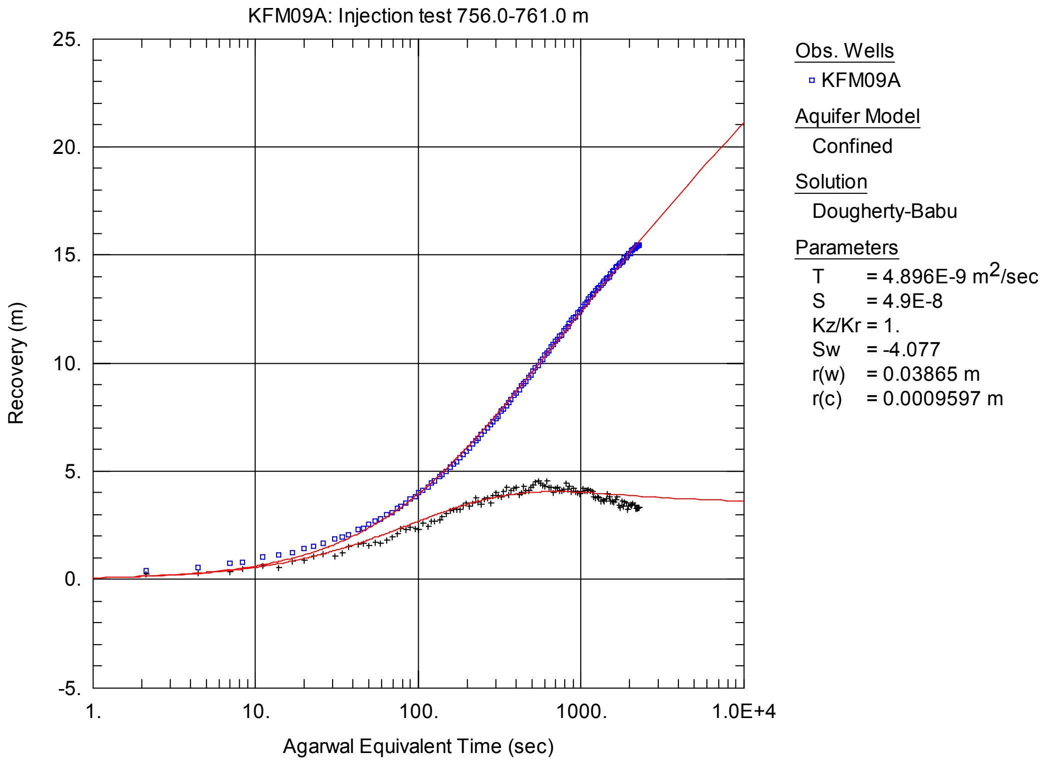


***Figure A3-570.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 756.0-761.0 m in KFM09A.*

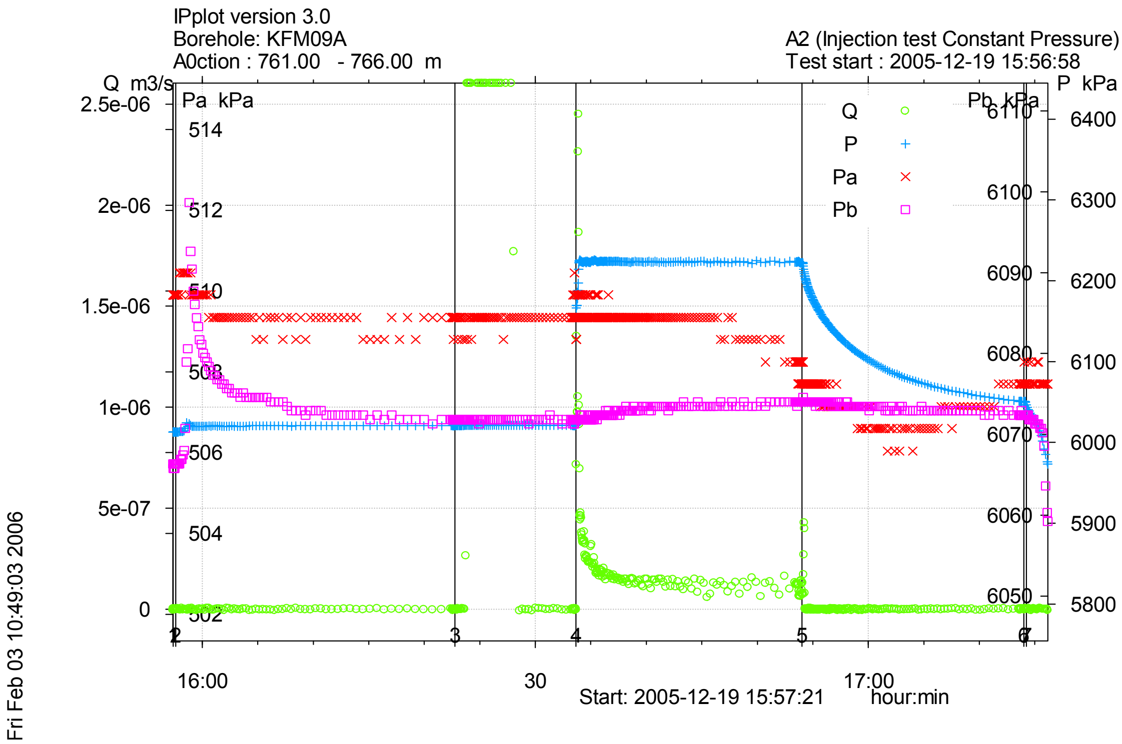


***Figure A3-571.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 761.0-766.0 m in borehole KFM09A.*

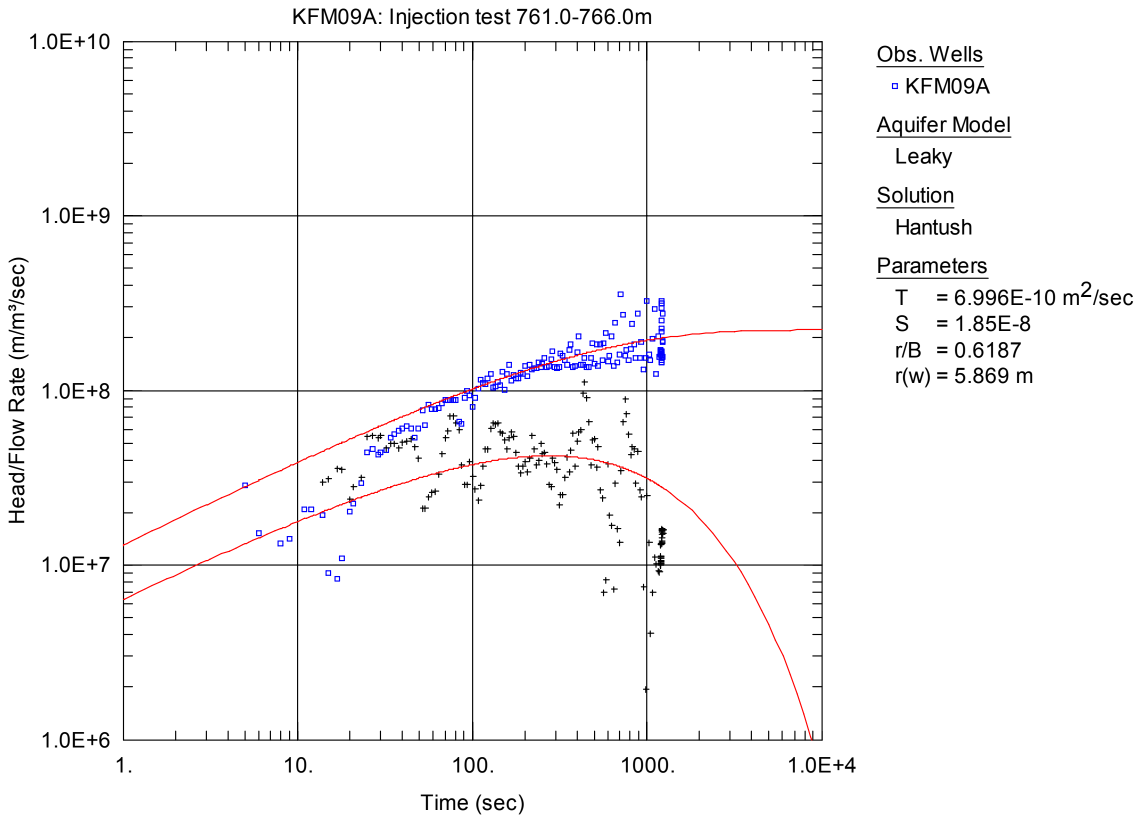


Figure A3-572. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 761.0-766.0 m in KFM09A.*

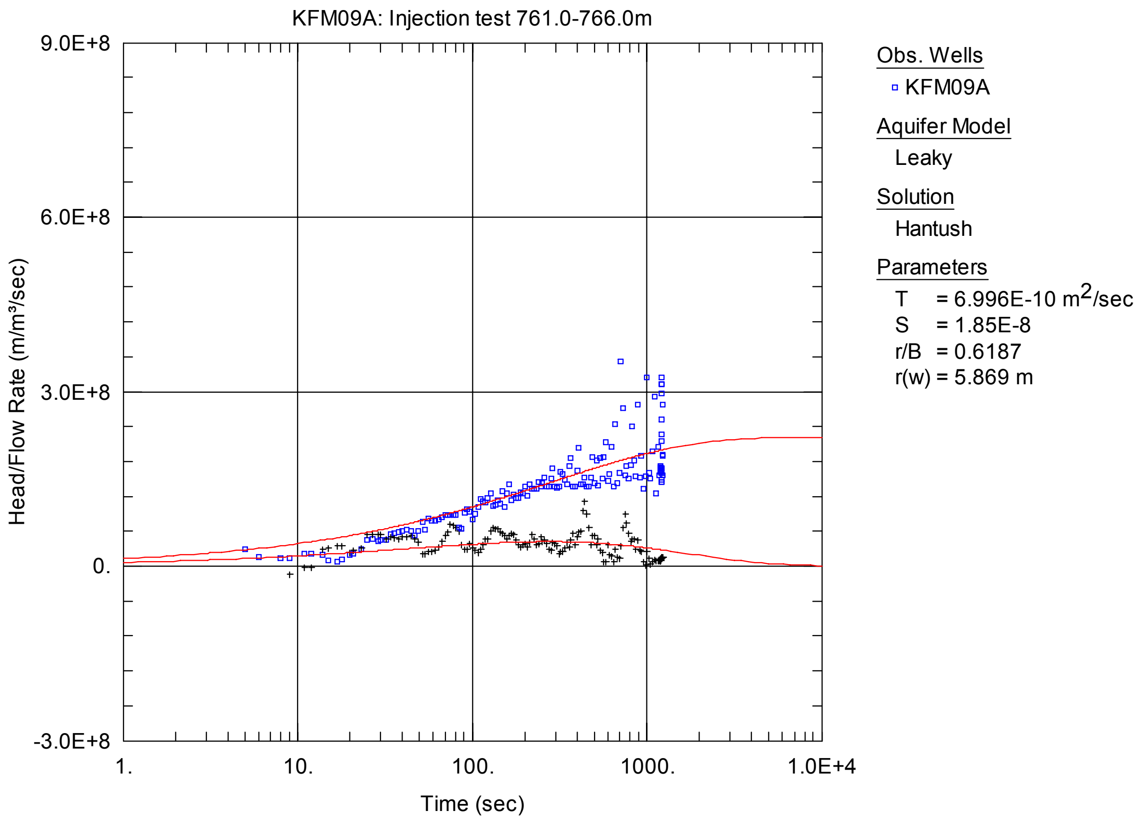


Figure A3-573. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 761.0-766.0 m in KFM09A.*

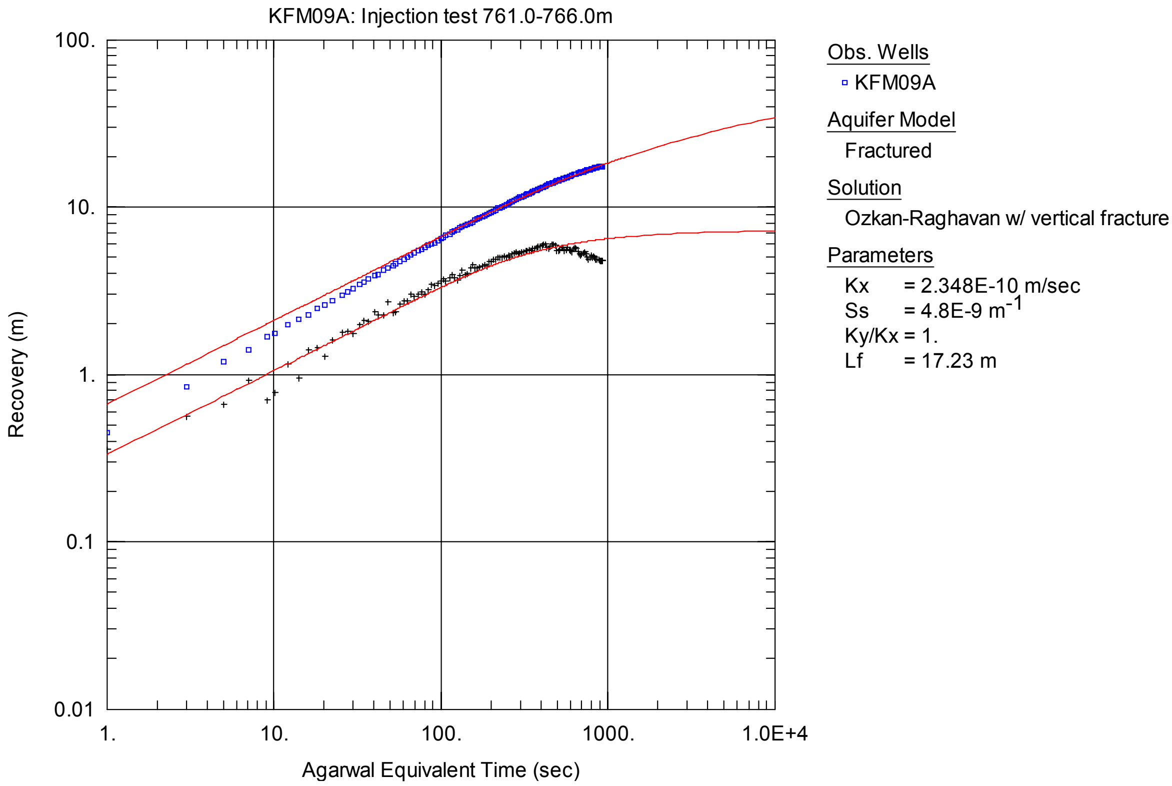


Figure A3-574. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 761.0-766.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

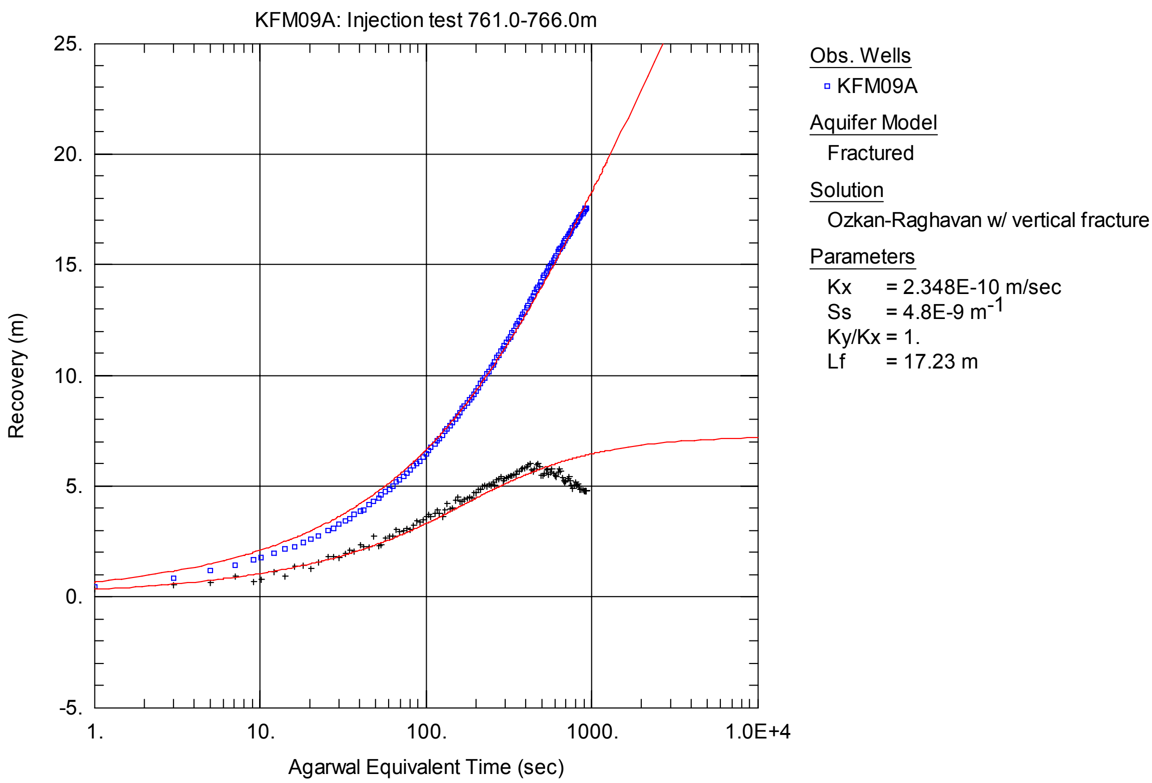


Figure A3-575. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 761.0-766.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

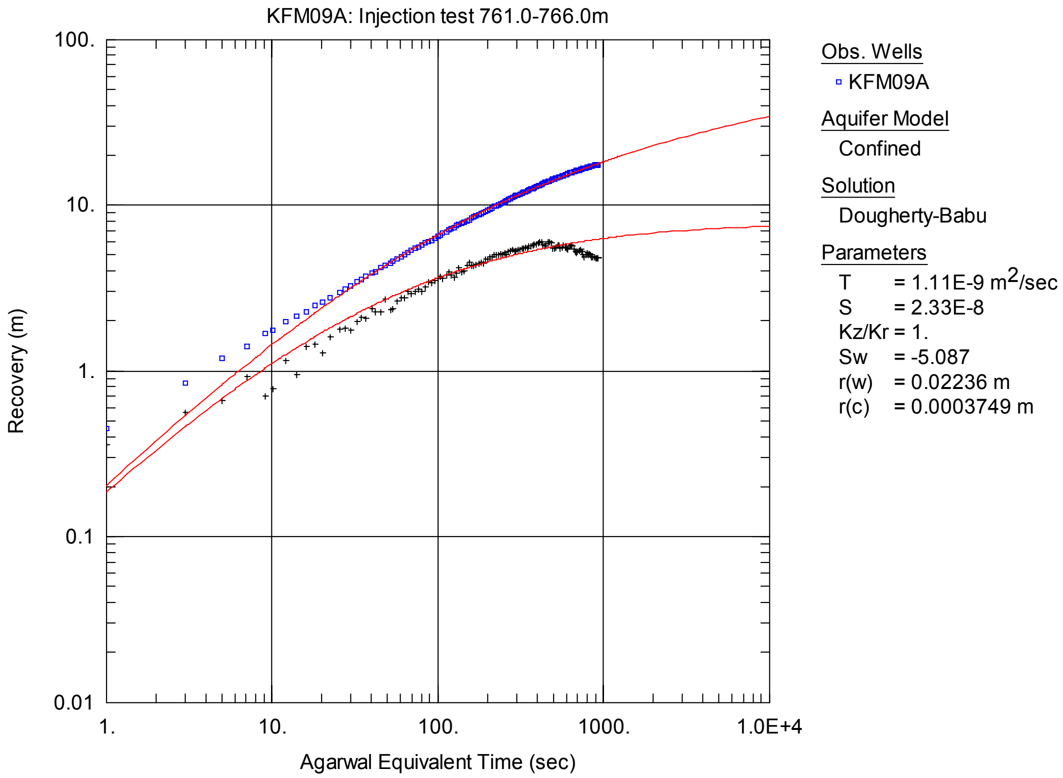


Figure A3-576. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 761.0-766.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

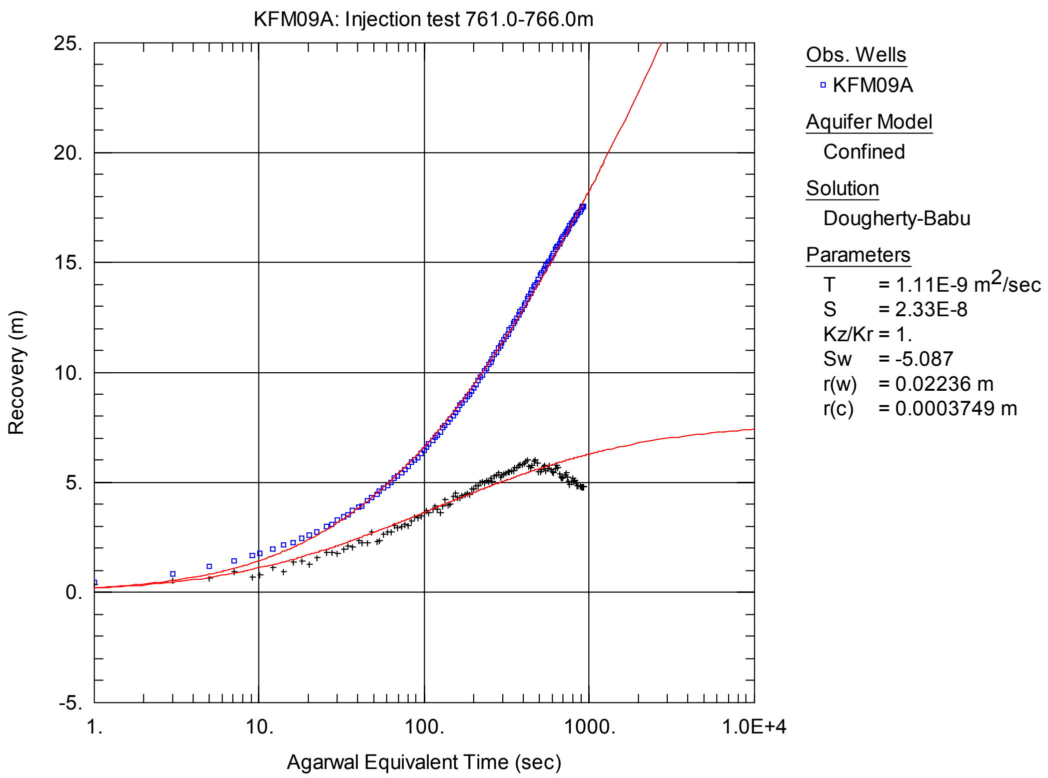


Figure A3-577. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 761.0-766.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

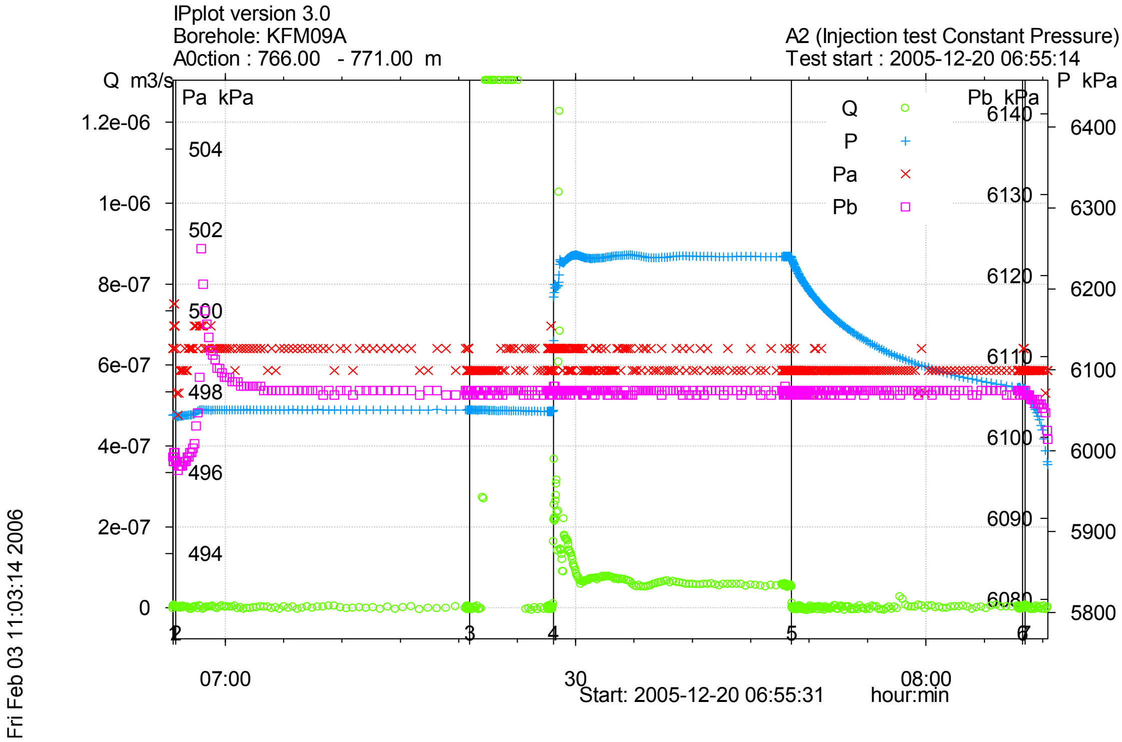


Figure A3-578. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 766.0-771.0 m in borehole KFM09A.*

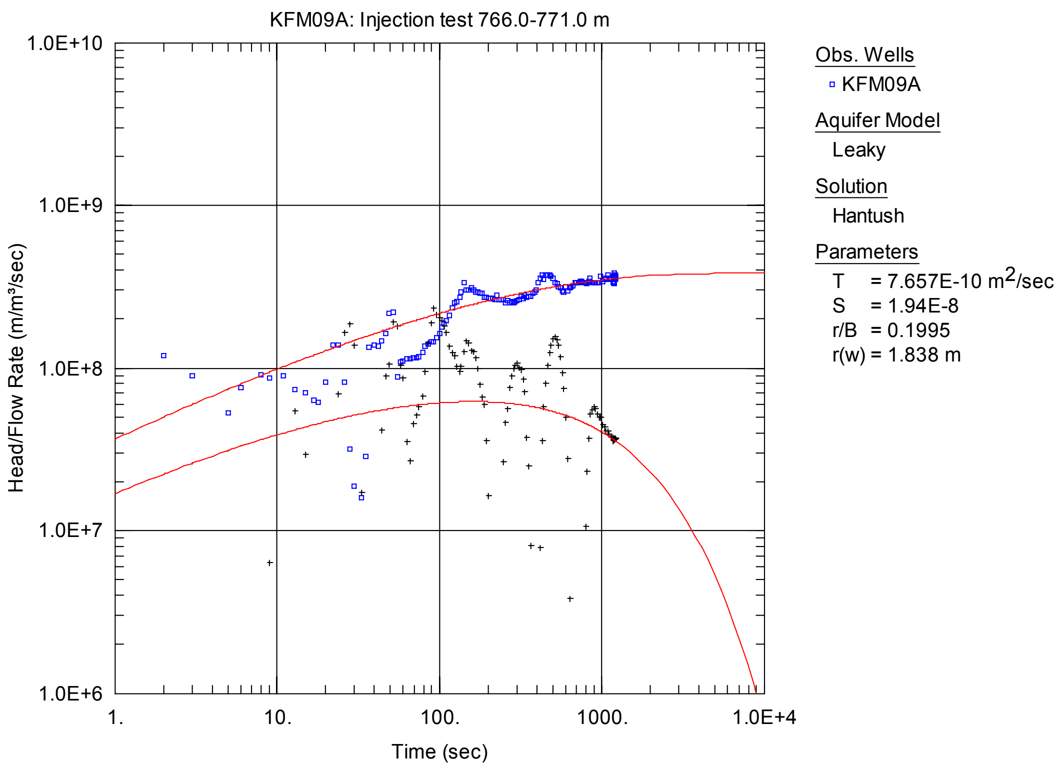


Figure A3-579. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 766.0-771.0 m in KFM09A.*

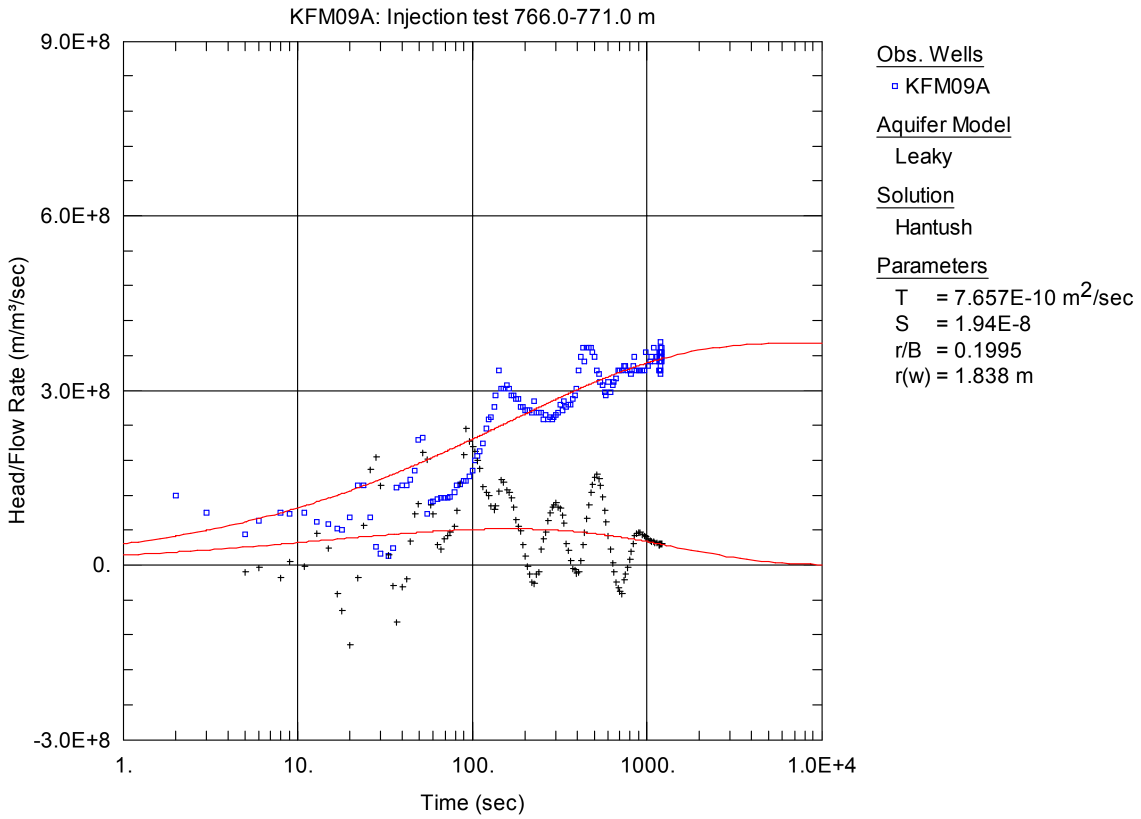


__Figure A3-580.__ Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 766.0-771.0 m in KFM09A.

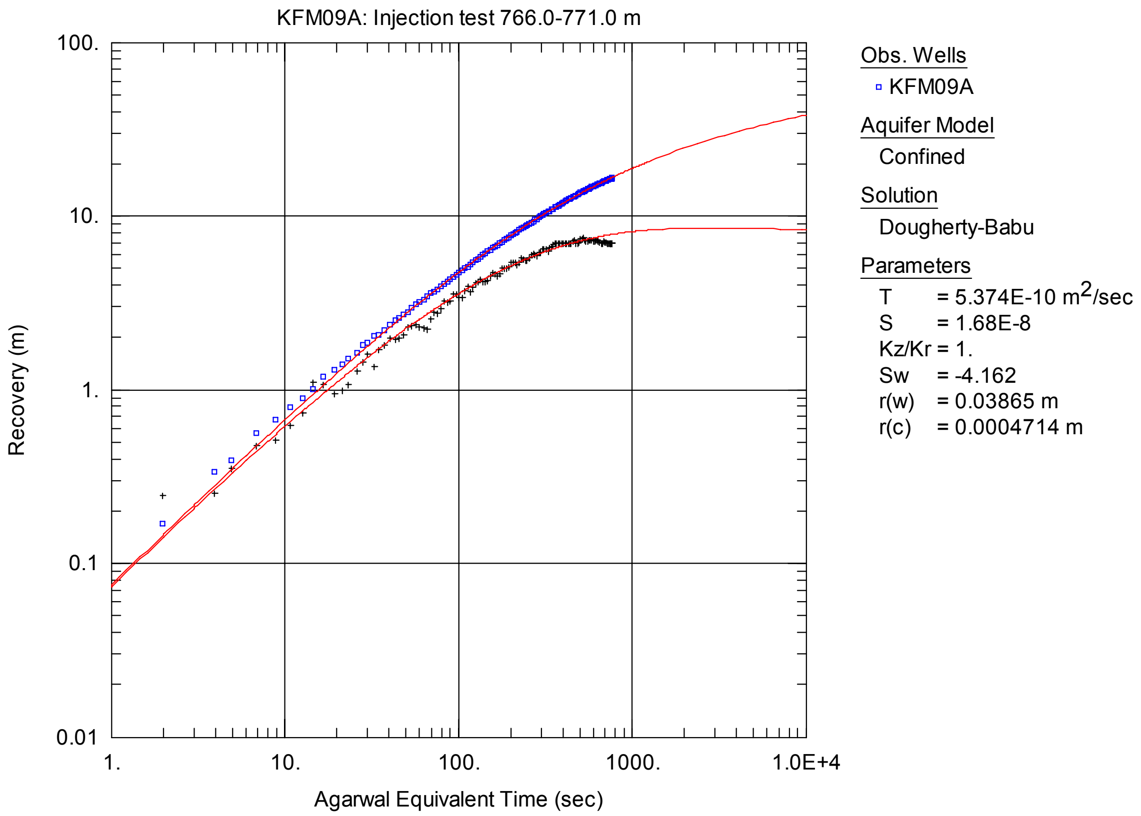


__Figure A3-581.__ Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 766.0-771.0 m in KFM09A.

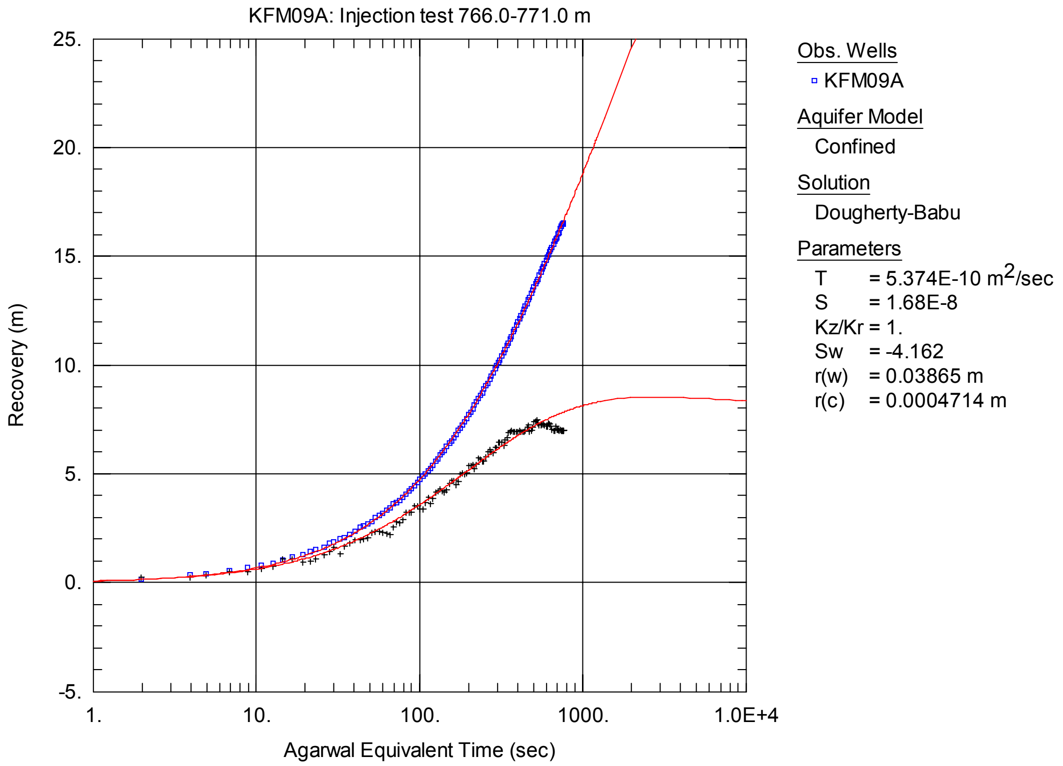


__Figure A3-582.__ Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 766.0-771.0 m in KFM09A.

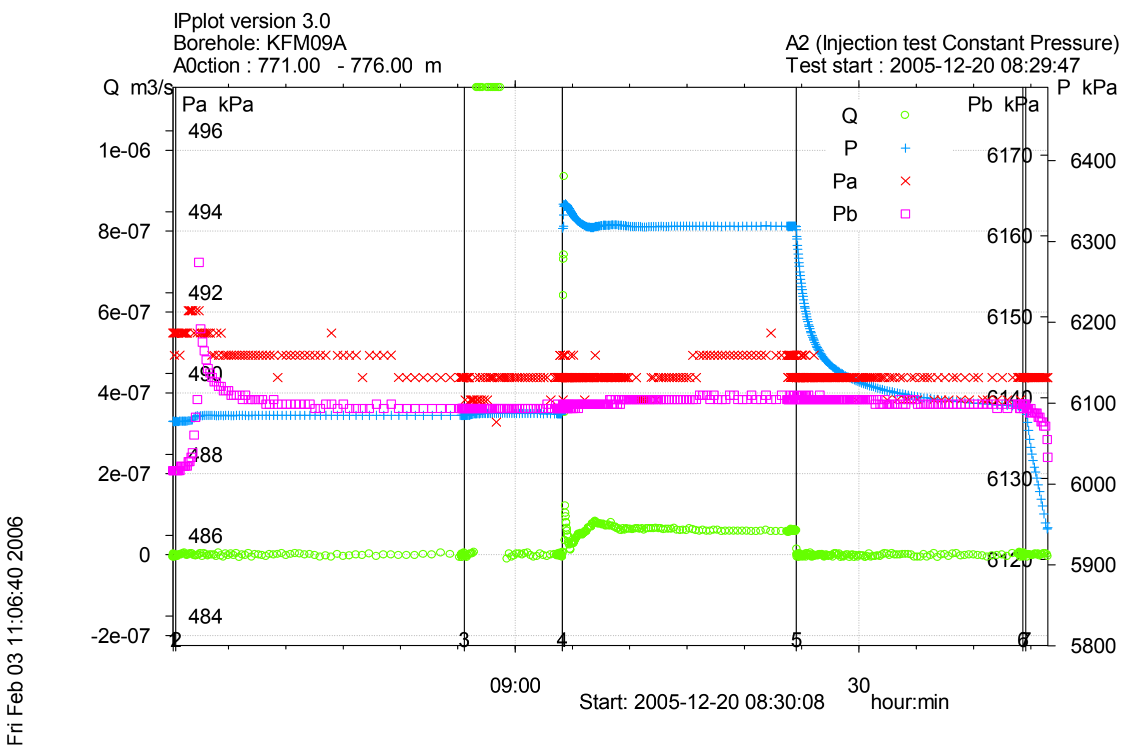


__Figure A3-583.__ Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 771.0-776.0 m in borehole KFM09A.

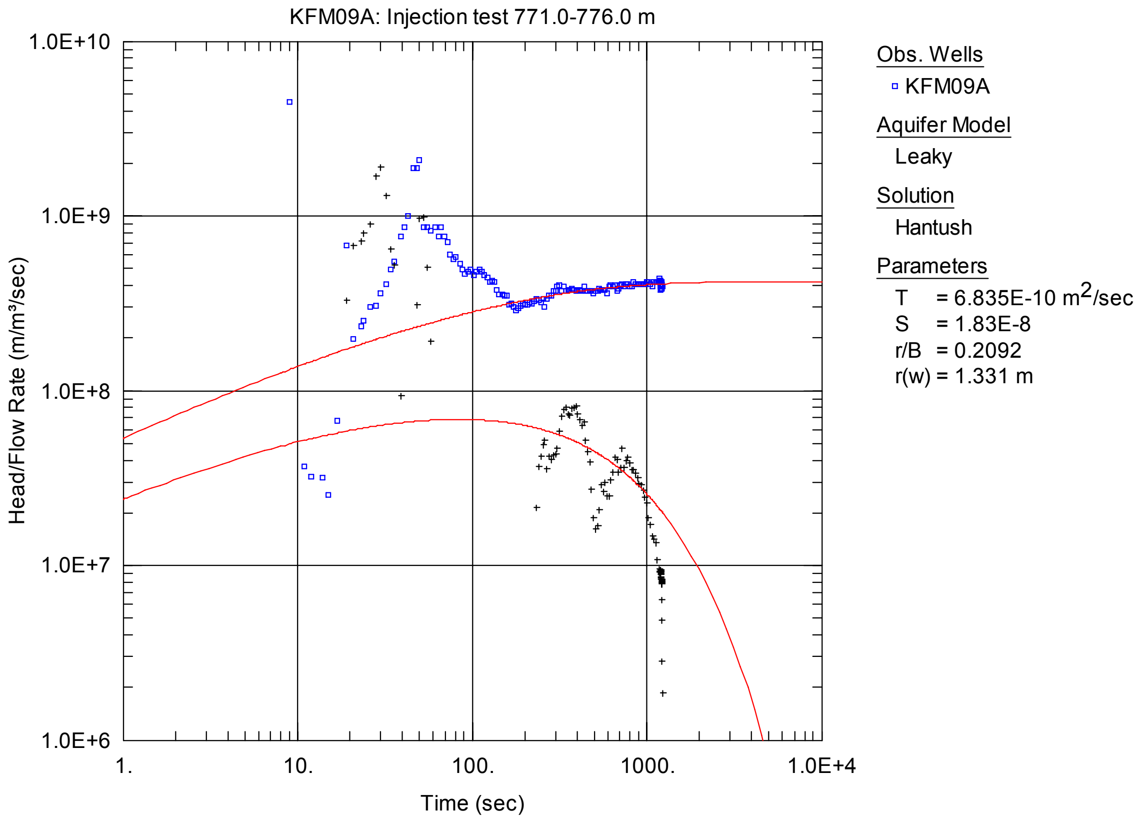


***Figure A3-584.** Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 771.0-776.0 m in KFM09A.*

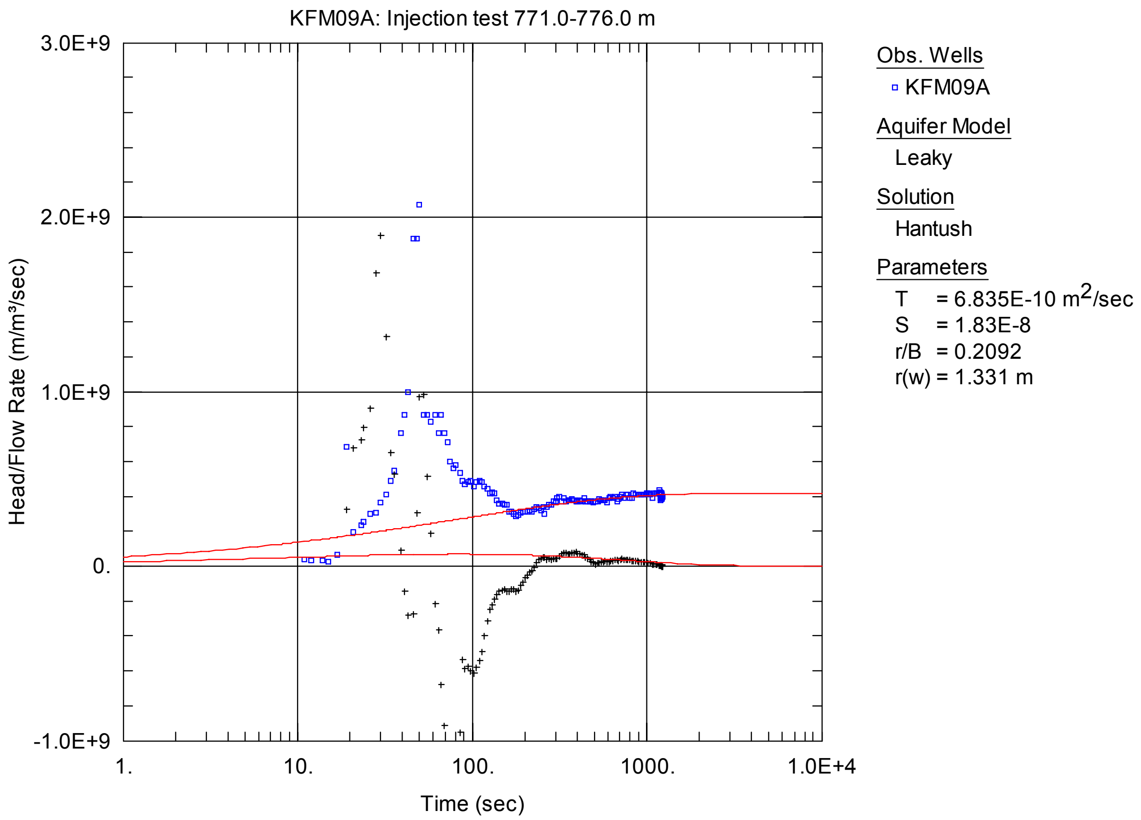


***Figure A3-585.** Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 771.0-776.0 m in KFM09A.*

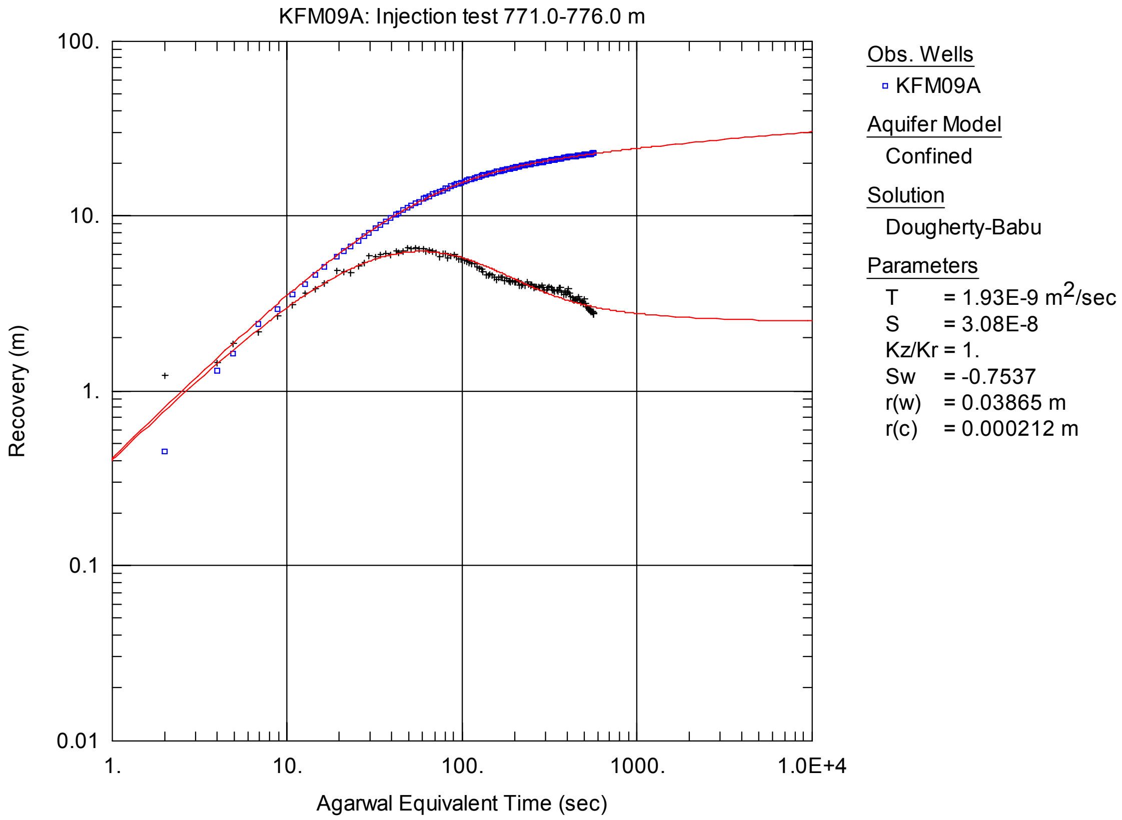


Figure A3-586. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 771.0-776.0 m in KFM09A.*

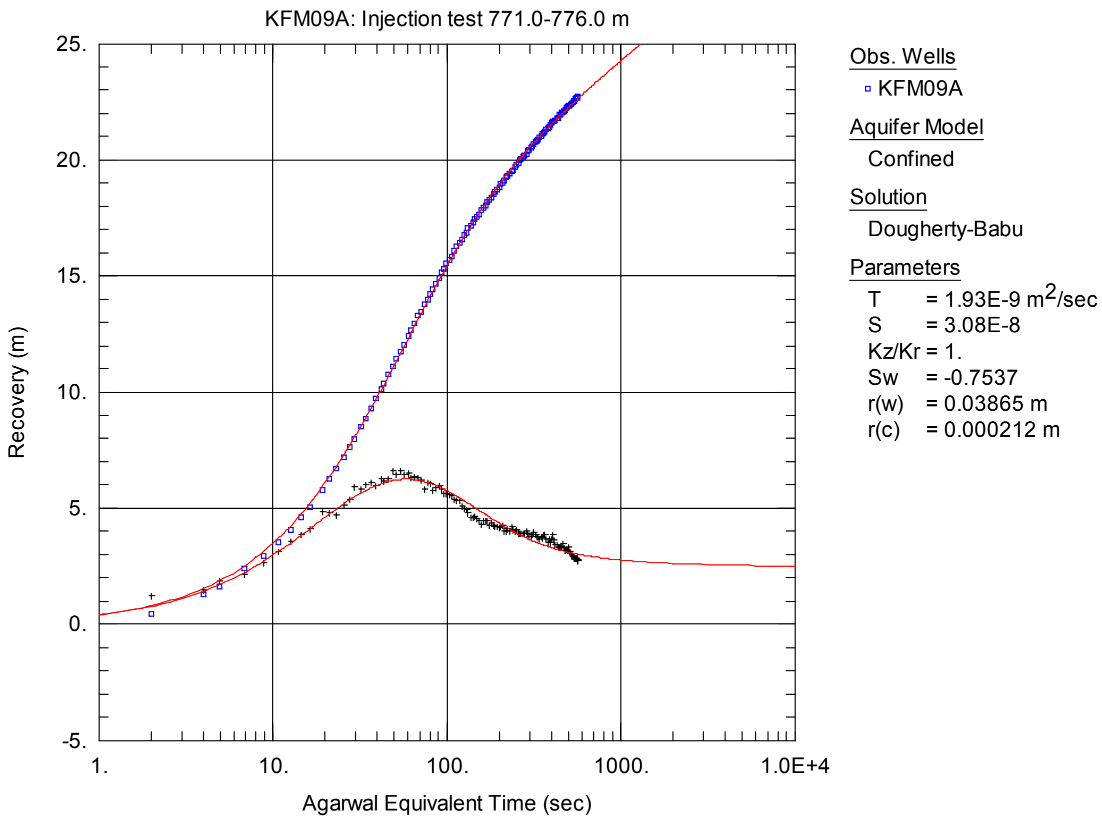


Figure A3-587. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 771.0-776.0 m in KFM09A.*

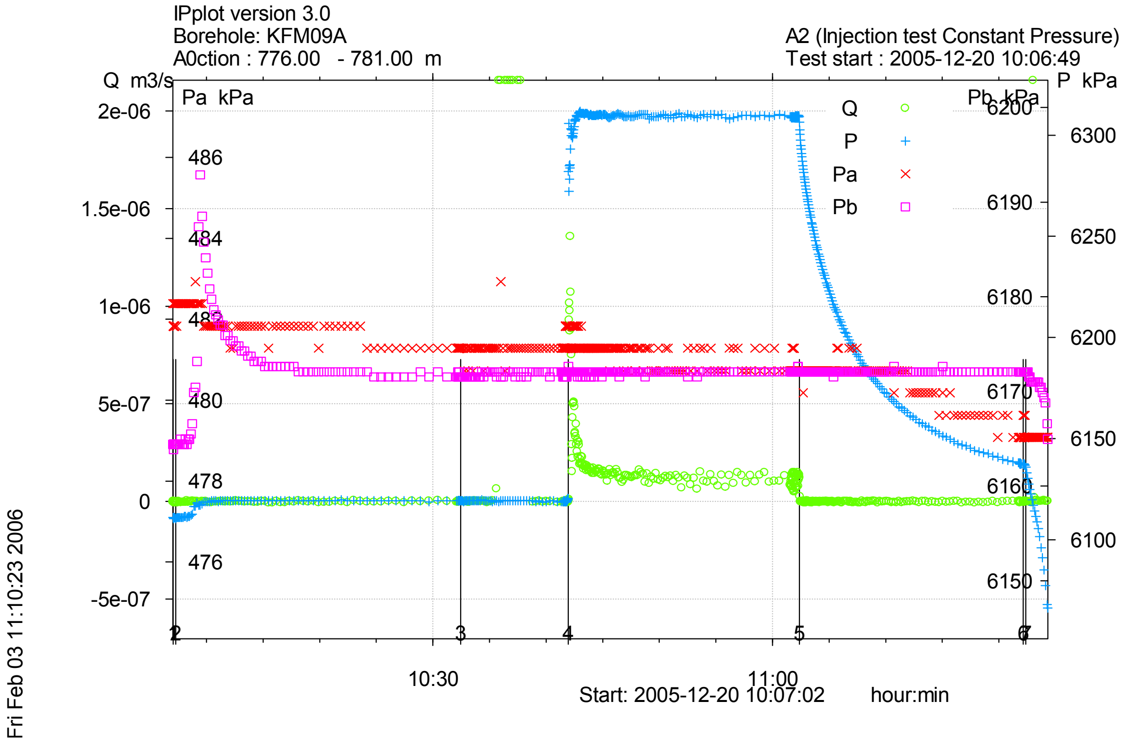


Figure A3-588. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 776.0-781.0 m in borehole KFM09A.*

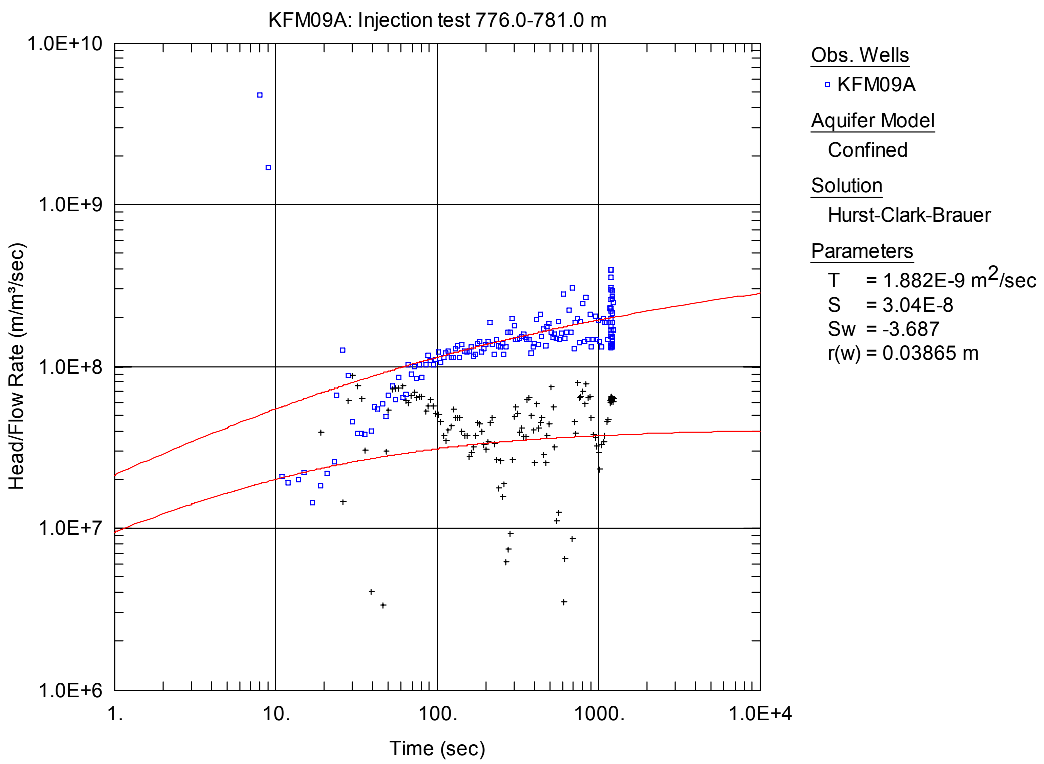


Figure A3-589. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 776.0-781.0 m in KFM09A.*

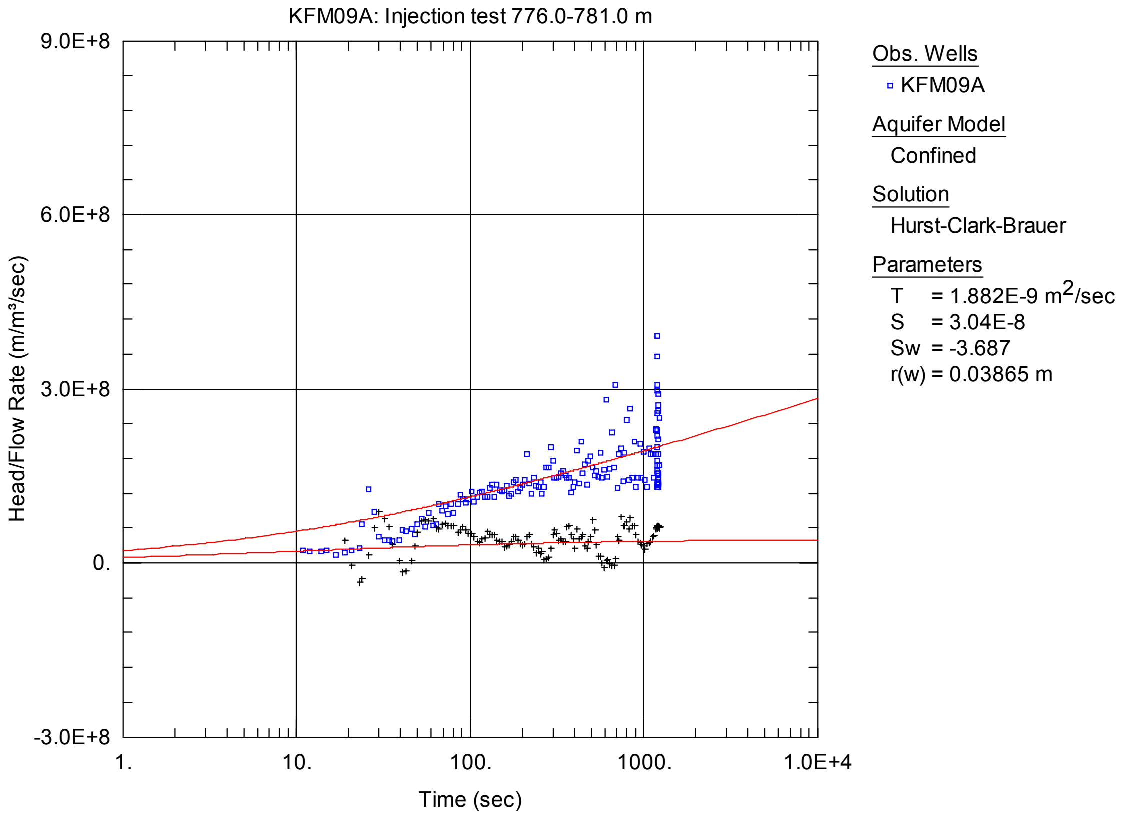


Figure A3-590. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 776.0-781.0 m in KFM09A.*

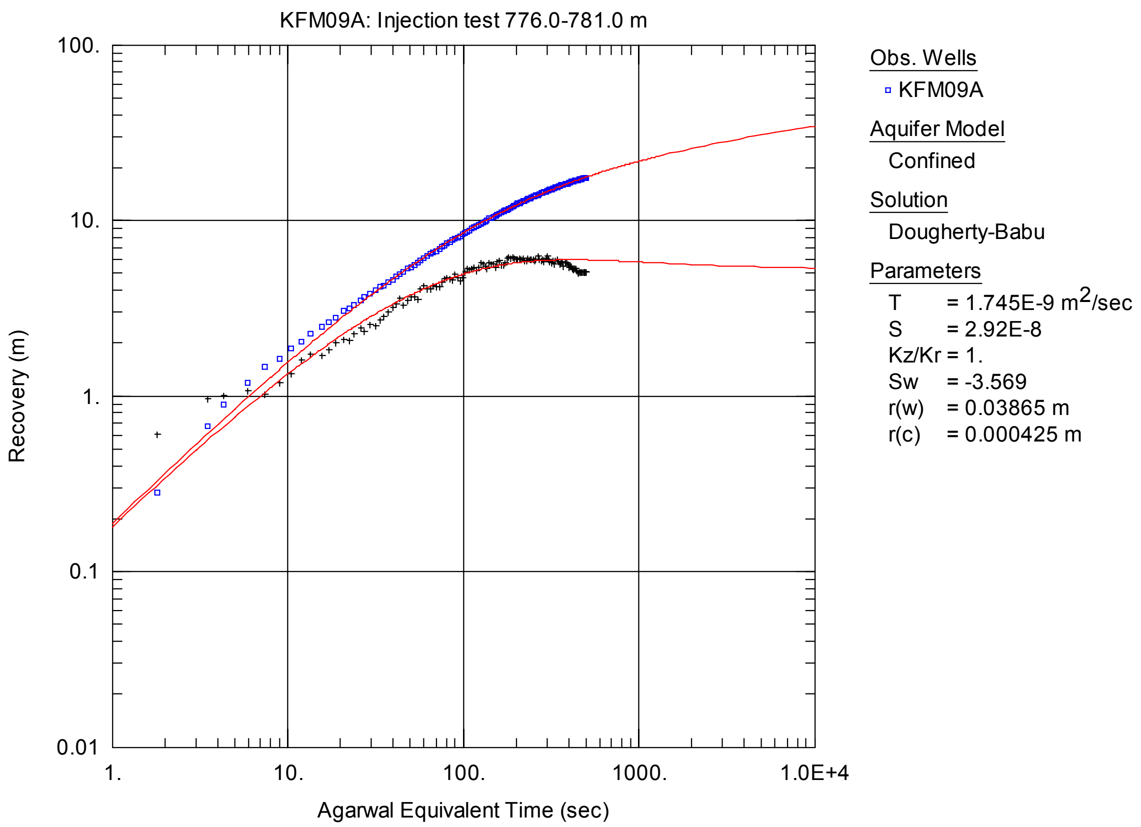


Figure A3-591. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 776.0-781.0 m in KFM09A.*

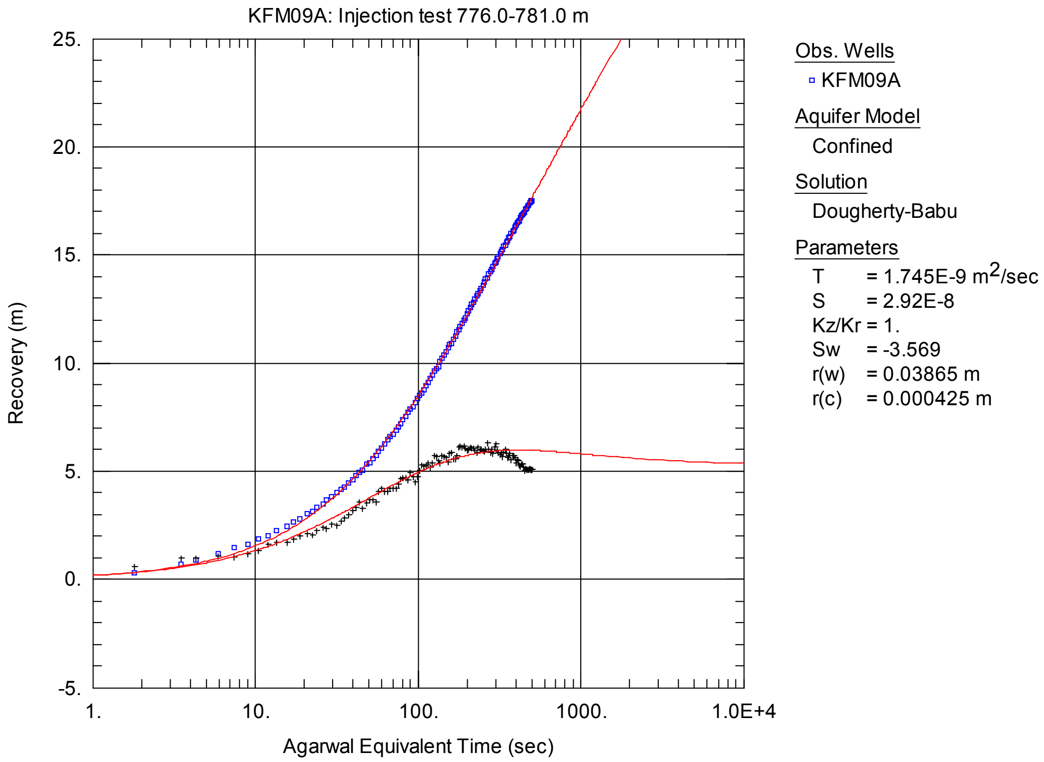


***Figure A3-592.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 776.0-781.0 m in KFM09A.*

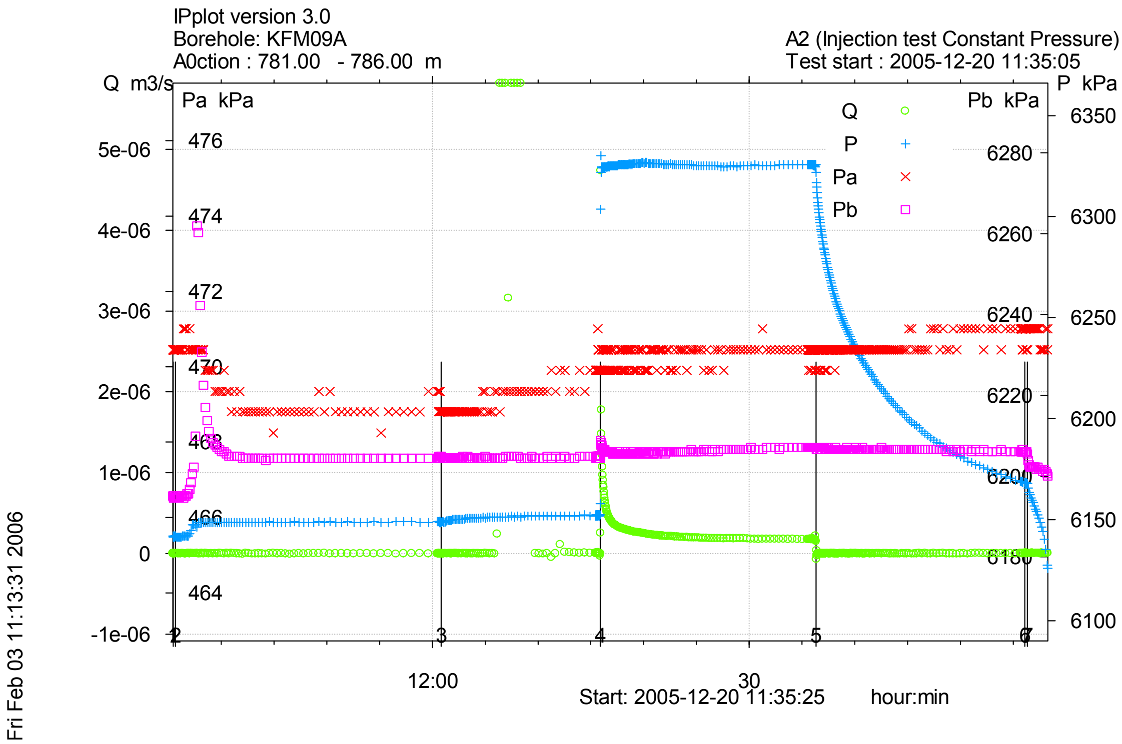


***Figure A3-593.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 781.0-786.0 m in borehole KFM09A.*

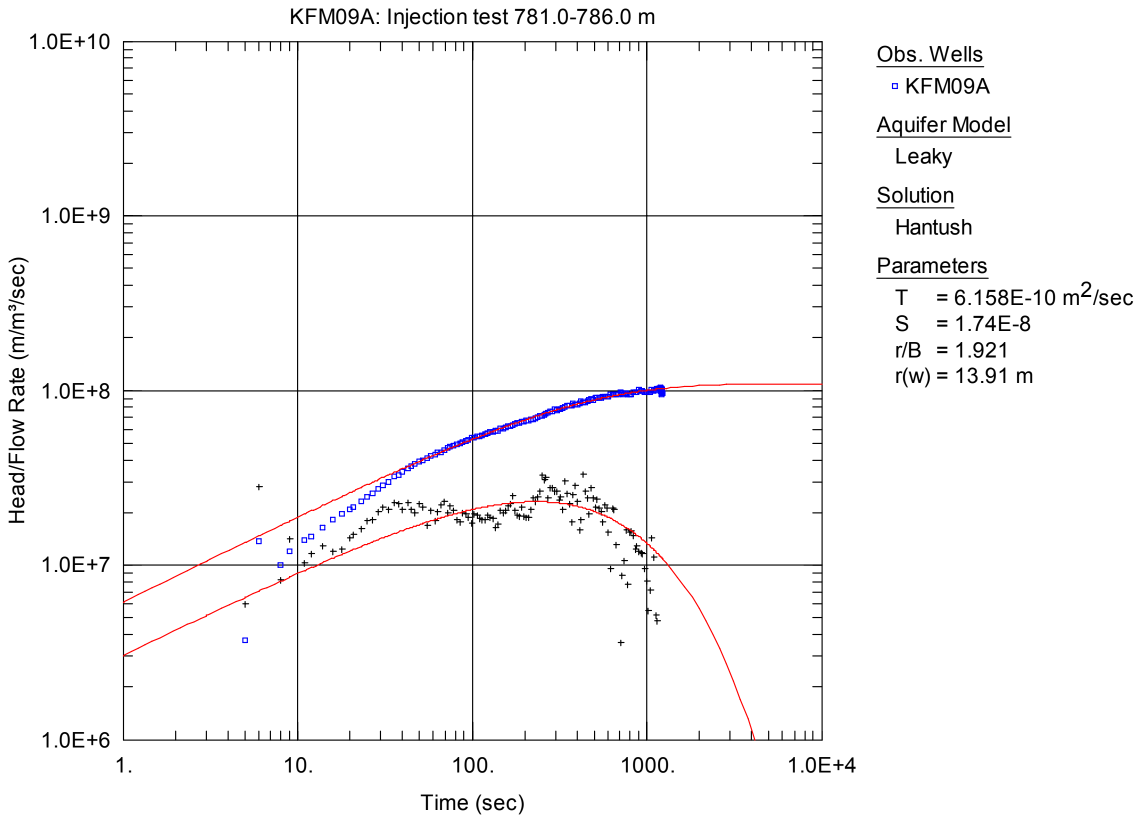


Figure A3-594. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 781.0-786.0 m in KFM09A.

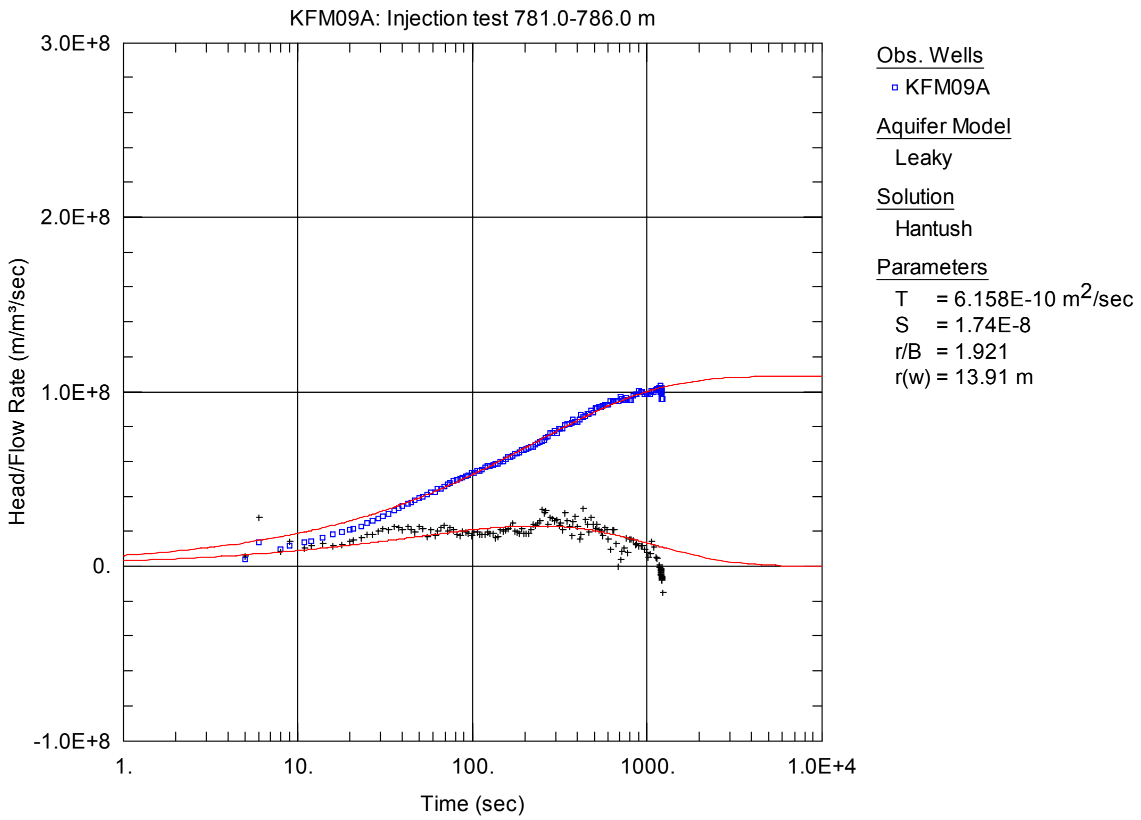


Figure A3-595. Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 781.0-786.0 m in KFM09A.

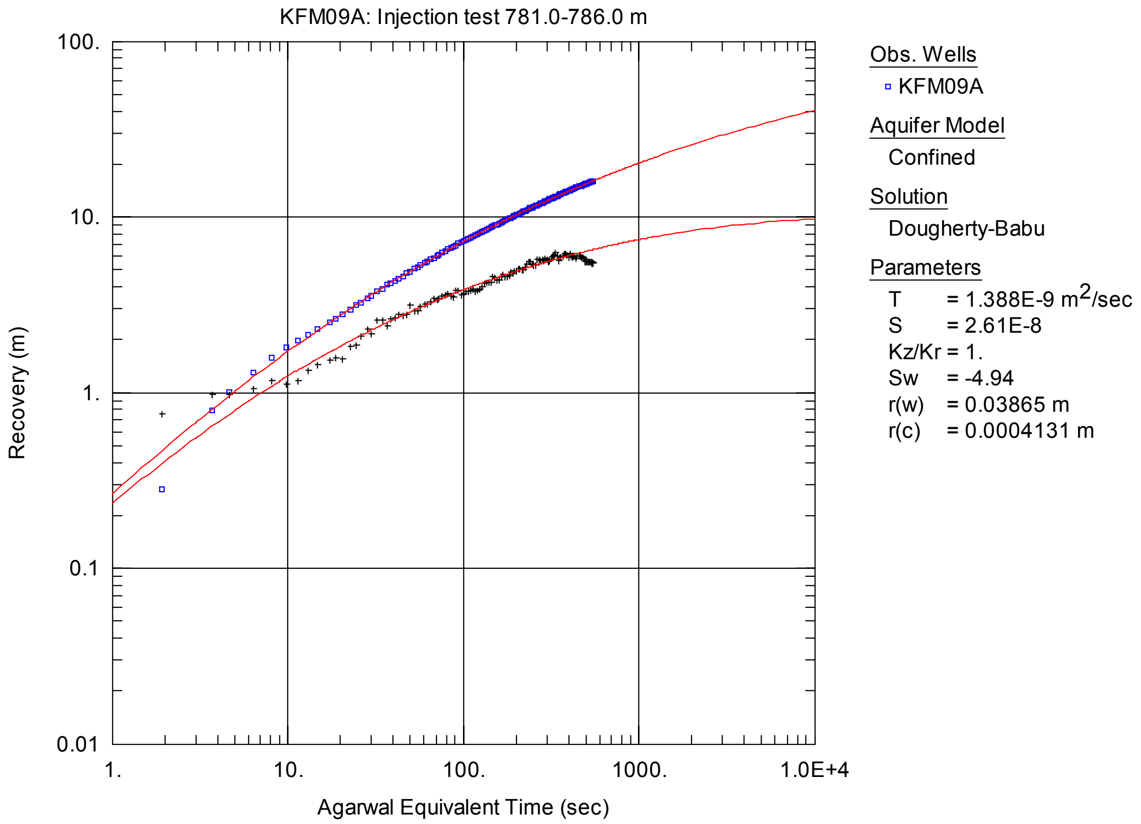


Figure A3-596. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 781.0-786.0 m in KFM09A.*

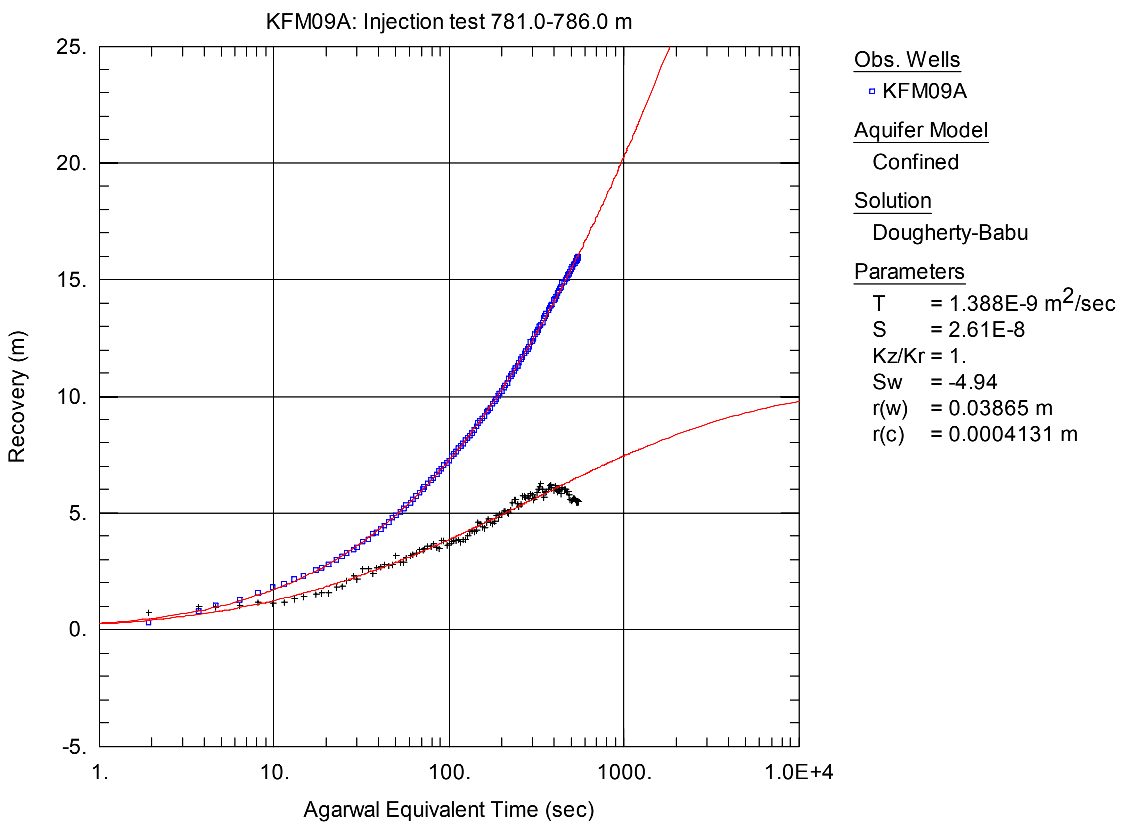


Figure A3-597. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 781.0-786.0 m in KFM09A.*

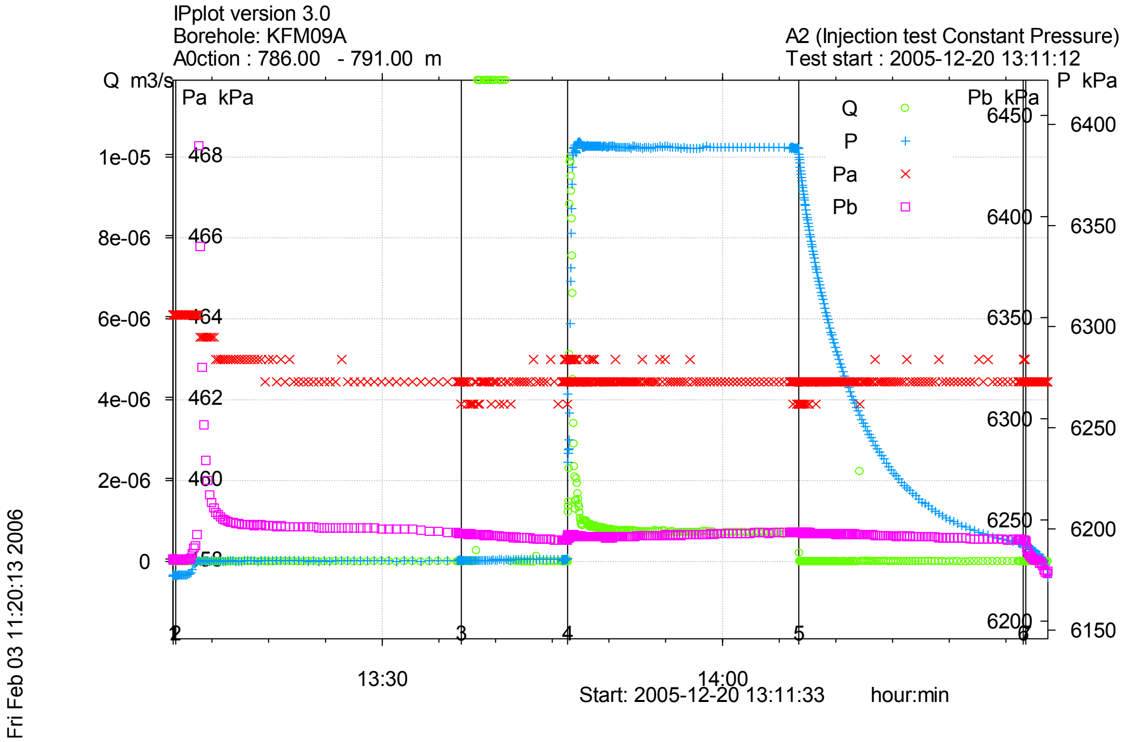


***Figure A3-598.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 786.0-791.0 m in borehole KFM09A.*

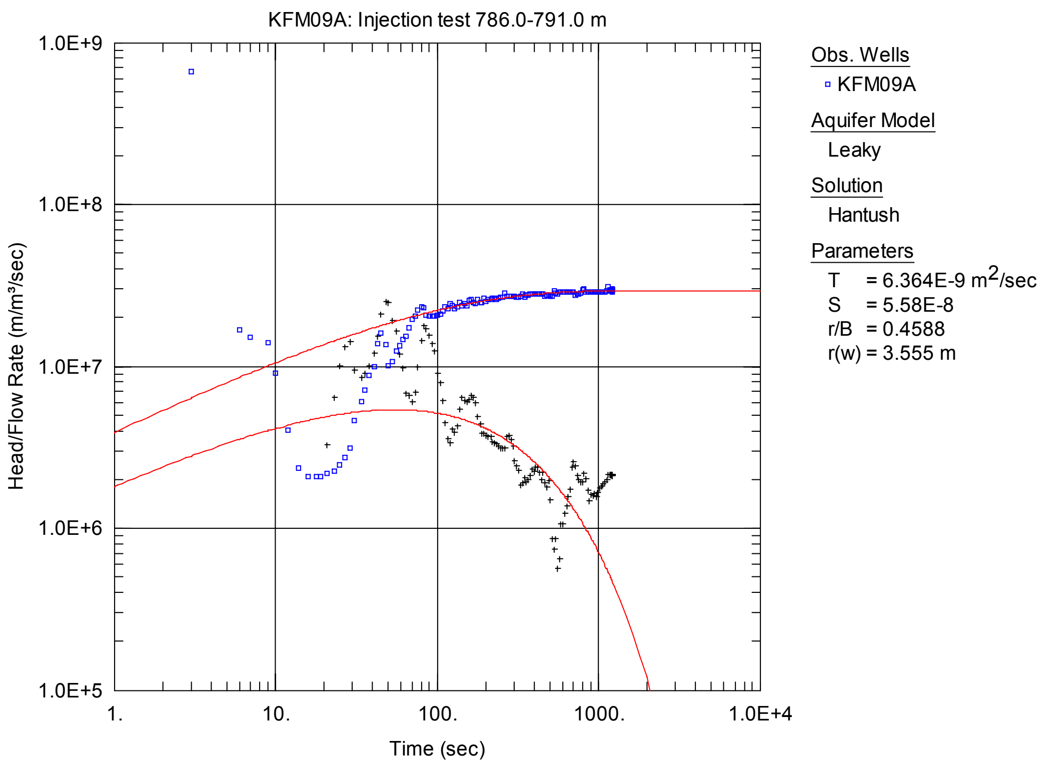


***Figure A3-599.** Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 786.0-791.0 m in KFM09A.*

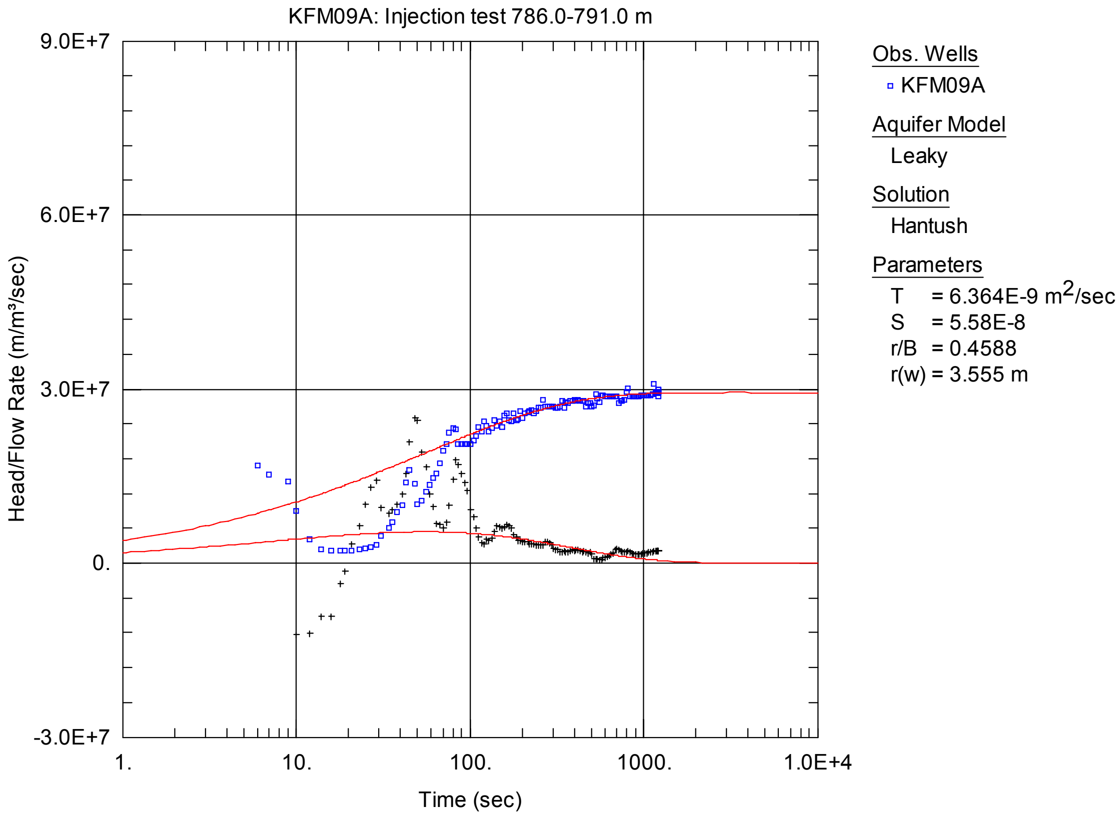


Figure A3-600. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 786.0-791.0 m in KFM09A.*

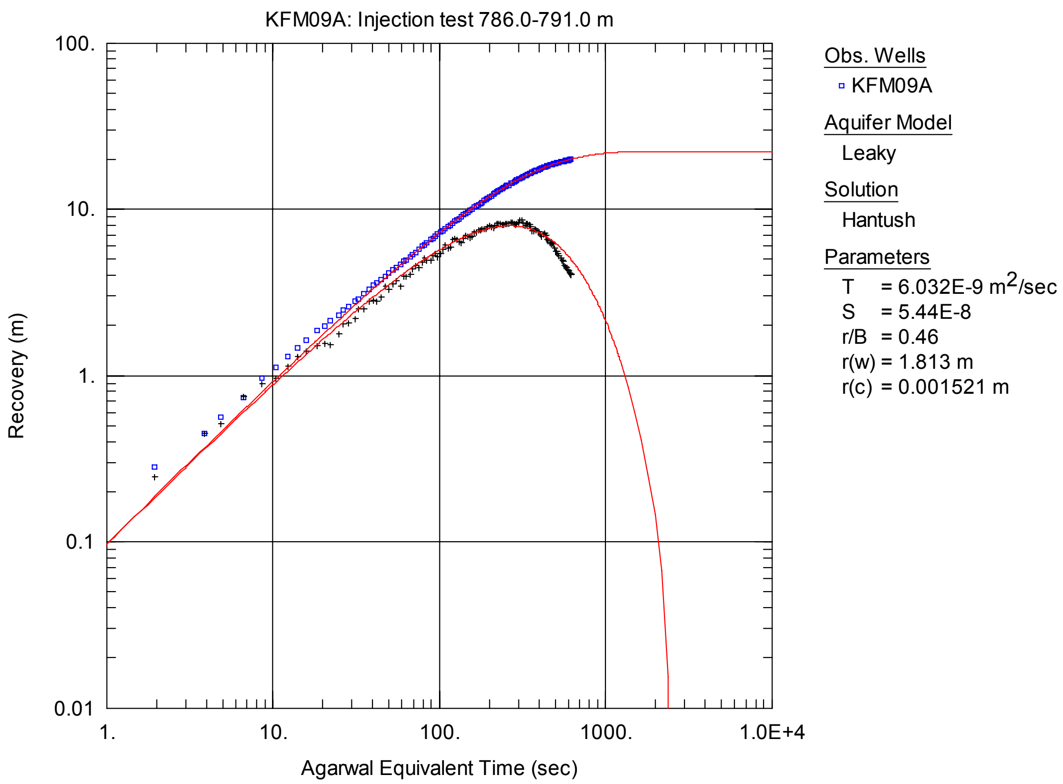


Figure A3-601. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 786.0-791.0 m in KFM09A. This evaluation is made with the Hantush model for a pseudo-spherical response.*

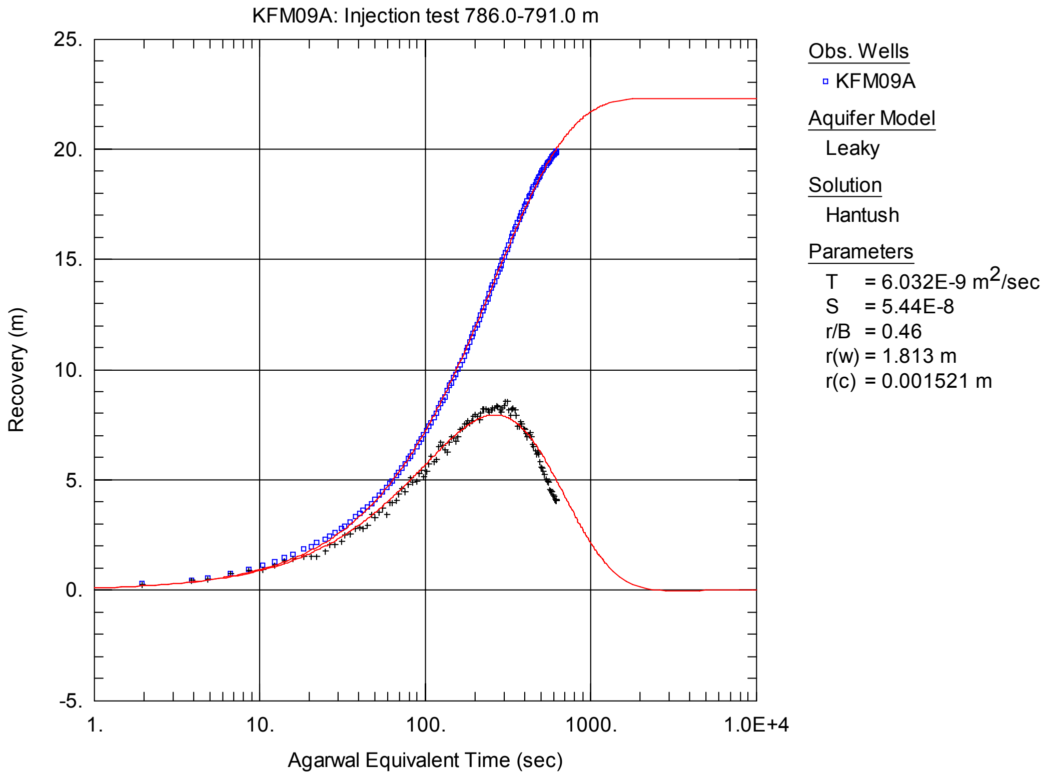


Figure A3-602. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 786.0-791.0 m in KFM09A. This evaluation is made with the Hantush model for a pseudo-spherical response.*

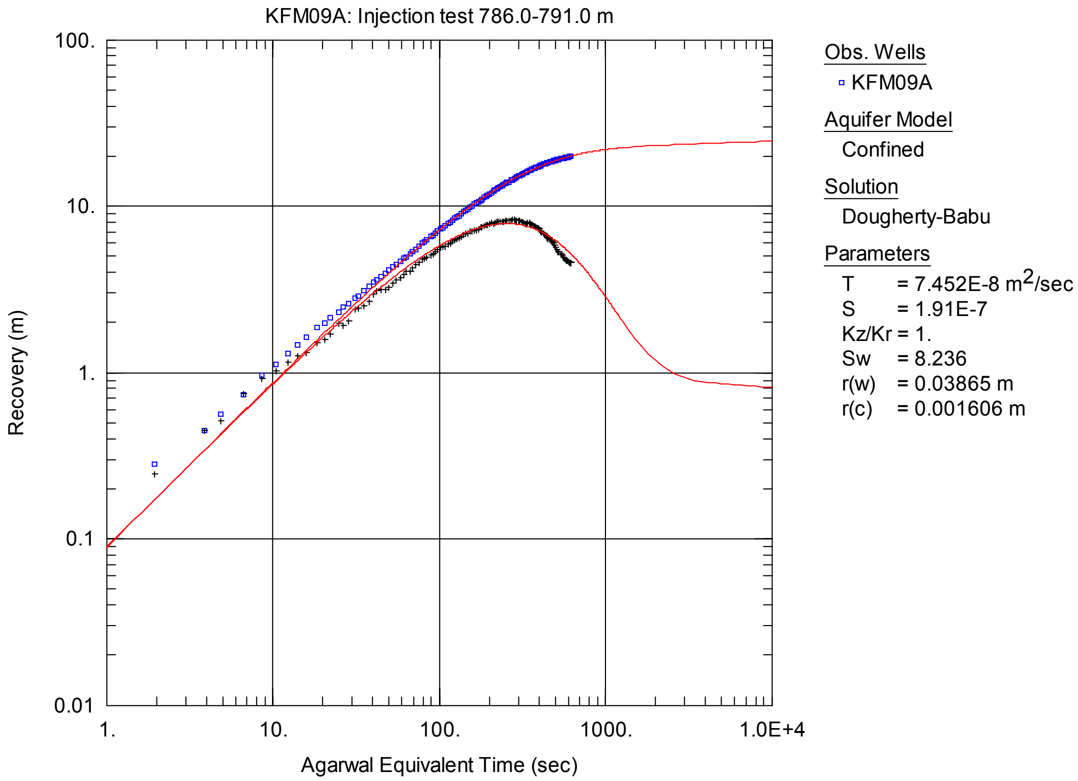


Figure A3-603. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 786.0-791.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

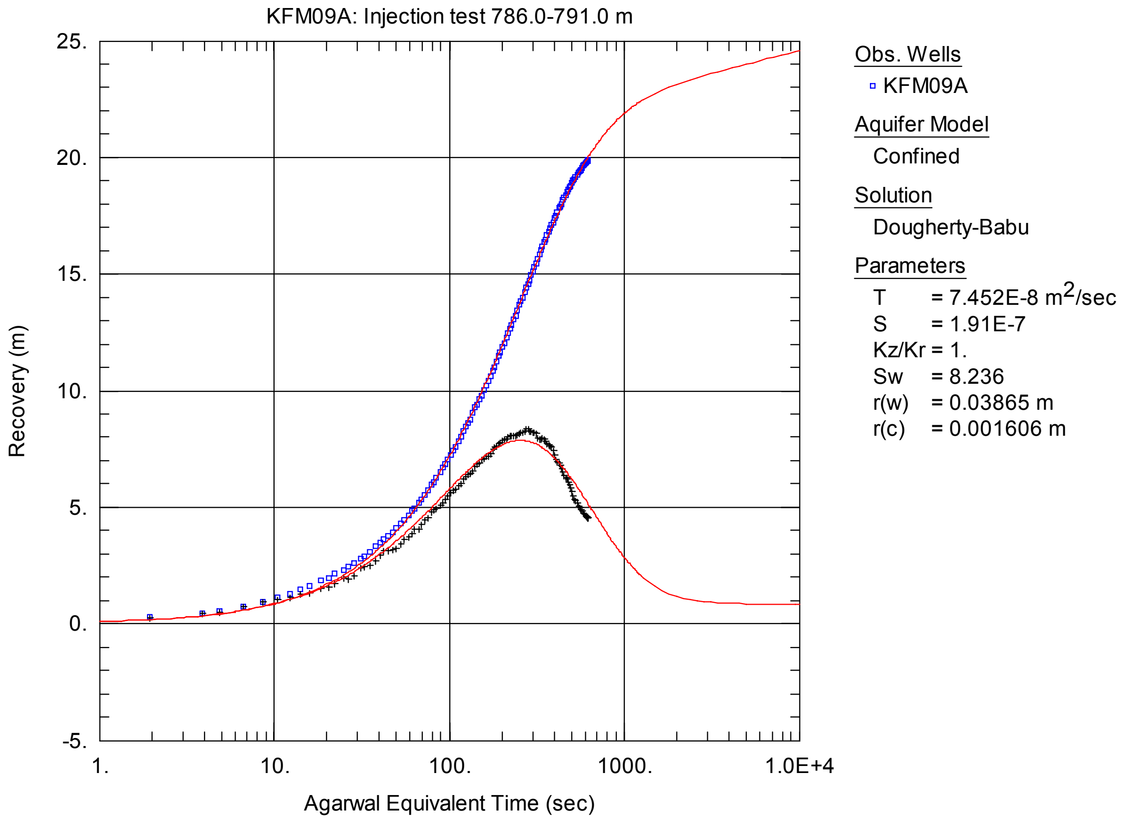
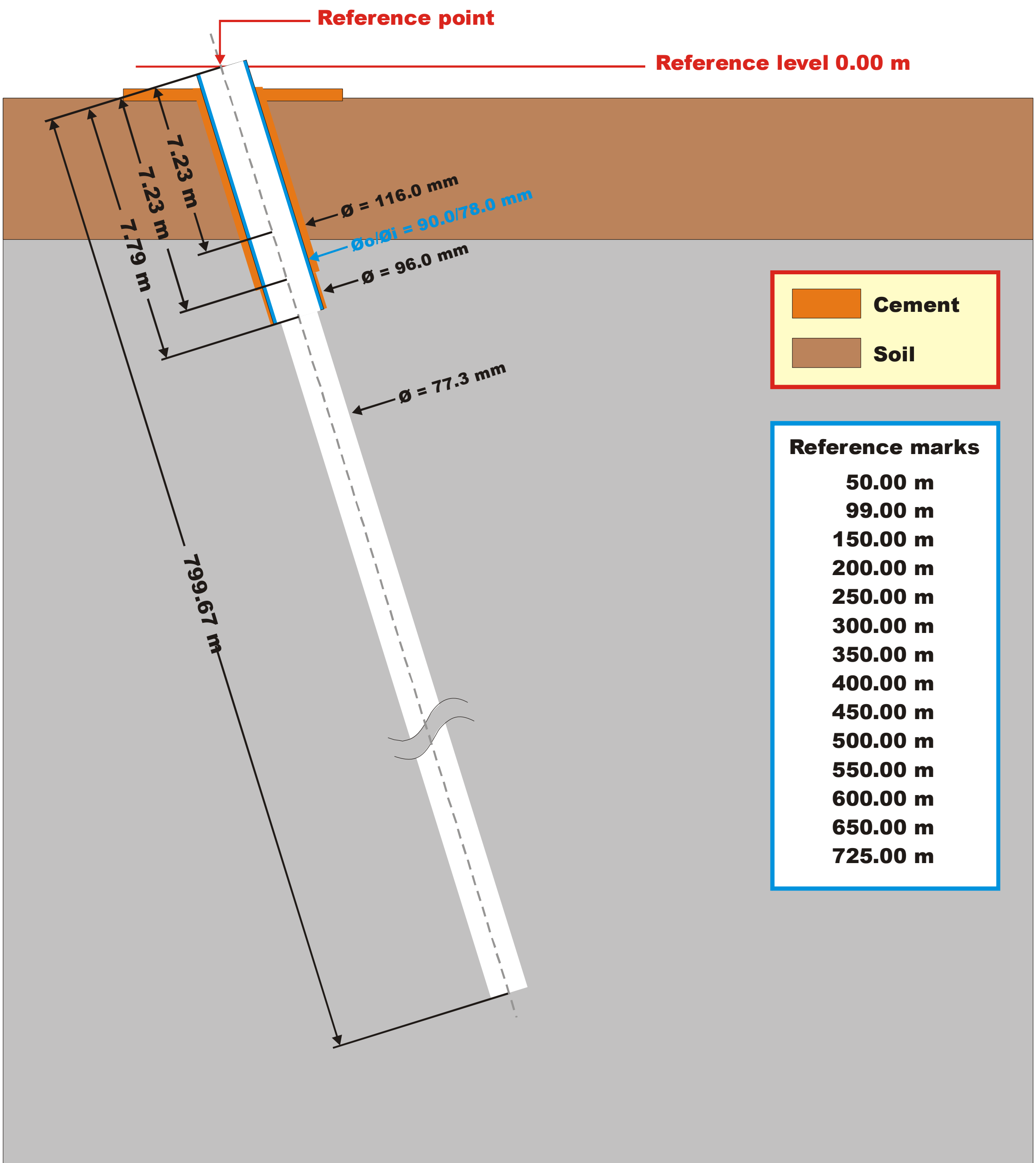


Figure A3-604. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 786.0-791.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

Appendix 4. Borehole technical data

Technical data

Borehole KFM09A



Drilling reference point

Northing: 6700115.04 (m), RT90 2,5 gon V 0:-15
Easting: 1630647.50 (m), RT90 2,5 gon V 0:-15
Elevation: 4.29 (m), RHB 70

Orientation

Bearing: 200.08°
Inclination: -59.46°

Drilling period

Drilling start date: 2005-09-05
Drilling stop date: 2005-10-27

2005-11-09 rev 2

Appendix 5. Sicada tables

Nomenclature plu_s_hole_test_d

Column	Datatype	Unit	Column Description	Alt. Symbol
site	CHAR		Investigation site name	
activity_type	CHAR		Activity type code	
start_date	DATE		Date (yymmdd hh:mm:ss)	
stop_date	DATE		Date (yymmdd hh:mm:ss)	
project	CHAR		project code	
idcode	CHAR		Object or borehole identification code	
secup	FLOAT	m	Upper section limit (m)	
seclow	FLOAT	m	Lower section limit (m)	
section_no	INTEGER	number	Section number	
test_type	CHAR		Test type code (1-7), see table description	
formation_type	CHAR		1: Rock, 2: Soil (superficial deposits)	
start_flow_period	DATE	yyyymmdd	Date & time of pumping/injection start (YYYY-MM-DD hh:mm:ss)	
stop_flow_period	DATE	yyyymmdd	Date & time of pumping/injection stop (YYYY-MM-DD hh:mm:ss)	
flow_rate_end_qp	FLOAT	m**3/s	Flow rate at the end of the flowing period	
value_type_qp	CHAR		0:true value,-1<lower meas.limit1:>upper meas.limit	
mean_flow_rate_qm	FLOAT	m**3/s	Arithmetic mean flow rate during flow period	
q_measl__l	FLOAT	m**3/s	Estimated lower measurement limit of flow rate	**Q-measl-L**
q_measl__u	FLOAT	m**3/s	Estimated upper measurement limit of flow rate	Q-measl-U
tot_volume_vp	FLOAT	m**3	Total volume of pumped or injected water	
dur_flow_phase_tp	FLOAT	s	Duration of the flowing period of the test	
dur_rec_phase_tf	FLOAT	s	Duration of the recovery period of the test	
initial_head_hi	FLOAT	m	Hydraulic head in test section at start of the flow period	
head_at_flow_end_hp	FLOAT	m	Hydraulic head in test section at stop of the flow period.	
final_head_hf	FLOAT	m	Hydraulic head in test section at stop of recovery period.	
initial_press_pi	FLOAT	kPa	Groundwater pressure in test section at start of flow period	
press_at_flow_end_pp	FLOAT	kPa	Groundwater pressure in test section at stop of flow period.	
final_press_pf	FLOAT	kPa	Ground water pressure at the end of the recovery period.	
fluid_temp_tew	FLOAT	oC	Measured section fluid temperature, see table description	
fluid_elcond_ecw	FLOAT	mS/m	Measured section fluid el. conductivity,see table descr.	
fluid_salinity_tdsw	FLOAT	mg/l	Total salinity of section fluid based on EC,see table descr.	
fluid_salinity_tdswm	FLOAT	mg/l	Tot. section fluid salinity based on water sampling,see...	
reference	CHAR		SKB report No for reports describing data and evaluation	
comments	VARCHAR		Short comment to data	
error_flag	CHAR		If error_flag = "*" then an error occured and an error	
in_use	CHAR		If in_use = "*" then the activity has been selected as	
sign	CHAR		Signature for QA data accknowledge (QA - OK)	
lp	FLOAT	m	Hydraulic point of application	

Nomenclature plu_s_hole_test_ed1

Column	Datatype	Unit	Column Description	Alt. Symbol
site	CHAR		Investigation site name	
activity_type	CHAR		Activity type code	
start_date	DATE		Date (yymmdd hh:mm:ss)	
stop_date	DATE		Date (yymmdd hh:mm:ss)	
project	CHAR		project code	

Column	Datatype	Unit	Column Description	Alt. Symbol
idcode	CHAR		Object or borehole identification code	
secup	FLOAT	m	Upper section limit (m)	
seclow	FLOAT	m	Lower section limit (m)	
section_no	INTEGER	number	Section number	
test_type	CHAR		Test type code (1-7), see table description!	
formation_type	CHAR		Formation type code. 1: Rock, 2: Soil (superficial deposits)	
lp	FLOAT	m	Hydraulic point of application for test section, see descr.	
seclen_class	FLOAT	m	Planned ordinary test interval during test campaign.	
spec_capacity_q_s	FLOAT	m**2/s	Specific capacity (Q/s) of test section, see table descript.	Q/s
value_type_q_s	CHAR		0:true value,-1:Q/s<lower meas.limit,1:Q/s>upper meas.limit	
transmissivity_tq	FLOAT	m**2/s	Tranmissivity based on Q/s, see table description	
value_type_tq	CHAR		0:true value,-1:TQ<lower meas.limit,1:TQ>upper meas.limit.	
bc_tq	CHAR		Best choice code. 1 means TQ is best choice of T, else 0	
transmissivity_moye	FLOAT	m**2/s	Transmissivity,TM, based on Moye (1967)	T_M
bc_tm	CHAR		Best choice code. 1 means Tmoye is best choice of T, else 0	
value_type_tm	CHAR		0:true value,-1:TM<lower meas.limit,1:TM>upper meas.limit.	
hydr_cond_moye	FLOAT	m/s	K_M: Hydraulic conductivity based on Moye (1967)	K_M
formation_width_b	FLOAT	m	b:Aquifer thickness repr. for T(generally b=Lw) ,see descr.	b
width_of_channel_b	FLOAT	m	B:Inferred width of formation for evaluated TB	
tb	FLOAT	m**3/s	TB:Flow capacity in 1D formation of T & width B, see descr.	
l_measl_tb	FLOAT	m**3/s	Estimated lower meas. limit for evaluated TB,see description	
u_measl_tb	FLOAT	m**3/s	Estimated upper meas. limit of evaluated TB,see description	
sb	FLOAT	m	SB:S=storativity,B=width of formation,1D model,see descript.	
assumed_sb	FLOAT	m	SB* : Assumed SB,S=storativity,B=width of formation,see...	
leakage_factor_lf	FLOAT	m	Lf:1D model for evaluation of Leakage factor	
transmissivity_tt	FLOAT	m**2/s	TT:Transmissivity of formation, 2D radial flow model,see...	T_T
value_type_tt	CHAR		0:true value,-1:TT<lower meas.limit,1:TT>upper meas.limit,	
bc_tt	CHAR		Best choice code. 1 means TT is best choice of T, else 0	
l_measl_q_s	FLOAT	m**2/s	Estimated lower meas. limit for evaluated TT,see table descr	Q/s-measl-L
u_measl_q_s	FLOAT	m**2/s	Estimated upper meas. limit for evaluated TT,see description	Q/s-measl-U
storativity_s	FLOAT		S:Storativity of formation based on 2D rad flow,see descr.	
assumed_s	FLOAT		Assumed Storativity,2D model evaluation,see table descr.	
bc_s	FLOAT		Best choice of S (Storativity) ,see descr.	
ri	FLOAT	m	Radius of influence	
ri_index	CHAR		ri index=index of radius of influence :-1,0 or 1, see descr.	
leakage_coeff	FLOAT	1/s	K'/b':2D rad flow model evaluation of leakage coeff,see desc	
hydr_cond_ksf	FLOAT	m/s	Ksf:3D model evaluation of hydraulic conductivity,see desc.	
value_type_ksf	CHAR		0:true value,-1:Ksf<lower meas.limit,1:Ksf>upper meas.limit,	
l_measl_ksf	FLOAT	m/s	Estimated lower meas.limit for evaluated Ksf,see table desc.	
u_measl_ksf	FLOAT	m/s	Estimated upper meas.limit for evaluated Ksf,see table descr	
spec_storage_ssf	FLOAT	1/m	Ssf:Specific storage,3D model evaluation,see table descr.	
assumed_ssf	FLOAT	1/m	Ssf*:Assumed Spec.storage,3D model evaluation,see table des.	
c	FLOAT	m**3/pa	C: Wellbore storage coefficient; flow or recovery period	C
cd	FLOAT		CD: Dimensionless wellbore storage coefficient	
skin	FLOAT		Skin factor;best estimate of flow/recovery period,see descr.	ξ
dt1	FLOAT	s	Estimated start time of evaluation, see table description	
dt2	FLOAT	s	Estimated stop time of evaluation. see table description	
t1	FLOAT	s	Start time for evaluated parameter from start flow period	t_1
t2	FLOAT	s	Stop time for evaluated parameter from start of flow period	t_2
dte1	FLOAT	s	Start time for evaluated parameter from start of recovery	dte_1
dte2	FLOAT	s	Stop time for evaluated parameter from start of recovery	dte_2
p_horner	FLOAT	kPa	p*:Horner extrapolated pressure, see table description	
transmissivity_t_nlr	FLOAT	m**2/s	T_NLR Transmissivity based on None Linear Regression...	

Column	Datatype	Unit	Column Description	Alt. Symbol
storativity_s_nlr	FLOAT		S_NLR=storativity based on None Linear Regression,see..	
value_type_t_nlr	CHAR		0:true value,-1:T_NLR<lower meas.limit,1:>upper meas.limit	
bc_t_nlr	CHAR		Best choice code. 1 means T_NLR is best choice of T, else 0	
c_nlr	FLOAT	m**3/pa	Wellbore storage coefficient, based on NLR, see descr.	
cd_nlr	FLOAT		Dimensionless wellbore storage constant, see table descrip.	
skin_nlr	FLOAT		Skin factor based on Non Linear Regression,see desc.	
transmissivity_t_grf	FLOAT	m**2/s	T_GRF:Transmissivity based on Genelized Radial Flow,see...	
value_type_t_grf	CHAR		0:true value,-1:T_GRF<lower meas.limit,1:>upper meas.limit	
bc_t_grf	CHAR		Best choice code. 1 means T_GRF is best choice of T, else 0	
storativity_s_grf	FLOAT		S_GRF:Storativity based on Generalized Radial Flow, see des.	
flow_dim_grf	FLOAT		Inferred flow dimesion based on Generalized Rad. Flow model	
comment	VARCHAR	no_unit	Short comment to the evaluated parameters	
error_flag	CHAR		If error_flag = "*" then an error occured and an error	
in_use	CHAR		If in_use = "*" then the activity has been selected as	
sign	CHAR		Signature for QA data accknowledge (QA - OK)	

Nomenclature plu_s_hole_test_obs

Column	Datatype	Unit	Column Description
site	CHAR		Investigation site name
activity_type	CHAR		Activity type code
idcode	CHAR		Object or borehole identification code
start_date	DATE		Date (yymmdd hh:mm:ss)
secup	FLOAT	m	Upper section limit (m)
seclow	FLOAT	m	Lower section limit (m)
obs_secup	FLOAT	m	Upper limit of observation section
obs_seclow	FLOAT	m	Lower limit of observation section
pi_above	FLOAT	kPa	Groundwater pressure above test section,start of flow period
pp_above	FLOAT	kPa	Groundwater pressure above test section,at stop flow period
pf_above	FLOAT	kPa	Groundwater pressure above test section at stop recovery per
pi_below	FLOAT	kPa	Groundwater pressure below test section at start flow period
pp_below	FLOAT	kPa	Groundwater pressure below test section at stop flow period
pf_below	FLOAT	kPa	Groundwater pressure below test section at stop recovery per
comments	VARCHAR		Comment text row (unformatted text)

KFM09A plu_s_hole_test_d. Left (This result table to SICADA includes more columns which are empty, these columns are not presented here.)

idcode	start_date	stop_date	secup	seclow	test_type	Formation_type	start_flow_period	stop_flow_period	flow_rate_end_qp	Value_type_qp	mean_flow_rate_qm
KFM09A	20051117 16:09	20051117 17:59	106.00	206.00	3	1	20051117 16:57:06	20051117 17:27:25	7.07E-05	0	9.33E-05
KFM09A	20051117 19:03	20051117 20:53	206.00	306.00	3	1	20051117 19:50:48	20051117 20:21:10	1.31E-06	0	1.62E-06
KFM09A	20051117 21:47	20051117 23:36	306.00	406.00	3	1	20051117 22:34:02	20051117 23:04:29	4.06E-06	0	7.19E-06
KFM09A	20051118 09:59	20051118 11:49	406.00	506.00	3	1	20051118 10:46:49	20051118 11:17:10	1.07E-05	0	3.77E-05
KFM09A	20051121 12:52	20051121 15:13	506.00	606.00	3	1	20051121 14:11:02	20051121 14:41:23	1.94E-06	0	8.12E-06
KFM09A	20051121 06:14	20051121 08:03	606.00	706.00	3	1	20051121 07:00:34	20051121 07:30:54	5.72E-07	0	8.03E-07
KFM09A	20051121 08:51	20051121 10:40	691.00	791.00	3	1	20051121 09:37:30	20051121 10:07:51	8.41E-07	0	1.23E-06
KFM09A	20051128 16:44	20051128 18:19	106.00	126.00	3	1	20051128 17:36:29	20051128 17:56:45	8.47E-06	0	9.98E-06
KFM09A	20051129 06:29	20051129 07:43	126.00	146.00	3	1	20051129 07:01:05	20051129 07:21:21	2.71E-05	0	4.44E-05
KFM09A	20051129 08:20	20051129 09:35	146.00	166.00	3	1	20051129 08:53:25	20051129 09:13:42	4.50E-06	0	1.26E-05
KFM09A	20051129 10:00	20051129 11:15	166.00	186.00	3	1	20051129 10:33:21	20051129 10:53:39	4.24E-05	0	4.98E-05
KFM09A	20051129 12:14	20051129 13:31	186.00	206.00	3	1	20051129 12:48:51	20051129 13:09:11	1.41E-07	0	1.63E-07
KFM09A	20051129 14:01	20051129 14:47	206.00	226.00	3	1	20051129 14:36:49	20051129 14:40:14		-1	
KFM09A	20051129 15:38	20051129 16:56	226.00	246.00	3	1	20051129 16:13:49	20051129 16:34:11	9.72E-07	0	1.18E-06
KFM09A	20051129 17:18	20051129 18:37	238.00	258.00	3	1	20051129 17:54:33	20051129 18:14:55	2.46E-07	0	3.84E-07
KFM09A	20051129 18:58	20051129 20:17	258.00	278.00	3	1	20051129 19:35:15	20051129 19:55:42	5.18E-08	0	9.90E-08
KFM09A	20051129 21:03	20051129 22:25	278.00	298.00	3	1	20051129 21:42:40	20051129 22:03:04	1.11E-07	0	1.57E-07
KFM09A	20051129 22:41	20051129 23:57	286.00	306.00	3	1	20051129 23:15:24	20051129 23:35:54	6.13E-08	0	9.62E-08
KFM09A	20051130 06:29	20051130 07:48	306.00	326.00	3	1	20051130 07:05:44	20051130 07:26:04	2.78E-07	0	6.73E-07
KFM09A	20051130 08:16	20051130 09:35	326.00	346.00	3	1	20051130 08:53:03	20051130 09:13:26	2.09E-08	0	4.56E-08
KFM09A	20051130 10:06	20051130 11:22	346.00	366.00	3	1	20051130 10:40:24	20051130 11:00:46	4.37E-08	0	5.89E-08
KFM09A	20051130 12:06	20051130 13:23	366.00	386.00	3	1	20051130 12:41:16	20051130 13:01:46	1.28E-06	0	1.60E-06
KFM09A	20051130 13:50	20051130 15:08	386.00	406.00	3	1	20051130 14:25:53	20051130 14:46:29	2.69E-06	0	5.50E-06
KFM09A	20051130 15:30	20051130 16:47	406.00	426.00	3	1	20051130 16:04:48	20051130 16:25:26	3.99E-07	0	4.89E-07
KFM09A	20051130 18:18	20051130 19:38	426.00	446.00	3	1	20051130 18:55:34	20051130 19:16:08	1.85E-05	0	4.93E-05
KFM09A	20051130 20:03	20051130 21:45	446.00	466.00	3	1	20051130 21:02:55	20051130 21:23:31	7.09E-08	0	9.94E-08
KFM09A	20051130 22:03	20051130 23:20	466.00	486.00	3	1	20051130 22:37:39	20051130 22:58:37	4.00E-08	0	7.55E-08

idcode	start_date	stop_date	secup	seclow	test_type	Formation_type	start_flow_period	stop_flow_period	flow_rate_end_qp	Value_type_qp	mean_flow_rate_qm
KFM09A	20051201 08:06	20051201 09:34	486.00	506.00	3	1	20051201 08:51:37	20051201 09:11:58	1.17E-07	0	2.67E-07
KFM09A	20051201 10:01	20051201 11:22	506.00	526.00	3	1	20051201 10:39:48	20051201 11:00:08	4.34E-08	0	7.76E-08
KFM09A	20051201 11:41	20051201 13:46	526.00	546.00	3	1	20051201 13:03:33	20051201 13:23:52	2.91E-06	0	9.83E-06
KFM09A	20051201 14:21	20051201 15:09	545.00	565.00	3	1	20051201 14:59:12	20051201 15:02:07		-1	
KFM09A	20051201 15:34	20051201 16:17	566.00	586.00	3	1	20051201 16:08:01	20051201 16:10:17		-1	
KFM09A	20051202 07:55	20051202 08:37	586.00	606.00	3	1	20051202 08:28:21	20051202 08:29:58		-1	
KFM09A	20051202 08:58	20051202 10:22	606.00	626.00	3	1	20051202 09:40:01	20051202 10:00:18	4.76E-07	0	7.39E-07
KFM09A	20051202 10:43	20051202 12:05	626.00	646.00	3	1	20051202 11:22:44	20051202 11:43:05	8.54E-08	0	1.15E-07
KFM09A	20051202 13:12	20051202 14:35	646.00	666.00	3	1	20051202 13:52:57	20051202 14:13:15	1.04E-07	0	1.27E-07
KFM09A	20051202 14:57	20051202 16:13	666.00	686.00	3	1	20051202 15:30:57	20051202 15:51:01	1.19E-08	0	3.11E-08
KFM09A	20051205 08:22	20051205 09:53	686.00	706.00	3	1	20051205 09:10:31	20051205 09:30:35	9.44E-09	0	2.33E-08
KFM09A	20051205 10:10	20051205 11:12	691.00	711.00	3	1	20051205 10:52:46	20051205 11:05:04		-1	
KFM09A	20051205 12:46	20051205 13:30	711.00	731.00	3	1	20051205 13:20:23	20051205 13:22:52		-1	
KFM09A	20051205 13:49	20051205 15:12	731.00	751.00	3	1	20051205 14:29:26	20051205 14:49:46	6.26E-08	0	8.05E-08
KFM09A	20051205 15:30	20051205 16:54	751.00	771.00	3	1	20051205 16:12:15	20051205 16:32:33	3.61E-07	0	1.07E-07
KFM09A	20051205 18:09	20051205 19:26	771.00	791.00	3	1	20051205 18:44:18	20051205 19:04:38	8.90E-07	0	4.69E-05
KFM09A	20051207 07:32	20051207 08:52	106.00	111.00	3	1	20051207 08:10:17	20051207 08:30:41	5.70E-07	0	6.88E-07
KFM09A	20051207 09:08	20051207 10:24	111.00	116.00	3	1	20051207 09:42:13	20051207 10:02:37	6.00E-08	0	7.52E-08
KFM09A	20051221 15:48	20051208 17:51	116.00	121.00	3	1	20051221 16:27:38	20051221 16:47:54	2.15E-06	0	1.42E-07
KFM09A	20051207 12:52	20051207 14:09	121.00	126.00	3	1	20051207 13:26:31	20051207 13:46:51	5.98E-06	0	6.93E-06
KFM09A	20051207 14:26	20051207 16:04	126.00	131.00	3	1	20051207 15:21:48	20051207 15:42:09	3.85E-08	0	1.12E-07
KFM09A	20051207 16:21	20051207 17:40	128.00	133.00	3	1	20051207 16:58:15	20051207 17:18:34	1.74E-05	0	2.61E-05
KFM09A	20051207 17:58	20051207 19:16	133.00	138.00	3	1	20051207 18:34:22	20051207 18:54:23	1.66E-05	0	2.67E-05
KFM09A	20051207 19:42	20051207 21:13	138.00	143.00	3	1	20051207 20:30:41	20051207 20:50:56	3.09E-07	0	3.51E-07
KFM09A	20051207 21:27	20051207 22:45	141.00	146.00	3	1	20051207 22:03:25	20051207 22:23:49	1.24E-06	0	2.35E-06
KFM09A	20051207 23:02	20051208 00:17	146.00	151.00	3	1	20051207 23:35:21	20051207 23:55:41	1.33E-06	0	5.33E-06
KFM09A	20051208 06:16	20051208 06:59	151.00	156.00	3	1	20051208 06:49:42	20051208 06:51:37		-1	
KFM09A	20051208 07:10	20051208 08:26	156.00	161.00	3	1	20051208 07:44:24	20051208 08:04:38	4.26E-06	0	1.07E-05
KFM09A	20051208 08:36	20051208 09:52	161.00	166.00	3	1	20051208 09:10:22	20051208 09:30:41	1.02E-07	0	1.07E-07
KFM09A	20051208 10:03	20051208 11:19	166.00	171.00	3	1	20051208 10:36:39	20051208 10:56:56	4.09E-05	0	4.69E-05
KFM09A	20051208 12:12	20051208 13:29	171.00	176.00	3	1	20051208 12:47:14	20051208 13:07:30	5.50E-08	0	8.37E-07

idcode	start_date	stop_date	secup	seclow	test_type	Formation_type	start_flow_period	stop_flow_period	flow_rate_end_qp	Value_type_qp	mean_flow_rate_qm
KFM09A	20051208 13:43	20051208 14:57	176.00	181.00	3	1	20051208 14:15:22	20051208 14:35:42	2.91E-07	0	3.41E-07
KFM09A	20051208 15:13	20051208 16:28	181.00	186.00	3	1	20051208 15:45:32	20051208 16:05:52	2.50E-07	0	1.90E-06
KFM09A	20051208 16:36	20051208 17:51	186.00	191.00	3	1	20051208 17:09:19	20051208 17:29:36	1.23E-07	0	1.42E-07
KFM09A	20051208 18:03	20051208 18:50	191.00	196.00	3	1	20051208 18:35:40	20051208 18:42:32		-1	
KFM09A	20051208 19:02	20051208 19:47	196.00	201.00	3	1	20051208 19:35:04	20051208 19:39:45		-1	
KFM09A	20051208 19:57	20051208 20:39	201.00	206.00	3	1	20051208 20:30:56	20051208 20:32:09		-1	
KFM09A	20051208 20:58	20051208 21:40	226.00	231.00	3	1	20051208 21:30:25	20051208 21:32:31		-1	
KFM09A	20051208 21:54	20051208 23:08	232.00	237.00	3	1	20051208 22:26:14	20051208 22:46:32	8.39E-07	0	8.63E-07
KFM09A	20051208 23:21	20051209 00:35	237.00	242.00	3	1	20051208 23:52:47	20051209 00:13:05	1.70E-06	0	1.86E-06
KFM09A	20051209 08:08	20051209 09:24	240.80	245.80	3	1	20051209 08:41:39	20051209 09:01:58	3.22E-07	0	4.57E-07
KFM09A	20051221 13:55	20051221 14:35	246.80	251.80	3	1	20051221 14:26:40	20051221 14:28:04		-1	
KFM09A	20051209 09:40	20051209 10:22	251.50	256.50	3	1	20051209 10:12:05	20051209 10:14:57		-1	
KFM09A	20051209 10:34	20051209 11:18	256.50	261.50	3	1	20051209 11:06:25	20051209 11:10:31		-1	
KFM09A	20051209 11:30	20051209 13:22	273.00	278.00	3	1	20051209 12:39:59	20051209 13:00:19	6.80E-08	0	1.00E-07
KFM09A	20051209 13:34	20051209 14:48	278.00	283.00	3	1	20051209 14:05:39	20051209 14:26:00	9.75E-08	0	1.44E-07
KFM09A	20051209 15:04	20051209 15:51	283.00	288.00	3	1	20051209 15:36:41	20051209 15:44:08		-1	
KFM09A	20051209 16:00	20051209 17:15	288.00	293.00	3	1	20051209 16:33:16	20051209 16:53:38	1.57E-08	0	2.83E-08
KFM09A	20051212 08:21	20051212 09:42	293.00	298.00	3	1	20051212 08:59:52	20051212 09:20:12	3.38E-08	0	4.10E-08
KFM09A	20051221 12:39	20051221 13:28	296.00	301.00	3	1	20051221 13:11:23	20051221 13:21:20		-1	
KFM09A	20051221 11:45	20051221 12:29	301.00	306.00	3	1	20051221 12:18:01	20051221 12:21:31		-1	
KFM09A	20051212 09:58	20051212 10:39	306.00	311.00	3	1	20051212 10:30:37	20051212 10:31:58		-1	
KFM09A	20051212 10:49	20051212 12:33	311.00	316.00	3	1	20051212 12:23:33	20051212 12:25:31		-1	
KFM09A	20051212 12:43	20051212 13:31	316.00	321.00	3	1	20051212 13:19:35	20051212 13:23:52		-1	
KFM09A	20051212 13:44	20051212 15:02	321.00	326.00	3	1	20051212 14:20:06	20051212 14:40:29	2.98E-07	0	6.68E-07
KFM09A	20051212 15:31	20051212 16:14	346.00	351.00	3	1	20051212 16:05:39	20051212 16:06:46		-1	
KFM09A	20051221 10:04	20051221 11:19	351.00	356.00	3	1	20051021 10:36:43	20051021 10:56:56	5.07E-08	0	6.90E-08
KFM09A	20051221 08:54	20051221 09:50	356.00	361.00	3	1	20051221 09:25:06	20051221 09:43:27		-1	
KFM09A	20051221 07:28	20051221 08:43	361.00	366.00	3	1	20051221 08:00:40	20051221 08:20:51	1.76E-08	0	9.48E-09
KFM09A	20051212 16:39	20051212 17:54	363.00	368.00	3	1	20051212 17:11:54	20051212 17:32:16	1.17E-08	0	1.62E-08
KFM09A	20051213 06:27	20051213 07:24	368.00	373.00	3	1	20051213 07:15:59	20051213 07:17:12		-1	
KFM09A	20051213 07:35	20051213 08:48	371.00	376.00	3	1	20051213 08:09:41	20051213 08:23:48	1.47E-06	0	2.13E-06
KFM09A	20051213 09:02	20051213 09:58	376.00	381.00	3	1	20051213 09:37:12	20051213 09:51:20		-1	

idcode	start_date	stop_date	secup	seclow	test_type	Formation_type	start_flow_period	stop_flow_period	flow_rate_end_qp	Value_type_qp	mean_flow_rate_qm
KFM09A	20051213 10:10	20051213 11:25	381.00	386.00	3	1	20051213 10:42:36	20051213 11:02:40		-1	
KFM09A	20051213 11:57	20051213 13:16	386.00	391.00	3	1	20051213 12:33:30	20051213 12:53:52	2.47E-06	0	5.33E-06
KFM09A	20051213 13:28	20051213 14:48	391.00	396.00	3	1	20051213 14:05:53	20051213 14:26:16	1.66E-07	0	1.87E-07
KFM09A	20051213 15:06	20051213 15:49	396.00	401.00	3	1	20051213 15:37:15	20051213 15:41:39		-1	
KFM09A	20051213 16:00	20051213 17:15	401.00	406.00	3	1	20051213 16:33:21	20051213 16:53:44	4.26E-07	0	4.98E-07
KFM09A	20051213 17:25	20051213 18:18	406.00	411.00	3	1	20051213 17:56:34	20051213 18:10:55		-1	
KFM09A	20051213 18:36	20051213 19:50	411.00	416.00	3	1	20051213 19:07:32	20051213 19:27:56	3.70E-07	0	5.52E-07
KFM09A	20051213 20:06	20051213 21:22	414.00	419.00	3	1	20051213 20:39:31	20051213 20:59:55	1.30E-08	0	1.05E-08
KFM09A	20051213 21:32	20051213 22:46	419.00	424.00	3	1	20051213 22:04:11	20051213 22:24:35	5.68E-08	0	6.90E-08
KFM09A	20051213 22:55	20051214 00:09	421.00	426.00	3	1	20051213 23:26:44	20051213 23:47:06	5.78E-08	0	7.13E-08
KFM09A	20051214 06:51	20051214 07:59	426.00	431.00	3	1	20051214 07:32:04	20051214 07:52:07		-1	
KFM09A	20051214 08:11	20051214 09:31	431.00	436.00	3	1	20051214 08:49:02	20051214 09:09:24	1.61E-05	0	5.02E-05
KFM09A	20051214 09:47	20051214 10:29	436.00	441.00	3	1	20051214 10:20:56	20051214 10:22:10		-1	
KFM09A	20051214 10:44	20051214 12:00	441.00	446.00	3	1	20051214 11:18:15	20051214 11:38:42	2.09E-07	0	1.94E-06
KFM09A	20051214 12:13	20051214 14:04	446.00	451.00	3	1	20051214 13:21:31	20051214 13:41:55	3.75E-08	0	1.55E-07
KFM09A	20051214 14:22	20051214 15:38	451.00	456.00	3	1	20051214 14:56:20	20051214 15:16:46	1.24E-08	0	1.48E-08
KFM09A	20051214 15:55	20051214 17:12	456.00	461.00	3	1	20051214 16:30:00	20051214 16:50:24	6.76E-08	0	5.90E-08
KFM09A	20051214 17:32	20051214 18:15	461.00	466.00	3	1	20051214 18:04:52	20051214 18:07:43		-1	
KFM09A	20051214 18:35	20051214 19:50	471.00	476.00	3	1	20051214 19:08:00	20051214 19:28:26	5.28E-08	0	7.96E-08
KFM09A	20051214 20:01	20051214 21:23	476.00	481.00	3	1	20051214 20:40:37	20051214 21:00:58	4.27E-08	0	5.18E-08
KFM09A	20051214 21:40	20051214 22:31	486.00	491.00	3	1	20051214 22:17:49	20051214 22:23:53		-1	
KFM09A	20051214 22:58	20051215 00:12	491.00	496.00	3	1	20051214 23:29:36	20051214 23:49:58	7.80E-08	0	1.03E-07
KFM09A	20051215 06:33	20051215 07:57	496.00	501.00	3	1	20051215 07:15:10	20051215 07:35:32	6.24E-08	0	1.75E-07
KFM09A	20051215 08:14	20051215 09:00	501.00	506.00	3	1	20051215 08:47:17	20051215 08:53:08		-1	
KFM09A	20051220 19:00	20051220 20:23	506.00	511.00	3	1	20051220 19:41:12	20051220 20:01:35	1.64E-08	0	1.77E-08
KFM09A	20051220 20:50	20051220 22:05	511.00	516.00	3	1	20051220 21:22:36	20051220 21:42:55	2.98E-08	0	2.82E-08
KFM09A	20051220 22:14	20051220 23:28	516.00	521.00	3	1	20051220 22:45:57	20051220 23:06:17	1.94E-08	0	2.24E-08
KFM09A	20051215 09:25	20051215 10:11	521.00	526.00	3	1	20051215 10:01:53	20051215 10:03:44		-1	
KFM09A	20051215 10:26	20051215 11:07	526.00	531.00	3	1	20051215 10:58:38	20051215 10:59:49		-1	
KFM09A	20051215 11:23	20051215 12:44	531.00	536.00	3	1	20051215 12:01:54	20051215 12:22:16	2.91E-06	0	1.06E-05
KFM09A	20051215 13:19	20051215 14:03	536.00	541.00	3	1	20051215 13:52:58	20051215 13:56:08		-1	
KFM09A	20051215 14:14	20051215 15:28	541.00	546.00	3	1	20051215 14:46:13	20051215 15:06:37	8.67E-09	0	5.55E-08

idcode	start_date	stop_date	secup	seclow	test_type	Formation_type	start_flow_period	stop_flow_period	flow_rate_end_qp	Value_type_qp	mean_flow_rate_qm
KFM09A	20051220 17:14	20051220 17:58	561.00	566.00	3	1	20051220 17:49:31	20051220 17:50:36		-1	
KFM09A	20051215 16:19	20051215 17:00	606.00	611.00	3	1	20051215 16:50:43	20051215 16:52:47		-1	
KFM09A	20051215 17:19	20051215 18:35	611.00	616.00	3	1	20051215 17:52:51	20051215 18:13:12	3.96E-07	0	6.14E-07
KFM09A	20051215 18:50	20051215 19:31	616.00	621.00	3	1	20051215 19:21:48	20051215 19:23:40		-1	
KFM09A	20051215 19:44	20051215 21:03	621.00	626.00	3	1	20051215 20:21:06	20051215 20:41:34	1.53E-07	0	2.22E-07
KFM09A	20051215 21:14	20051215 22:01	626.00	631.00	3	1	20051215 21:45:46	20051215 21:54:10		-1	
KFM09A	20051215 22:08	20051215 23:33	631.00	636.00	3	1	20051215 22:51:11	20051215 23:11:40	1.17E-08	0	2.06E-08
KFM09A	20051215 23:43	20051216 00:58	636.00	641.00	3	1	20051216 00:15:28	20051216 00:35:56	1.35E-07	0	1.34E-07
KFM09A	20051216 08:21	20051216 09:36	641.00	646.00	3	1	20051216 08:53:39	20051216 09:14:01	1.27E-08	0	9.09E-07
KFM09A	20051216 09:55	20051216 10:38	646.00	651.00	3	1	20051216 10:28:16	20051216 10:31:02		-1	
KFM09A	20051216 10:53	20051216 12:10	651.00	656.00	3	1	20051216 11:27:51	20051216 11:48:20	1.27E-07	0	2.02E-05
KFM09A	20051216 12:21	20051216 13:20	656.00	661.00	3	1	20051216 13:03:34	20051216 13:12:30		-1	
KFM09A	20051216 13:31	20051216 14:14	661.00	666.00	3	1	20051216 14:04:48	20051216 14:06:57		-1	
KFM09A	20051219 08:19	20051219 09:01	731.00	736.00	3	1	20051219 08:52:49	20051219 08:54:27		-1	
KFM09A	20051219 09:15	20051219 09:56	736.00	741.00	3	1	20051219 09:46:55	20051219 09:49:06		-1	
KFM09A	20051219 10:11	20051219 11:30	741.00	746.00	3	1	20051219 10:47:39	20051219 11:08:09	8.87E-08	0	7.57E-08
KFM09A	20051219 11:44	20051219 12:36	746.00	751.00	3	1	20051219 12:22:11	20051219 12:29:10		-1	
KFM09A	20051219 12:50	20051219 14:05	751.00	756.00	3	1	20051219 13:23:07	20051219 13:43:35	7.95E-08	0	1.26E-07
KFM09A	20051219 14:20	20051219 15:42	756.00	761.00	3	1	20051219 15:00:30	20051219 15:20:59	2.15E-07	0	3.66E-07
KFM09A	20051219 15:56	20051219 17:16	761.00	766.00	3	1	20051219 16:33:37	20051219 16:54:07	1.07E-07	0	1.57E-07
KFM09A	20051220 06:55	20051220 08:10	766.00	771.00	3	1	20051220 07:28:05	20051220 07:48:28	5.47E-08	0	7.57E-08
KFM09A	20051220 08:29	20051220 09:46	771.00	776.00	3	1	20051220 09:04:02	20051220 09:24:27	5.99E-08	0	6.39E-08
KFM09A	20051220 10:06	20051220 11:24	776.00	781.00	3	1	20051220 10:41:52	20051220 11:02:21	1.15E-07	0	1.40E-07
KFM09A	20051220 11:35	20051220 12:58	781.00	786.00	3	1	20051220 12:15:53	20051220 12:36:19	1.85E-07	0	2.36E-07
KFM09A	20051220 13:11	20051220 14:28	786.00	791.00	3	1	20051220 13:46:19	20051220 14:06:43	7.06E-07	0	9.09E-07
KFM09A	20051118 13:32	20051118 14:28	506.00 [1)]	606.00	3	1	20051118 14:18:02	20051118 14:26:00			
KFM09A	20051130 17:10	20051130 18:03	426.00[1)]	446.00	3	1	20051130 17:43:55	20051130 17:56:57			
KFM09A	20051207 10:38	20051207 12:39	116.00[1)]	121.00	3	1	20051207 12:36:48	20051207 12:38:34			

[1)] Incomplete test, interrupted and re-performed later.

KFM09A plu_s_hole_test_d. Right (This result table to SICADA includes more columns which are empty, these columns are not presented here.)

idcode	secup	seclow	q_measl__l	q_measl__u	tot_volume_vp	dur_flow_phase_tp	dur_rec_phase_tf	initial_press_pi	press_at_flow_end_pp	final_press_pf	fluid_temp_tew
KFM09A	106.00	206.00	1.7E-08	1.0E-03	1.70E-01	1819	1800	929.78	1114.19	948.54	7.92
KFM09A	206.00	306.00	1.7E-08	1.0E-03	2.95E-03	1822	1800	1746.27	1963.05	1759.94	8.08
KFM09A	306.00	406.00	1.7E-08	1.0E-03	1.31E-02	1827	1797	2542.61	2753.18	2631.48	8.87
KFM09A	406.00	506.00	1.7E-08	1.0E-03	6.87E-02	1821	1800	3314.26	3517.70	3472.12	9.51
KFM09A	506.00	606.00	1.7E-08	1.0E-03	1.48E-02	1821	1800	4075.97	4296.20	4263.63	10.58
KFM09A	606.00	706.00	1.7E-08	1.0E-03	1.46E-03	1820	1803	4781.92	4987.26	4843.19	11.54
KFM09A	691.00	791.00	1.7E-08	1.0E-03	2.24E-03	1821	1801	5371.98	5548.07	5405.64	12.22
KFM09A	106.00	126.00	1.7E-08	1.0E-03	1.22E-02	1216	1206	939.44	1152.92	946.07	7.29
KFM09A	126.00	146.00	1.7E-08	1.0E-03	5.40E-02	1216	1206	1108.50	1324.71	1158.02	7.35
KFM09A	146.00	166.00	1.7E-08	1.0E-03	1.54E-02	1217	1200	1277.24	1460.00	1389.29	7.52
KFM09A	166.00	186.00	1.7E-08	1.0E-03	6.07E-02	1218	1205	1439.66	1628.85	1451.67	7.50
KFM09A	186.00	206.00	1.7E-08	1.0E-03	1.99E-04	1220	1202	1609.00	1908.70	1627.19	7.82
KFM09A	206.00	226.00	5.1E-09	1.0E-03		205	321	1799.82	1971.07	1959.47	7.99
KFM09A	226.00	246.00	1.7E-08	1.0E-03	1.45E-03	1222	1200	1936.29	2142.18	1942.92	8.15
KFM09A	238.00	258.00	1.7E-08	1.0E-03	4.70E-04	1222	1197	2036.61	2246.50	2073.17	8.27
KFM09A	258.00	278.00	1.7E-08	1.0E-03	1.22E-04	1227	1194	2205.79	2409.18	2271.89	8.43
KFM09A	278.00	298.00	1.7E-08	1.0E-03	1.92E-04	1224	1194	2363.51	2574.60	2423.68	8.61
KFM09A	286.00	306.00	1.7E-08	1.0E-03	1.19E-04	1230	1191	2426.85	2640.10	2497.64	8.67
KFM09A	306.00	326.00	1.7E-08	1.0E-03	8.23E-04	1220	1203	2588.71	2788.52	2720.63	8.83
KFM09A	326.00	346.00	1.7E-08	1.0E-03	5.58E-05	1223	1202	2751.68	2952.80	2816.12	8.99
KFM09A	346.00	366.00	1.7E-08	1.0E-03	7.20E-05	1222	1200	2908.57	3113.84	2949.69	9.17
KFM09A	366.00	386.00	1.7E-08	1.0E-03	1.98E-03	1230	1189	3063.39	3264.59	3103.70	9.33
KFM09A	386.00	406.00	1.7E-08	1.0E-03	6.80E-03	1236	1185	3219.88	3419.73	3326.14	9.51
KFM09A	406.00	426.00	1.7E-08	1.0E-03	6.05E-04	1238	1184	3378.16	3578.01	3432.11	9.68
KFM09A	426.00	446.00	1.7E-08	1.0E-03	6.10E-02	1234	1185	3545.41	3765.49	3714.71	9.66
KFM09A	446.00	466.00	1.7E-08	1.0E-03	1.23E-04	1236	1184	3693.33	3922.81	3730.72	10.03
KFM09A	466.00	486.00	1.7E-08	1.0E-03	9.52E-05	1258	1162	3856.58	4029.33	3923.36	10.21

idcode	secup	seclow	q_measl__l	q_measl__u	tot_volume_vp	dur_flow_phase_tp	dur_rec_phase_tf	initial_press_pi	press_at_flow_end_pp	final_press_pf	fluid_temp_tew
KFM09A	486.00	506.00	1.7E-08	1.0E-03	3.27E-04	1221	1200	4001.32	4206.10	4108.27	10.39
KFM09A	506.00	526.00	1.7E-08	1.0E-03	9.50E-05	1220	1200	4171.74	4362.23	4210.38	10.56
KFM09A	526.00	546.00	1.7E-08	1.0E-03	1.20E-02	1219	1203	4303.10	4508.03	4472.57	10.73
KFM09A	545.00	565.00	5.1E-09	1.0E-03		175	321	4514.10	4661.19	4675.69	10.91
KFM09A	566.00	586.00	5.1E-09	1.0E-03		136	321	4631.11	4820.31	4823.61	11.09
KFM09A	586.00	606.00	5.1E-09	1.0E-03		97	322	4765.93	4982.58	4989.21	11.28
KFM09A	606.00	626.00	1.7E-08	1.0E-03	9.01E-04	1217	1205	4896.47	5096.82	4980.92	11.45
KFM09A	626.00	646.00	1.7E-08	1.0E-03	1.41E-04	1221	1200	5050.61	5258.42	5072.55	11.61
KFM09A	646.00	666.00	1.7E-08	1.0E-03	1.55E-04	1218	1205	5186.25	5389.93	5211.64	11.79
KFM09A	666.00	686.00	5.1E-09	1.0E-03	3.74E-05	1204	1221	5355.15	5533.99	5469.96	11.97
KFM09A	686.00	706.00	5.1E-09	1.0E-03	2.81E-05	1204	1221	5498.11	5687.43	5619.55	12.13
KFM09A	691.00	711.00	3.9E-09	1.0E-03		738	321	5561.73	5724.42	5713.38	12.17
KFM09A	711.00	731.00	3.9E-09	1.0E-03		149	321	5679.43	5864.34	5869.58	12.36
KFM09A	731.00	751.00	1.7E-08	1.0E-03	9.84E-05	1220	1203	5782.93	5995.56	5819.36	12.52
KFM09A	751.00	771.00	1.7E-08	1.0E-03	1.31E-04	1218	1203	5915.12	6118.38	1406.62	12.67
KFM09A	771.00	791.00	1.7E-08	1.0E+00	5.72E-02	1220	1184	6056.14	6271.55	1456.30	12.83
KFM09A	106.00	111.00	1.7E-08	1.0E-03	8.42E-04	1224	1195	948.90	1151.62	995.96	7.28
KFM09A	111.00	116.00	1.7E-08	1.0E-03	9.20E-05	1224	1197	993.19	1200.74	1037.91	7.30
KFM09A	116.00	121.00	1.7E-08	1.1E+01	1.73E-04	1216	1206	1025.62	1225.72	1627.41	7.26
KFM09A	121.00	126.00	1.7E-08	1.0E-03	8.47E-03	1220	1197	1074.34	1252.70	1076.55	7.31
KFM09A	126.00	131.00	1.7E-08	1.0E-03	1.37E-04	1221	1196	1121.53	1323.83	1249.86	7.42
KFM09A	128.00	133.00	1.7E-08	1.0E-03	3.18E-02	1219	1197	1131.88	1348.66	1163.76	7.30
KFM09A	133.00	138.00	1.7E-08	1.0E-03	3.21E-02	1201	1197	1174.24	1409.45	1217.29	7.36
KFM09A	138.00	143.00	1.7E-08	1.0E-03	4.28E-04	1215	1197	1215.08	1415.79	1219.50	7.51
KFM09A	141.00	146.00	1.7E-08	1.0E-03	2.88E-03	1224	1194	1240.89	1466.23	1321.06	7.53
KFM09A	146.00	151.00	1.7E-08	1.0E-03	6.51E-03	1220	1187	1284.09	1510.35	1450.22	7.53
KFM09A	151.00	156.00	5.1E-09	1.0E-03		115	321	1349.21	1565.72	1571.10	7.56
KFM09A	156.00	161.00	1.7E-08	1.0E-03	1.31E-02	1214	1197	1365.50	1573.10	1482.79	7.57
KFM09A	161.00	166.00	1.7E-08	1.0E-03	1.31E-04	1219	1199	1408.00	1586.50	1406.62	7.70
KFM09A	166.00	171.00	1.7E-08	1.0E-03	5.72E-02	1217	1200	1447.05	1626.80	1456.30	7.44
KFM09A	171.00	176.00	1.7E-08	1.0E-03	1.03E-03	1216	1184	1496.45	1703.03	1687.02	7.76

idcode	secup	seclow	q_measl__l	q_measl__u	tot_volume_vp	dur_flow_phase_tp	dur_rec_phase_tf	initial_press_pi	press_at_flow_end_pp	final_press_pf	fluid_temp_tew
KFM09A	176.00	181.00	1.7E-08	1.0E-03	4.15E-04	1220	1199	1534.00	1734.49	1557.86	7.76
KFM09A	181.00	186.00	1.7E-08	1.0E-03	2.35E-03	1220	1184	1575.38	1803.90	1780.30	7.77
KFM09A	186.00	191.00	1.7E-08	1.0E-03	1.73E-04	1217	1200	1616.92	1832.60	1627.41	7.81
KFM09A	191.00	196.00	5.3E-09	1.0E-03		412	322	1677.49	1875.23	1828.87	7.85
KFM09A	196.00	201.00	4.1E-09	1.0E-03		281	321	1710.62	1916.50	1891.79	7.88
KFM09A	201.00	206.00	5.3E-09	1.0E-03		73	322	1766.78	1957.48	1965.21	7.93
KFM09A	226.00	231.00	5.3E-09	1.0E-03		126	321	1961.89	2161.15	2158.94	8.13
KFM09A	232.00	237.00	1.7E-08	1.0E-03	1.05E-03	1218	1202	1992.95	2191.65	1995.02	8.20
KFM09A	237.00	242.00	1.7E-08	1.0E-03	2.27E-03	1218	1203	2032.55	2232.77	2040.28	8.25
KFM09A	240.80	245.80	1.7E-08	1.0E-03	5.58E-04	1219	1202	2060.01	2263.69	2071.18	8.29
KFM09A	246.80	251.80	4.1E-09	1.0E+01		84	322	2184.89	2323.99	2971.99	8.27
KFM09A	251.50	256.50	5.3E-09	1.0E-03		172	321	2217.45	2385.25	2408.43	8.35
KFM09A	256.50	261.50	6.5E-09	1.0E-03		246	321	2239.39	2427.20	2424.45	8.39
KFM09A	273.00	278.00	1.7E-08	1.0E-03	1.22E-04	1220	1200	2328.68	2560.78	2393.53	8.54
KFM09A	278.00	283.00	1.7E-08	1.0E-03	1.76E-04	1221	1202	2369.80	2576.30	2435.48	8.58
KFM09A	283.00	288.00	5.3E-09	1.0E-03		447	321	2409.26	2618.73	2574.58	8.62
KFM09A	288.00	293.00	1.0E-08	1.0E-03	3.40E-05	1222	1221	2459.90	2659.88	2540.35	8.67
KFM09A	293.00	298.00	1.7E-08	1.0E-03	5.00E-05	1220	1203	2493.43	2728.00	2549.74	8.71
KFM09A	296.00	301.00	4.1E-09	7.0E+00		597	322	2521.45	2730.23	3349.53	8.72
KFM09A	301.00	306.00	4.1E-09	8.0E+00		210	321	2567.81	2767.21	3301.51	8.73
KFM09A	306.00	311.00	6.5E-09	1.0E-03		81	321	2678.48	2831.80	2864.35	8.81
KFM09A	311.00	316.00	2.8E-09	1.0E-03		118	322	2652.96	2872.36	2868.77	8.85
KFM09A	316.00	321.00	4.1E-09	1.0E-03		257	321	2674.48	2942.73	2935.01	8.88
KFM09A	321.00	326.00	1.7E-08	1.0E-03	8.16E-04	1223	1202	2712.56	2913.42	2845.04	8.94
KFM09A	346.00	351.00	6.5E-09	1.0E-03		67	321	3017.39	3117.02	3125.44	9.14
KFM09A	351.00	356.00	1.7E-08	3.0E+00	8.44E-05	1213	1211	2958.18	3169.22	3512.92	9.19
KFM09A	356.00	361.00	4.1E-09	4.0E+00		1101	321	2991.17	3206.99	3532.23	9.25
KFM09A	361.00	366.00	4.1E-09	5.0E+00	1.14E-05	1211	1221	3026.22	3242.46	3698.38	9.25
KFM09A	363.00	368.00	5.0E-09	1.0E-03	1.95E-05	1222	1221	3062.65	3254.73	3095.07	9.29
KFM09A	368.00	373.00	5.3E-09	1.0E-03		73	321	3128.47	3316.41	3294.88	9.35
KFM09A	371.00	376.00	1.7E-08	1.0E-03	2.12E-03	847	1221	3108.19	3309.50	3140.33	9.38
KFM09A	376.00	381.00	5.0E-09	1.0E-03		848	321	3174.01	3361.53	3334.08	9.40

idcode	secup	seclow	q_measl__l	q_measl__u	tot_volume_vp	dur_flow_phase_tp	dur_rec_phase_tf	initial_press_pi	press_at_flow_end_pp	final_press_pf	fluid_temp_tew
KFM09A	381.00	386.00	5.3E-09	1.0E-03		1204	1221	3234.58	3403.07	3284.95	9.45
KFM09A	386.00	391.00	1.7E-08	1.0E-03	6.53E-03	1222	1200	3226.58	3437.98	3349.53	9.52
KFM09A	391.00	396.00	1.7E-08	1.0E-03	2.29E-04	1223	1202	3274.47	3481.73	3301.51	9.55
KFM09A	396.00	401.00	6.5E-09	1.0E-03		264	321	3321.10	3524.50	3485.87	9.57
KFM09A	401.00	406.00	1.7E-08	1.0E-03	6.09E-04	1223	1200	3346.08	3547.69	3369.95	9.61
KFM09A	406.00	411.00	5.3E-09	1.0E-03		861	321	3392.03	3584.11	3550.45	9.65
KFM09A	411.00	416.00	1.7E-08	1.0E-03	6.76E-04	1224	1200	3426.25	3621.31	3496.35	9.69
KFM09A	414.00	419.00	5.3E-09	1.0E-03	1.27E-05	1224	1221	3460.47	3654.12	3480.91	9.72
KFM09A	419.00	424.00	1.7E-08	1.0E-03	8.44E-05	1224	1200	3488.63	3692.58	3512.92	9.77
KFM09A	421.00	426.00	1.7E-08	1.0E-03	8.73E-05	1222	1200	3515.00	3708.32	3532.23	9.79
KFM09A	426.00	431.00	7.8E-09	1.0E-03		1203	322	3560.79	3773.30	3698.38	9.89
KFM09A	431.00	436.00	1.7E-08	1.0E-03	6.15E-02	1222	1200	3579.70	3802.83	3753.02	9.65
KFM09A	436.00	441.00	6.0E-09	1.0E-03		74	321	3649.79	3829.74	3837.47	10.00
KFM09A	441.00	446.00	1.7E-08	1.0E-03	2.41E-03	1227	1182	3661.40	3888.20	3871.14	10.03
KFM09A	446.00	451.00	1.7E-08	1.0E-03	1.90E-04	1224	1200	3702.24	3909.77	3866.72	10.02
KFM09A	451.00	456.00	5.3E-09	1.0E-03	1.78E-05	1226	1221	3761.02	3951.96	3840.22	10.05
KFM09A	456.00	461.00	1.7E-08	1.0E-03	7.22E-05	1224	1200	3787.78	3990.92	3815.94	10.09
KFM09A	461.00	466.00	2.8E-09	1.0E-03		171	322	3916.81	4031.76	4071.50	10.13
KFM09A	471.00	476.00	1.7E-08	1.0E-03	9.75E-05	1226	1199	3902.46	4111.10	3964.42	10.23
KFM09A	476.00	481.00	1.7E-08	1.0E-03	6.33E-05	1221	1203	3964.43	4153.74	4008.03	10.28
KFM09A	486.00	491.00	5.3E-09	1.0E-03		364	321	4047.08	4229.36	4217.76	10.36
KFM09A	491.00	496.00	1.7E-08	1.0E-03	1.26E-04	1222	1200	4063.22	4261.51	4095.23	10.41
KFM09A	496.00	501.00	1.7E-08	1.0E-03	2.15E-04	1222	1200	4090.13	4297.53	4222.18	10.46
KFM09A	501.00	506.00	5.0E-09	1.0E-03		351	321	4165.19	4330.23	4289.52	10.49
KFM09A	506.00	511.00	4.1E-09	1.0E-03	2.13E-05	1223	1221	4215.56	4366.80	4289.52	10.54
KFM09A	511.00	516.00	1.7E-08	1.0E-03	3.44E-05	1219	1206	4232.67	4403.23	4229.36	10.60
KFM09A	516.00	521.00	7.7E-09	1.0E-03	2.70E-05	1220	1221	4254.20	4440.03	4285.67	10.63
KFM09A	521.00	526.00	5.3E-09	1.0E-03		111	321	4405.30	4484.51	4539.01	10.67
KFM09A	526.00	531.00	5.3E-09	1.0E-03		71	321	4442.14	4520.81	4592.00	10.73
KFM09A	531.00	536.00	1.7E-08	1.0E-03	1.30E-02	1222	1199	4354.65	4571.03	4535.15	10.76
KFM09A	536.00	541.00	5.3E-09	1.0E-03		190	320	4479.13	4594.76	4560.54	10.86
KFM09A	541.00	546.00	5.3E-09	1.0E-03	6.67E-05	1224	1221	4437.45	4632.29	4613.53	10.88

idcode	secup	seclow	q_measl__l	q_measl__u	tot_volume_vp	dur_flow_phase_tp	dur_rec_phase_tf	initial_press_pi	press_at_flow_end_pp	final_press_pf	fluid_temp_tew
KFM09A	561.00	566.00	5.3E-09	1.0E-03		65	321	4726.95	4774.42	4801.19	11.02
KFM09A	606.00	611.00	4.1E-09	1.0E-03		124	322	5042.26	5120.24	5224.00	11.42
KFM09A	611.00	616.00	1.7E-08	1.0E-03	7.50E-04	1221	1200	4956.43	5148.26	5044.06	11.46
KFM09A	616.00	621.00	5.3E-09	1.0E-03		112	322	5077.59	5206.34	5272.02	11.51
KFM09A	621.00	626.00	1.7E-08	1.0E-03	2.73E-04	1228	1194	5032.46	5244.56	5127.97	11.55
KFM09A	626.00	631.00	4.1E-09	1.0E-03		504	322	5085.18	5263.75	5233.38	11.60
KFM09A	631.00	636.00	5.3E-09	1.0E-03	2.47E-05	1229	1220	5136.79	5301.28	5249.39	11.64
KFM09A	636.00	641.00	1.7E-08	1.0E-03	1.64E-04	1228	1194	5144.52	5335.36	5146.73	11.68
KFM09A	641.00	646.00	2.8E-09	1.0E-03	1.11E-03	1222	1221	5195.30	5374.69	5235.59	11.75
KFM09A	646.00	651.00	2.8E-09	1.0E-03		166	321	5309.69	5410.56	5419.40	11.78
KFM09A	651.00	656.00	1.7E-08	1.0E-03	9.65E-03	1229	1194	5248.56	5444.23	5280.30	11.82
KFM09A	656.00	661.00	6.5E-09	1.0E-03		536	321	5344.46	5486.74	5472.94	11.87
KFM09A	661.00	666.00	4.1E-09	1.0E-03		129	321				
KFM09A	731.00	736.00	5.3E-09	1.0E-03		98	321	5867.31	6009.44	5986.26	12.49
KFM09A	736.00	741.00	5.3E-09	1.0E-03		131	321	5860.27	6044.22	5996.20	12.57
KFM09A	741.00	746.00	1.7E-08	1.0E-03	9.31E-05	1230	1191	5881.11	6078.44	5914.50	12.59
KFM09A	746.00	751.00	5.3E-09	1.0E-03		419	321	5928.44	6112.66	6074.02	12.64
KFM09A	751.00	756.00	1.7E-08	1.0E-03	1.55E-04	1228	1194	5957.42	6143.29	6000.07	12.66
KFM09A	756.00	761.00	1.7E-08	1.0E-03	4.51E-04	1229	1189	5986.68	6192.63	6040.91	12.71
KFM09A	761.00	766.00	1.7E-08	1.0E-03	1.92E-04	1230	1199	6021.04	6221.97	6050.29	12.75
KFM09A	766.00	771.00	1.7E-08	1.0E-03	9.27E-05	1223	1187	6049.32	6239.82	6077.34	12.79
KFM09A	771.00	776.00	1.7E-08	1.0E-03	7.84E-05	1225	1187	6086.85	6319.41	6096.65	12.83
KFM09A	776.00	781.00	1.7E-08	1.0E-03	1.71E-04	1229	1187	6119.15	6309.34	6137.49	12.87
KFM09A	781.00	786.00	1.7E-08	1.0E-03	2.90E-04	1226	1187	6152.12	6325.44	6168.40	12.92
KFM09A	786.00	791.00	1.7E-08	1.0E-03	1.11E-03	1224	1187	6184.96	6388.23	6192.69	12.96
KFM09A	506.00 [1)]	606.00				478	24	4063.27	4265.15	4264.74	10.56
KFM09A	426.00[1)]	446.00				782	253	3535.19	3703.67	3675.53	9.70
KFM09A	116.00[1)]	121.00				106	13	1074.89	1242.69	1074.34	7.32

[1)] Incomplete test, interrupted and re-performed later.

KFM09A plu_s_hole_test_ed1. Left (This result table to SICADA includes more columns which are empty, these columns are not presented here.)

idcode	start_date	stop_date	secup	seclow	test_type	formation_type	spec_capacity_q_s	value_type_q_s	transmissivity_moye	bc_tm	value_type_tm	hydr_cond_moye	formation_width_b
KFM09A	20051117 16:09	20051117 17:59	106.00	206.00	3	1	3.76E-06	0	4.89E-06	0	0	4.89E-08	100.00
KFM09A	20051117 19:03	20051117 20:53	206.00	306.00	3	1	5.92E-08	0	7.69E-08	0	0	7.69E-10	100.00
KFM09A	20051117 21:47	20051117 23:36	306.00	406.00	3	1	1.89E-07	0	2.46E-07	0	0	2.46E-09	100.00
KFM09A	20051118 09:59	20051118 11:49	406.00	506.00	3	1	5.18E-07	0	6.74E-07	1	0	6.74E-09	100.00
KFM09A	20051121 12:52	20051121 15:13	506.00	606.00	3	1	8.66E-08	0	1.13E-07	1	0	1.13E-09	100.00
KFM09A	20051121 06:14	20051121 08:03	606.00	706.00	3	1	2.74E-08	0	3.56E-08	0	0	3.56E-10	100.00
KFM09A	20051121 08:51	20051121 10:40	691.00	791.00	3	1	4.69E-08	0	6.09E-08	0	0	6.09E-10	100.00
KFM09A	20051128 16:44	20051128 18:19	106.00	126.00	3	1	3.89E-07	0	4.06E-07	0	0	2.03E-08	20.00
KFM09A	20051129 06:29	20051129 07:43	126.00	146.00	3	1	1.23E-06	0	1.28E-06	0	0	6.42E-08	20.00
KFM09A	20051129 08:20	20051129 09:35	146.00	166.00	3	1	2.41E-07	0	2.52E-07	0	0	1.26E-08	20.00
KFM09A	20051129 10:00	20051129 11:15	166.00	186.00	3	1	2.20E-06	0	2.29E-06	0	0	1.15E-07	20.00
KFM09A	20051129 12:14	20051129 13:31	186.00	206.00	3	1	4.62E-09	0	4.82E-09	0	0	2.41E-10	20.00
KFM09A	20051129 14:01	20051129 14:47	206.00	226.00	3	1	2.55E-10	-1	2.66E-10	0	-1	1.33E-11	20.00
KFM09A	20051129 15:38	20051129 16:56	226.00	246.00	3	1	4.63E-08	0	4.83E-08	0	0	2.42E-09	20.00
KFM09A	20051129 17:18	20051129 18:37	238.00	258.00	3	1	1.15E-08	0	1.20E-08	0	0	6.00E-10	20.00
KFM09A	20051129 18:58	20051129 20:17	258.00	278.00	3	1	2.50E-09	0	2.61E-09	0	0	1.30E-10	20.00
KFM09A	20051129 21:03	20051129 22:25	278.00	298.00	3	1	5.15E-09	0	5.37E-09	0	0	2.69E-10	20.00
KFM09A	20051129 22:41	20051129 23:57	286.00	306.00	3	1	2.82E-09	0	2.95E-09	0	0	1.47E-10	20.00
KFM09A	20051130 06:29	20051130 07:48	306.00	326.00	3	1	1.37E-08	0	1.43E-08	0	0	7.13E-10	20.00
KFM09A	20051130 08:16	20051130 09:35	326.00	346.00	3	1	1.02E-09	0	1.06E-09	0	0	5.31E-11	20.00
KFM09A	20051130 10:06	20051130 11:22	346.00	366.00	3	1	2.09E-09	0	2.18E-09	0	0	1.09E-10	20.00
KFM09A	20051130 12:06	20051130 13:23	366.00	386.00	3	1	6.23E-08	0	6.50E-08	0	0	3.25E-09	20.00
KFM09A	20051130 13:50	20051130 15:08	386.00	406.00	3	1	1.32E-07	0	1.38E-07	1	0	6.89E-09	20.00
KFM09A	20051130 15:30	20051130 16:47	406.00	426.00	3	1	1.96E-08	0	2.04E-08	1	0	1.02E-09	20.00
KFM09A	20051130 18:18	20051130 19:38	426.00	446.00	3	1	8.24E-07	0	8.60E-07	1	0	4.30E-08	20.00
KFM09A	20051130 20:03	20051130 21:45	446.00	466.00	3	1	3.03E-09	0	3.16E-09	0	0	1.58E-10	20.00
KFM09A	20051130 22:03	20051130 23:20	466.00	486.00	3	1	2.27E-09	0	2.37E-09	0	0	1.19E-10	20.00
KFM09A	20051201 08:06	20051201 09:34	486.00	506.00	3	1	5.62E-09	0	5.86E-09	0	0	2.93E-10	20.00
KFM09A	20051201 10:01	20051201 11:22	506.00	526.00	3	1	2.24E-09	0	2.33E-09	0	0	1.17E-10	20.00

idcode	start_date	stop_date	secup	seclow	test_type	formation_type	spec_capacity_q_s	value_type_q_s	transmissivity_moye	bc_tm	value_type_tm	hydr_cond_moye	formation_width_b
KFM09A	20051201 11:41	20051201 13:46	526.00	546.00	3	1	1.39E-07	0	1.45E-07	1	0	7.27E-09	20.00
KFM09A	20051201 14:21	20051201 15:09	545.00	565.00	3	1	2.55E-10	-1	2.66E-10	0	-1	1.33E-11	20.00
KFM09A	20051201 15:34	20051201 16:17	566.00	586.00	3	1	2.55E-10	-1	2.66E-10	0	-1	1.33E-11	20.00
KFM09A	20051202 07:55	20051202 08:37	586.00	606.00	3	1	2.55E-10	-1	2.66E-10	0	-1	1.33E-11	20.00
KFM09A	20051202 08:58	20051202 10:22	606.00	626.00	3	1	2.33E-08	0	2.43E-08	0	0	1.22E-09	20.00
KFM09A	20051202 10:43	20051202 12:05	626.00	646.00	3	1	4.03E-09	0	4.21E-09	0	0	2.10E-10	20.00
KFM09A	20051202 13:12	20051202 14:35	646.00	666.00	3	1	5.01E-09	0	5.22E-09	0	0	2.61E-10	20.00
KFM09A	20051202 14:57	20051202 16:13	666.00	686.00	3	1	6.54E-10	0	6.82E-10	1	0	3.41E-11	20.00
KFM09A	20051205 08:22	20051205 09:53	686.00	706.00	3	1	4.89E-10	0	5.10E-10	0	0	2.55E-11	20.00
KFM09A	20051205 10:10	20051205 11:12	691.00	711.00	3	1	1.94E-10	-1	2.02E-10	0	-1	1.01E-11	20.00
KFM09A	20051205 12:46	20051205 13:30	711.00	731.00	3	1	1.94E-10	-1	2.02E-10	0	-1	1.01E-11	20.00
KFM09A	20051205 13:49	20051205 15:12	731.00	751.00	3	1	2.89E-09	0	3.01E-09	0	0	1.51E-10	20.00
KFM09A	20051205 15:30	20051205 16:54	751.00	771.00	3	1	1.74E-08	0	1.82E-08	0	0	9.10E-10	20.00
KFM09A	20051205 18:09	20051205 19:26	771.00	791.00	3	1	4.06E-08	0	4.23E-08	0	0	2.12E-09	20.00
KFM09A	20051207 07:32	20051207 08:52	106.00	111.00	3	1	2.76E-08	0	2.27E-08	0	0	4.54E-09	5.00
KFM09A	20051207 09:08	20051207 10:24	111.00	116.00	3	1	2.84E-09	0	2.33E-09	0	0	4.67E-10	5.00
KFM09A	20051221 15:48	20051208 17:51	116.00	121.00	3	1	1.06E-07	0	8.68E-08	0	0	1.74E-08	5.00
KFM09A	20051207 12:52	20051207 14:09	121.00	126.00	3	1	3.29E-07	0	2.71E-07	0	0	5.41E-08	5.00
KFM09A	20051207 14:26	20051207 16:04	126.00	131.00	3	1	1.87E-09	0	1.54E-09	0	0	3.07E-10	5.00
KFM09A	20051207 16:21	20051207 17:40	128.00	133.00	3	1	7.90E-07	0	6.50E-07	0	0	1.30E-07	5.00
KFM09A	20051207 17:58	20051207 19:16	133.00	138.00	3	1	6.94E-07	0	5.71E-07	0	0	1.14E-07	5.00
KFM09A	20051207 19:42	20051207 21:13	138.00	143.00	3	1	1.51E-08	0	1.24E-08	0	0	2.49E-09	5.00
KFM09A	20051207 21:27	20051207 22:45	141.00	146.00	3	1	5.38E-08	0	4.43E-08	0	0	8.86E-09	5.00
KFM09A	20051207 23:02	20051208 00:17	146.00	151.00	3	1	5.77E-08	0	4.75E-08	0	0	9.49E-09	5.00
KFM09A	20051208 06:16	20051208 06:59	151.00	156.00	3	1	2.55E-10	-1	2.10E-10	0	-1	4.20E-11	5.00
KFM09A	20051208 07:10	20051208 08:26	156.00	161.00	3	1	2.02E-07	0	1.66E-07	0	0	3.32E-08	5.00
KFM09A	20051208 08:36	20051208 09:52	161.00	166.00	3	1	5.60E-09	0	4.60E-09	1	0	9.21E-10	5.00
KFM09A	20051208 10:03	20051208 11:19	166.00	171.00	3	1	2.23E-06	0	1.84E-06	0	0	3.67E-07	5.00
KFM09A	20051208 12:12	20051208 13:29	171.00	176.00	3	1	2.61E-09	0	2.15E-09	1	0	4.30E-10	5.00
KFM09A	20051208 13:43	20051208 14:57	176.00	181.00	3	1	1.42E-08	0	1.17E-08	0	0	2.34E-09	5.00
KFM09A	20051208 15:13	20051208 16:28	181.00	186.00	3	1	1.07E-08	0	8.83E-09	1	0	1.77E-09	5.00
KFM09A	20051208 16:36	20051208 17:51	186.00	191.00	3	1	5.60E-09	0	4.60E-09	0	0	9.21E-10	5.00
KFM09A	20051208 18:03	20051208 18:50	191.00	196.00	3	1	2.64E-10	-1	2.17E-10	0	-1	4.35E-11	5.00

idcode	start_date	stop_date	secup	seclow	test_type	formation_type	spec_capacity_q_s	value_type_q_s	transmissivity_moye	bc_tm	value_type_tm	hydr_cond_moye	formation_width_b
KFM09A	20051208 19:02	20051208 19:47	196.00	201.00	3	1	2.04E-10	-1	1.68E-10	0	-1	3.36E-11	5.00
KFM09A	20051208 19:57	20051208 20:39	201.00	206.00	3	1	2.64E-10	-1	2.17E-10	0	-1	4.35E-11	5.00
KFM09A	20051208 20:58	20051208 21:40	226.00	231.00	3	1	2.64E-10	-1	2.17E-10	0	-1	4.35E-11	5.00
KFM09A	20051208 21:54	20051208 23:08	232.00	237.00	3	1	4.14E-08	0	3.41E-08	0	0	6.81E-09	5.00
KFM09A	20051208 23:21	20051209 00:35	237.00	242.00	3	1	8.31E-08	0	6.84E-08	0	0	1.37E-08	5.00
KFM09A	20051209 08:08	20051209 09:24	240.80	245.80	3	1	1.55E-08	0	1.27E-08	0	0	2.55E-09	5.00
KFM09A	20051221 13:55	20051221 14:35	246.80	251.80	3	1	2.04E-10	-1	1.68E-10	0	-1	3.36E-11	5.00
KFM09A	20051209 09:40	20051209 10:22	251.50	256.50	3	1	2.64E-10	-1	2.17E-10	0	-1	4.35E-11	5.00
KFM09A	20051209 10:34	20051209 11:18	256.50	261.50	3	1	3.27E-10	-1	2.69E-10	0	-1	5.37E-11	5.00
KFM09A	20051209 11:30	20051209 13:22	273.00	278.00	3	1	2.88E-09	0	2.37E-09	0	0	4.73E-10	5.00
KFM09A	20051209 13:34	20051209 14:48	278.00	283.00	3	1	4.63E-09	0	3.81E-09	0	0	7.62E-10	5.00
KFM09A	20051209 15:04	20051209 15:51	283.00	288.00	3	1	2.64E-10	-1	2.17E-10	0	-1	4.35E-11	5.00
KFM09A	20051209 16:00	20051209 17:15	288.00	293.00	3	1	7.71E-10	0	6.35E-10	1	0	1.27E-10	5.00
KFM09A	20051212 08:21	20051212 09:42	293.00	298.00	3	1	1.41E-09	0	1.16E-09	0	0	2.33E-10	5.00
KFM09A	20051221 12:39	20051221 13:28	296.00	301.00	3	1	2.04E-10	-1	1.68E-10	0	-1	3.36E-11	5.00
KFM09A	20051221 11:45	20051221 12:29	301.00	306.00	3	1	2.04E-10	-1	1.68E-10	0	-1	3.36E-11	5.00
KFM09A	20051212 09:58	20051212 10:39	306.00	311.00	3	1	3.25E-10	-1	2.67E-10	0	-1	5.35E-11	5.00
KFM09A	20051212 10:49	20051212 12:33	311.00	316.00	3	1	1.42E-10	-1	1.16E-10	0	-1	2.33E-11	5.00
KFM09A	20051212 12:43	20051212 13:31	316.00	321.00	3	1	2.04E-10	-1	1.67E-10	0	-1	3.35E-11	5.00
KFM09A	20051212 13:44	20051212 15:02	321.00	326.00	3	1	1.46E-08	0	1.20E-08	0	0	2.40E-09	5.00
KFM09A	20051212 15:31	20051212 16:14	346.00	351.00	3	1	3.27E-10	-1	2.69E-10	0	-1	5.37E-11	5.00
KFM09A	20051221 10:04	20051221 11:19	351.00	356.00	3	1	2.36E-09	0	1.94E-09	0	0	3.88E-10	5.00
KFM09A	20051221 08:54	20051221 09:50	356.00	361.00	3	1	2.04E-10	-1	1.67E-10	0	-1	3.35E-11	5.00
KFM09A	20051221 07:28	20051221 08:43	361.00	366.00	3	1	7.97E-10	0	6.56E-10	0	0	1.31E-10	5.00
KFM09A	20051212 16:39	20051212 17:54	363.00	368.00	3	1	5.99E-10	0	4.93E-10	0	0	9.86E-11	5.00
KFM09A	20051213 06:27	20051213 07:24	368.00	373.00	3	1	2.64E-10	-1	2.17E-10	0	-1	4.35E-11	5.00
KFM09A	20051213 07:35	20051213 08:48	371.00	376.00	3	1	7.16E-08	0	5.89E-08	0	0	1.18E-08	5.00
KFM09A	20051213 09:02	20051213 09:58	376.00	381.00	3	1	2.50E-10	-1	2.06E-10	0	-1	4.11E-11	5.00
KFM09A	20051213 10:10	20051213 11:25	381.00	386.00	3	1	2.64E-10	-1	2.17E-10	0	-1	4.34E-11	5.00
KFM09A	20051213 11:57	20051213 13:16	386.00	391.00	3	1	1.15E-07	0	9.43E-08	1	0	1.89E-08	5.00
KFM09A	20051213 13:28	20051213 14:48	391.00	396.00	3	1	7.87E-09	0	6.48E-09	0	0	1.30E-09	5.00
KFM09A	20051213 15:06	20051213 15:49	396.00	401.00	3	1	3.27E-10	-1	2.69E-10	0	-1	5.37E-11	5.00
KFM09A	20051213 16:00	20051213 17:15	401.00	406.00	3	1	2.07E-08	0	1.70E-08	0	0	3.41E-09	5.00
KFM09A	20051213 17:25	20051213 18:18	406.00	411.00	3	1	2.65E-10	-1	2.18E-10	0	-1	4.35E-11	5.00

idcode	start_date	stop_date	secup	seclow	test_type	formation_type	spec_capacity_q_s	value_type_q_s	transmissivity_moye	bc_tm	value_type_tm	hydr_cond_moye	formation_width_b
KFM09A	20051213 18:36	20051213 19:50	411.00	416.00	3	1	1.86E-08	0	1.53E-08	0	0	3.06E-09	5.00
KFM09A	20051213 20:06	20051213 21:22	414.00	419.00	3	1	6.59E-10	0	5.42E-10	0	0	1.08E-10	5.00
KFM09A	20051213 21:32	20051213 22:46	419.00	424.00	3	1	2.73E-09	0	2.25E-09	0	0	4.50E-10	5.00
KFM09A	20051213 22:55	20051214 00:09	421.00	426.00	3	1	2.93E-09	0	2.41E-09	0	0	4.82E-10	5.00
KFM09A	20051214 06:51	20051214 07:59	426.00	431.00	3	1	3.88E-10	-1	3.19E-10	0	-1	6.38E-11	5.00
KFM09A	20051214 08:11	20051214 09:31	431.00	436.00	3	1	7.09E-07	0	5.83E-07	1	0	1.17E-07	5.00
KFM09A	20051214 09:47	20051214 10:29	436.00	441.00	3	1	3.00E-10	-1	2.47E-10	0	-1	4.94E-11	5.00
KFM09A	20051214 10:44	20051214 12:00	441.00	446.00	3	1	9.04E-09	0	7.44E-09	1	0	1.49E-09	5.00
KFM09A	20051214 12:13	20051214 14:04	446.00	451.00	3	1	1.77E-09	0	1.46E-09	0	0	2.92E-10	5.00
KFM09A	20051214 14:22	20051214 15:38	451.00	456.00	3	1	6.35E-10	0	5.22E-10	1	0	1.04E-10	5.00
KFM09A	20051214 15:55	20051214 17:12	456.00	461.00	3	1	3.26E-09	0	2.69E-09	0	0	5.37E-10	5.00
KFM09A	20051214 17:32	20051214 18:15	461.00	466.00	3	1	1.42E-10	-1	1.16E-10	0	-1	2.33E-11	5.00
KFM09A	20051214 18:35	20051214 19:50	471.00	476.00	3	1	2.49E-09	0	2.04E-09	0	0	4.09E-10	5.00
KFM09A	20051214 20:01	20051214 21:23	476.00	481.00	3	1	2.21E-09	0	1.82E-09	0	0	3.64E-10	5.00
KFM09A	20051214 21:40	20051214 22:31	486.00	491.00	3	1	2.64E-10	-1	2.17E-10	0	-1	4.35E-11	5.00
KFM09A	20051214 22:58	20051215 00:12	491.00	496.00	3	1	3.86E-09	0	3.18E-09	0	0	6.35E-10	5.00
KFM09A	20051215 06:33	20051215 07:57	496.00	501.00	3	1	2.95E-09	0	2.43E-09	0	0	4.85E-10	5.00
KFM09A	20051215 08:14	20051215 09:00	501.00	506.00	3	1	2.50E-10	-1	2.06E-10	0	-1	4.11E-11	5.00
KFM09A	20051220 19:00	20051220 20:23	506.00	511.00	3	1	1.06E-09	0	8.76E-10	0	0	1.75E-10	5.00
KFM09A	20051220 20:50	20051220 22:05	511.00	516.00	3	1	1.44E-09	0	1.19E-09	0	0	2.37E-10	5.00
KFM09A	20051220 22:14	20051220 23:28	516.00	521.00	3	1	1.03E-09	0	8.43E-10	0	0	1.69E-10	5.00
KFM09A	20051215 09:25	20051215 10:11	521.00	526.00	3	1	2.64E-10	-1	2.17E-10	0	-1	4.35E-11	5.00
KFM09A	20051215 10:26	20051215 11:07	526.00	531.00	3	1	2.64E-10	-1	2.17E-10	0	-1	4.34E-11	5.00
KFM09A	20051215 11:23	20051215 12:44	531.00	536.00	3	1	1.32E-07	0	1.09E-07	1	0	2.17E-08	5.00
KFM09A	20051215 13:19	20051215 14:03	536.00	541.00	3	1	2.65E-10	-1	2.18E-10	0	-1	4.35E-11	5.00
KFM09A	20051215 14:14	20051215 15:28	541.00	546.00	3	1	4.36E-10	0	3.59E-10	0	0	7.18E-11	5.00
KFM09A	20051220 17:14	20051220 17:58	561.00	566.00	3	1	2.65E-10	-1	2.18E-10	0	-1	4.35E-11	5.00
KFM09A	20051215 16:19	20051215 17:00	606.00	611.00	3	1	2.04E-10	-1	1.68E-10	0	-1	3.36E-11	5.00
KFM09A	20051215 17:19	20051215 18:35	611.00	616.00	3	1	2.03E-08	0	1.67E-08	0	0	3.33E-09	5.00
KFM09A	20051215 18:50	20051215 19:31	616.00	621.00	3	1	2.65E-10	-1	2.18E-10	0	-1	4.35E-11	5.00
KFM09A	20051215 19:44	20051215 21:03	621.00	626.00	3	1	7.07E-09	0	5.82E-09	0	0	1.16E-09	5.00
KFM09A	20051215 21:14	20051215 22:01	626.00	631.00	3	1	2.04E-10	-1	1.67E-10	0	-1	3.35E-11	5.00
KFM09A	20051215 22:08	20051215 23:33	631.00	636.00	3	1	7.00E-10	0	5.76E-10	0	0	1.15E-10	5.00
KFM09A	20051215 23:43	20051216 00:58	636.00	641.00	3	1	6.96E-09	0	5.72E-09	0	0	1.14E-09	5.00

idcode	start_date	stop_date	secup	seclow	test_type	formation_type	spec_capacity_q_s	value_type_q_s	transmissivity_moye	bc_tm	value_type_tm	hydr_cond_moye	formation_width_b
KFM09A	20051216 08:21	20051216 09:36	641.00	646.00	3	1	6.92E-10	0	5.70E-10	0	0	1.14E-10	5.00
KFM09A	20051216 09:55	20051216 10:38	646.00	651.00	3	1	1.42E-10	-1	1.16E-10	0	-1	2.33E-11	5.00
KFM09A	20051216 10:53	20051216 12:10	651.00	656.00	3	1	6.35E-09	0	5.23E-09	0	0	1.05E-09	5.00
KFM09A	20051216 12:21	20051216 13:20	656.00	661.00	3	1	3.27E-10	-1	2.69E-10	0	-1	5.37E-11	5.00
KFM09A	20051216 13:31	20051216 14:14	661.00	666.00	3	1	2.04E-10	-1	1.68E-10	0	-1	3.36E-11	5.00
KFM09A	20051219 08:19	20051219 09:01	731.00	736.00	3	1	2.65E-10	-1	2.18E-10	0	-1	4.35E-11	5.00
KFM09A	20051219 09:15	20051219 09:56	736.00	741.00	3	1	2.65E-10	-1	2.18E-10	0	-1	4.35E-11	5.00
KFM09A	20051219 10:11	20051219 11:30	741.00	746.00	3	1	4.41E-09	0	3.63E-09	0	0	7.26E-10	5.00
KFM09A	20051219 11:44	20051219 12:36	746.00	751.00	3	1	2.65E-10	-1	2.18E-10	0	-1	4.35E-11	5.00
KFM09A	20051219 12:50	20051219 14:05	751.00	756.00	3	1	4.20E-09	0	3.45E-09	0	0	6.91E-10	5.00
KFM09A	20051219 14:20	20051219 15:42	756.00	761.00	3	1	1.03E-08	0	8.44E-09	0	0	1.69E-09	5.00
KFM09A	20051219 15:56	20051219 17:16	761.00	766.00	3	1	5.25E-09	0	4.32E-09	0	0	8.63E-10	5.00
KFM09A	20051220 06:55	20051220 08:10	766.00	771.00	3	1	2.82E-09	0	2.32E-09	0	0	4.64E-10	5.00
KFM09A	20051220 08:29	20051220 09:46	771.00	776.00	3	1	2.53E-09	0	2.08E-09	0	0	4.16E-10	5.00
KFM09A	20051220 10:06	20051220 11:24	776.00	781.00	3	1	5.95E-09	0	4.90E-09	0	0	9.80E-10	5.00
KFM09A	20051220 11:35	20051220 12:58	781.00	786.00	3	1	1.05E-08	0	8.62E-09	0	0	1.72E-09	5.00
KFM09A	20051220 13:11	20051220 14:28	786.00	791.00	3	1	3.41E-08	0	2.81E-08	0	0	5.61E-09	5.00
KFM09A	20051118 13:32	20051118 14:28	506.00 [1)]	606.00	3	1							100.00
KFM09A	20051130 17:10	20051130 18:03	426.00 [1)]	446.00	3	1							20.00
KFM09A	20051207 10:38	20051207 12:39	116.00 [1)]	121.00	3	1							5.00

[1)] Incomplete test, interrupted and re-performed later.

KFM09A plu_s_hole_test_ed1. Right (This result table to SICADA includes more columns which are empty, these columns are not presented here.)

idcode	secup	seclow	transmissivity_tt	value_type_tt	bc_tt	l_measl_q_s	u_measl_q_s	assumed_s	bc_s	ri	ri_index	c	skin	t1	t2	dte1	dte2
KFM09A	106.00	206.00	4.56E-07	0	1	8.9E-10	5.0E-04	4.73E-07	4.73E-07	62.84	-1		-6.79				
KFM09A	206.00	306.00	4.19E-08	0	1	7.5E-10	5.0E-04	1.43E-07	1.43E-07	34.41	0		-2.54	150	1800		
KFM09A	306.00	406.00	1.29E-07	0	1	7.8E-10	5.0E-04	2.51E-07	2.51E-07	45.55	1		-5.13				
KFM09A	406.00	506.00	1.14E-06	0	0	8.0E-10	5.0E-04	5.75E-07	5.75E-07	69.31	1		-5.76				
KFM09A	506.00	606.00	3.17E-07	0	0	7.4E-10	5.0E-04	2.35E-07	2.35E-07	44.31	1		-5.12				
KFM09A	606.00	706.00	1.64E-08	0	1	8.0E-10	5.0E-04	8.95E-08	8.95E-08	12.82	1	3.24E-10	-3.54	20	400		
KFM09A	691.00	791.00	6.92E-09	0	1	9.3E-10	5.0E-04	5.82E-08	5.82E-08	22.07	-1		-5.60				
KFM09A	106.00	126.00	2.51E-07	0	1	7.7E-10	5.0E-04	3.51E-07	3.51E-07	43.97	0		-3.14	100	1200		
KFM09A	126.00	146.00	5.35E-07	0	1	7.6E-10	5.0E-04	5.12E-07	5.12E-07	53.12	0		-4.71	550	1200		
KFM09A	146.00	166.00	4.22E-08	0	1	8.9E-10	5.0E-04	1.44E-07	1.44E-07	28.35	0						
KFM09A	166.00	186.00	6.19E-07	0	1	8.6E-10	5.0E-04	5.51E-07	5.51E-07	55.49	-1		-5.02				
KFM09A	186.00	206.00	3.28E-09	0	1	5.5E-10	5.0E-04	4.01E-08	4.01E-08	14.99	-1	5.75E-11	-1.13				
KFM09A	206.00	226.00		-1	0	2.6E-10	5.0E-04										
KFM09A	226.00	246.00	4.65E-08	0	1	7.9E-10	5.0E-04	1.51E-07	1.51E-07	28.85	0		-0.24	300	1200		
KFM09A	238.00	258.00	4.90E-09	0	1	7.8E-10	5.0E-04	4.90E-08	4.90E-08	16.43	0	5.01E-10	-3.44	200	1200		
KFM09A	258.00	278.00	1.46E-09	0	1	8.0E-10	5.0E-04	2.68E-08	2.68E-08	12.12	0	7.53E-11	-3.09				
KFM09A	278.00	298.00	2.59E-09	0	1	7.7E-10	5.0E-04	3.56E-08	3.56E-08	7.01	0		-3.42	10	300		
KFM09A	286.00	306.00	1.39E-09	0	1	7.7E-10	5.0E-04	2.61E-08	2.61E-08	11.95	-1		-3.56				
KFM09A	306.00	326.00	3.12E-08	0	1	8.2E-10	5.0E-04	1.24E-07	1.24E-07	7.53	1		-2.23	20	100		
KFM09A	326.00	346.00	4.17E-10	0	1	8.1E-10	5.0E-04	1.43E-08	1.43E-08	8.87	0		-3.21	30	1200		
KFM09A	346.00	366.00	7.25E-10	0	1	8.0E-10	5.0E-04	1.88E-08	1.88E-08	10.19	0	5.57E-11	-3.71	300	1200		
KFM09A	366.00	386.00	2.44E-08	0	1	8.1E-10	5.0E-04	1.09E-07	1.09E-07	24.54	0		-4.23	200	1200		
KFM09A	386.00	406.00	4.53E-08	0	0	8.2E-10	5.0E-04	2.60E-07	2.60E-07	38.40	1		-6.01				
KFM09A	406.00	426.00	2.31E-08	0	0	8.2E-10	5.0E-04	1.00E-07	1.00E-07	23.85	1		-1.36				
KFM09A	426.00	446.00	1.26E-06	0	0	7.4E-10	5.0E-04	6.49E-07	6.49E-07	60.65	1		-5.73				
KFM09A	446.00	466.00	1.97E-09	0	1	7.1E-10	5.0E-04	3.11E-08	3.11E-08	13.08	0		-1.90	200	1200		
KFM09A	466.00	486.00	1.86E-09	0	1	9.5E-10	5.0E-04	3.02E-08	3.02E-08	8.32	1		-2.90			100	500

idcode	secup	seclow	transmissivity_tt	value_type_tt	bc_tt	l_measl_q_s	u_measl_q_s	assumed_s	bc_s	ri	ri_index	c	skin	t1	t2	dte1	dte2
KFM09A	486.00	506.00	1.00E-09	0	1	8.0E-10	5.0E-04	2.21E-08	2.21E-08	11.14	1						
KFM09A	506.00	526.00	2.06E-10	0	1	8.6E-10	5.0E-04	1.00E-08	1.00E-08	7.44	0		-5.47				
KFM09A	526.00	546.00	4.12E-07	0	0	8.0E-10	5.0E-04	2.67E-07	2.67E-07	38.65	0		-4.72			100	1400
KFM09A	545.00	565.00		-1	0	2.6E-10	5.0E-04										
KFM09A	566.00	586.00		-1	0	2.6E-10	5.0E-04										
KFM09A	586.00	606.00		-1	0	2.6E-10	5.0E-04										
KFM09A	606.00	626.00	1.28E-08	0	1	8.2E-10	5.0E-04	7.92E-08	7.92E-08	10.44	1		-3.99	50	300		
KFM09A	626.00	646.00	2.70E-09	0	1	7.9E-10	5.0E-04	3.64E-08	3.64E-08	14.16	-1	7.25E-11	-1.83				
KFM09A	646.00	666.00	4.21E-09	0	1	8.0E-10	5.0E-04	4.54E-08	4.54E-08	15.82	0		-0.94	50	1200		
KFM09A	666.00	686.00	2.40E-11	0	0	2.8E-10	5.0E-04	1.83E-08	1.83E-08	10.05	1		-6.35				
KFM09A	686.00	706.00	9.24E-11	0	1	2.6E-10	5.0E-04	6.73E-09	6.73E-09	6.10	1						
KFM09A	691.00	711.00		-1	0	1.9E-10	5.0E-04										
KFM09A	711.00	731.00		-1	0	1.9E-10	5.0E-04										
KFM09A	731.00	751.00	3.41E-09	0	1	7.7E-10	5.0E-04	4.09E-08	4.09E-08	15.03	-1	6.28E-11	0.71				
KFM09A	751.00	771.00	3.50E-09	0	1	8.0E-10	5.0E-04	4.14E-08	4.14E-08	15.22	1		-5.20				
KFM09A	771.00	791.00	6.54E-09	0	1	7.6E-10	5.0E-04	5.66E-08	5.66E-08	17.81	-1	1.41E-09	-5.10				
KFM09A	106.00	111.00	1.32E-08	0	1	8.1E-10	5.0E-04	8.04E-08	8.04E-08	21.26	-1		-2.89				
KFM09A	111.00	116.00	1.04E-09	0	1	7.9E-10	5.0E-04	2.26E-08	2.26E-08	11.26	-1		-3.22				
KFM09A	116.00	121.00	4.25E-08	0	1	8.2E-10	5.0E-04	1.44E-07	1.44E-07	16.28	0		-4.44	50	400		
KFM09A	121.00	126.00	1.69E-07	0	1	9.2E-10	5.0E-04	2.88E-07	2.88E-07	21.51	0		-3.66	80	350		
KFM09A	126.00	131.00	6.83E-10	0	1	8.1E-10	5.0E-04	1.83E-08	1.83E-08	10.02	1						
KFM09A	128.00	133.00	2.69E-07	0	1	7.5E-10	5.0E-04	3.63E-07	3.63E-07	45.08	-1		-4.87				
KFM09A	133.00	138.00	2.10E-07	0	1	7.0E-10	5.0E-04	3.21E-07	3.21E-07	41.99	0		-4.48				
KFM09A	138.00	143.00	8.19E-09	0	1	8.1E-10	5.0E-04	6.33E-08	6.33E-08	18.68	0		-2.86	100	1200		
KFM09A	141.00	146.00	2.77E-08	0	1	7.3E-10	5.0E-04	1.16E-07	1.16E-07	25.58	0		-3.50				
KFM09A	146.00	151.00	7.80E-09	0	1	7.2E-10	5.0E-04	6.18E-08	6.18E-08	18.36	1						
KFM09A	151.00	156.00		-1	0	2.6E-10	5.0E-04										
KFM09A	156.00	161.00	3.44E-08	0	1	7.9E-10	5.0E-04	1.30E-07	1.30E-07	26.90	0						
KFM09A	161.00	166.00	4.85E-09	0	0	9.2E-10	5.0E-04	4.75E-08	4.75E-08	16.31	-1		0.00				
KFM09A	166.00	171.00	1.13E-06	0	1	9.1E-10	5.0E-04	7.44E-07	7.44E-07	64.48	-1		-3.98				
KFM09A	171.00	176.00		0	0	7.9E-10	5.0E-04	3.25E-08	3.25E-08	13.46							

idcode	secup	seclow	transmissivity_tt	value_type_tt	bc_tt	l_measl_q_s	u_measl_q_s	assumed_s	bc_s	ri	ri_index	c	skin	t1	t2	dte1	dte2
KFM09A	176.00	181.00	4.78E-09	0	1	8.2E-10	5.0E-04	4.84E-08	4.84E-08	16.33	0	7.41E-11	-3.96	50	1200		
KFM09A	181.00	186.00		0	0	7.2E-10	5.0E-04	6.58E-08	6.58E-08	19.20							
KFM09A	186.00	191.00	4.58E-09	0	1	7.6E-10	5.0E-04	4.74E-08	4.74E-08	16.16	0	2.51E-11	-0.92	40	1200		
KFM09A	191.00	196.00		-1	0	2.6E-10	5.0E-04										
KFM09A	196.00	201.00		-1	0	2.0E-10	5.0E-04										
KFM09A	201.00	206.00		-1	0	2.6E-10	5.0E-04										
KFM09A	226.00	231.00		-1	0	2.6E-10	5.0E-04										
KFM09A	232.00	237.00	6.48E-08	0	1	8.2E-10	5.0E-04	1.78E-07	1.78E-07	31.56	-1		3.62				
KFM09A	237.00	242.00	7.88E-08	0	1	8.2E-10	5.0E-04	1.96E-07	1.96E-07	32.90	0		-0.90	50	1200		
KFM09A	240.80	245.80	4.95E-09	0	1	8.0E-10	5.0E-04	4.92E-08	4.92E-08	16.60	-1		-3.88				
KFM09A	246.80	251.80		-1	0	2.0E-10	5.0E-04										
KFM09A	251.50	256.50		-1	0	2.6E-10	5.0E-04										
KFM09A	256.50	261.50		-1	0	3.3E-10	5.0E-04										
KFM09A	273.00	278.00	2.00E-09	0	1	7.0E-10	5.0E-04	3.13E-08	3.13E-08	5.36	0	3.85E-11	-2.81	30	200		
KFM09A	278.00	283.00	1.47E-09	0	1	7.9E-10	5.0E-04	2.68E-08	2.68E-08	7.84	1		-4.20	60	500		
KFM09A	283.00	288.00		-1	0	2.6E-10	5.0E-04										
KFM09A	288.00	293.00	6.90E-11	0	0	4.9E-10	5.0E-04	1.76E-08	1.76E-08	9.95	0	1.73E-11	-5.42				
KFM09A	293.00	298.00	6.79E-10	0	1	7.0E-10	5.0E-04	1.82E-08	1.82E-08	10.02	0	1.72E-11	-2.68	10	1200		
KFM09A	296.00	301.00		-1	0	2.0E-10	5.0E-04										
KFM09A	301.00	306.00		-1	0	2.0E-10	5.0E-04										
KFM09A	306.00	311.00		-1	0	3.3E-10	5.0E-04										
KFM09A	311.00	316.00		-1	0	1.4E-10	5.0E-04										
KFM09A	316.00	321.00		-1	0	2.0E-10	5.0E-04										
KFM09A	321.00	326.00	2.01E-08	0	1	8.1E-10	5.0E-04	9.92E-08	9.92E-08	9.54	1		-3.28	30	200		
KFM09A	346.00	351.00		-1	0	3.3E-10	5.0E-04										
KFM09A	351.00	356.00	1.42E-09	0	1	7.8E-10	5.0E-04	2.63E-08	2.63E-08	12.05	0	1.74E-11	-1.68	30	1200		
KFM09A	356.00	361.00		-1	0	2.0E-10	5.0E-04										
KFM09A	361.00	366.00	2.32E-10	0	1	1.9E-10	5.0E-04	1.07E-08	1.07E-08	7.67	0		-2.96	20	1200		
KFM09A	363.00	368.00	2.32E-10	0	1	2.5E-10	5.0E-04	1.07E-08	1.07E-08	7.66	0	1.84E-11	-2.93	30	1200		
KFM09A	368.00	373.00		-1	0	2.6E-10	5.0E-04										
KFM09A	371.00	376.00	3.05E-08	0	1	8.1E-10	5.0E-04	1.22E-07	1.22E-07	18.36	0		-5.05	100	600		
KFM09A	376.00	381.00		-1	0	2.5E-10	5.0E-04										

idcode	secup	seclow	transmissivity_tt	value_type_tt	bc_tt	l_measl_q_s	u_measl_q_s	assumed_s	bc_s	ri	ri_index	c	skin	t1	t2	dte1	dte2
KFM09A	381.00	386.00		-1	0	2.6E-10	5.0E-04										
KFM09A	386.00	391.00	8.27E-08	0	0	7.7E-10	5.0E-04	2.15E-07	2.15E-07	34.73	1						
KFM09A	391.00	396.00	1.42E-09	0	1	7.9E-10	5.0E-04	2.64E-08	2.64E-08	6.03	-1		-4.46	20	300		
KFM09A	396.00	401.00		-1	0	3.3E-10	5.0E-04										
KFM09A	401.00	406.00	2.04E-08	0	1	8.1E-10	5.0E-04	1.00E-07	1.00E-07	10.71	1	1.30E-10	-0.66	100	250		
KFM09A	406.00	411.00		-1	0	2.6E-10	5.0E-04										
KFM09A	411.00	416.00	2.37E-08	0	1	8.4E-10	5.0E-04	1.08E-07	1.08E-07	7.03	0		-1.98	20	100		
KFM09A	414.00	419.00	3.17E-10	0	1	2.7E-10	5.0E-04	1.25E-08	1.25E-08	8.29	0		-1.85	30	1200		
KFM09A	419.00	424.00	1.95E-09	0	1	8.0E-10	5.0E-04	3.09E-08	3.09E-08	9.23	0	1.61E-11	-1.79	30	600		
KFM09A	421.00	426.00	1.68E-09	0	1	8.5E-10	5.0E-04	2.87E-08	2.87E-08	12.57	0	1.90E-11	-2.50	20	1200		
KFM09A	426.00	431.00		-1	0	3.9E-10	5.0E-04										
KFM09A	431.00	436.00	1.51E-06	0	0	7.3E-10	5.0E-04	5.35E-07	5.35E-07	54.77	1		-5.47				
KFM09A	436.00	441.00		-1	0	3.0E-10	5.0E-04										
KFM09A	441.00	446.00	4.01E-08	0	0	7.2E-10	5.0E-04	6.04E-08	6.04E-08	18.44	1		-6.42				
KFM09A	446.00	451.00	8.19E-10	0	1	7.9E-10	5.0E-04	2.00E-08	2.00E-08	10.51	1		-6.02				
KFM09A	451.00	456.00	1.57E-10	0	0	2.7E-10	5.0E-04	1.60E-08	1.60E-08	9.49	0		-3.30				
KFM09A	456.00	461.00	2.00E-09	0	1	8.1E-10	5.0E-04	3.13E-08	3.13E-08	9.29	1		-1.04	20	600		
KFM09A	461.00	466.00		-1	0	1.4E-10	5.0E-04										
KFM09A	471.00	476.00	2.93E-10	0	1	7.8E-10	5.0E-04	1.20E-08	1.20E-08	8.22	-1		-5.33				
KFM09A	476.00	481.00	1.65E-09	0	1	8.6E-10	5.0E-04	2.84E-08	2.84E-08	3.61	1		-1.97	20	100		
KFM09A	486.00	491.00		-1	0	2.6E-10	5.0E-04										
KFM09A	491.00	496.00	1.58E-09	0	1	8.2E-10	5.0E-04	2.78E-08	2.78E-08	12.38	0	7.15E-11	-3.36	60	1200		
KFM09A	496.00	501.00	2.97E-10	0	1	7.9E-10	5.0E-04	1.21E-08	1.21E-08	8.15	1						
KFM09A	501.00	506.00		-1	0	2.5E-10	5.0E-04										
KFM09A	506.00	511.00	4.79E-10	0	1	2.6E-10	5.0E-04	1.53E-08	1.53E-08	9.28	-1		0.00				
KFM09A	511.00	516.00	4.65E-10	0	1	8.1E-10	5.0E-04	1.51E-08	1.51E-08	9.19	-1		-1.98				
KFM09A	516.00	521.00	2.41E-10	0	1	4.1E-10	5.0E-04	1.09E-08	1.09E-08	7.81	0	1.56E-11	-3.69				
KFM09A	521.00	526.00		-1	0	2.6E-10	5.0E-04										
KFM09A	526.00	531.00		-1	0	2.6E-10	5.0E-04										
KFM09A	531.00	536.00	4.23E-07	0	0	7.6E-10	5.0E-04	2.31E-07	2.31E-07	35.98	1		-4.75			100	5000
KFM09A	536.00	541.00		-1	0	2.6E-10	5.0E-04										
KFM09A	541.00	546.00	3.09E-09	0	1	2.7E-10	5.0E-04	3.89E-08	3.89E-08	2.99	1		-3.26	10	50		

idcode	secup	seclow	transmissivity_tt	value_type_tt	bc_tt	l_measl_q_s	u_measl_q_s	assumed_s	bc_s	ri	ri_index	c	skin	t1	t2	dte1	dte2
KFM09A	561.00	566.00		-1	0	2.6E-10	5.0E-04										
KFM09A	606.00	611.00		-1	0	2.0E-10	5.0E-04										
KFM09A	611.00	616.00	1.56E-08	0	1	8.5E-10	5.0E-04	8.75E-08	8.75E-08	8.96	1		-3.50	30	200		
KFM09A	616.00	621.00		-1	0	2.6E-10	5.0E-04										
KFM09A	621.00	626.00	2.38E-09	0	1	7.7E-10	5.0E-04	3.41E-08	3.41E-08	7.92	1		-4.28	40	400		
KFM09A	626.00	631.00		-1	0	2.0E-10	5.0E-04										
KFM09A	631.00	636.00	2.58E-10	0	1	3.2E-10	5.0E-04	1.12E-08	1.12E-08	2.27	1	1.71E-11	-3.98	30	100		
KFM09A	636.00	641.00	6.19E-09	0	1	8.6E-10	5.0E-04	5.51E-08	5.51E-08	17.42	0	2.64E-11	0.08	20	1200		
KFM09A	641.00	646.00	9.03E-11	0	1	1.5E-10	5.0E-04	6.65E-09	6.65E-09	6.11	0		-4.31				
KFM09A	646.00	651.00		-1	0	1.4E-10	5.0E-04										
KFM09A	651.00	656.00	3.71E-09	0	1	8.4E-10	5.0E-04	4.26E-08	4.26E-08	15.33	0		-2.52	40	1200		
KFM09A	656.00	661.00		-1	0	3.3E-10	5.0E-04										
KFM09A	661.00	666.00															
KFM09A	731.00	736.00		-1	0	2.6E-10	5.0E-04										
KFM09A	736.00	741.00		-1	0	2.6E-10	5.0E-04										
KFM09A	741.00	746.00	2.75E-09	0	1	8.3E-10	5.0E-04	3.67E-08	3.67E-08	7.11	0	1.92E-11	-0.91	40	300		
KFM09A	746.00	751.00		-1	0	2.6E-10	5.0E-04										
KFM09A	751.00	756.00	1.04E-09	0	1	8.8E-10	5.0E-04	2.26E-08	2.26E-08	8.51	-1			200	700		
KFM09A	756.00	761.00	5.14E-09	0	1	7.9E-10	5.0E-04	5.02E-08	5.02E-08	16.63	0		-3.58	70	1200		
KFM09A	761.00	766.00	7.00E-10	0	1	8.1E-10	5.0E-04	1.85E-08	1.85E-08	10.23	-1		-5.02				
KFM09A	766.00	771.00	7.66E-10	0	1	8.6E-10	5.0E-04	1.94E-08	1.94E-08	10.43	-1	7.66E-11	-3.86				
KFM09A	771.00	776.00	6.84E-10	0	1	7.0E-10	5.0E-04	1.83E-08	1.83E-08	10.15	-1		-3.54				
KFM09A	776.00	781.00	1.88E-09	0	1	8.6E-10	5.0E-04	3.04E-08	3.04E-08	12.93	0	7.00E-11	-3.69	100	1200		
KFM09A	781.00	786.00	6.16E-10	0	1	9.4E-10	5.0E-04	1.74E-08	1.74E-08	9.89	-1		-5.89				
KFM09A	786.00	791.00	6.36E-09	0	1	8.0E-10	5.0E-04	5.58E-08	5.58E-08	17.71	0	6.30E-10	-4.52				

KFM09A plu_s_hole_test_obs (This result table to SICADA includes more columns which are empty, these columns are not presented here.)

idcode	start_date	stop_date	secup	seclow	obs_secup	obs_seclow	pi_above	pp_above	pf_above	pi_below	pp_below	pf_below	comments
KFM09A	20051117 16:09	20051117 17:59	106.00	206.00	7.79	105.00	938.78	938.36	938.36				
KFM09A	20051117 16:09	20051117 17:59	106.00	206.00	207.00	799.67				1792.58	1793.95	1794.77	
KFM09A	20051117 19:03	20051117 20:53	206.00	306.00	7.79	205.00	944.46	943.92	943.92				
KFM09A	20051117 19:03	20051117 20:53	206.00	306.00	307.00	799.67				2608.72	2610.37	2611.60	
KFM09A	20051117 21:47	20051117 23:36	306.00	406.00	7.79	305.00	910.90	910.90	910.36				
KFM09A	20051117 21:47	20051117 23:36	306.00	406.00	407.00	799.67				3403.22	3405.41	3407.06	
KFM09A	20051118 09:59	20051118 11:49	406.00	506.00	7.79	405.00	858.19	857.91	858.05				
KFM09A	20051118 09:59	20051118 11:49	406.00	506.00	507.00	799.67				4184.43	4188.82	4191.57	
KFM09A	20051121 12:52	20051121 15:13	506.00	606.00	7.79	505.00	818.01	815.81	821.72				
KFM09A	20051121 12:52	20051121 15:13	506.00	606.00	607.00	799.67				4947.58	4948.68	4949.22	
KFM09A	20051121 06:14	20051121 08:03	606.00	706.00	7.79	605.00	693.26	692.84	692.84				
KFM09A	20051121 06:14	20051121 08:03	606.00	706.00	707.00	799.67				5659.22	5661.27	5662.50	
KFM09A	20051121 08:51	20051121 10:40	691.00	791.00	7.79	690.00	586.37	585.41	599.74				
KFM09A	20051121 08:51	20051121 10:40	691.00	791.00	792.00	799.67				6238.42	6243.76	6242.12	
KFM09A	20051128 16:44	20051128 18:19	106.00	126.00	7.79	105.00	943.46	943.32	943.32				
KFM09A	20051128 16:44	20051128 18:19	106.00	126.00	127.00	799.67				1128.14	1129.23	1129.23	
KFM09A	20051129 06:29	20051129 07:43	126.00	146.00	7.79	125.00	961.18	964.76	961.18				
KFM09A	20051129 06:29	20051129 07:43	126.00	146.00	147.00	799.67				1299.06	1299.61	1298.52	
KFM09A	20051129 08:20	20051129 09:35	146.00	166.00	7.79	145.00	958.79	962.51	960.86				
KFM09A	20051129 08:20	20051129 09:35	146.00	166.00	167.00	799.67				1463.96	1464.92	1463.96	
KFM09A	20051129 10:00	20051129 11:15	166.00	186.00	7.79	165.00	954.47	957.78	953.91				
KFM09A	20051129 10:00	20051129 11:15	166.00	186.00	187.00	799.67				1633.25	1633.79	1633.79	
KFM09A	20051129 12:14	20051129 13:31	186.00	206.00	7.79	185.00	948.78	953.60	951.95				
KFM09A	20051129 12:14	20051129 13:31	186.00	206.00	207.00	799.67				1798.01	1798.56	1799.24	
KFM09A	20051129 14:01	20051129 14:47	206.00	226.00	7.79	205.00	947.77	948.33	949.42				
KFM09A	20051129 14:01	20051129 14:47	206.00	226.00	227.00	799.67				1963.32	1963.59	1963.59	

idcode	start_date	stop_date	secup	seclow	obs_secup	obs_seclow	pi_above	pp_above	pf_above	pi_below	pp_below	pf_below	comments
KFM09A	20051129 15:38	20051129 16:56	226.00	246.00	7.79	225.00	938.22	943.45	940.29				
KFM09A	20051129 15:38	20051129 16:56	226.00	246.00	247.00	799.67				2128.49	2129.03	2129.59	
KFM09A	20051129 17:18	20051129 18:37	238.00	258.00	7.79	237.00	934.81	934.39	937.01				
KFM09A	20051129 17:18	20051129 18:37	238.00	258.00	259.00	799.67				2226.01	2226.82	2227.10	
KFM09A	20051129 18:58	20051129 20:17	258.00	278.00	7.79	257.00	933.38	929.52	930.62				
KFM09A	20051129 18:58	20051129 20:17	258.00	278.00	279.00	799.67				2389.81	2390.36	2390.91	
KFM09A	20051129 21:03	20051129 22:25	278.00	298.00	7.79	277.00	927.00	925.89	922.04				
KFM09A	20051129 21:03	20051129 22:25	278.00	298.00	299.00	799.67				2549.77	2550.87	2551.42	
KFM09A	20051129 22:41	20051129 23:57	286.00	306.00	7.79	285.00	921.14	919.49	921.14				
KFM09A	20051129 22:41	20051129 23:57	286.00	306.00	307.00	799.67				2611.00	2612.23	2613.33	
KFM09A	20051130 06:29	20051130 07:48	306.00	326.00	7.79	305.00	914.76	916.00	914.21				
KFM09A	20051130 06:29	20051130 07:48	306.00	326.00	327.00	799.67				2774.38	2774.38	2774.94	
KFM09A	20051130 08:16	20051130 09:35	326.00	346.00	7.79	325.00	903.28	903.97	905.07				
KFM09A	20051130 08:16	20051130 09:35	326.00	346.00	347.00	799.67				2932.72	2933.27	2933.81	
KFM09A	20051130 10:06	20051130 11:22	346.00	366.00	7.79	345.00	895.93	894.56	897.03				
KFM09A	20051130 10:06	20051130 11:22	346.00	366.00	367.00	799.67				3093.23	3093.78	3093.78	
KFM09A	20051130 12:06	20051130 13:23	366.00	386.00	7.79	365.00	883.49	886.79	888.44				
KFM09A	20051130 12:06	20051130 13:23	366.00	386.00	387.00	799.67				3250.46	3251.42	3252.11	
KFM09A	20051130 13:50	20051130 15:08	386.00	406.00	7.79	385.00	872.14	873.66	873.80				
KFM09A	20051130 13:50	20051130 15:08	386.00	406.00	407.00	799.67				3407.28	3408.78	3409.33	
KFM09A	20051130 15:30	20051130 16:47	406.00	426.00	7.79	405.00	865.21	864.11	865.21				
KFM09A	20051130 15:30	20051130 16:47	406.00	426.00	427.00	799.67				3564.37	3565.47	3566.56	
KFM09A	20051130 18:18	20051130 19:38	426.00	446.00	7.79	425.00	852.77	854.83	853.87				
KFM09A	20051130 18:18	20051130 19:38	426.00	446.00	447.00	799.67				3730.38	3732.01	3732.57	
KFM09A	20051130 20:03	20051130 21:45	446.00	466.00	7.79	445.00	840.32	842.80	836.47				
KFM09A	20051130 20:03	20051130 21:45	446.00	466.00	467.00	799.67				3887.60	3888.28	3888.69	
KFM09A	20051130 22:03	20051130 23:20	466.00	486.00	7.79	465.00	825.13	824.58	827.33				
KFM09A	20051130 22:03	20051130 23:20	466.00	486.00	487.00	799.67				4036.74	4038.80	4040.45	
KFM09A	20051201 08:06	20051201 09:34	486.00	506.00	7.79	485.00	813.24	813.93	811.59				
KFM09A	20051201 08:06	20051201 09:34	486.00	506.00	507.00	799.67				4187.67	4189.46	4190.55	
KFM09A	20051201 10:01	20051201 11:22	506.00	526.00	7.79	505.00	794.46	797.48	798.04				
KFM09A	20051201 10:01	20051201 11:22	506.00	526.00	527.00	799.67				4340.66	4342.17	4343.40	

idcode	start_date	stop_date	secup	seclow	obs_secup	obs_seclow	pi_above	pp_above	pf_above	pi_below	pp_below	pf_below	comments
KFM09A	20051201 11:41	20051201 13:46	526.00	546.00	7.79	525.00	776.23	775.68	775.68				
KFM09A	20051201 11:41	20051201 13:46	526.00	546.00	547.00	799.67				4497.61	4497.88	4498.44	
KFM09A	20051201 14:21	20051201 15:09	545.00	565.00	7.79	544.00	843.61	843.06	842.92				
KFM09A	20051201 14:21	20051201 15:09	545.00	565.00	566.00	799.67				4637.86	4638.13	4638.13	
KFM09A	20051201 15:34	20051201 16:17	566.00	586.00	7.79	565.00	823.27	823.14	823.14				
KFM09A	20051201 15:34	20051201 16:17	566.00	586.00	587.00	799.67				4793.72	4793.72	4794.27	
KFM09A	20051202 07:55	20051202 08:37	586.00	606.00	7.79	585.00	802.83	802.56	802.42				
KFM09A	20051202 07:55	20051202 08:37	586.00	606.00	607.00	799.67				4940.00	4940.00	4940.54	
KFM09A	20051202 08:58	20051202 10:22	606.00	626.00	7.79	605.00	782.13	781.72	782.27				
KFM09A	20051202 08:58	20051202 10:22	606.00	626.00	627.00	799.67				5089.54	5090.10	5090.64	
KFM09A	20051202 10:43	20051202 12:05	626.00	646.00	7.79	625.00	676.40	675.72	675.99				
KFM09A	20051202 10:43	20051202 12:05	626.00	646.00	647.00	799.67				5235.55	5236.37	5236.93	
KFM09A	20051202 13:12	20051202 14:35	646.00	666.00	7.79	645.00	738.51	737.54	738.10				
KFM09A	20051202 13:12	20051202 14:35	646.00	666.00	667.00	799.67				5379.90	5381.00	5381.55	
KFM09A	20051202 14:57	20051202 16:13	666.00	686.00	7.79	665.00	629.20	628.93	628.51				
KFM09A	20051202 14:57	20051202 16:13	666.00	686.00	687.00	799.67				5521.80	5522.48	5522.89	
KFM09A	20051205 08:22	20051205 09:53	686.00	706.00	7.79	685.00	690.62	692.27	693.92				
KFM09A	20051205 08:22	20051205 09:53	686.00	706.00	707.00	799.67				5660.53	5661.22	5661.49	
KFM09A	20051205 10:10	20051205 11:12	691.00	711.00	7.79	690.00	601.52	600.28	601.38				
KFM09A	20051205 10:10	20051205 11:12	691.00	711.00	712.00	799.67				5695.46	5696.01	5696.01	
KFM09A	20051205 12:46	20051205 13:30	711.00	731.00	7.79	710.00	573.37	572.97	571.87				
KFM09A	20051205 12:46	20051205 13:30	711.00	731.00	732.00	799.67				5832.14	5832.56	5832.42	
KFM09A	20051205 13:49	20051205 15:12	731.00	751.00	7.79	730.00	542.48	542.89	538.49				
KFM09A	20051205 13:49	20051205 15:12	731.00	751.00	752.00	799.67				5968.29	5968.56	5968.83	
KFM09A	20051205 15:30	20051205 16:54	751.00	771.00	7.79	750.00	507.99	507.85	508.41				
KFM09A	20051205 15:30	20051205 16:54	751.00	771.00	772.00	799.67				6104.56	6104.70	6105.24	
KFM09A	20051205 18:09	20051205 19:26	771.00	791.00	7.79	770.00	475.99	476.68	477.78				
KFM09A	20051205 18:09	20051205 19:26	771.00	791.00	792.00	799.67				6234.67	6240.97	6238.92	
KFM09A	20051207 07:32	20051207 08:52	106.00	111.00	7.79	105.00	971.33	973.12	970.79				
KFM09A	20051207 07:32	20051207 08:52	106.00	111.00	112.00	799.67				1005.56	1004.74	1004.87	

idcode	start_date	stop_date	secup	seclow	obs_secup	obs_seclow	pi_above	pp_above	pf_above	pi_below	pp_below	pf_below	comments
KFM09A	20051207 09:08	20051207 10:24	111.00	116.00	7.79	110.00	967.12	971.94	972.08				
KFM09A	20051207 09:08	20051207 10:24	111.00	116.00	117.00	799.67				1047.60	1046.51	1045.41	
KFM09A	20051221 15:48	20051208 17:51	116.00	121.00	7.79	115.00	964.65	964.65	964.65				
KFM09A	20051221 15:48	20051208 17:51	116.00	121.00	122.00	799.67				1078.83	1079.93	1080.48	
KFM09A	20051207 12:52	20051207 14:09	121.00	126.00	7.79	120.00	966.41	970.82	969.72				
KFM09A	20051207 12:52	20051207 14:09	121.00	126.00	127.00	799.67				1131.42	1131.42	1130.87	
KFM09A	20051207 14:26	20051207 16:04	126.00	131.00	7.79	125.00	968.12	965.50	967.15				
KFM09A	20051207 14:26	20051207 16:04	126.00	131.00	132.00	799.67				1172.51	1173.06	1172.51	
KFM09A	20051207 16:21	20051207 17:40	128.00	133.00	7.79	127.00	969.68	969.00	969.54				
KFM09A	20051207 16:21	20051207 17:40	128.00	133.00	134.00	799.67				1189.09	1194.43	1191.69	
KFM09A	20051207 17:58	20051207 19:16	133.00	138.00	7.79	132.00	965.88	969.75	966.44				
KFM09A	20051207 17:58	20051207 19:16	133.00	138.00	139.00	799.67				1231.68	1232.23	1231.68	
KFM09A	20051207 19:42	20051207 21:13	138.00	143.00	7.79	137.00	967.19	968.29	965.53				
KFM09A	20051207 19:42	20051207 21:13	138.00	143.00	144.00	799.67				1272.77	1272.49	1272.77	
KFM09A	20051207 21:27	20051207 22:45	141.00	146.00	7.79	140.00	962.51	962.64	963.33				
KFM09A	20051207 21:27	20051207 22:45	141.00	146.00	147.00	799.67				1297.69	1297.97	1297.42	
KFM09A	20051207 23:02	20051208 00:17	146.00	151.00	7.79	145.00	962.42	962.98	962.42				
KFM09A	20051207 23:02	20051208 00:17	146.00	151.00	152.00	799.67				1339.05	1339.19	1339.05	
KFM09A	20051208 06:16	20051208 06:59	151.00	156.00	7.79	150.00	965.79	965.51	965.37				
KFM09A	20051208 06:16	20051208 06:59	151.00	156.00	157.00	799.67				1381.24	1381.24	1381.24	
KFM09A	20051208 07:10	20051208 08:26	156.00	161.00	7.79	155.00	965.57	965.57	960.62				
KFM09A	20051208 07:10	20051208 08:26	156.00	161.00	162.00	799.67				1422.32	1423.42	1423.42	
KFM09A	20051208 08:36	20051208 09:52	161.00	166.00	7.79	160.00	964.66	962.46	964.66				
KFM09A	20051208 08:36	20051208 09:52	161.00	166.00	167.00	799.67				1464.10	1463.83	1463.42	
KFM09A	20051208 10:03	20051208 11:19	166.00	171.00	7.79	165.00	958.10	962.65	962.65				
KFM09A	20051208 10:03	20051208 11:19	166.00	171.00	172.00	799.67				1508.88	1509.43	1508.88	
KFM09A	20051208 12:12	20051208 13:29	171.00	176.00	7.79	170.00	958.45	958.45	958.45				
KFM09A	20051208 12:12	20051208 13:29	171.00	176.00	177.00	799.67				1549.84	1550.52	1550.52	
KFM09A	20051208 13:43	20051208 14:57	176.00	181.00	7.79	175.00	957.95	957.53	957.53				
KFM09A	20051208 13:43	20051208 14:57	176.00	181.00	182.00	799.67				1590.52	1591.06	1591.61	
KFM09A	20051208 15:13	20051208 16:28	181.00	186.00	7.79	180.00	956.63	956.08	956.08				
KFM09A	20051208 15:13	20051208 16:28	181.00	186.00	187.00	799.67				1631.59	1632.15	1632.69	

idcode	start_date	stop_date	secup	seclow	obs_secup	obs_seclow	pi_above	pp_above	pf_above	pi_below	pp_below	pf_below	comments
KFM09A	20051208 16:36	20051208 17:51	186.00	191.00	7.79	185.00	955.17	954.76	954.62				
KFM09A	20051208 16:36	20051208 17:51	186.00	191.00	192.00	799.67				1673.78	1674.32	1674.88	
KFM09A	20051208 18:03	20051208 18:50	191.00	196.00	7.79	190.00	953.71	953.71	953.71				
KFM09A	20051208 18:03	20051208 18:50	191.00	196.00	197.00	799.67				1714.60	1714.87	1714.87	
KFM09A	20051208 19:02	20051208 19:47	196.00	201.00	7.79	195.00	953.08	952.80	953.35				
KFM09A	20051208 19:02	20051208 19:47	196.00	201.00	202.00	799.67				1755.42	1755.96	1755.96	
KFM09A	20051208 19:57	20051208 20:39	201.00	206.00	7.79	200.00	951.76	951.62	951.35				
KFM09A	20051208 19:57	20051208 20:39	201.00	206.00	207.00	799.67				1796.91	1796.64	1797.05	
KFM09A	20051208 20:58	20051208 21:40	226.00	231.00	7.79	225.00	945.16	945.16	945.16				
KFM09A	20051208 20:58	20051208 21:40	226.00	231.00	232.00	799.67				2002.07	2002.07	2002.49	
KFM09A	20051208 21:54	20051208 23:08	232.00	237.00	7.79	231.00	943.24	942.83	942.96				
KFM09A	20051208 21:54	20051208 23:08	232.00	237.00	238.00	799.67				2050.15	2052.48	2052.90	
KFM09A	20051208 23:21	20051209 00:35	237.00	242.00	7.79	236.00	941.65	941.51	941.51				
KFM09A	20051208 23:21	20051209 00:35	237.00	242.00	243.00	799.67				2091.78	2092.88	2093.43	
KFM09A	20051209 08:08	20051209 09:24	240.80	245.80	7.79	239.80	940.36	940.36	939.81				
KFM09A	20051209 08:08	20051209 09:24	240.80	245.80	246.80	799.67				2119.73	2120.55	2121.37	
KFM09A	20051221 13:55	20051221 14:35	246.80	251.80	7.79	245.80	936.51	936.51	936.51				
KFM09A	20051221 13:55	20051221 14:35	246.80	251.80	252.80	799.67				2155.47	2155.61	2156.43	
KFM09A	20051209 09:40	20051209 10:22	251.50	256.50	7.79	250.50	936.76	936.62	936.49				
KFM09A	20051209 09:40	20051209 10:22	251.50	256.50	257.50	799.67				2208.47	2208.61	2209.02	
KFM09A	20051209 10:34	20051209 11:18	256.50	261.50	7.79	255.50	935.03	935.03	935.03				
KFM09A	20051209 10:34	20051209 11:18	256.50	261.50	262.50	799.67				2248.74	2249.01	2249.01	
KFM09A	20051209 11:30	20051209 13:22	273.00	278.00	7.79	272.00	929.01	929.01	929.01				
KFM09A	20051209 11:30	20051209 13:22	273.00	278.00	279.00	799.67				2384.88	2385.43	2385.98	
KFM09A	20051209 13:34	20051209 14:48	278.00	283.00	7.79	277.00	927.55	927.41	927.55				
KFM09A	20051209 13:34	20051209 14:48	278.00	283.00	284.00	799.67				2423.36	2424.73	2424.87	
KFM09A	20051209 15:04	20051209 15:51	283.00	288.00	7.79	282.00	925.96	925.82	925.54				
KFM09A	20051209 15:04	20051209 15:51	283.00	288.00	289.00	799.67				2463.21	2463.63	2463.77	
KFM09A	20051209 16:00	20051209 17:15	288.00	293.00	7.79	287.00	924.08	924.08	924.08				
KFM09A	20051209 16:00	20051209 17:15	288.00	293.00	294.00	799.67				2504.58	2505.40	2506.50	
KFM09A	20051212 08:21	20051212 09:42	293.00	298.00	7.79	292.00	923.18	923.73	924.83				
KFM09A	20051212 08:21	20051212 09:42	293.00	298.00	299.00	799.67				2542.66	2542.66	2542.66	

idcode	start_date	stop_date	secup	seclow	obs_secup	obs_seclow	pi_above	pp_above	pf_above	pi_below	pp_below	pf_below	comments
KFM09A	20051221 12:39	20051221 13:28	296.00	301.00	7.79	295.00	920.42	920.56	920.42				
KFM09A	20051221 12:39	20051221 13:28	296.00	301.00	302.00	799.67				2558.54	2559.09	2559.63	
KFM09A	20051221 11:45	20051221 12:29	301.00	306.00	7.79	300.00	917.86	917.86	918.42				
KFM09A	20051221 11:45	20051221 12:29	301.00	306.00	307.00	799.67				2595.26	2595.53	2596.35	
KFM09A	20051212 09:58	20051212 10:39	306.00	311.00	7.79	305.00	917.10	916.97	916.41				
KFM09A	20051212 09:58	20051212 10:39	306.00	311.00	312.00	799.67				2648.39	2648.39	2648.39	
KFM09A	20051212 10:49	20051212 12:33	311.00	316.00	7.79	310.00	917.15	917.02	917.15				
KFM09A	20051212 10:49	20051212 12:33	311.00	316.00	317.00	799.67				2687.83	2688.25	2687.83	
KFM09A	20051212 12:43	20051212 13:31	316.00	321.00	7.79	315.00	914.87	914.59	914.59				
KFM09A	20051212 12:43	20051212 13:31	316.00	321.00	322.00	799.67				2728.10	2728.37	2728.37	
KFM09A	20051212 13:44	20051212 15:02	321.00	326.00	7.79	320.00	912.73	910.38	912.04				
KFM09A	20051212 13:44	20051212 15:02	321.00	326.00	327.00	799.67				2767.81	2768.37	2768.91	
KFM09A	20051212 15:31	20051212 16:14	346.00	351.00	7.79	345.00	896.35	896.49	896.49				
KFM09A	20051212 15:31	20051212 16:14	346.00	351.00	352.00	799.67				2966.27	2966.68	2966.68	
KFM09A	20051221 10:04	20051221 11:19	351.00	356.00	7.79	350.00	895.85	895.99	896.13				
KFM09A	20051221 10:04	20051221 11:19	351.00	356.00	357.00	799.67				2999.56	3000.65	3001.75	
KFM09A	20051221 08:54	20051221 09:50	356.00	361.00	7.79	355.00	892.47	892.88	893.02				
KFM09A	20051221 08:54	20051221 09:50	356.00	361.00	362.00	799.67				3037.62	3038.86	3039.00	
KFM09A	20051221 07:28	20051221 08:43	361.00	366.00	7.79	360.00	888.39	889.35	889.35				
KFM09A	20051221 07:28	20051221 08:43	361.00	366.00	367.00	799.67				3071.87	3073.65	3075.70	
KFM09A	20051212 16:39	20051212 17:54	363.00	368.00	7.79	362.00	888.98	888.98	888.98				
KFM09A	20051212 16:39	20051212 17:54	363.00	368.00	369.00	799.67				3099.80	3100.49	3101.45	
KFM09A	20051213 06:27	20051213 07:24	368.00	373.00	7.79	367.00	890.70	890.83	890.83				
KFM09A	20051213 06:27	20051213 07:24	368.00	373.00	374.00	799.67				3141.44	3141.44	3141.44	
KFM09A	20051213 07:35	20051213 08:48	371.00	376.00	7.79	370.00	889.19	889.05	886.43				
KFM09A	20051213 07:35	20051213 08:48	371.00	376.00	377.00	799.67				3165.55	3166.10	3166.65	
KFM09A	20051213 09:02	20051213 09:58	376.00	381.00	7.79	375.00	886.50	883.61	884.98				
KFM09A	20051213 09:02	20051213 09:58	376.00	381.00	382.00	799.67				3205.40	3205.95	3205.54	
KFM09A	20051213 10:10	20051213 11:25	381.00	386.00	7.79	380.00	883.66	881.88	882.98				
KFM09A	20051213 10:10	20051213 11:25	381.00	386.00	387.00	799.67				3244.71	3245.53	3245.53	
KFM09A	20051213 11:57	20051213 13:16	386.00	391.00	7.79	385.00	880.55	880.42	878.75				
KFM09A	20051213 11:57	20051213 13:16	386.00	391.00	392.00	799.67				3283.88	3284.57	3285.52	

idcode	start_date	stop_date	secup	seclow	obs_secup	obs_seclow	pi_above	pp_above	pf_above	pi_below	pp_below	pf_below	comments
KFM09A	20051213 13:28	20051213 14:48	391.00	396.00	7.79	390.00	877.86	875.10	877.86				
KFM09A	20051213 13:28	20051213 14:48	391.00	396.00	397.00	799.67				3324.97	3325.51	3326.07	
KFM09A	20051213 15:06	20051213 15:49	396.00	401.00	7.79	395.00	874.60	873.36	873.09				
KFM09A	20051213 15:06	20051213 15:49	396.00	401.00	402.00	799.67				3363.18	3363.32	3363.32	
KFM09A	20051213 16:00	20051213 17:15	401.00	406.00	7.79	400.00	872.18	869.42	872.18				
KFM09A	20051213 16:00	20051213 17:15	401.00	406.00	407.00	799.67				3403.03	3403.86	3404.40	
KFM09A	20051213 17:25	20051213 18:18	406.00	411.00	7.79	405.00	866.86	868.79	868.52				
KFM09A	20051213 17:25	20051213 18:18	406.00	411.00	412.00	799.67				3442.61	3443.17	3442.75	
KFM09A	20051213 18:36	20051213 19:50	411.00	416.00	7.79	410.00	863.61	865.41	865.96				
KFM09A	20051213 18:36	20051213 19:50	411.00	416.00	417.00	799.67				3480.83	3481.65	3482.20	
KFM09A	20051213 20:06	20051213 21:22	414.00	419.00	7.79	413.00	864.32	864.04	861.56				
KFM09A	20051213 20:06	20051213 21:22	414.00	419.00	420.00	799.67				3504.39	3505.20	3505.76	
KFM09A	20051213 21:32	20051213 22:46	419.00	424.00	7.79	418.00	857.90	857.90	857.35				
KFM09A	20051213 21:32	20051213 22:46	419.00	424.00	425.00	799.67				3542.45	3543.55	3544.11	
KFM09A	20051213 22:55	20051214 00:09	421.00	426.00	7.79	420.00	857.53	856.99	858.09				
KFM09A	20051213 22:55	20051214 00:09	421.00	426.00	427.00	799.67				3558.34	3559.44	3559.99	
KFM09A	20051214 06:51	20051214 07:59	426.00	431.00	7.79	425.00	857.17	853.87	855.53				
KFM09A	20051214 06:51	20051214 07:59	426.00	431.00	432.00	799.67				3597.80	3598.34	3598.34	
KFM09A	20051214 08:11	20051214 09:31	431.00	436.00	7.79	430.00	854.76	854.76	854.07				
KFM09A	20051214 08:11	20051214 09:31	431.00	436.00	437.00	799.67				3641.20	3644.35	3644.35	
KFM09A	20051214 09:47	20051214 10:29	436.00	441.00	7.79	435.00	852.33	852.06	852.06				
KFM09A	20051214 09:47	20051214 10:29	436.00	441.00	442.00	799.67				3683.25	3683.25	3683.25	
KFM09A	20051214 10:44	20051214 12:00	441.00	446.00	7.79	440.00	848.67	848.39	846.74				
KFM09A	20051214 10:44	20051214 12:00	441.00	446.00	447.00	799.67				3719.96	3721.61	3721.61	
KFM09A	20051214 12:13	20051214 14:04	446.00	451.00	7.79	445.00	844.32	845.29	845.83				
KFM09A	20051214 12:13	20051214 14:04	446.00	451.00	452.00	799.67				3760.91	3761.59	3762.15	
KFM09A	20051214 14:22	20051214 15:38	451.00	456.00	7.79	450.00	842.17	842.46	840.53				
KFM09A	20051214 14:22	20051214 15:38	451.00	456.00	457.00	799.67				3797.62	3798.85	3799.95	
KFM09A	20051214 15:55	20051214 17:12	456.00	461.00	7.79	455.00	839.21	837.41	839.07				
KFM09A	20051214 15:55	20051214 17:12	456.00	461.00	462.00	799.67				3836.65	3837.88	3838.84	
KFM09A	20051214 17:32	20051214 18:15	461.00	466.00	7.79	460.00	836.37	836.09	836.51				
KFM09A	20051214 17:32	20051214 18:15	461.00	466.00	467.00	799.67				3875.54	3875.68	3876.10	

idcode	start_date	stop_date	secup	seclow	obs_secup	obs_seclow	pi_above	pp_above	pf_above	pi_below	pp_below	pf_below	comments
KFM09A	20051214 18:35	20051214 19:50	471.00	476.00	7.79	470.00	829.18	829.18	828.08				
KFM09A	20051214 18:35	20051214 19:50	471.00	476.00	477.00	799.67				3952.23	3953.89	3954.98	
KFM09A	20051214 20:01	20051214 21:23	476.00	481.00	7.79	475.00	826.34	826.20	826.07				
KFM09A	20051214 20:01	20051214 21:23	476.00	481.00	482.00	799.67				3992.38	3993.34	3994.43	
KFM09A	20051214 21:40	20051214 22:31	486.00	491.00	7.79	485.00	861.26	860.98	860.98				
KFM09A	20051214 21:40	20051214 22:31	486.00	491.00	492.00	799.67				4070.03	4070.03	4070.03	
KFM09A	20051214 22:58	20051215 00:12	491.00	496.00	7.79	490.00	858.42	856.77	857.32				
KFM09A	20051214 22:58	20051215 00:12	491.00	496.00	497.00	799.67				4108.38	4109.47	4110.02	
KFM09A	20051215 06:33	20051215 07:57	496.00	501.00	7.79	495.00	853.52	852.83	853.11				
KFM09A	20051215 06:33	20051215 07:57	496.00	501.00	502.00	799.67				4145.63	4146.73	4147.83	
KFM09A	20051215 08:14	20051215 09:00	501.00	506.00	7.79	500.00	807.49	807.21	807.76				
KFM09A	20051215 08:14	20051215 09:00	501.00	506.00	507.00	799.67				4184.11	4184.52	4184.52	
KFM09A	20051220 19:00	20051220 20:23	506.00	511.00	7.79	505.00	806.16	806.30	805.75				
KFM09A	20051220 19:00	20051220 20:23	506.00	511.00	512.00	799.67				4220.68	4222.87	4224.52	
KFM09A	20051220 20:50	20051220 22:05	511.00	516.00	7.79	510.00	797.41	794.65	794.38				
KFM09A	20051220 20:50	20051220 22:05	511.00	516.00	517.00	799.67				4262.59	4263.97	4265.06	
KFM09A	20051220 22:14	20051220 23:28	516.00	521.00	7.79	515.00	794.02	794.84	795.67				
KFM09A	20051220 22:14	20051220 23:28	516.00	521.00	522.00	799.67				4299.57	4301.36	4302.86	
KFM09A	20051215 09:25	20051215 10:11	521.00	526.00	7.79	520.00	792.29	792.15	792.57				
KFM09A	20051215 09:25	20051215 10:11	521.00	526.00	527.00	799.67				4337.92	4338.19	4338.47	
KFM09A	20051215 10:26	20051215 11:07	526.00	531.00	7.79	525.00	789.04	788.91	787.80				
KFM09A	20051215 10:26	20051215 11:07	526.00	531.00	532.00	799.67				4375.17	4375.17	4375.73	
KFM09A	20051215 11:23	20051215 12:44	531.00	536.00	7.79	530.00	785.10	782.62	784.14				
KFM09A	20051215 11:23	20051215 12:44	531.00	536.00	537.00	799.67				4416.27	4417.22	4417.36	
KFM09A	20051215 13:19	20051215 14:03	536.00	541.00	7.79	535.00	777.58	777.72	777.17				
KFM09A	20051215 13:19	20051215 14:03	536.00	541.00	542.00	799.67				4454.61	4454.61	4454.61	
KFM09A	20051215 14:14	20051215 15:28	541.00	546.00	7.79	540.00	773.92	773.51	773.51				
KFM09A	20051215 14:14	20051215 15:28	541.00	546.00	547.00	799.67				4492.55	4493.09	4493.50	
KFM09A	20051220 17:14	20051220 17:58	561.00	566.00	7.79	560.00	760.10	760.10	760.52				
KFM09A	20051220 17:14	20051220 17:58	561.00	566.00	567.00	799.67				4643.07	4643.07	4643.07	
KFM09A	20051215 16:19	20051215 17:00	606.00	611.00	7.79	605.00	712.54	712.12	711.58				
KFM09A	20051215 16:19	20051215 17:00	606.00	611.00	612.00	799.67				4977.25	4977.25	4977.25	

idcode	start_date	stop_date	secup	seclow	obs_secup	obs_seclow	pi_above	pp_above	pf_above	pi_below	pp_below	pf_below	comments
KFM09A	20051215 17:19	20051215 18:35	611.00	616.00	7.79	610.00	706.40	706.40	706.26				
KFM09A	20051215 17:19	20051215 18:35	611.00	616.00	617.00	799.67				5014.09	5014.77	5015.04	
KFM09A	20051215 18:50	20051215 19:31	616.00	621.00	7.79	615.00	701.91	701.50	701.50				
KFM09A	20051215 18:50	20051215 19:31	616.00	621.00	622.00	799.67				5051.48	5051.20	5051.76	
KFM09A	20051215 19:44	20051215 21:03	621.00	626.00	7.79	620.00	696.18	695.63	695.63				
KFM09A	20051215 19:44	20051215 21:03	621.00	626.00	627.00	799.67				5087.91	5088.18	5088.45	
KFM09A	20051215 21:14	20051215 22:01	626.00	631.00	7.79	625.00	690.32	690.32	690.32				
KFM09A	20051215 21:14	20051215 22:01	626.00	631.00	632.00	799.67				5124.61	5124.75	5125.17	
KFM09A	20051215 22:08	20051215 23:33	631.00	636.00	7.79	630.00	684.99	684.72	684.45				
KFM09A	20051215 22:08	20051215 23:33	631.00	636.00	637.00	799.67				5160.77	5161.32	5161.87	
KFM09A	20051215 23:43	20051216 00:58	636.00	641.00	7.79	635.00	679.13	678.86	679.13				
KFM09A	20051215 23:43	20051216 00:58	636.00	641.00	642.00	799.67				5197.61	5198.02	5198.02	
KFM09A	20051216 08:21	20051216 09:36	641.00	646.00	7.79	640.00	672.72	672.72	672.72				
KFM09A	20051216 08:21	20051216 09:36	641.00	646.00	647.00	799.67				5232.40	5233.08	5233.64	
KFM09A	20051216 09:55	20051216 10:38	646.00	651.00	7.79	645.00	667.82	667.68	667.95				
KFM09A	20051216 09:55	20051216 10:38	646.00	651.00	652.00	799.67				5270.33	5270.33	5270.89	
KFM09A	20051216 10:53	20051216 12:10	651.00	656.00	7.79	650.00	661.82	661.53	661.53				
KFM09A	20051216 10:53	20051216 12:10	651.00	656.00	657.00	799.67				5307.04	5307.32	5307.04	
KFM09A	20051216 12:21	20051216 13:20	656.00	661.00	7.79	655.00	655.67	655.67	655.67				
KFM09A	20051216 12:21	20051216 13:20	656.00	661.00	662.00	799.67				5343.20	5343.20	5343.20	
KFM09A	20051216 13:31	20051216 14:14	661.00	666.00	667.00	799.67	649.39	649.39	649.26				
KFM09A	20051216 13:31	20051216 14:14	661.00	666.00	667.00	667.00				5379.36	5379.22	5379.36	
KFM09A	20051219 08:19	20051219 09:01	731.00	736.00	7.79	730.00	557.22	556.94	556.66				
KFM09A	20051219 08:19	20051219 09:01	731.00	736.00	737.00	799.67				5867.48	5867.48	5867.48	
KFM09A	20051219 09:15	20051219 09:56	736.00	741.00	7.79	735.00	548.59	548.59	548.59				
KFM09A	20051219 09:15	20051219 09:56	736.00	741.00	742.00	799.67				5902.00	5902.13	5902.00	
KFM09A	20051219 10:11	20051219 11:30	741.00	746.00	7.79	740.00	541.76	539.98	539.98				
KFM09A	20051219 10:11	20051219 11:30	741.00	746.00	747.00	799.67				5936.37	5936.51	5936.51	
KFM09A	20051219 11:44	20051219 12:36	746.00	751.00	7.79	745.00	533.55	533.55	533.55				
KFM09A	20051219 11:44	20051219 12:36	746.00	751.00	752.00	799.67				5970.48	5970.48	5970.48	
KFM09A	20051219 12:50	20051219 14:05	751.00	756.00	7.79	750.00	524.93	524.11	524.93				
KFM09A	20051219 12:50	20051219 14:05	751.00	756.00	757.00	799.67				6004.58	6006.09	6005.00	

idcode	start_date	stop_date	secup	seclow	obs_secup	obs_seclow	pi_above	pp_above	pf_above	pi_below	pp_below	pf_below	comments
KFM09A	20051219 14:20	20051219 15:42	756.00	761.00	7.79	755.00	516.73	516.32	516.87				
KFM09A	20051219 14:20	20051219 15:42	756.00	761.00	762.00	799.67				6038.00	6038.40	6038.40	
KFM09A	20051219 15:56	20051219 17:16	761.00	766.00	7.79	760.00	509.21	508.11	507.70				
KFM09A	20051219 15:56	20051219 17:16	761.00	766.00	767.00	799.67				6071.83	6074.02	6072.38	
KFM09A	20051220 06:55	20051220 08:10	766.00	771.00	7.79	765.00	498.80	498.66	498.52				
KFM09A	20051220 06:55	20051220 08:10	766.00	771.00	772.00	799.67				6105.65	6105.52	6105.79	
KFM09A	20051220 08:29	20051220 09:46	771.00	776.00	7.79	770.00	489.90	490.04	489.90				
KFM09A	20051220 08:29	20051220 09:46	771.00	776.00	777.00	799.67				6138.67	6139.76	6139.21	
KFM09A	20051220 10:06	20051220 11:24	776.00	781.00	7.79	775.00	481.56	480.73	479.08				
KFM09A	20051220 10:06	20051220 11:24	776.00	781.00	782.00	799.67				6172.08	6172.35	6172.08	
KFM09A	20051220 11:35	20051220 12:58	781.00	786.00	7.79	780.00	469.90	470.18	471.01				
KFM09A	20051220 11:35	20051220 12:58	781.00	786.00	787.00	799.67				6204.54	6207.14	6206.04	
KFM09A	20051220 13:11	20051220 14:28	786.00	791.00	7.79	785.00	462.38	462.38	462.38				
KFM09A	20051220 13:11	20051220 14:28	786.00	791.00	792.00	799.67				6240.56	6243.85	6240.01	
KFM09A	20051118 13:32	20051118 14:28	506.00	606.00	7.79	505.00	789.23	789.09	789.23				Incomplete test, interrupted and re-performed later.
KFM09A	20051118 13:32	20051118 14:28	506.00	606.00	607.00	799.67				4942.10	4943.06	4942.65	Incomplete test, interrupted and re-performed later.
KFM09A	20051130 17:10	20051130 18:03	426.00	446.00	7.79	425.00	855.53	855.39	854.97				Incomplete test, interrupted and re-performed later.
KFM09A	20051130 17:10	20051130 18:03	426.00	446.00	447.00	799.67				3726.67	3728.72	3728.72	Incomplete test, interrupted and re-performed later.
KFM09A	20051207 10:38	20051207 12:39	116.00	121.00	7.79	115.00	970.07	969.51	970.07				Incomplete test, interrupted and re-performed later.
KFM09A	20051207 10:38	20051207 12:39	116.00	121.00	122.00	799.67				1088.56	1088.70	1088.70	Incomplete test, interrupted and re-performed later.

Appendix 2.2 Pressure and flow data

Summary of pressure and flow data for all tests in KFM09A

Test section		Pressure			Flow		
secup	seclow	p_i	p_p	p_F	Q_p 1)	Q_m 2)	V_p 2)
(m)	(m)	(kPa)	(kPa)	(kPa)	(m^3/s)	(m^3/s)	(m^3)
106.00	206.00	929.78	1114.19	948.54	7.07E-05	9.33E-05	1.70E-01
206.00	306.00	1746.27	1963.05	1759.94	1.31E-06	1.62E-06	2.95E-03
306.00	406.00	2542.61	2753.18	2631.48	4.06E-06	7.19E-06	1.31E-02
406.00	506.00	3314.26	3517.7	3472.12	1.07E-05	3.77E-05	6.87E-02
506.00	606.00	4075.97	4296.2	4263.63	1.94E-06	8.12E-06	1.48E-02
606.00	706.00	4781.92	4987.26	4843.19	5.72E-07	8.03E-07	1.46E-03
691.00	791.00	5371.98	5548.07	5405.64	8.41E-07	1.23E-06	2.24E-03
106.00	126.00	939.44	1152.92	946.07	8.47E-06	9.98E-06	1.22E-02
126.00	146.00	1108.5	1324.71	1158.02	2.71E-05	4.44E-05	5.40E-02
146.00	166.00	1277.24	1460	1389.29	4.5E-06	1.26E-05	1.54E-02
166.00	186.00	1439.66	1628.85	1451.67	4.24E-05	4.98E-05	6.07E-02
186.00	206.00	1609	1908.7	1627.19	1.41E-07	1.63E-07	1.99E-04
206.00	226.00	1799.82	1971.07	1959.47			
226.00	246.00	1936.29	2142.18	1942.92	9.72E-07	1.18E-06	1.45E-03
238.00	258.00	2036.61	2246.5	2073.17	2.46E-07	3.84E-07	4.70E-04
258.00	278.00	2205.79	2409.18	2271.89	5.18E-08	9.9E-08	1.22E-04
278.00	298.00	2363.51	2574.6	2423.68	1.11E-07	1.57E-07	1.92E-04
286.00	306.00	2426.85	2640.1	2497.64	6.13E-08	9.62E-08	1.19E-04
306.00	326.00	2588.71	2788.52	2720.63	2.78E-07	6.73E-07	8.23E-04
326.00	346.00	2751.68	2952.8	2816.12	2.09E-08	4.56E-08	5.58E-05
346.00	366.00	2908.57	3113.84	2949.69	4.37E-08	5.89E-08	7.20E-05
366.00	386.00	3063.39	3264.59	3103.70	1.28E-06	1.6E-06	1.98E-03
386.00	406.00	3219.88	3419.73	3326.14	2.69E-06	5.5E-06	6.80E-03
406.00	426.00	3378.16	3578.01	3432.11	3.99E-07	4.89E-07	6.05E-04
426.00	446.00	3545.41	3765.49	3714.71	1.85E-05	4.93E-05	6.10E-02
446.00	466.00	3693.33	3922.81	3730.72	7.09E-08	9.94E-08	1.23E-04
466.00	486.00	3856.58	4029.33	3923.36	4E-08	7.55E-08	9.52E-05
486.00	506.00	4001.32	4206.1	4108.27	1.17E-07	2.67E-07	3.27E-04
506.00	526.00	4171.74	4362.23	4210.38	4.34E-08	7.76E-08	9.50E-05
526.00	546.00	4303.1	4508.03	4472.57	2.91E-06	9.83E-06	1.20E-02
545.00	565.00	4514.1	4661.19	4675.69			
566.00	586.00	4631.11	4820.31	4823.61			
586.00	606.00	4765.93	4982.58	4989.21			
606.00	626.00	4896.47	5096.82	4980.92	4.76E-07	7.39E-07	9.01E-04
626.00	646.00	5050.61	5258.42	5072.55	8.54E-08	1.15E-07	1.41E-04
646.00	666.00	5186.25	5389.93	5211.64	1.04E-07	1.27E-07	1.55E-04
666.00	686.00	5355.15	5533.99	5469.96	1.19E-08	3.11E-08	3.74E-05
686.00	706.00	5498.11	5687.43	5619.55	9.44E-09	2.33E-08	2.81E-05
691.00	711.00	5561.73	5724.42	5713.38			
711.00	731.00	5679.43	5864.34	5869.58			
731.00	751.00	5782.93	5995.56	5819.36	6.26E-08	8.05E-08	9.84E-05
751.00	771.00	5915.12	6118.38	1406.62	3.61E-07	1.07E-07	1.31E-04
771.00	791.00	6056.14	6271.55	1456.30	8.9E-07	4.69E-05	5.72E-02
106.00	111.00	948.9	1151.62	995.96	5.7E-07	6.88E-07	8.42E-04
111.00	116.00	993.19	1200.74	1037.91	6E-08	7.52E-08	9.20E-05
116.00	121.00	1025.62	1225.72	1627.41	2.15E-06	1.42E-07	1.73E-04
121.00	126.00	1074.34	1252.7	1076.55	5.98E-06	6.93E-06	8.47E-03
126.00	131.00	1121.53	1323.83	1249.86	3.85E-08	1.12E-07	1.37E-04
128.00	133.00	1131.88	1348.66	1163.76	1.74E-05	2.61E-05	3.18E-02
133.00	138.00	1174.24	1409.45	1217.29	1.66E-05	2.67E-05	3.21E-02
138.00	143.00	1215.08	1415.79	1219.50	3.09E-07	3.51E-07	4.28E-04
141.00	146.00	1240.89	1466.23	1321.06	1.24E-06	2.35E-06	2.88E-03
146.00	151.00	1284.09	1510.35	1450.22	1.33E-06	5.33E-06	6.51E-03
151.00	156.00	1349.21	1565.72	1571.10			
156.00	161.00	1365.5	1573.1	1482.79	4.26E-06	1.07E-05	1.31E-02
161.00	166.00	1408	1586.5	1406.62	1.02E-07	1.07E-07	1.31E-04
166.00	171.00	1447.05	1626.8	1456.30	4.09E-05	4.69E-05	5.72E-02
171.00	176.00	1496.45	1703.03	1687.02	5.5E-08	8.37E-07	1.03E-03
176.00	181.00	1534	1734.49	1557.86	2.91E-07	3.41E-07	4.15E-04
181.00	186.00	1575.38	1803.9	1780.30	2.5E-07	1.9E-06	2.35E-03
186.00	191.00	1616.92	1832.6	1627.41	1.23E-07	1.42E-07	1.73E-04
191.00	196.00	1677.49	1875.23	1828.87			
196.00	201.00	1710.62	1916.5	1891.79			
201.00	206.00	1766.78	1957.48	1965.21			
226.00	231.00	1961.89	2161.15	2158.94			
232.00	237.00	1992.95	2191.65	1995.02	8.39E-07	8.63E-07	1.05E-03

Test section		Pressure			Flow		
secup	seclow	p_i	p_p	p_F	Q_p [1)]	Q_m [2)]	V_p [2)]
(m)	(m)	(kPa)	(kPa)	(kPa)	(m^3/s)	(m^3/s)	(m^3)
237.00	242.00	2032.55	2232.77	2040.28	1.7E-06	1.86E-06	2.27E-03
240.80	245.80	2060.01	2263.69	2071.18	3.22E-07	4.57E-07	5.58E-04
246.80	251.80	2184.89	2323.99	2971.99			
251.50	256.50	2217.45	2385.25	2408.43			
256.50	261.50	2239.39	2427.2	2424.45			
273.00	278.00	2328.68	2560.78	2393.53	6.8E-08	1E-07	1.22E-04
278.00	283.00	2369.8	2576.3	2435.48	9.75E-08	1.44E-07	1.76E-04
283.00	288.00	2409.26	2618.73	2574.58			
288.00	293.00	2459.9	2659.88	2540.35	1.57E-08	2.83E-08	3.40E-05
293.00	298.00	2493.43	2728	2549.74	3.38E-08	4.1E-08	5.00E-05
296.00	301.00	2521.45	2730.23	3349.53			
301.00	306.00	2567.81	2767.21	3301.51			
306.00	311.00	2678.48	2831.8	2864.35			
311.00	316.00	2652.96	2872.36	2868.77			
316.00	321.00	2674.48	2942.73	2935.01			
321.00	326.00	2712.56	2913.42	2845.04	2.98E-07	6.68E-07	8.16E-04
346.00	351.00	3017.39	3117.02	3125.44			
351.00	356.00	2958.18	3169.22	3512.92	5.07E-08	6.9E-08	8.44E-05
356.00	361.00	2991.17	3206.99	3532.23			
361.00	366.00	3026.221	3242.46	3698.38	1.76E-08	9.48E-09	1.14E-05
363.00	368.00	3062.65	3254.73	3095.07	1.17E-08	1.62E-08	1.95E-05
368.00	373.00	3128.47	3316.41	3294.88			
371.00	376.00	3108.19	3309.5	3140.33	1.47E-06	2.13E-06	2.12E-03
376.00	381.00	3174.01	3361.53	3334.08			
381.00	386.00	3234.58	3403.07	3284.95			
386.00	391.00	3226.58	3437.98	3349.53	2.47E-06	5.33E-06	6.53E-03
391.00	396.00	3274.47	3481.73	3301.51	1.66E-07	1.87E-07	2.29E-04
396.00	401.00	3321.1	3524.5	3485.87			
401.00	406.00	3346.08	3547.69	3369.95	4.26E-07	4.98E-07	6.09E-04
406.00	411.00	3392.03	3584.11	3550.45			
411.00	416.00	3426.25	3621.31	3496.35	3.7E-07	5.52E-07	6.76E-04
414.00	419.00	3460.47	3654.12	3480.91	1.3E-08	1.05E-08	1.27E-05
419.00	424.00	3488.626	3692.58	3512.92	5.68E-08	6.9E-08	8.44E-05
421.00	426.00	3515	3708.32	3532.23	5.78E-08	7.13E-08	8.73E-05
426.00	431.00	3560.79	3773.3	3698.38			
431.00	436.00	3579.7	3802.83	3753.02	1.61E-05	5.02E-05	6.15E-02
436.00	441.00	3649.79	3829.74	3837.47			
441.00	446.00	3661.4	3888.2	3871.14	2.09E-07	1.94E-06	2.41E-03
446.00	451.00	3702.236	3909.77	3866.72	3.75E-08	1.55E-07	1.90E-04
451.00	456.00	3761.02	3951.96	3840.22	1.24E-08	1.48E-08	1.78E-05
456.00	461.00	3787.78	3990.92	3815.94	6.76E-08	5.9E-08	7.22E-05
461.00	466.00	3916.81	4031.76	4071.50			
471.00	476.00	3902.457	4111.1	3964.42	5.28E-08	7.96E-08	9.75E-05
476.00	481.00	3964.425	4153.74	4008.03	4.27E-08	5.18E-08	6.33E-05
486.00	491.00	4047.08	4229.36	4217.76			
491.00	496.00	4063.22	4261.51	4095.23	7.8E-08	1.03E-07	1.26E-04
496.00	501.00	4090.13	4297.53	4222.18	6.24E-08	1.75E-07	2.15E-04
501.00	506.00	4165.19	4330.23	4289.52			
506.00	511.00	4215.56	4366.8	4289.52	1.64E-08	1.77E-08	2.13E-05
511.00	516.00	4232.67	4403.23	4229.36	2.98E-08	2.82E-08	3.44E-05
516.00	521.00	4254.199	4440.03	4285.67	1.94E-08	2.24E-08	2.70E-05
521.00	526.00	4405.3	4484.51	4539.01			
526.00	531.00	4442.14	4520.81	4592.00			
531.00	536.00	4354.65	4571.03	4535.15	2.91E-06	1.06E-05	1.30E-02
536.00	541.00	4479.13	4594.76	4560.54			
541.00	546.00	4437.45	4632.29	4613.53	8.67E-09	5.55E-08	6.67E-05
561.00	566.00	4726.95	4774.42	4801.19			
606.00	611.00	5042.26	5120.24	5224.00			
611.00	616.00	4956.43	5148.26	5044.06	3.96E-07	6.14E-07	7.50E-04
616.00	621.00	5077.59	5206.34	5272.02			
621.00	626.00	5032.46	5244.56	5127.97	1.53E-07	2.22E-07	2.73E-04
626.00	631.00	5085.18	5263.75	5233.38			
631.00	636.00	5136.79	5301.28	5249.39	1.17E-08	2.06E-08	2.47E-05
636.00	641.00	5144.52	5335.36	5146.73	1.35E-07	1.34E-07	1.64E-04
641.00	646.00	5195.3	5374.69	5235.59	1.27E-08	9.09E-07	1.11E-03
646.00	651.00	5309.69	5410.56	5419.40			
651.00	656.00	5248.56	5444.23	5280.30	1.27E-07	2.02E-05	9.65E-03
656.00	661.00	5344.46	5486.74	5472.94			
661.00	666.00	5426.71	5523.99	5534.21			
731.00	736.00	5867.31	6009.44	5986.26			
736.00	741.00	5860.27	6044.22	5996.20			

Test section		Pressure			Flow		
secup	seclow	p_i	p_p	p_F	Q_p [1)]	Q_m [2)]	V_p [2)]
(m)	(m)	(kPa)	(kPa)	(kPa)	(m^3/s)	(m^3/s)	(m^3)
741.00	746.00	5881.11	6078.44	5914.50	8.87E-08	7.57E-08	9.31E-05
746.00	751.00	5928.44	6112.66	6074.02			
751.00	756.00	5957.42	6143.29	6000.07	7.95E-08	1.26E-07	1.55E-04
756.00	761.00	5986.68	6192.63	6040.91	2.15E-07	3.66E-07	4.51E-04
761.00	766.00	6021.04	6221.97	6050.29	1.07E-07	1.57E-07	1.92E-04
766.00	771.00	6049.32	6239.82	6077.34	5.47E-08	7.57E-08	9.27E-05
771.00	776.00	6086.85	6319.41	6096.65	5.99E-08	6.39E-08	7.84E-05
776.00	781.00	6119.15	6309.34	6137.49	1.15E-07	1.4E-07	1.71E-04
781.00	786.00	6152.12	6325.44	6168.40	1.85E-07	2.36E-07	2.90E-04
786.00	791.00	6184.96	6388.23	6192.69	7.06E-07	9.09E-07	1.11E-03
506.00 [3)]	606.00	4063.27	4265.15	4264.74			
426.00 [3)]	446.00	3535.19	3703.67	3675.53			
116.00 [3)]	121.00	1074.89	1242.69	1074.34			

[1)] No value indicates a flow below measurement limit (measurement limit is unique for each test but nominally 1.67 E-8 m^3/s).
[2)] No value indicates that the parameter could not be calculated due to low and uncertain flow rates during a major part of flow period
[3)] The tests were interrupted for various reasons or did not provide satisfying data for the evaluation and were hence re-performed later.

p_i	Pressure in test section before start of flow period
p_p	Pressure in test section before stop of flow period
p_F	Pressure in test section at the end of recovery period
Q_p	Flow rate just before stop of flow period
Q_m	Mean (arithmetic) flow rate during flow period
V_p	Total volume injected during flow period

Appendix 3. Test diagrams – Injection Tests

In the following pages diagrams are presented for all test sections. A linear diagram of pressure and flow rate is presented for each test. For most tests are lin-log and log-log diagrams presented, from injection and recovery period respectively.

Nomenclature for Aqtesolv:

T	=	transmissivity (m^2/s)
S	=	storativity (-)
K_z/K_r	=	ratio of hydraulic conductivities in the vertical and radial direction (set to 1)
Sw	=	skin factor
r(w)	=	borehole radius (m)
r(c)	=	effective casing radius (m)
C	=	well loss constant (set to 0)
r/B	=	leakage factor (-)

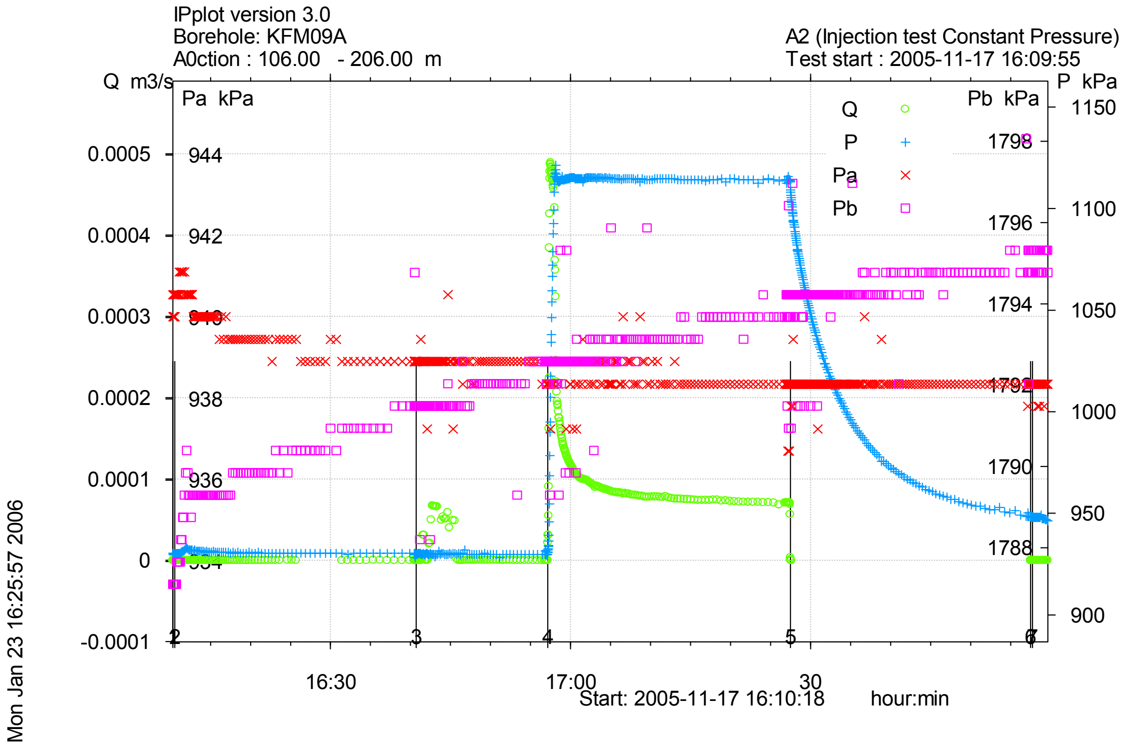


Figure A3-2. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 106.0-206.0 m in borehole KFM09A.*

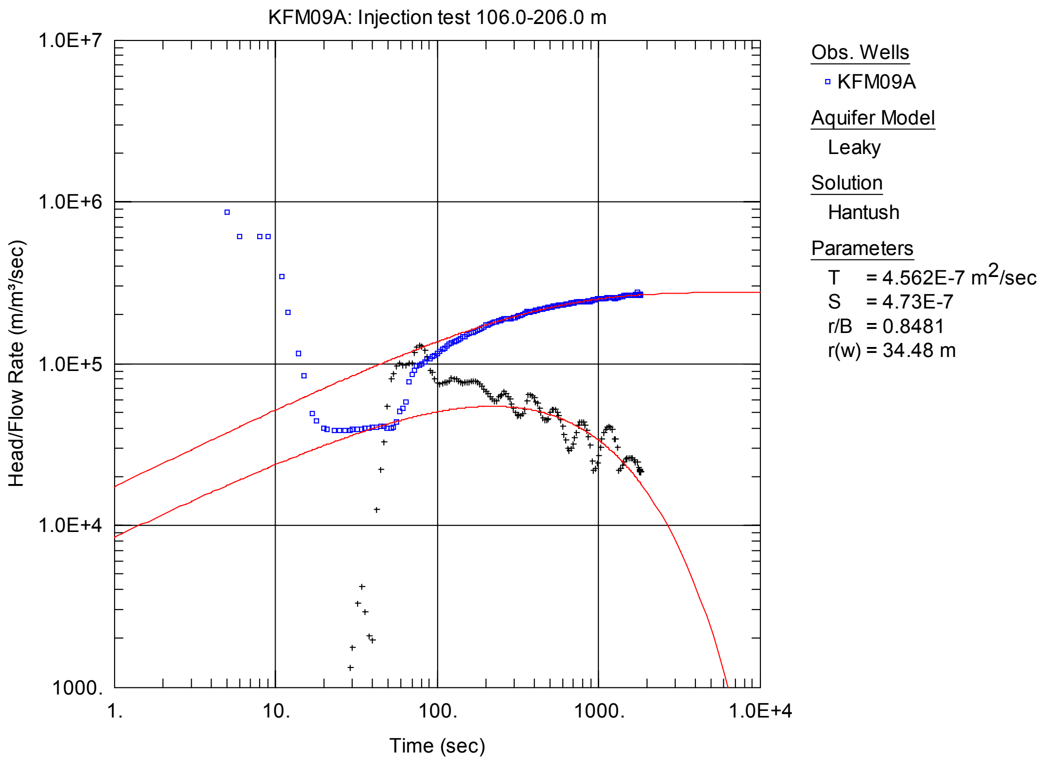


Figure A3-3. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 106.0-206.0 m in KFM09A.*

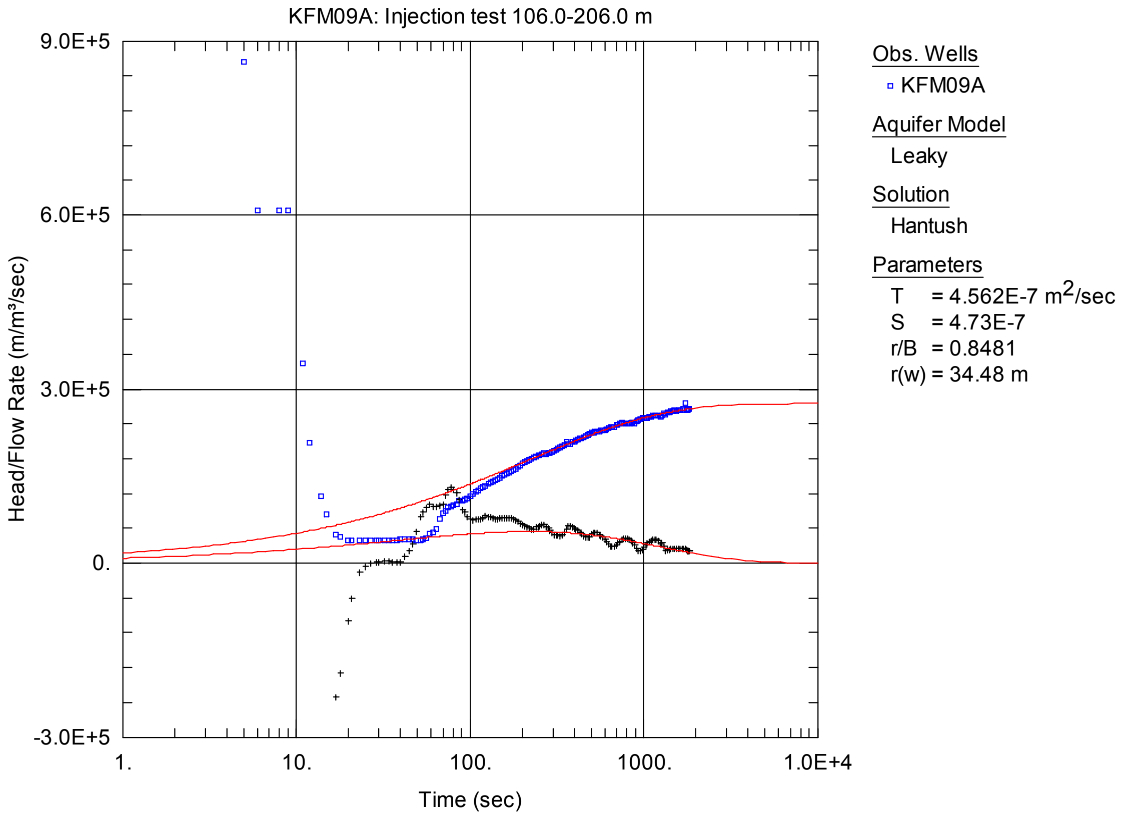


Figure A3-4. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 106.0-206.0 m in KFM09A.*

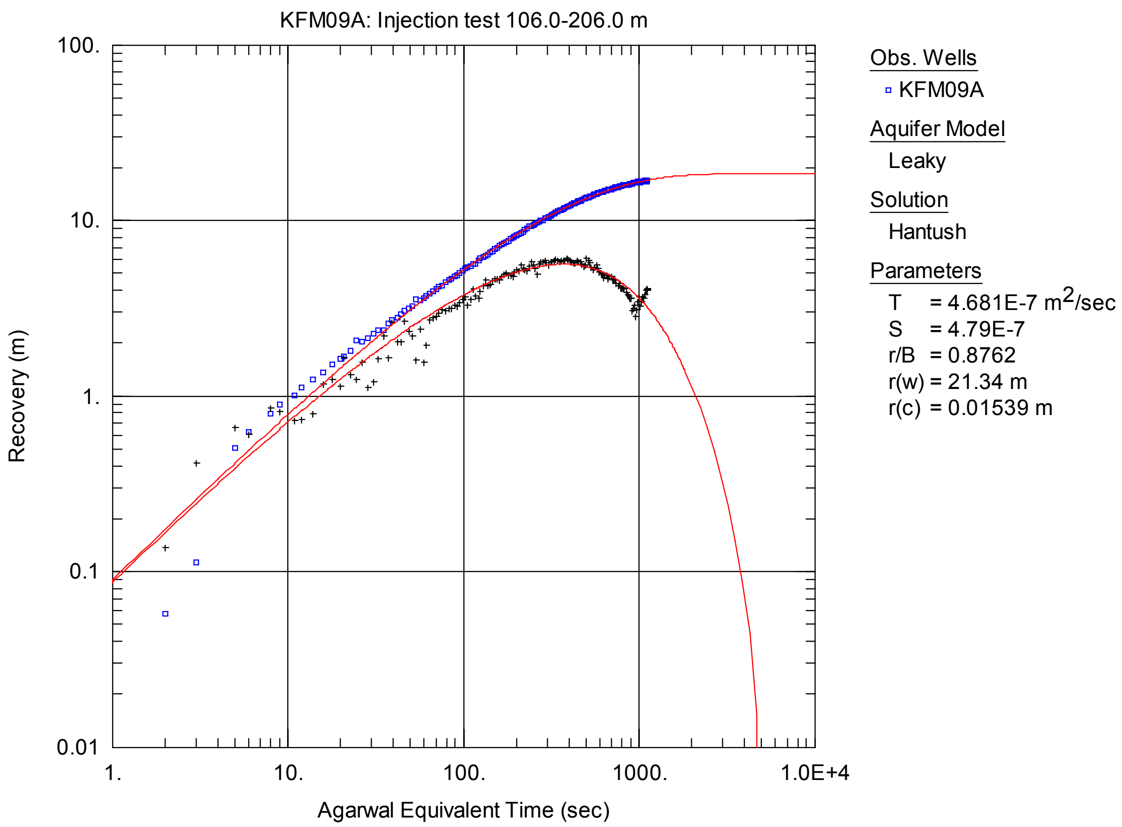


Figure A3-5. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 106.0-206.0 m in KFM09A.*

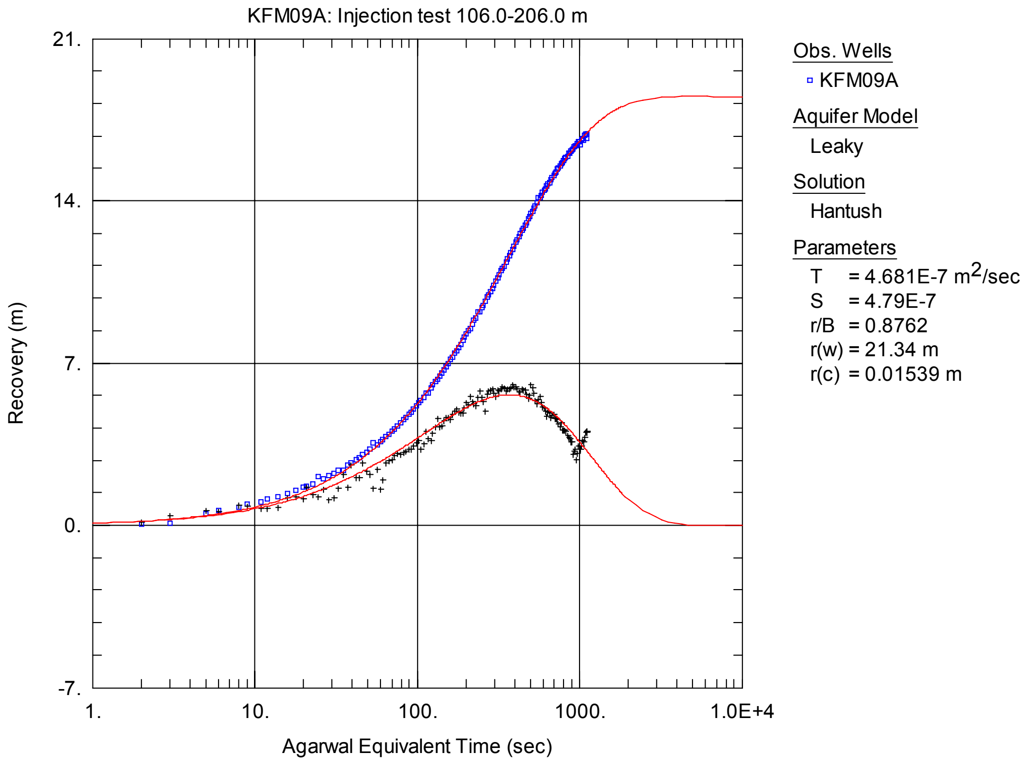


Figure A3-6. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 106.0-206.0 m in KFM09A.*

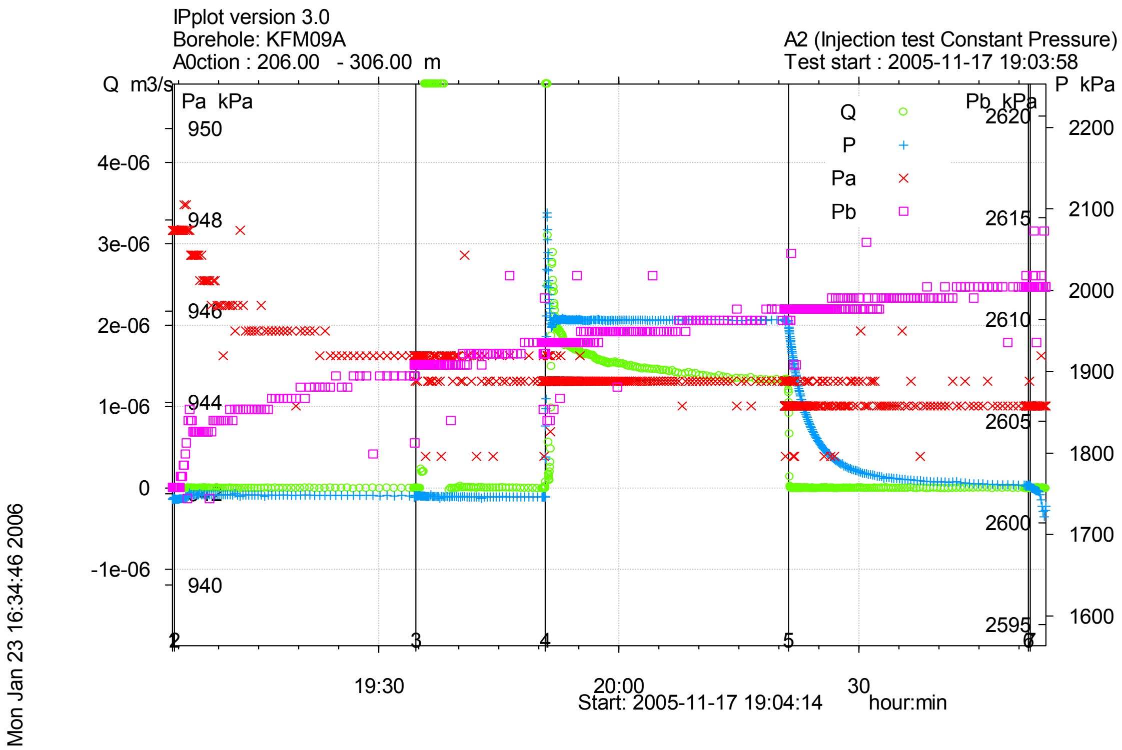


Figure A3-7. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 206.0-306.0 m in borehole KFM09A.*

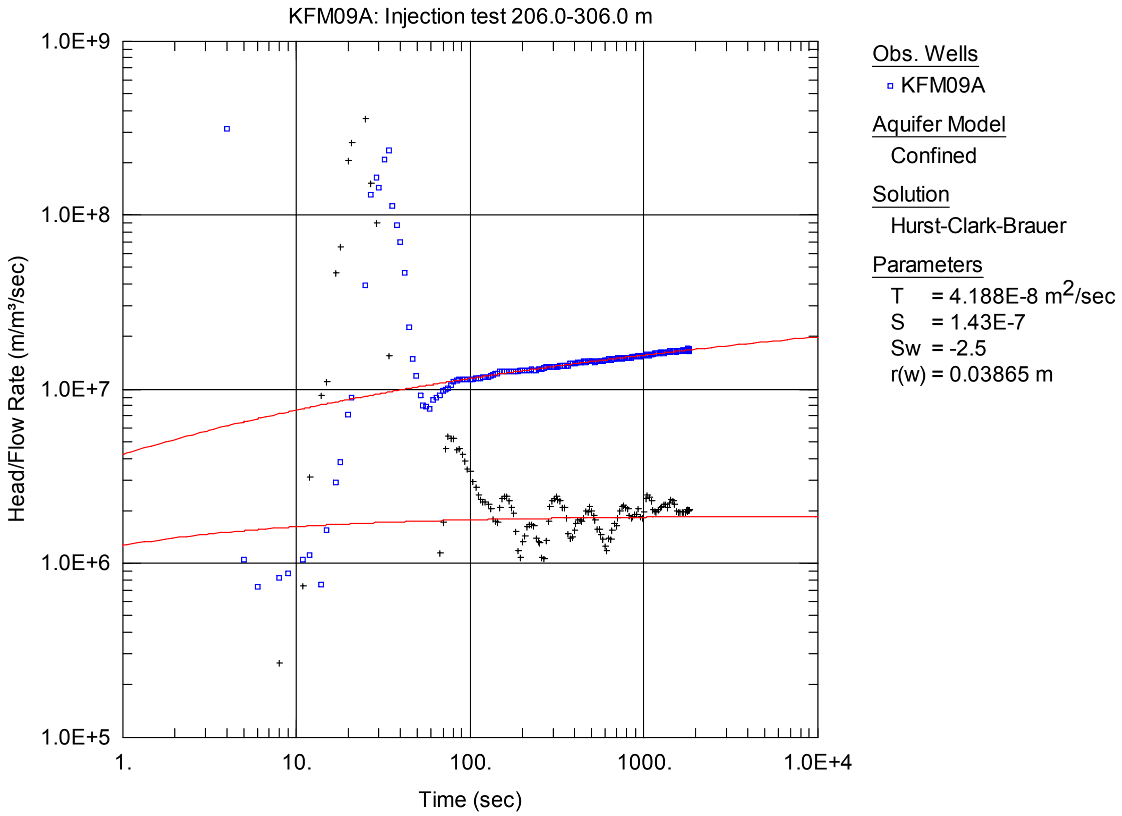


Figure A3-8. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 206.0-306.0 m in KFM09A.*

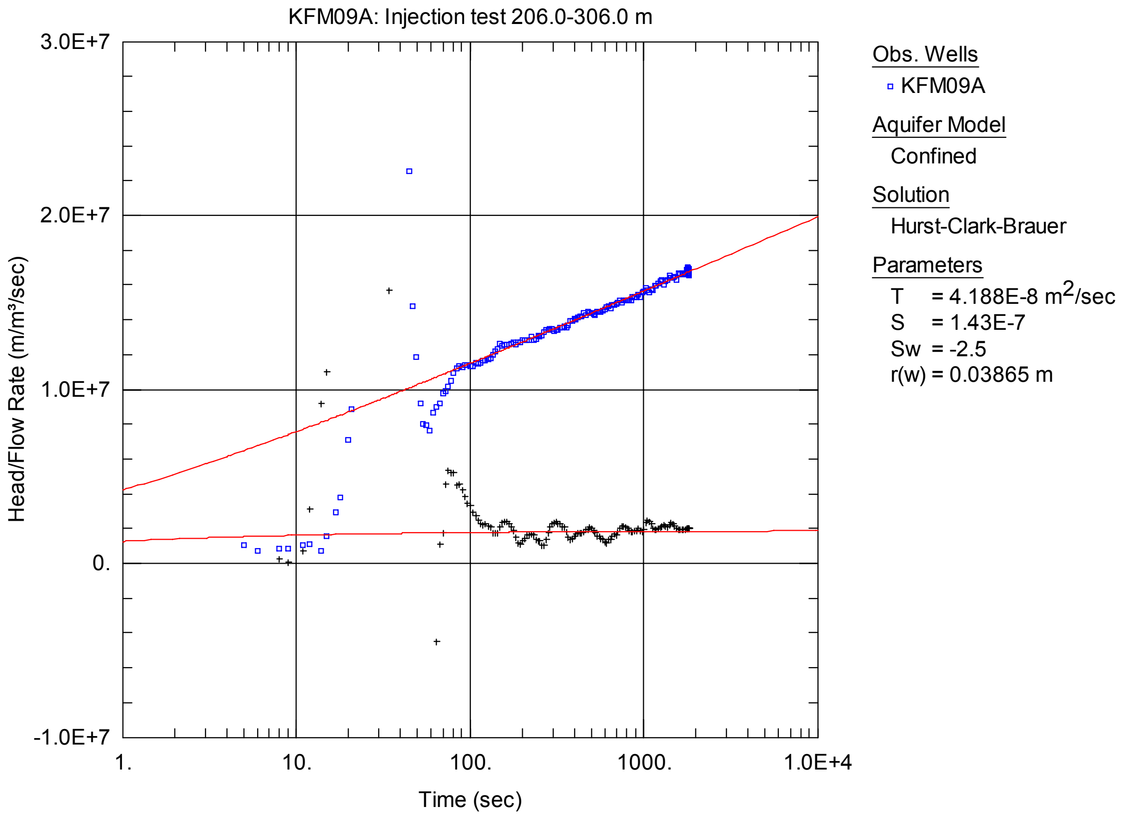


Figure A3-9. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 206.0-306.0 m in KFM09A.*

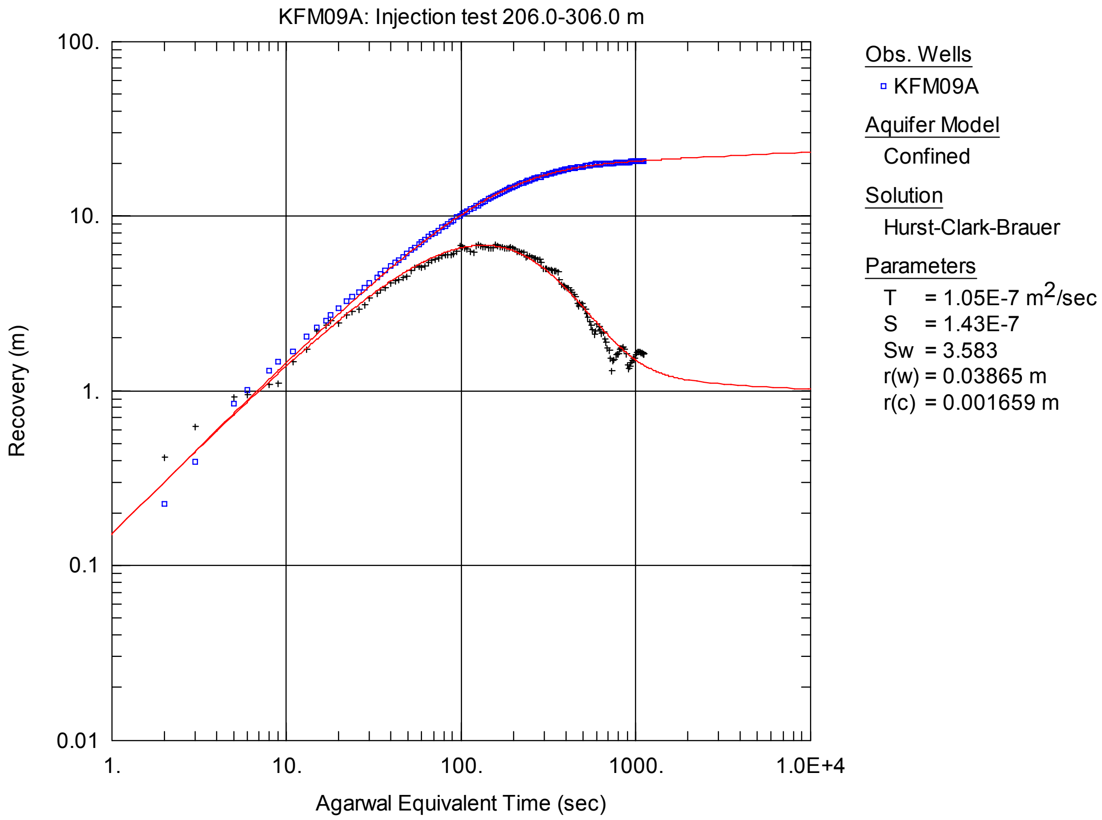


Figure A3-10. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 206.0-306.0 m in KFM09A.*

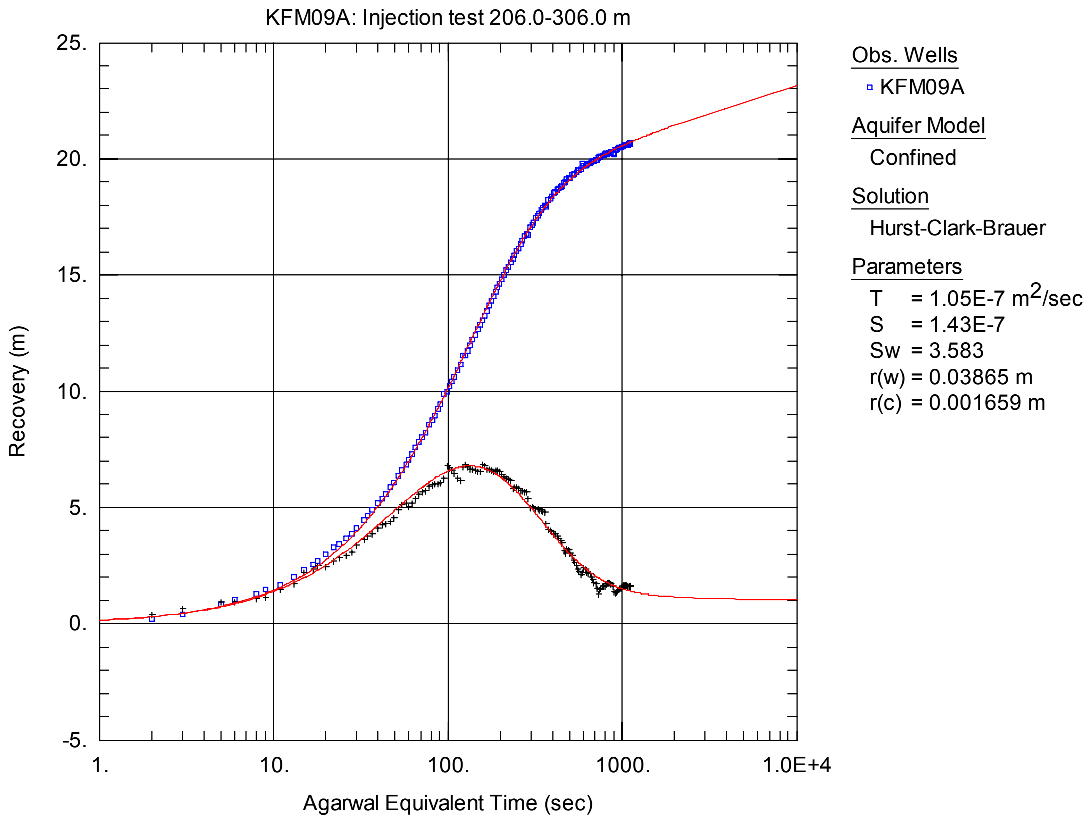


Figure A3-11. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 206.0-306.0 m in KFM09A.*

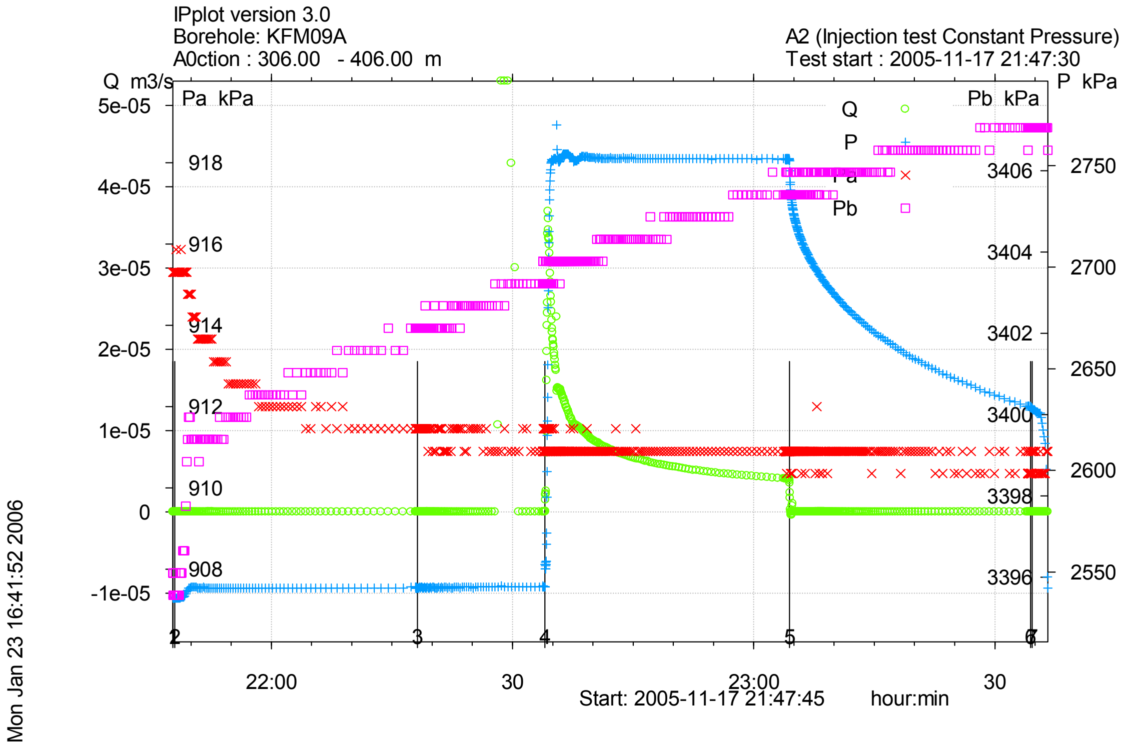


Figure A3-12. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 306.0-406.0 m in borehole KFM09A.*

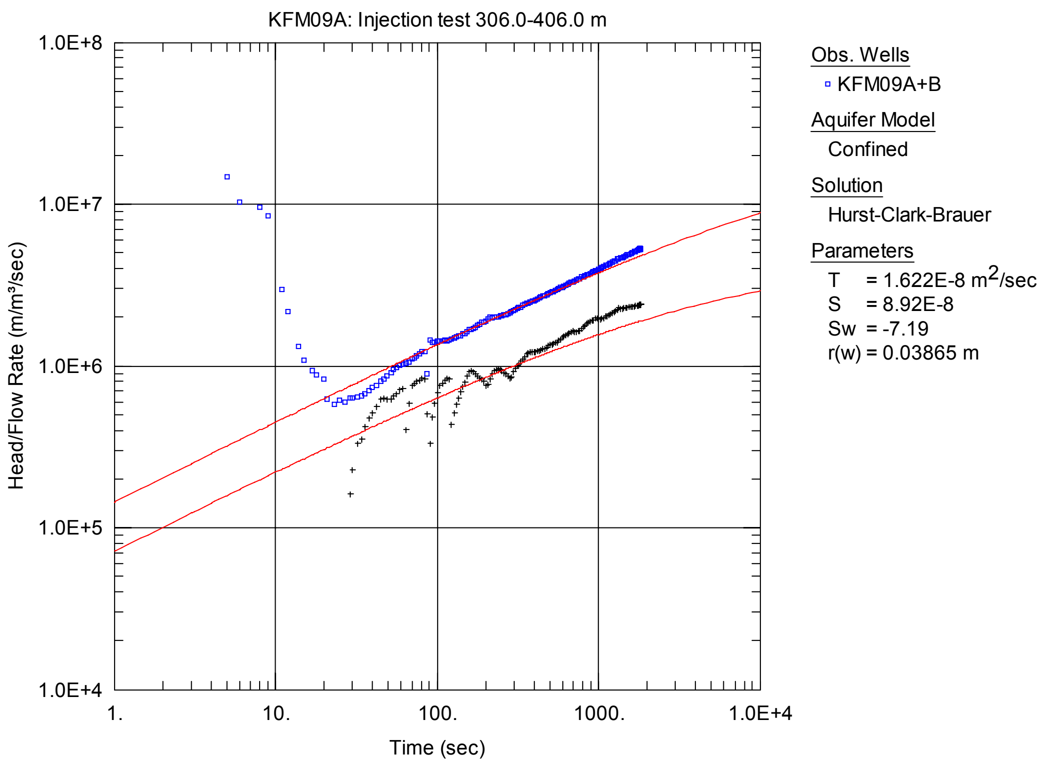


Figure A3-13. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 306.0-406.0 m in KFM09A.*

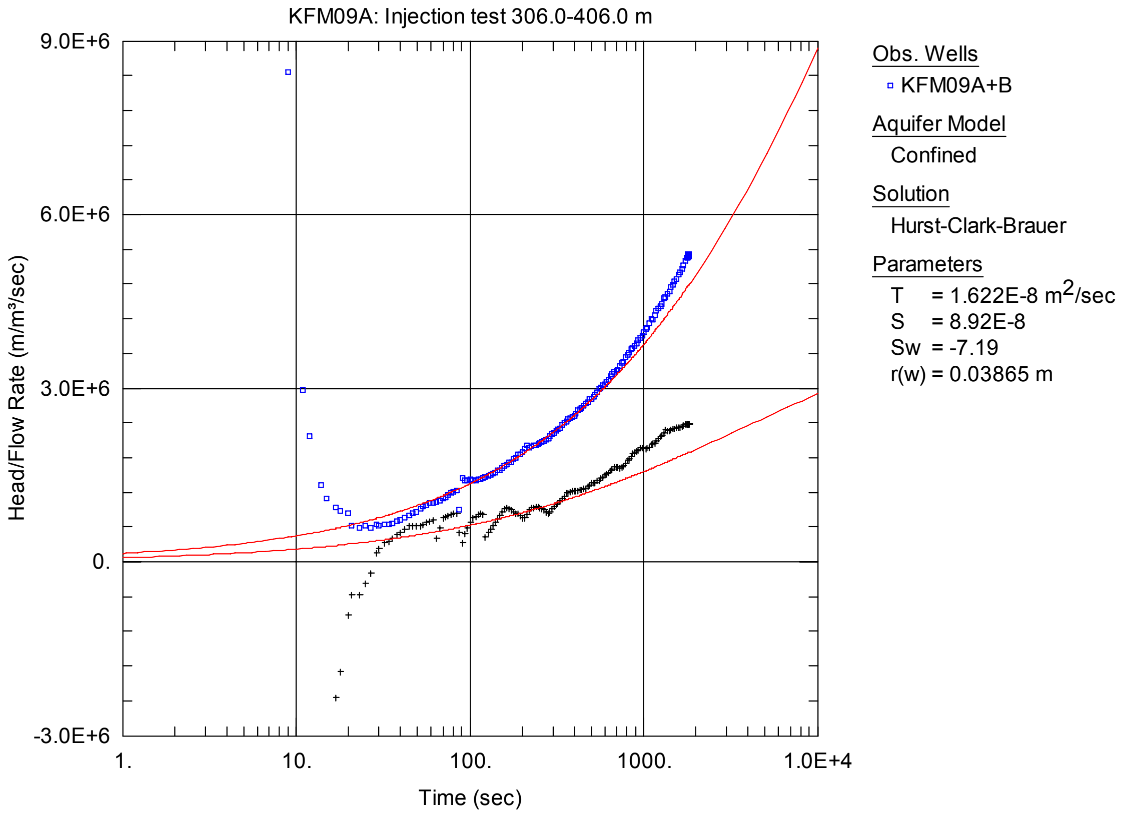


Figure A3-14. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 306.0-406.0 m in KFM09A.*

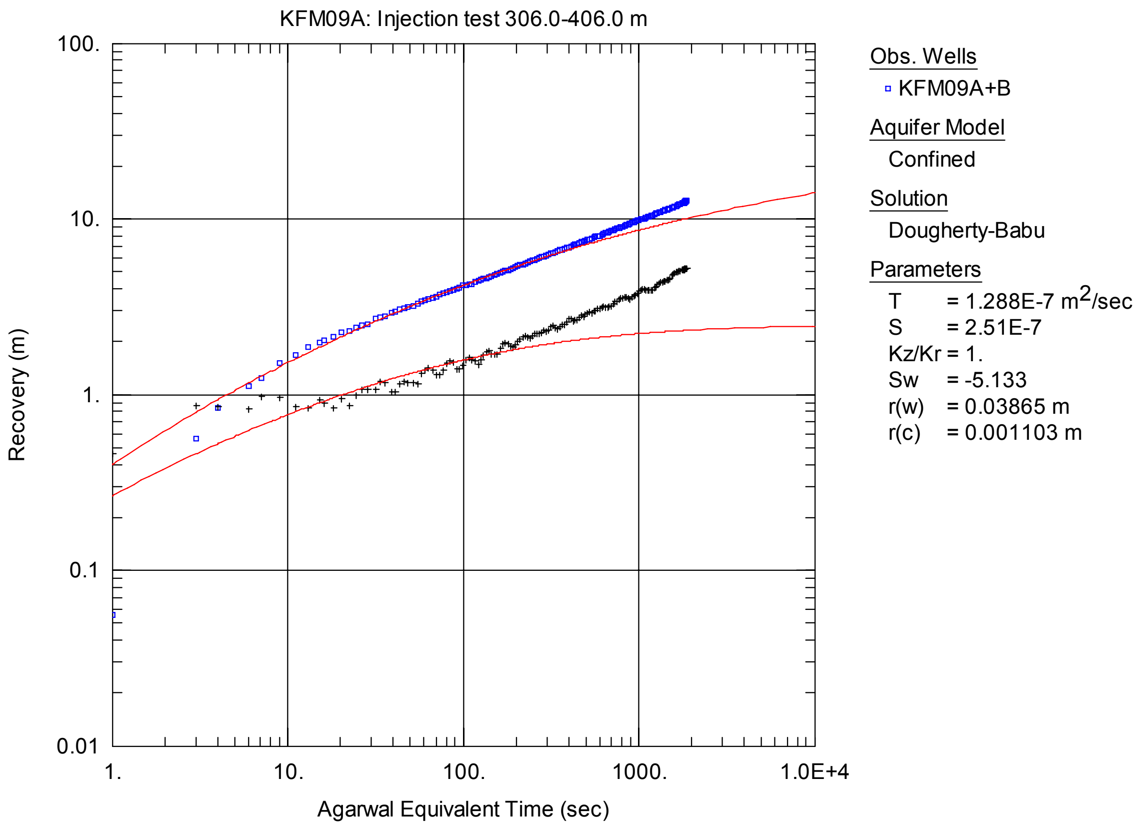


Figure A3-15. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 306.0-406.0x m in KFM09A.*

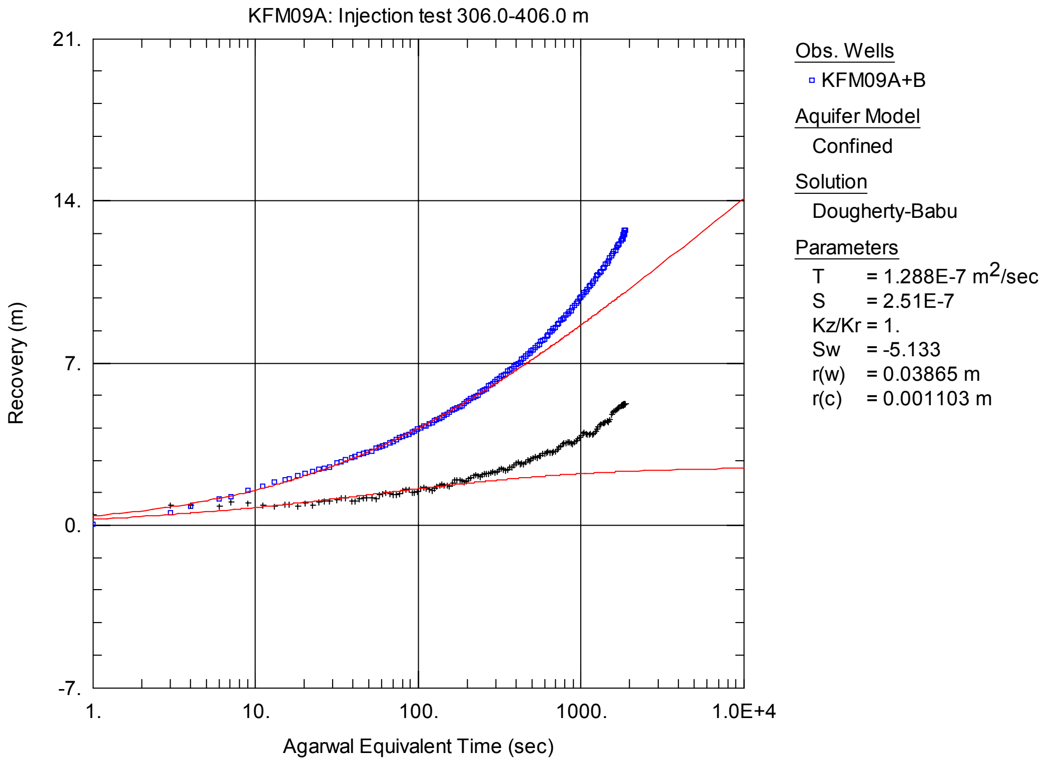


Figure A3-16. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 306.0-406.0 m in KFM09A.*

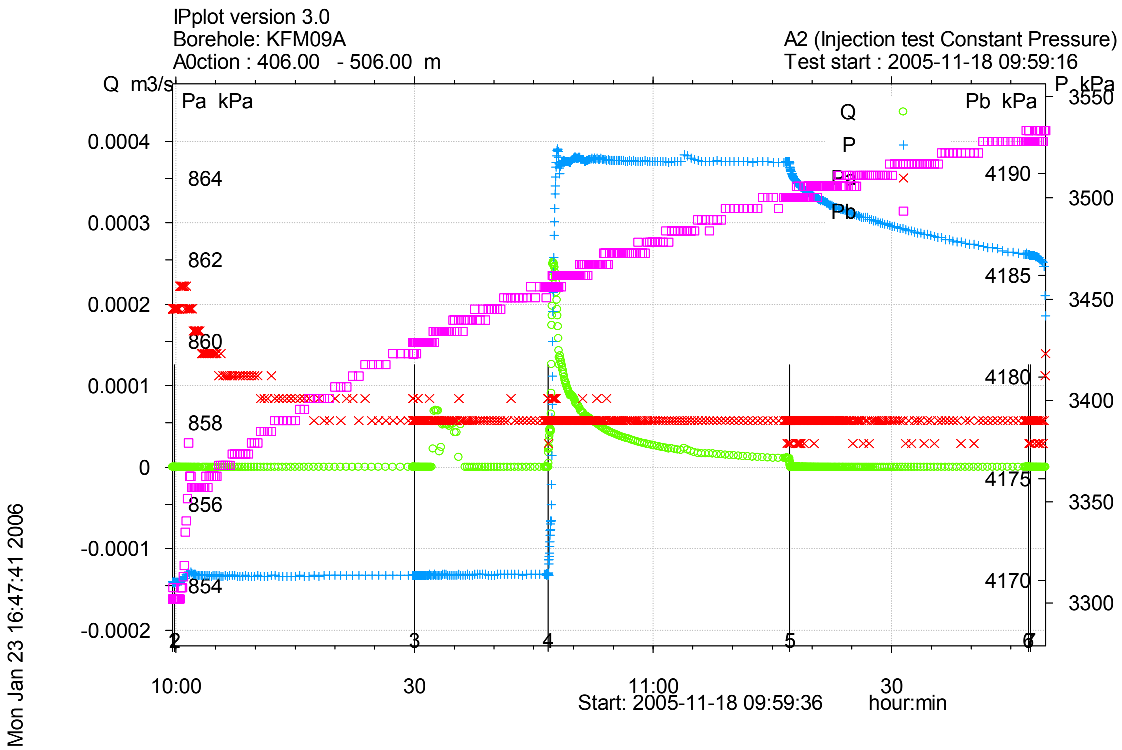


Figure A3-17. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 406.0-506.0 m in borehole KFM09A.*

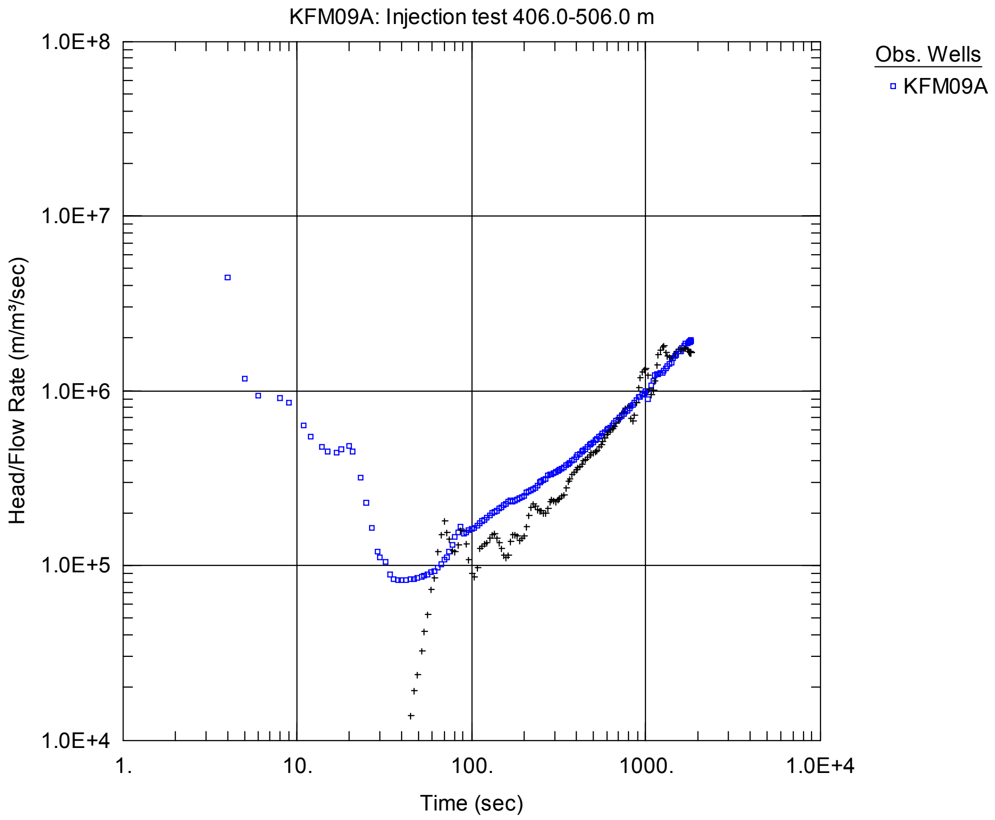


Figure A3-18. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 406.0-506.0 m in KFM09A.*

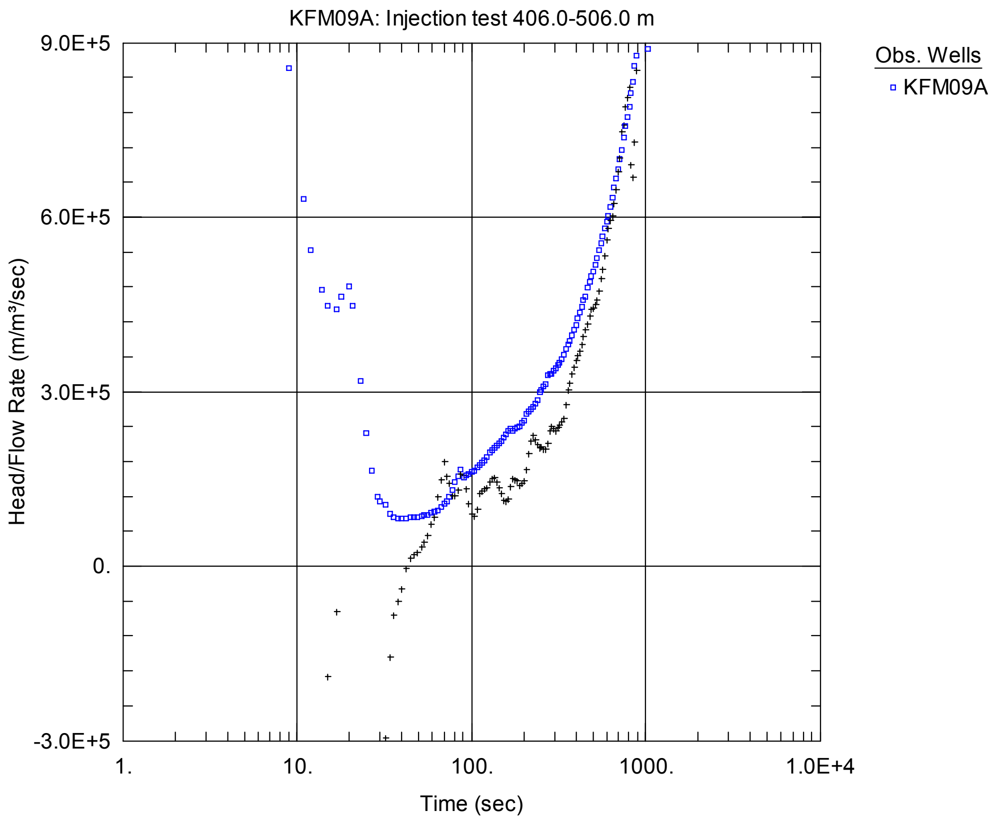


Figure A3-19. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 406.0-506.0 m in KFM09A.*

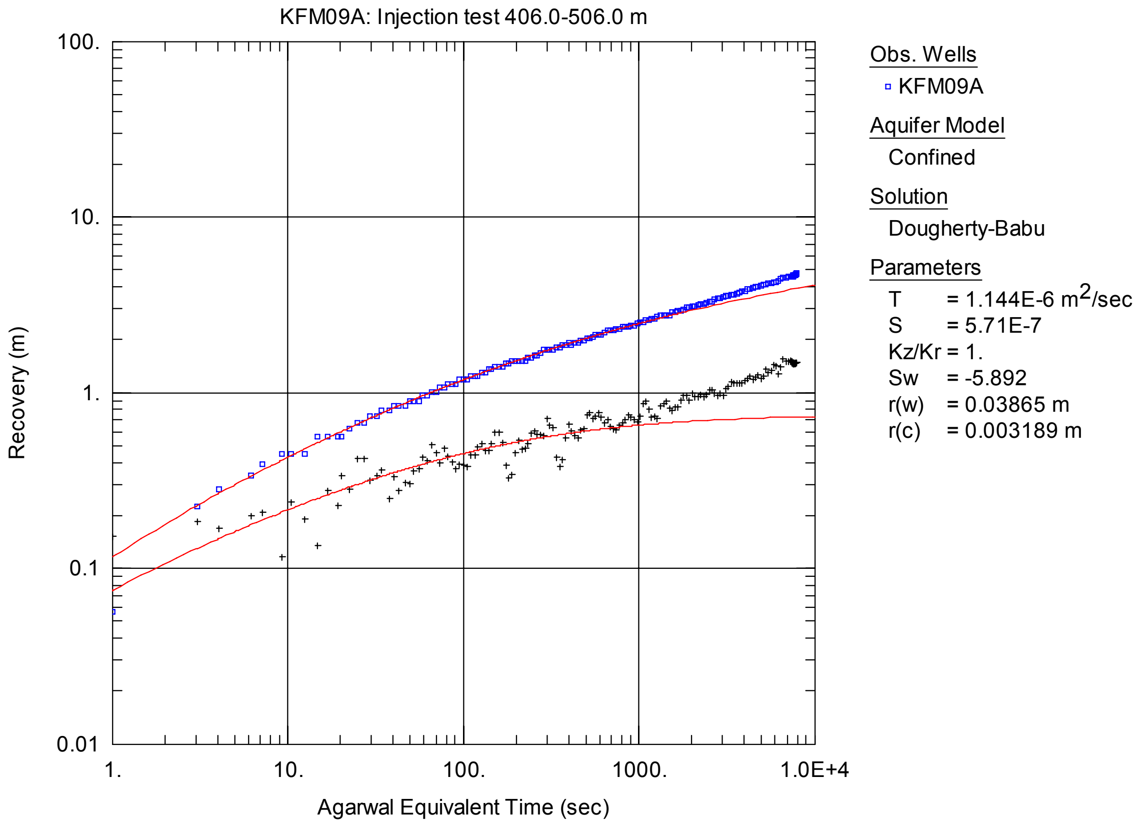


Figure A3-20. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 406.0-506.0 m in KFM09A.*

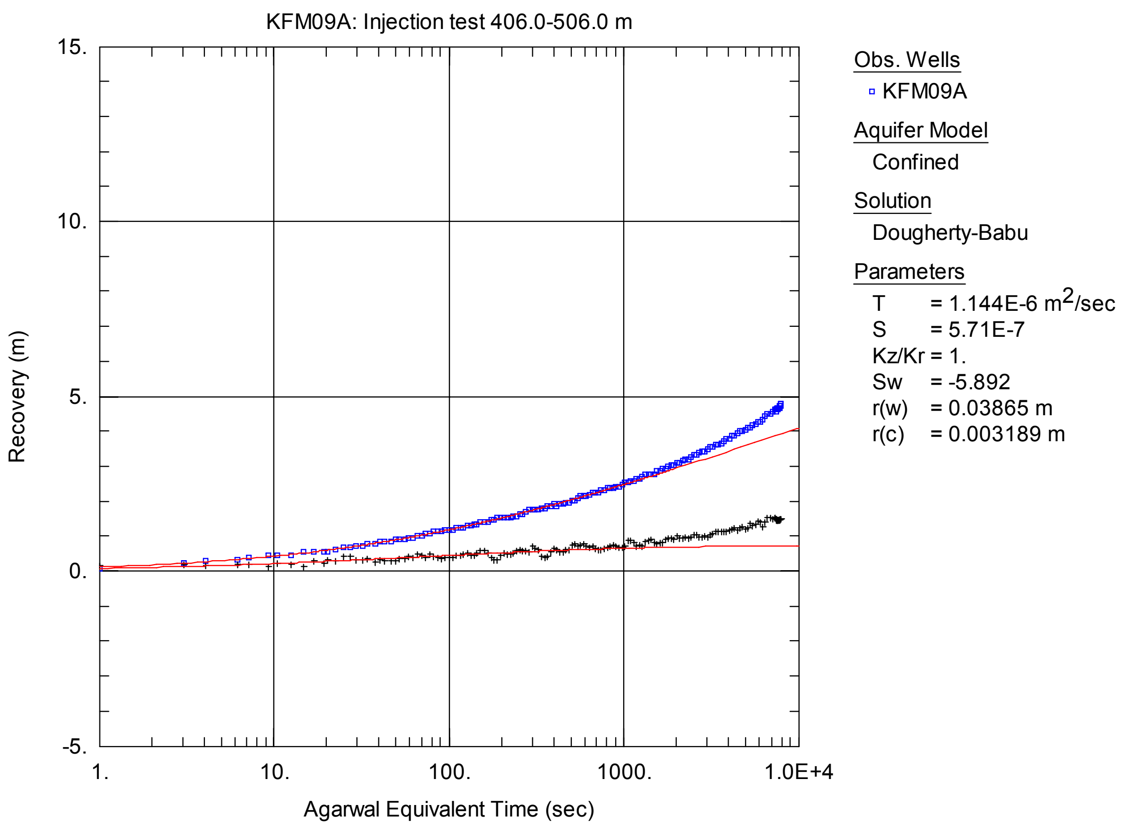


Figure A3-21. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 406.0-506.0 m in KFM09A.*

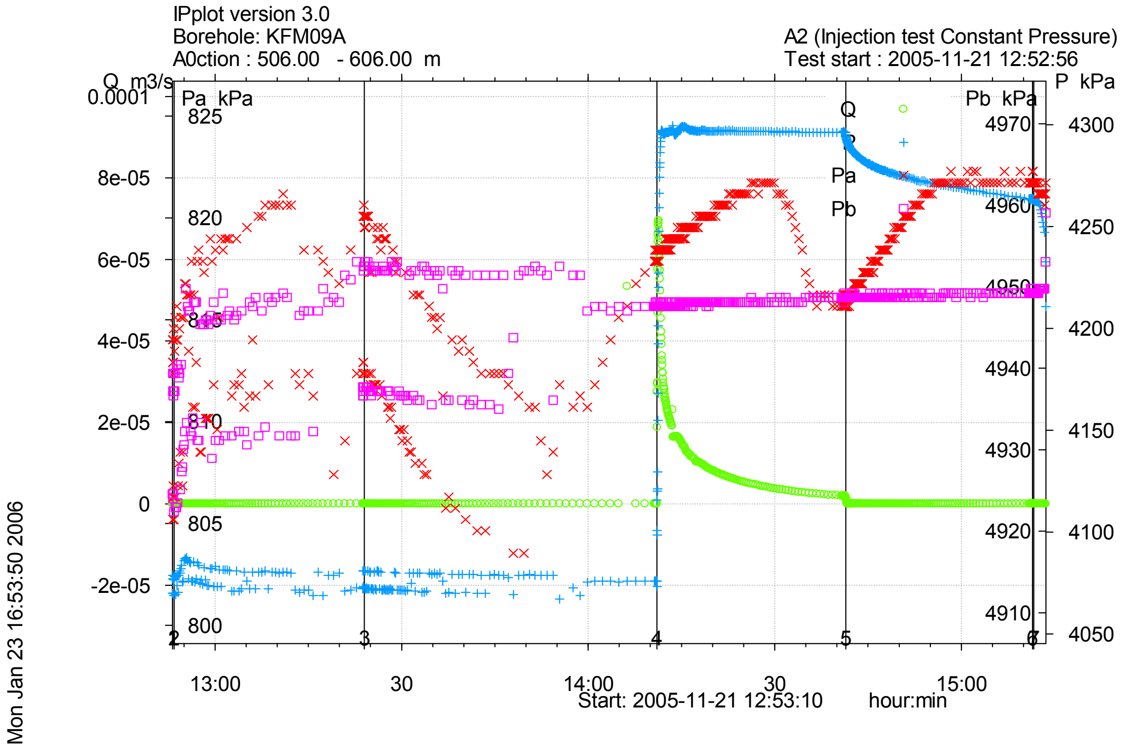


Figure A3-22. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 506.0-606.0 m in borehole KFM09A.*

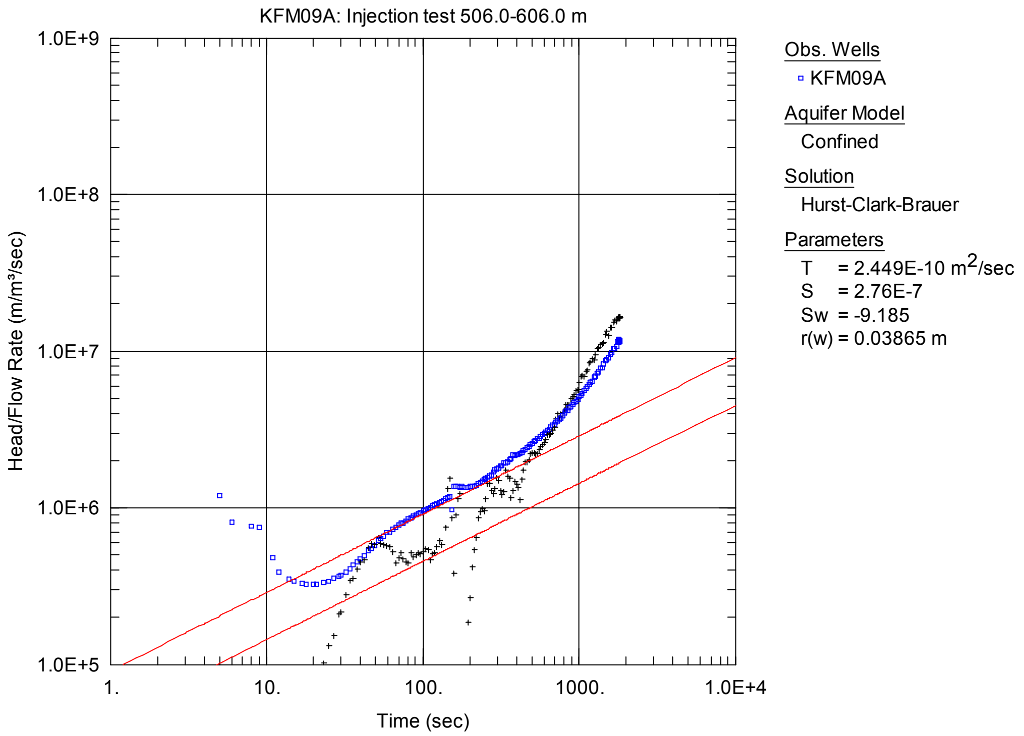


Figure A3-23. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 506.0-606.0 m in KFM09A. No unambiguous transit evaluation of transmissivity on this period is possible.*

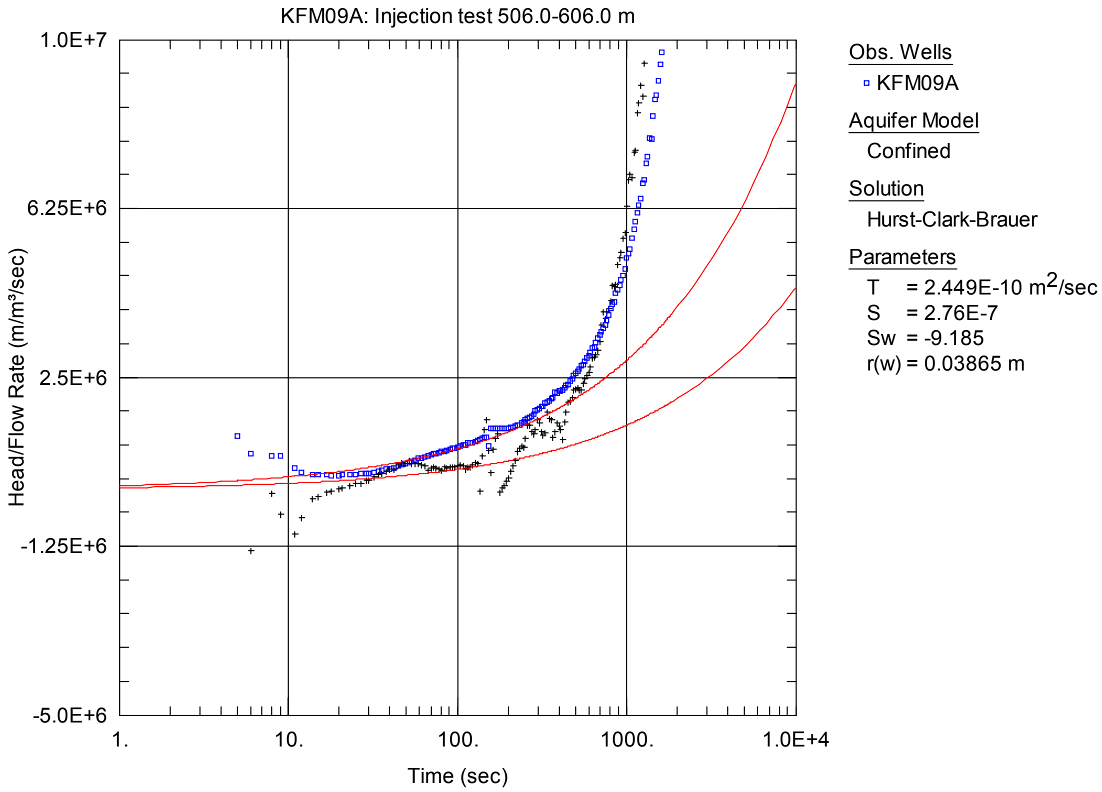


Figure A3-24. Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 506.0-606.0 m in KFM09A. No unambiguous transit evaluation of transmissivity on this period is possible.

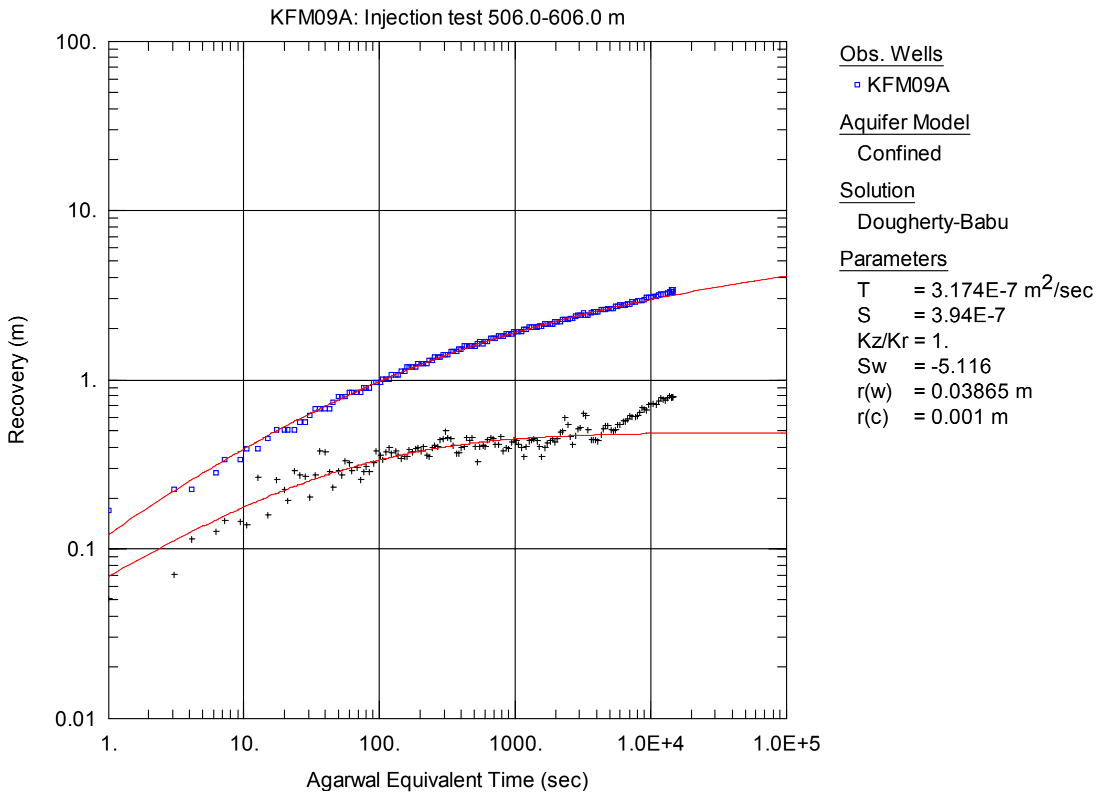


Figure A3-25. Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 506.0-606.0 m in KFM09A.

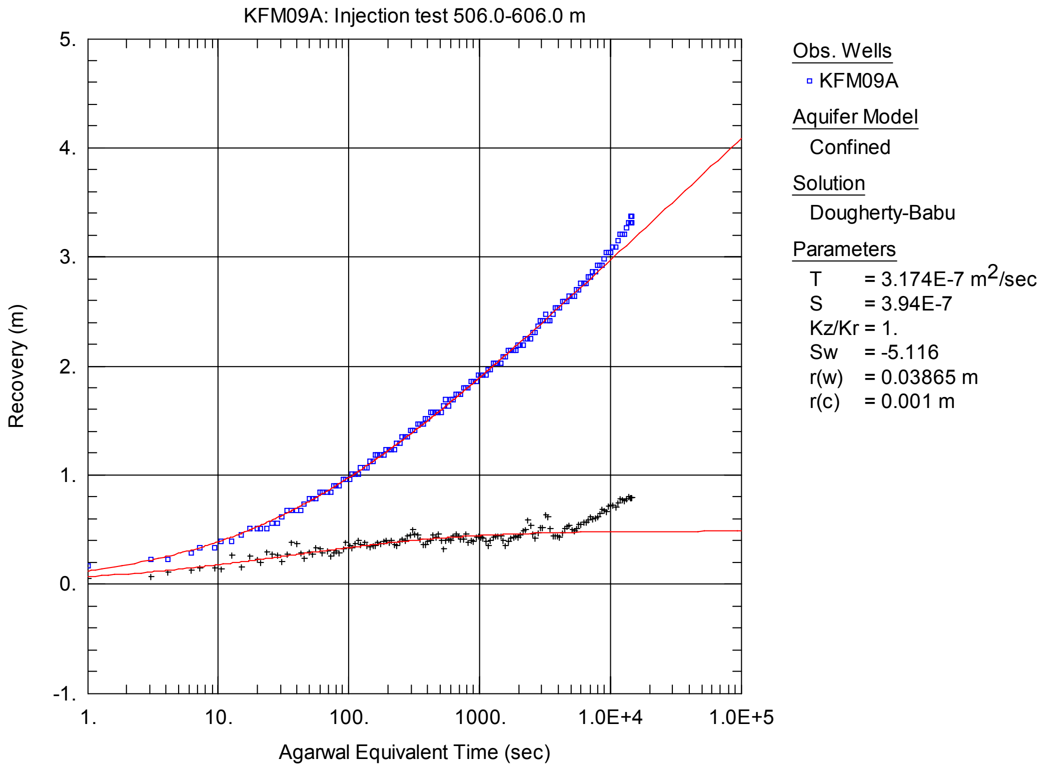


Figure A3-26. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 506.0-606.0 m in KFM09A.*

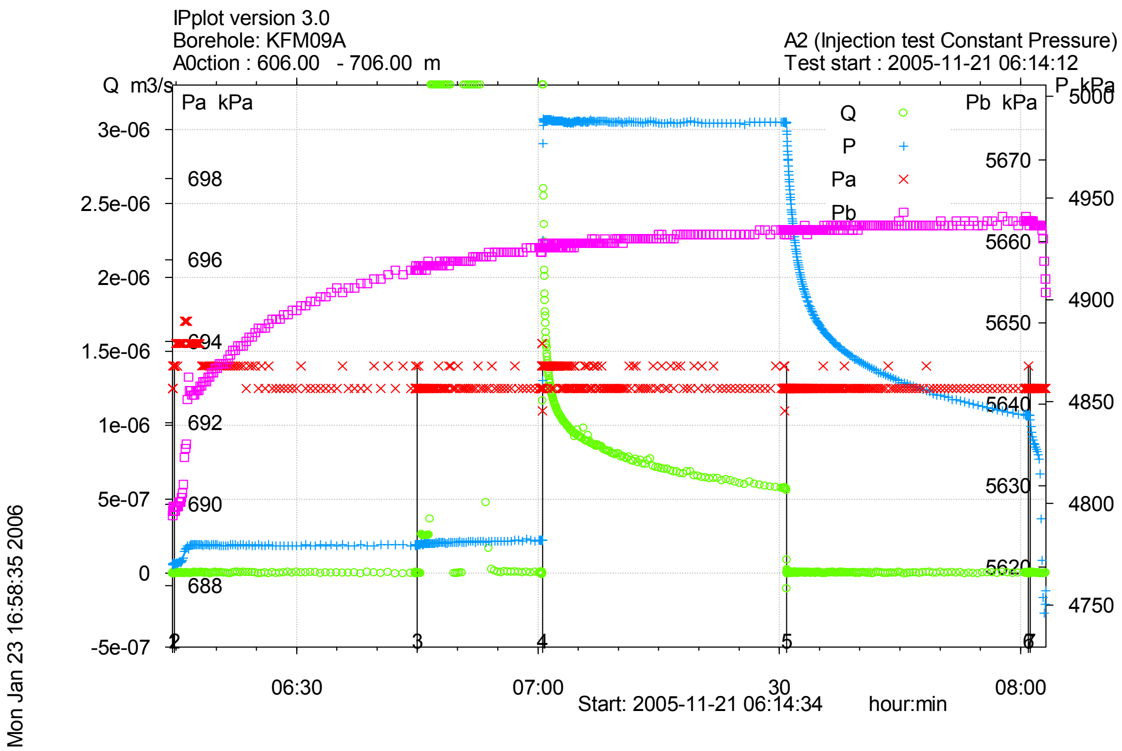


Figure A3-27. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 606.0-706.0 m in borehole KFM09A.*

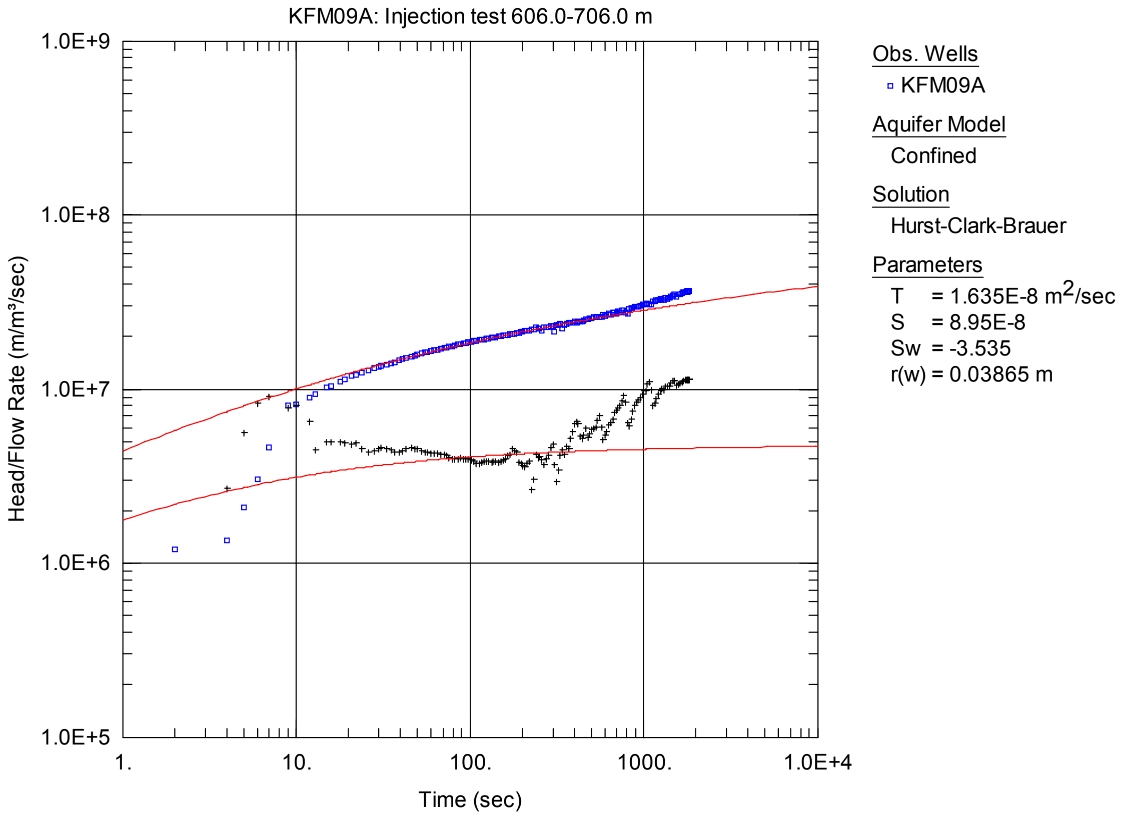


Figure A3-28. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 606.0-706.0 m in KFM09A.*

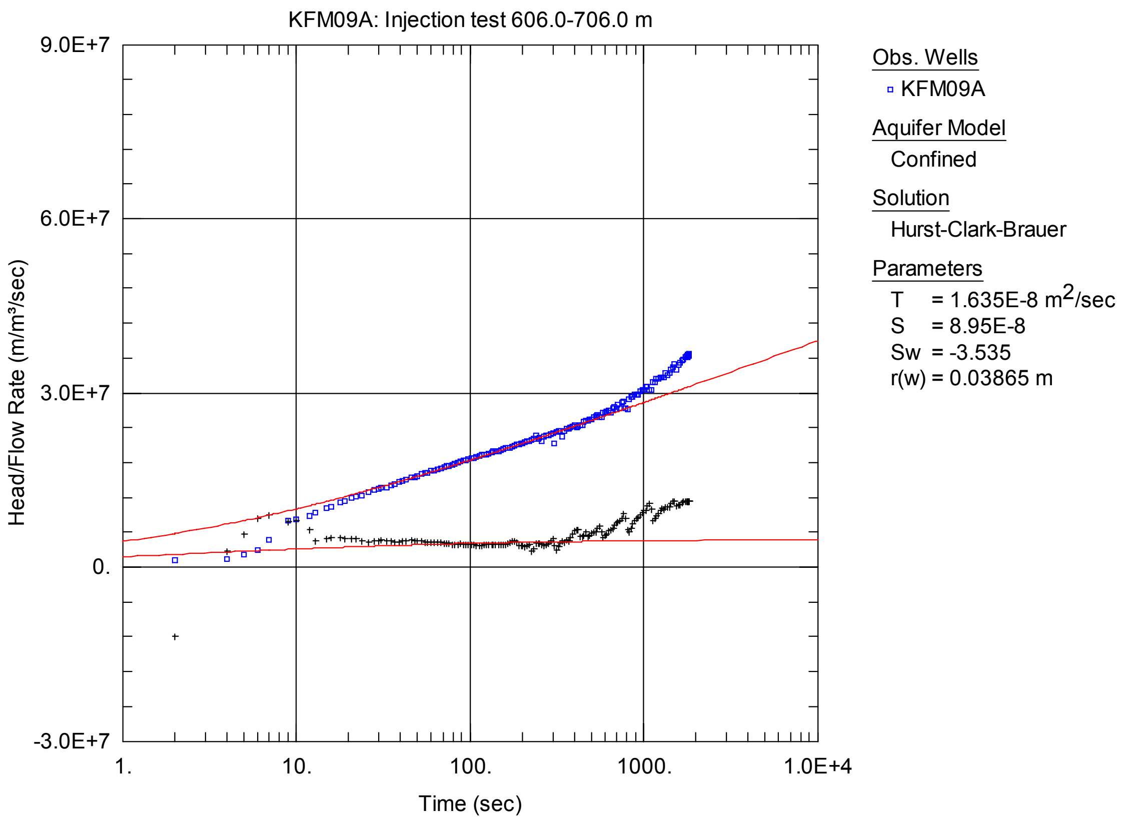


Figure A3-29. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 606.0-706.0 m in KFM09A.*

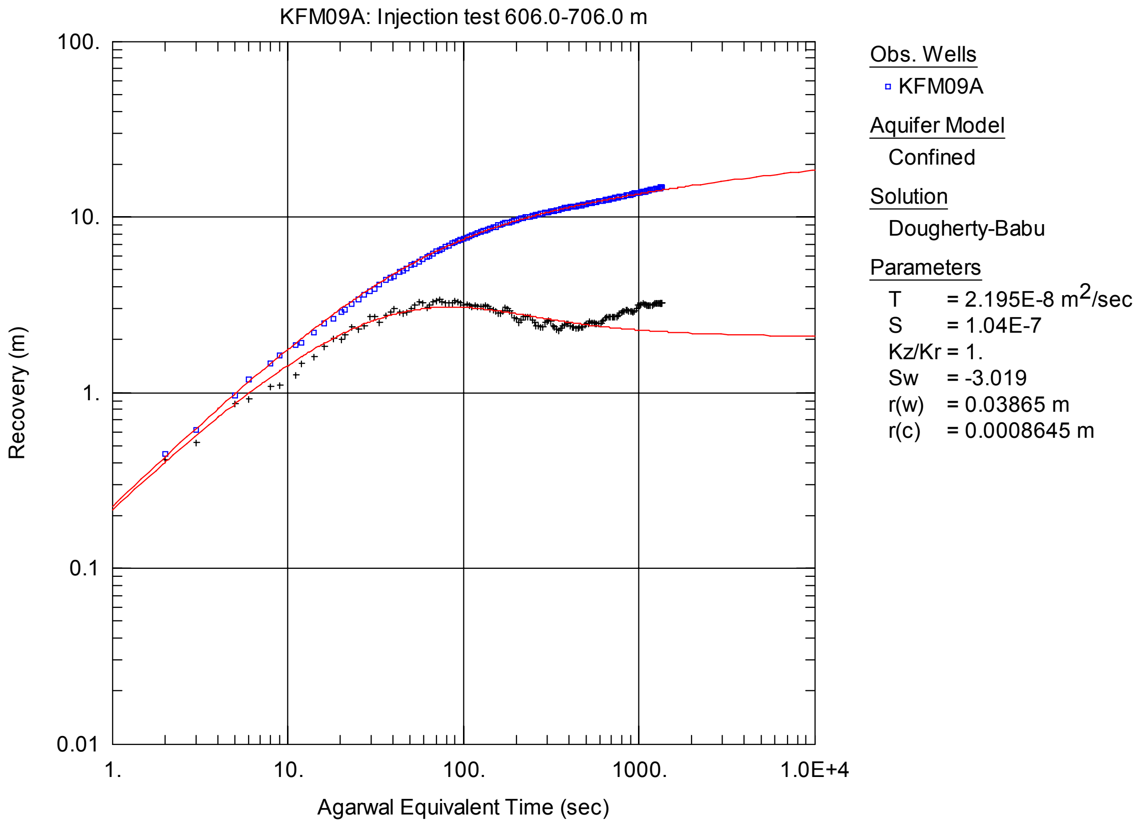


Figure A3-30. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 606.0-706.0 m in KFM09A.*

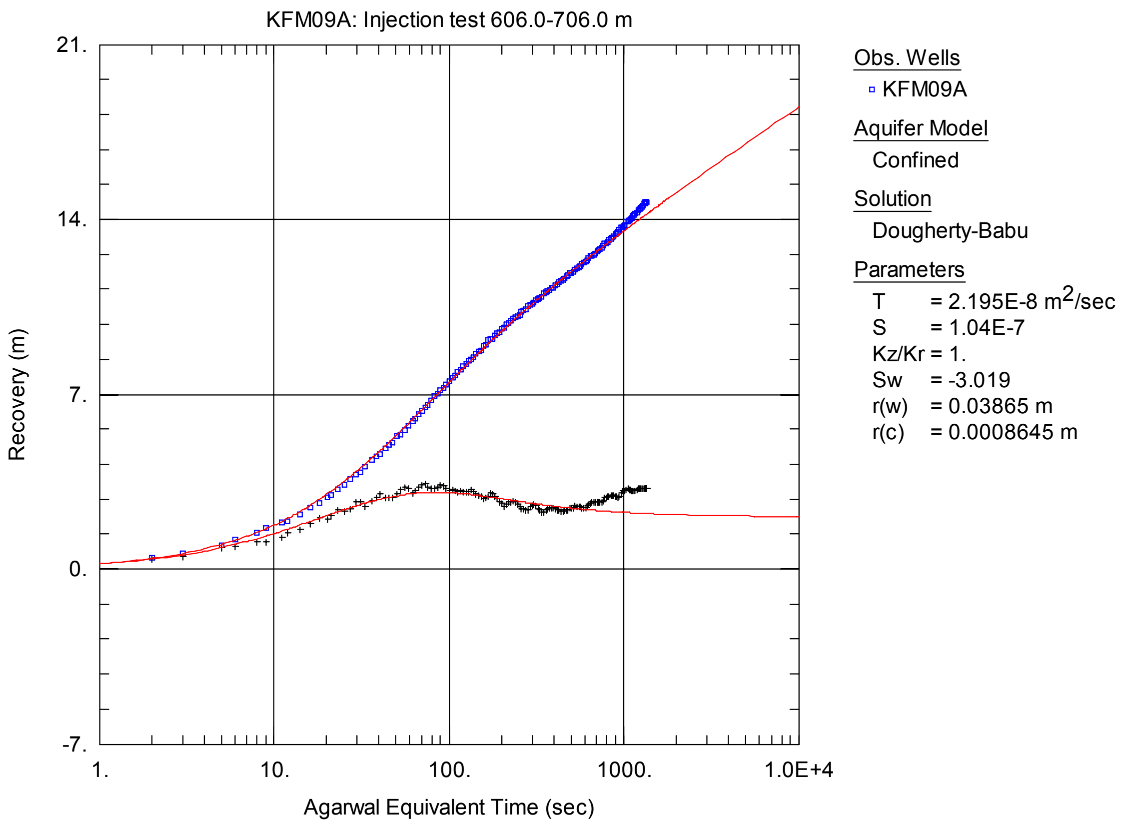


Figure A3-31. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 606.0-706.0 m in KFM09A.*

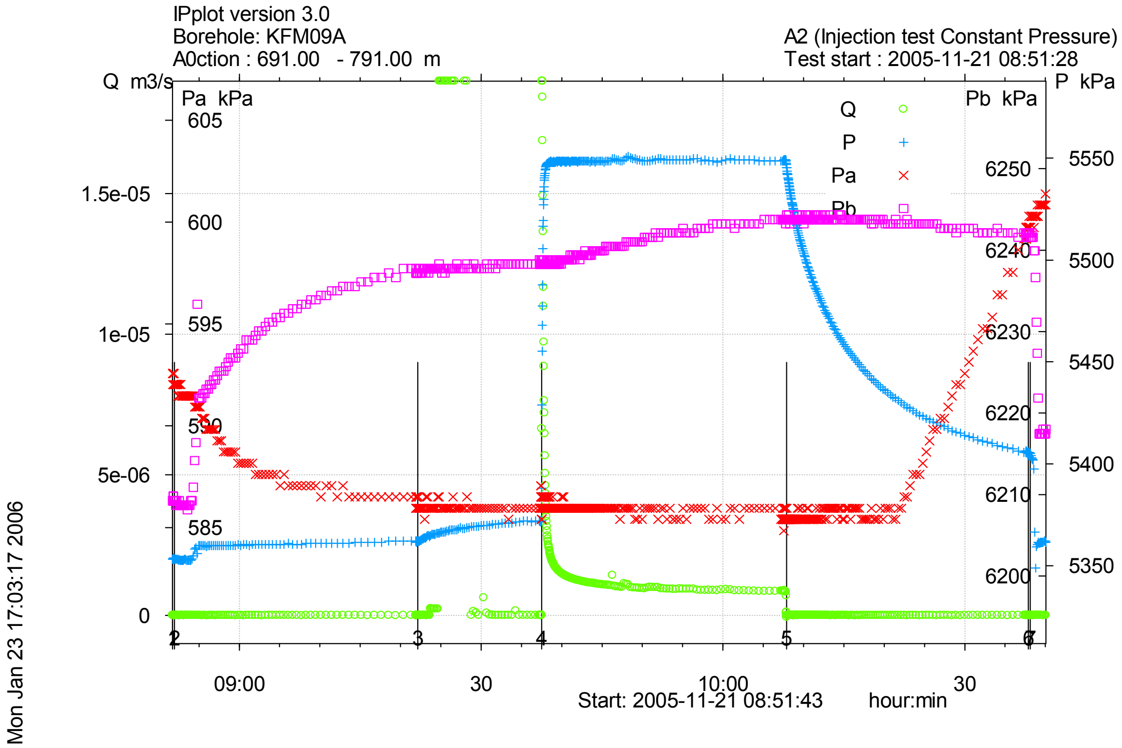


Figure A3-32. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 691.0-791.0 m in borehole KFM09A.

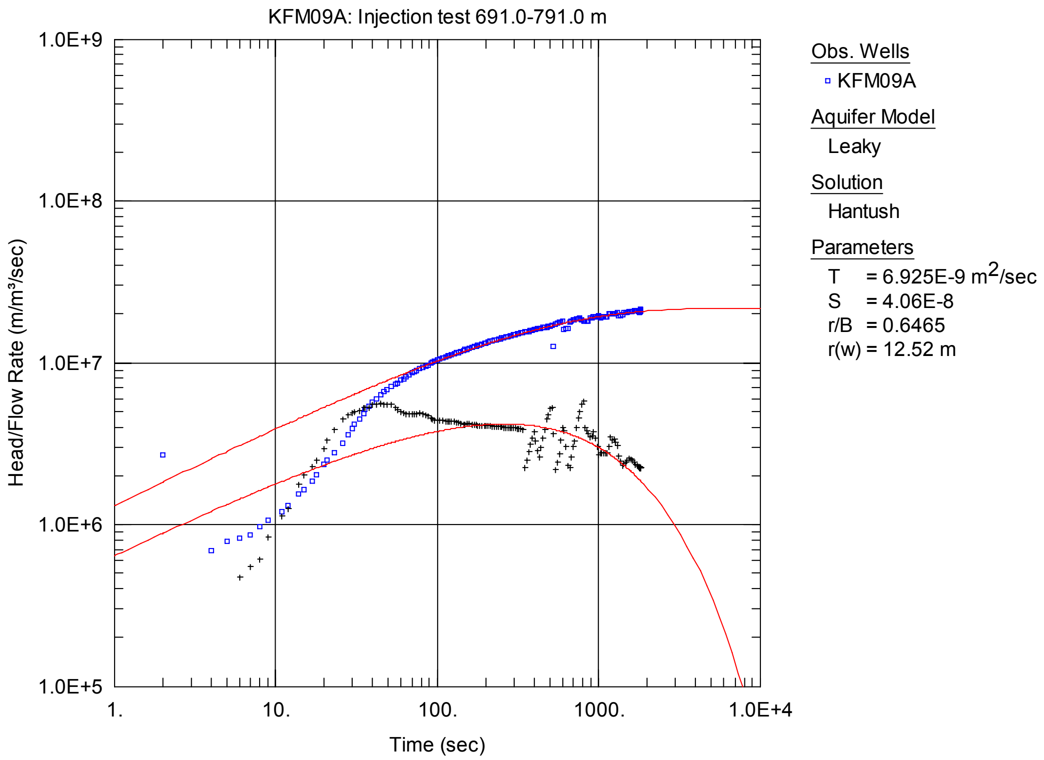


Figure A3-33. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 691.0-791.0 m in KFM09A.

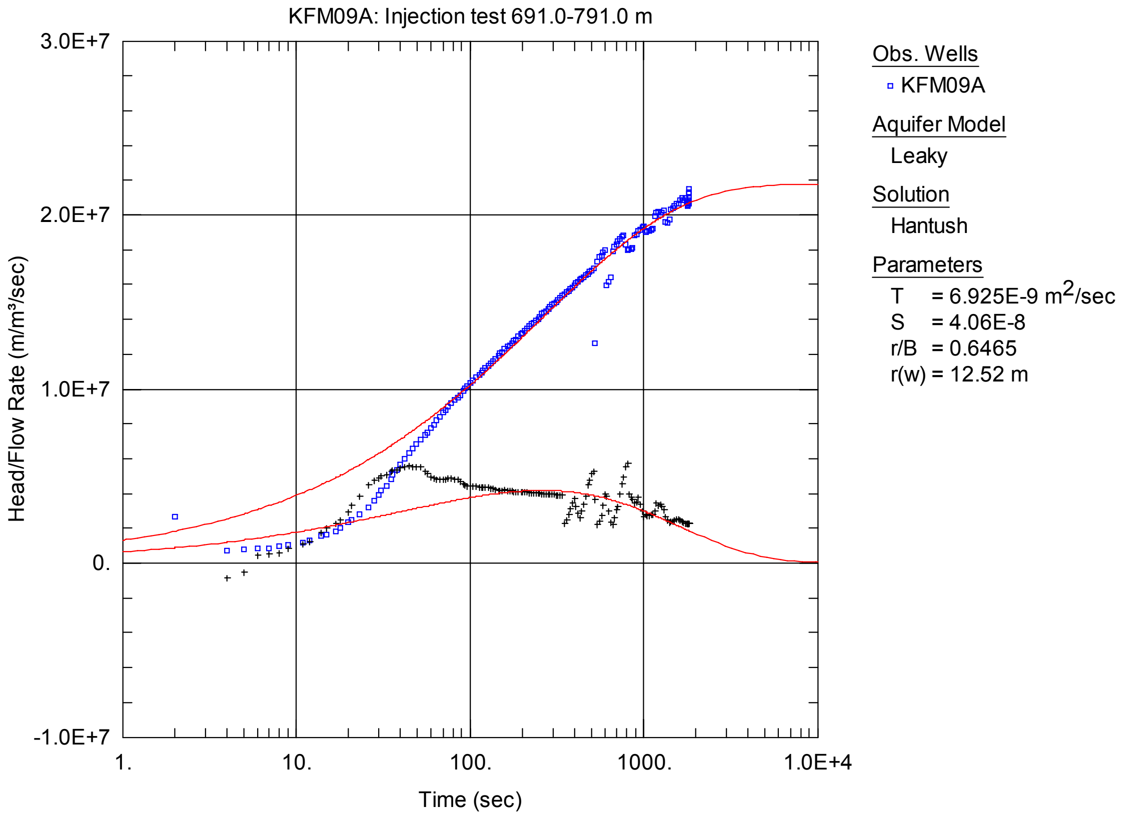


Figure A3-34. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 691.0-791.0 m in KFM09A.*

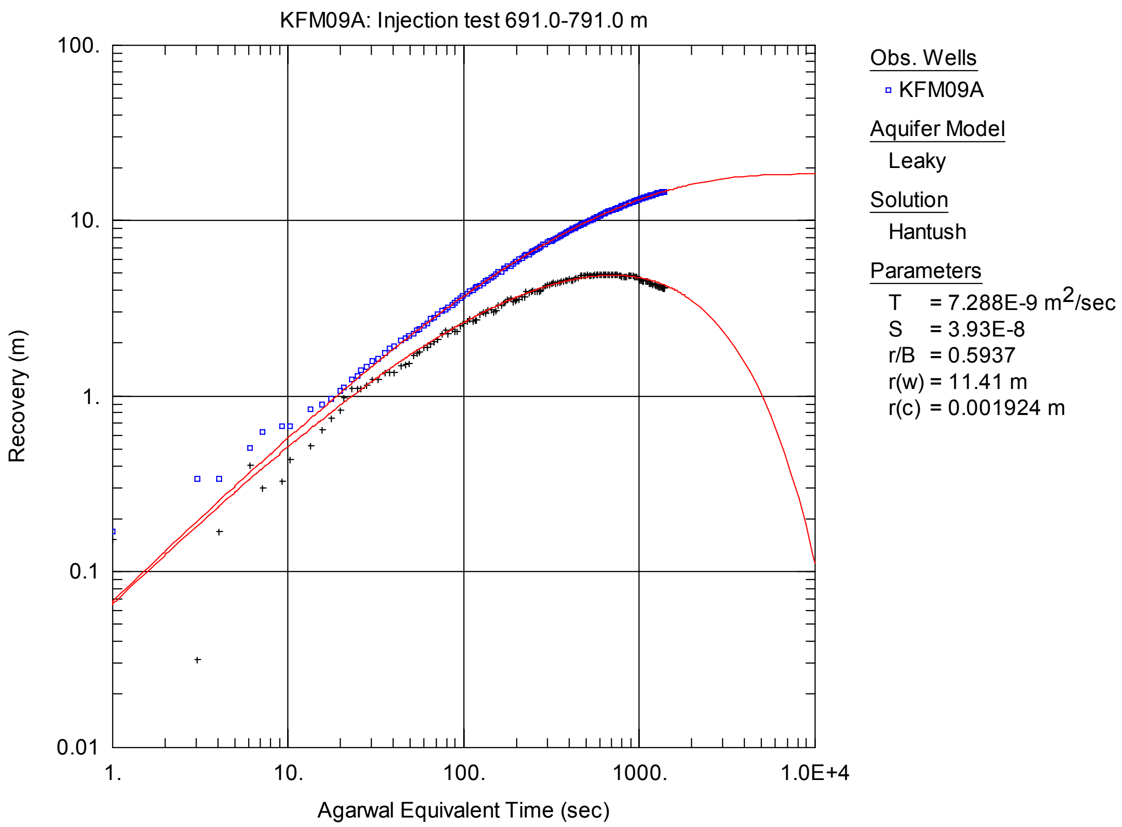


Figure A3-35. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 691.0-791.0 m in KFM09A.*

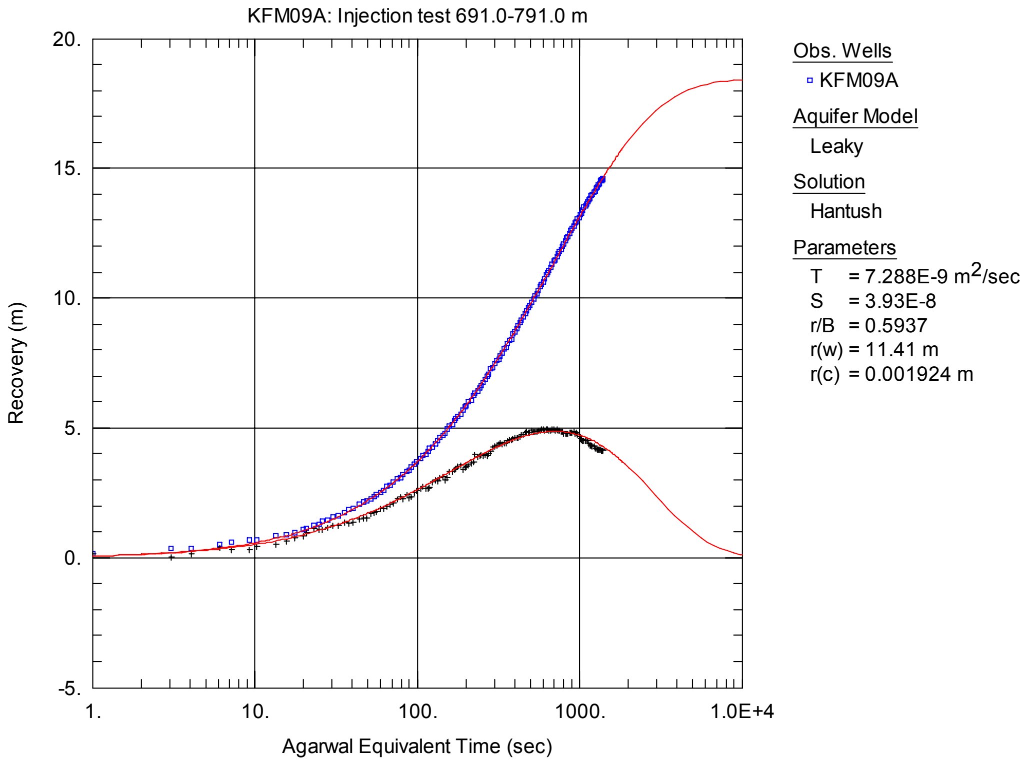


Figure A3-36. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 691.0-791.0 m in KFM09A.*

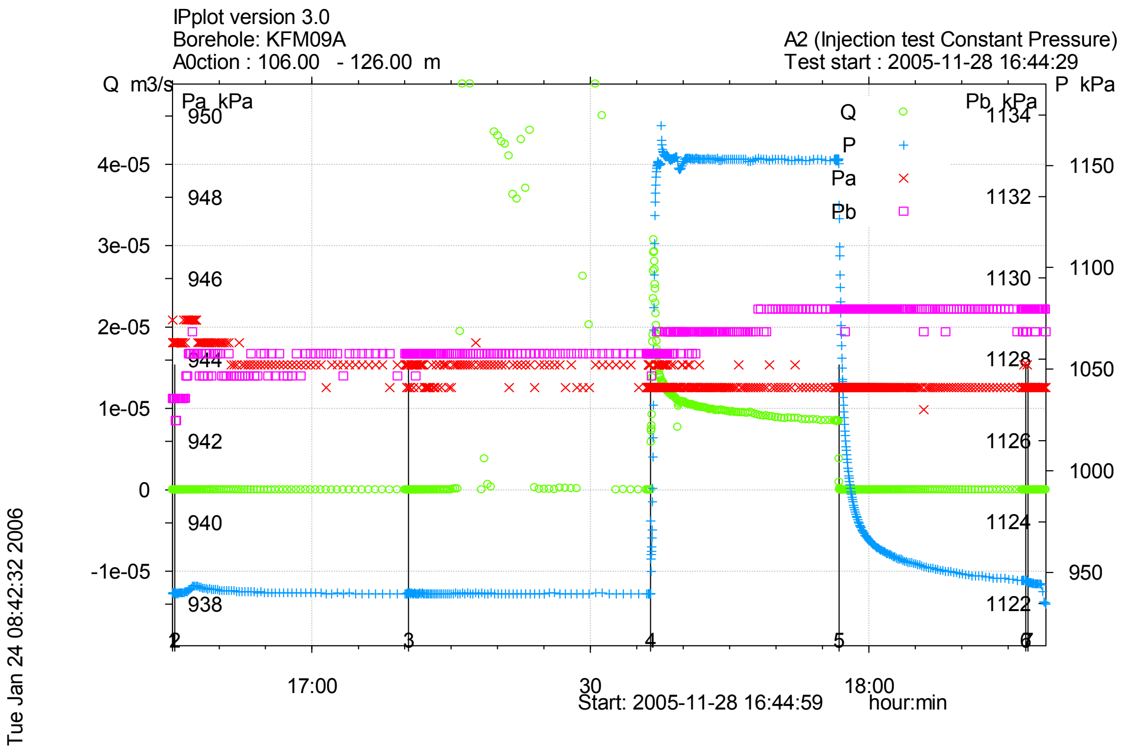


Figure A3-37. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 106.0-126.0 m in borehole KFM09A.*

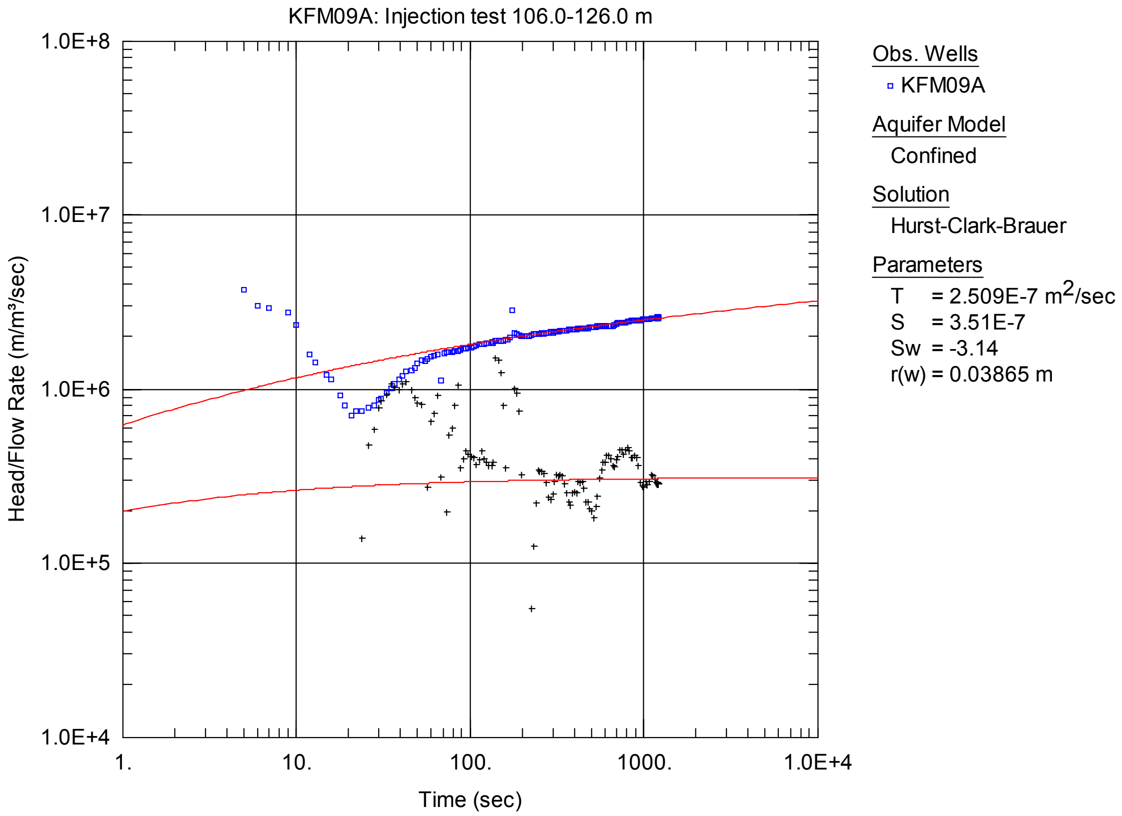


Figure A3-38. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 106.0-126.0 m in KFM09A.*

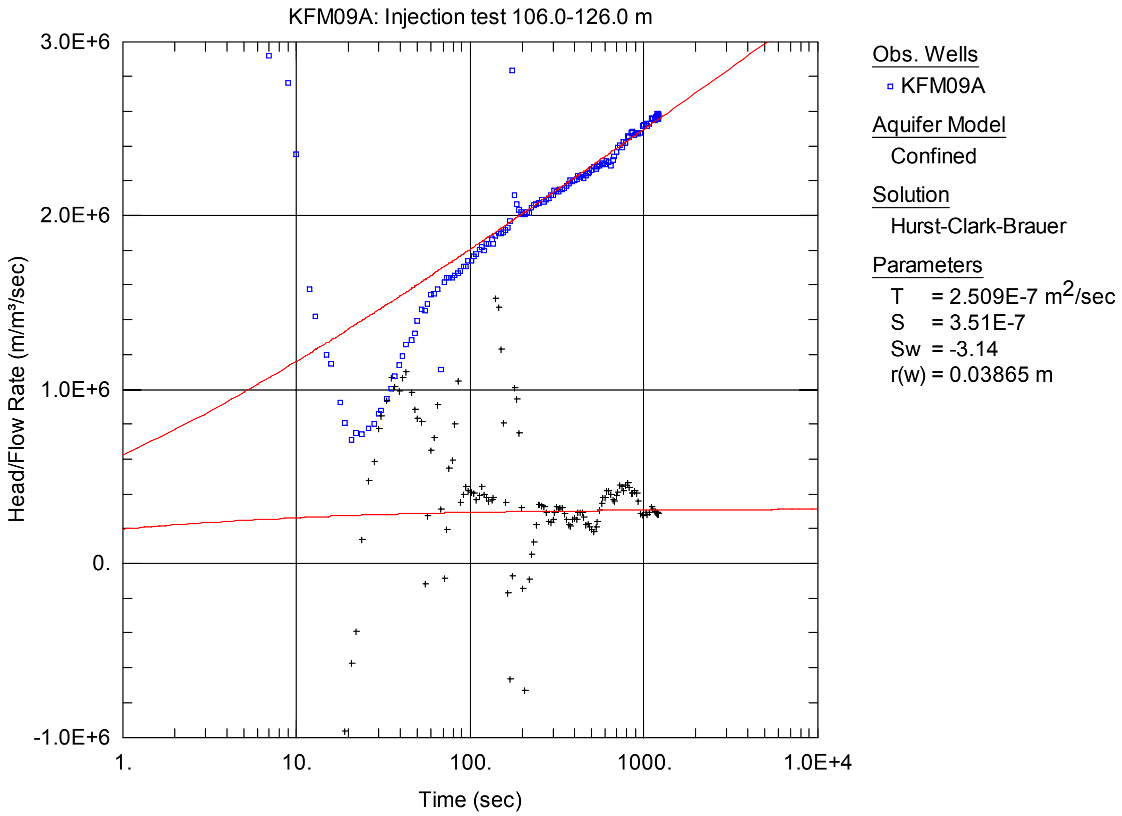


Figure A3-39. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 106.0-126.0 m in KFM09A.*

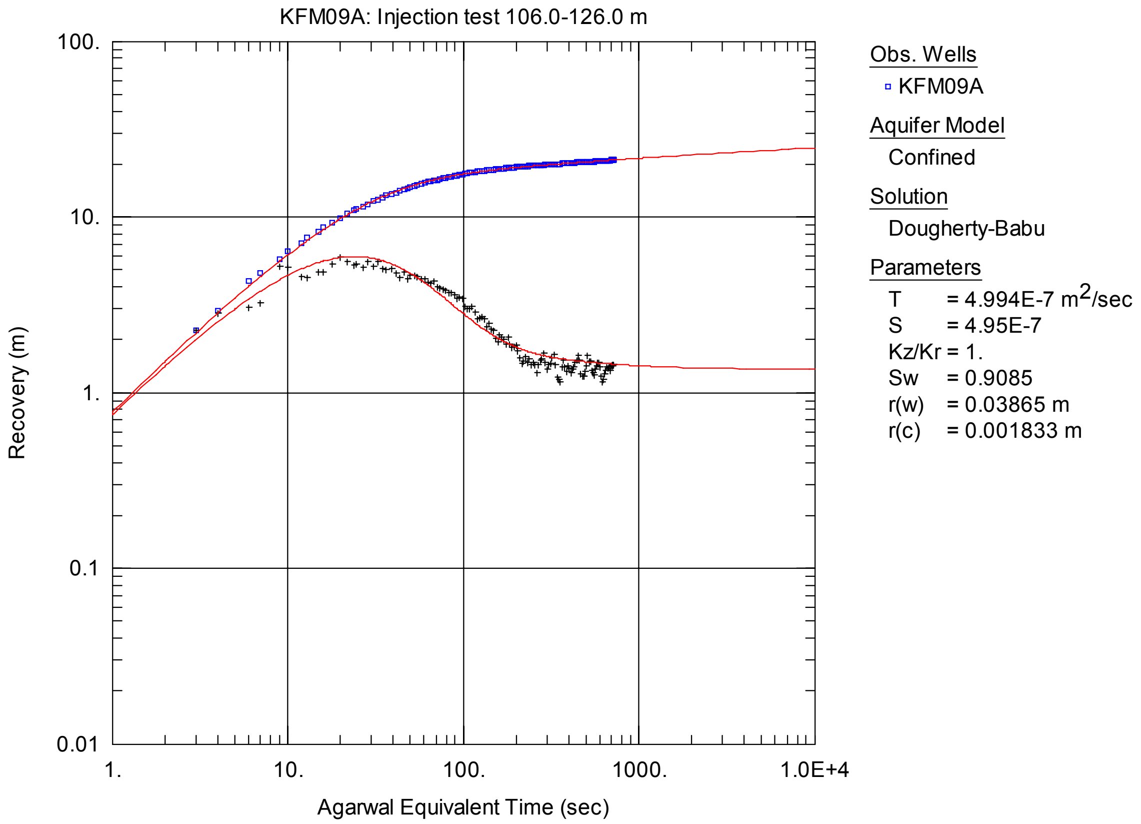


Figure A3-40. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 106.0-126.0 m in KFM09A.*

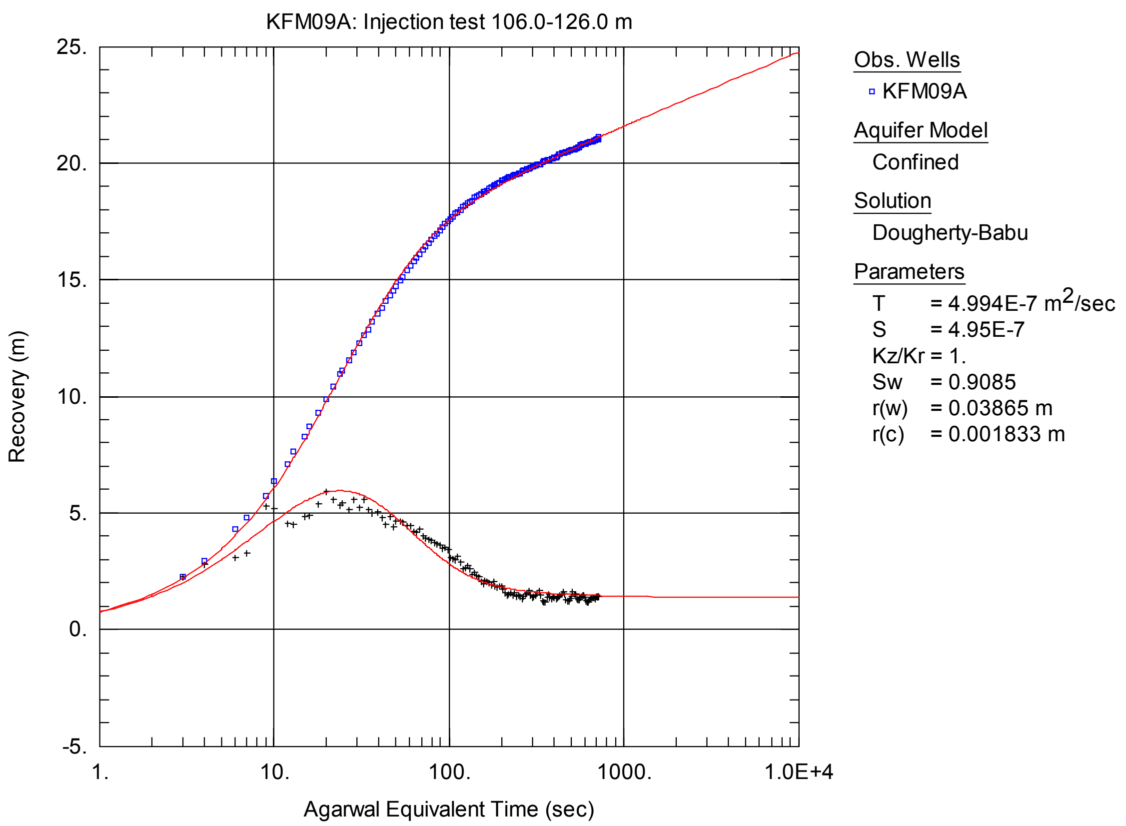


Figure A3-41. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 106.0-126.0 m in KFM09A.*

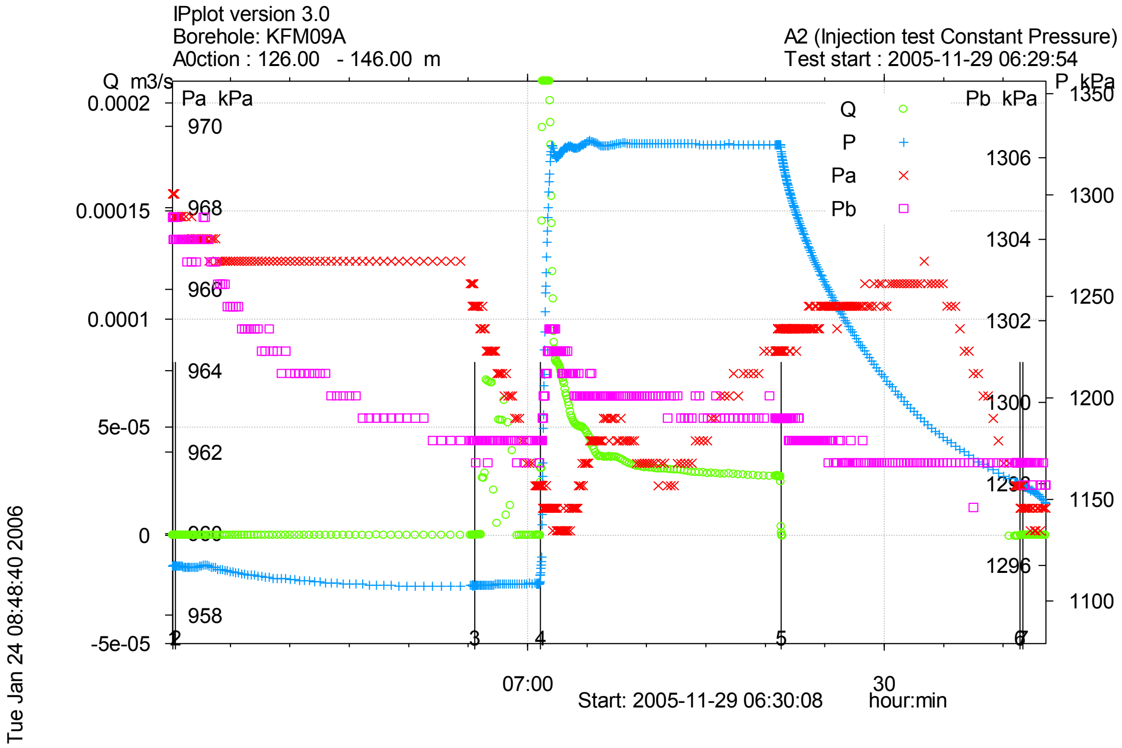


Figure A3-42. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 126.0-146.0 m in borehole KFM09A.*

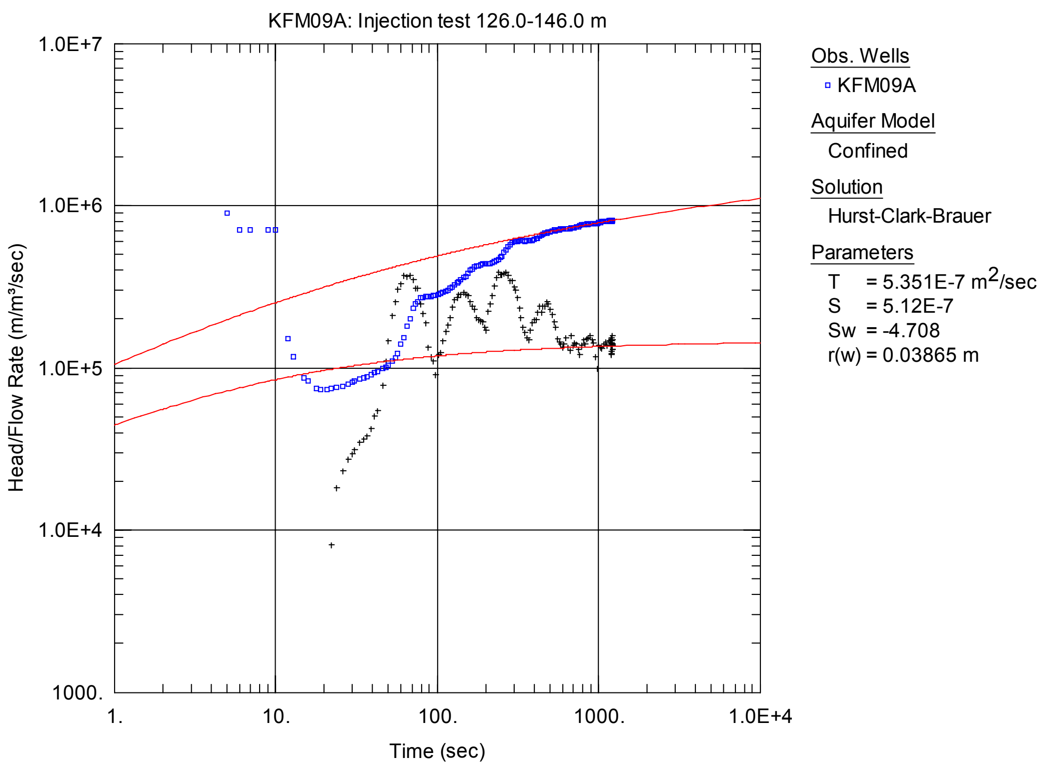


Figure A3-43. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 126.0-146.0 m in KFM09A.*

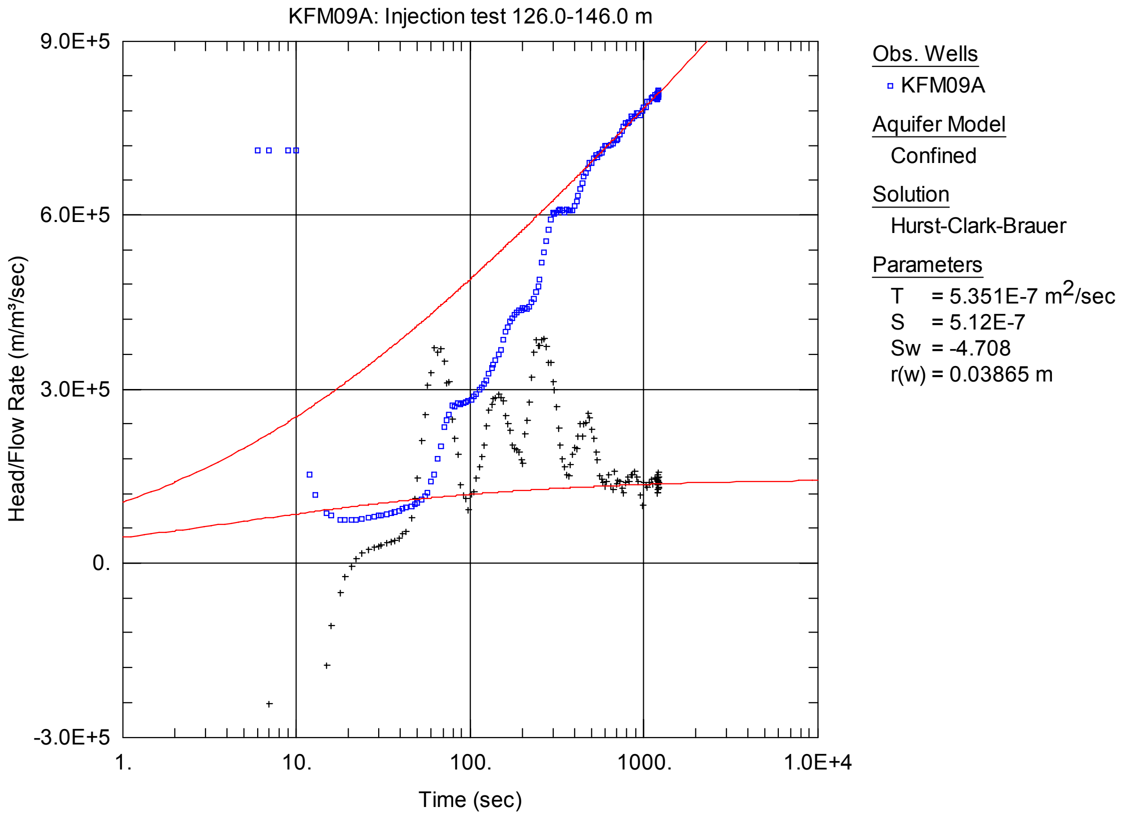


Figure A3-44. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 126.0-146.0 m in KFM09A.*

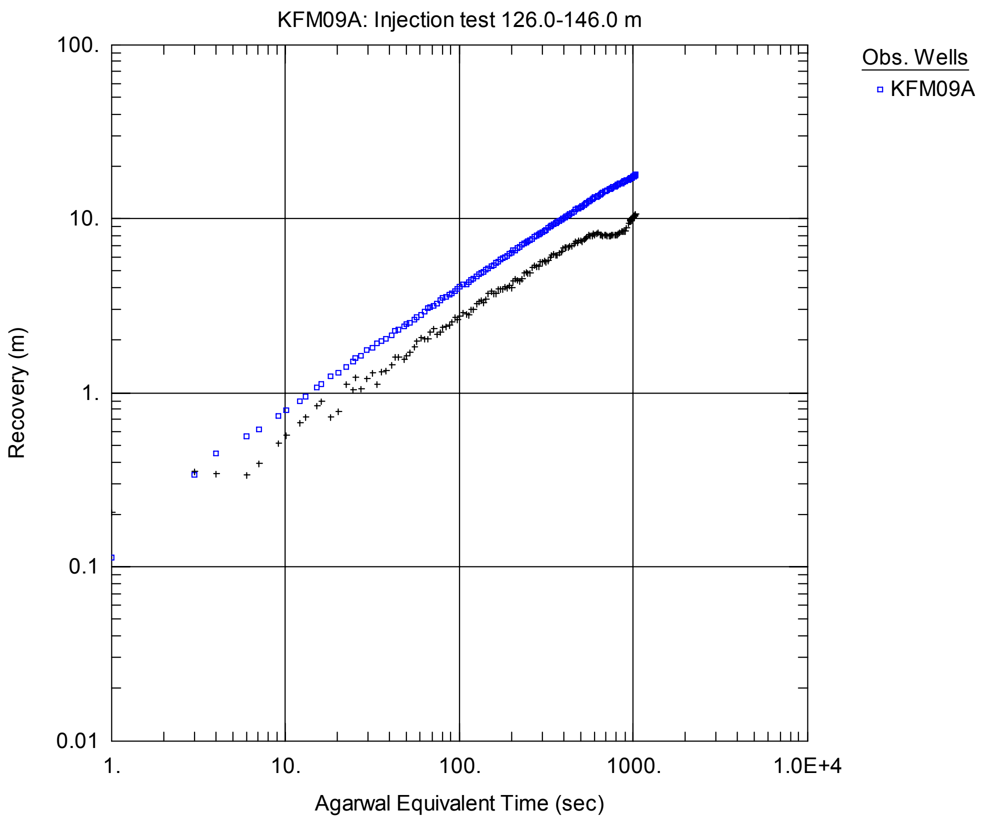


Figure A3-45. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 126.0-146.0 m in KFM09A.*

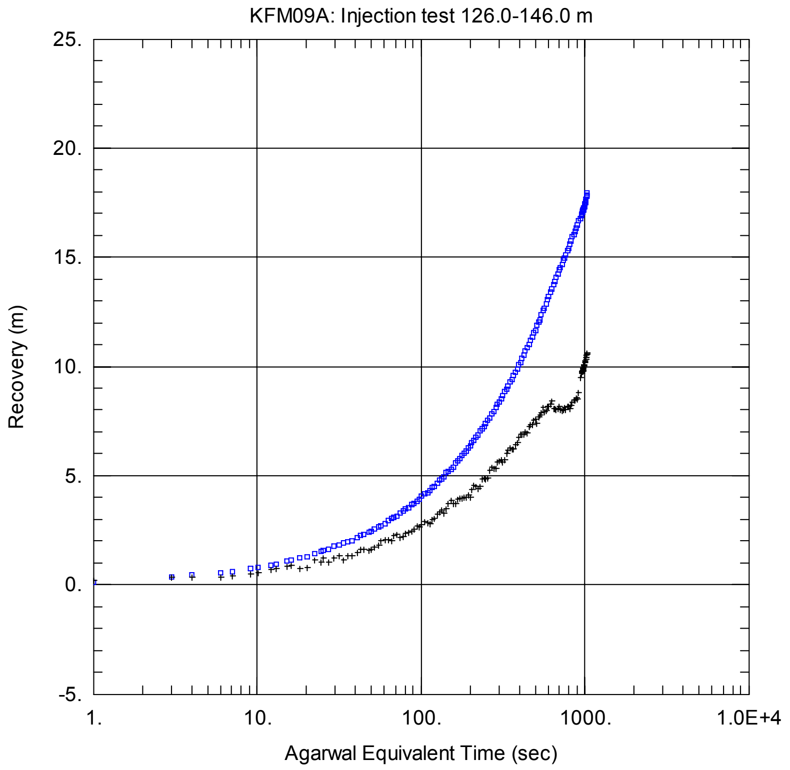


Figure A3-46. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 126.0-146.0 m in KFM09A.*

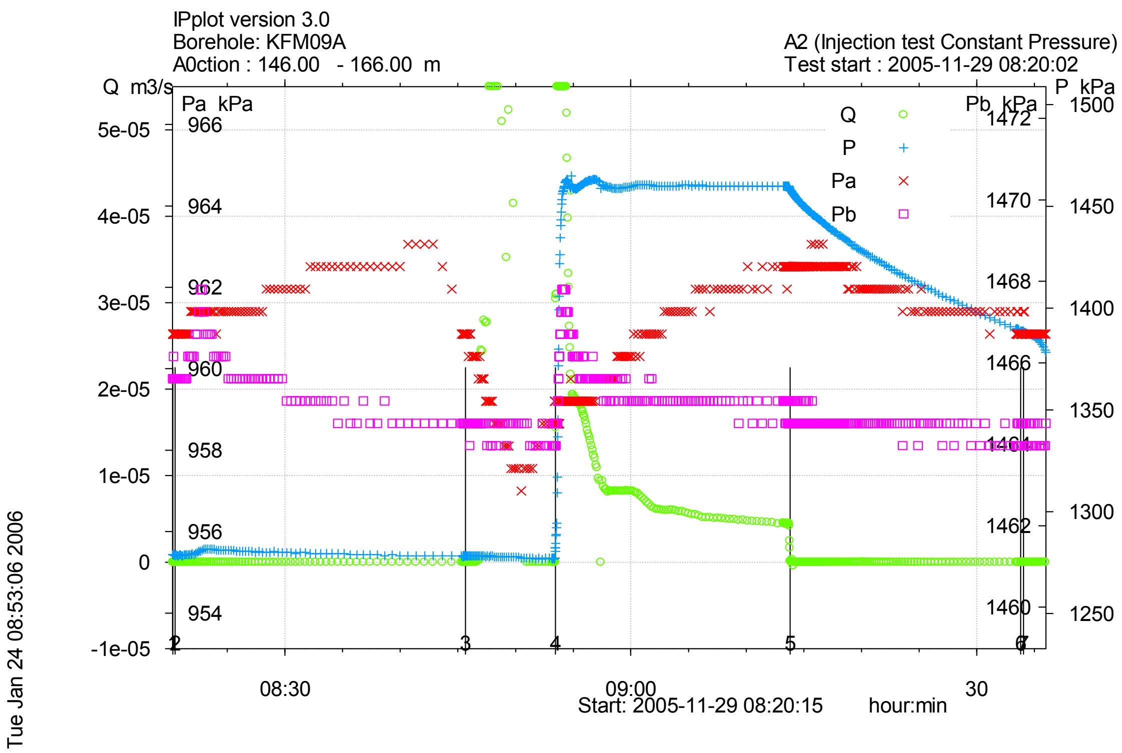


Figure A3-47. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 146.0-166.0 m in borehole KFM09A.*

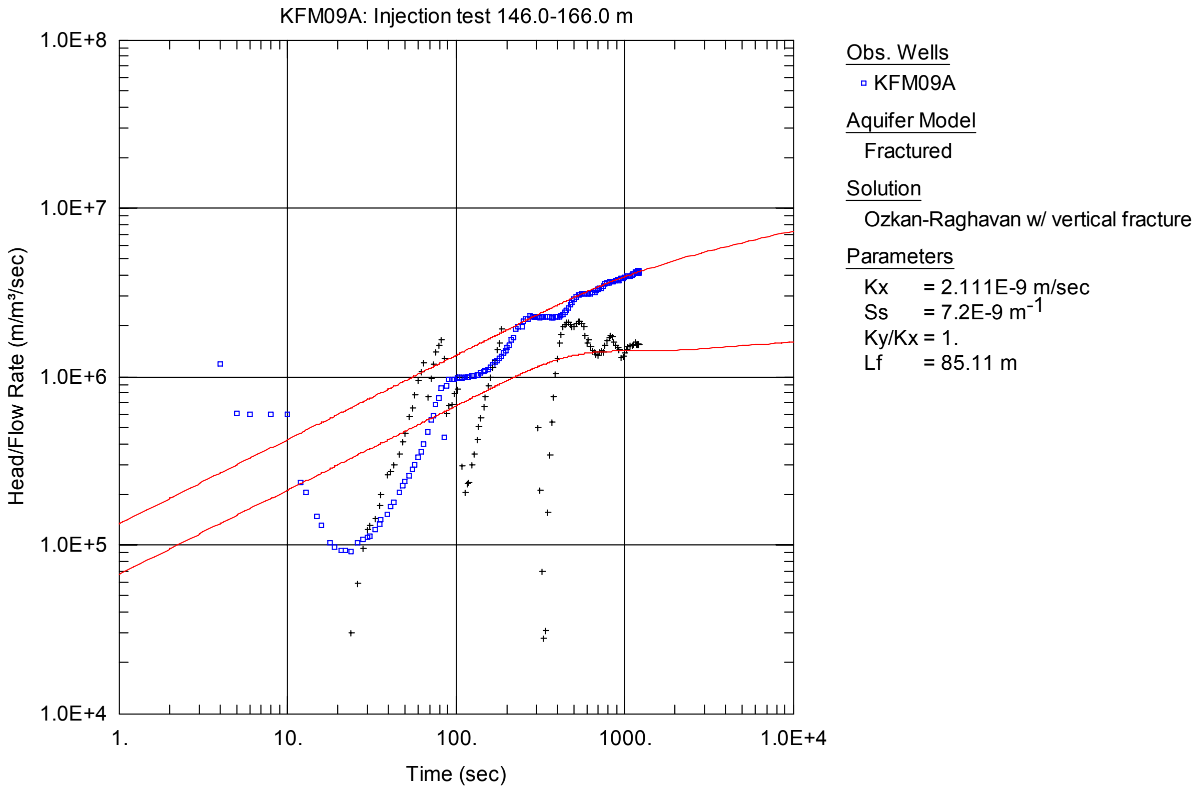


Figure A3-48. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 146.0-166.0 m in KFM09A.*

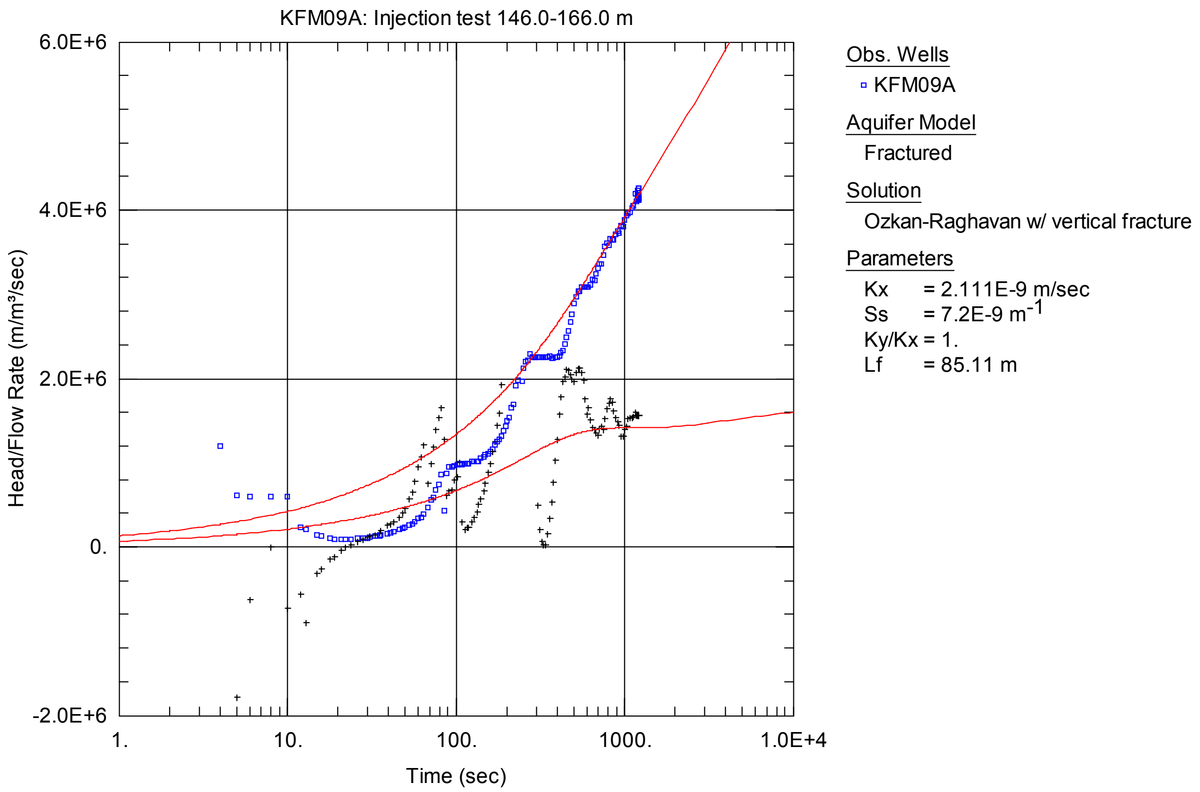


Figure A3-49. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 146.0-166.0 m in KFM09A.*

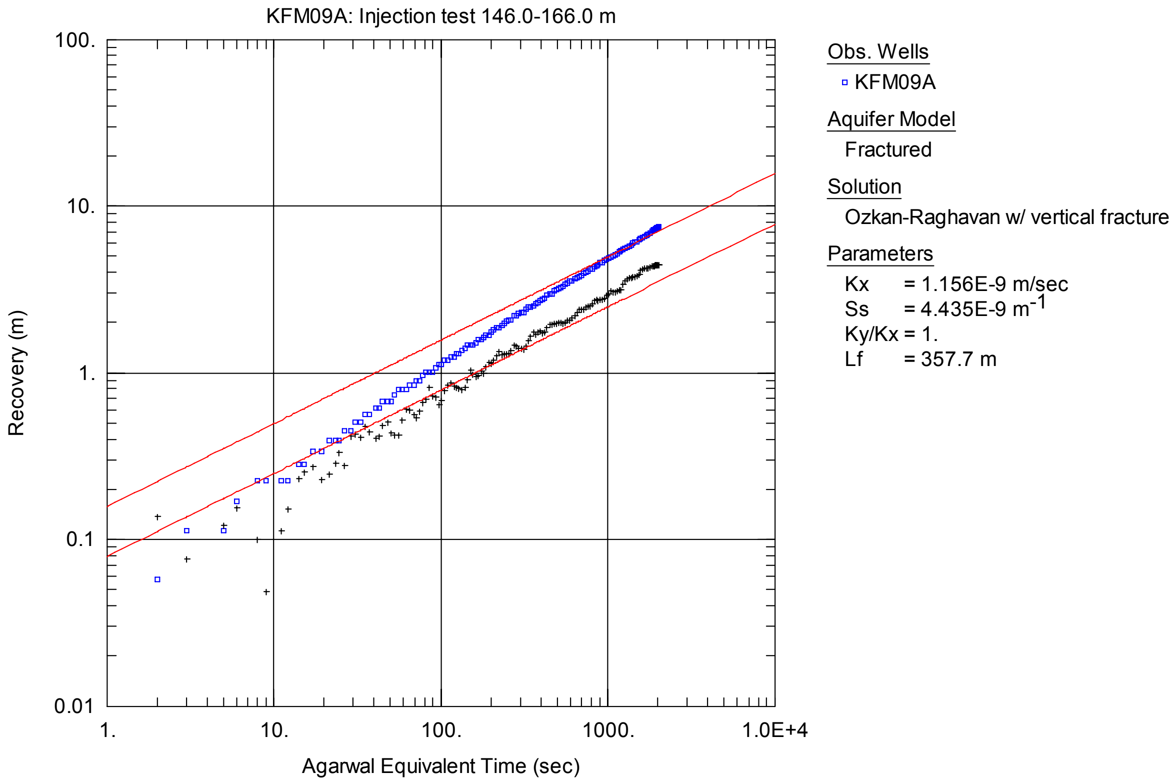


Figure A3-50. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 146.0-166.0 m in KFM09A. No unambiguous transient evaluation of transmissivity on this period is possible.*

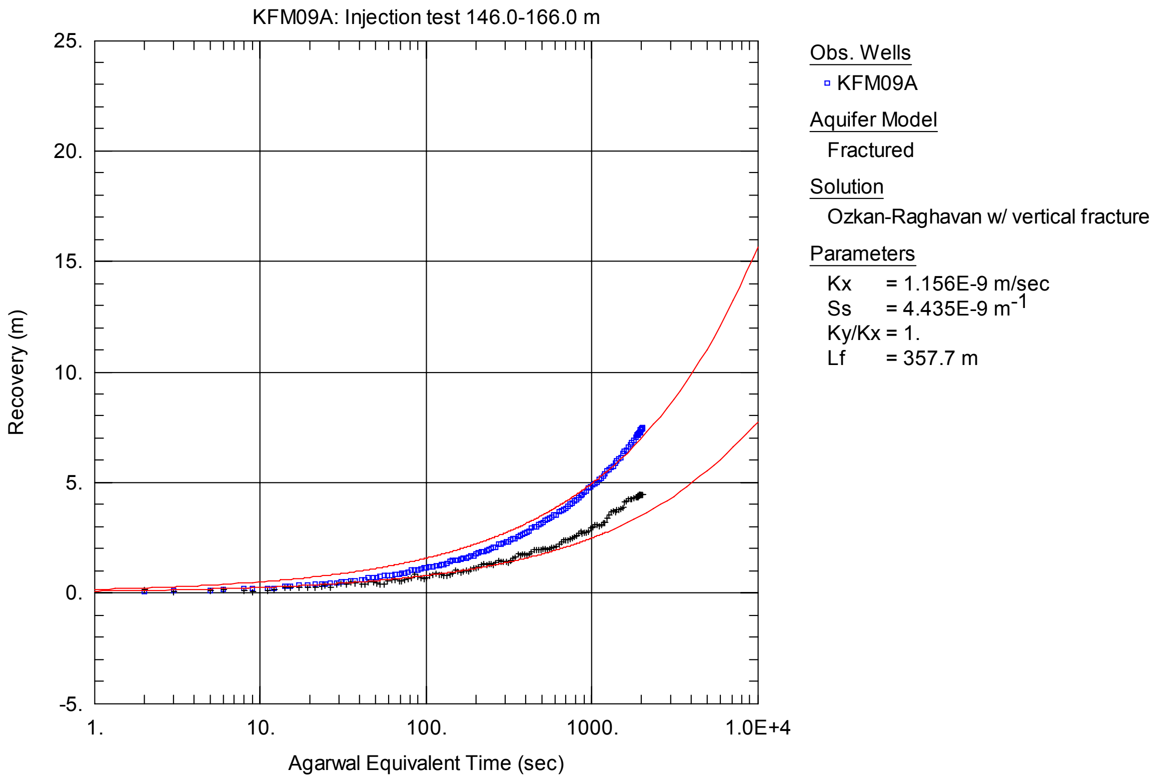


Figure A3-51. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 146.0-166.0 m in KFM09A. No unambiguous transient evaluation of transmissivity on this period is possible.*

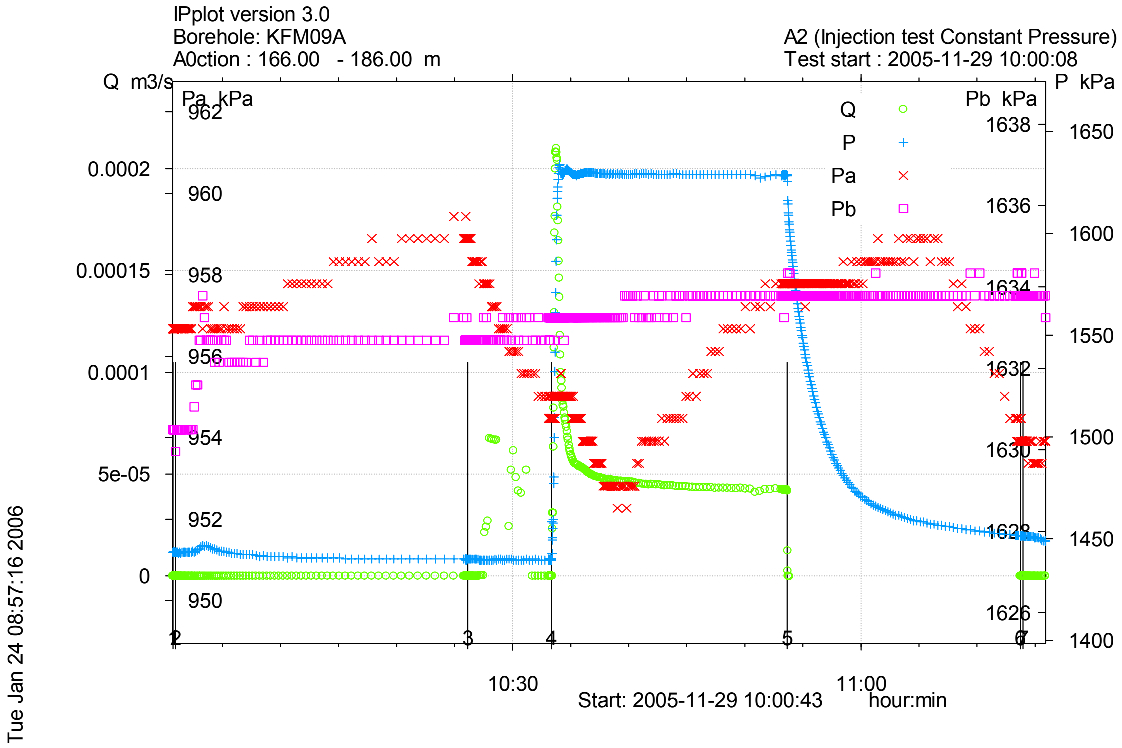


Figure A3-52. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 166.0-186.0 m in borehole KFM09A.*

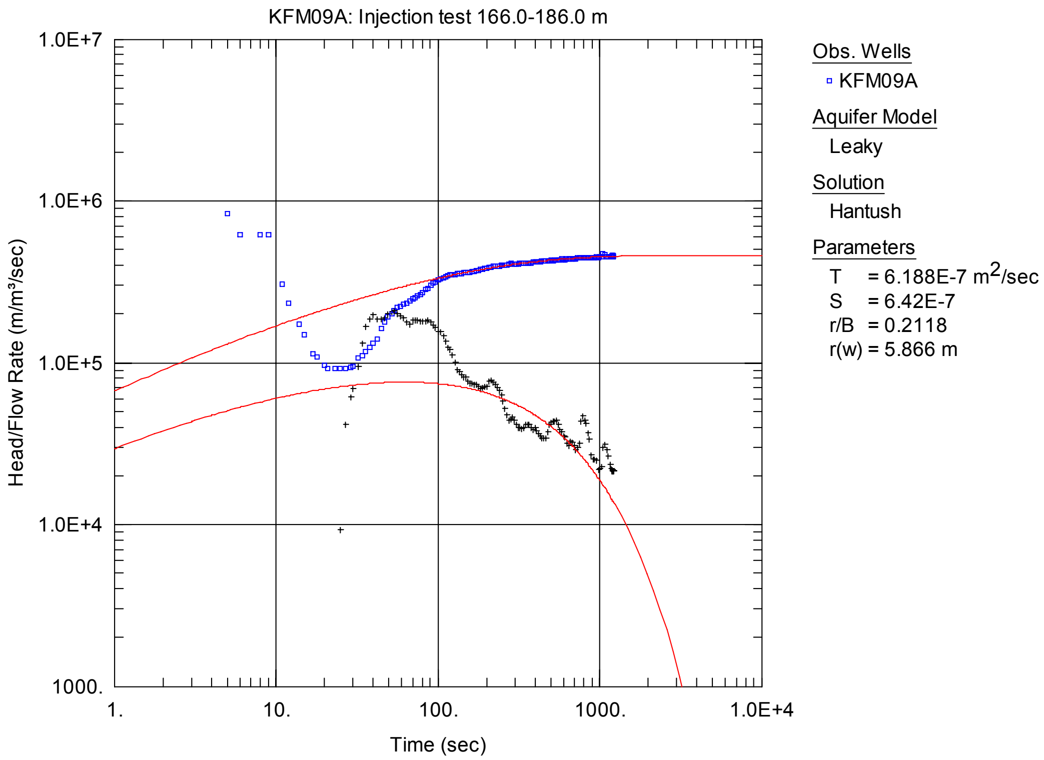


Figure A3-53. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 166.0-186.0 m in KFM09A.*

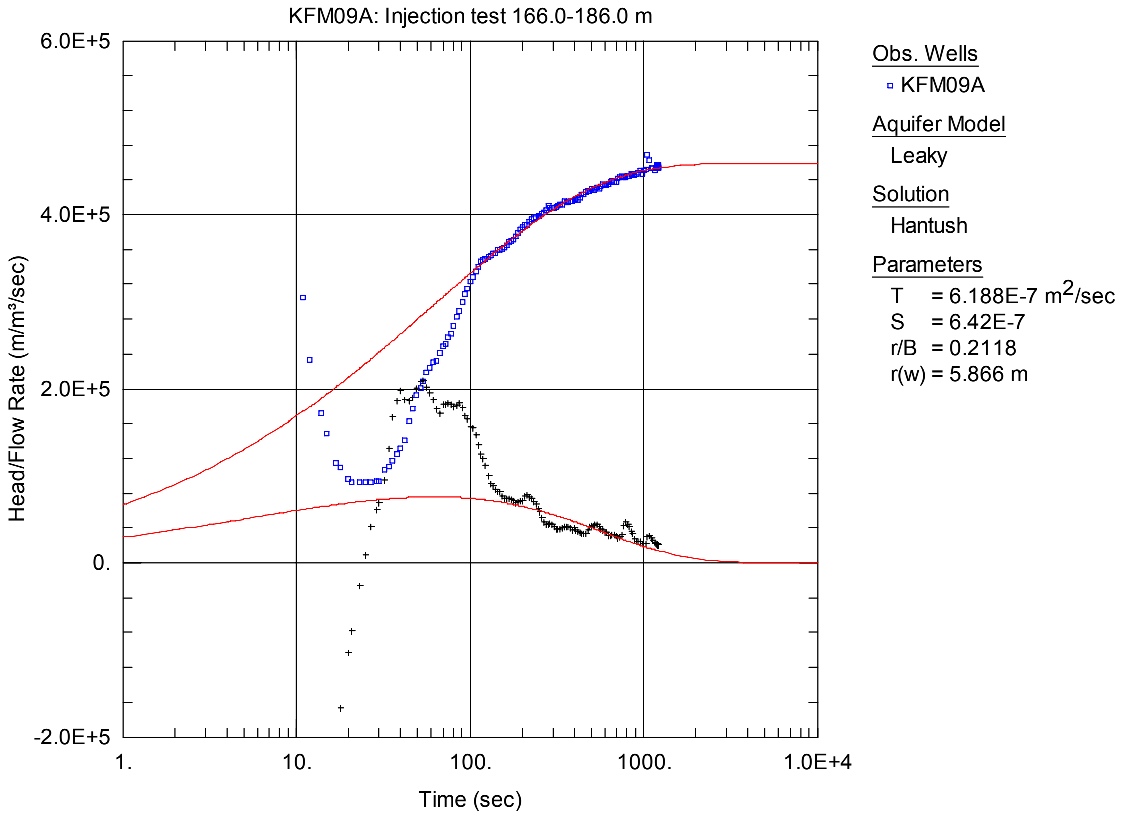


Figure A3-54. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 166.0-186.0 m in KFM09A.*

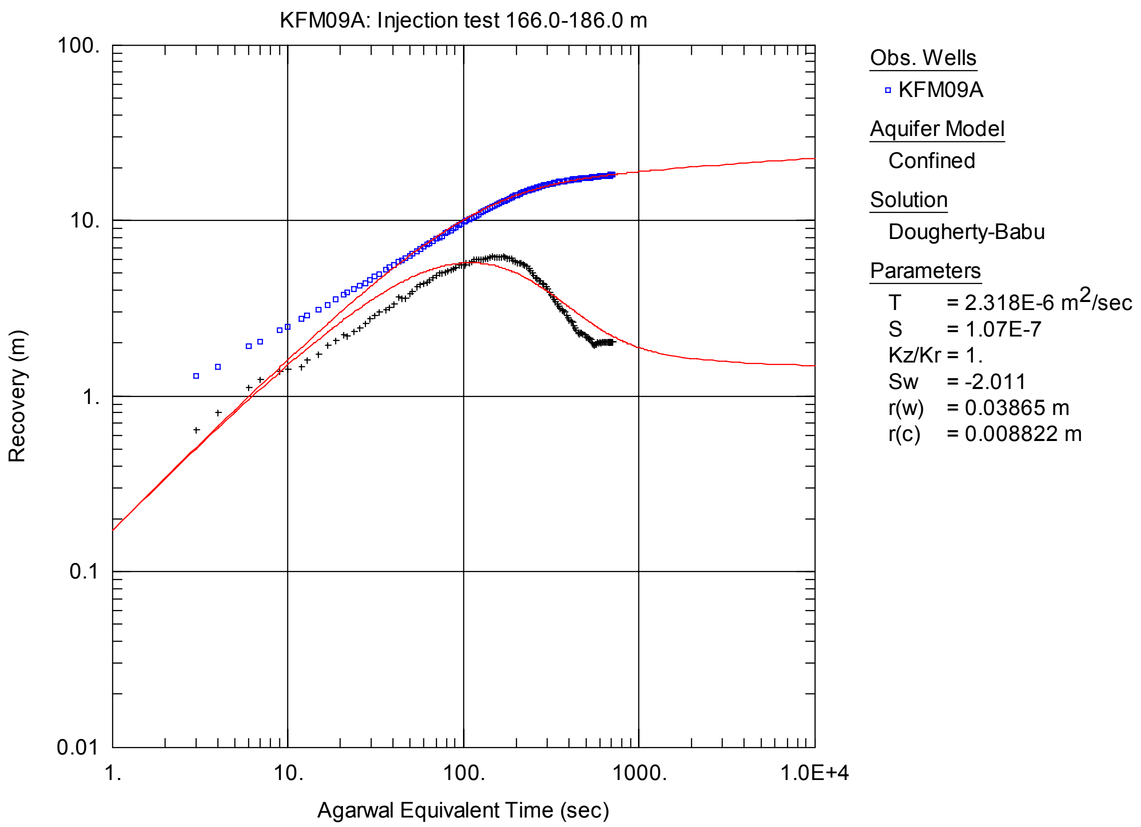


Figure A3-55. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 166.0-186.0 m in KFM09A.*

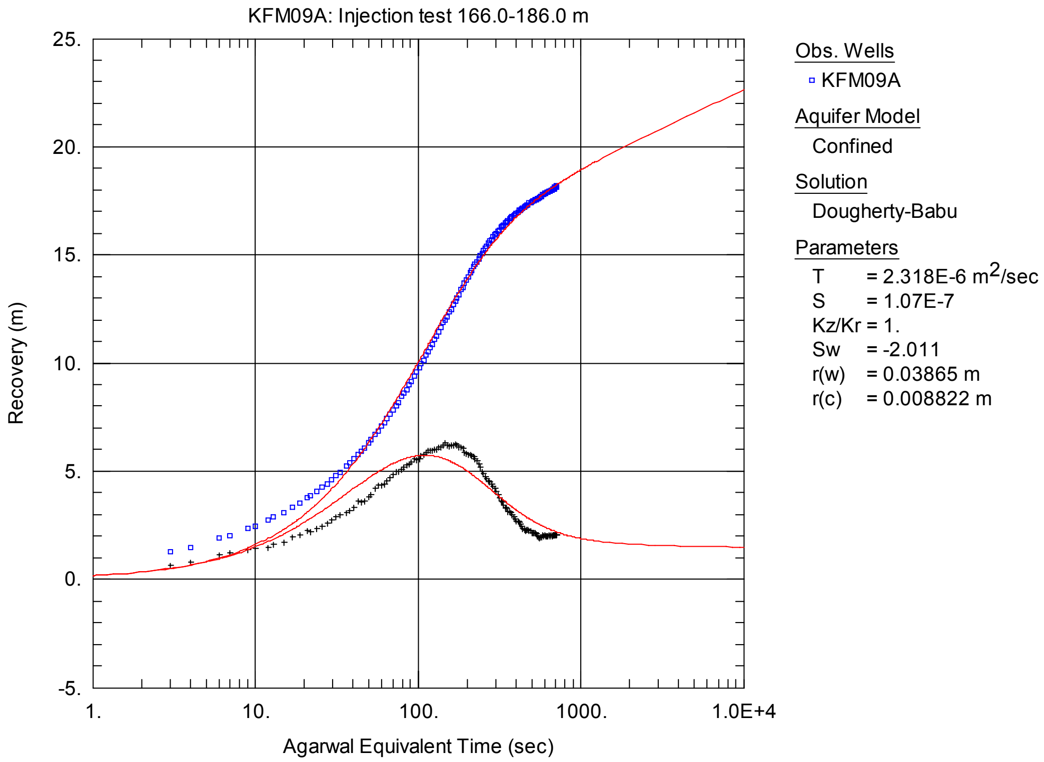


Figure A3-56. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 166.0-186.0 m in KFM09A.*

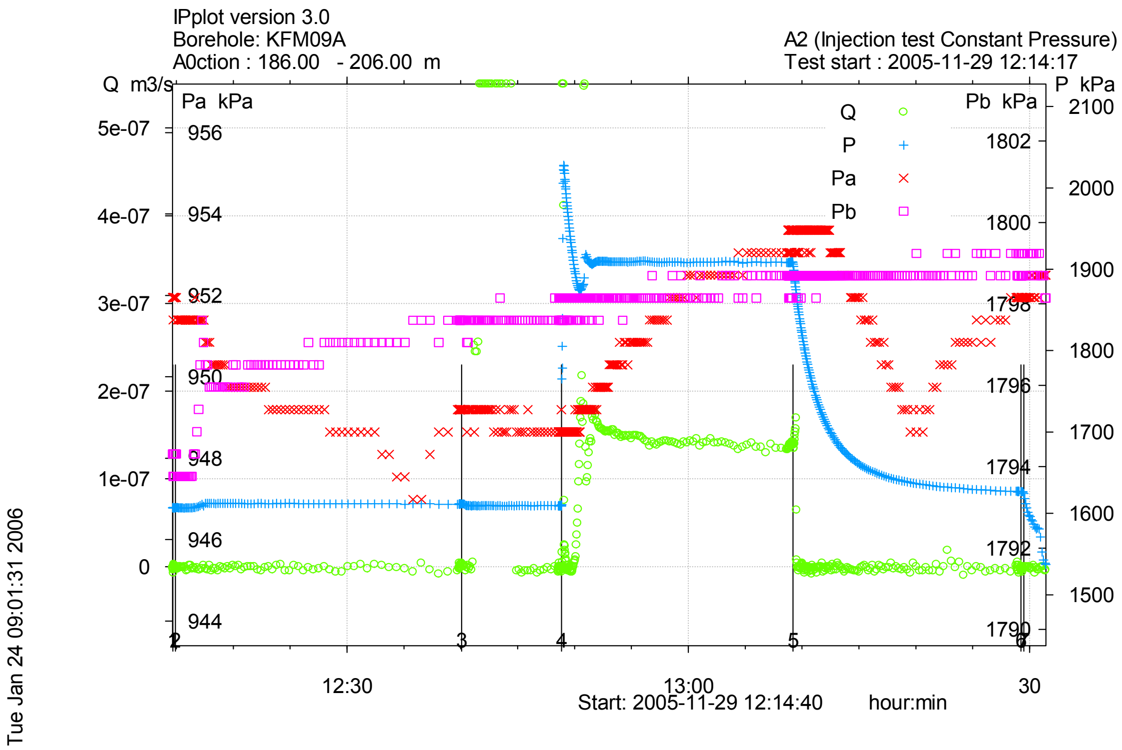


Figure A3-57. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 186.0-206.0 m in borehole KFM09A.*

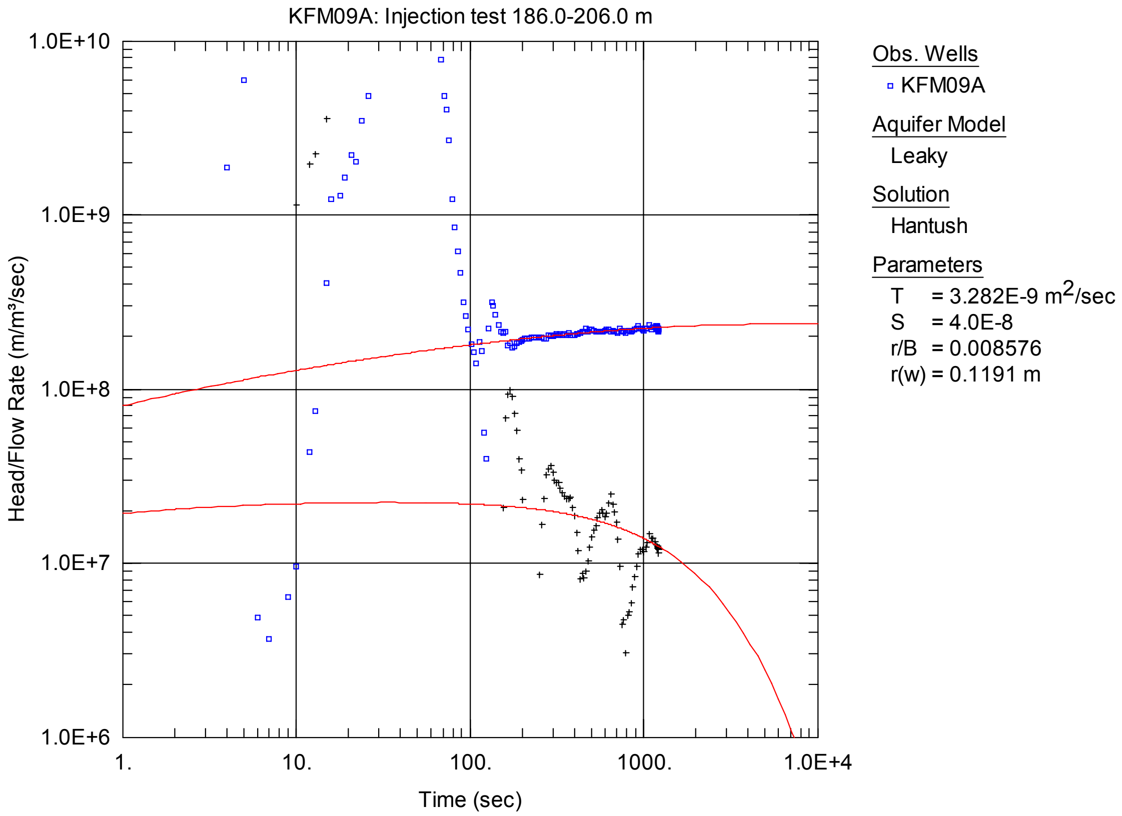


Figure A3-58. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 186.0-206.0 m in KFM09A.*

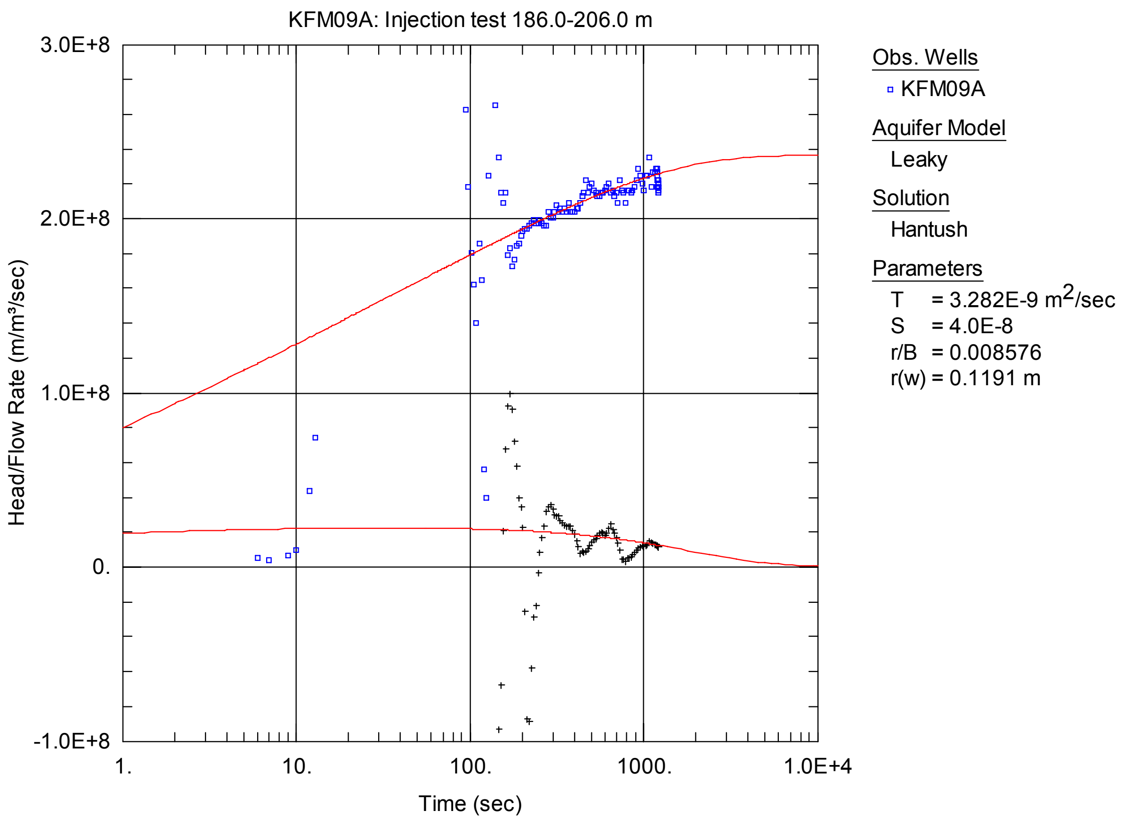


Figure A3-59. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 186.0-206.0 m in KFM09A.*

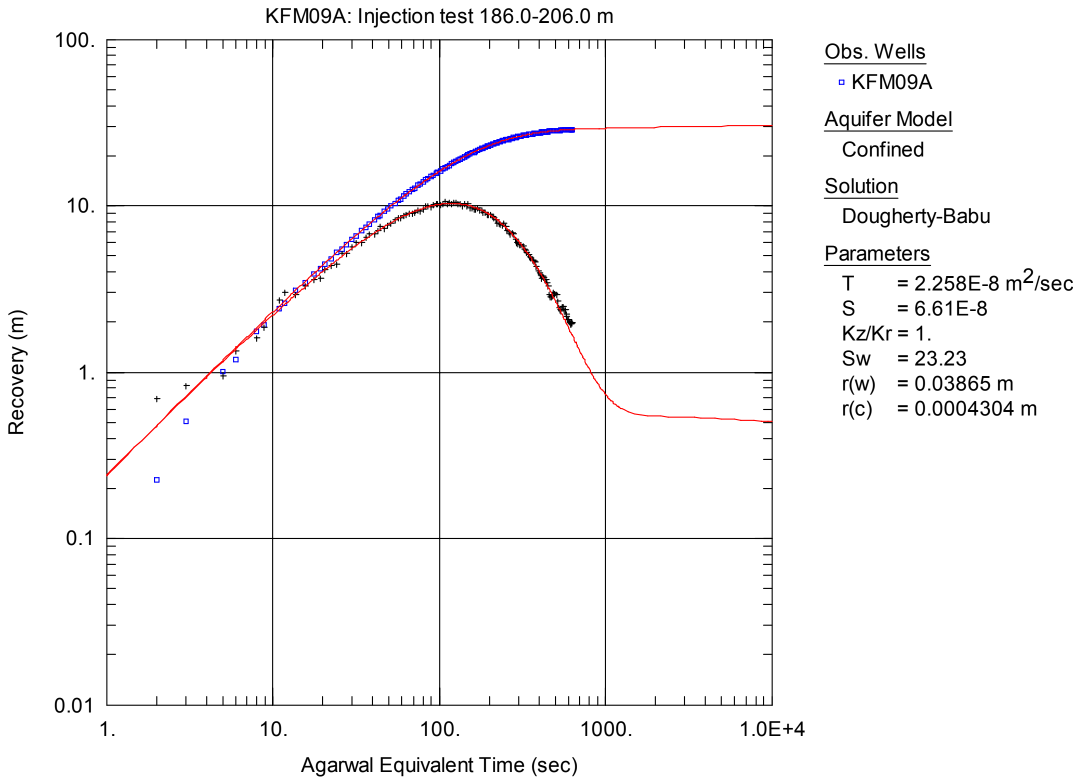


Figure A3-60. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 186.0-206.0 m in KFM09A. The transient evaluation on the recovery period is not regarded as representative.*

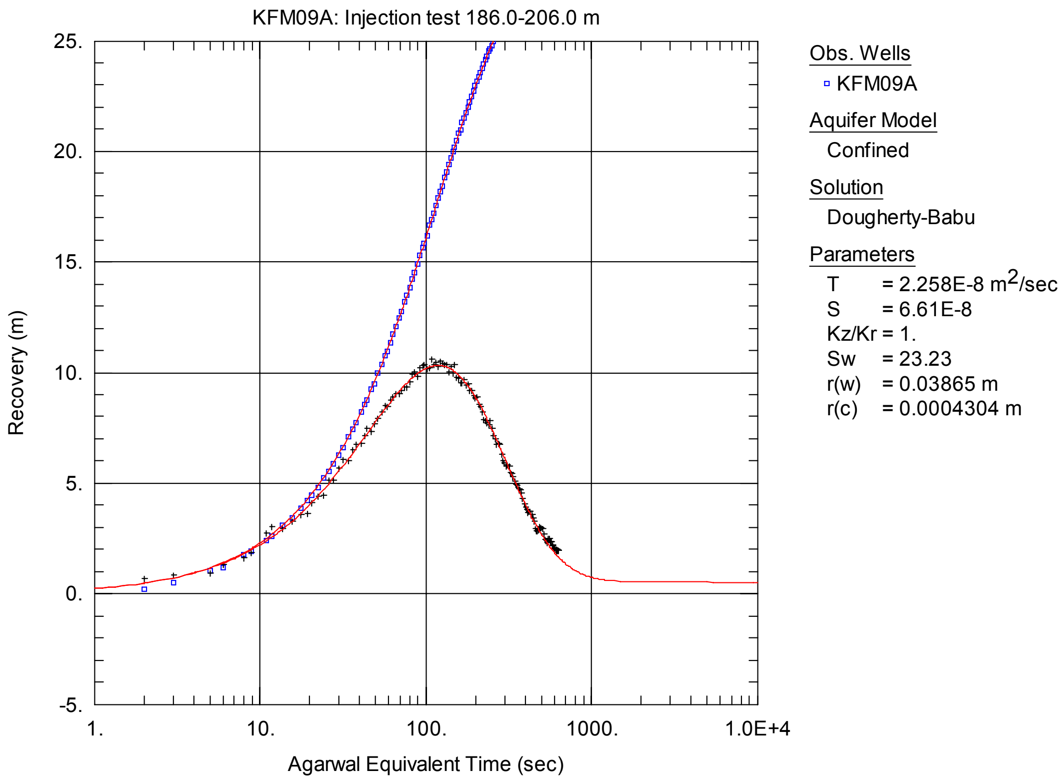


Figure A3-61. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in 186.0-206.0 m in KFM09A. The transient evaluation on the recovery period is not regarded as representative.*

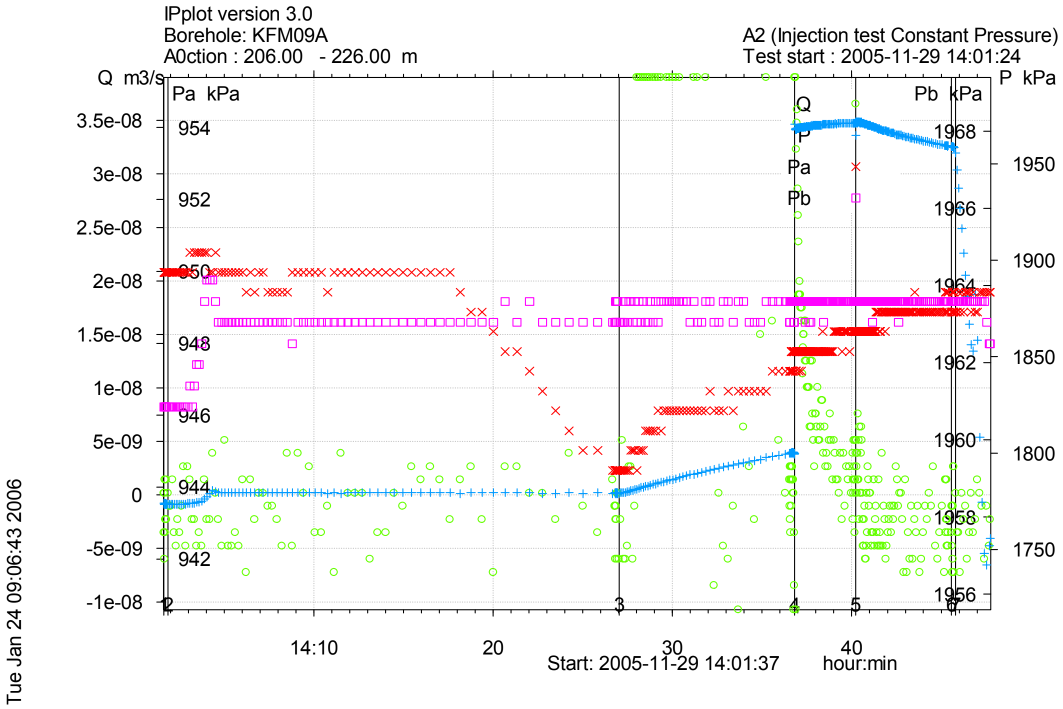


Figure A3-62. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 206.0-226.0 m in borehole KFM09A.

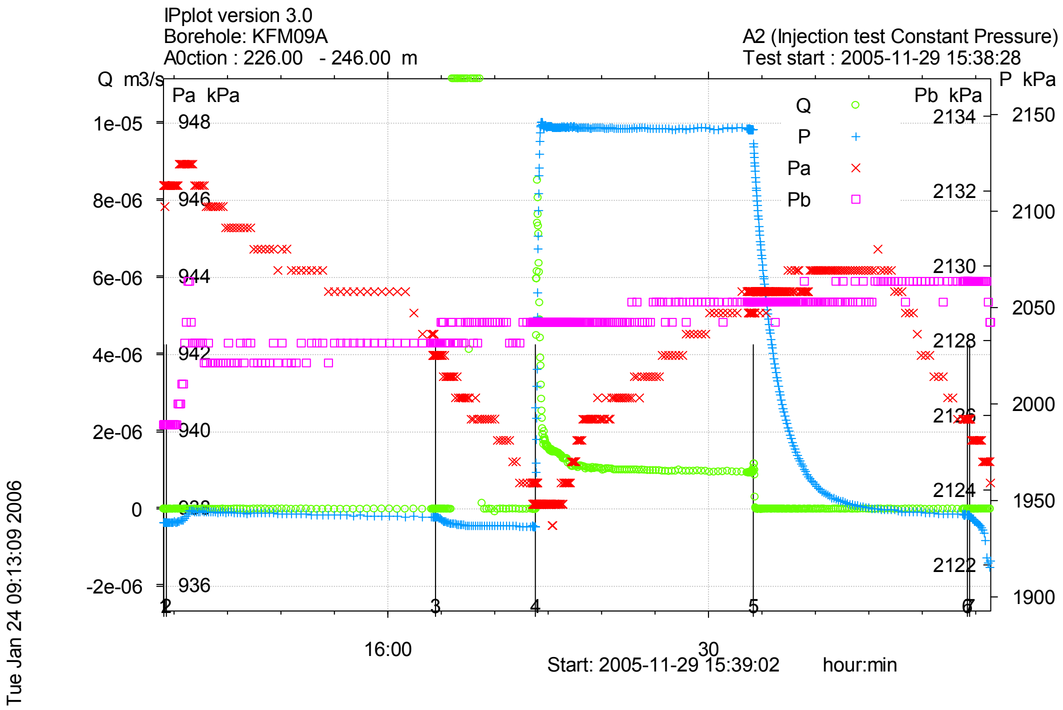


Figure A3-63. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 226.0-246.0 m in borehole KFM09A.

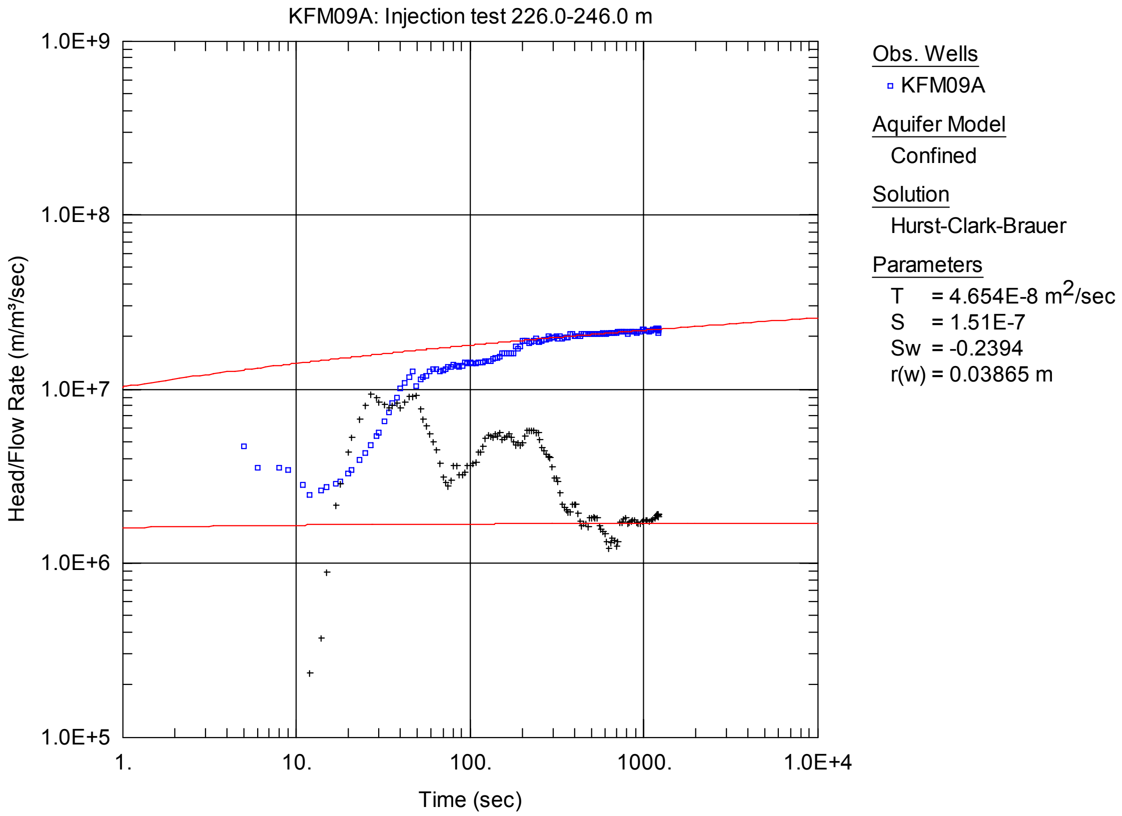


Figure A3-64. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 226.0-246.0 m in KFM09A.*

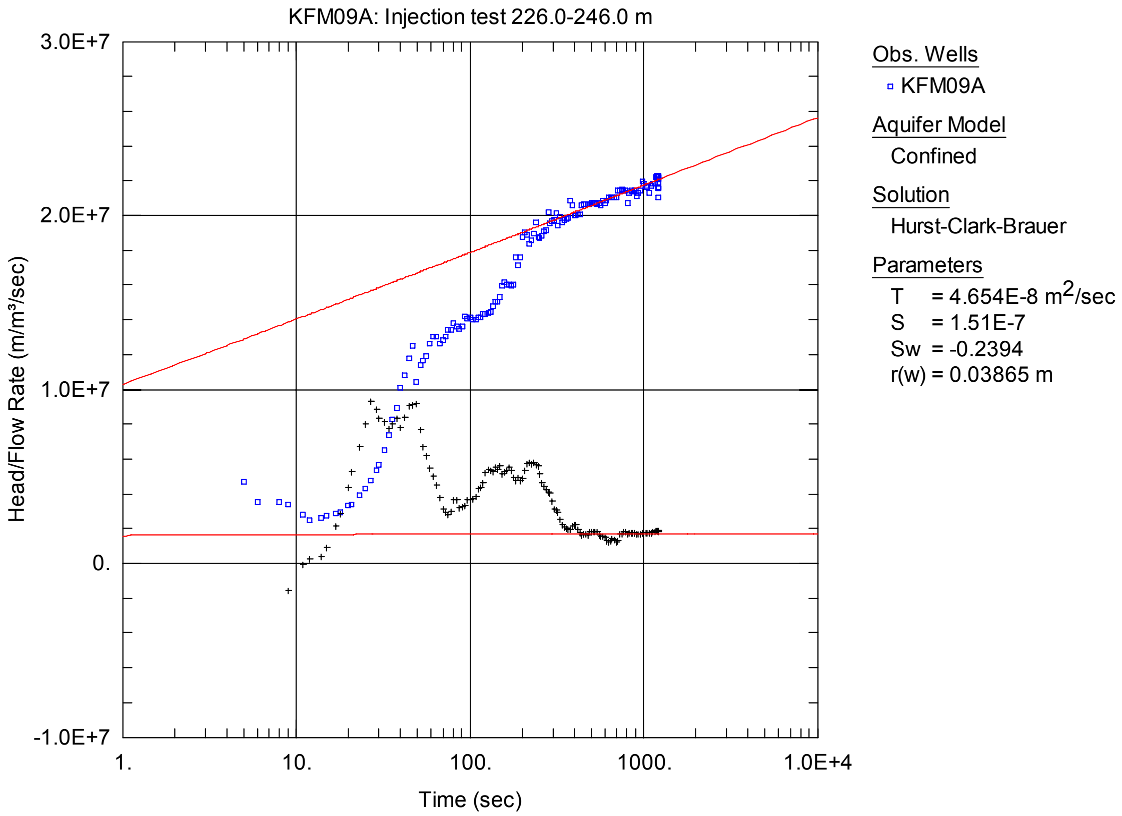


Figure A3-65. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 226.0-246.0 m in KFM09A.*

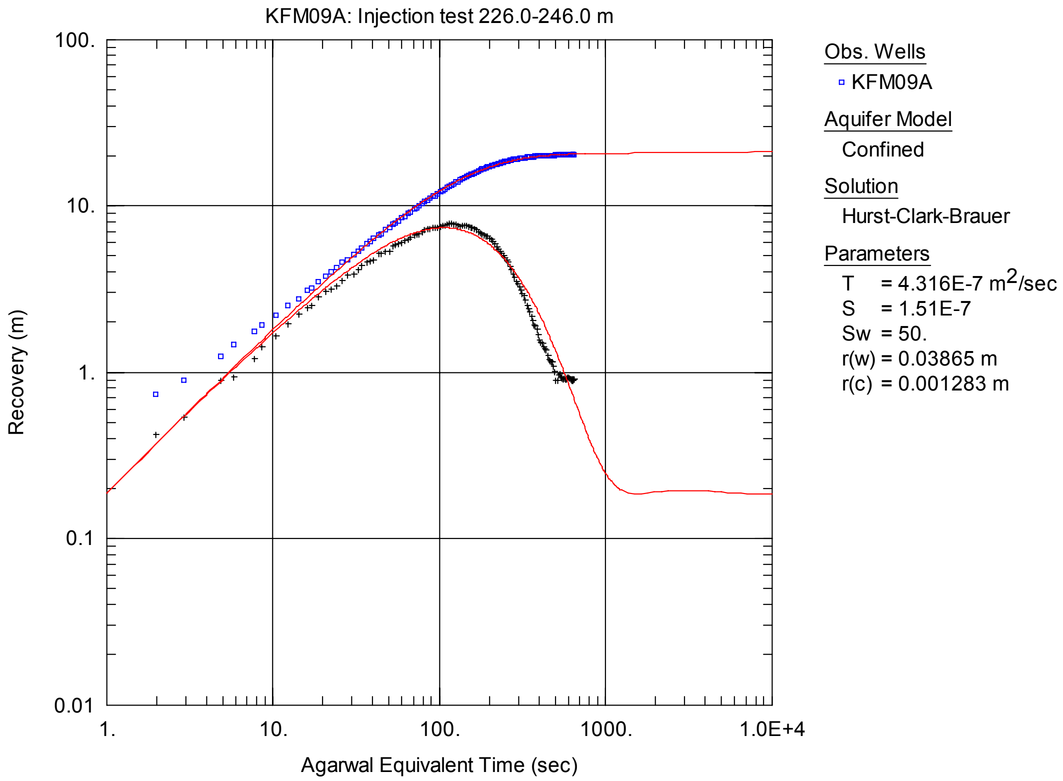


Figure A3-66. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in 226.0-246.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.*

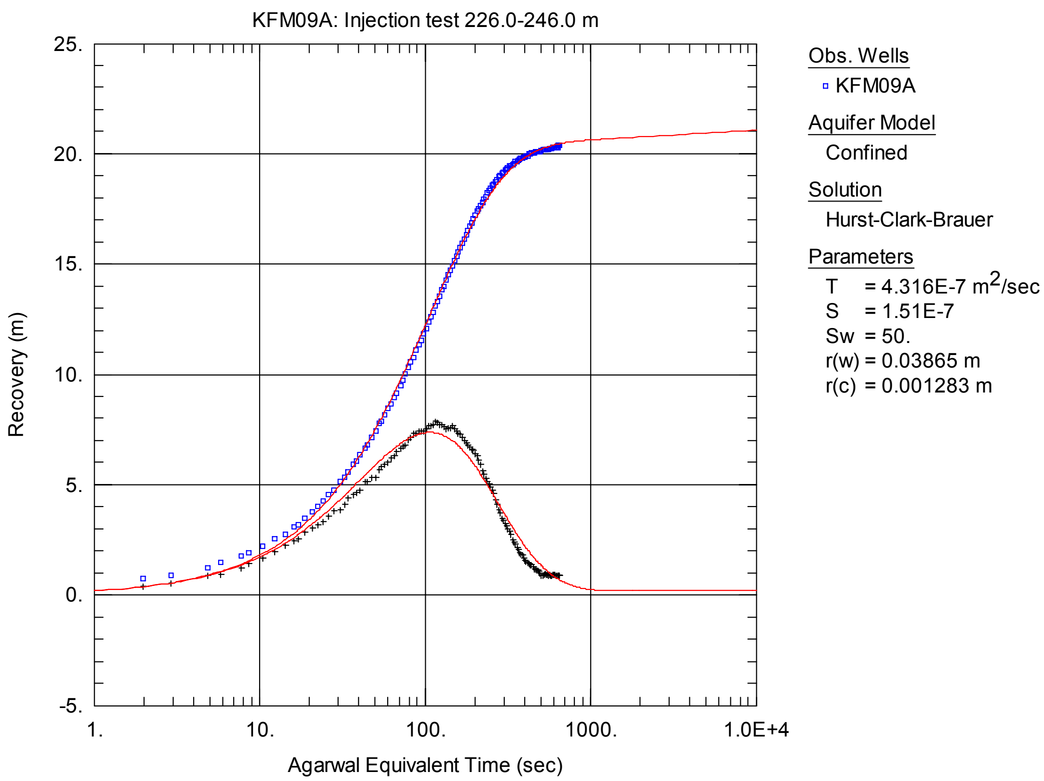


Figure A3-67. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 226.0-246.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period*

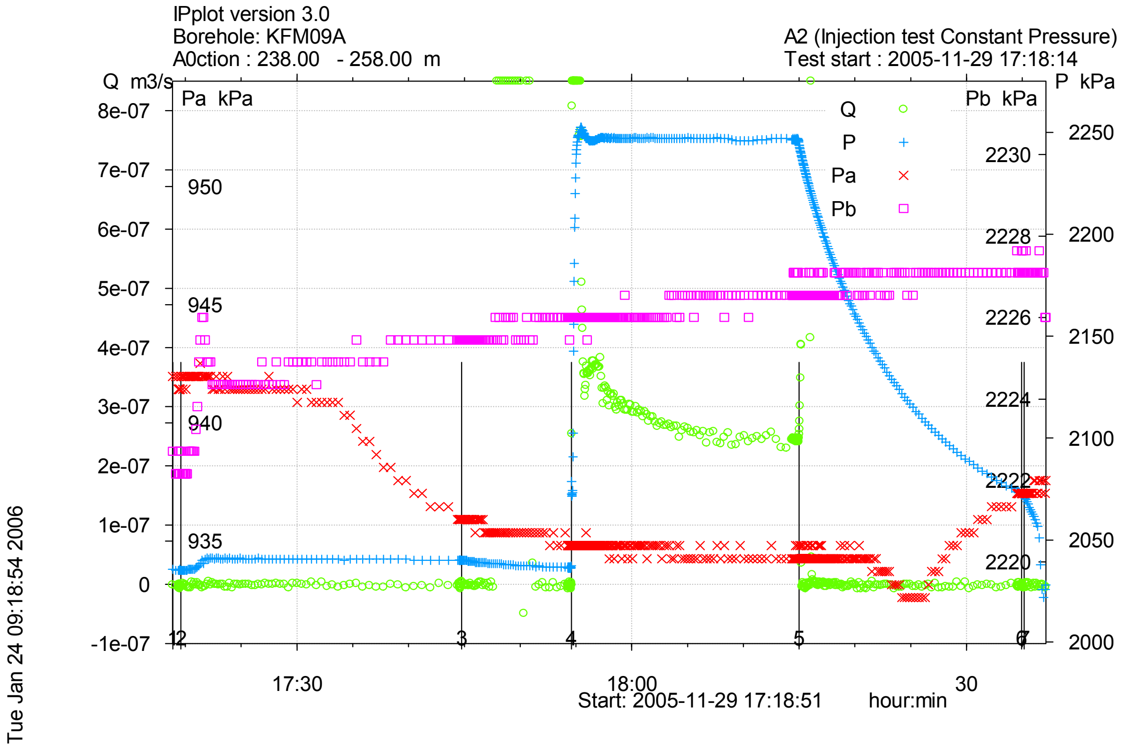


Figure A3-68. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 238.0-258.0 m in borehole KFM09A.*

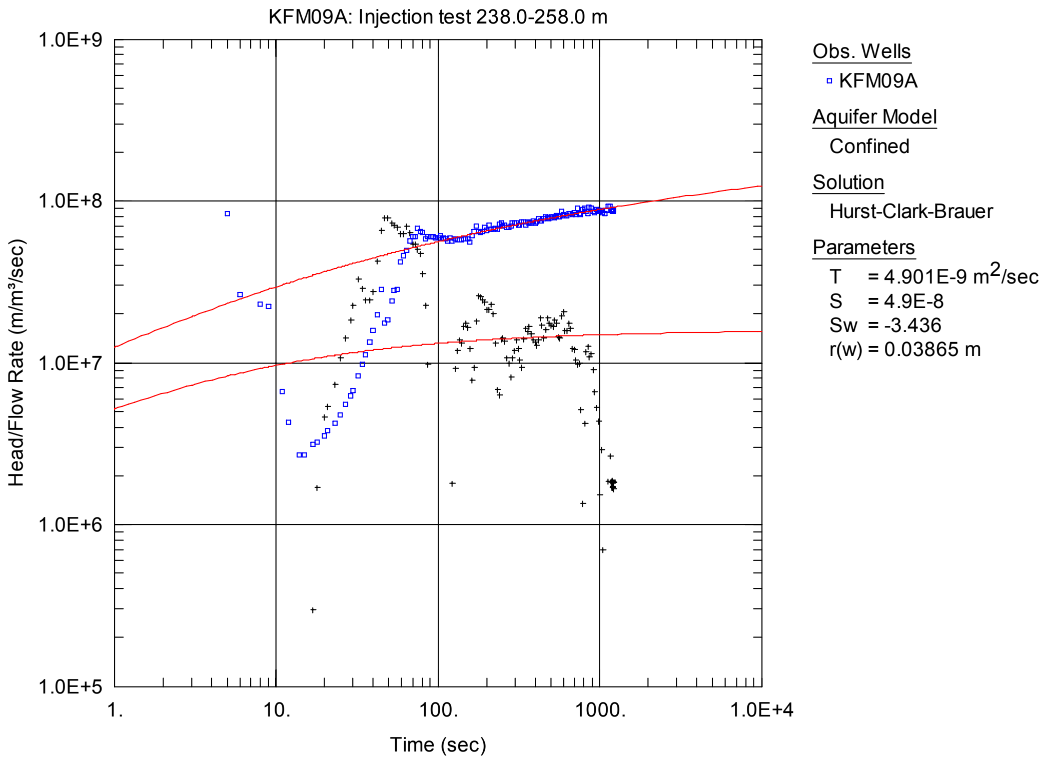


Figure A3-69. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 238.0-258.0 m in KFM09A.*

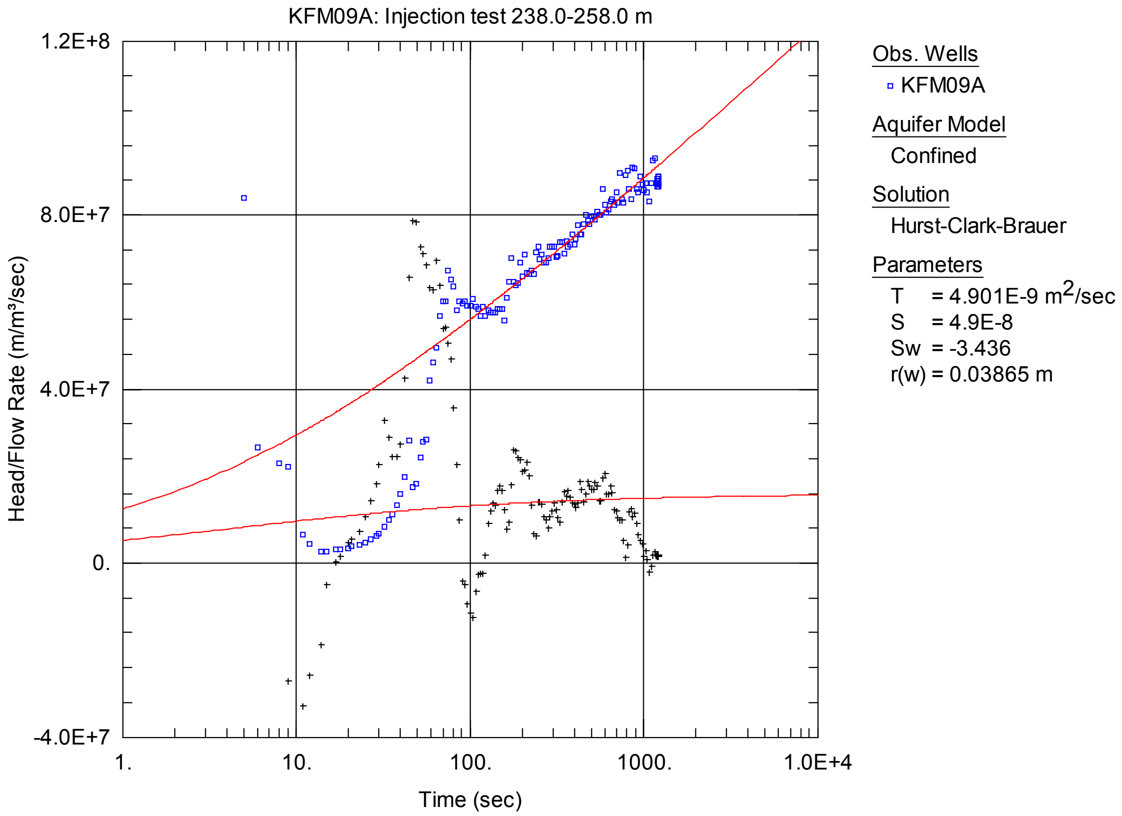


Figure A3-70. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 238.0-258.0 m in KFM09A.*

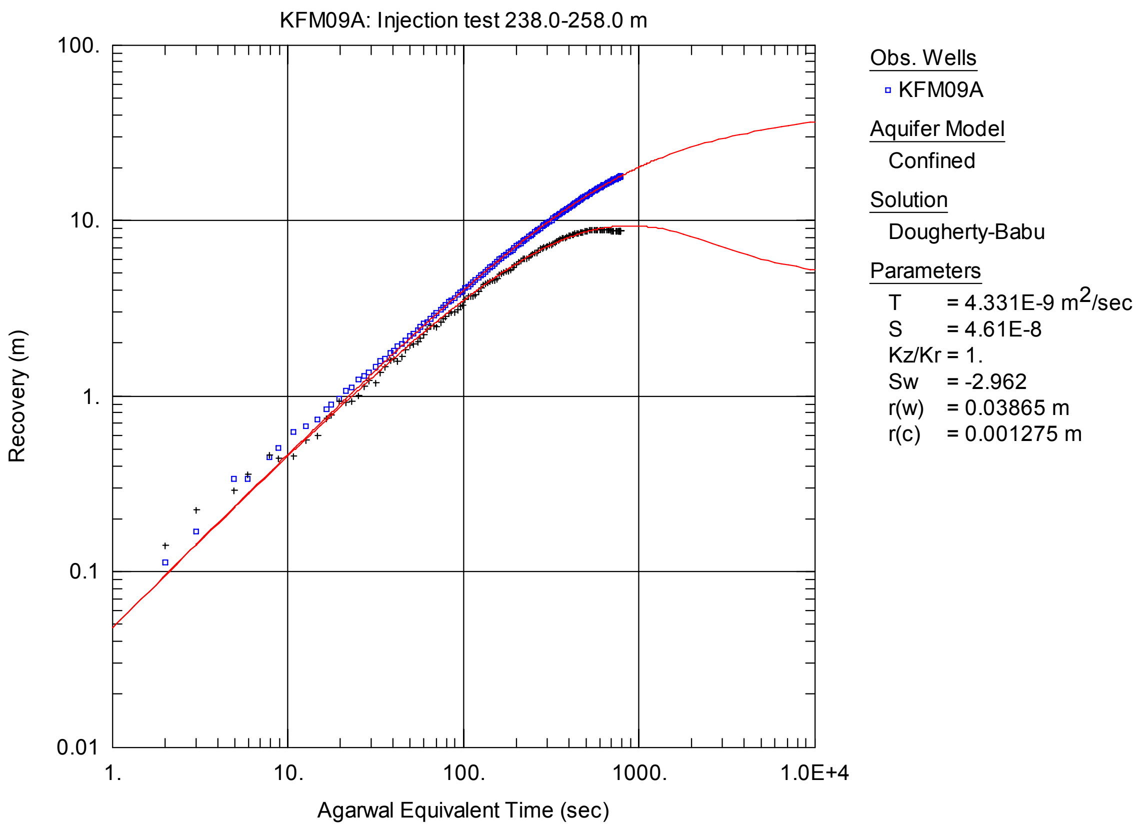


Figure A3-71. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 238.0-258.0 m in KFM09A.*

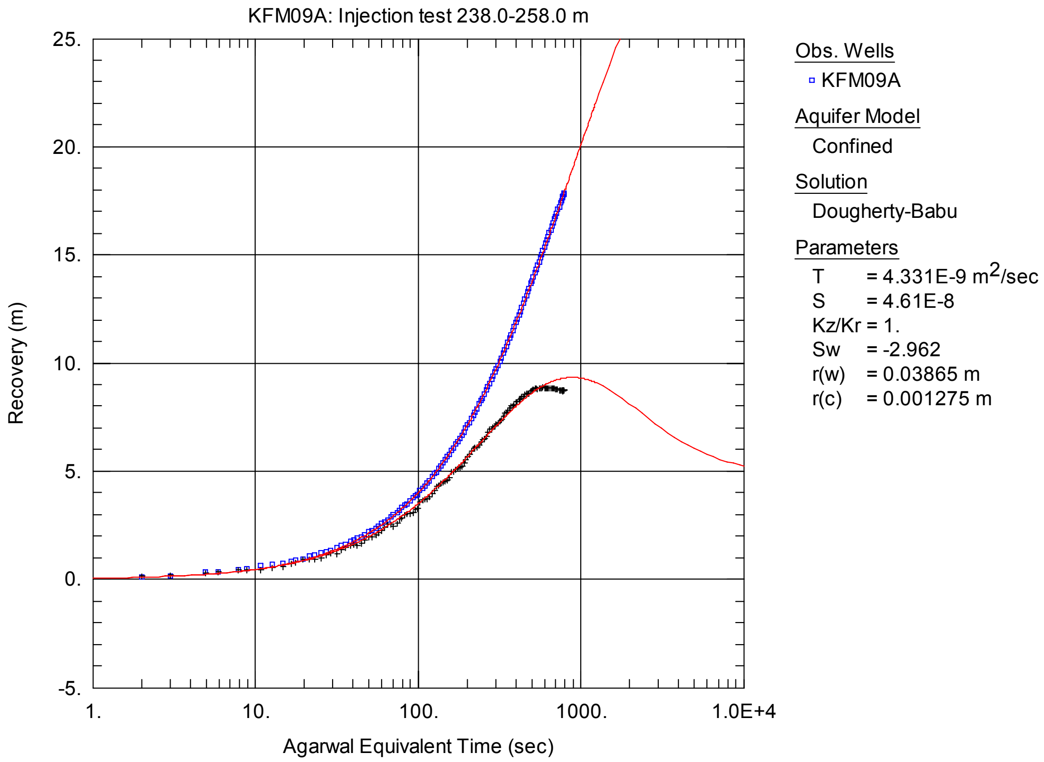


Figure A3-72. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in 238.0-258.0 m in KFM09A.*

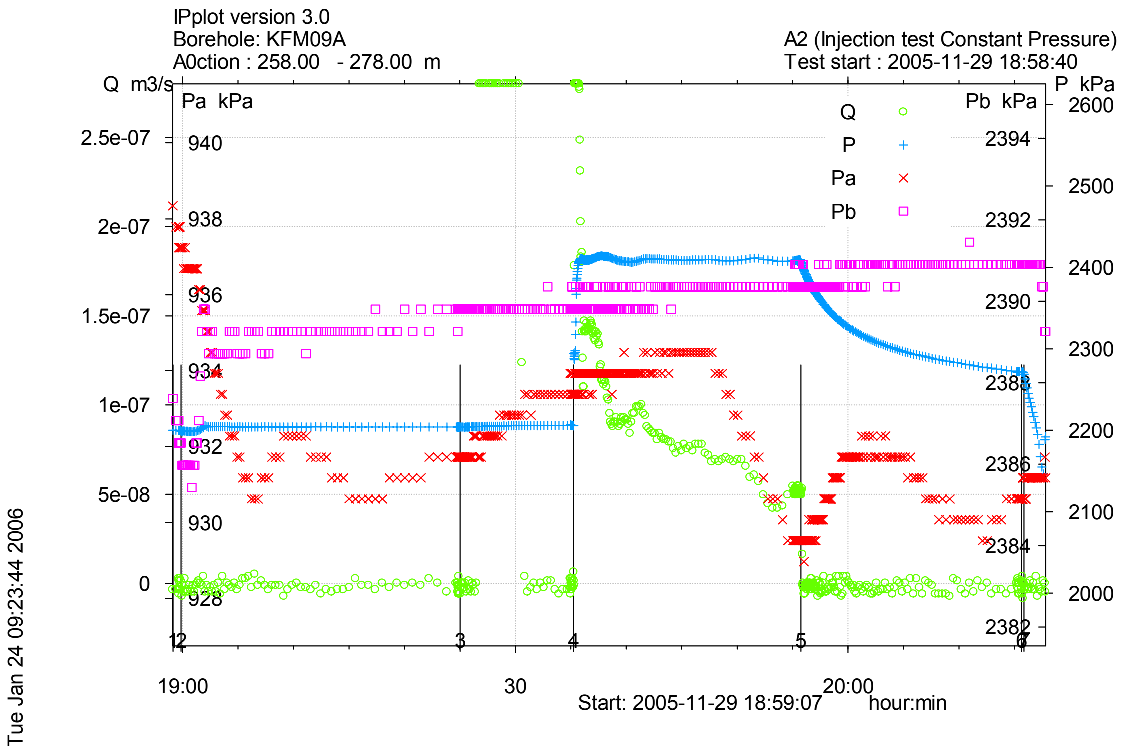


Figure A3-73. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 258.0-278.0 m in borehole KFM09A.*

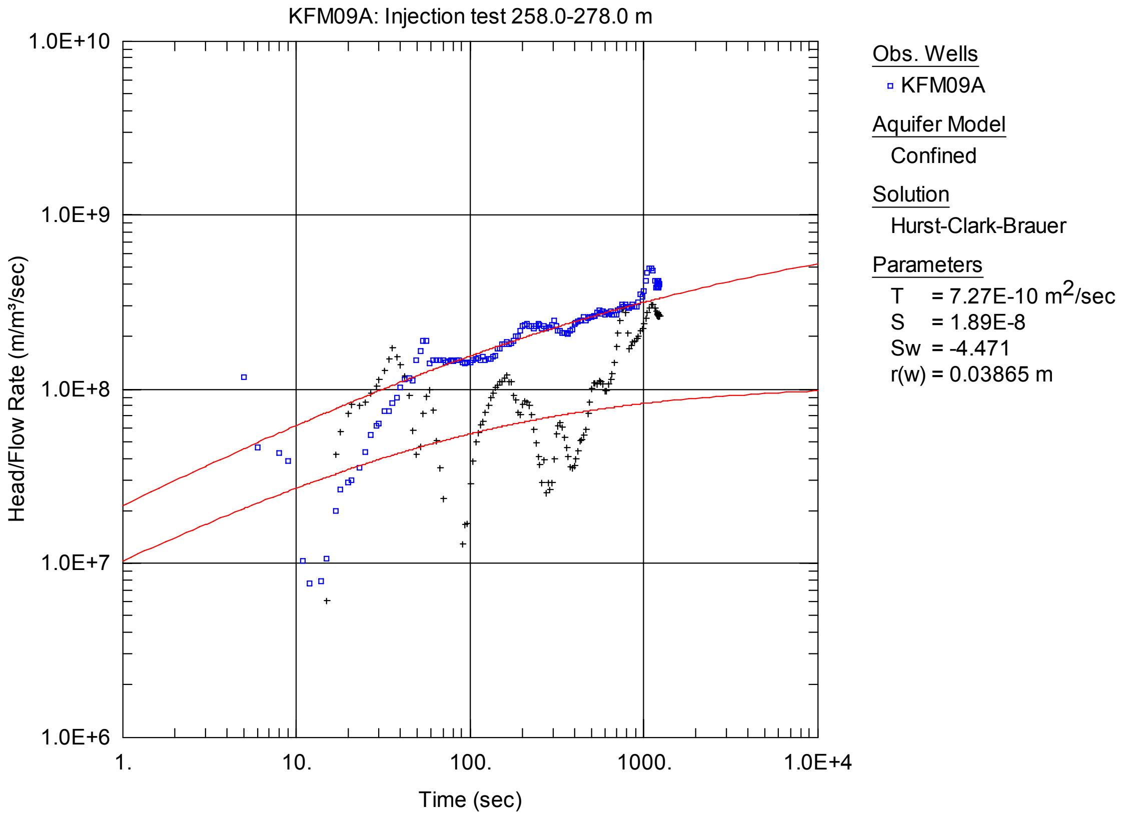


Figure A3-74. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 258.0-278.0 m in KFM09A.*

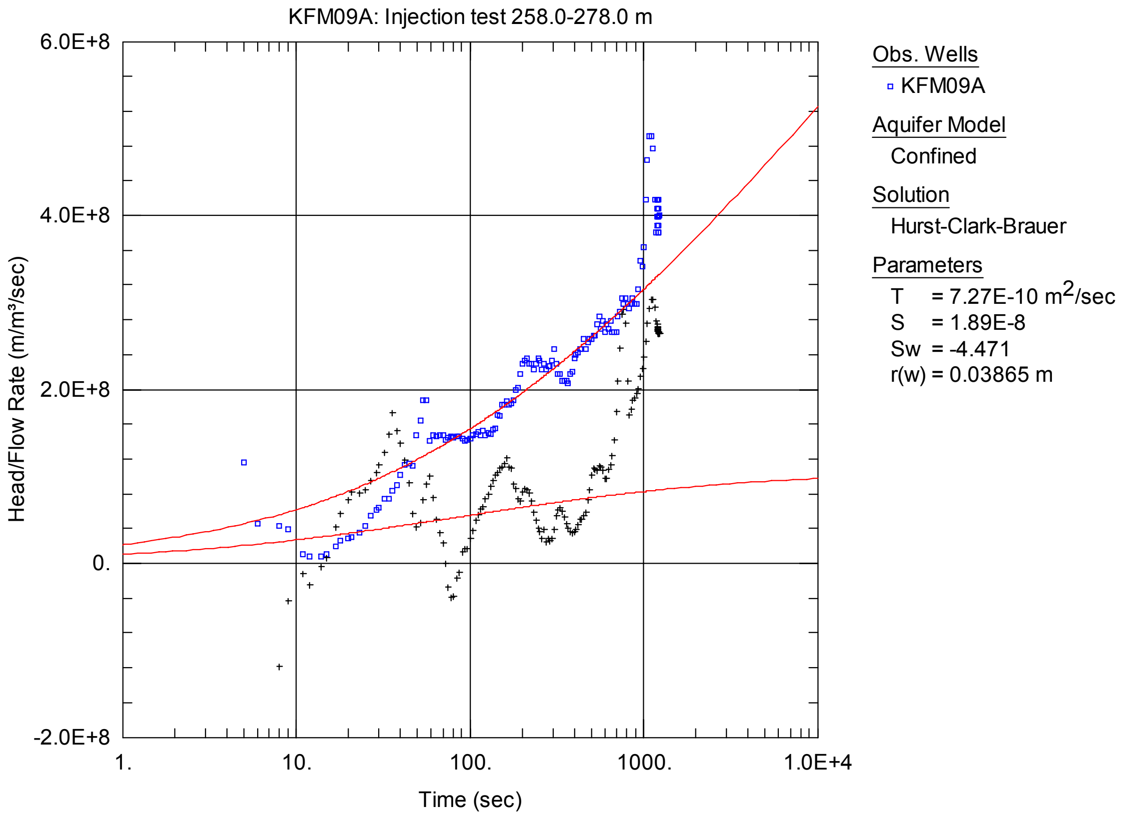


Figure A3-75. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 258.0-278.0 m in KFM09A.*

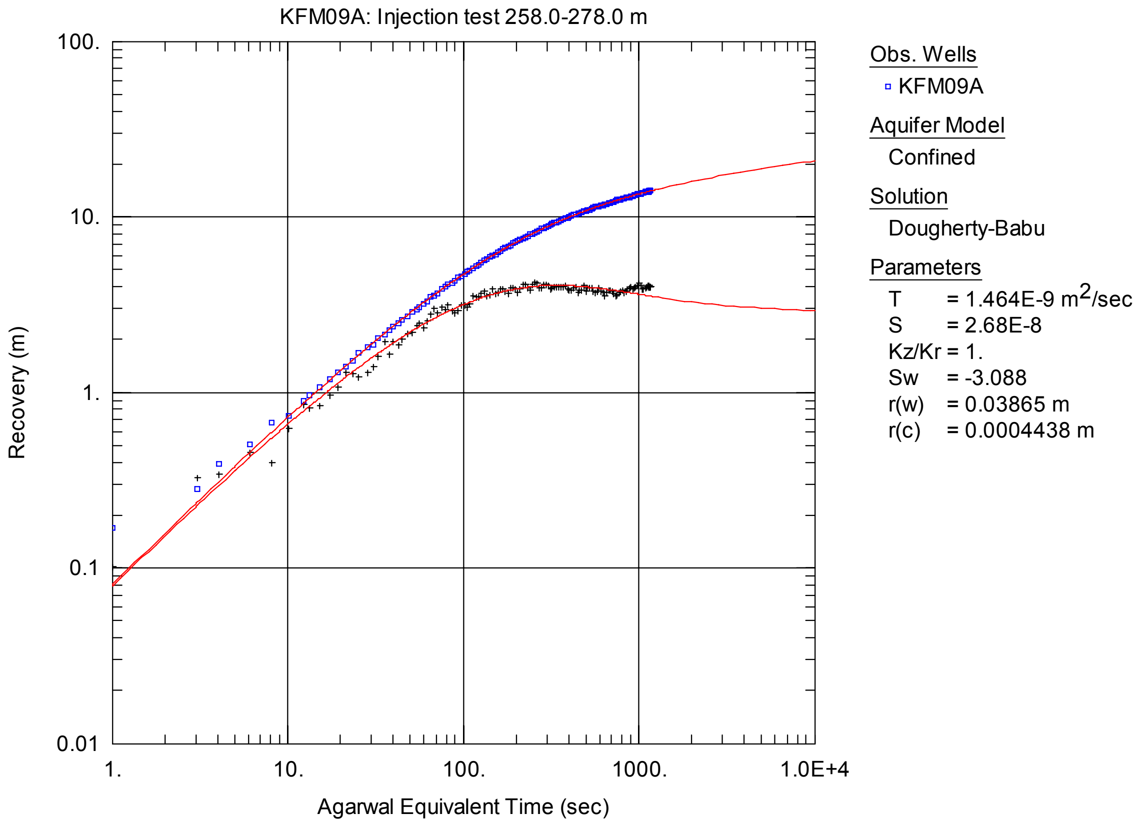


Figure A3-76. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 258.0-278.0 m in KFM09A.*

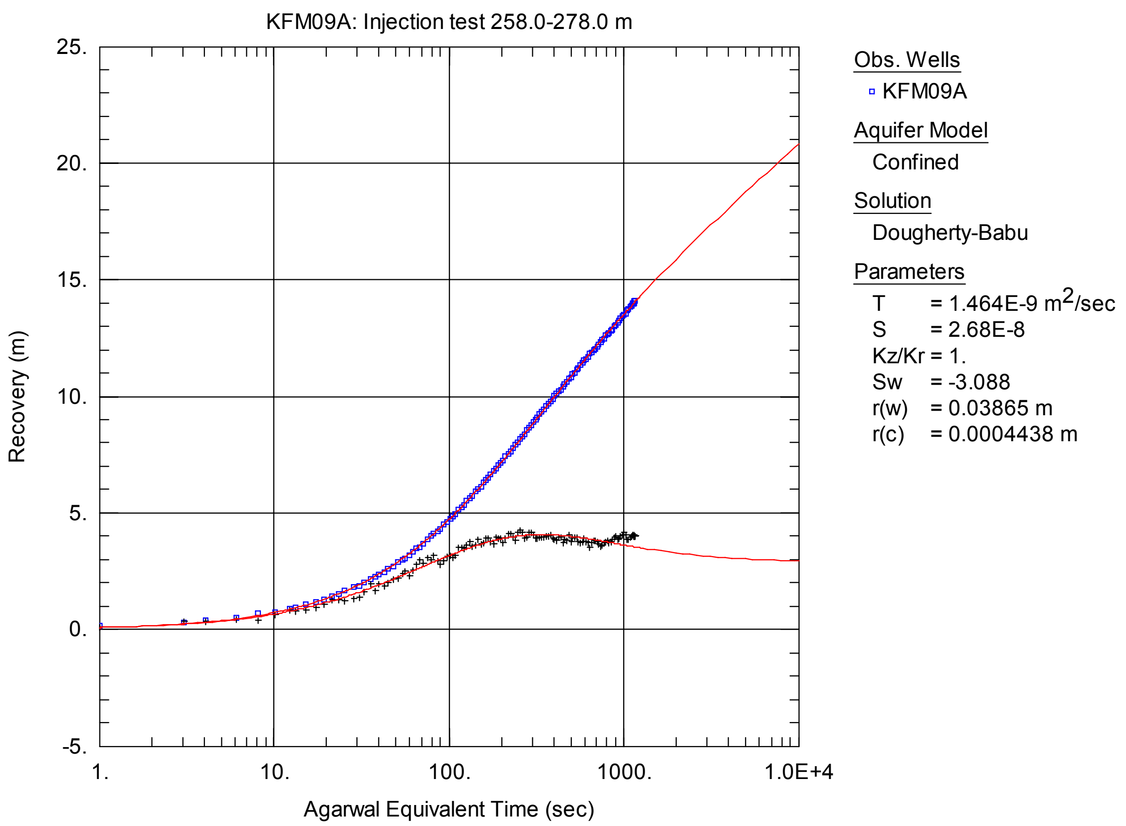


Figure A3-77. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 258.0-278.0 m in KFM09A.*

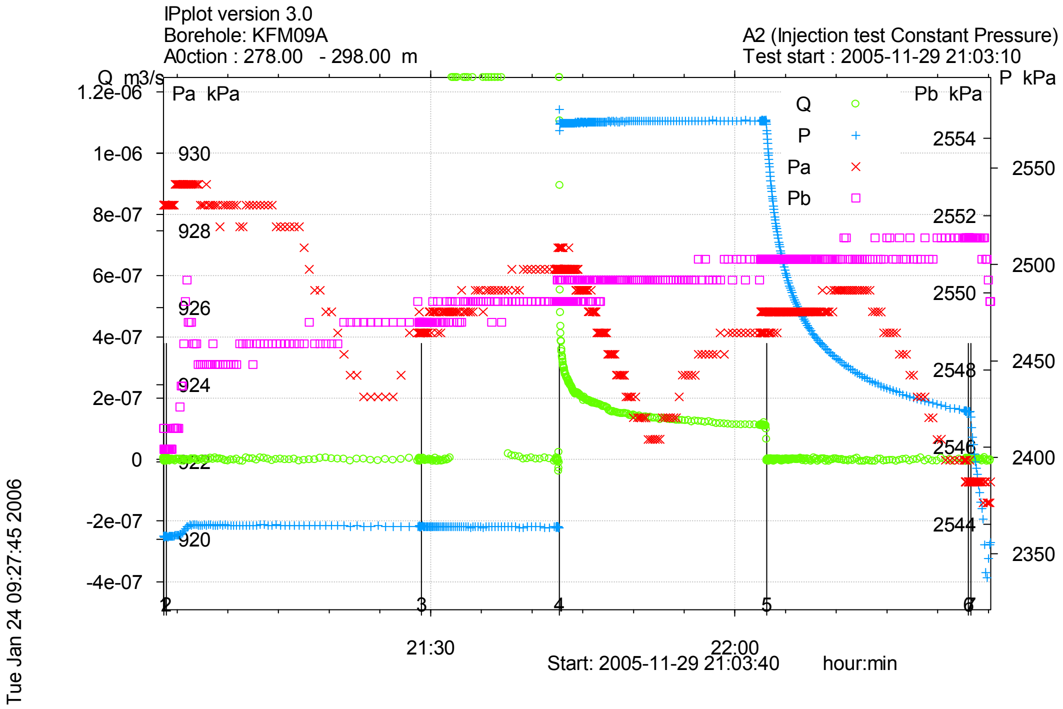


Figure A3-78. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 278.0-298.0 m in borehole KFM09A.*

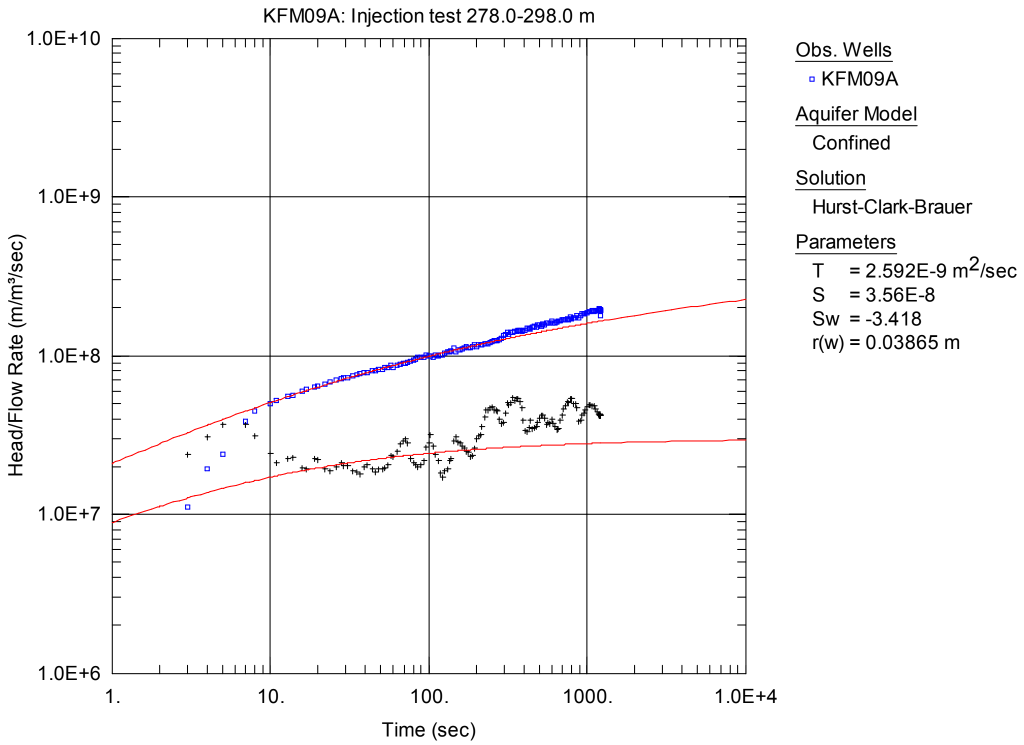


Figure A3-79. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 278.0-298.0 m in KFM09A. This plot shows the first of two different PRF:s during the injection period in this section.*

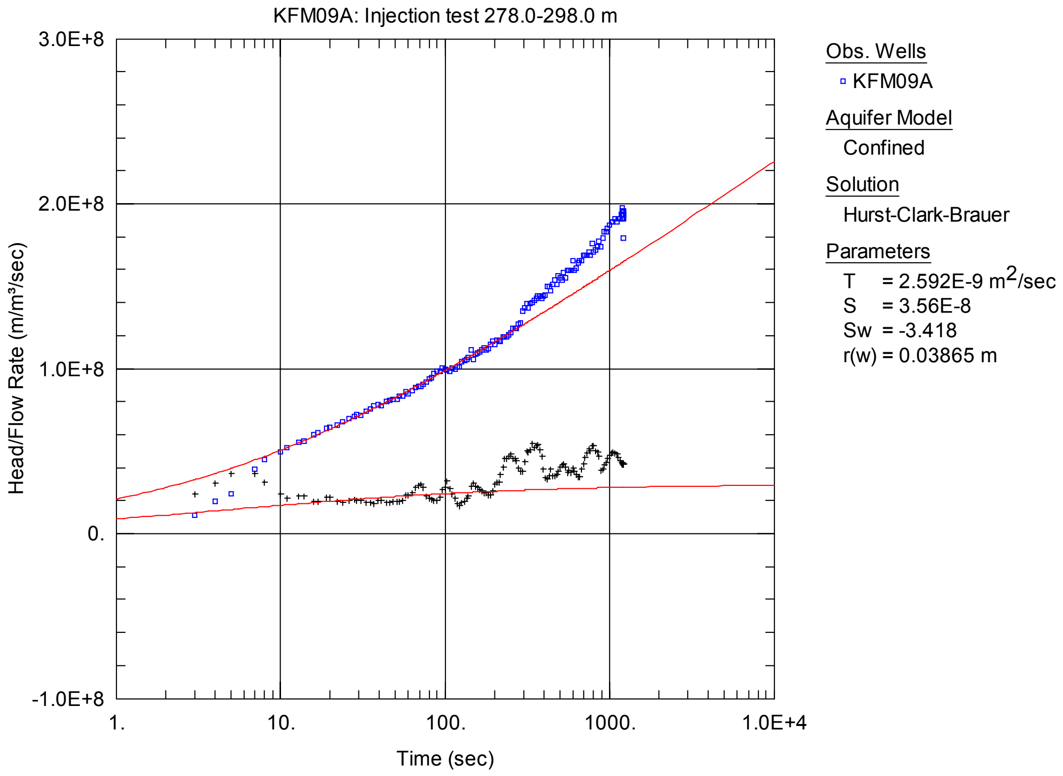


Figure A3-80. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 278.0-298.0x m in KFM09A. This plot shows the first of two different PRF:s during the injection period in this section.*

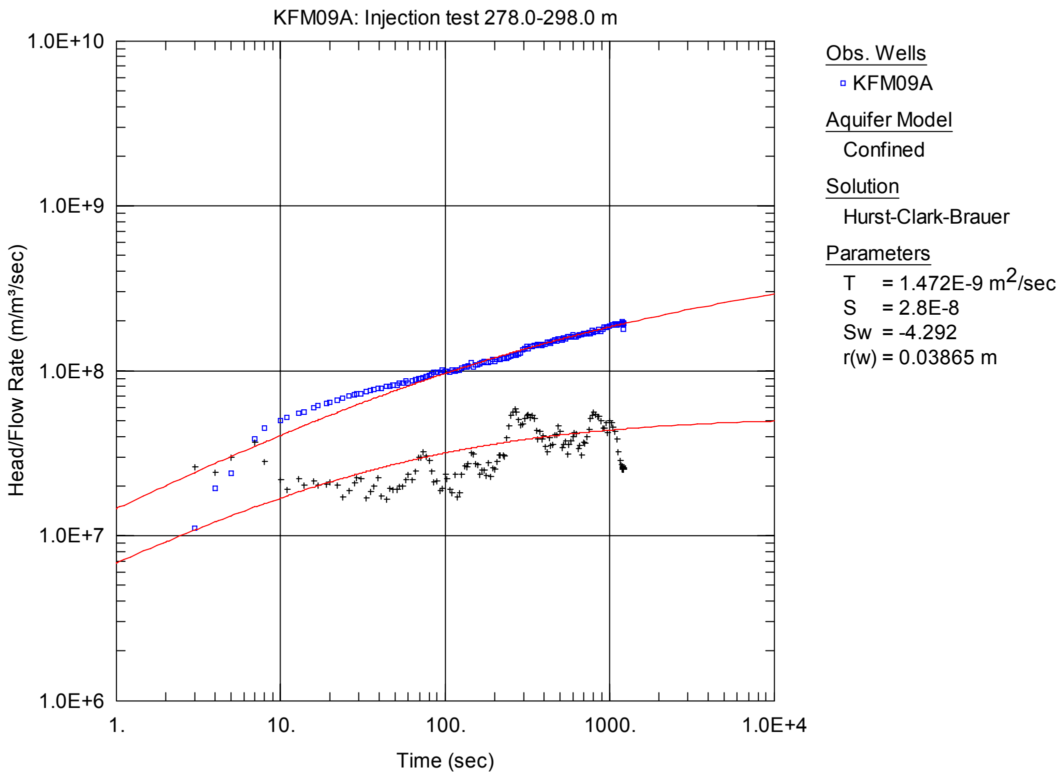


Figure A3-81. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 278.0-298.0 m in KFM09A. This plot shows the second of two different PRF:s during the injection period in this section.*

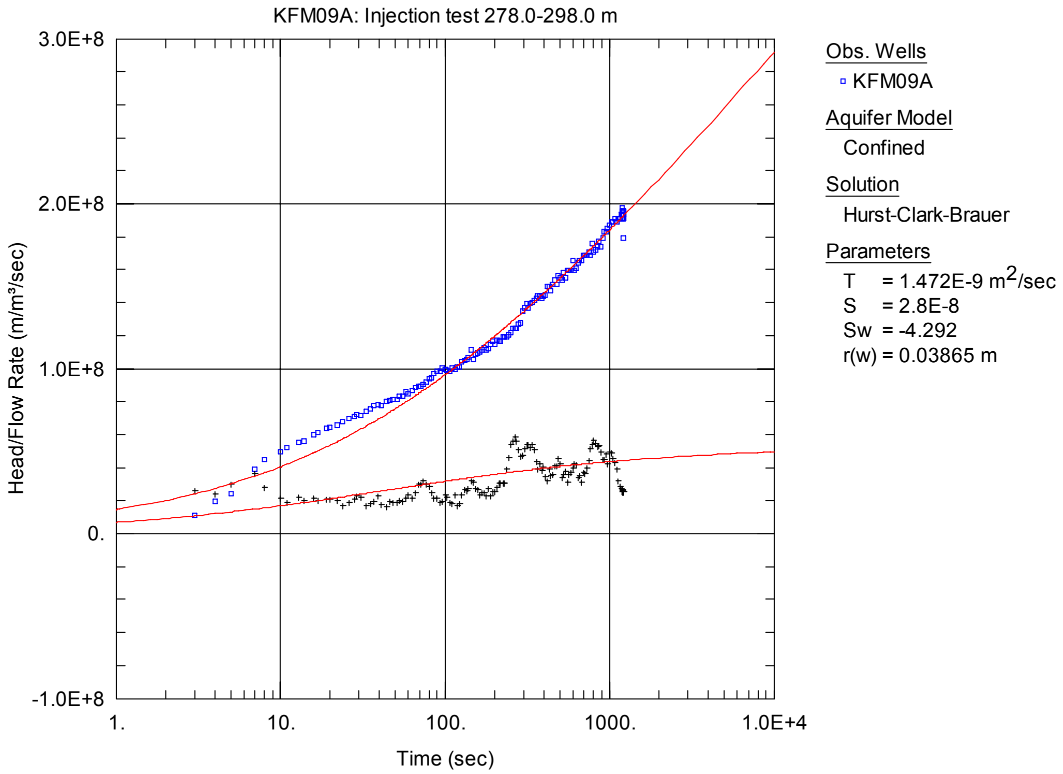


Figure A3-82. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 278.0-298.0 m in KFM09A. This plot shows the second of two different PRF:s during the injection period in this section.*

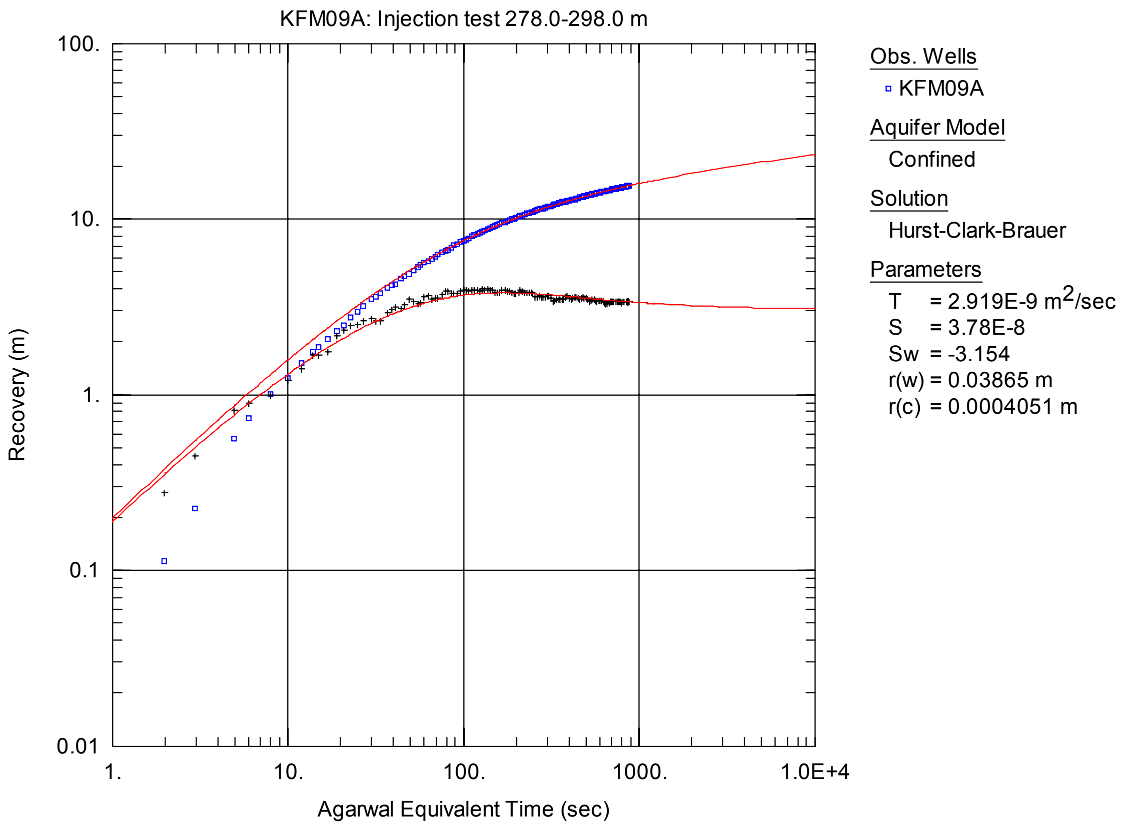


Figure A3-83. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 278.0-298.0 m in KFM09A.*

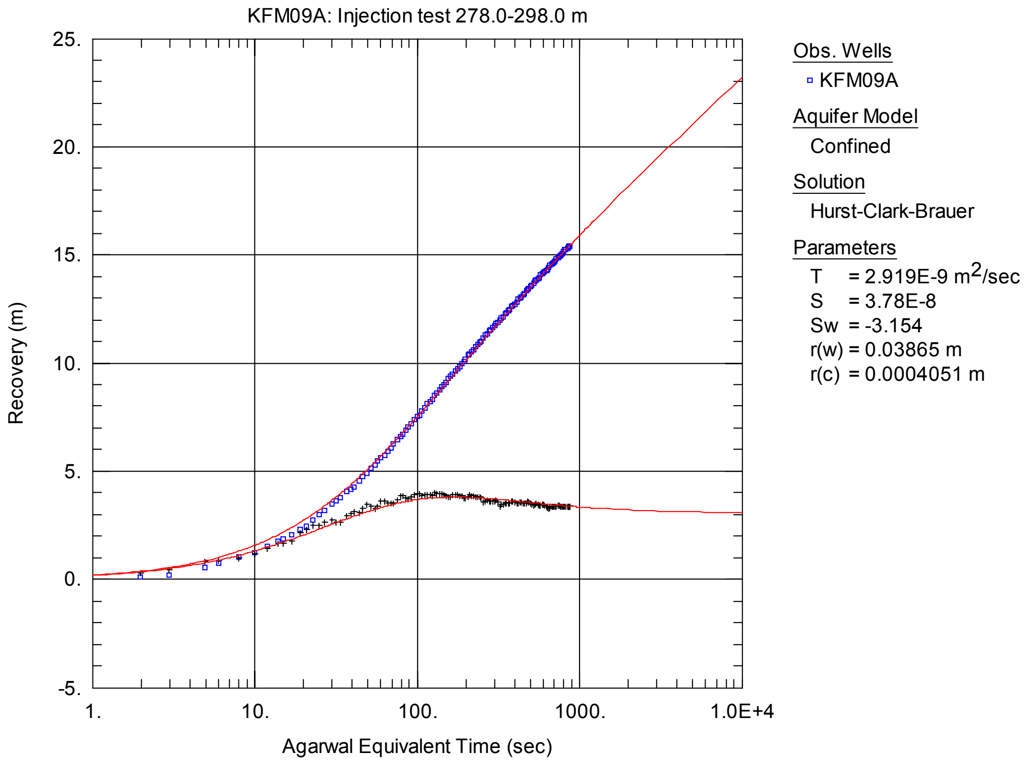


Figure A3-84. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in 278.0-298.0 m in KFM09A.*

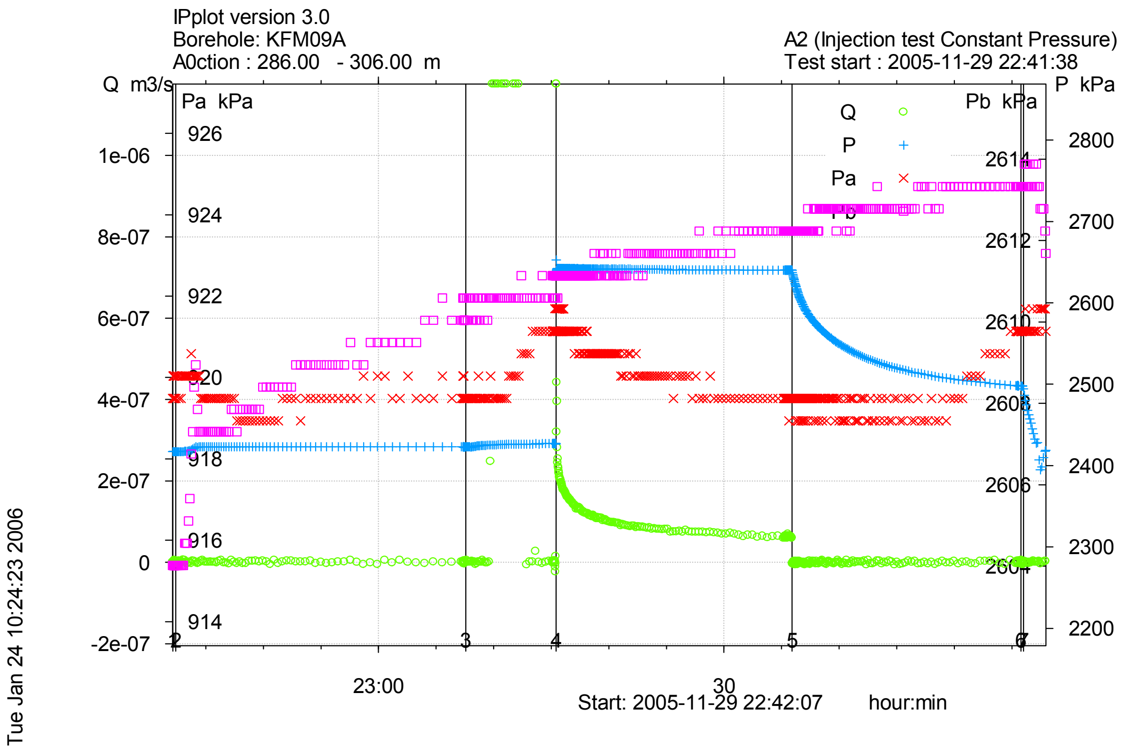


Figure A3-85. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 286.0-306.0 m in borehole KFM09A.*

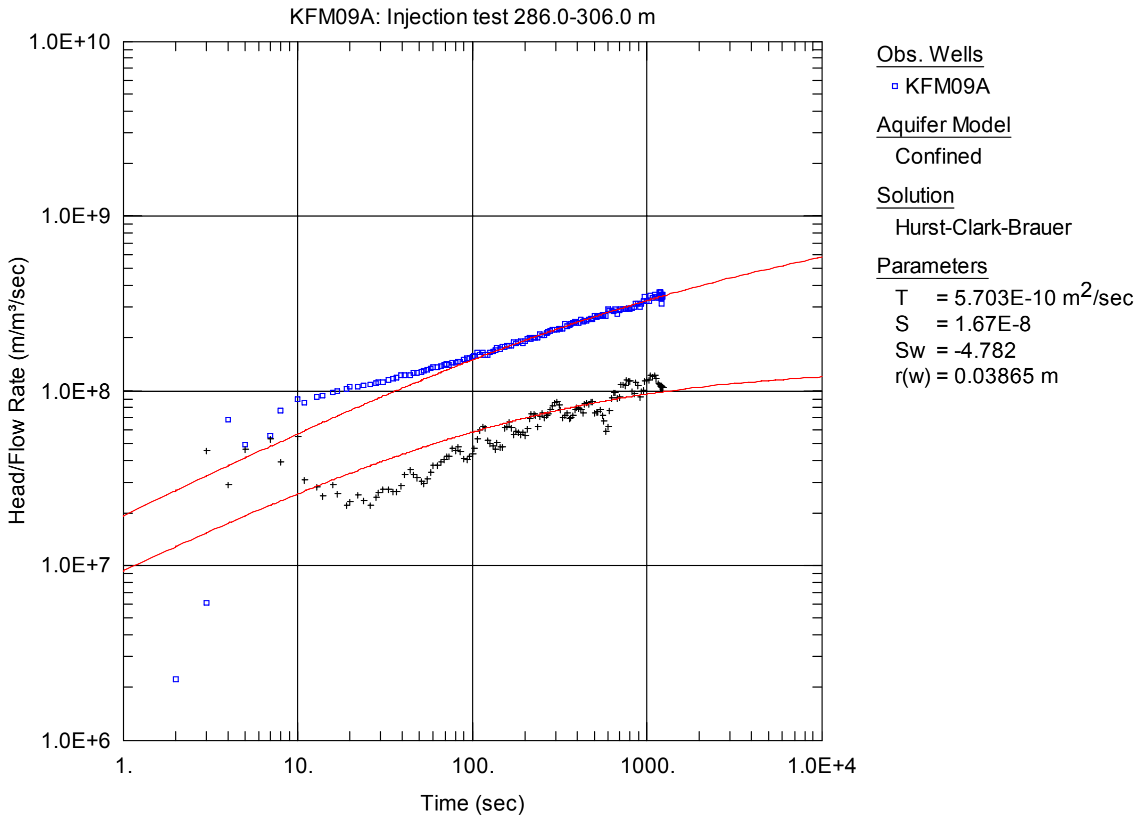


Figure A3-86. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 286.0-306.0 m in KFM09A.*

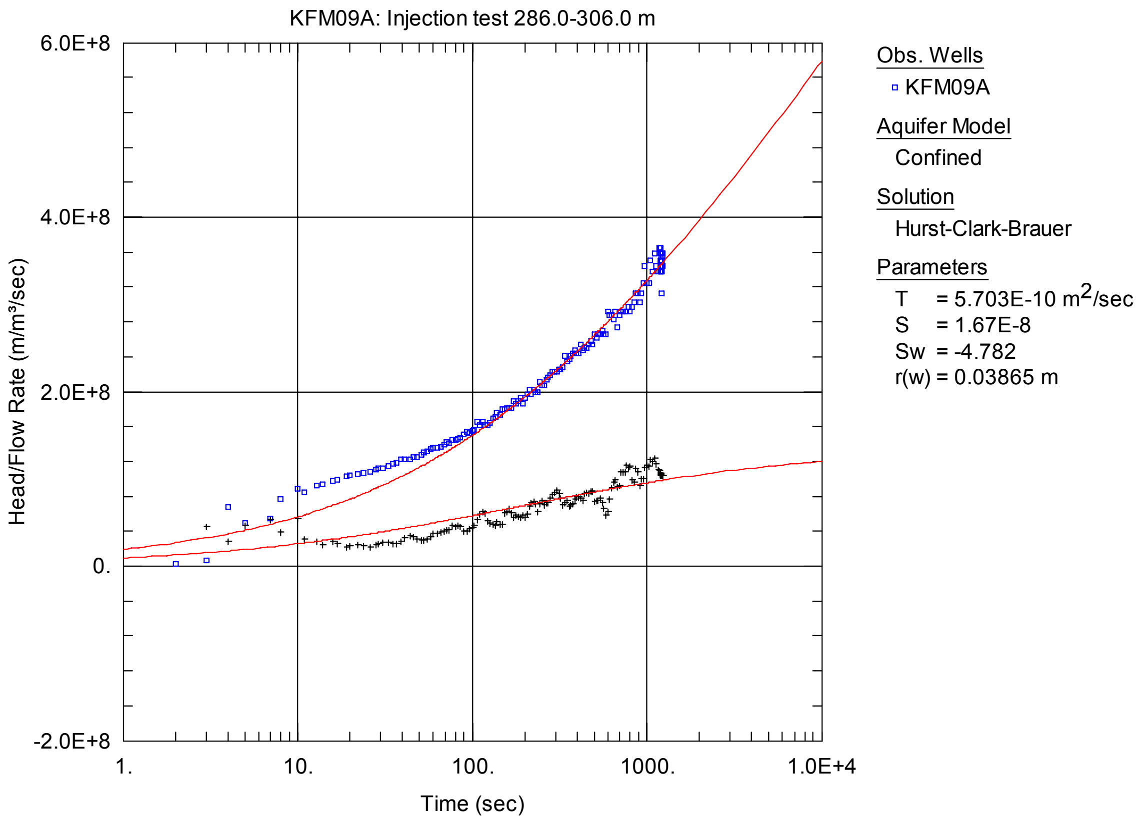


Figure A3-87. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 286.0-306.0 m in KFM09A.*

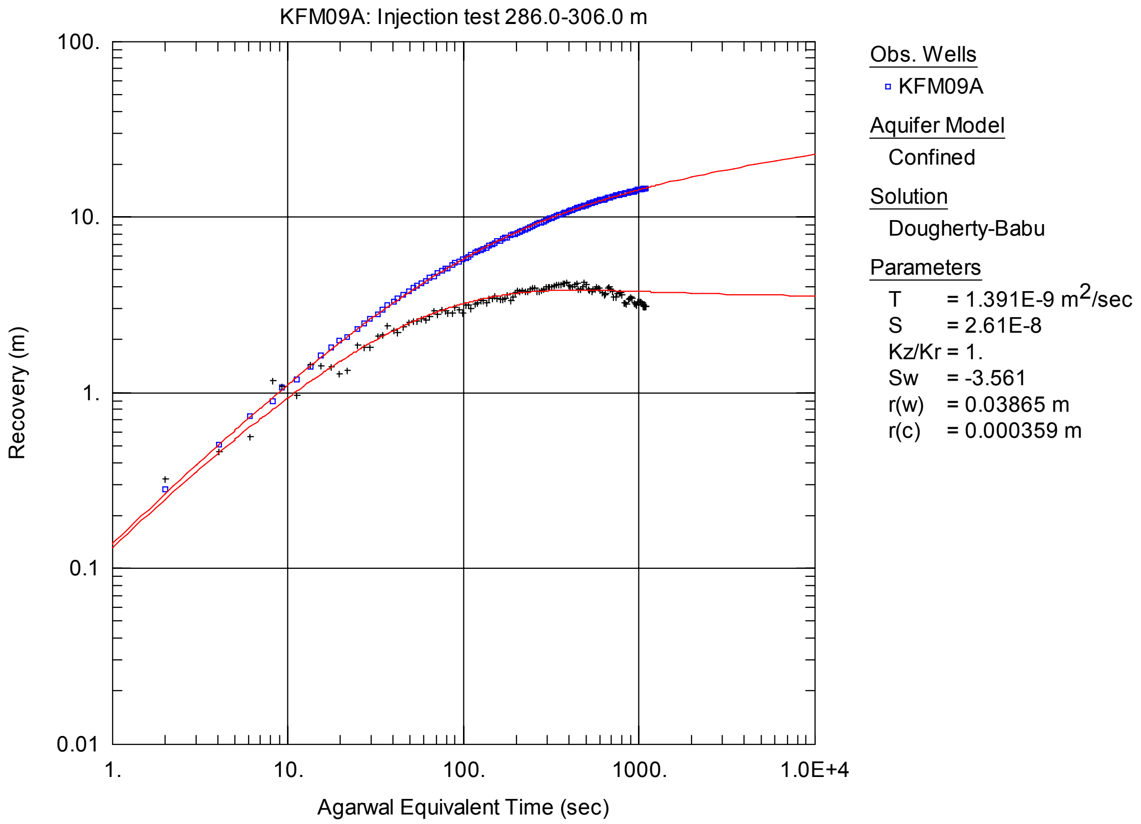


Figure A3-88. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 286.0-306.0 m in KFM09A.*

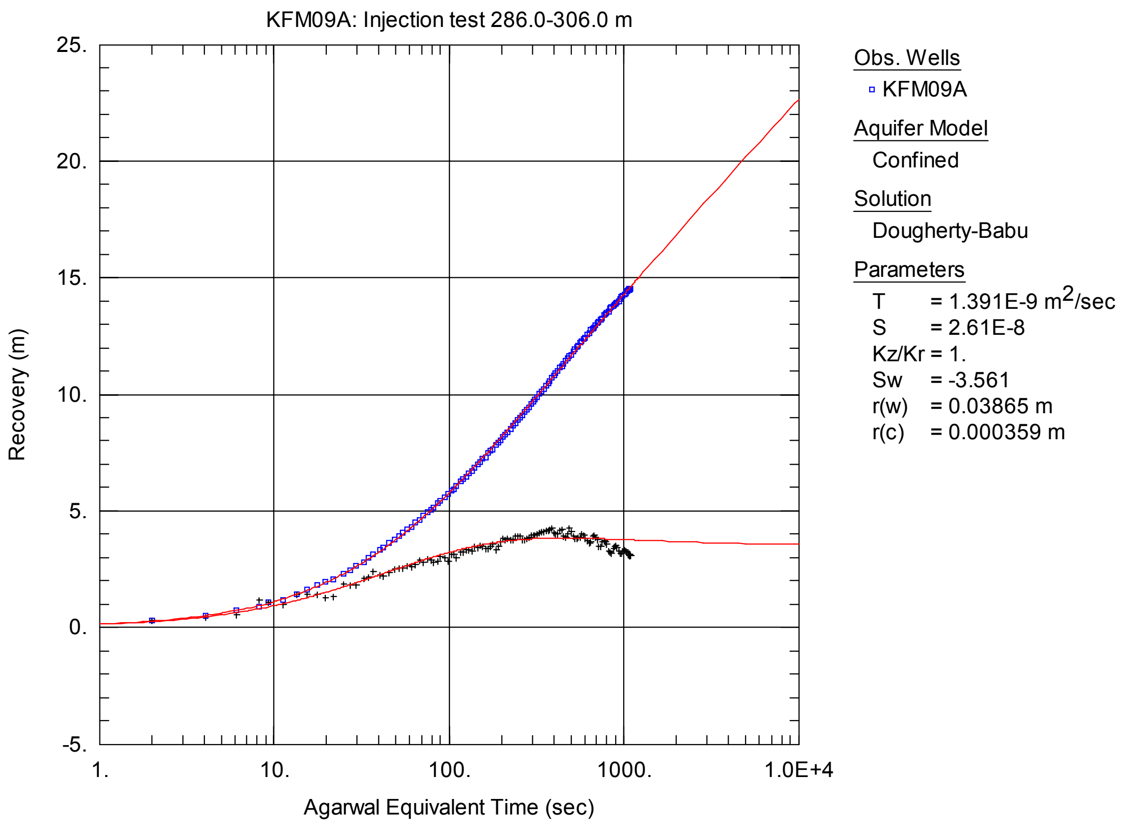


Figure A3-89. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 286.0-306.0 m in KFM09A.*

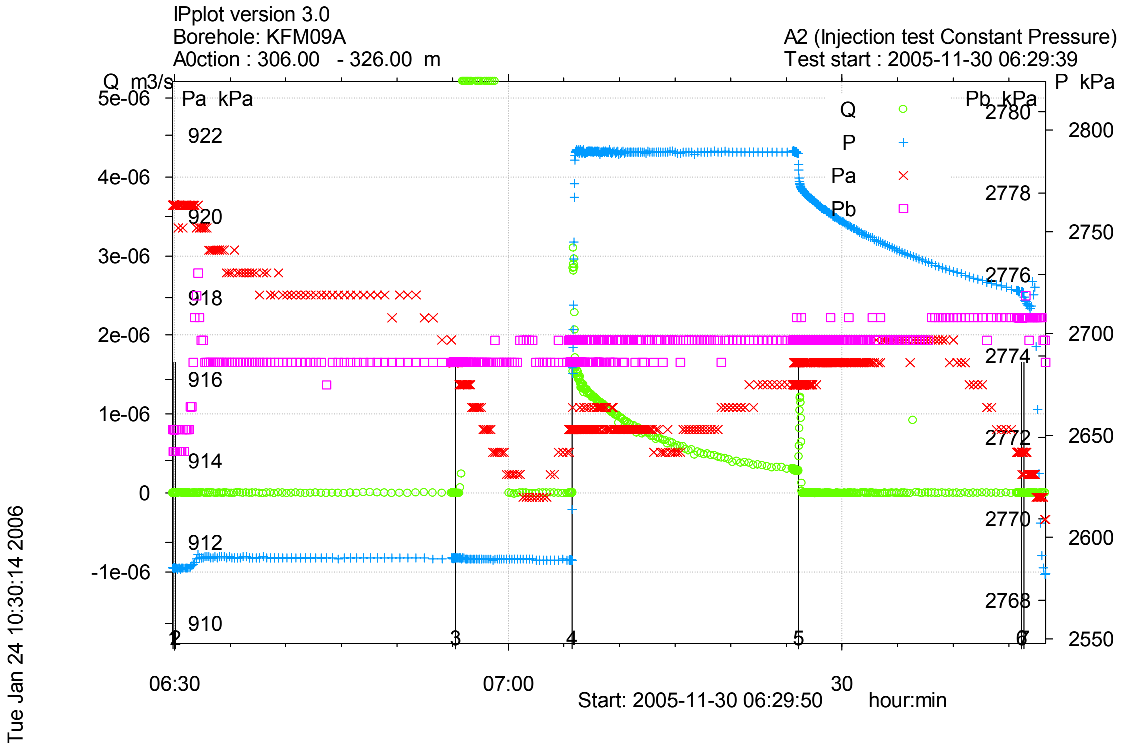


Figure A3-90. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 306.0-326.0 m in borehole KFM09A.*

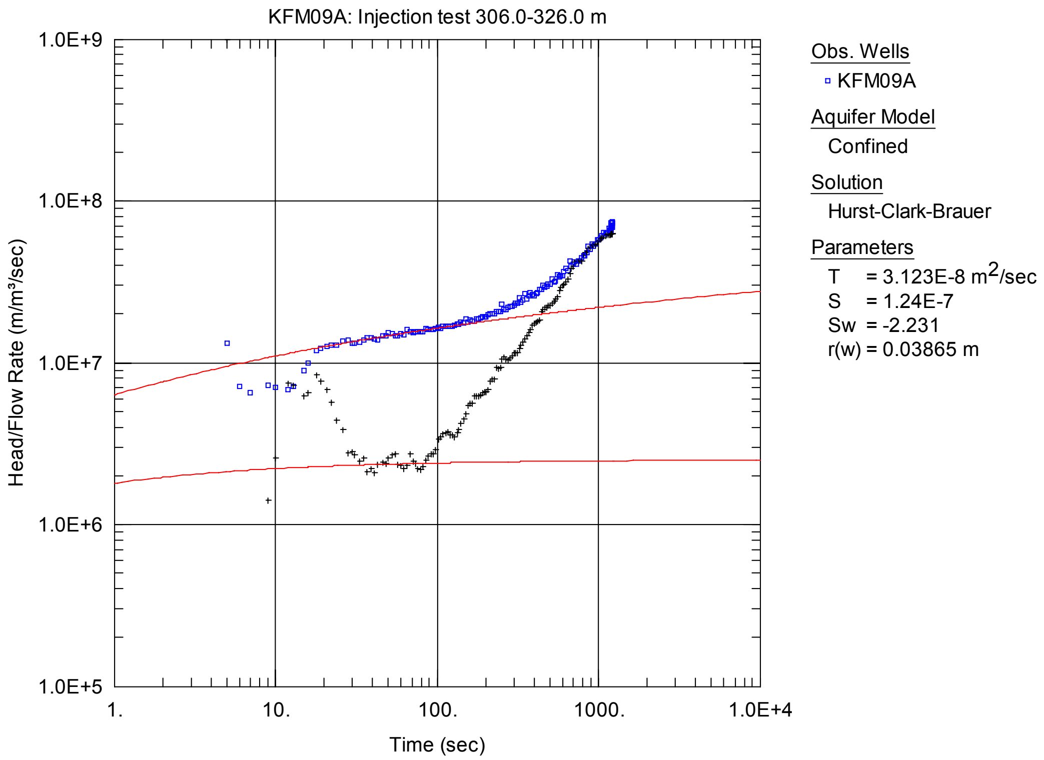


Figure A3-91. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 306.0-326.0 m in KFM09A.*

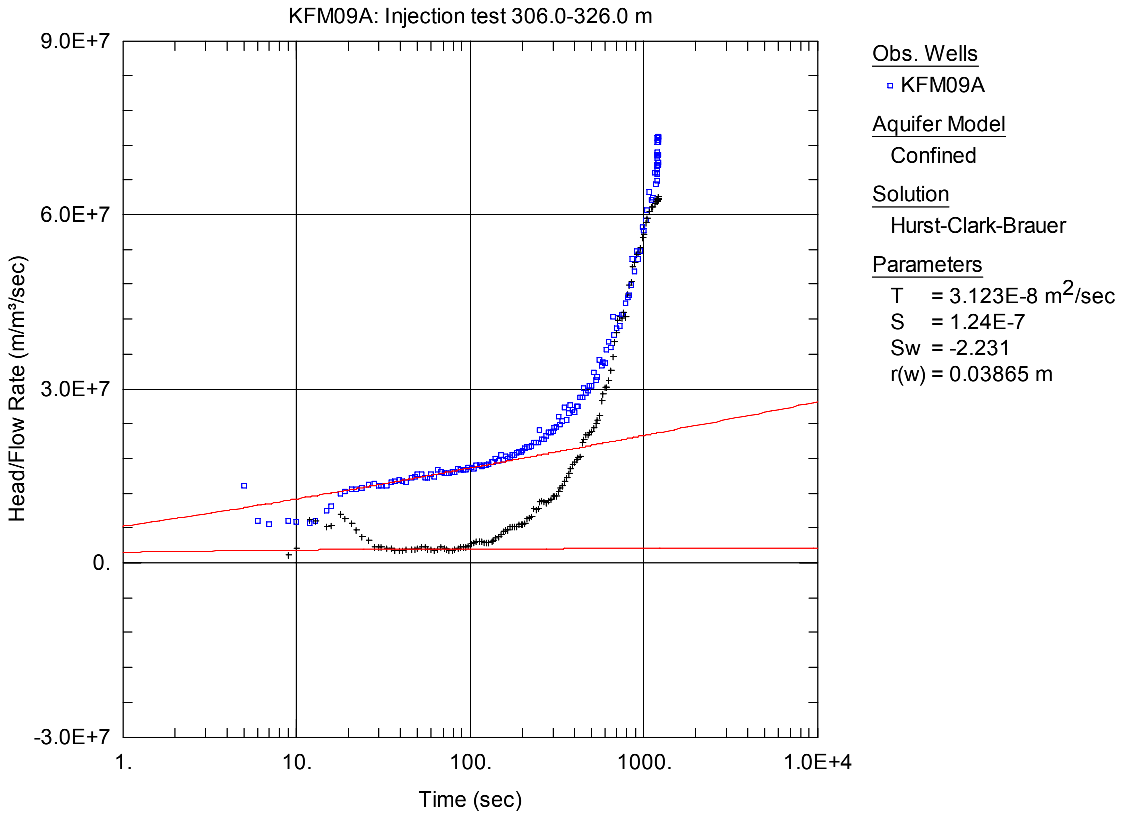


Figure A3-92. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 306.0-326.0 m in KFM09A.*

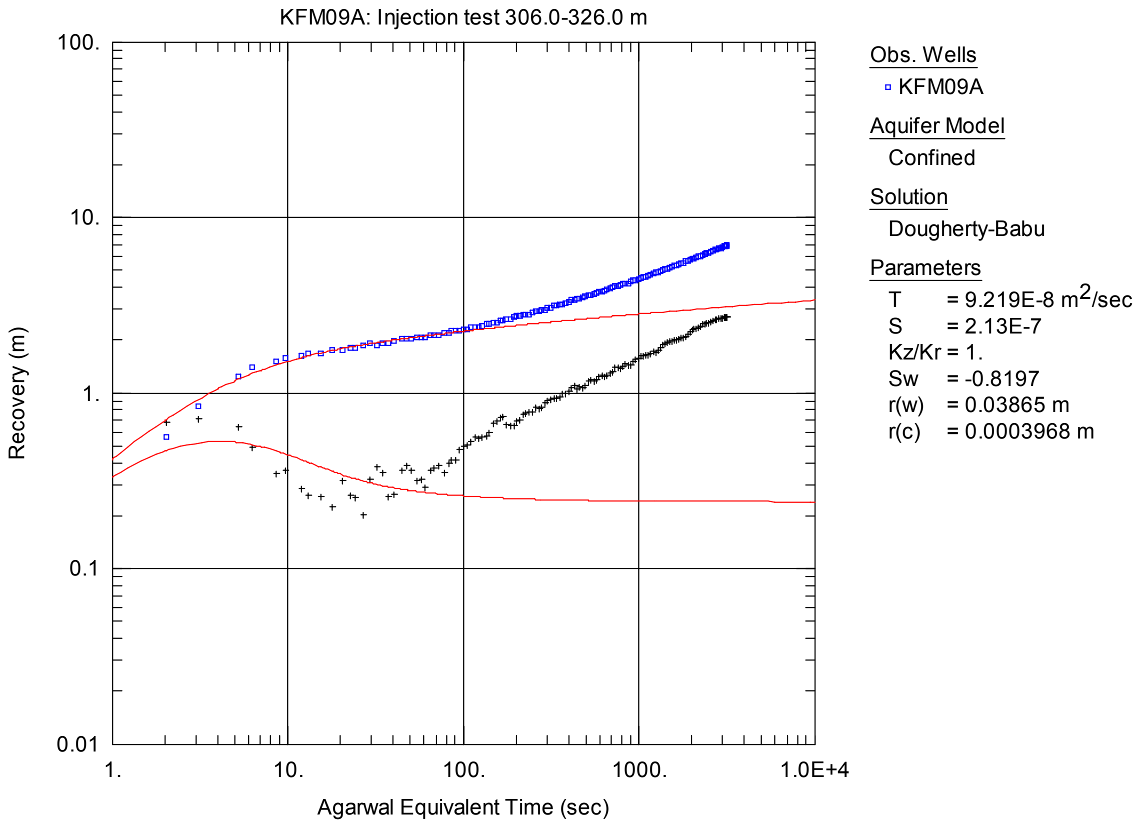


Figure A3-93. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 306.0-326.0 m in KFM09A.*

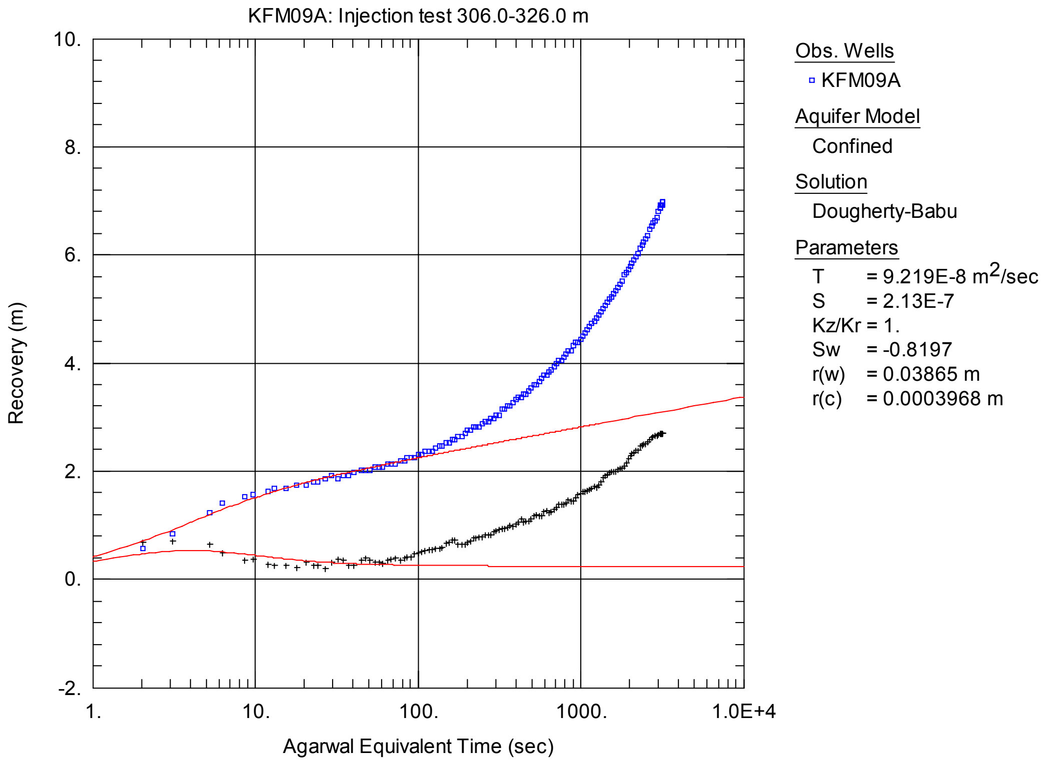


Figure A3-94. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 306.0-326.0 m in KFM09A.*

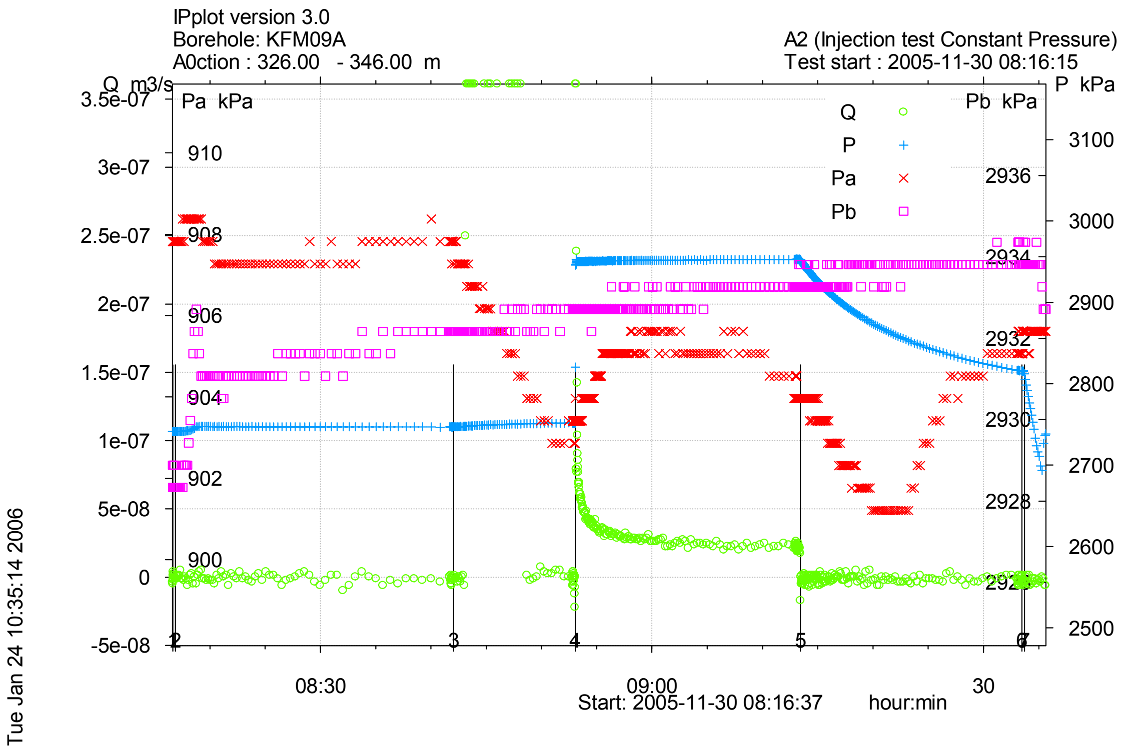


Figure A3-95. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 326.0-346.0 m in borehole KFM09A.*

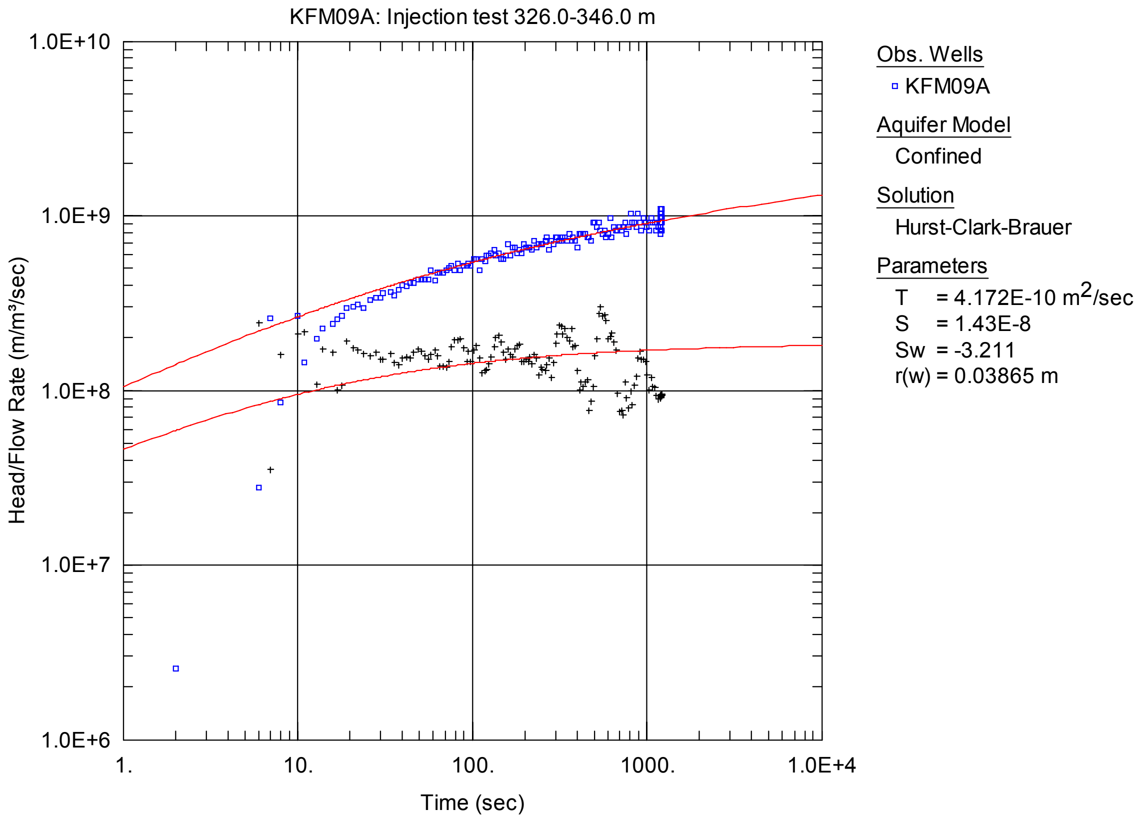


Figure A3-96. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in 326.0-346.0 m in KFM09A.*

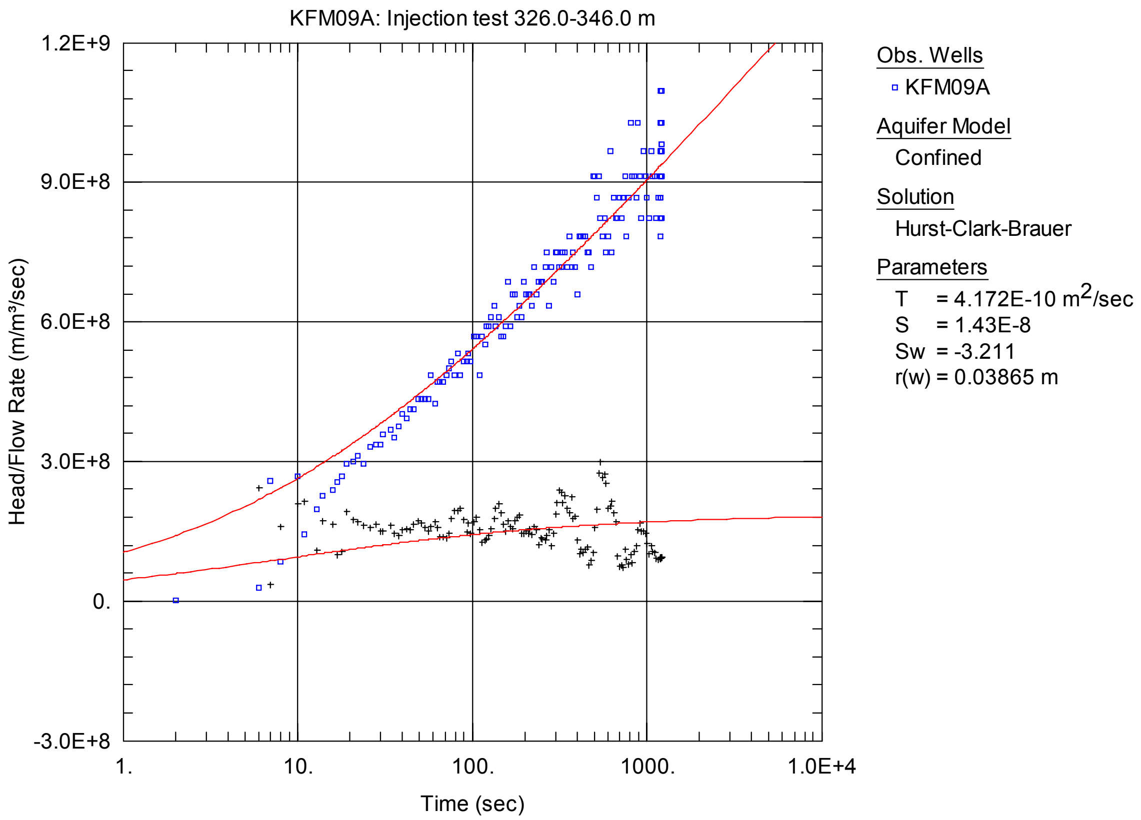


Figure A3-97. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 326.0-346.0 m in KFM09A.*

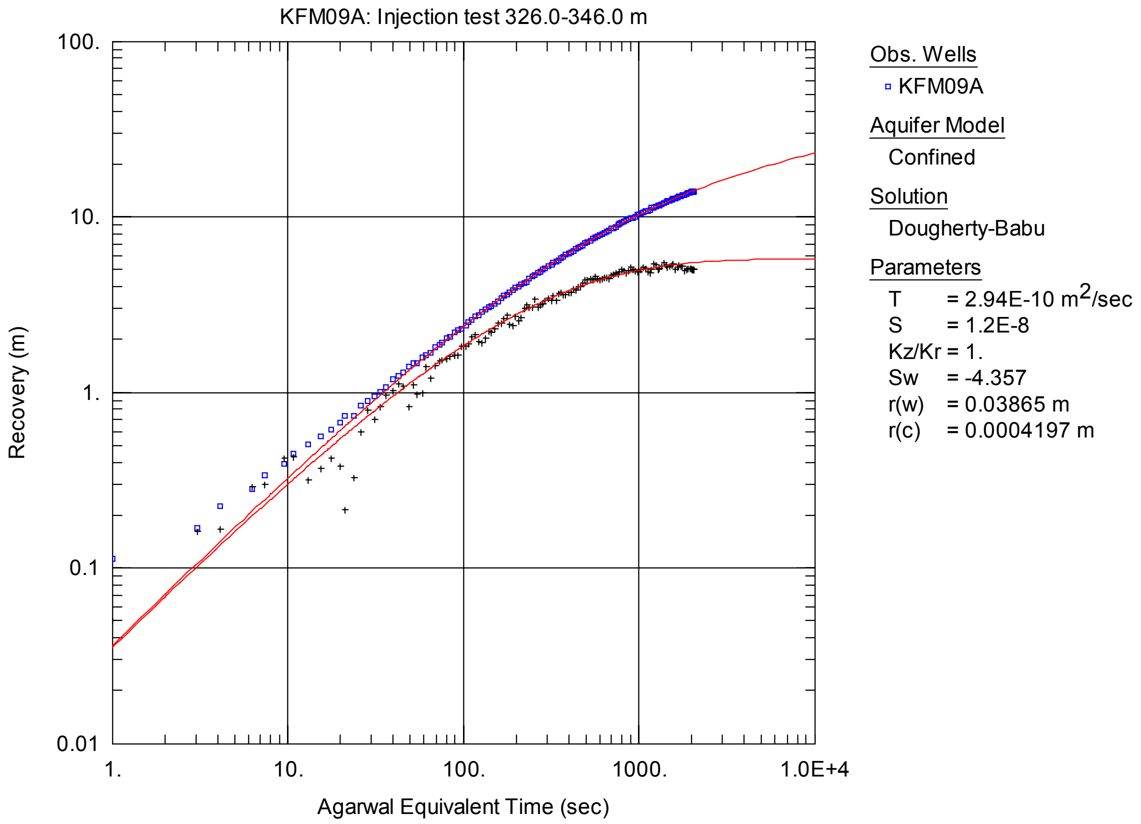


Figure A3-98. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 326.0-346.0 m in KFM09A.*

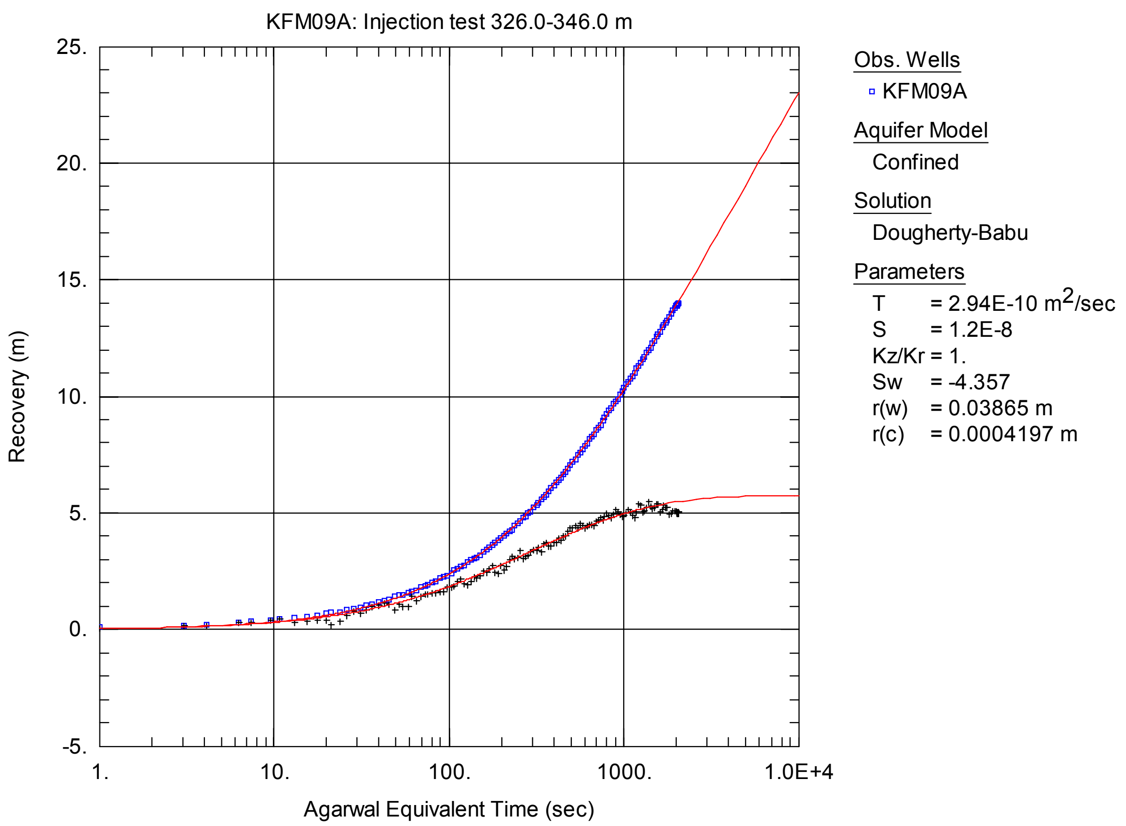


Figure A3-99. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 326.0-346.0 m in KFM09A.*

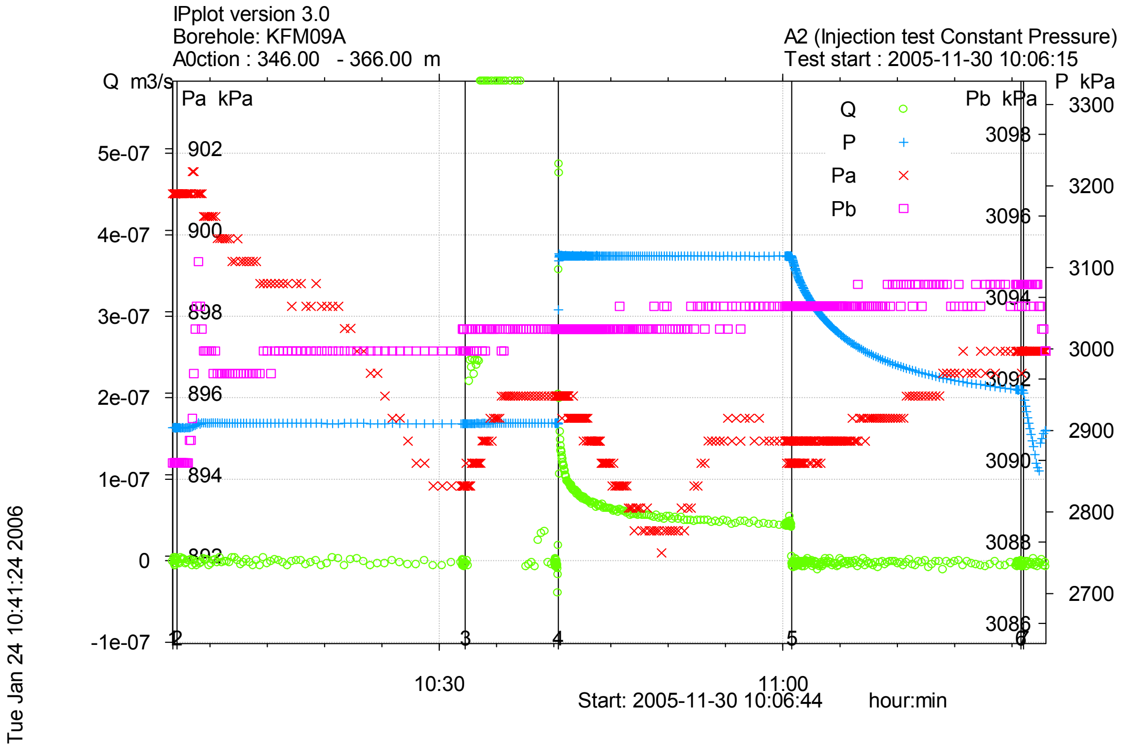


Figure A3-100. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 346.0-366.0 m in borehole KFM09A.*

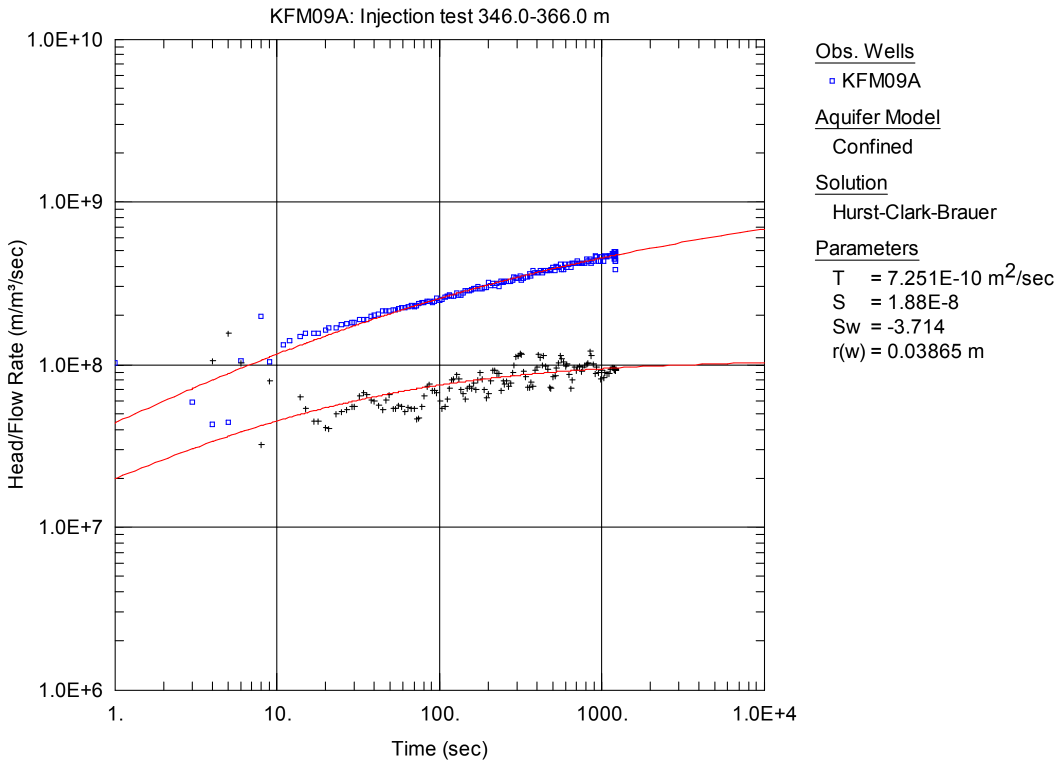


Figure A3-101. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 346.0-366.0 m in KFM09A.*

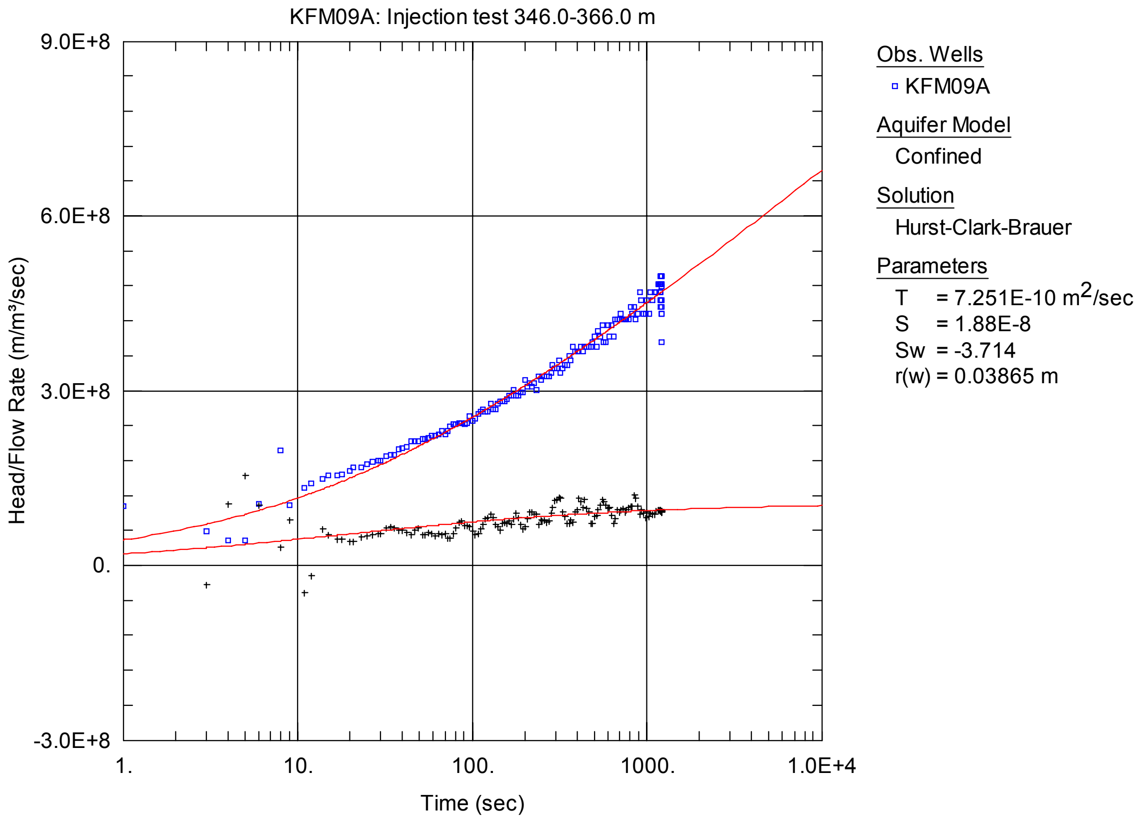


Figure A3-102. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in 346.0-366.0 m in KFM09A.*

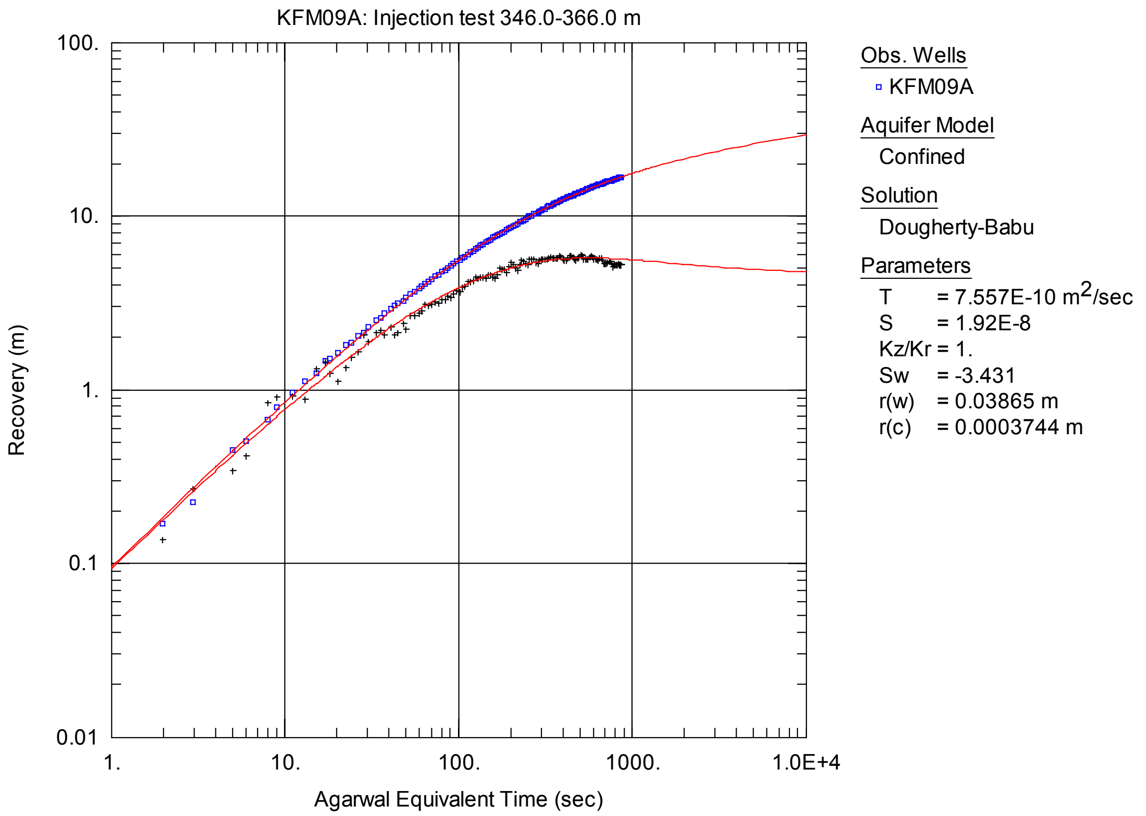


Figure A3-103. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 346.0-366.0 m in KFM09A.*

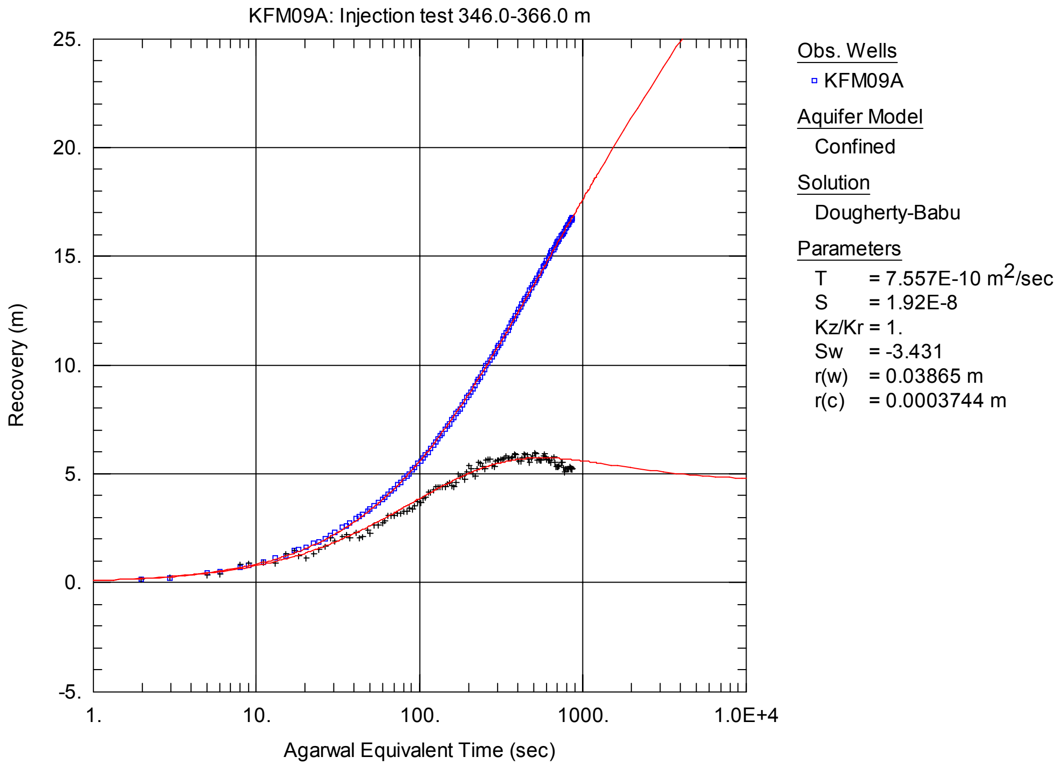


Figure A3-104. Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 346.0-366.0 m in KFM09A.

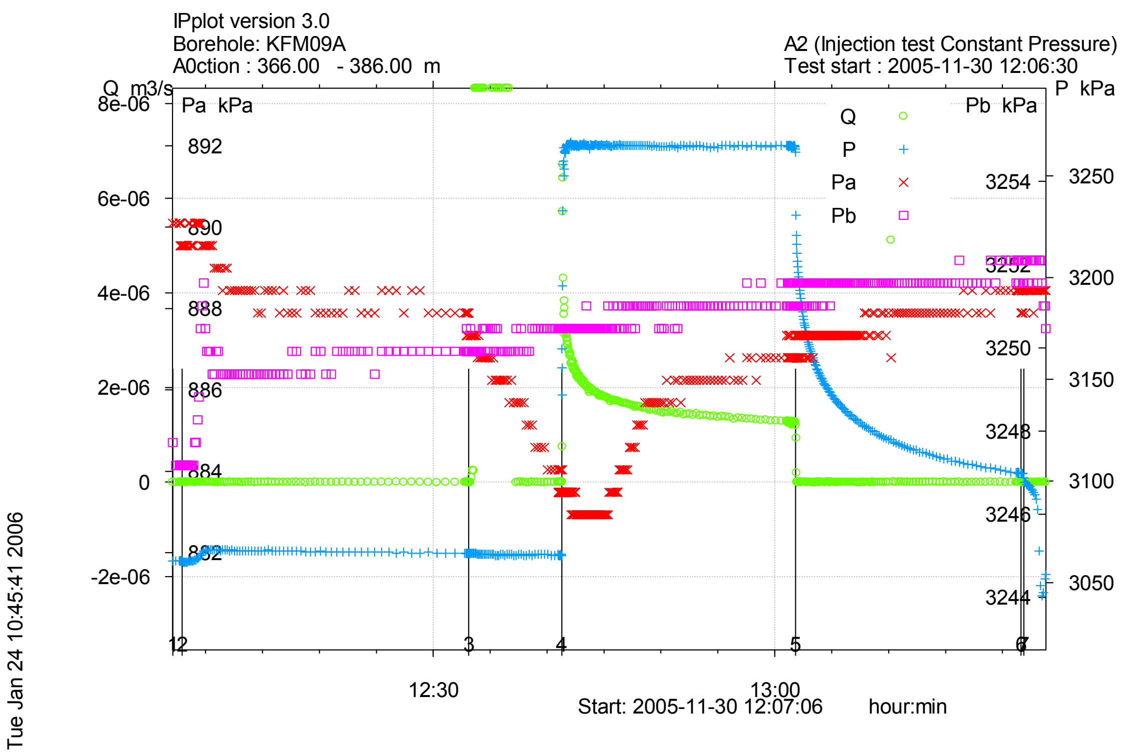


Figure A3-105. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 366.0-386.0 m in borehole KFM09A.

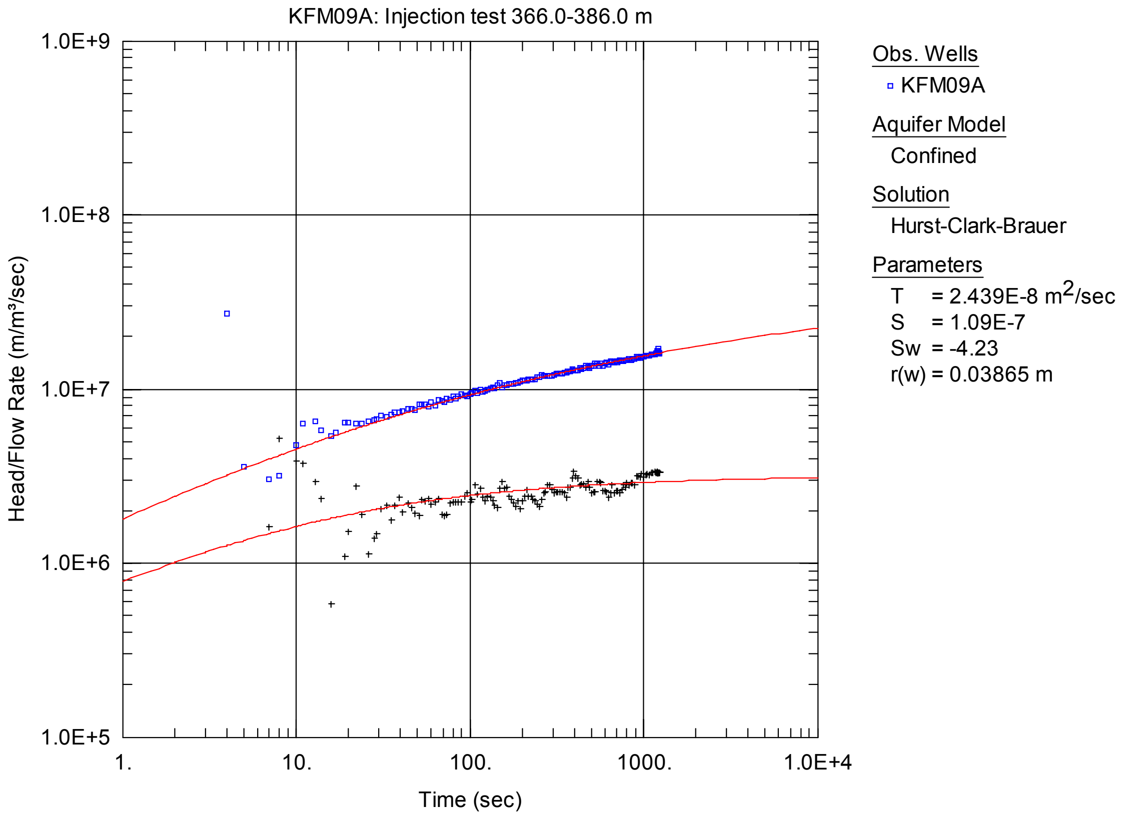


Figure A3-106. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 366.0-386.0 m in KFM09A.*

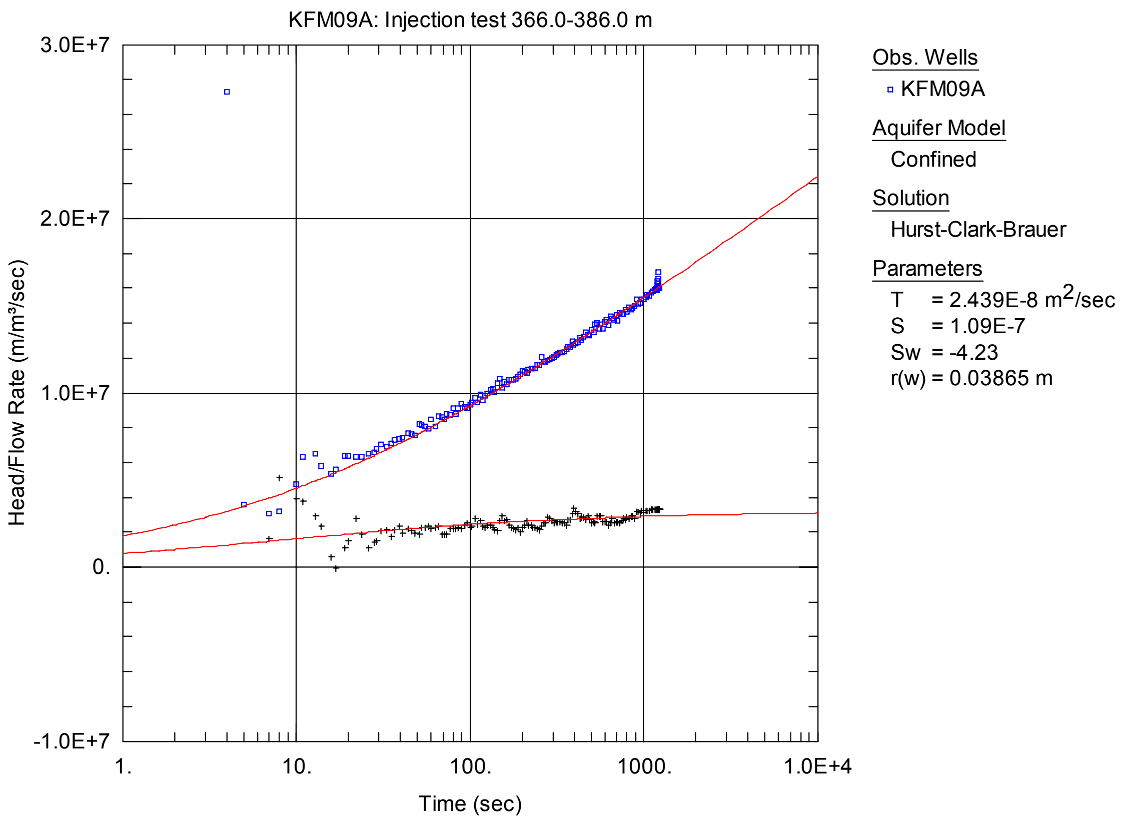


Figure A3-107. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 366.0-386.0 m in KFM09A.*

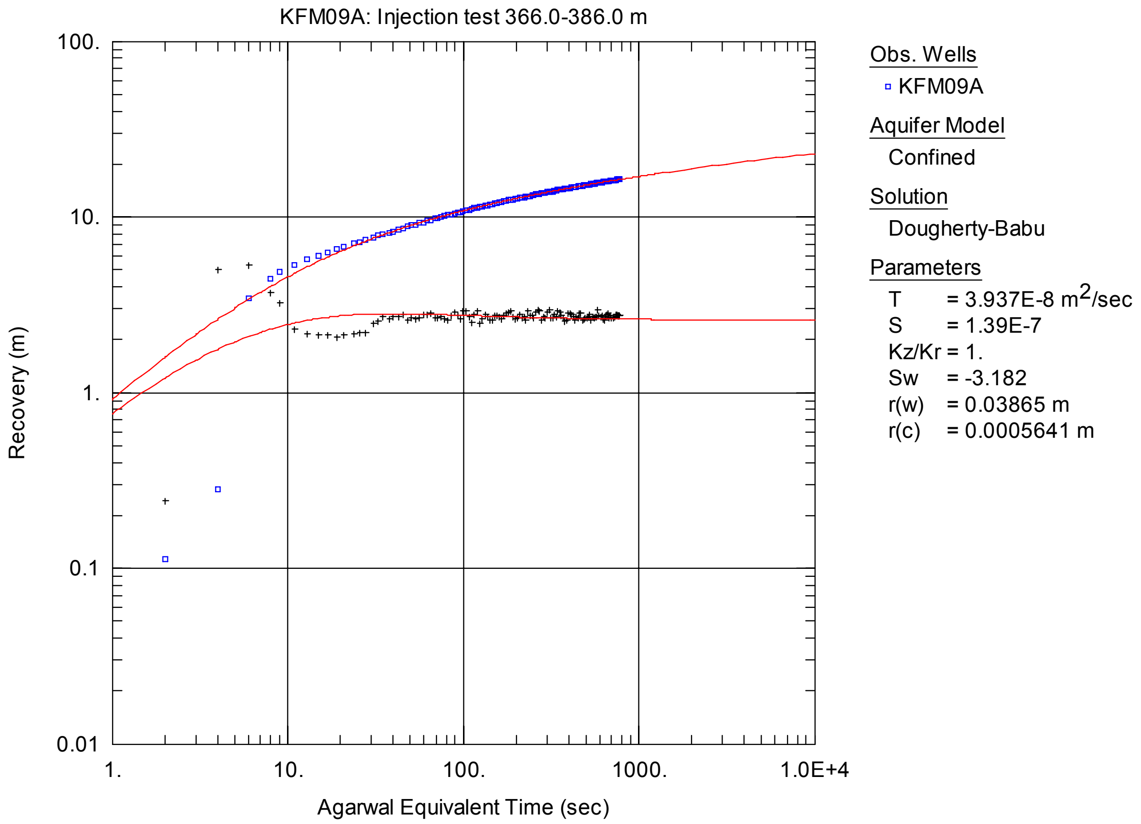


Figure A3-108. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 366.0-386.0 m in KFM09A.*

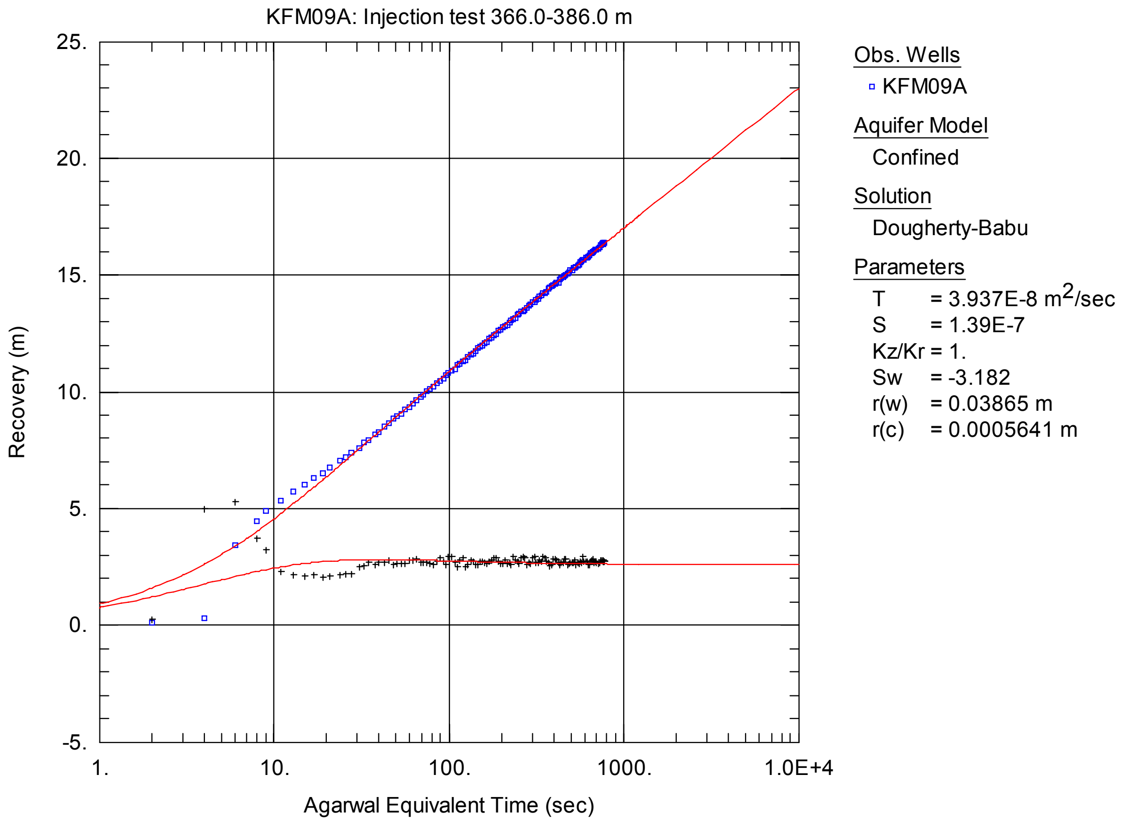


Figure A3-109. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 366.0-386.0 m in KFM09A.*

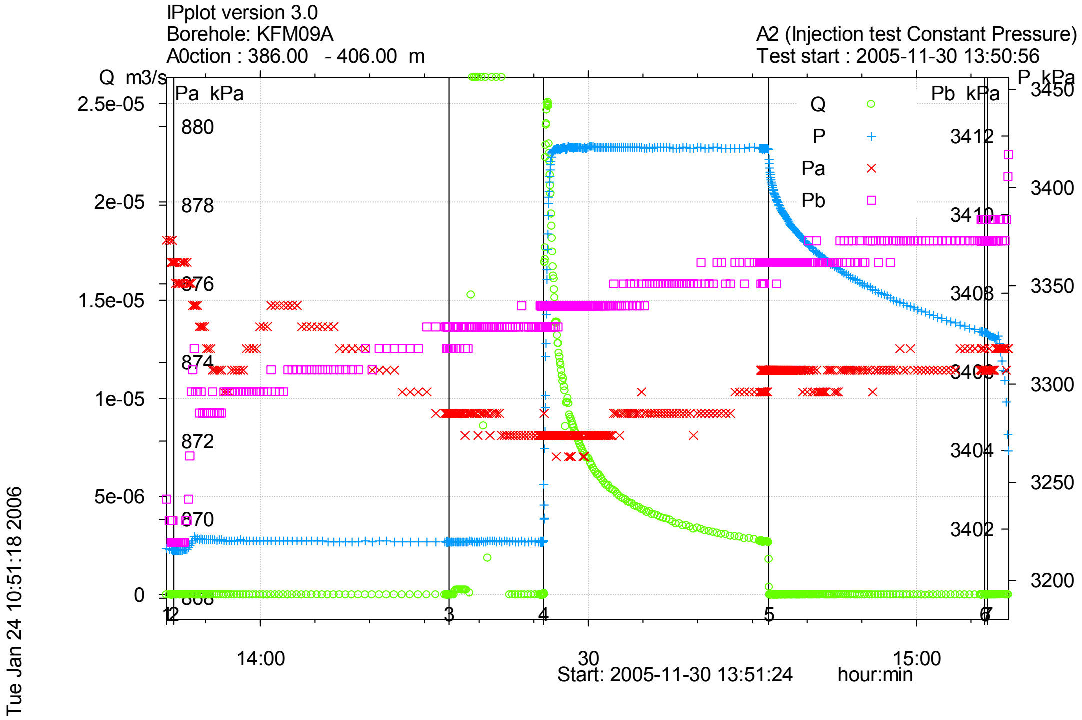


Figure A3-110. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 386.0-406.0 m in borehole KFM09A.

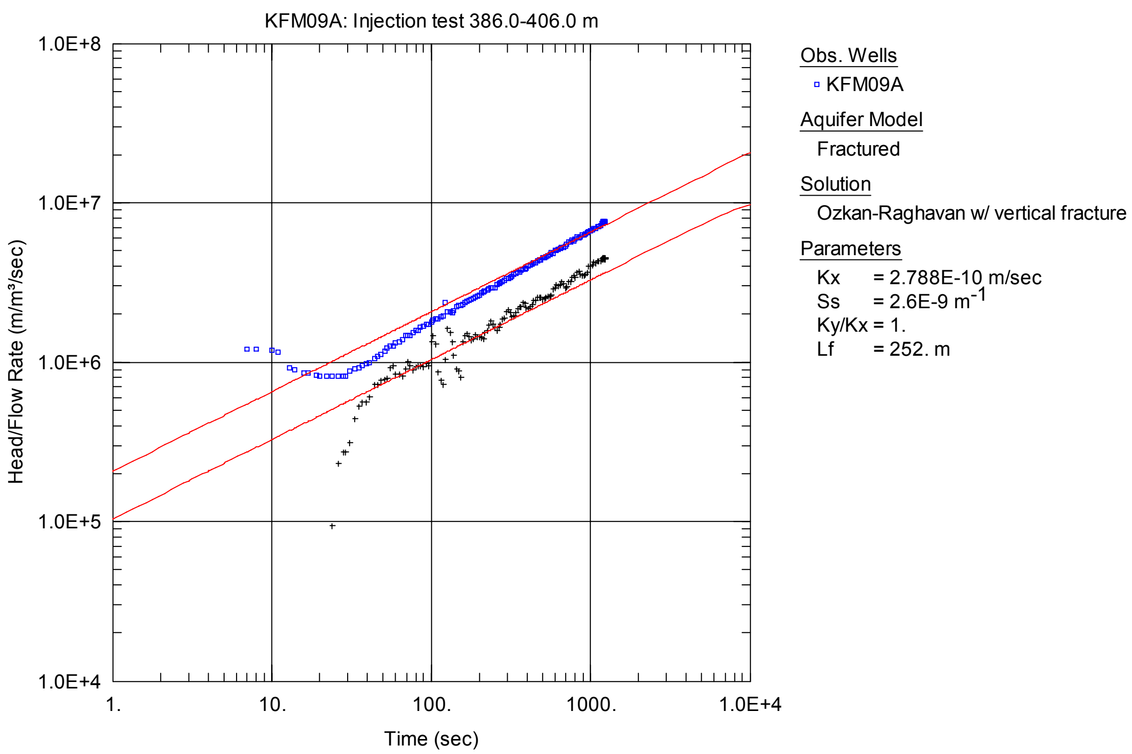


Figure A3-111. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 386.0-406.0 m in KFM09A. No transient evaluation is possible on the injection period.

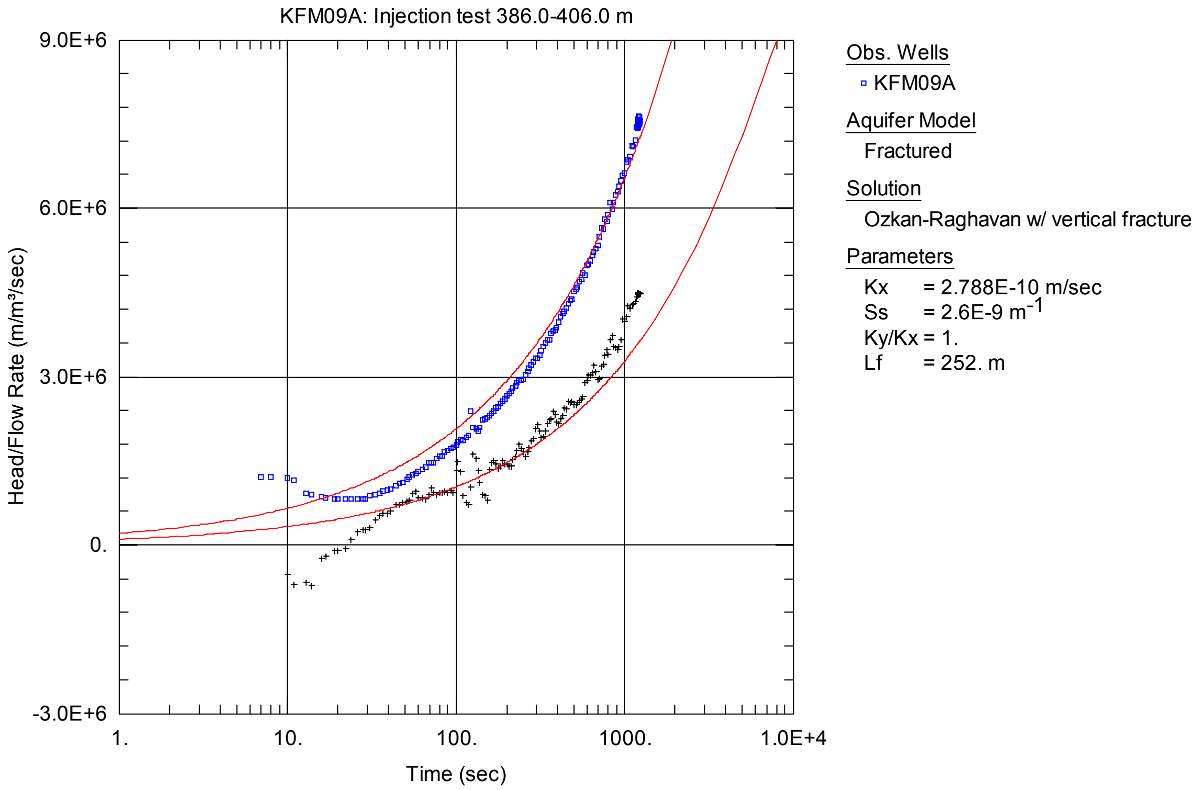


Figure A3-112. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 386.0-406.0 m in KFM09A. No transient evaluation is possible on the injection period.*

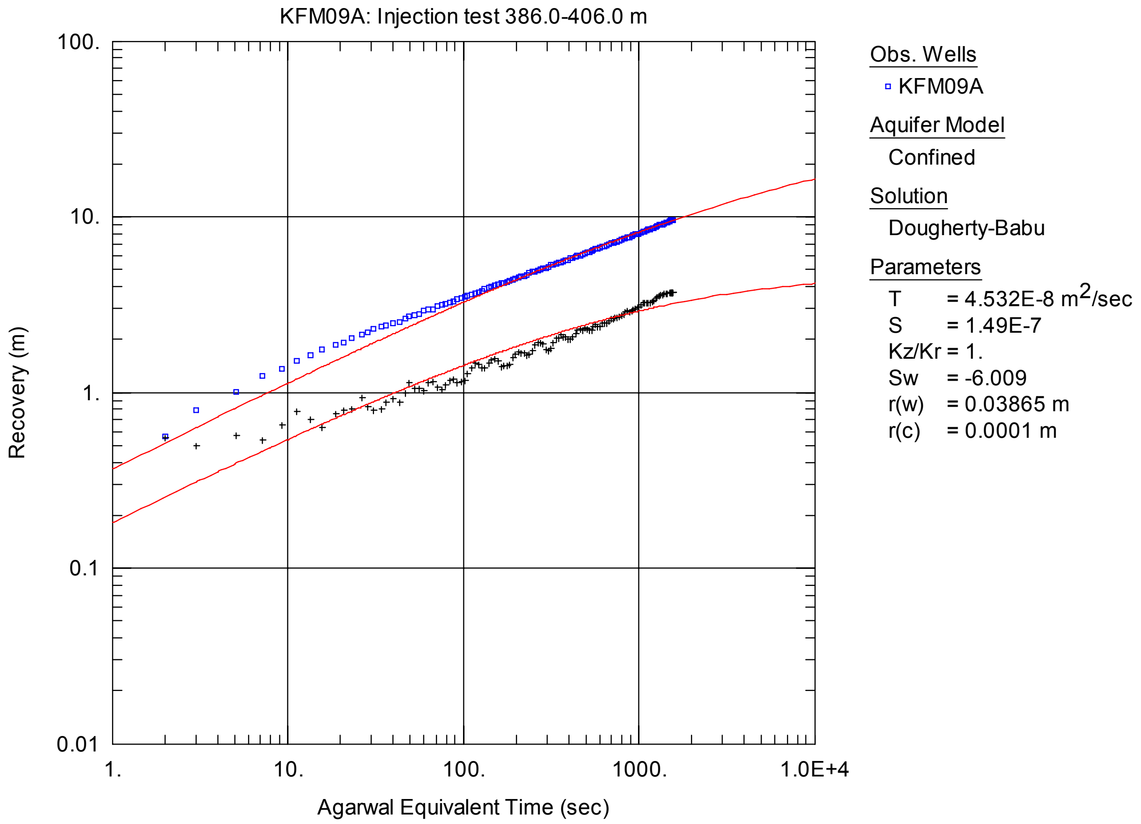


Figure A3-113. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 386.0-406.0 m in KFM09A.*

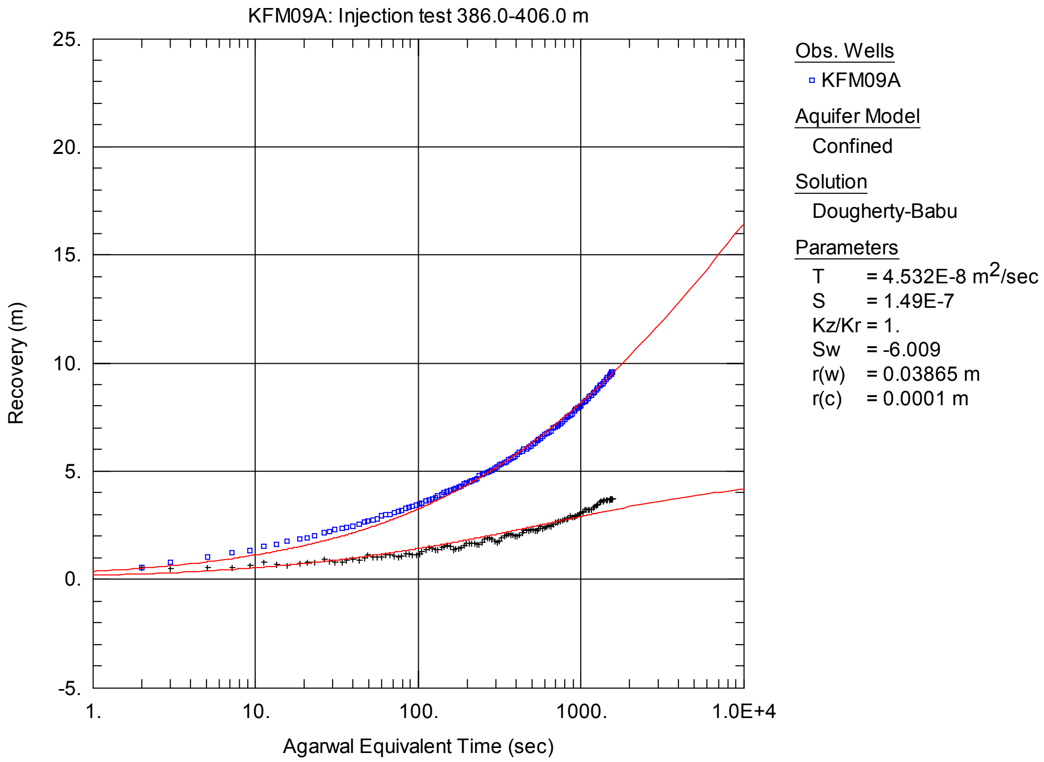


Figure A3-114. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in 386.0-406.0 m in KFM09A.*

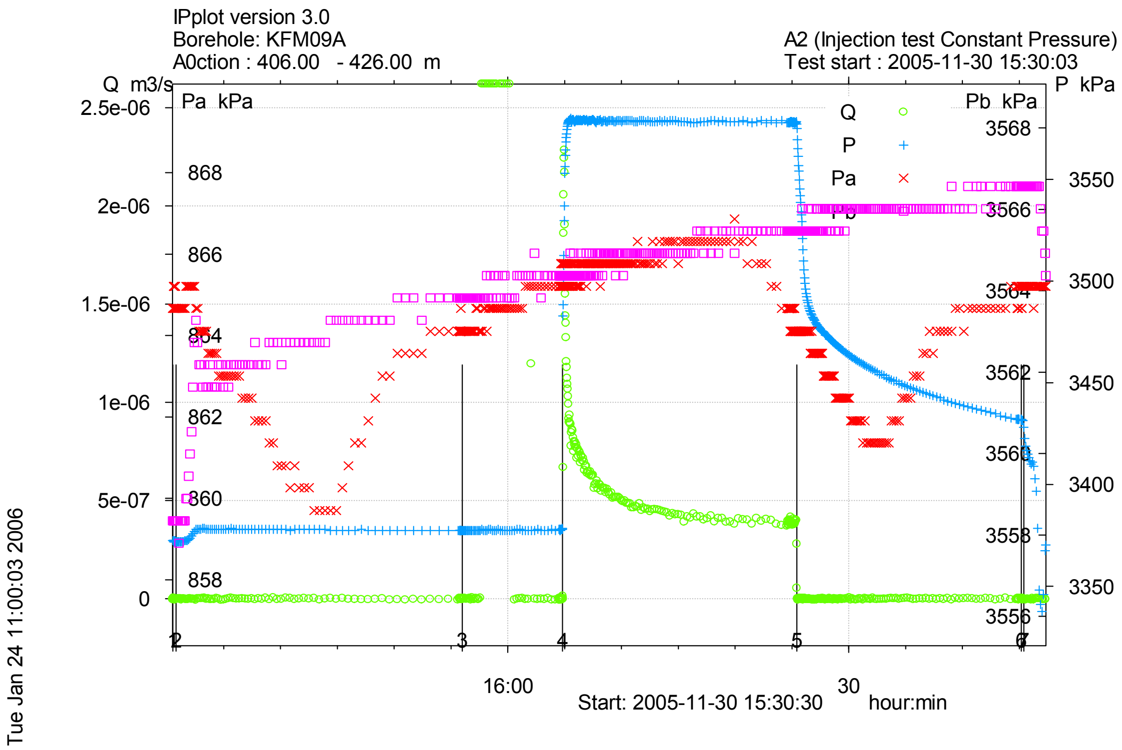


Figure A3-115. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 406.0-426.0 m in borehole KFM09A.*

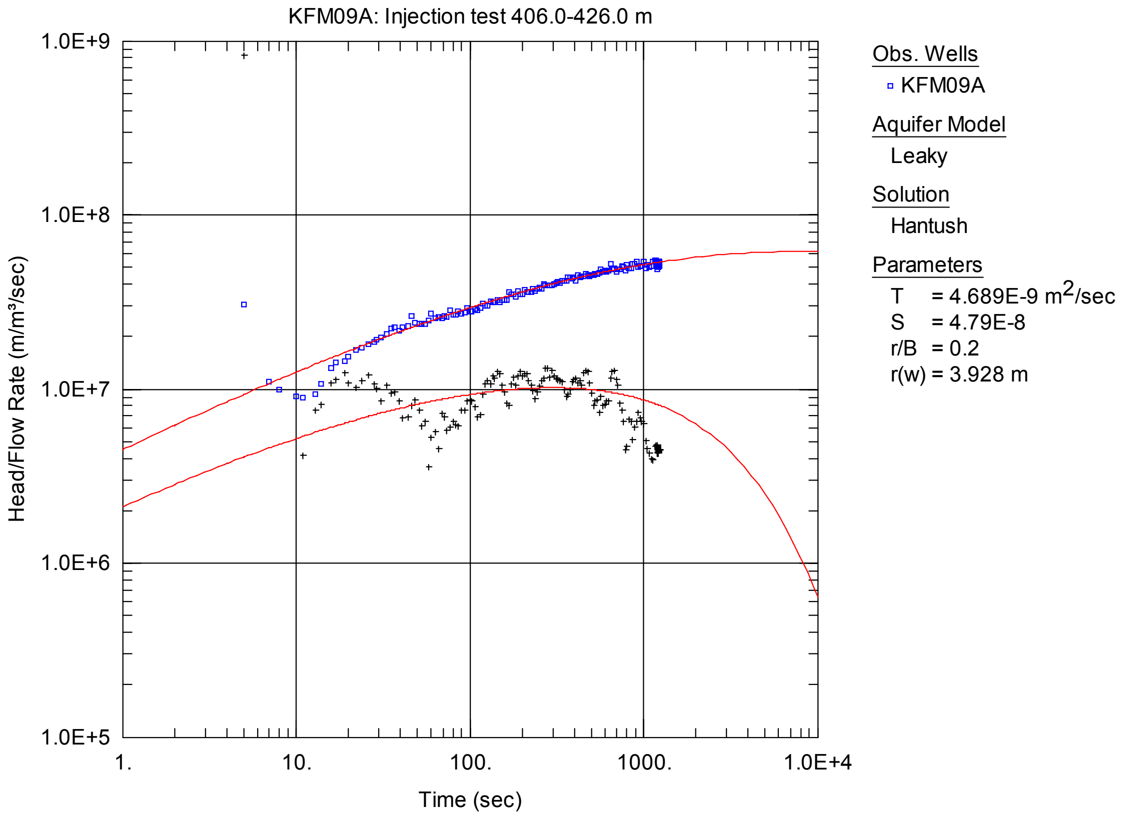


Figure A3-116. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 406.0-426.0 m in KFM09A.*

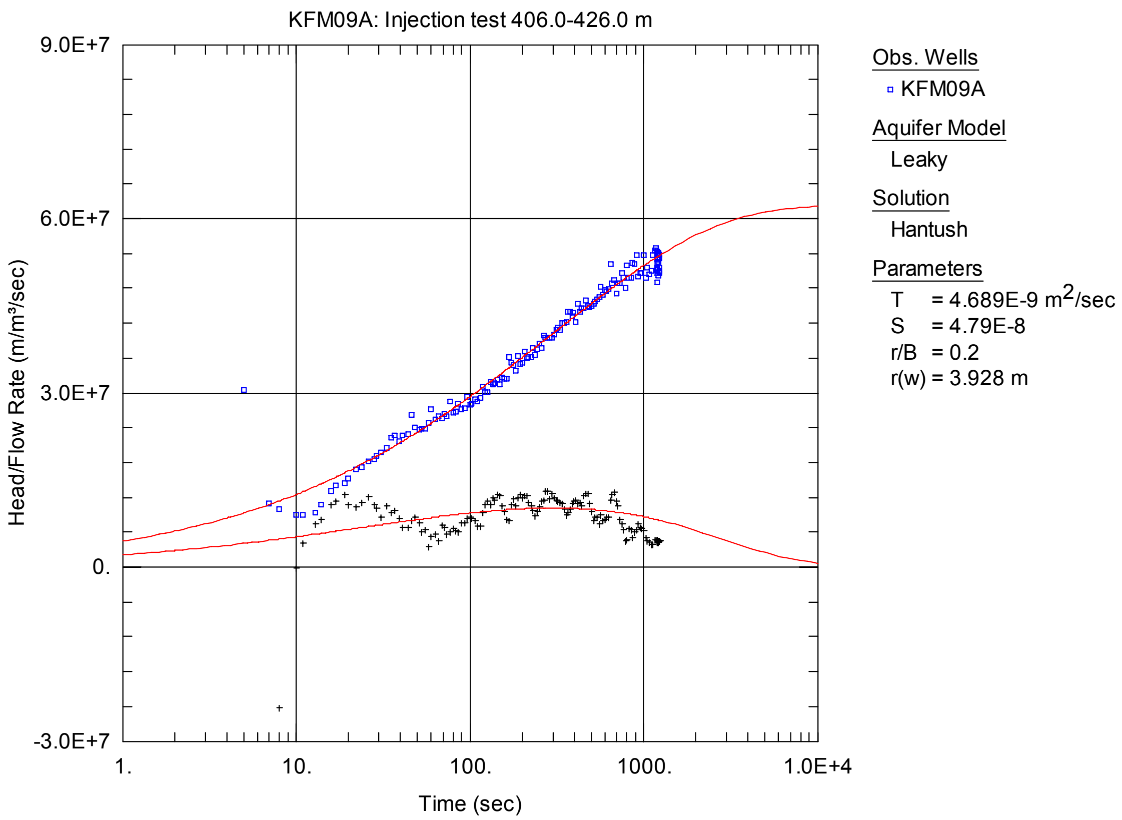


Figure A3-117. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 406.0-426.0 m in KFM09A.*

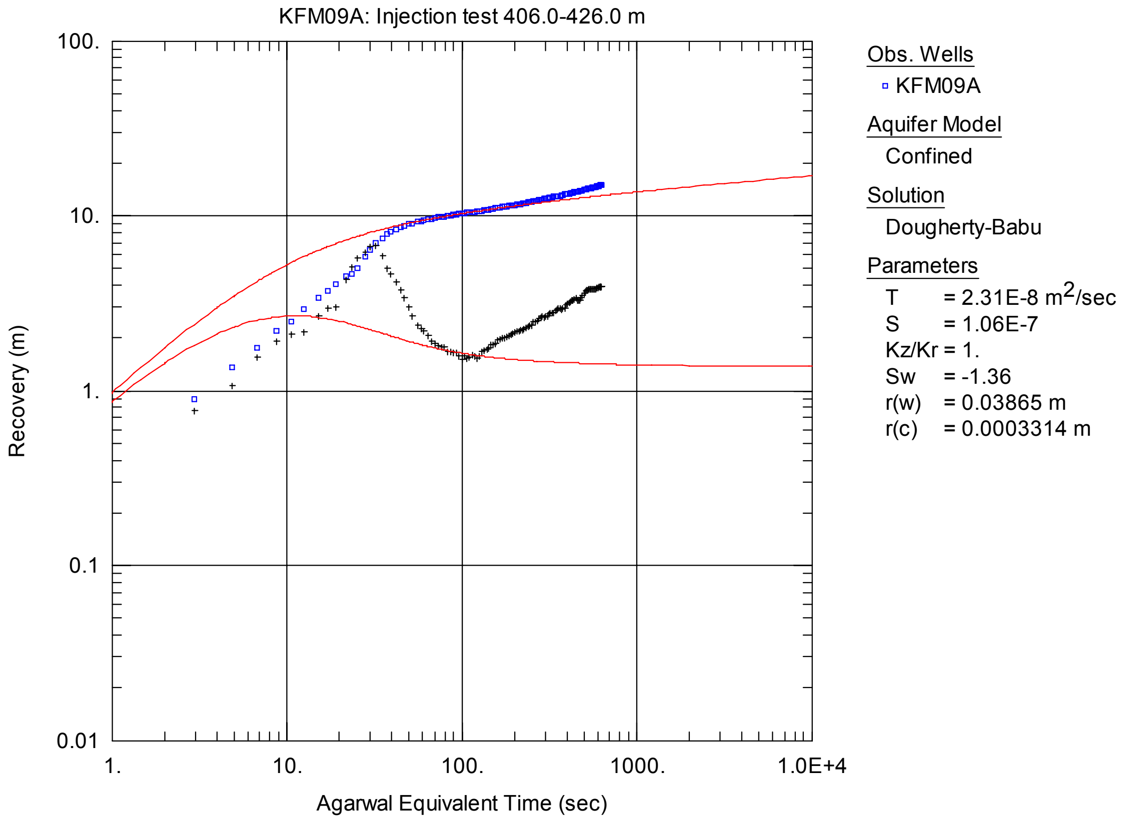


***Figure A3-118.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 406.0-426.0 m in KFM09A.*

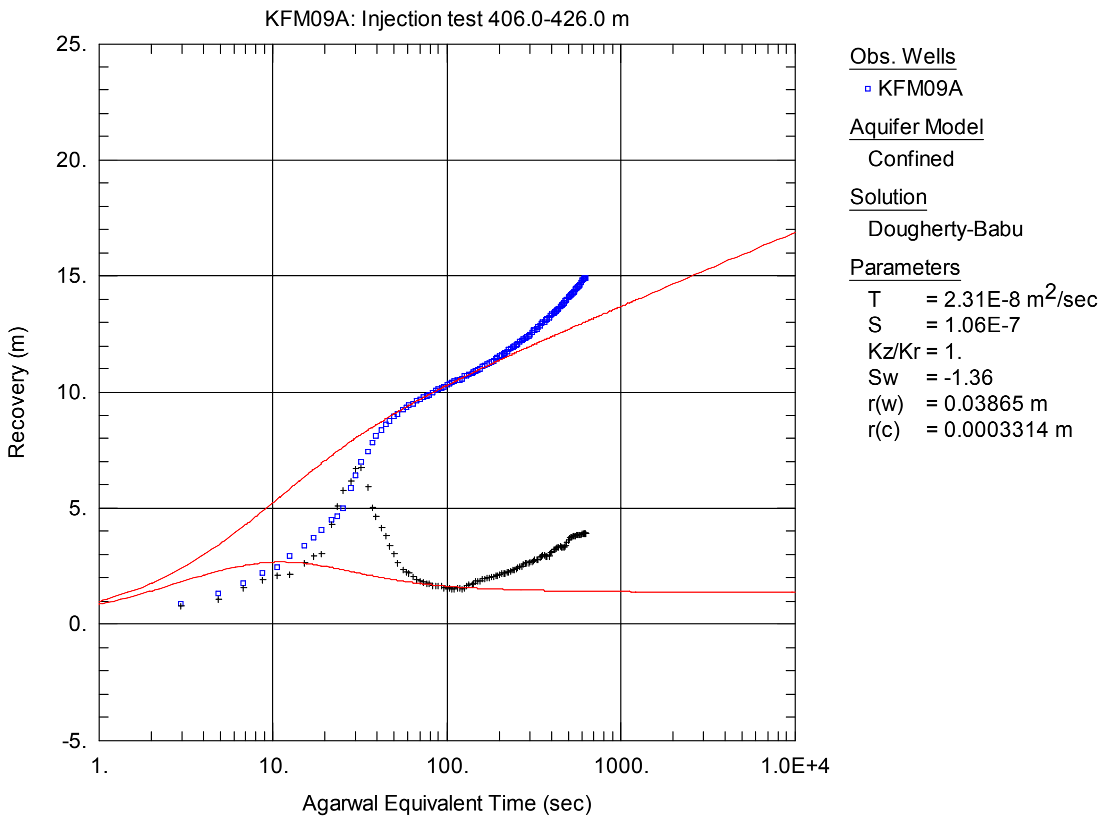


***Figure A3-119.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 406.0-426.0 m in KFM09A.*

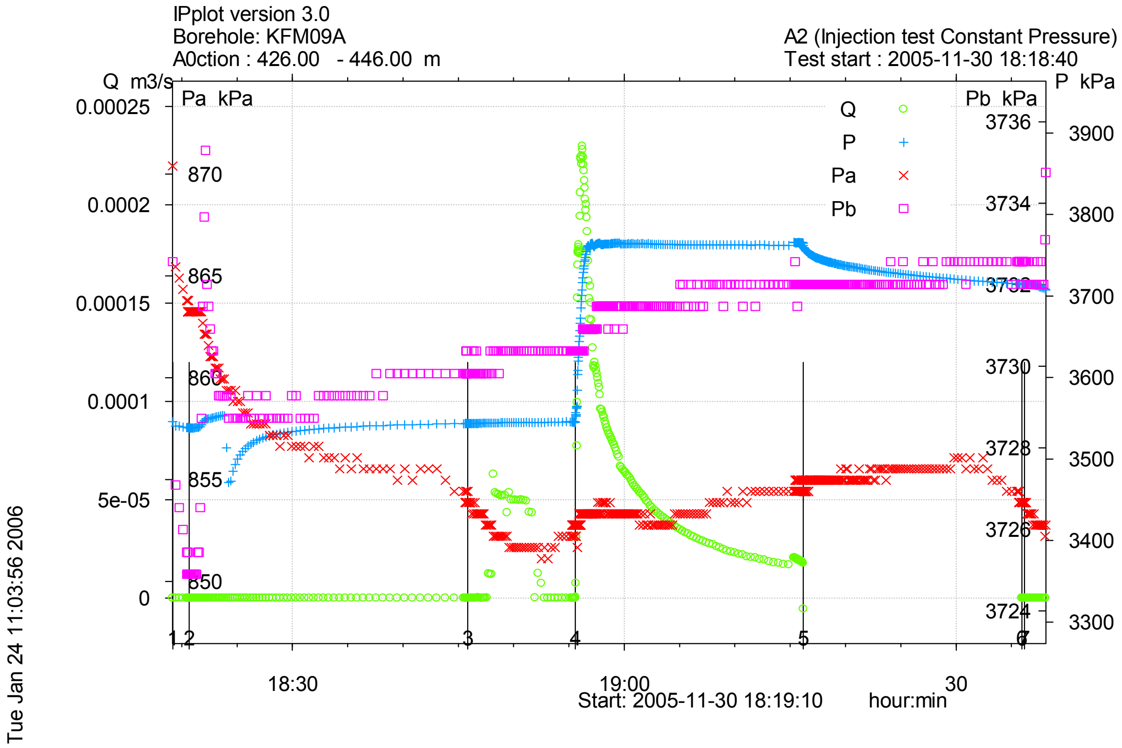


Figure A3-120. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in 426.0-446.0 m in borehole KFM09A.*

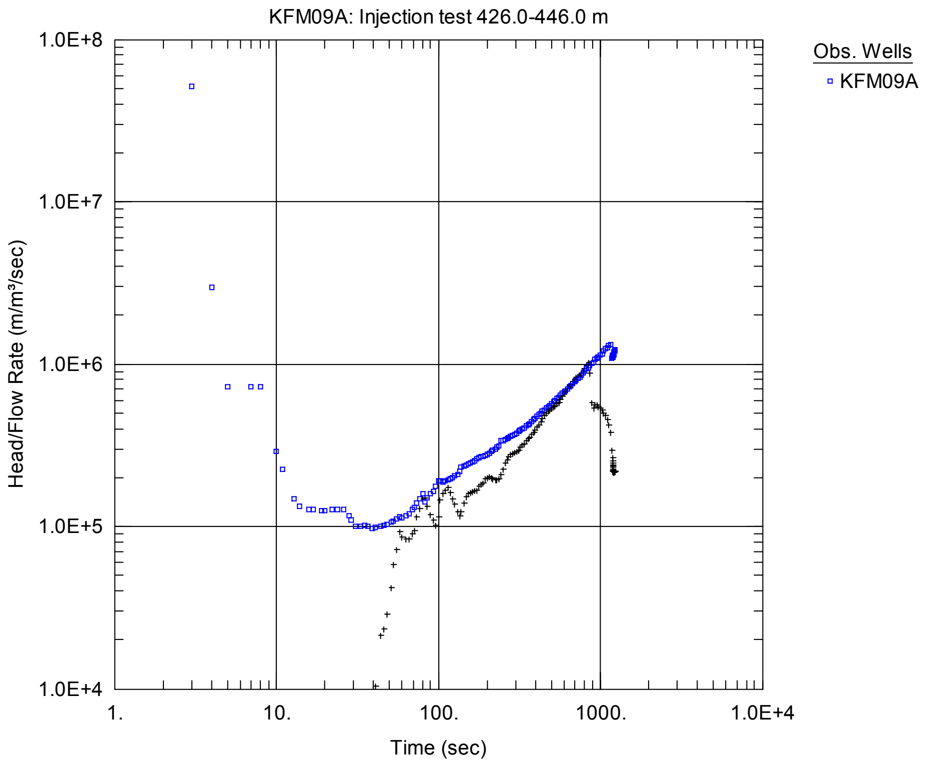


Figure A3-121. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 426.0-446.0 m in KFM09A.*

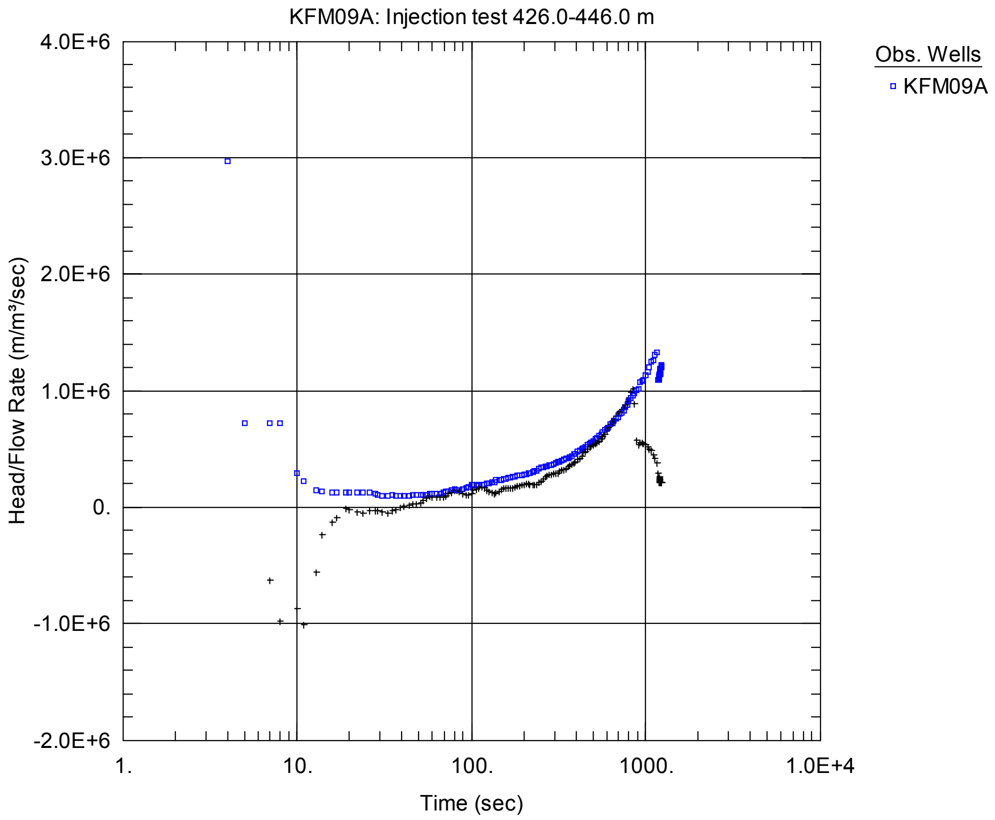


Figure A3-122. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 426.0-446.0 m in KFM09A.*

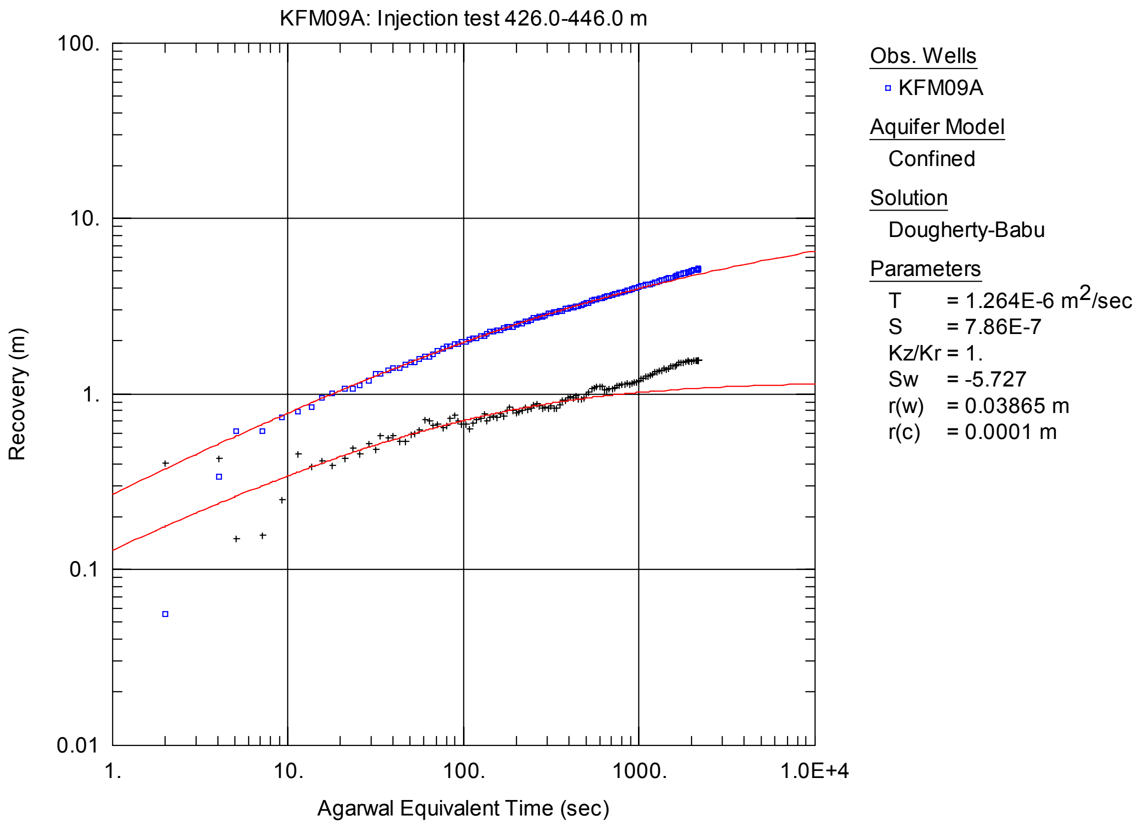


Figure A3-123. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 426.0-446.0 m in KFM09A.*

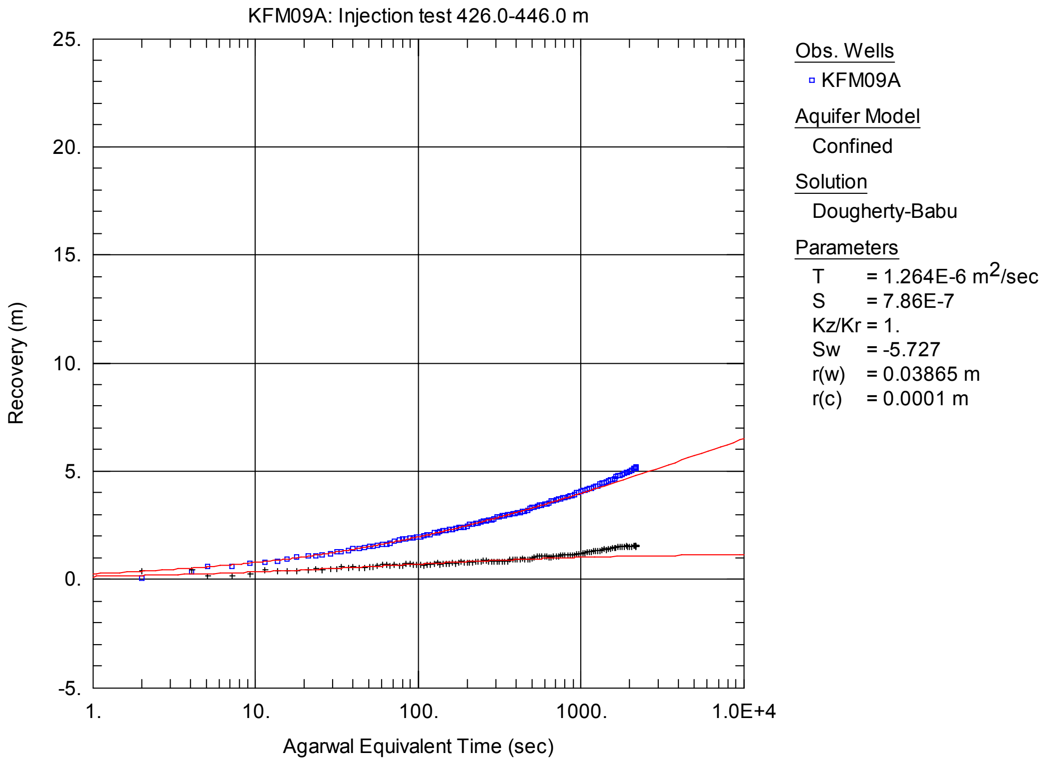


Figure A3-124. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 426.0-446.0 m in KFM09A.*

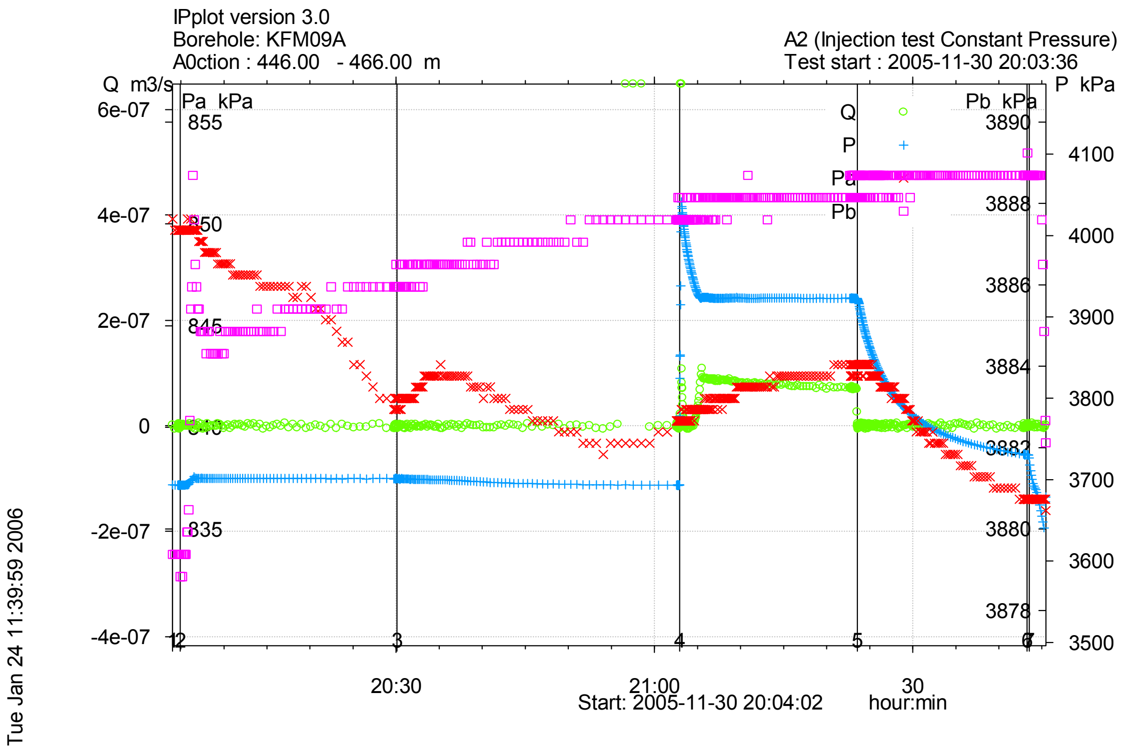


Figure A3-125. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 446.0-466.0 m in borehole KFM09A.*

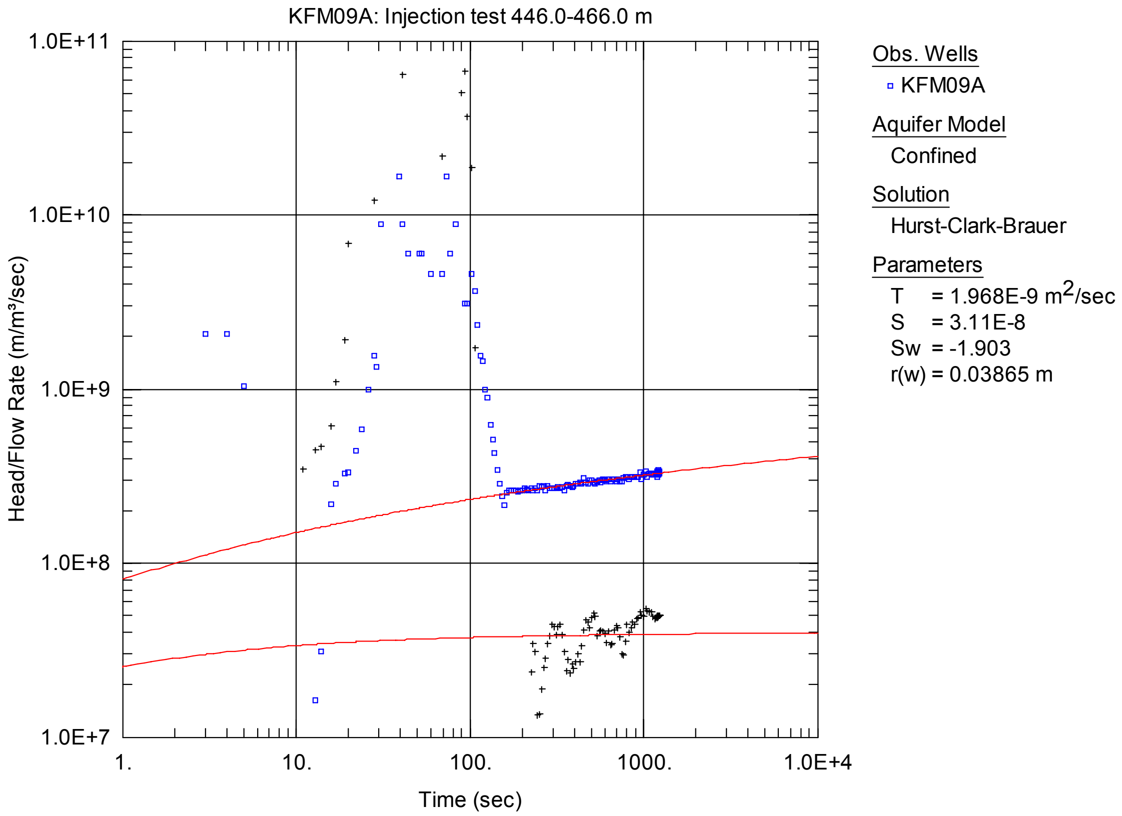


***Figure A3-126.** Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 446.0-466.0 m in KFM09A.*

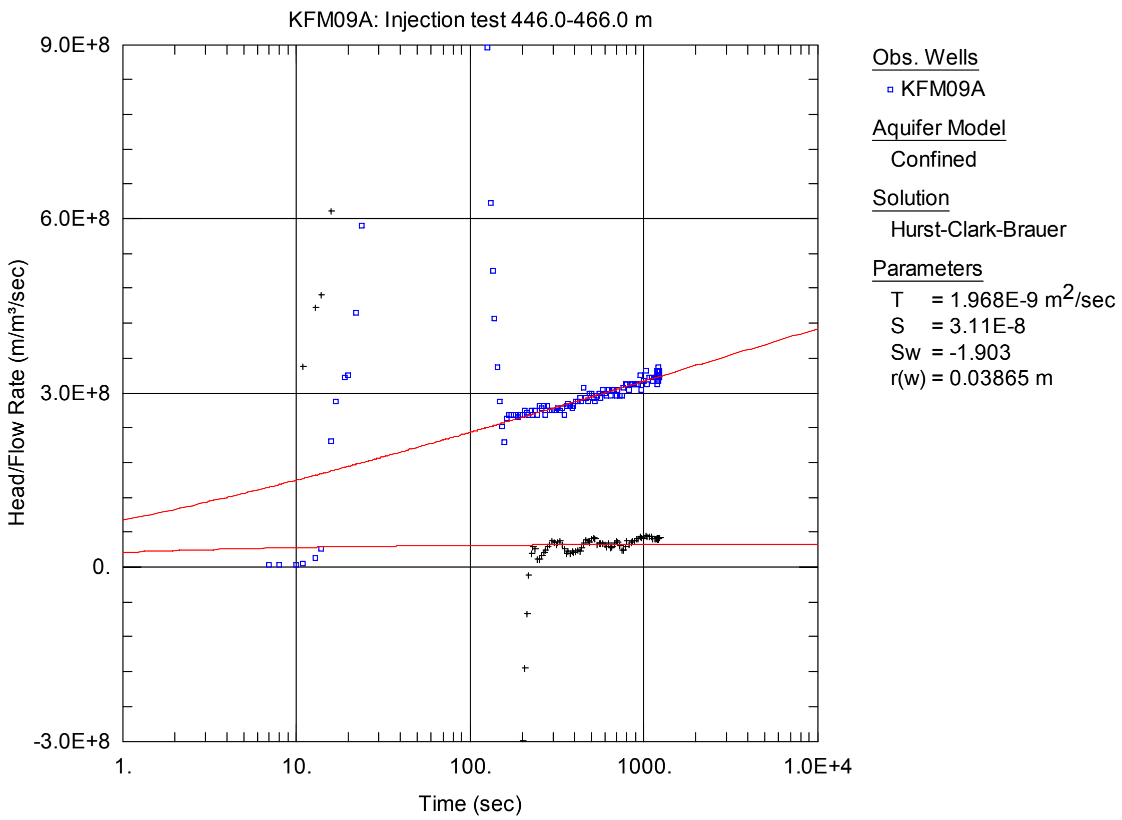


***Figure A3-127.** Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 446.0-466.0 m in KFM09A.*

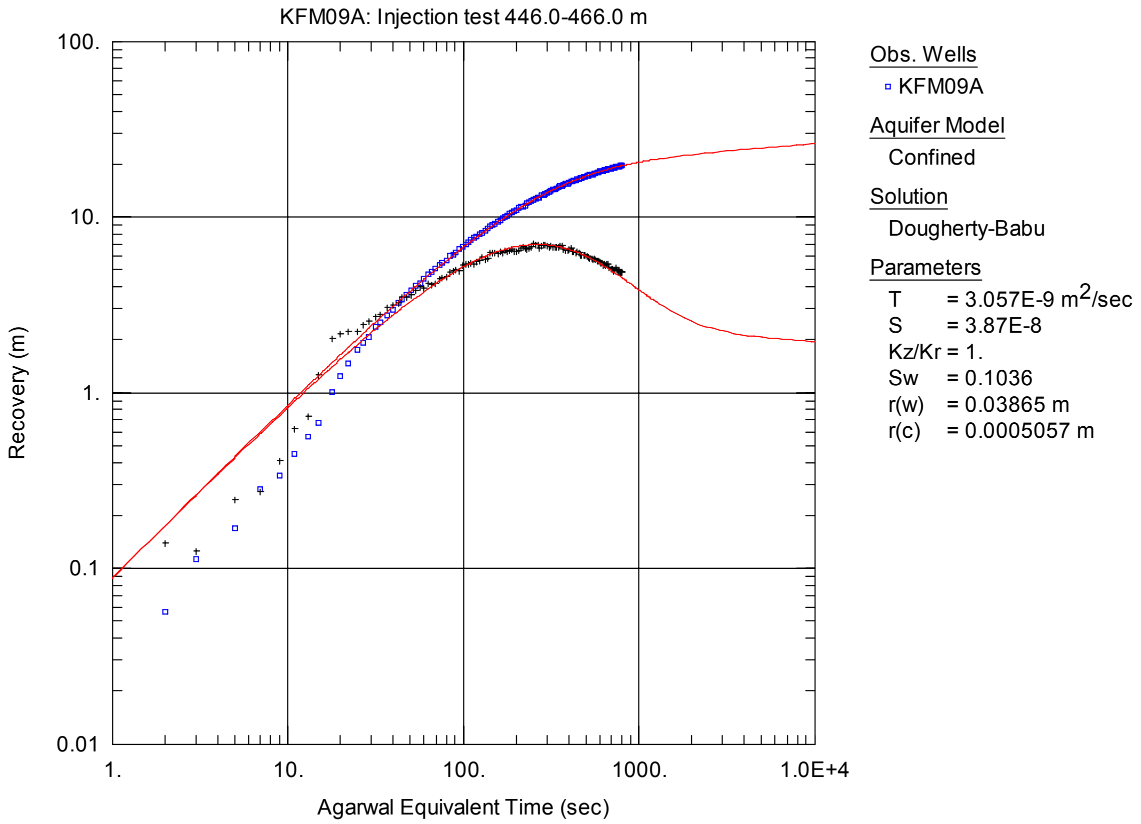


Figure A3-128. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in 446.0-466.0 m in KFM09A.*

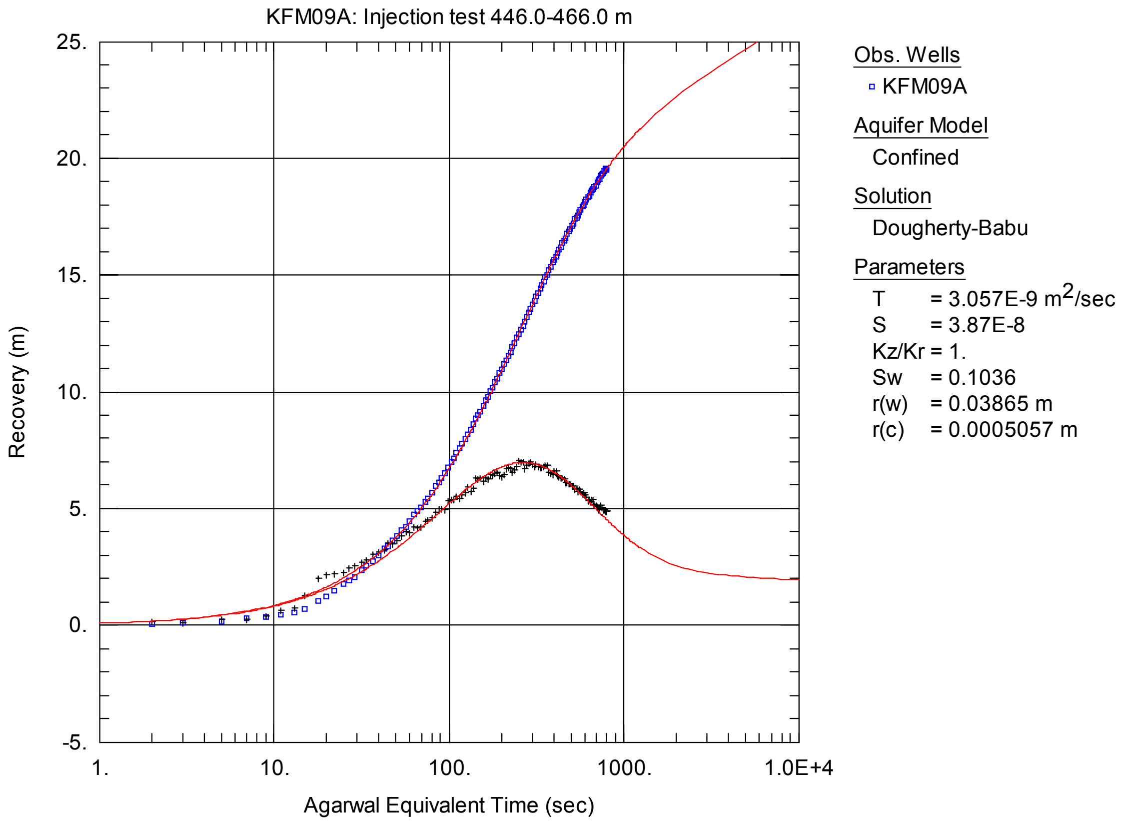


Figure A3-129. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 446.0-466.0 m in KFM09A.*

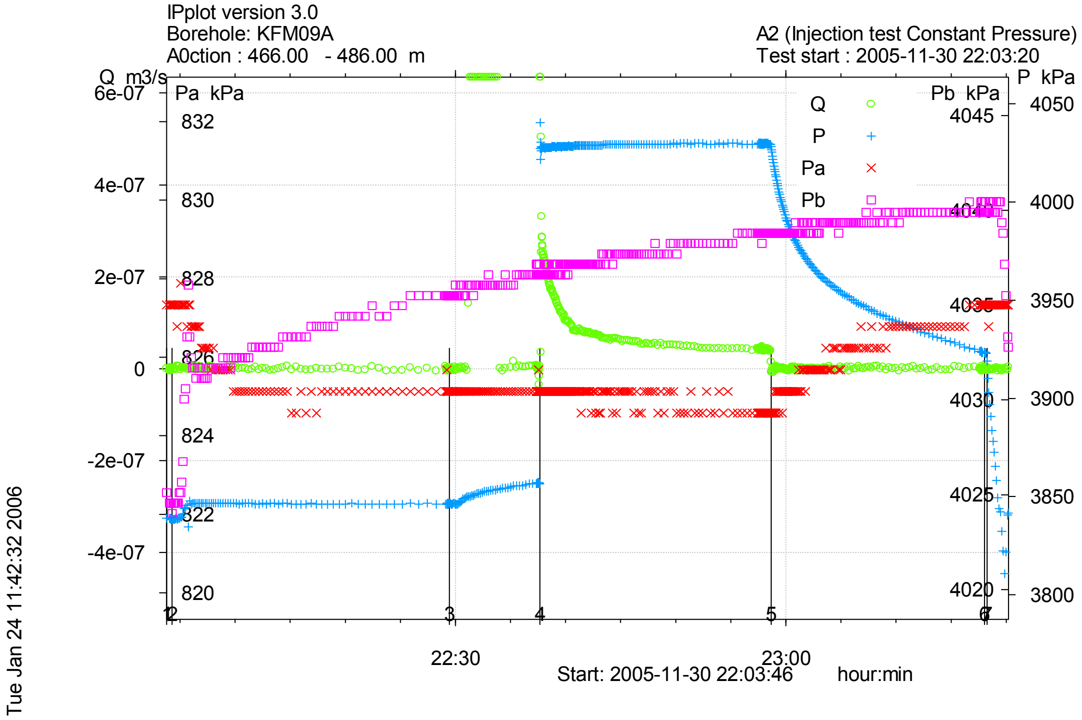


Figure A3-130. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 466.0-486.0 m in borehole KFM09A.*

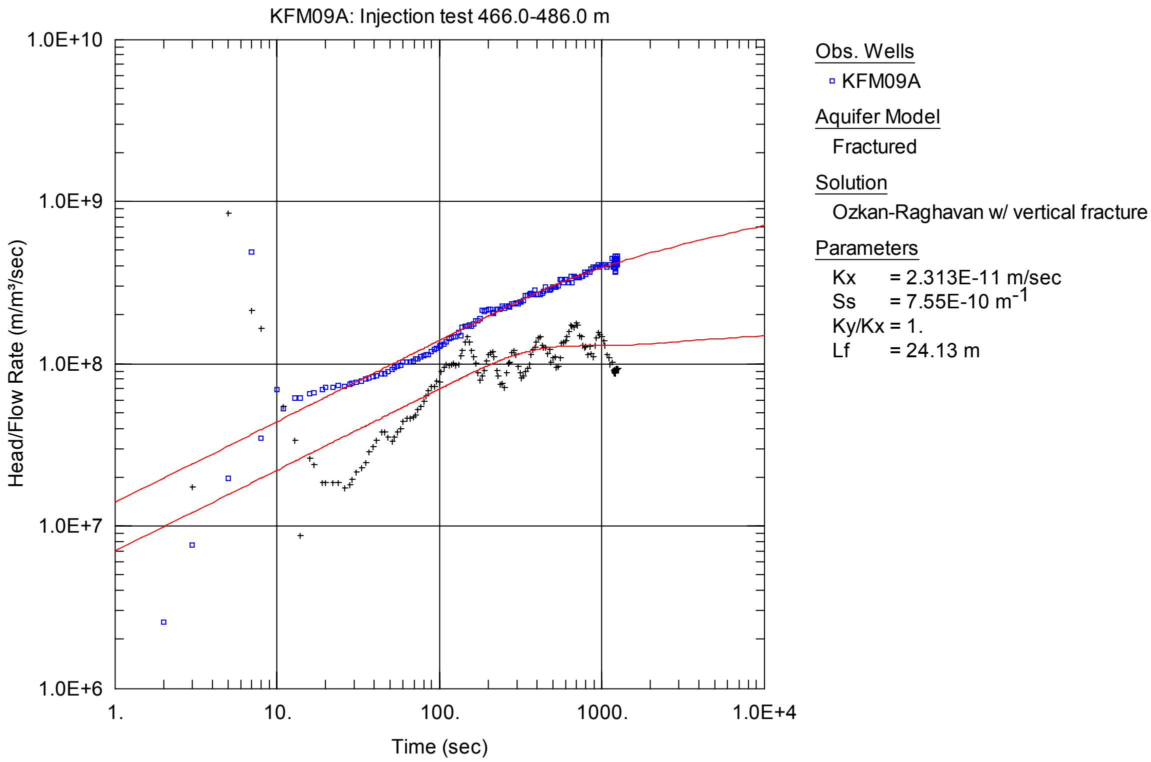


Figure A3-131. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 466.0-486.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

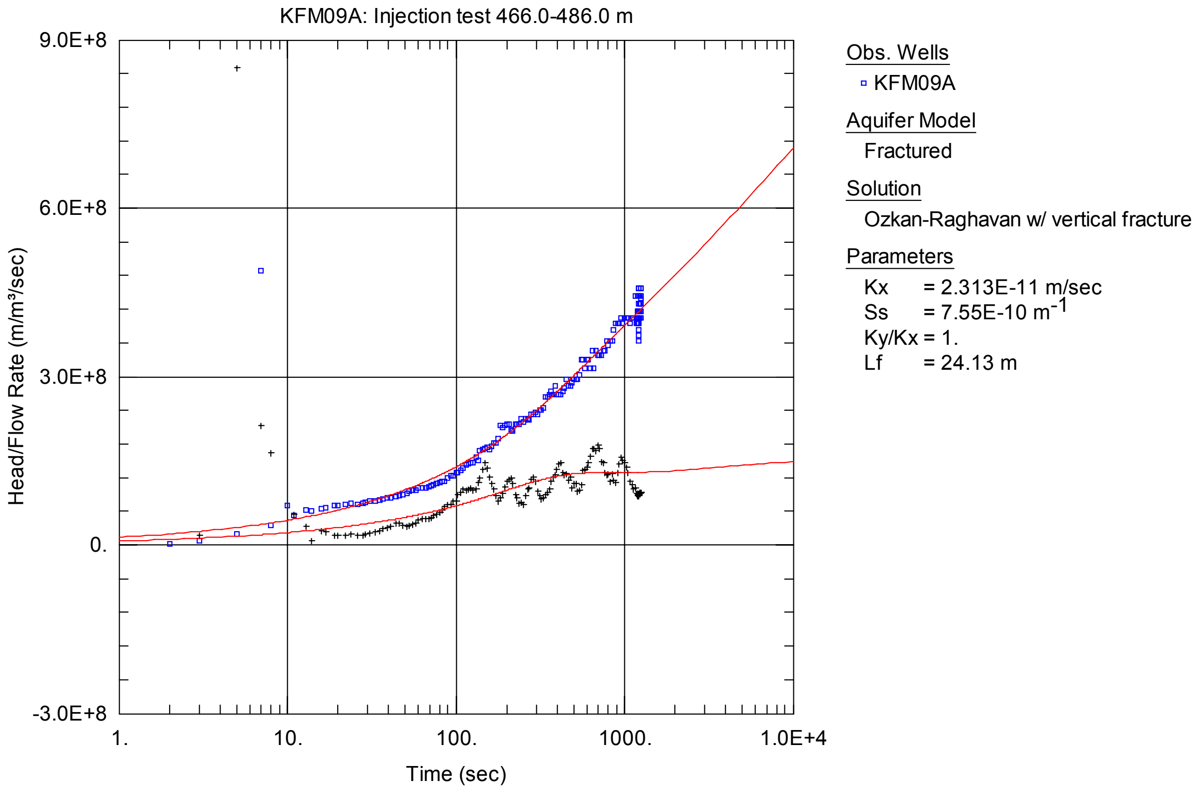


Figure A3-132. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 466.0-486.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

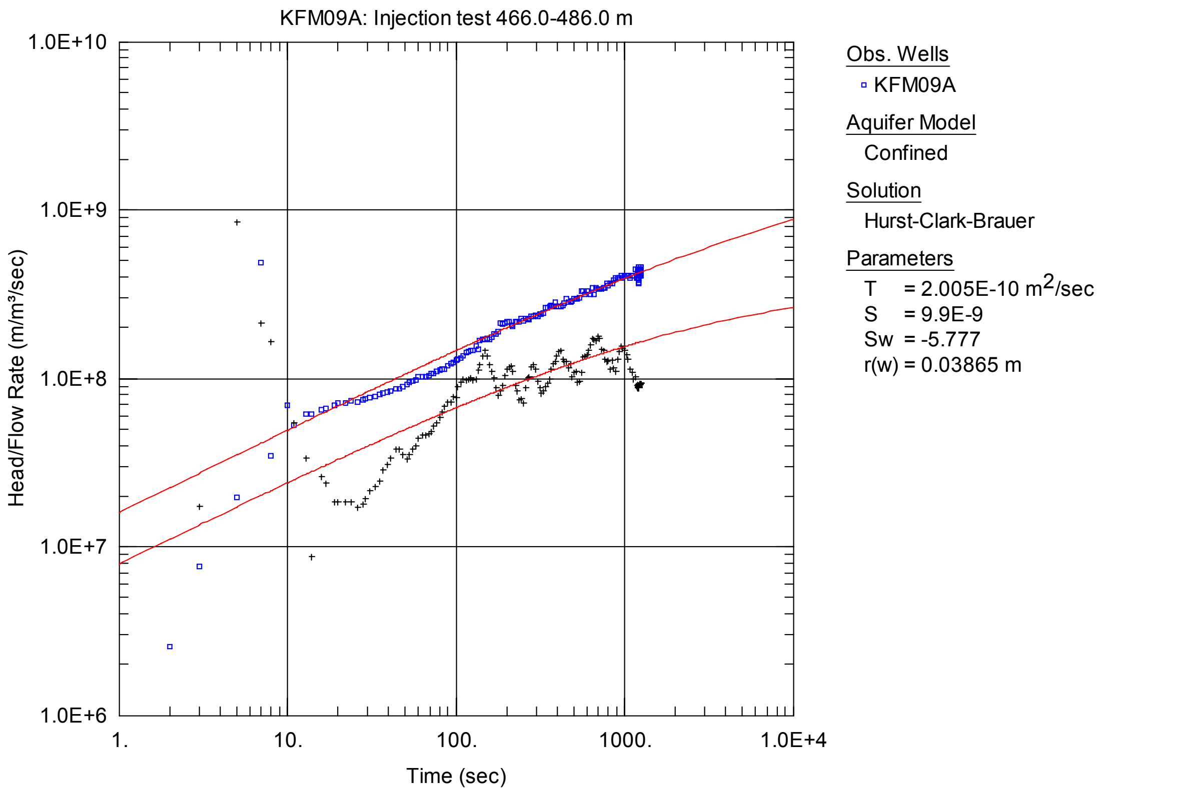


Figure A3-133. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 466.0-486.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for pseudo-radial flow.*

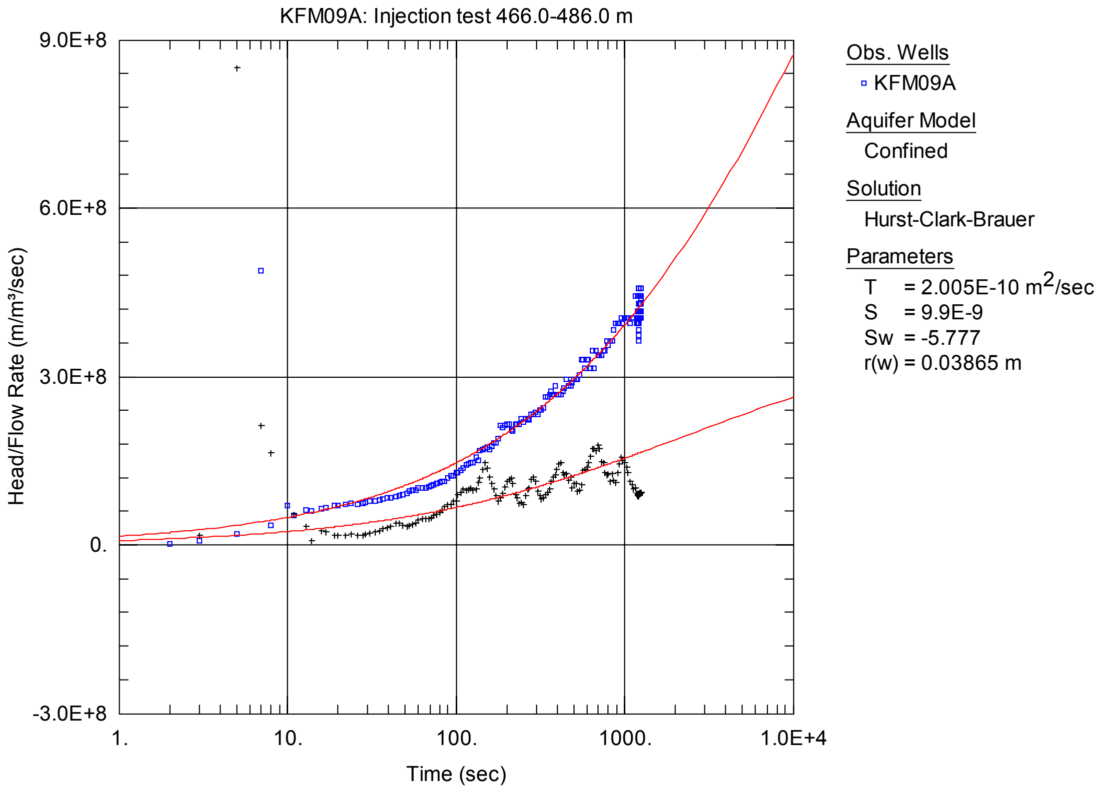


__Figure A3-134.__ Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 466.0-486.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for pseudo-radial flow.

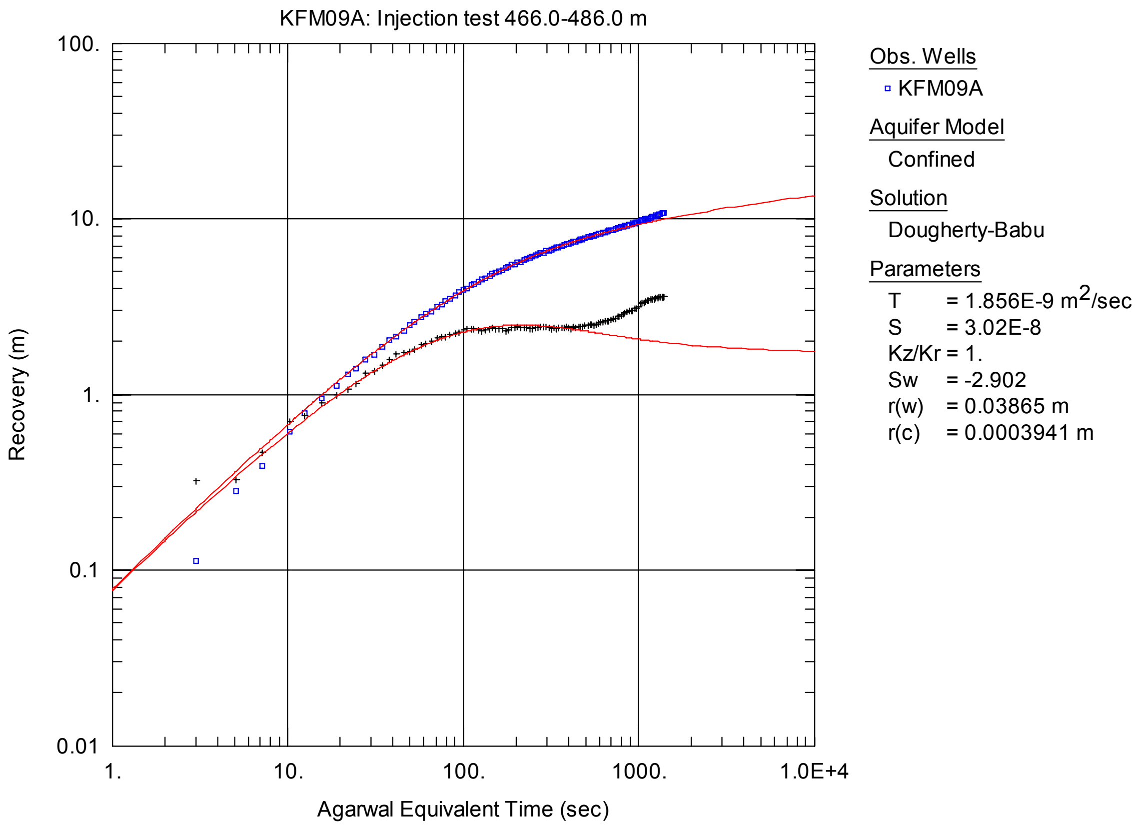


__Figure A3-135.__ Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 466.0-486.0 m in KFM09A.

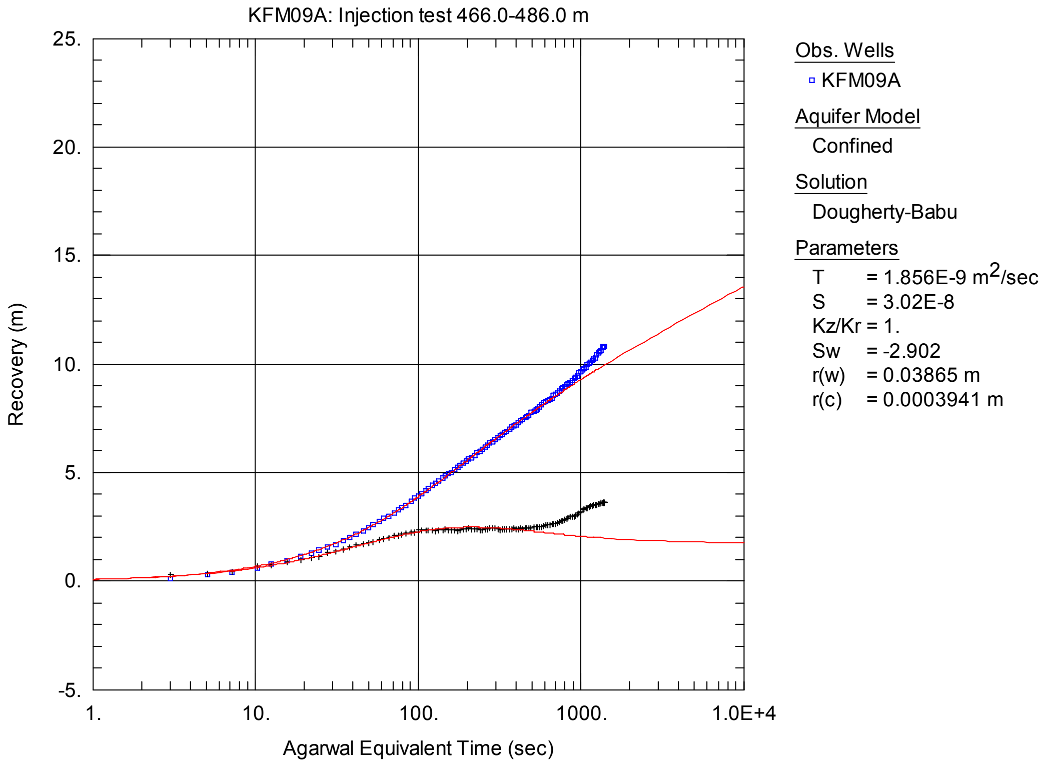


Figure A3-136. Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 466.0-486.0 m in KFM09A.

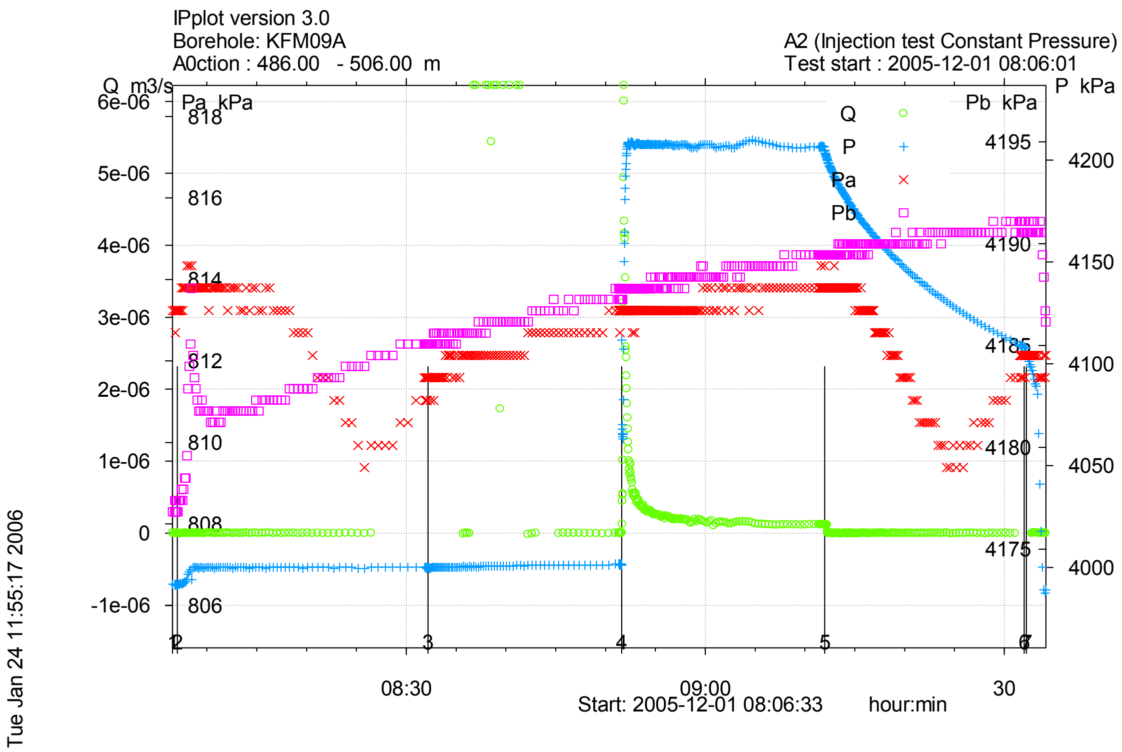


Figure A3-137. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 486.0-506.0 m in borehole KFM09A.

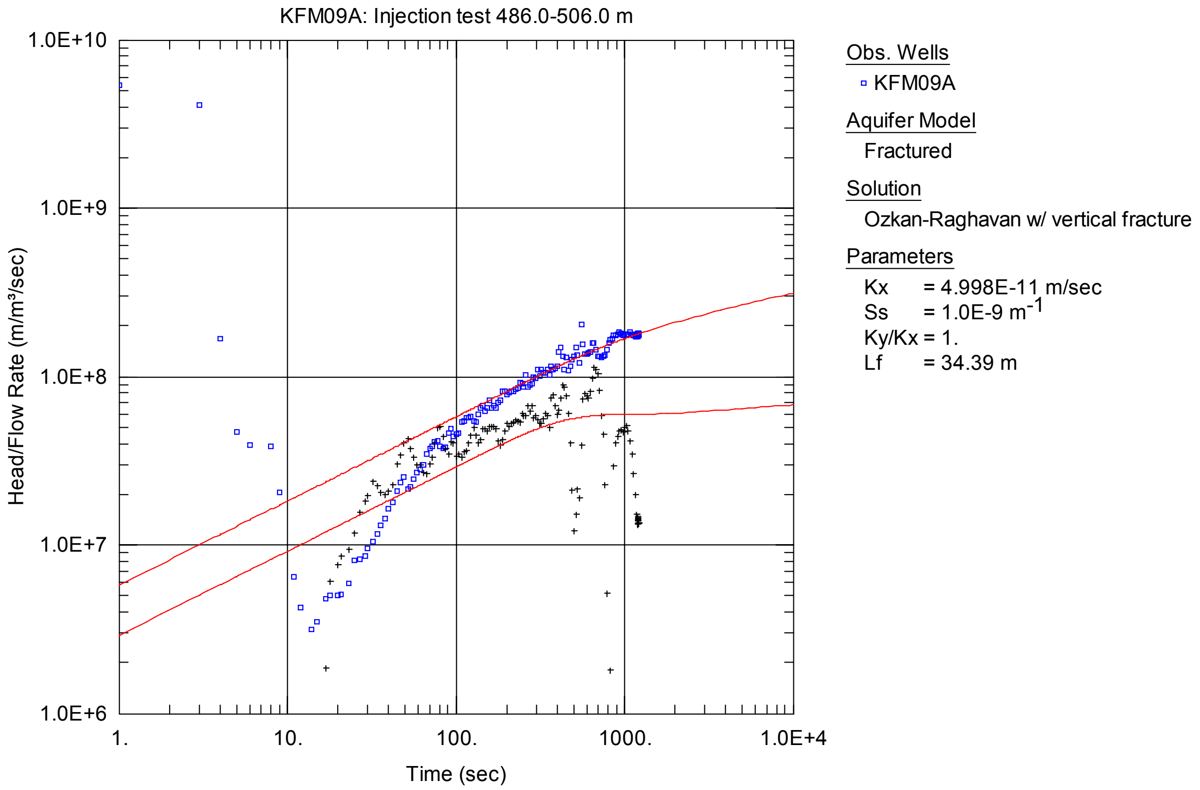


Figure A3-138. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 486.0-506.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

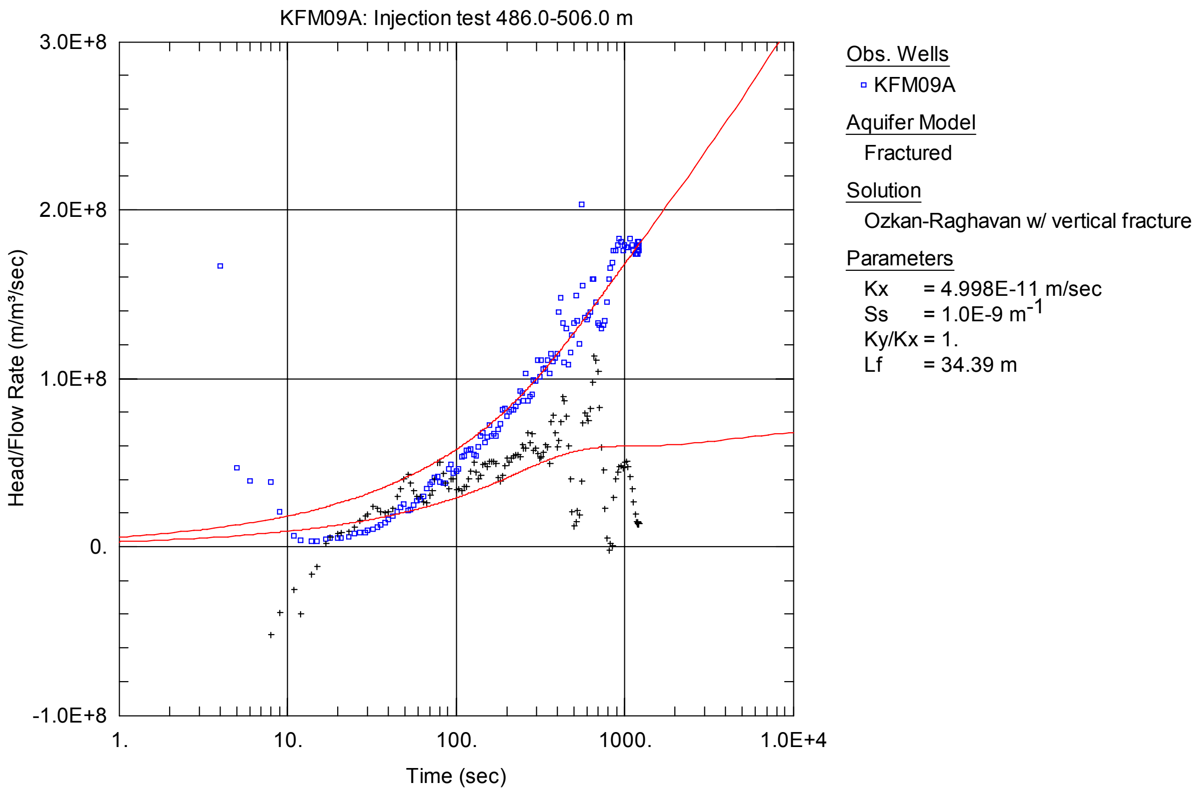


Figure A3-139. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 486.0-506.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

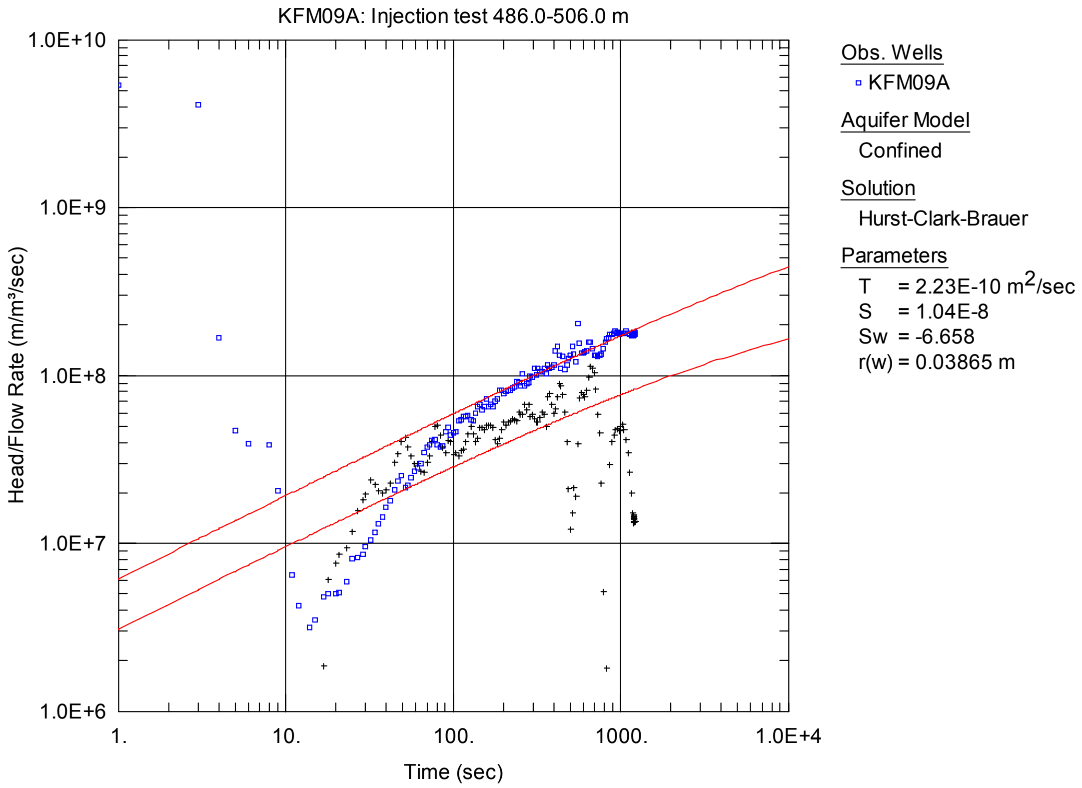


Figure A3-140. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 486.0-506.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for pseudo-radial flow.*

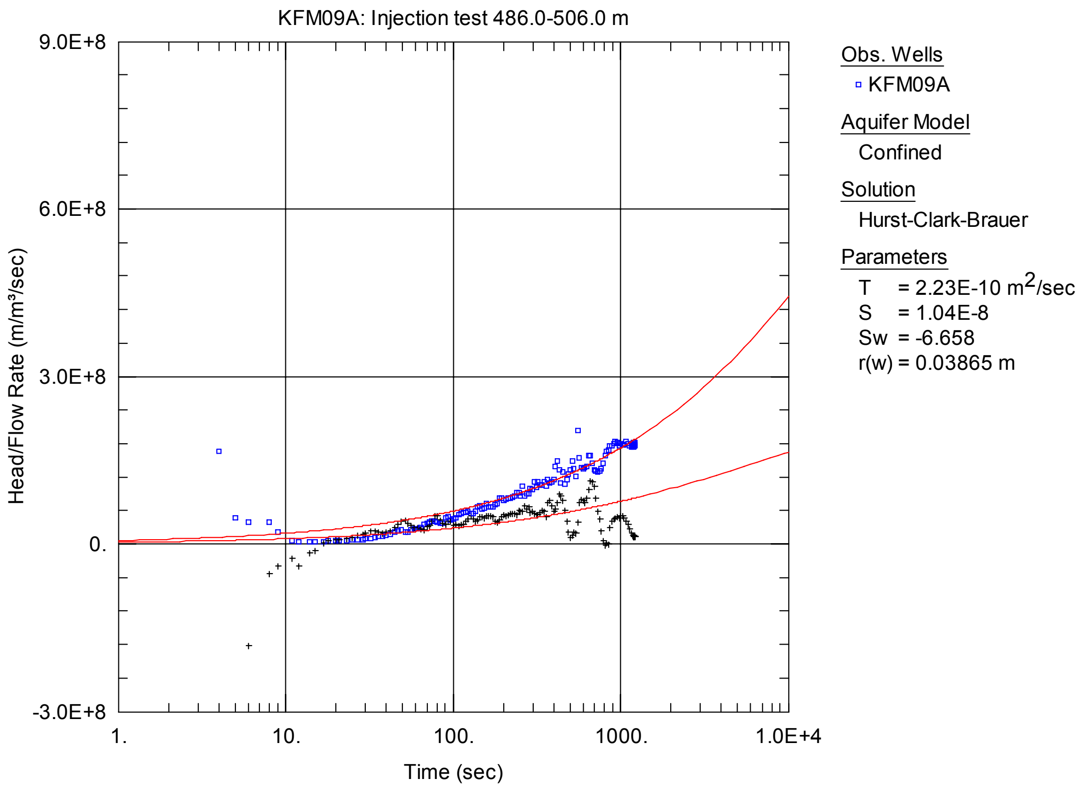


Figure A3-141. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 486.0-506.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for pseudo-radial flow.*

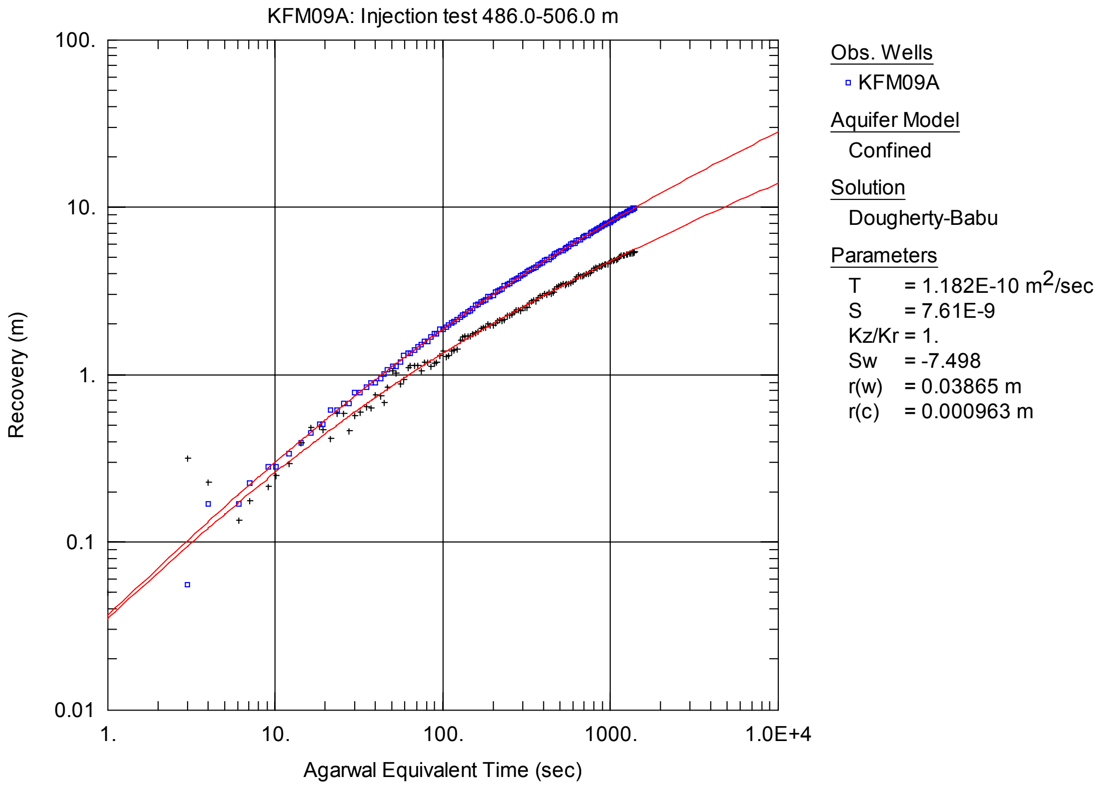


Figure A3-142. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 486.0-506.0 m in KFM09A. The transient evaluation on the recovery period is not regarded as representative.*

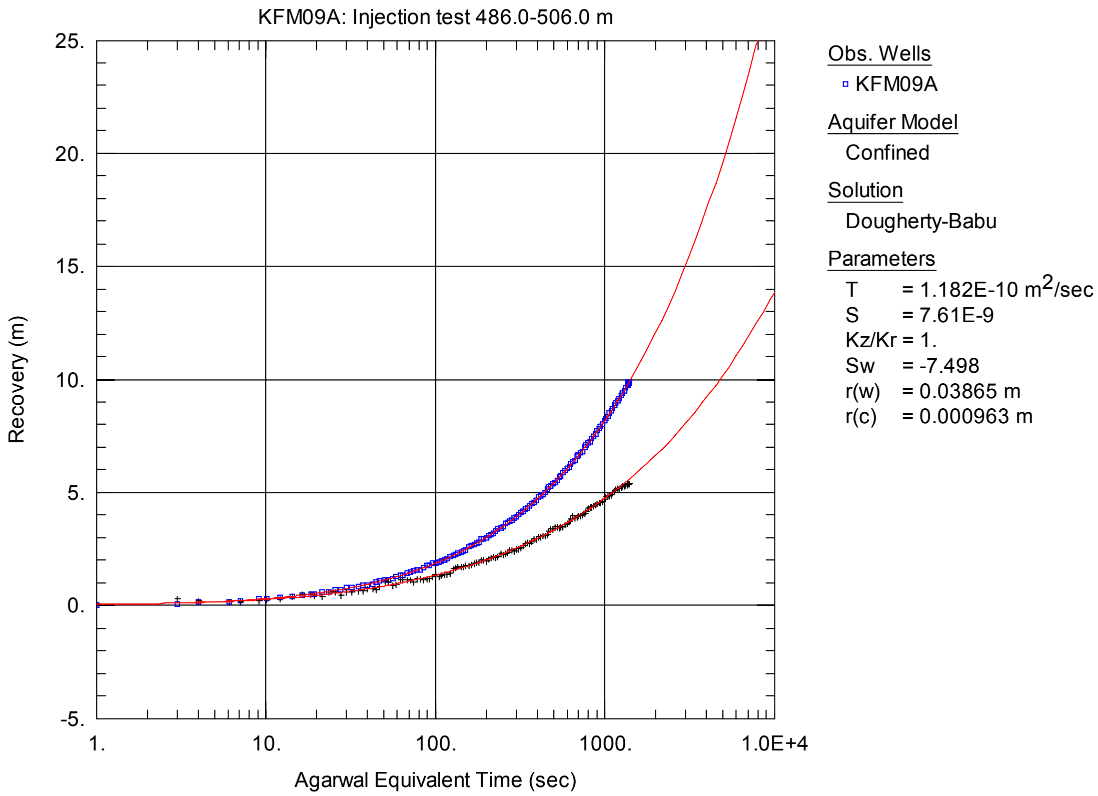


Figure A3-143. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 486.0-506.0 m in KFM09A. The transient evaluation on the recovery period is not regarded as representative.*

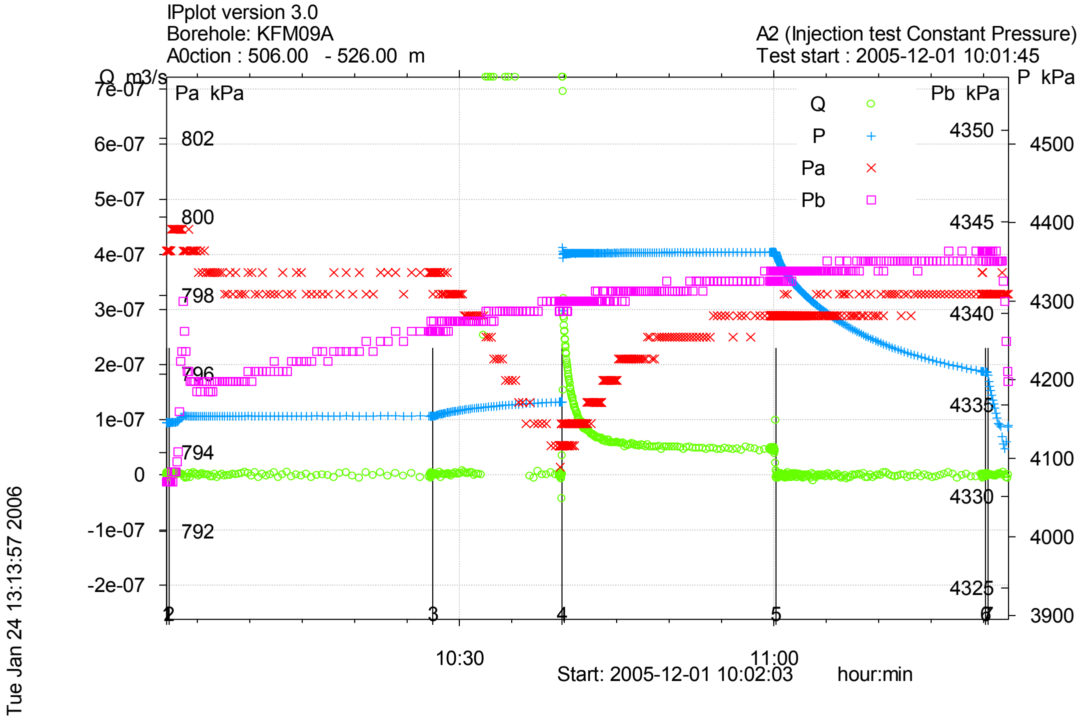


__Figure A3-144.__ Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 506.0-526.0 m in borehole KFM09A.

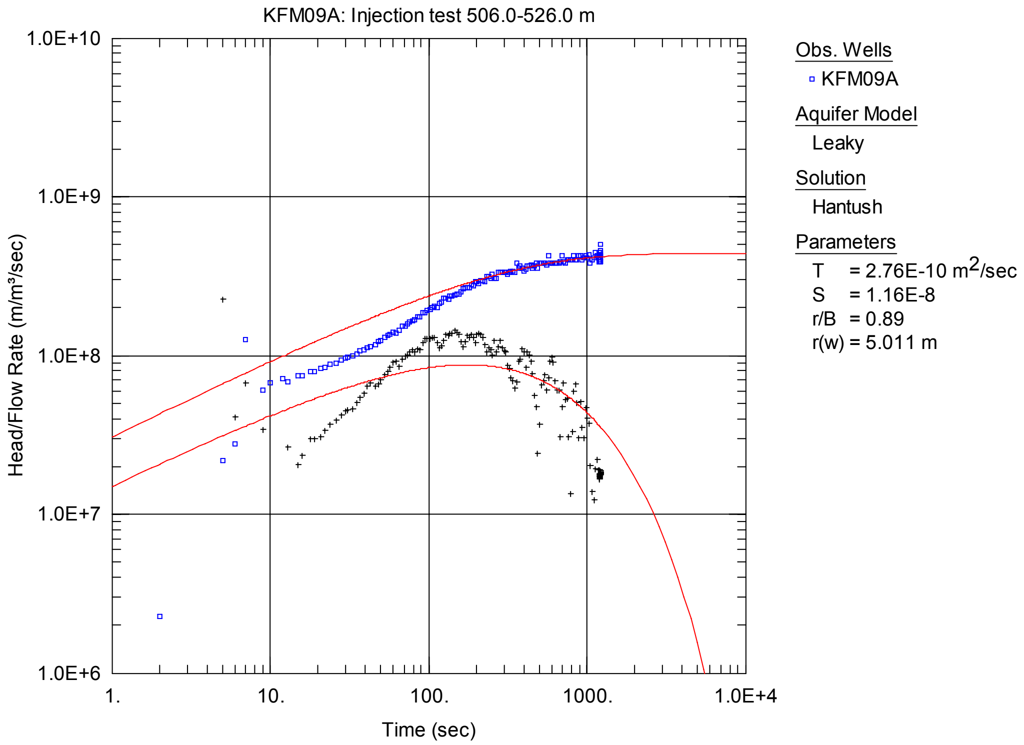


__Figure A3-145.__ Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 506.0-526.0 m in KFM09A. No unambiguous evaluation could be made on the injection period.

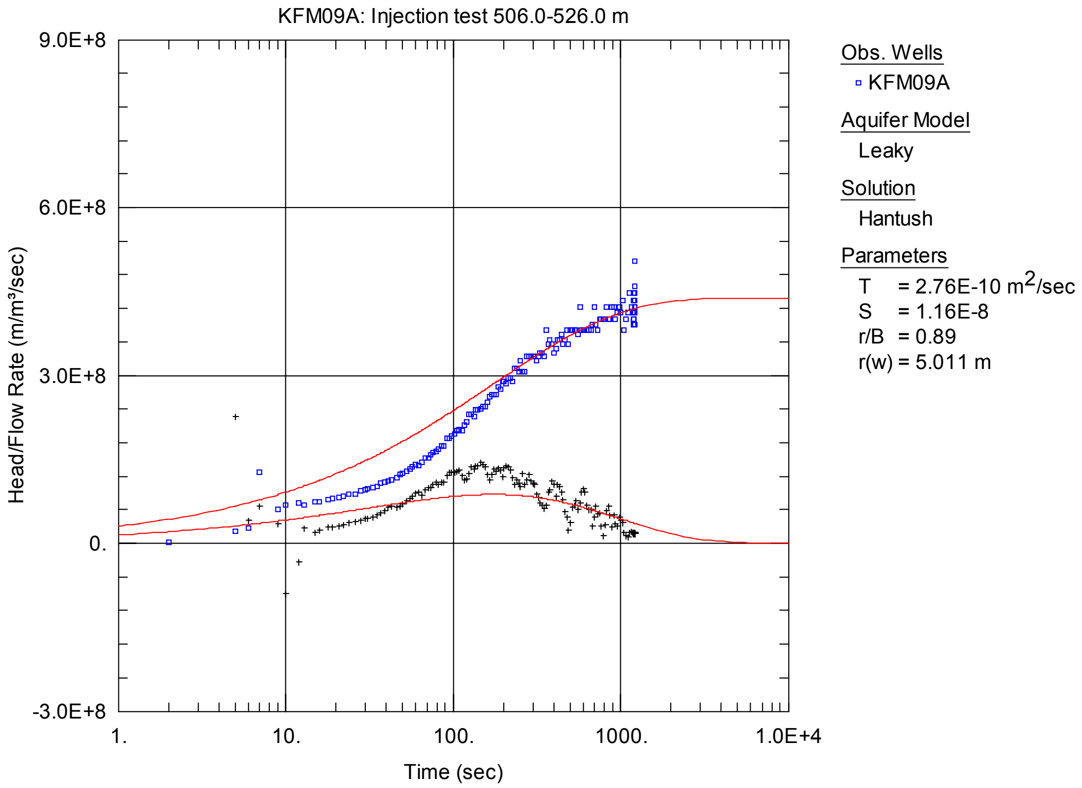


Figure A3-146. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 506.0-526.0 m in KFM09A. No unambiguous evaluation could be made on the injection period.*

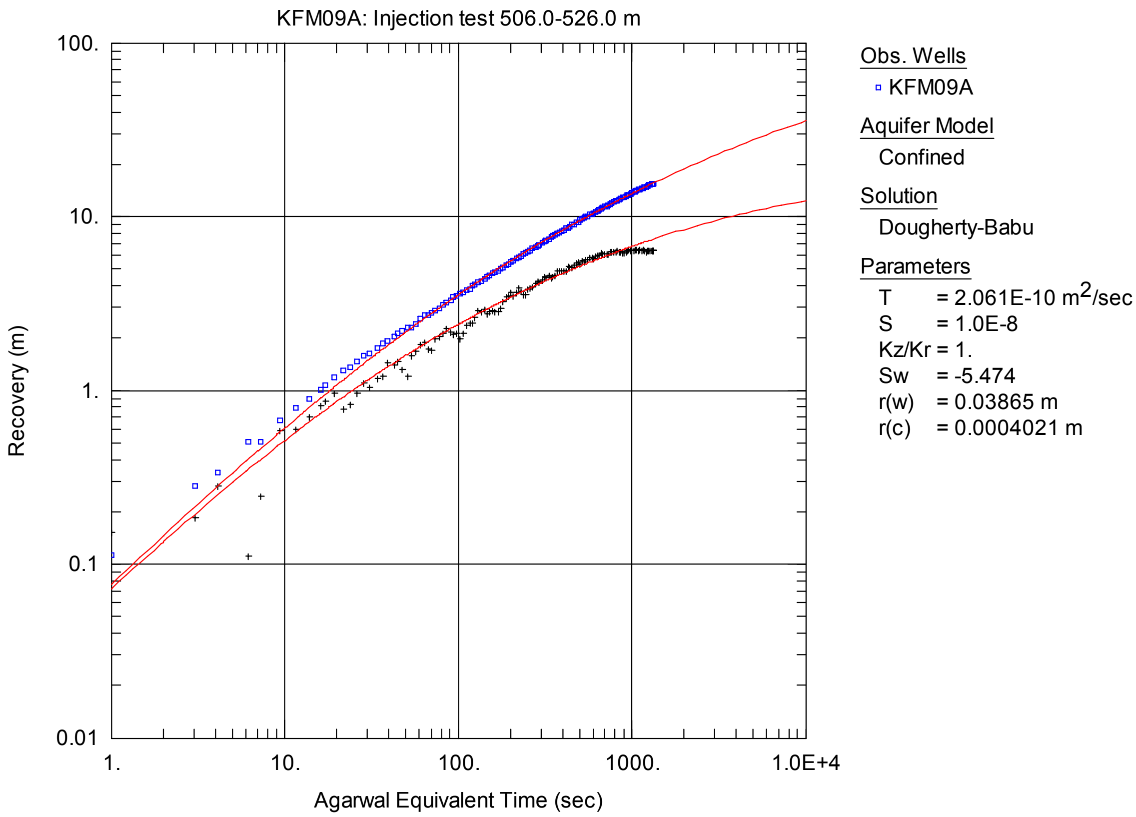


Figure A3-147. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 506.0-526.0 m in KFM09A.*

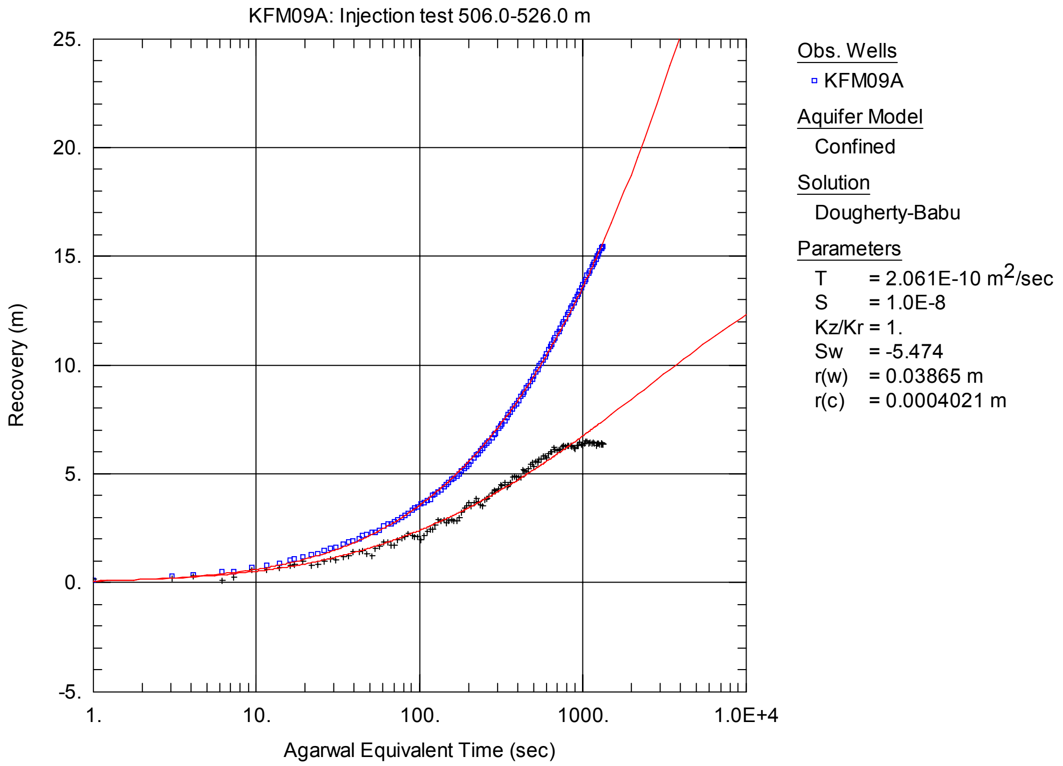


Figure A3-148. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 506.0-526.0 m in KFM09A.*

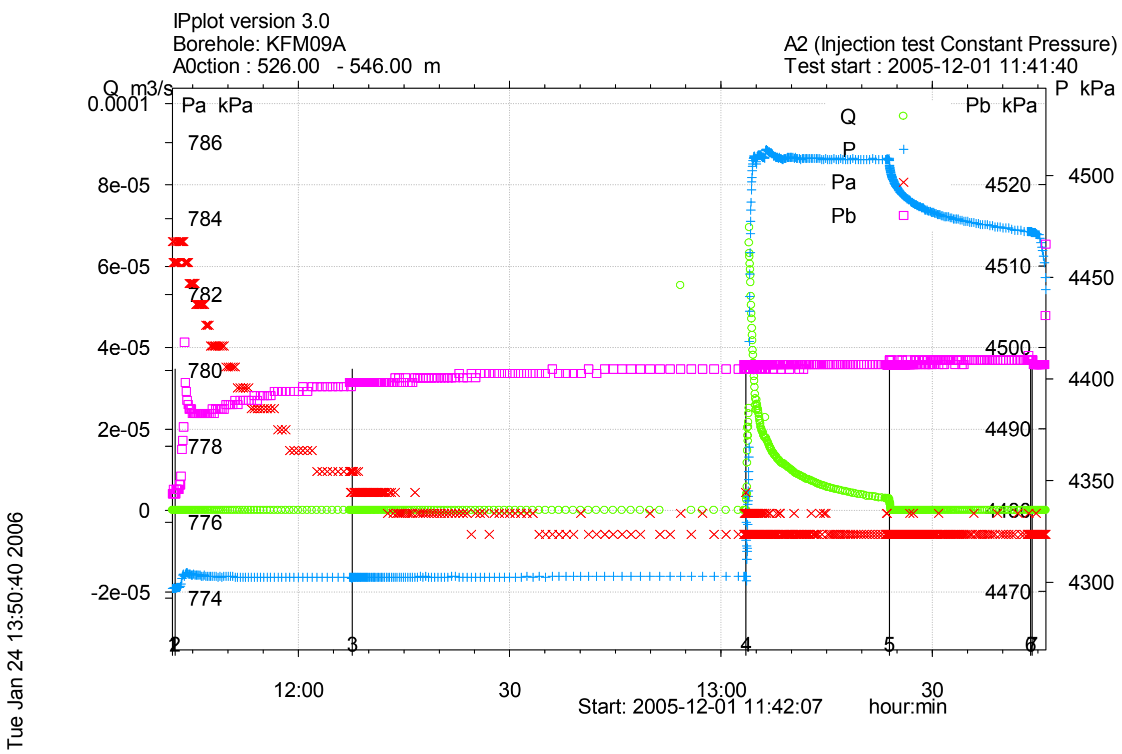


Figure A3-149. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 526.0-546.0 m in borehole KFM09A.*

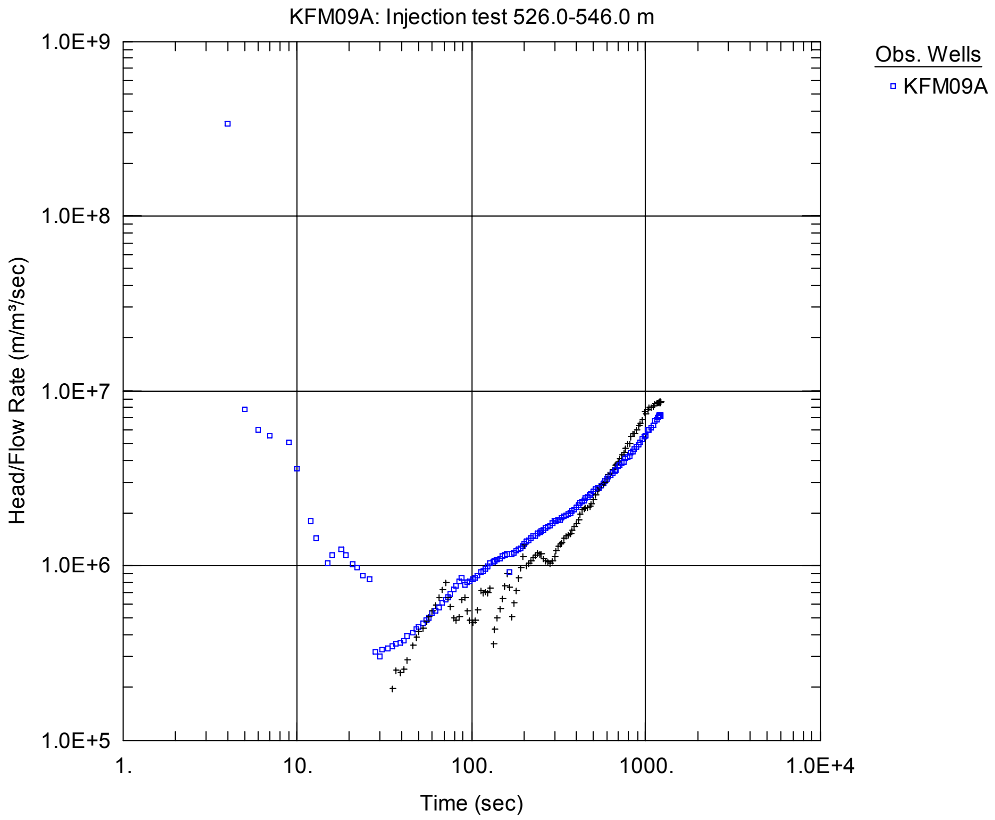


Figure A3-150. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 526.0-546.0 m in KFM09A.*

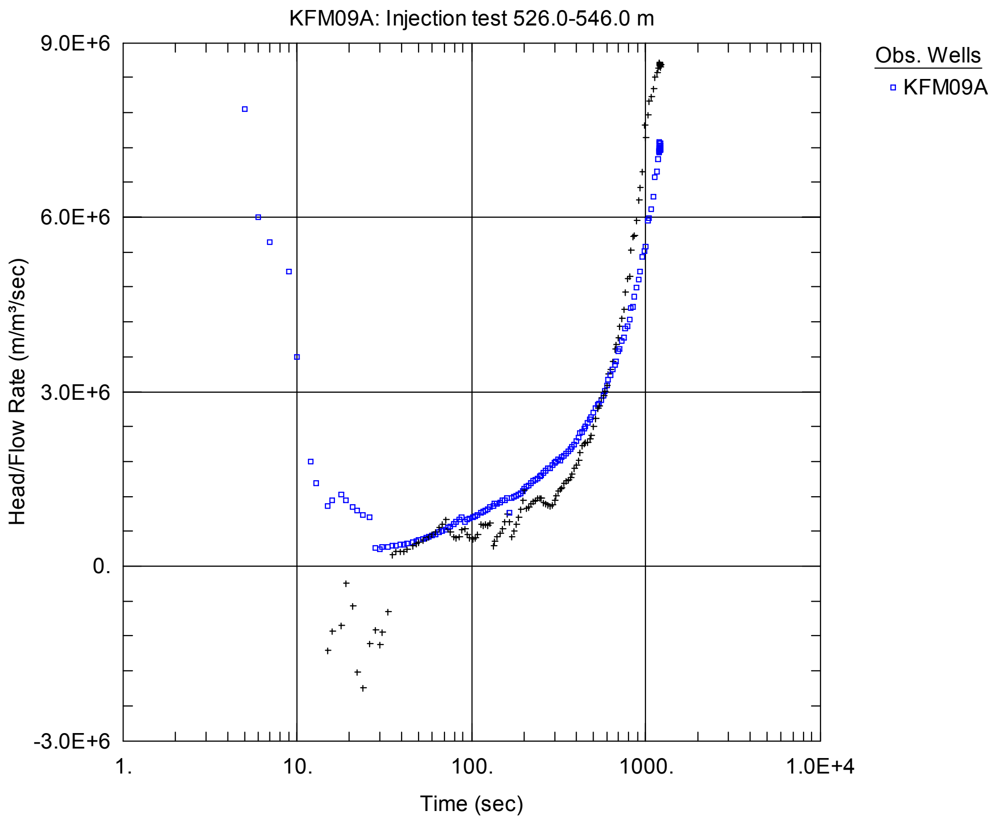


Figure A3-151. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 526.0-546.0 m in KFM09A.*

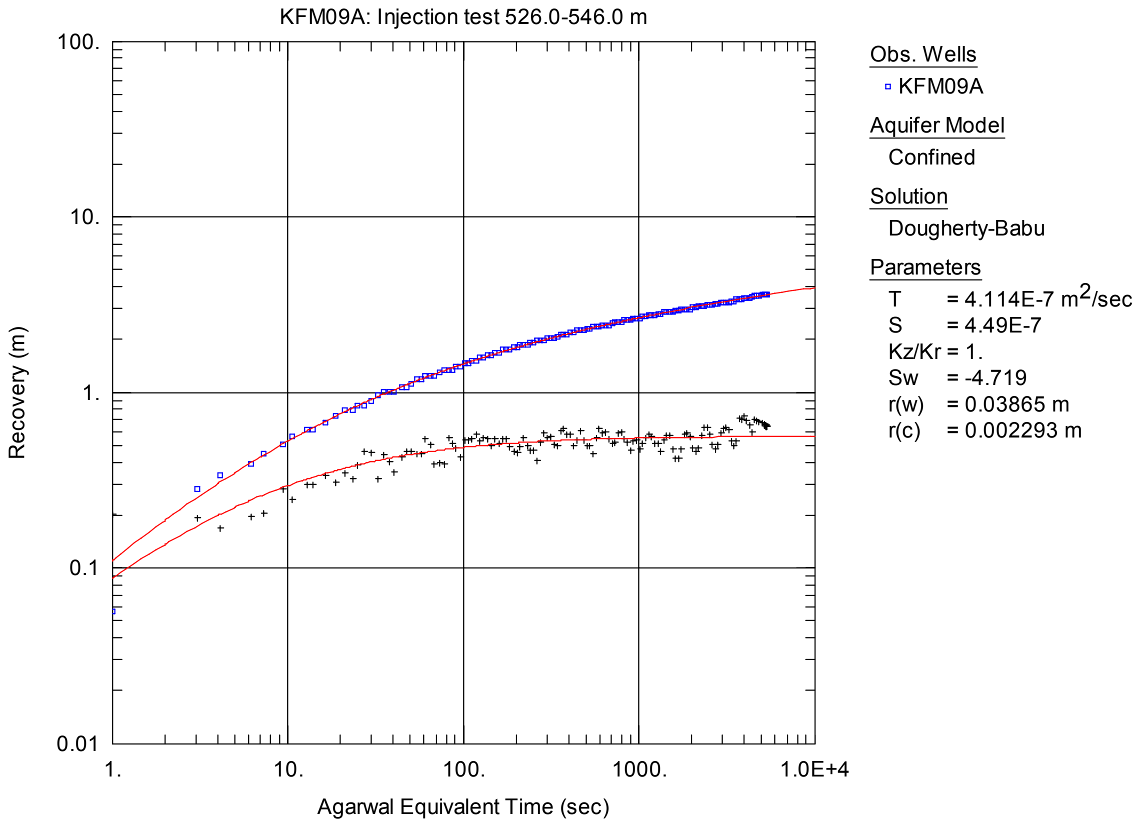


Figure A3-152. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 526.0-546.0 m in KFM09A.*

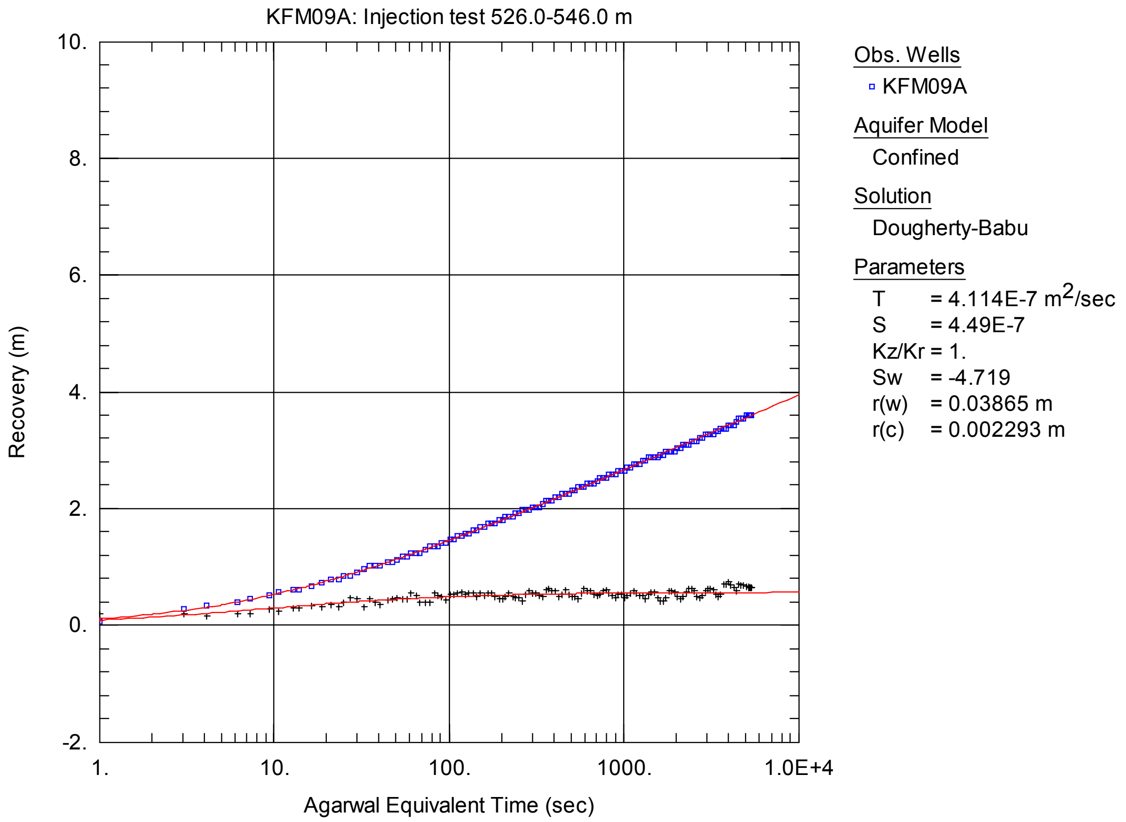


Figure A3-153. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 526.0-546.0 m in KFM09A.*

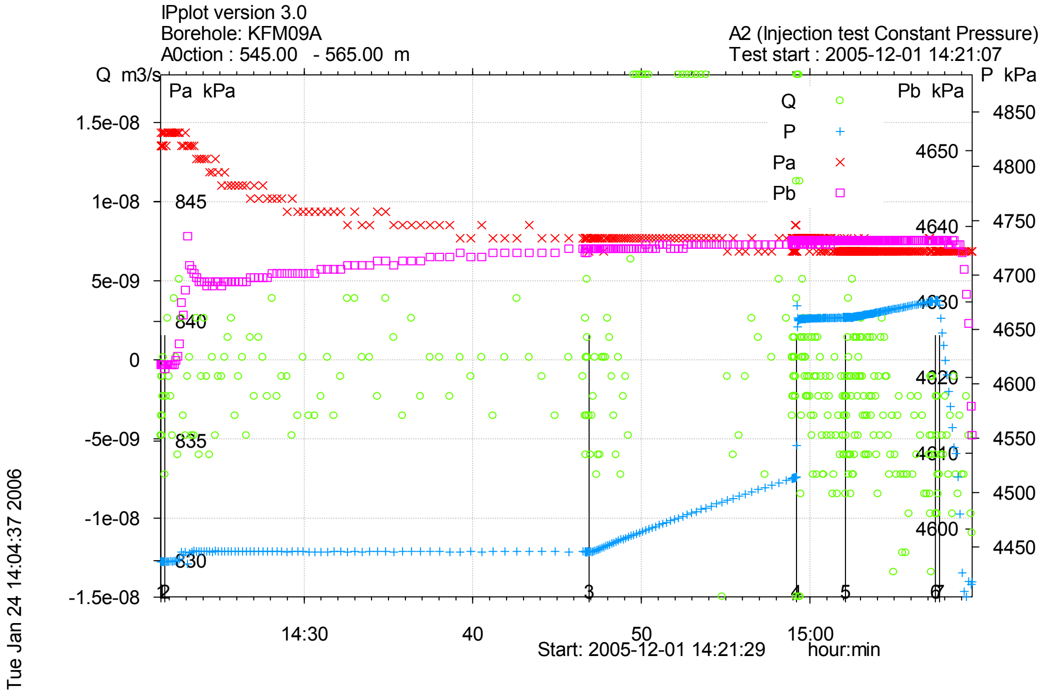


Figure A3-154. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 545.0-565.0 m in borehole KFM09A.*

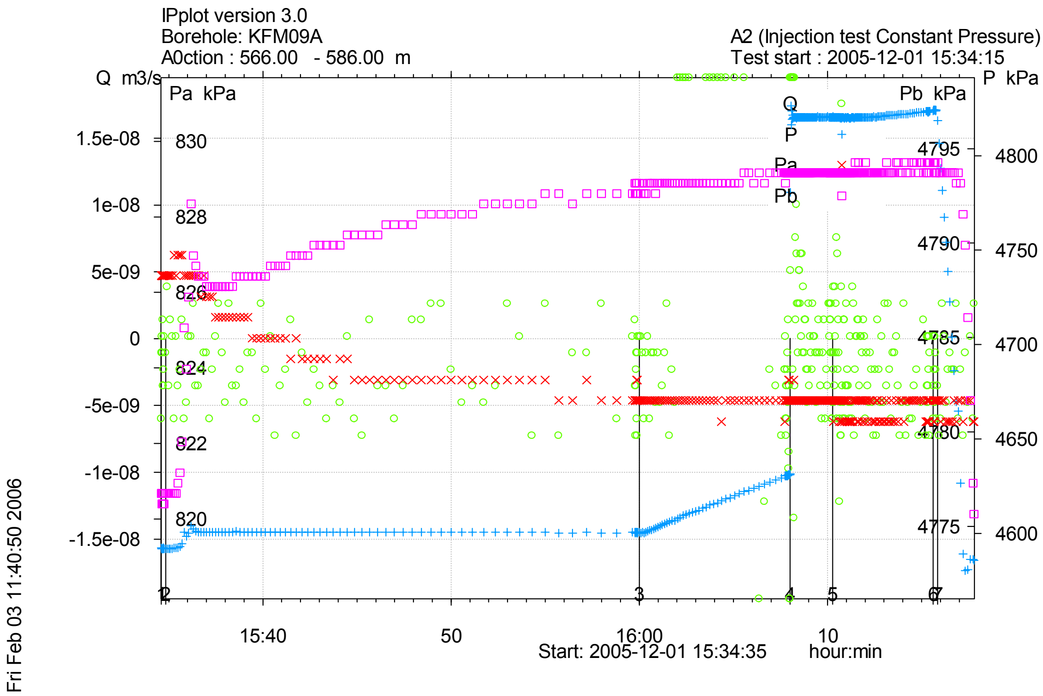


Figure A3-155. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 566.0-586.0 m in borehole KFM09A.*

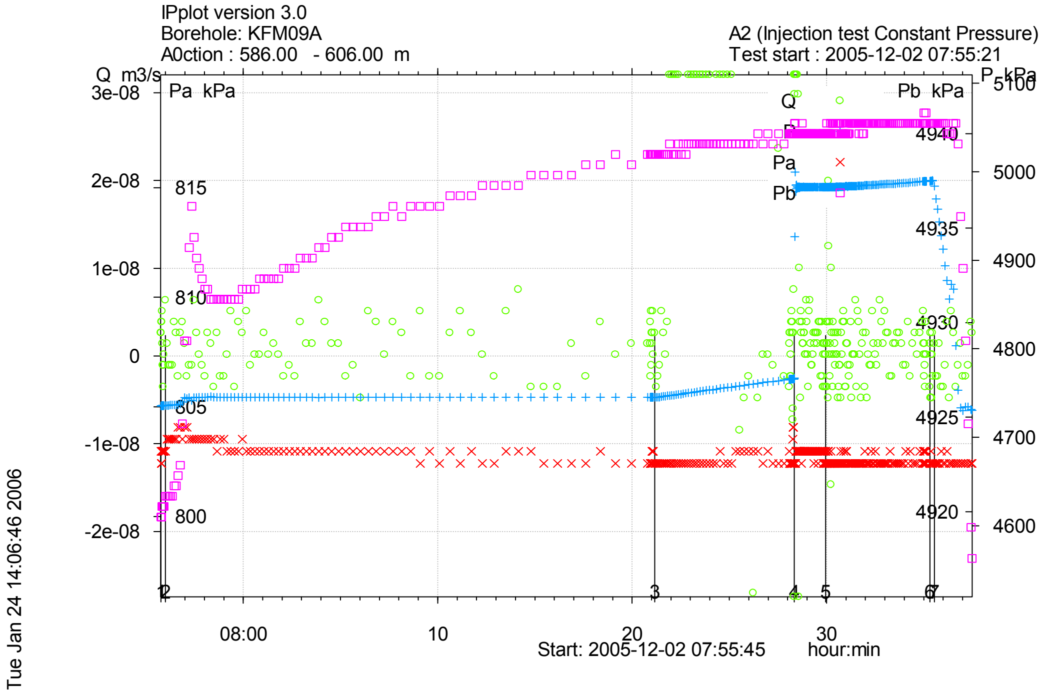


Figure A3-156. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 586.0-606.0 m in borehole KFM09A.*

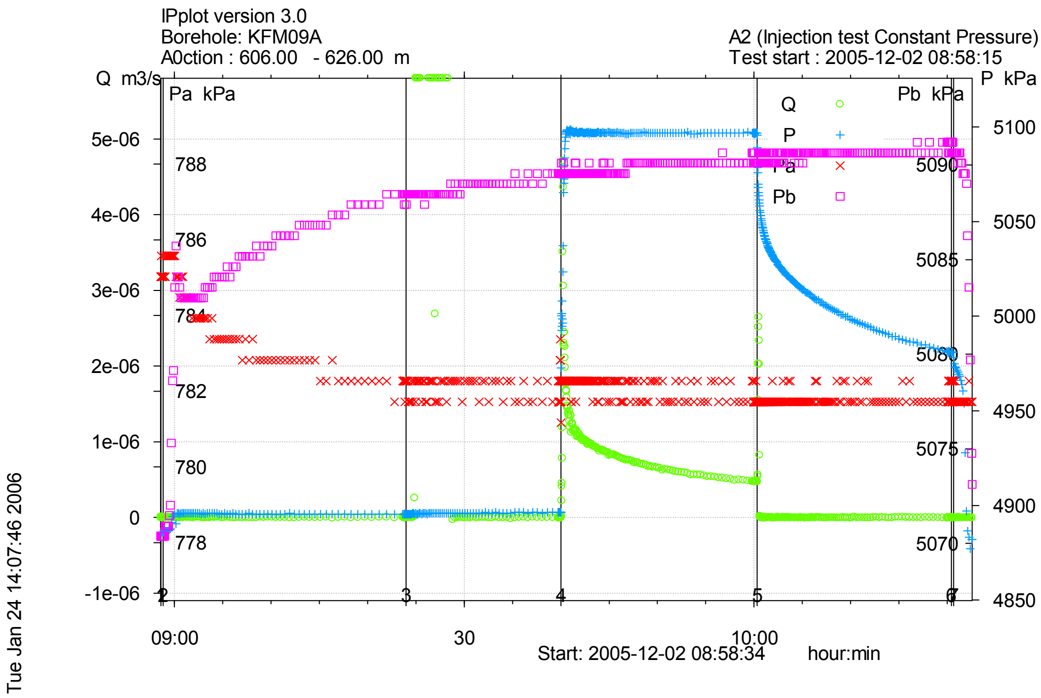


Figure A3-157. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 606.0-626.0 m in borehole KFM09A.*

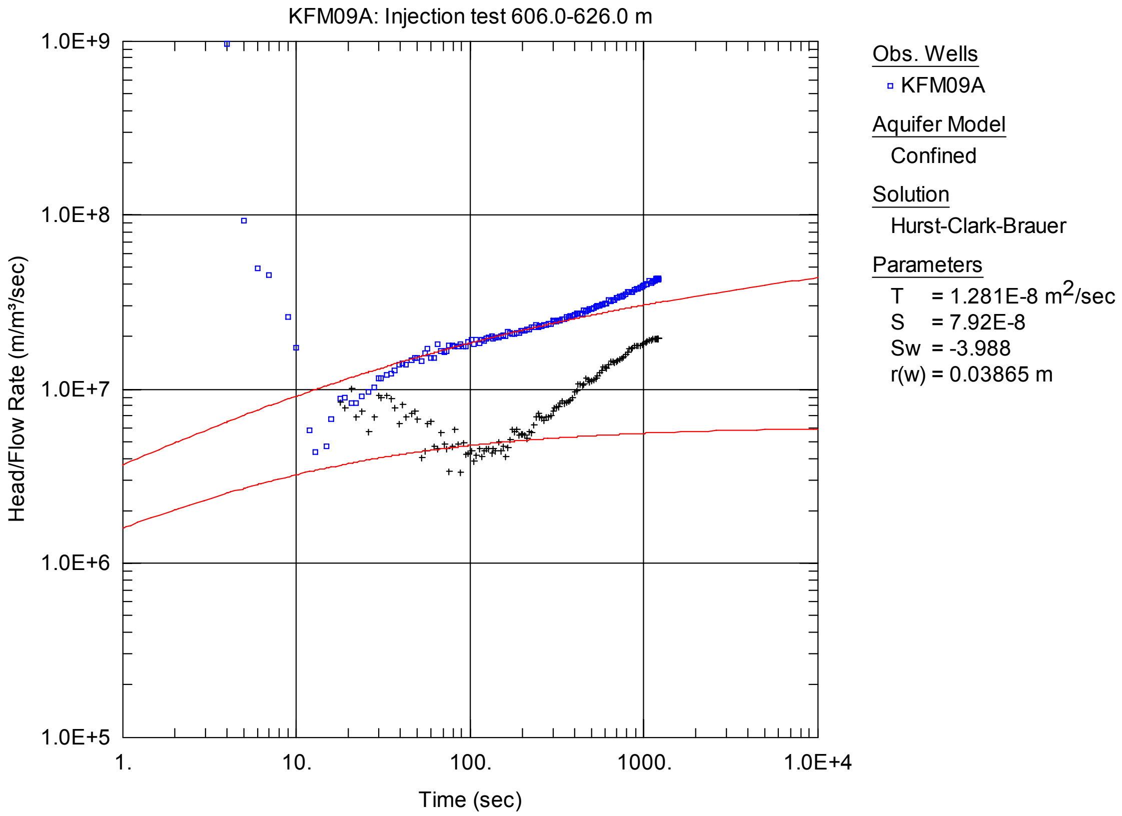


Figure A3-158. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 606.0-626.0 m in KFM09A.*

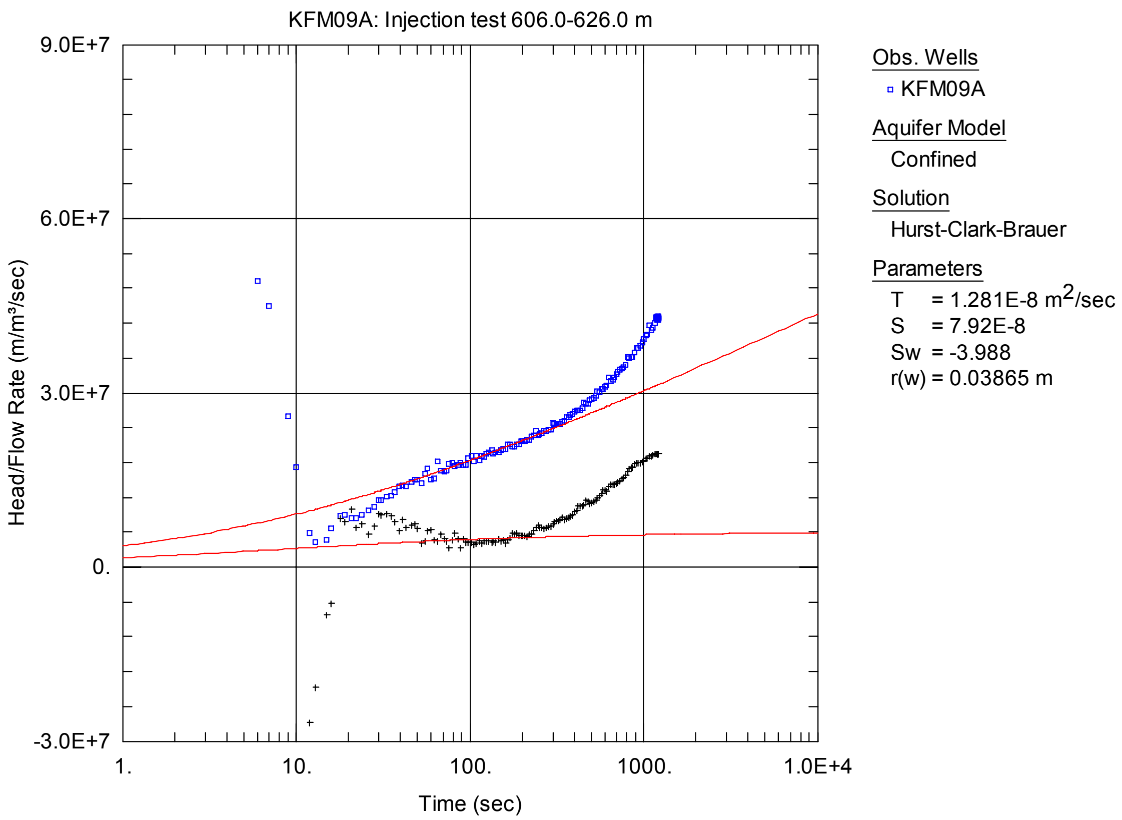


Figure A3-159. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 606.0-626.0 m in KFM09A.*

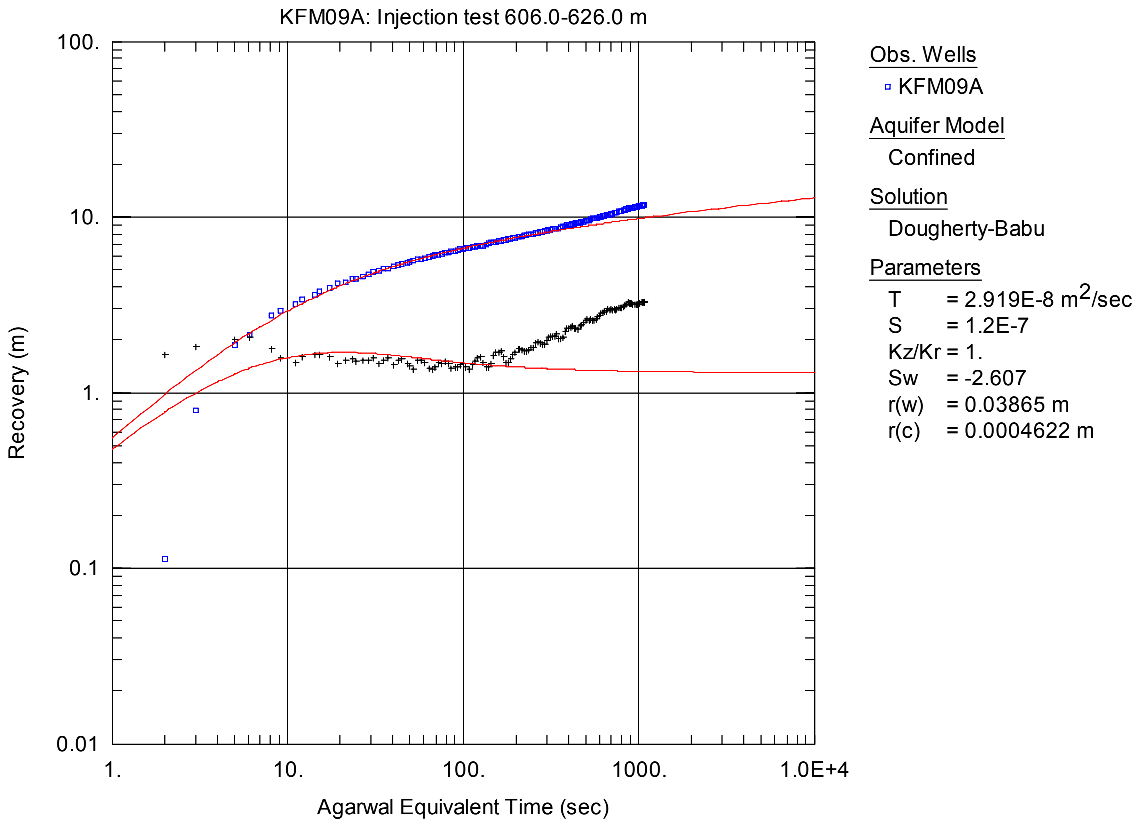


Figure A3-160. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 606.0-626.0 m in KFM09A.*

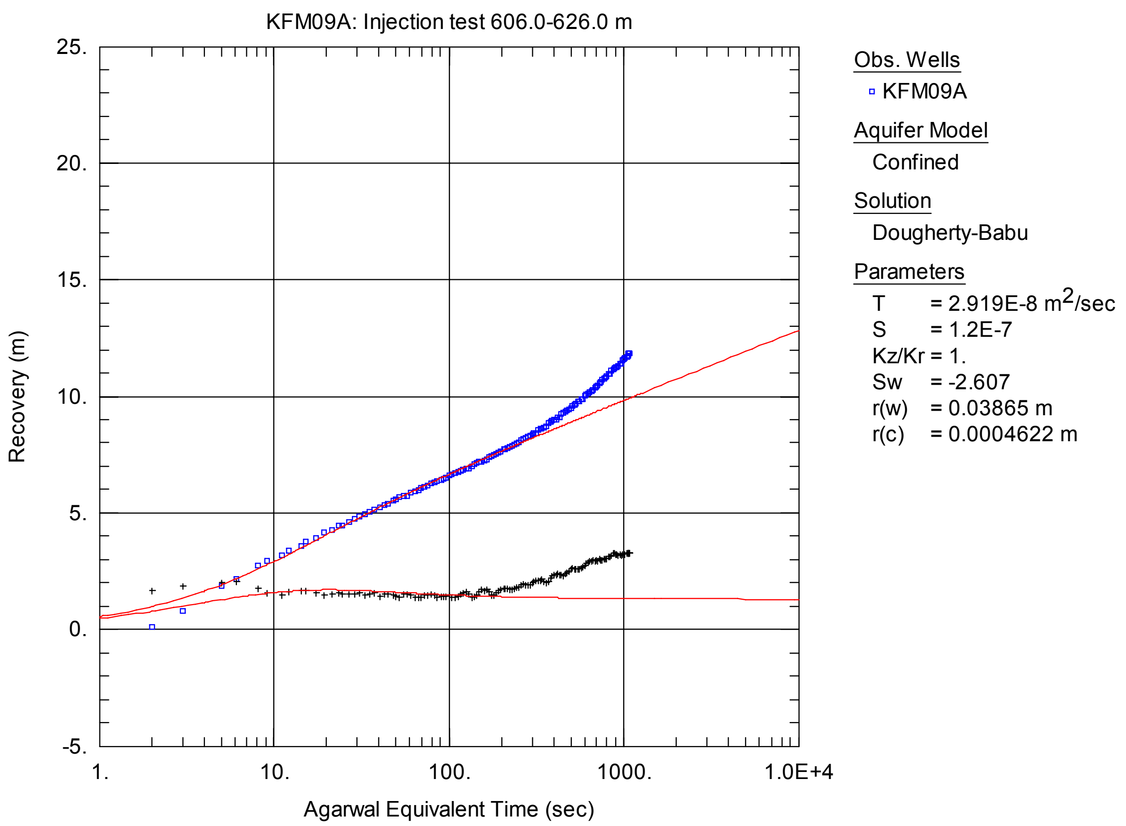


Figure A3-161. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 606.0-626.0 m in KFM09A.*

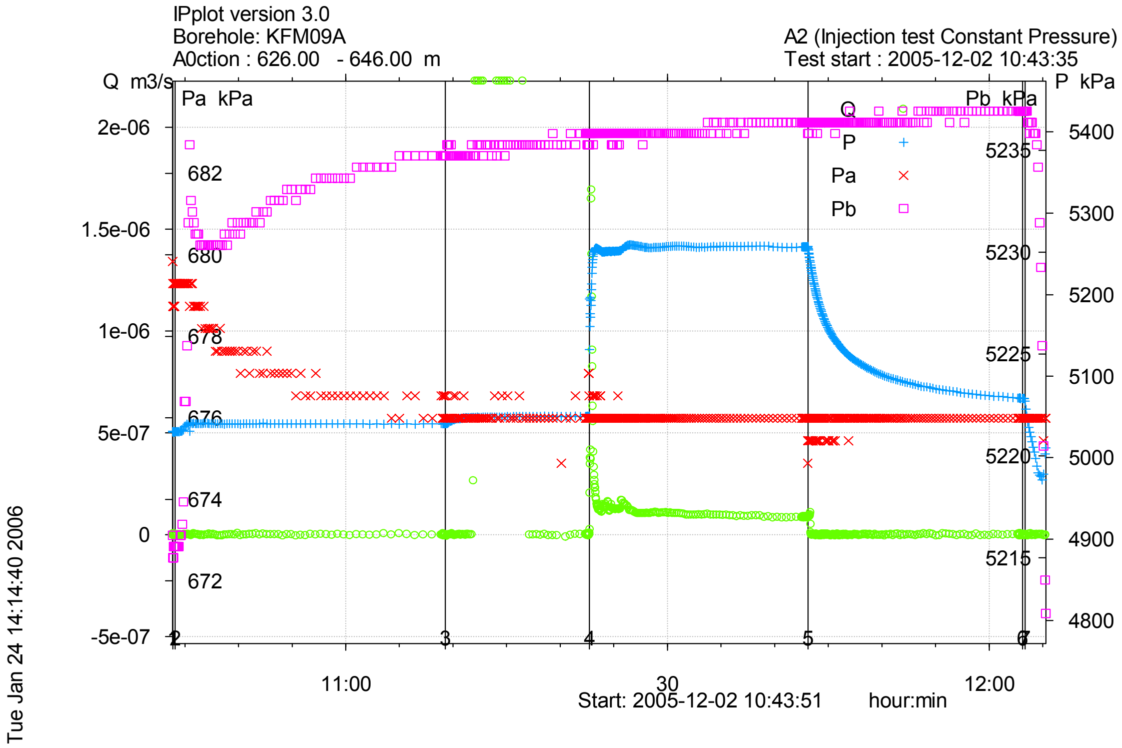


Figure A3-162. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in 626.0-646.0 m in borehole KFM09A.*

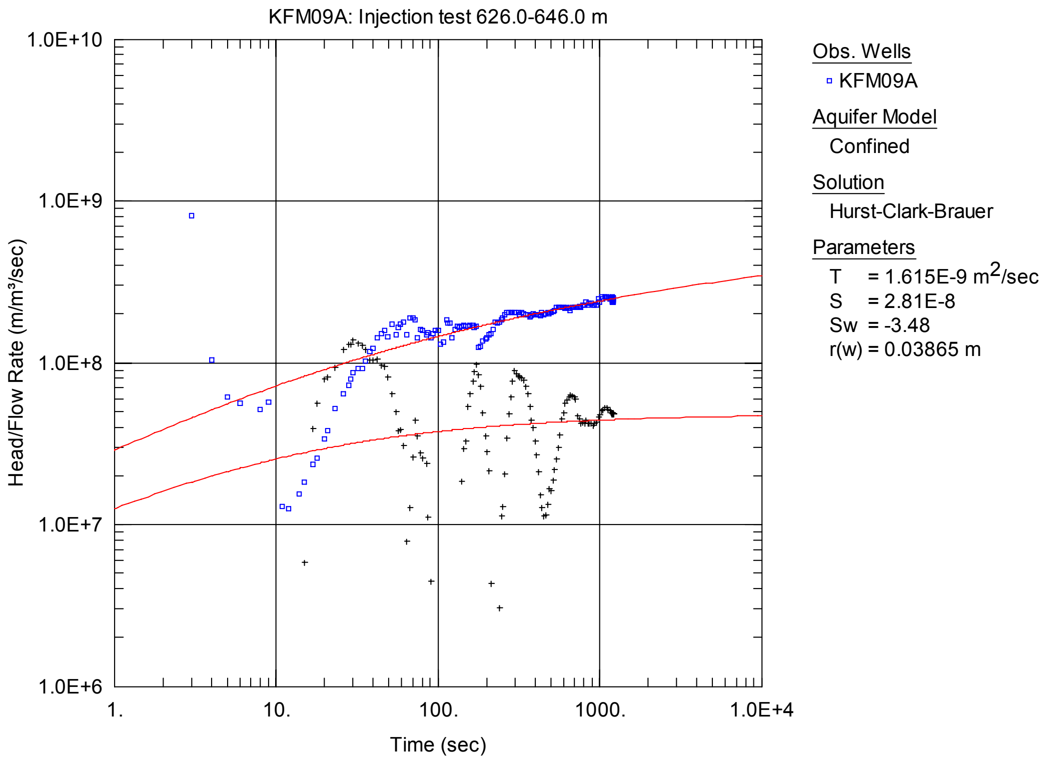


Figure A3-163. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 626.0-646.0 m in KFM09A.*

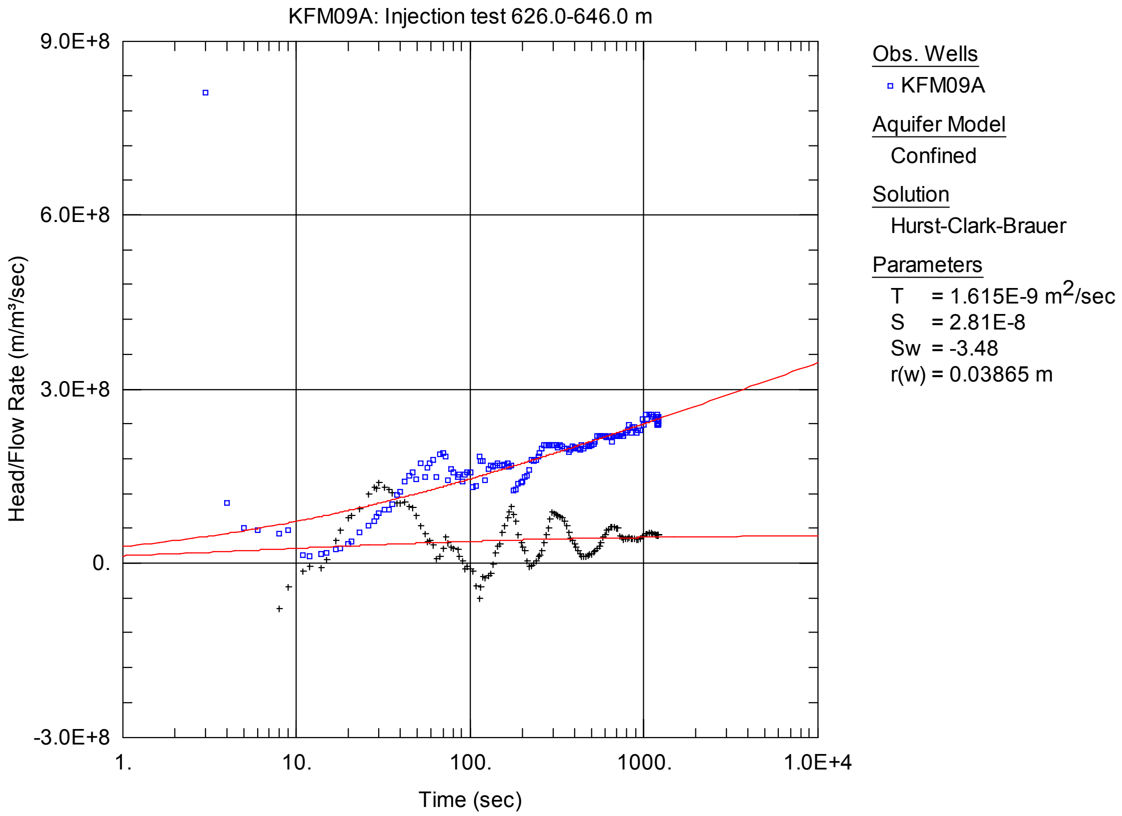


Figure A3-164. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in 626.0-646.0 m in KFM09A.*

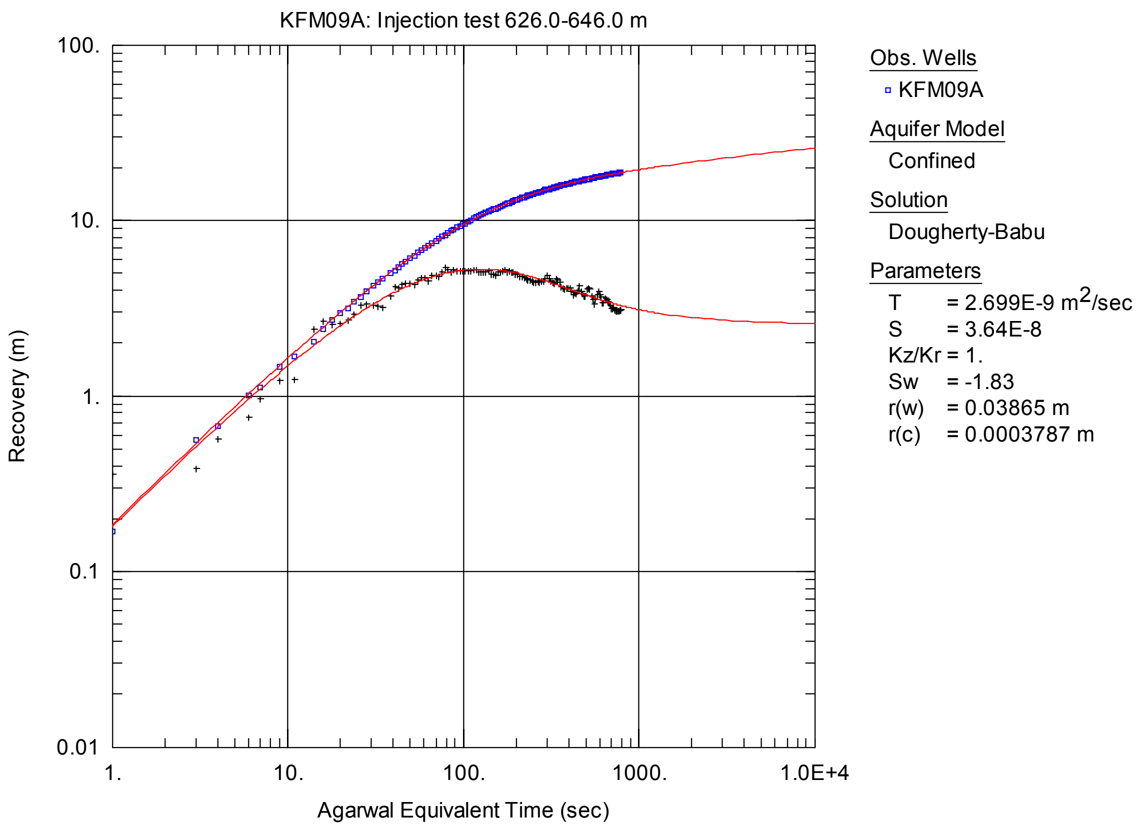


Figure A3-165. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 626.0-646.0 m in KFM09A.*

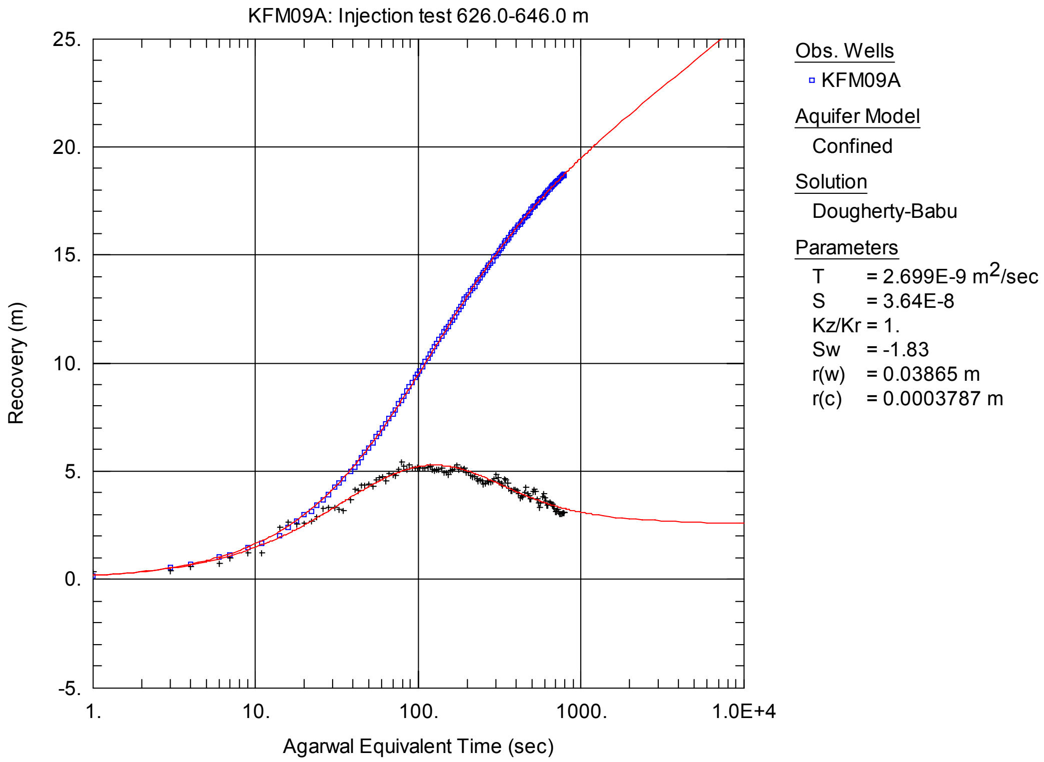


Figure A3-166. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 626.0-646.0 m in KFM09A.*

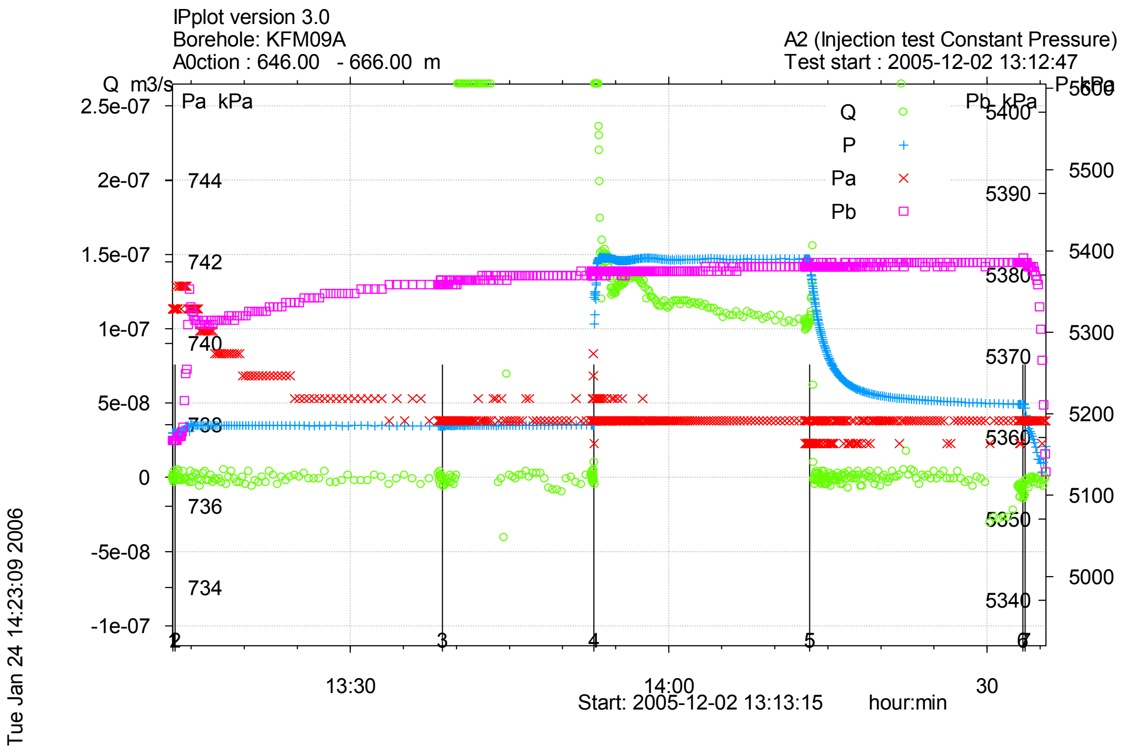


Figure A3-167. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 646.0-666.0 m in borehole KFM09A.*

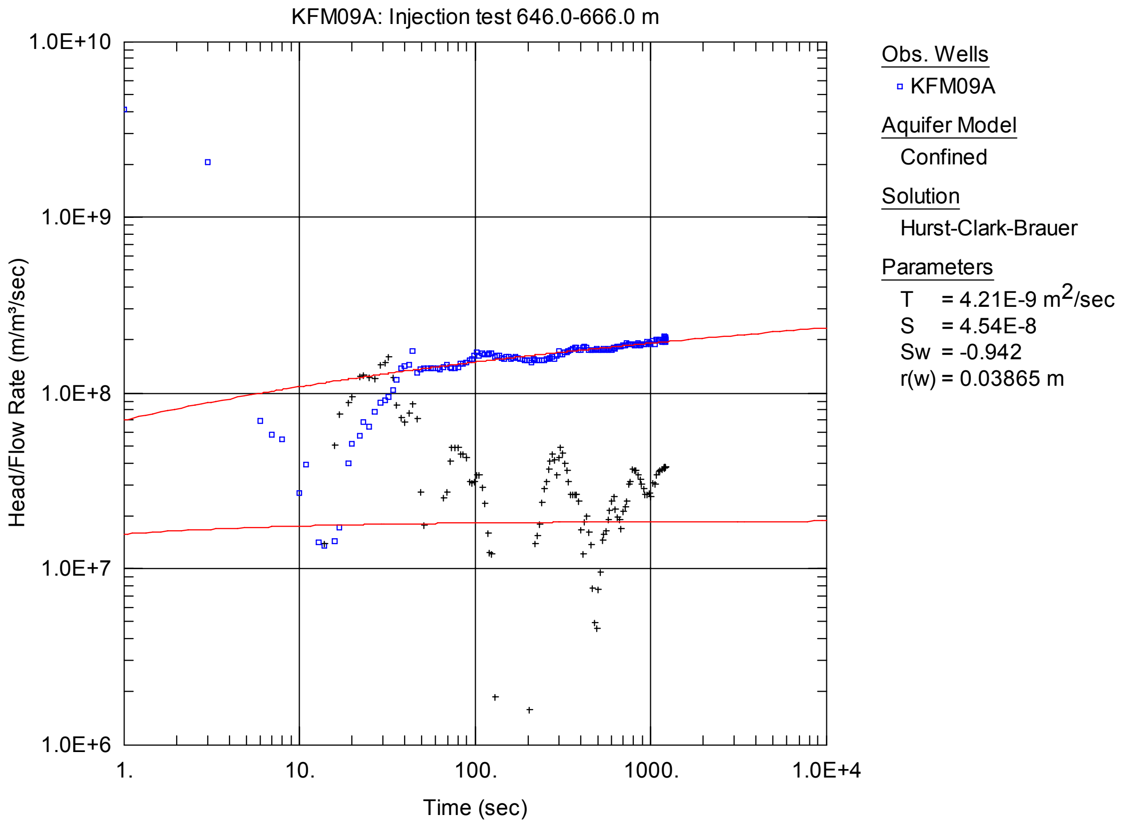


__Figure A3-168.__ Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 646.0-666.0 m in KFM09A.

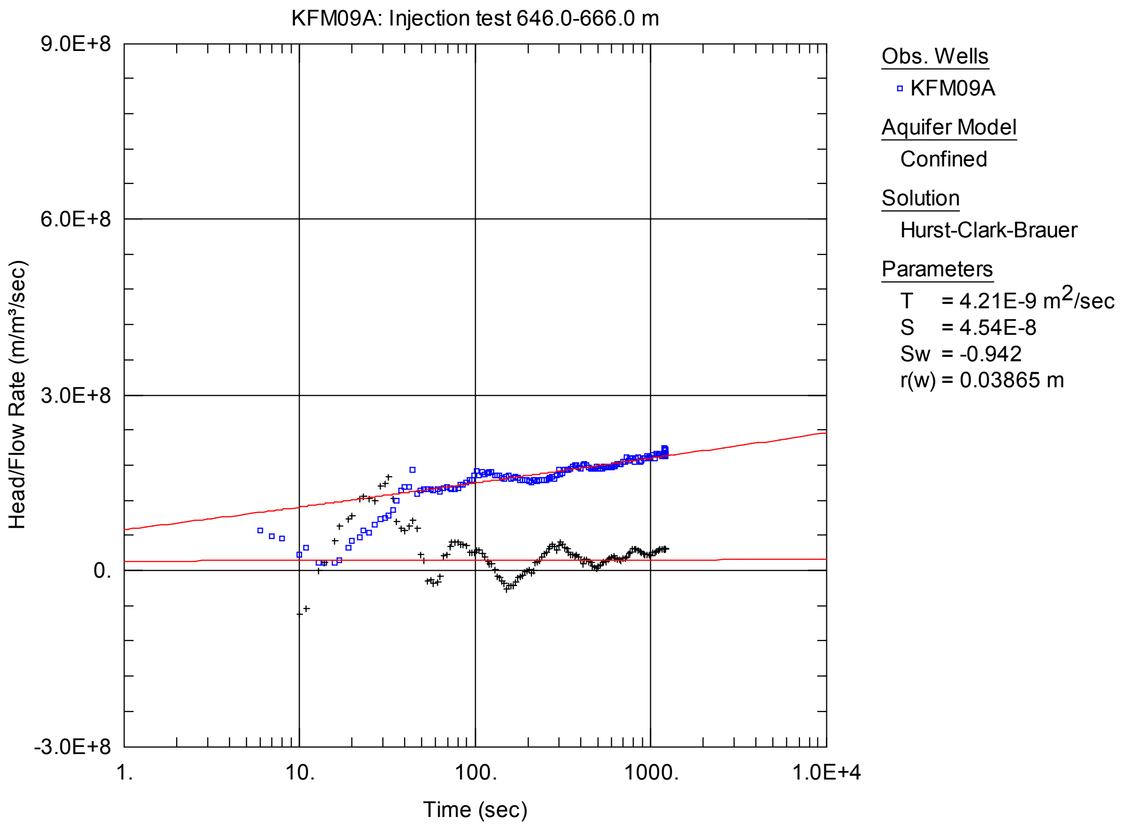


__Figure A3-169.__ Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 646.0-666.0m in KFM09A.

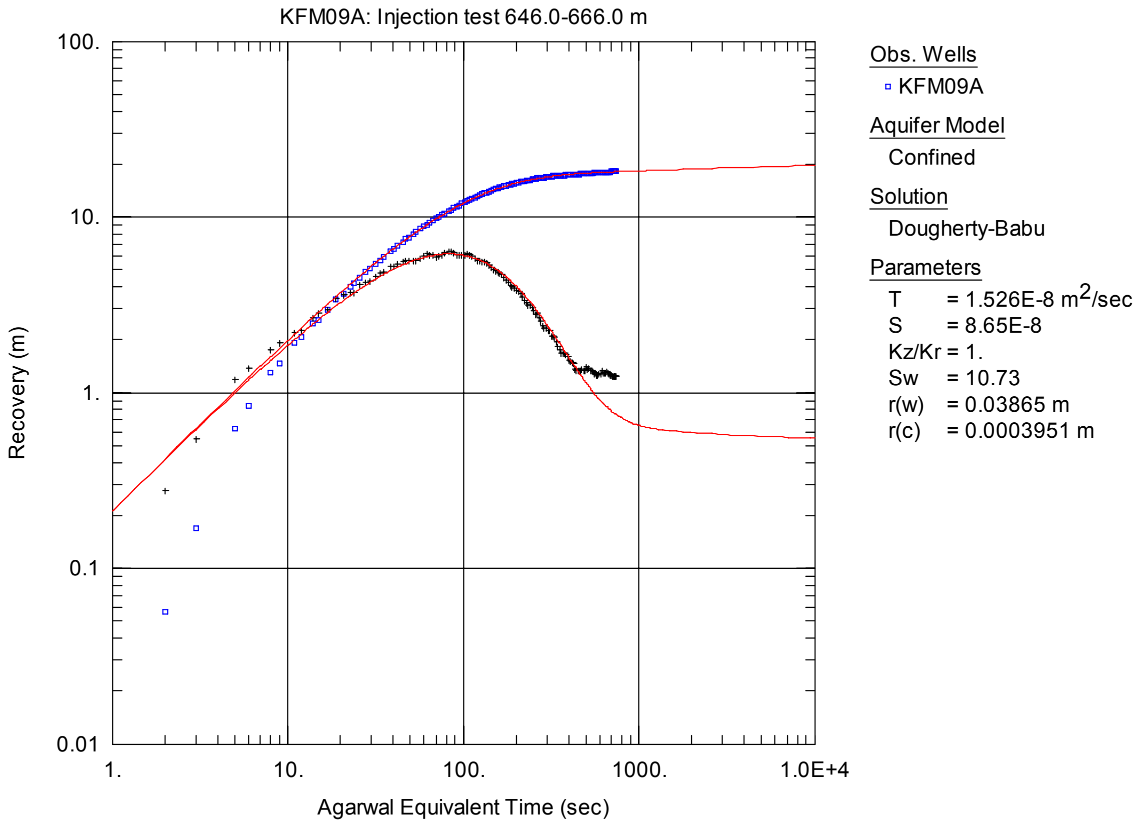


Figure A3-170. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 646.0-666.0 m in KFM09A.*

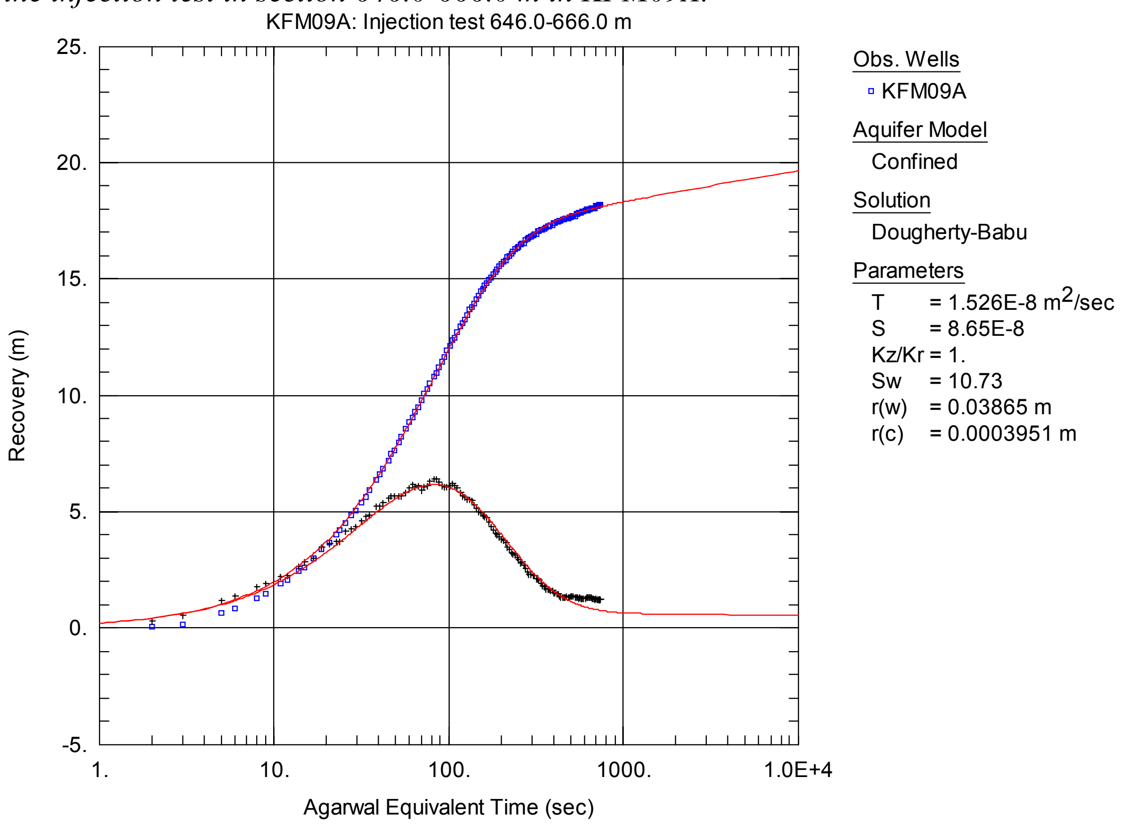


Figure A3-171. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 646.0-666.0 m in KFM09A.*

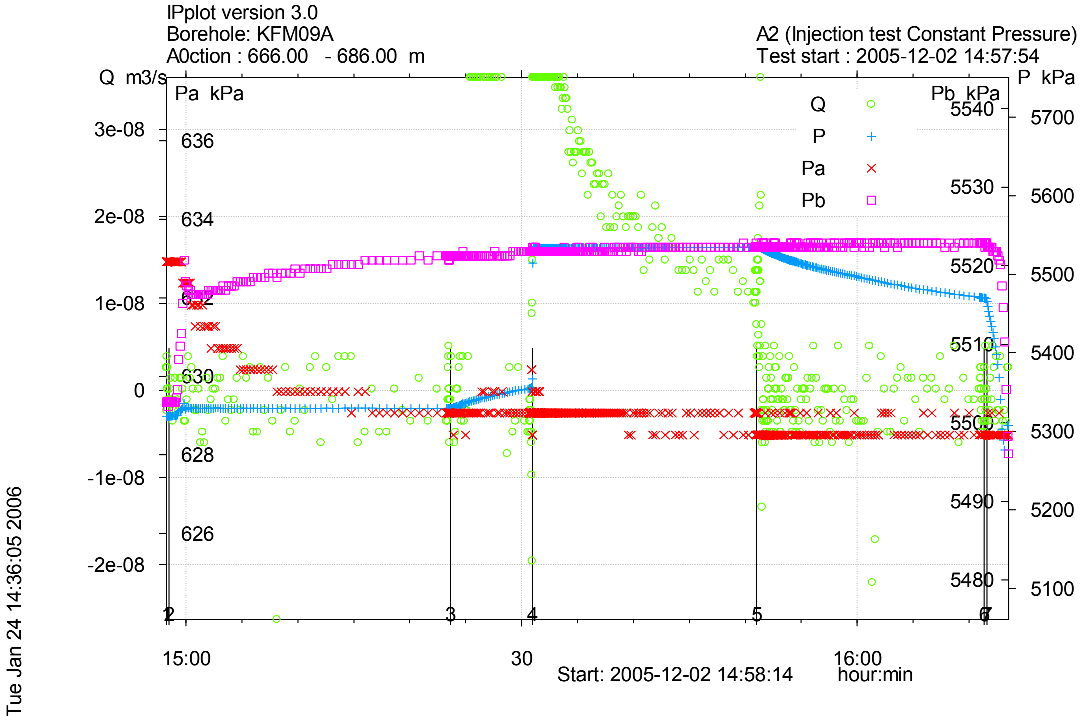


Figure A3-172. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 666.0-686.0 m in borehole KFM09A.*

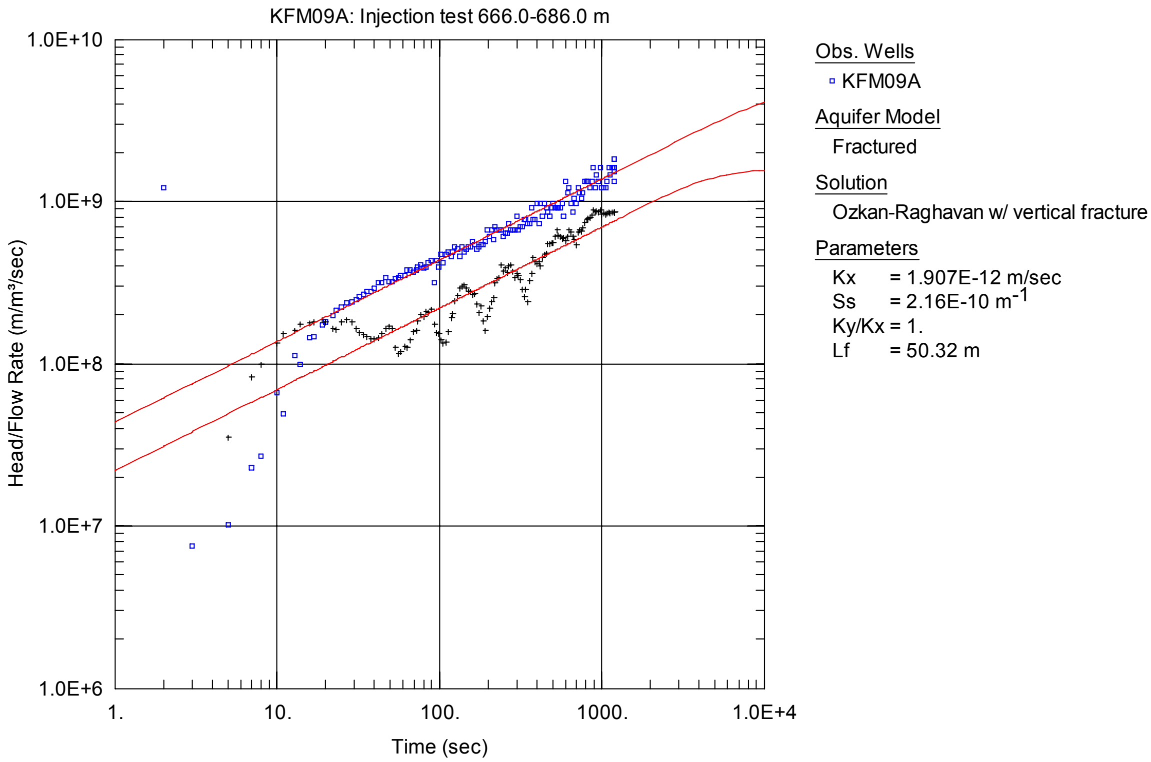


Figure A3-173. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 666.0-686.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

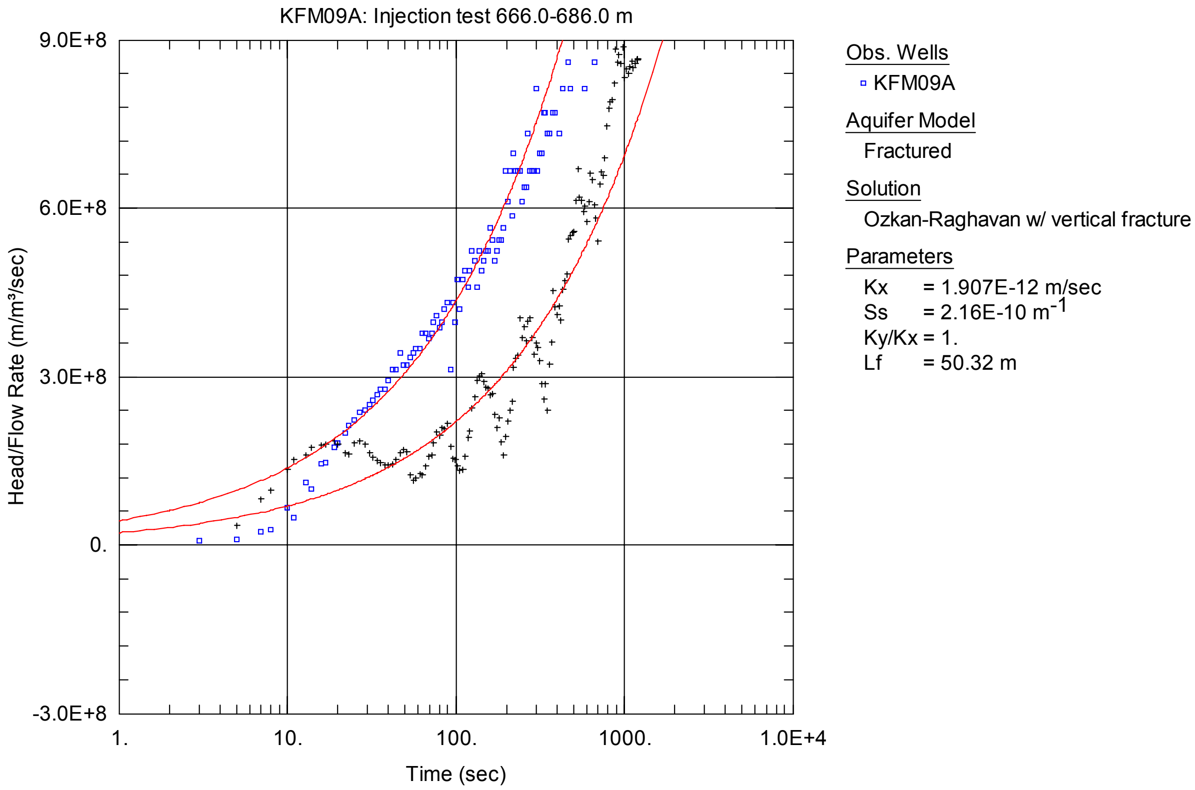


__Figure A3-174.__ Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 666.0-686.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.

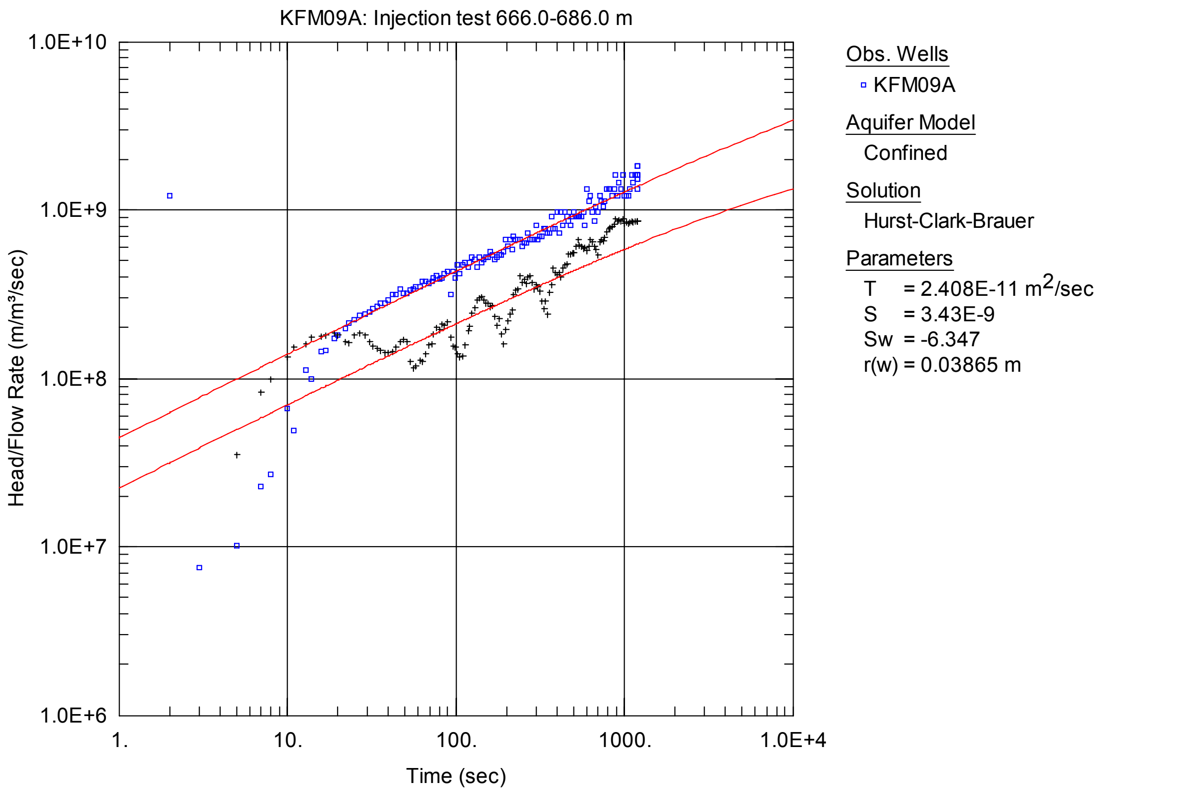


__Figure A3-175.__ Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 666.0-686.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for pseudo-radial flow.

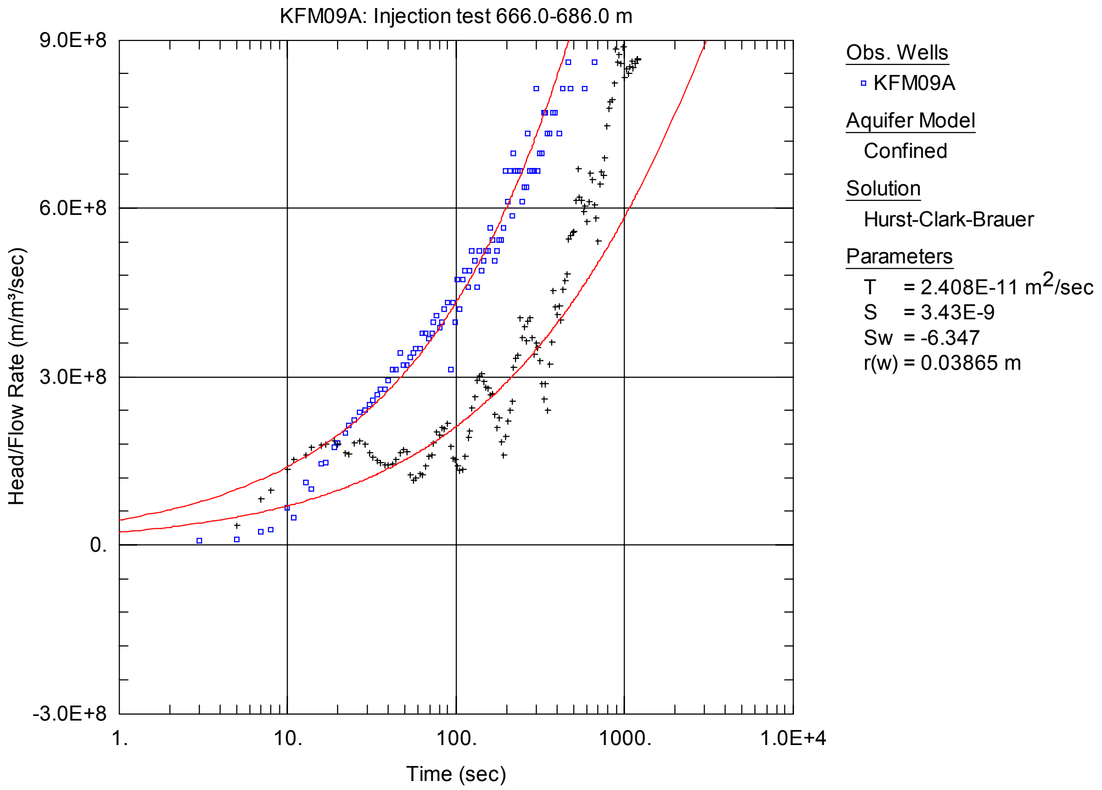


Figure A3-176. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 666.0-686.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for pseudo-radial flow.*

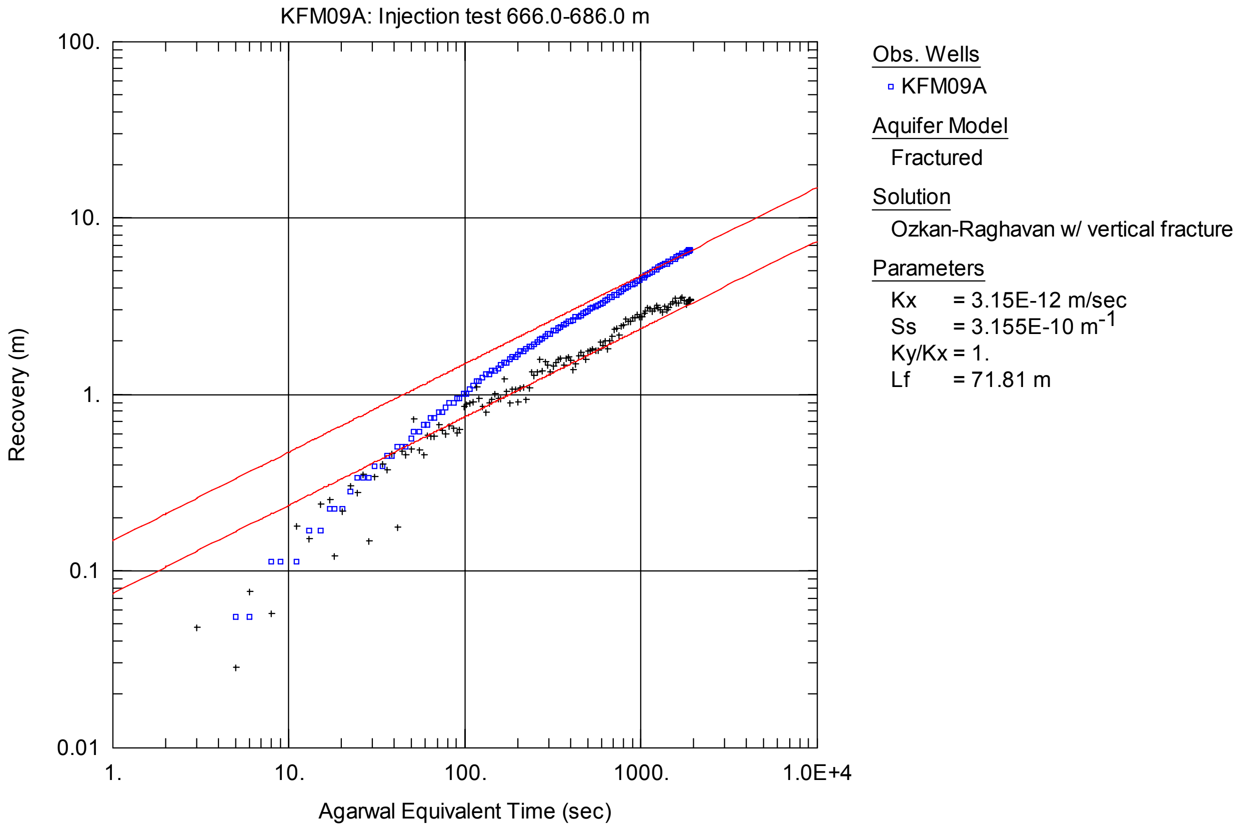


Figure A3-177. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 666.0-686.0 m in KFM09A.*

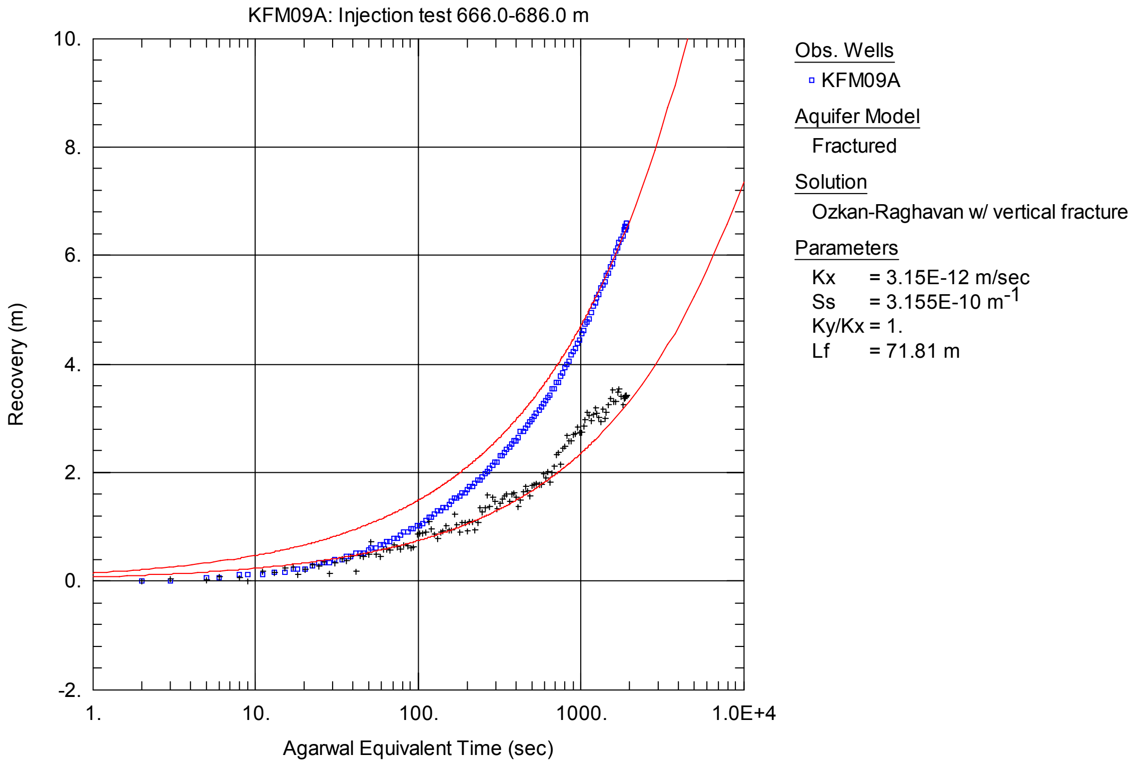


Figure A3-178. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 666.0-686.0 m in KFM09A.*

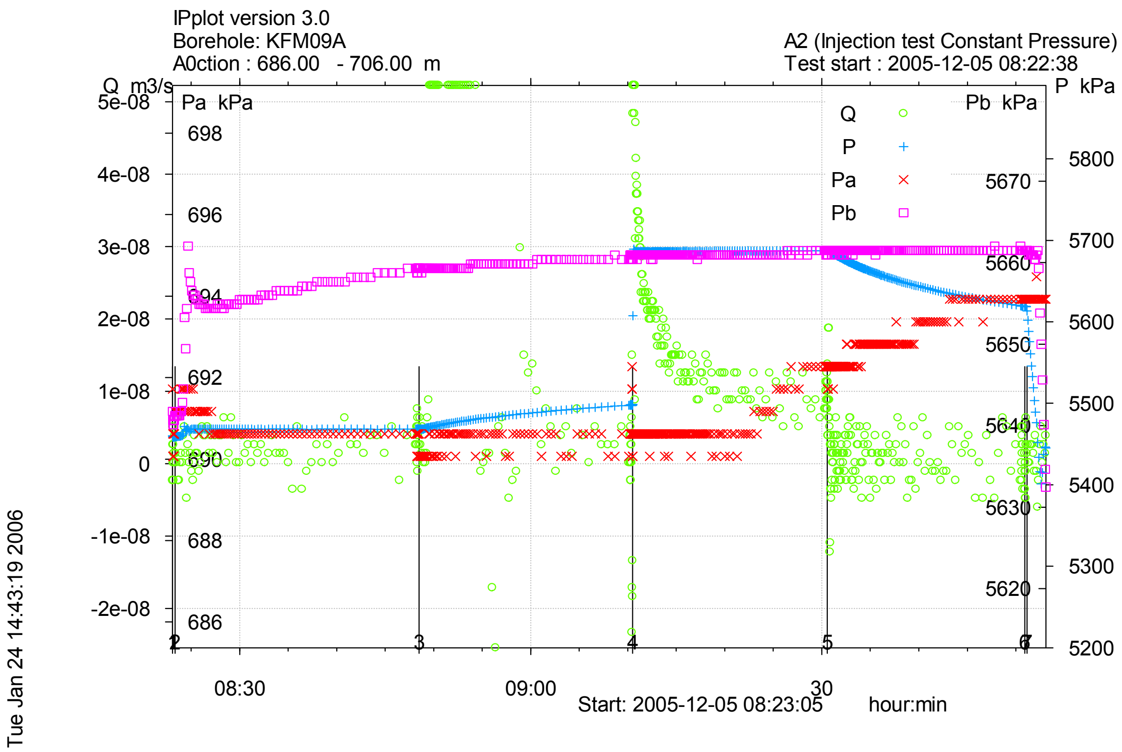


Figure A3-179. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 686.0-706.0 m in borehole KFM09A.*

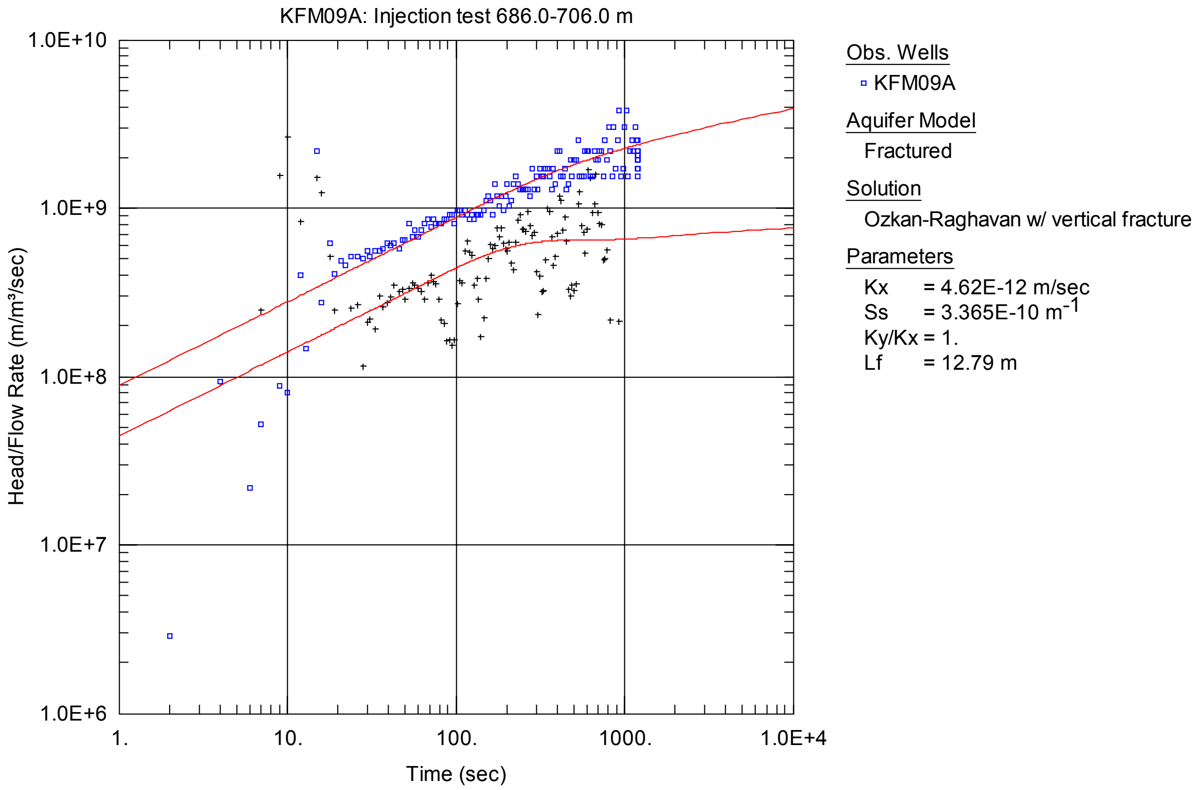


Figure A3-180. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 686.0-706.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

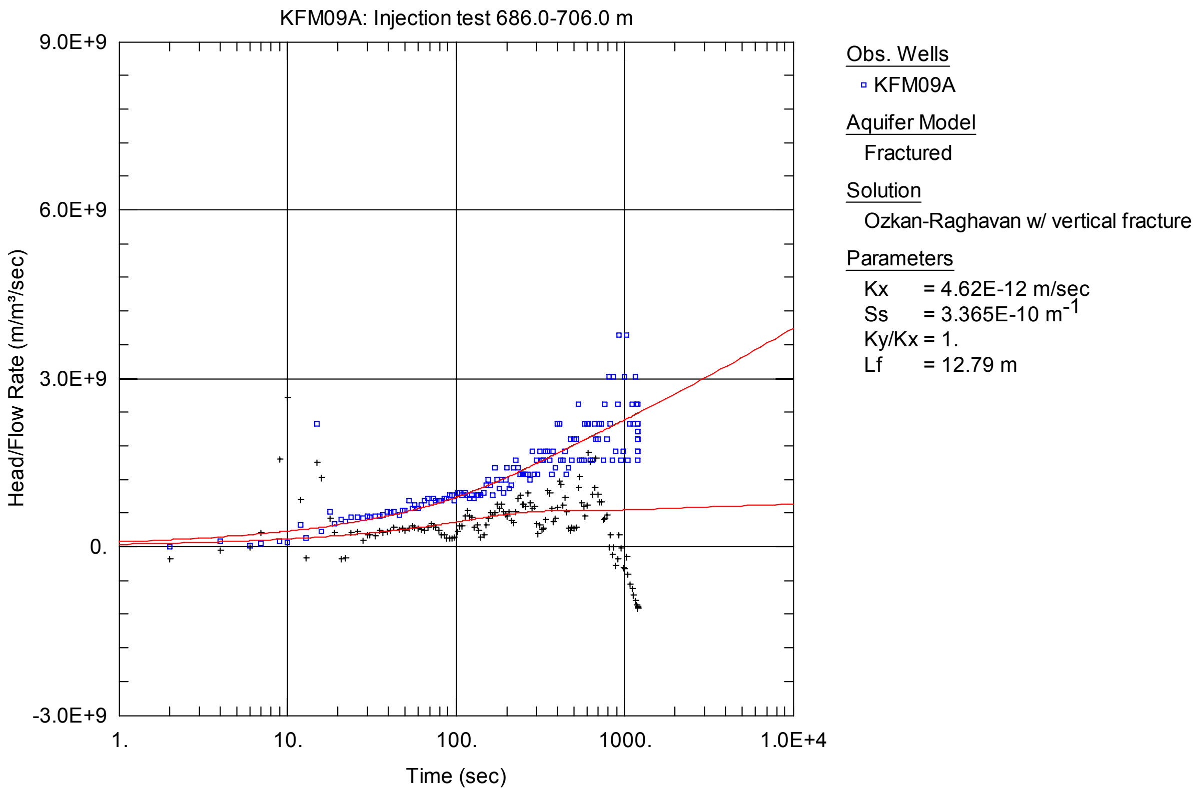


Figure A3-181. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 686.0-706.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

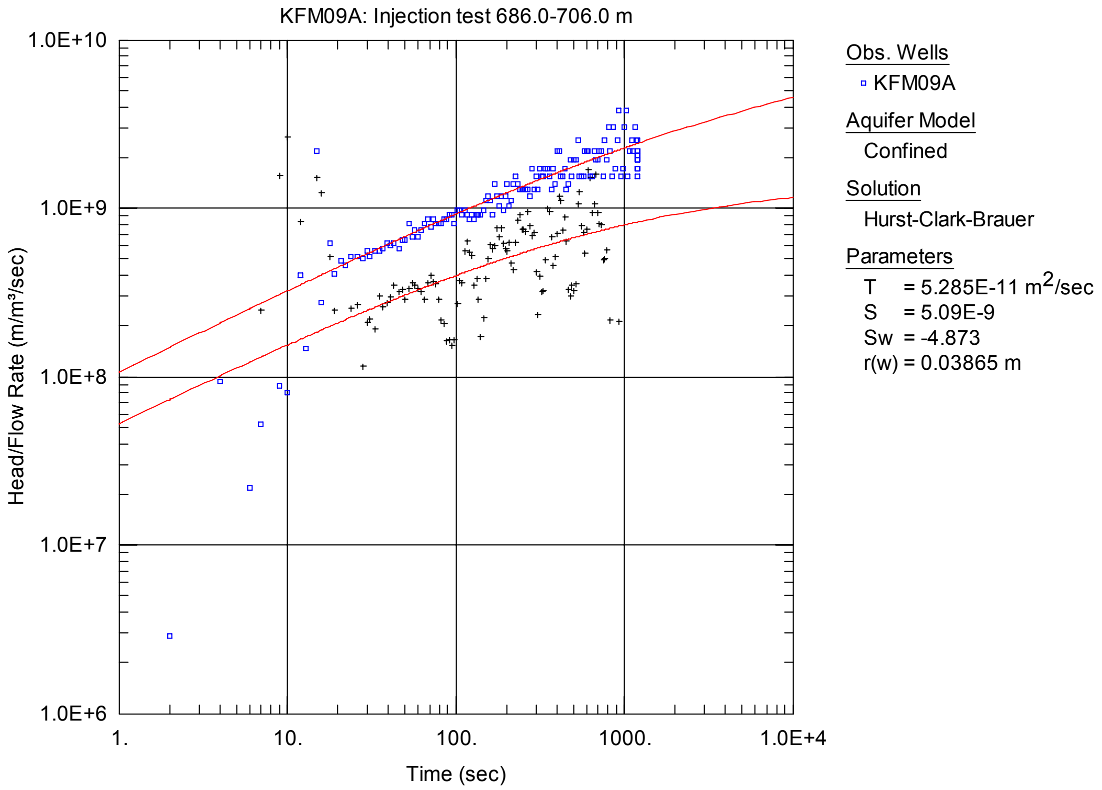


__Figure A3-182.__ Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 686.0-706.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for pseudo-radial flow.

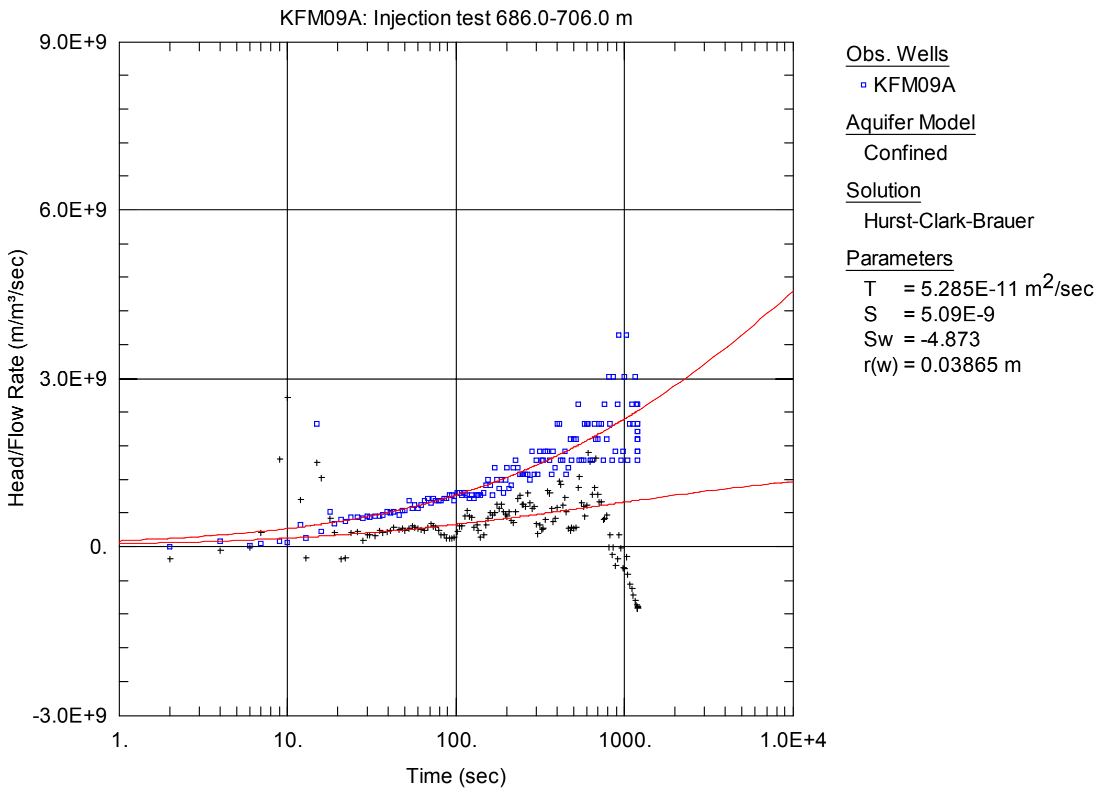


__Figure A3-183.__ Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 686.0-706.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for pseudo-radial flow.

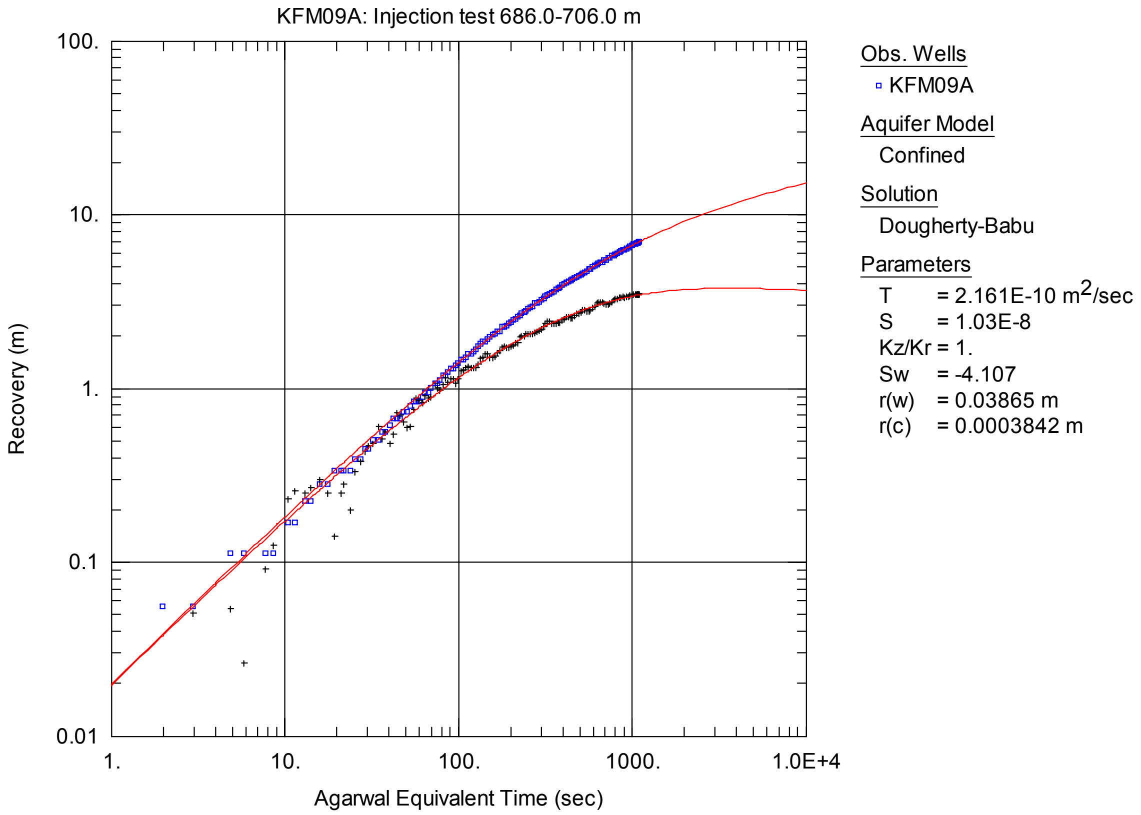


Figure A3-184. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 686.0-706.0m in KFM09A.*

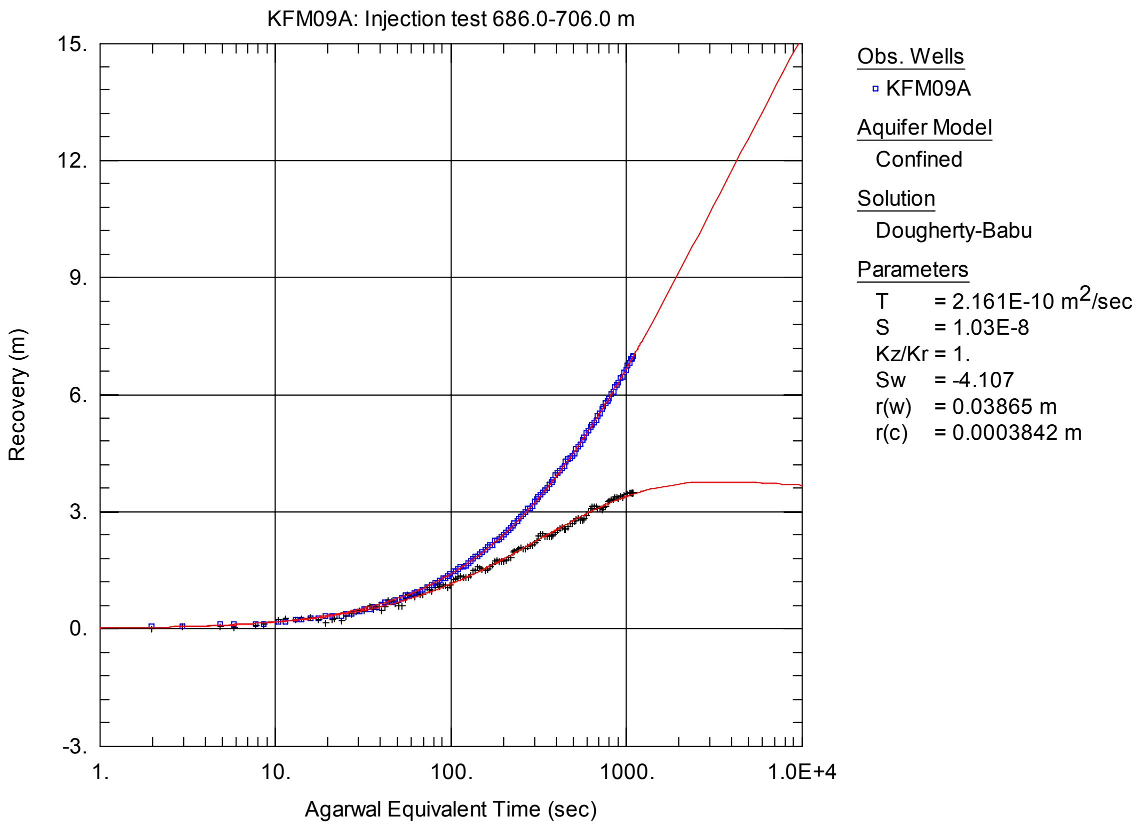


Figure A3-185. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 686.0-706.0 m in KFM09A.*

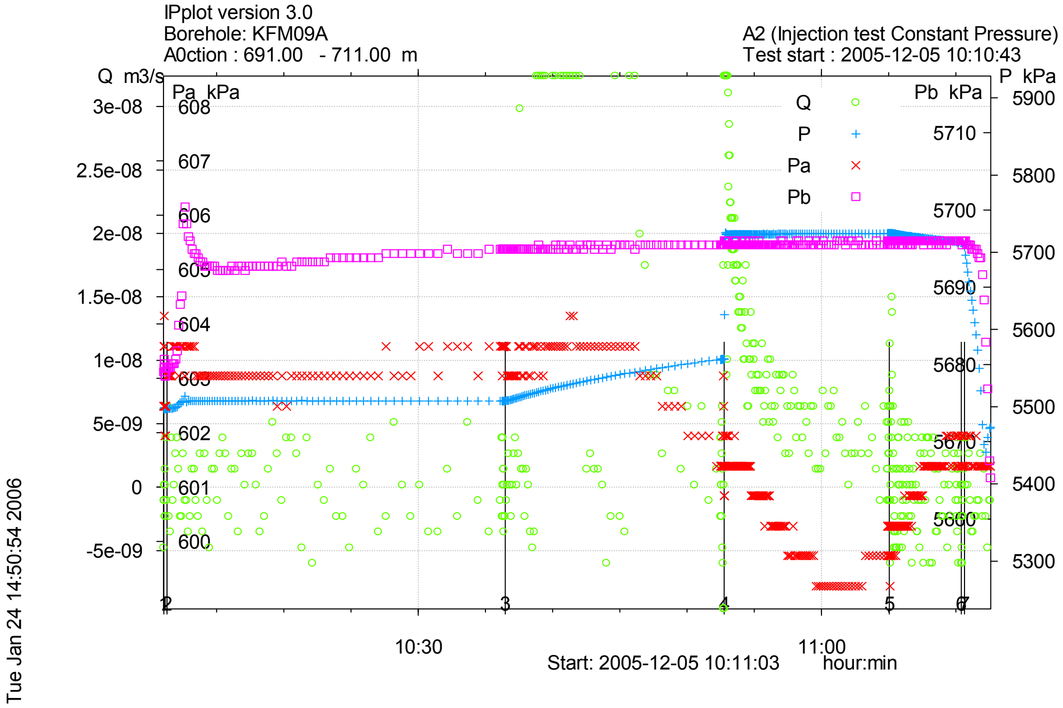


Figure A3-186. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 691.0-711.0 m in borehole KFM09A.

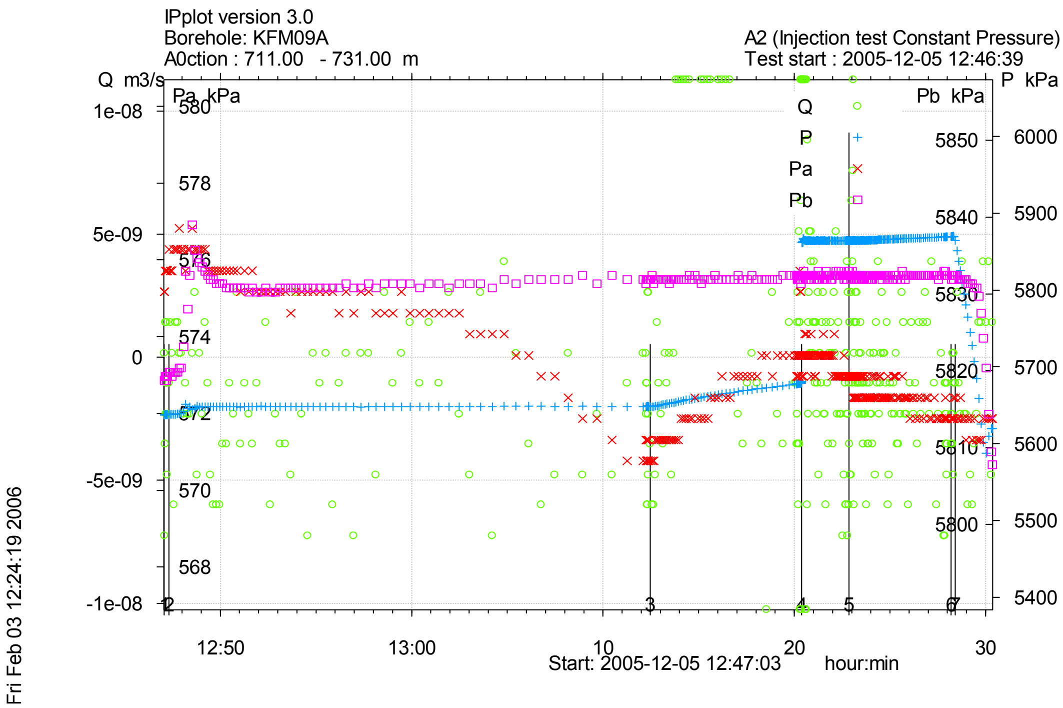


Figure A3-187. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 711.0-731.0 m in borehole KFM09A.

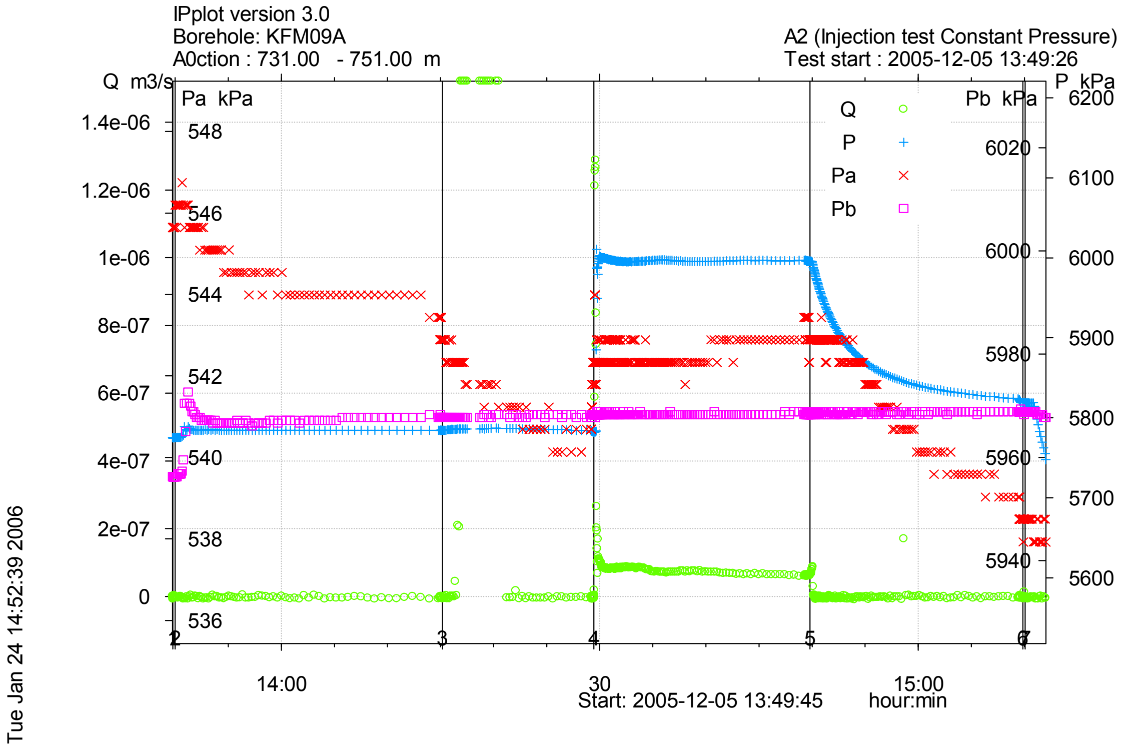


Figure A3-188. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 731.0-751.0 m in borehole KFM09A.*

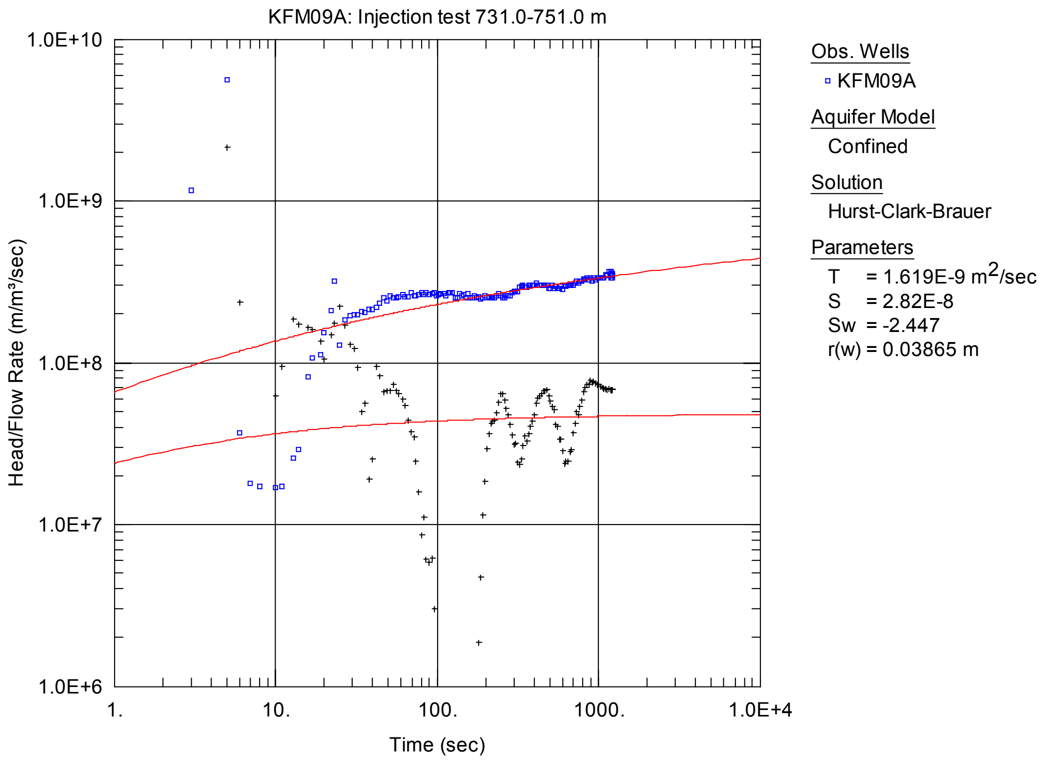


Figure A3-189. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 731.0-751.0 m in KFM09A.*

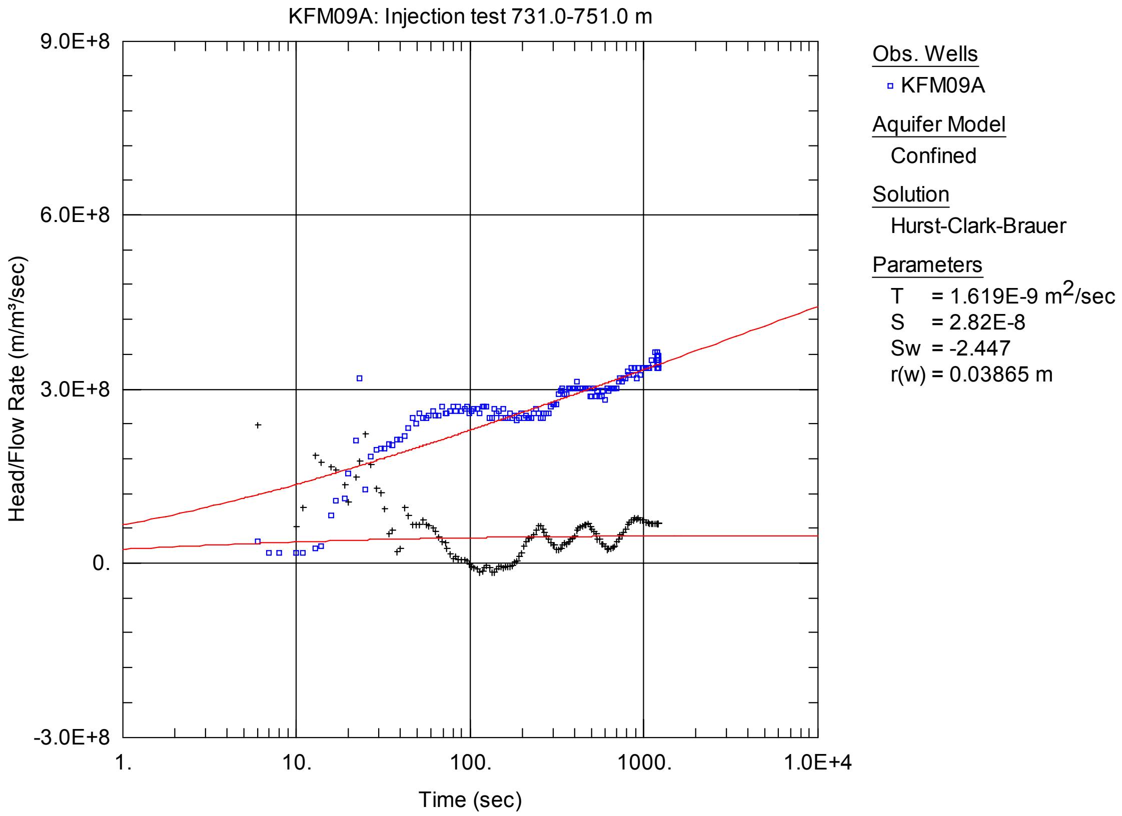


Figure A3-190. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 731.0-751.0 m in KFM09A.*

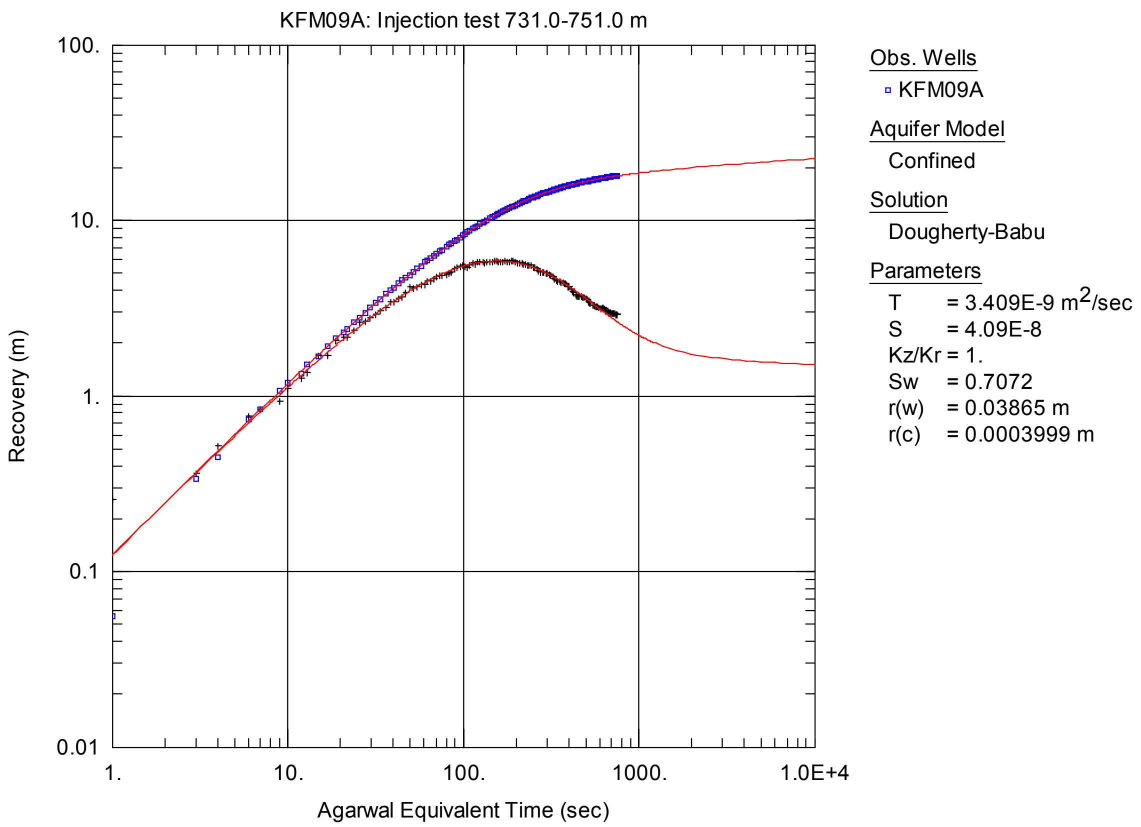


Figure A3-191. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in 731.0-751.0 m in KFM09A.*

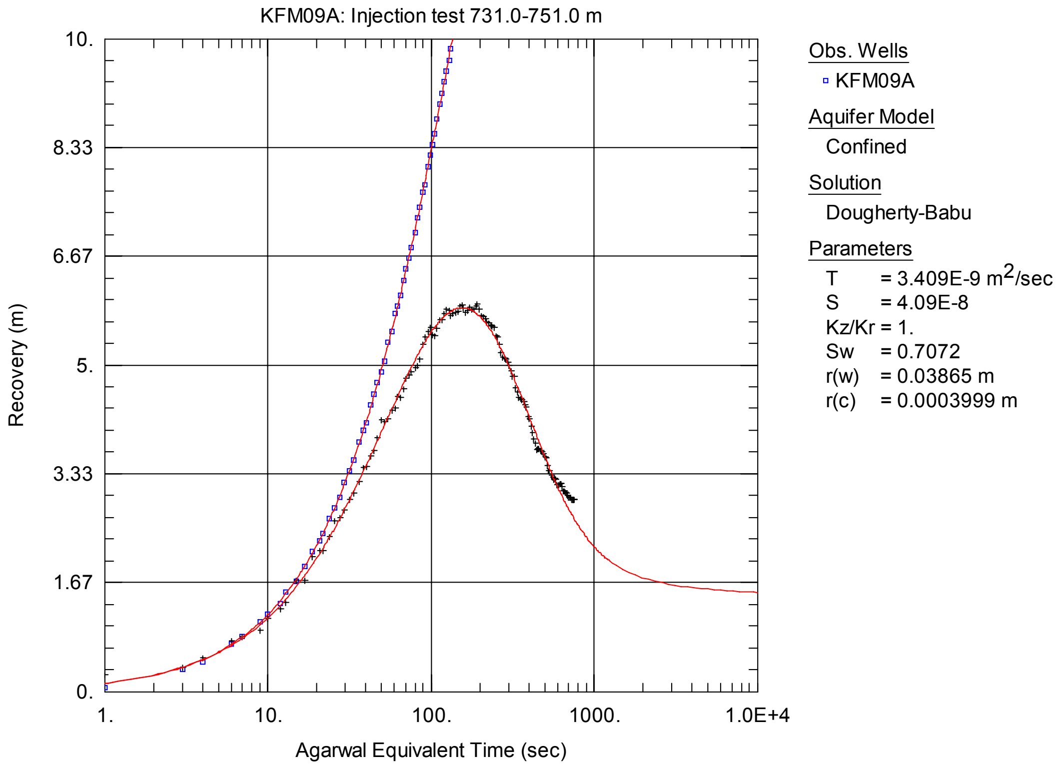


Figure A3-192. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 731.0-751.0 m in KFM09A.*

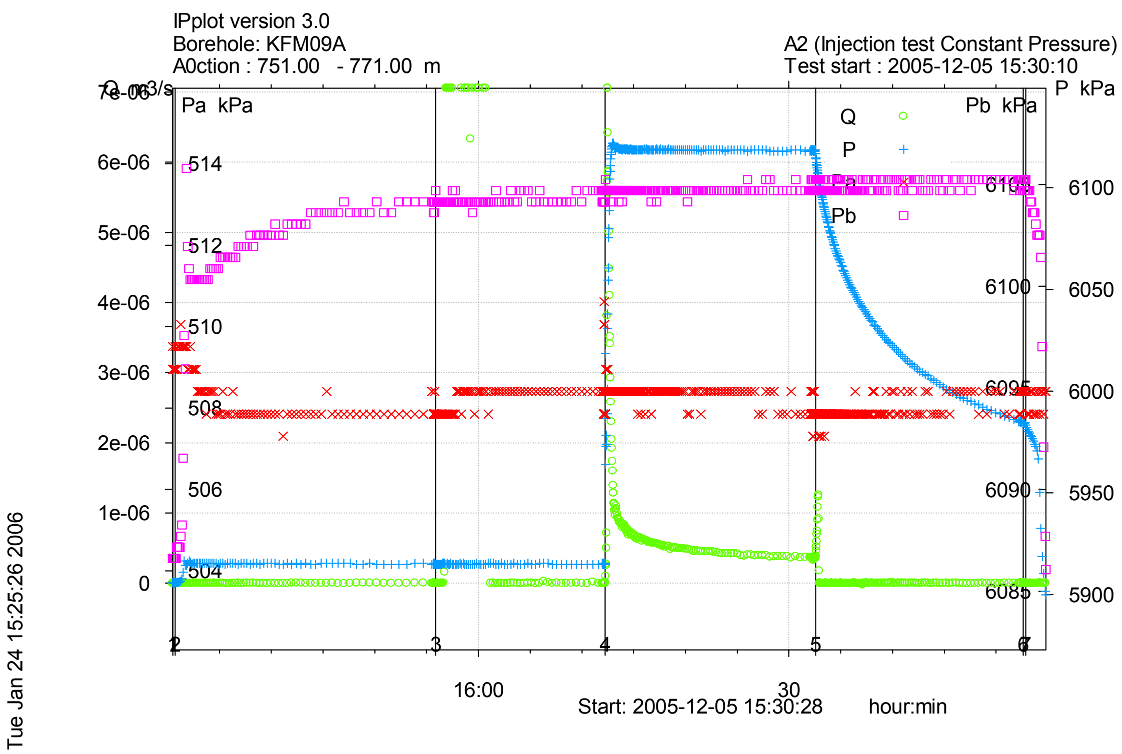


Figure A3-193. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 751.0-771.0 m in borehole KFM09A.*

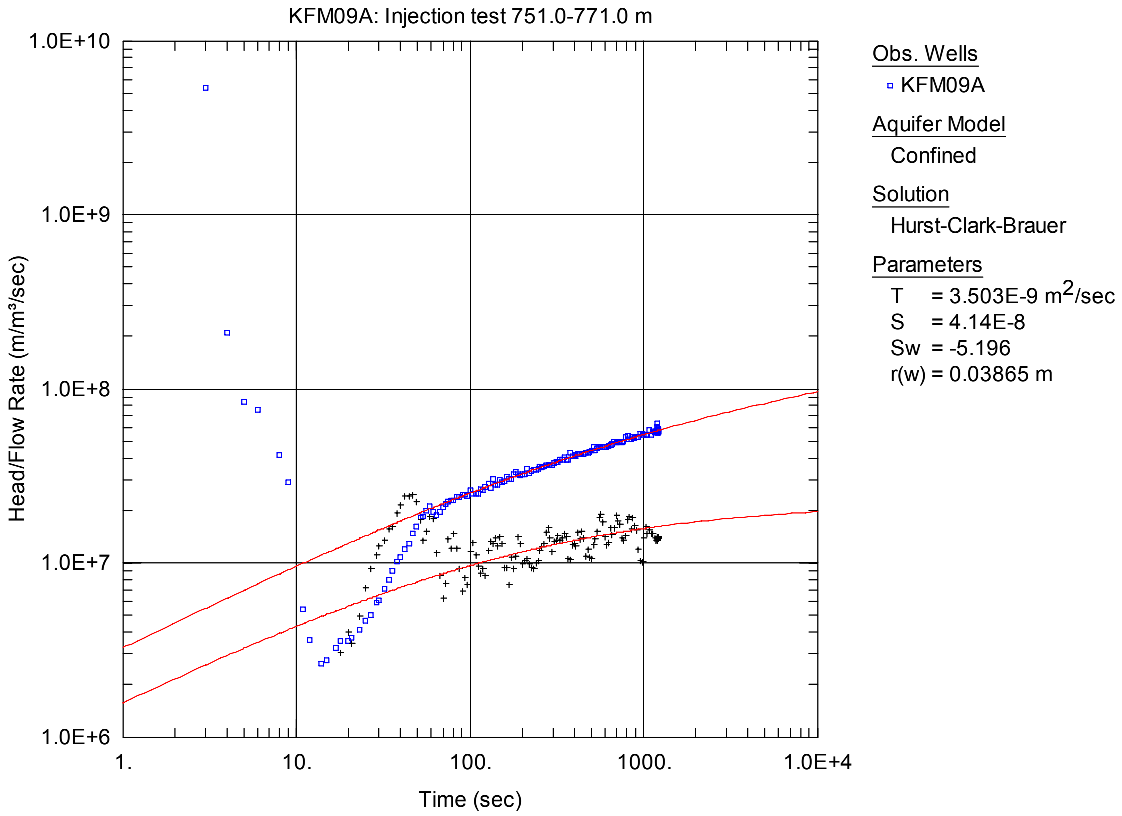


Figure A3-194. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 751.0-771.0 m in KFM09A.*

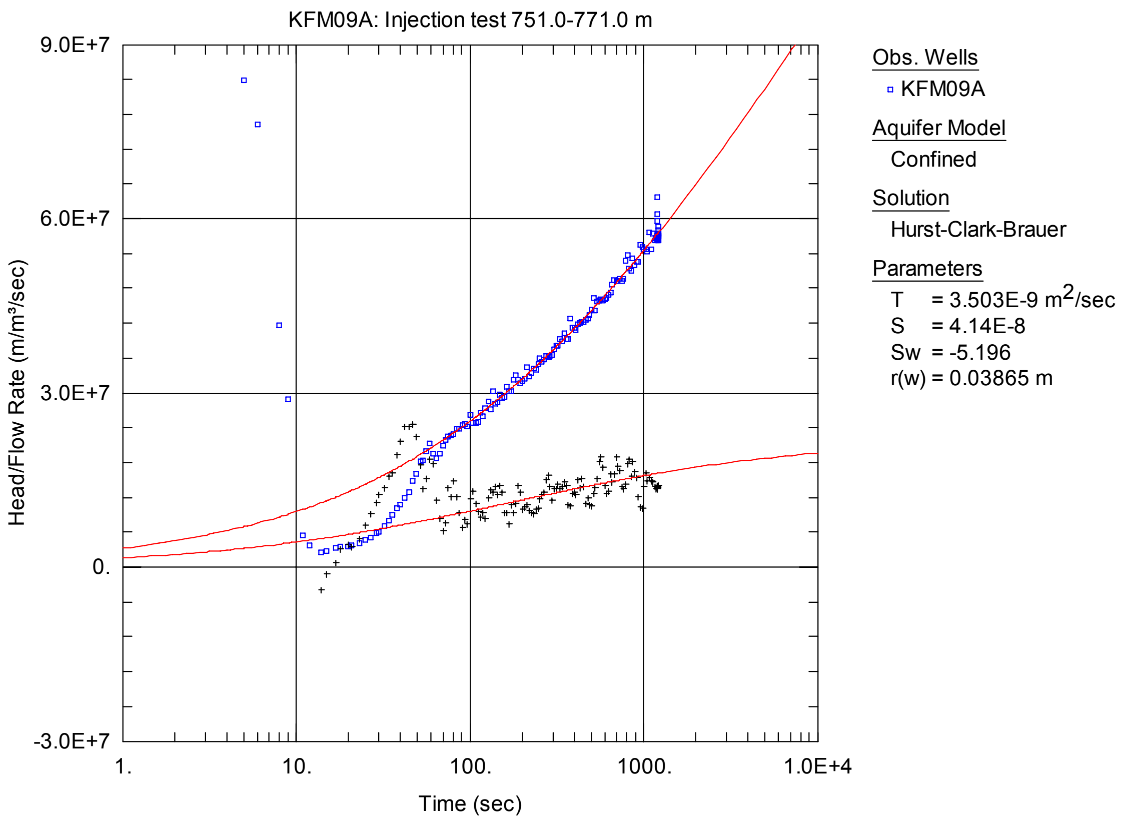


Figure A3-195. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in 751.0-771.0 m in KFM09A.*

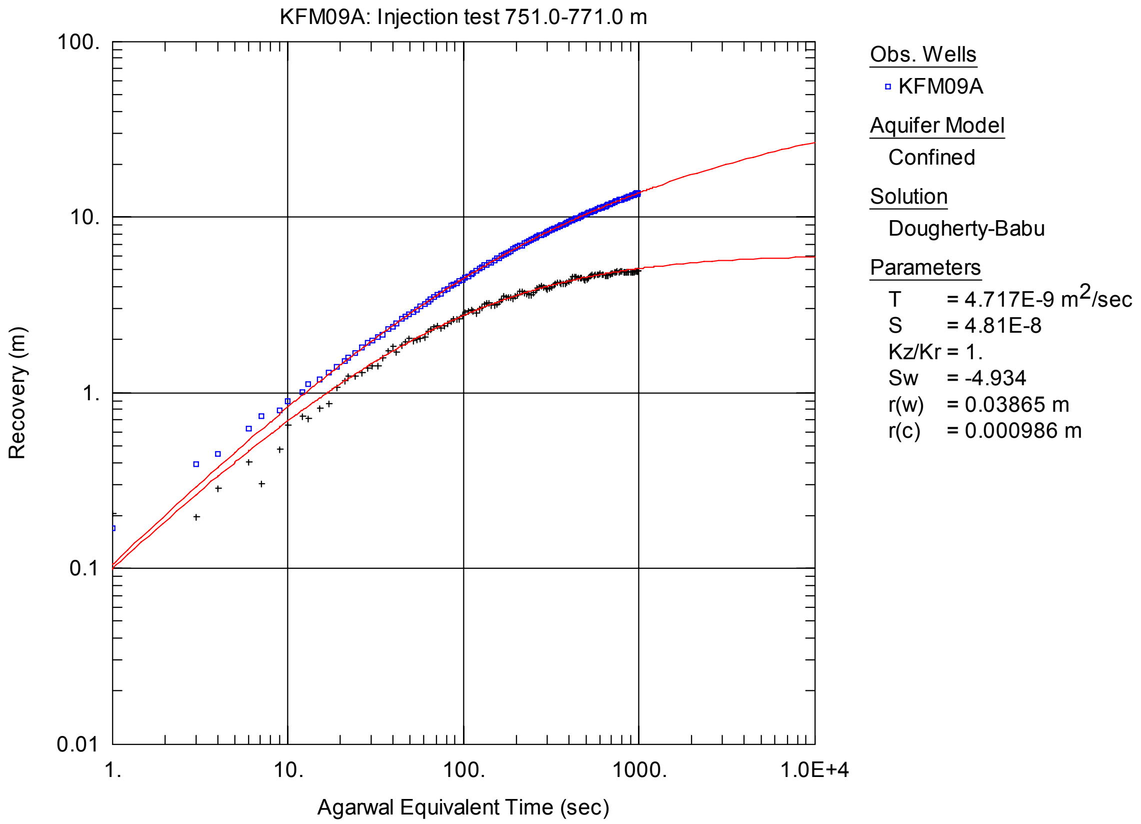


Figure A3-196. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 751.0-771.0 m in KFM09A.*

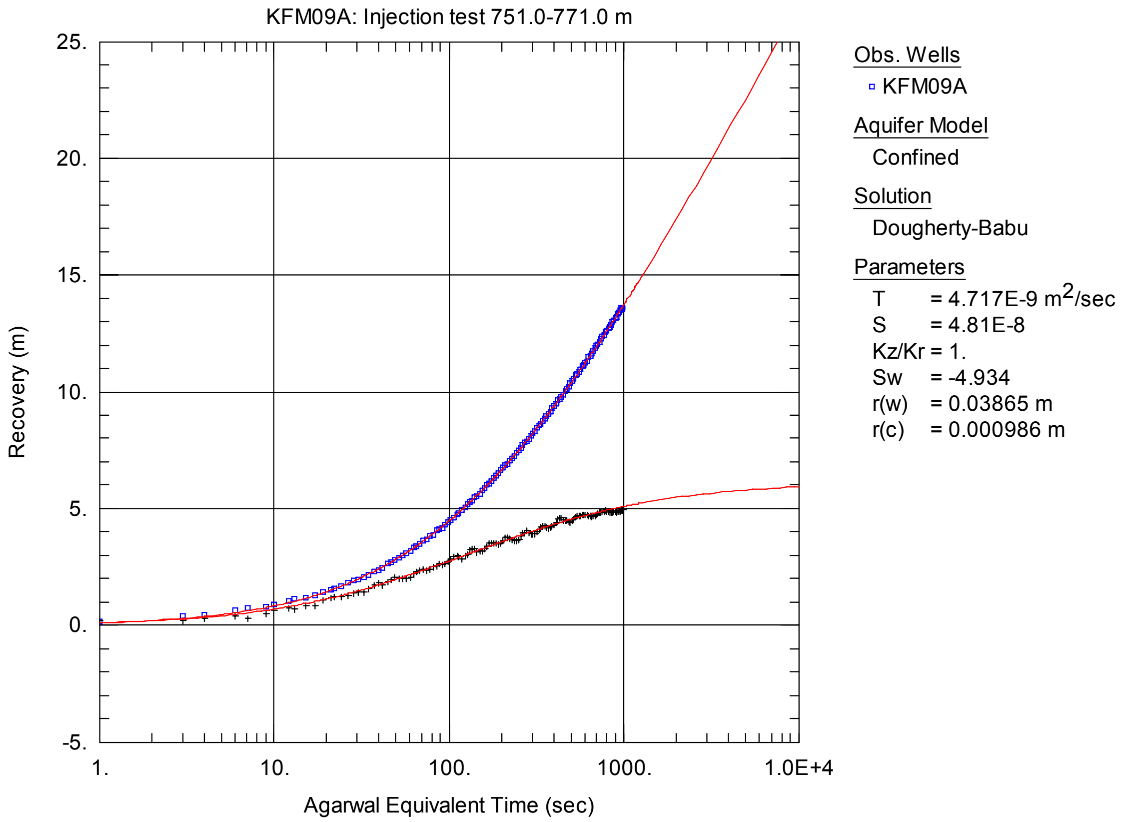


Figure A3-197. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 751.0-771.0 m in KFM09A.*

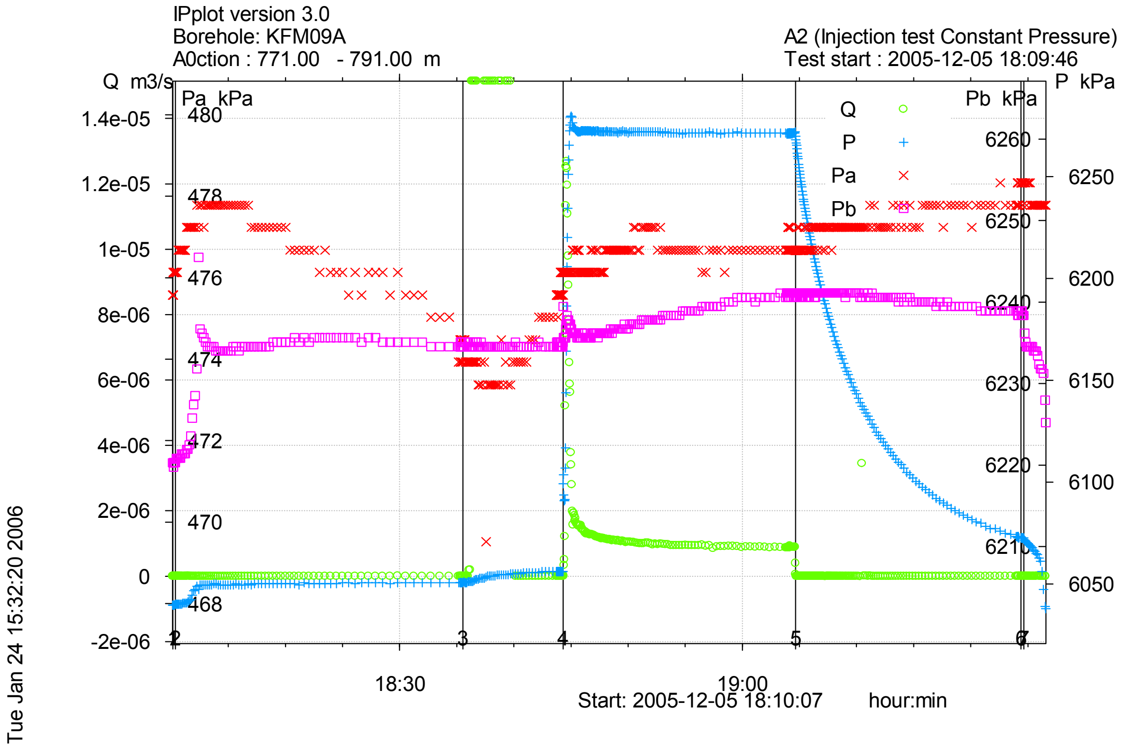


Figure A3-198. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 771.0-791.0 m in borehole KFM09A.*

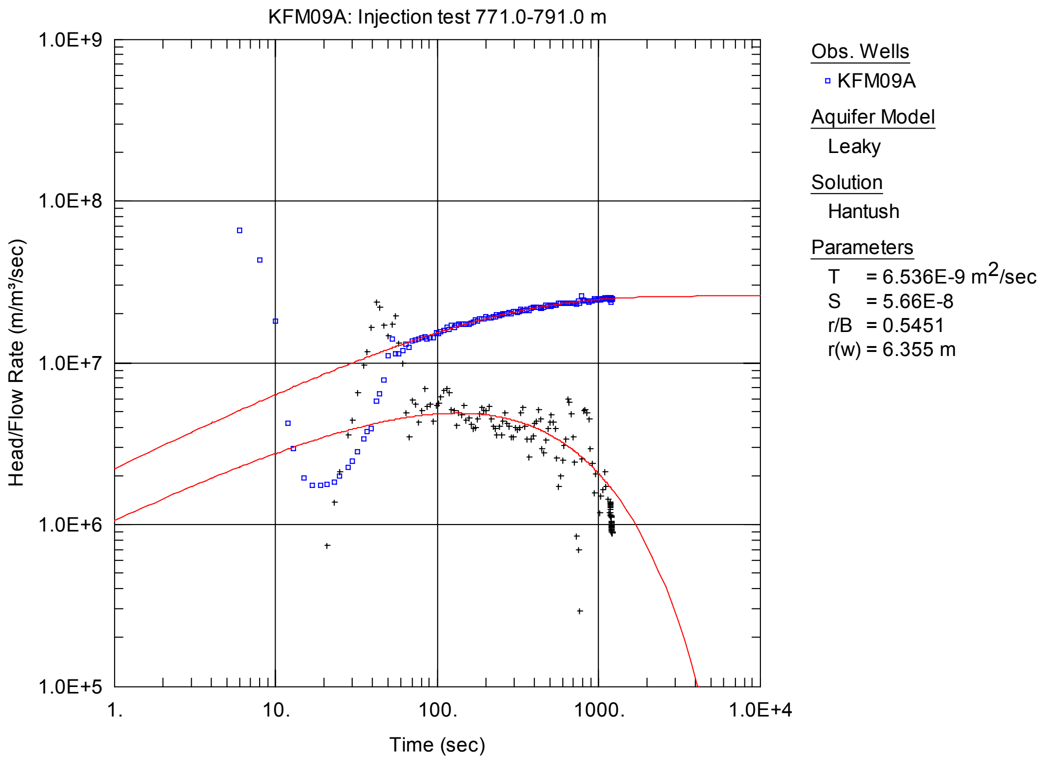


Figure A3-199. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 771.0-791.0 m in KFM09A.*

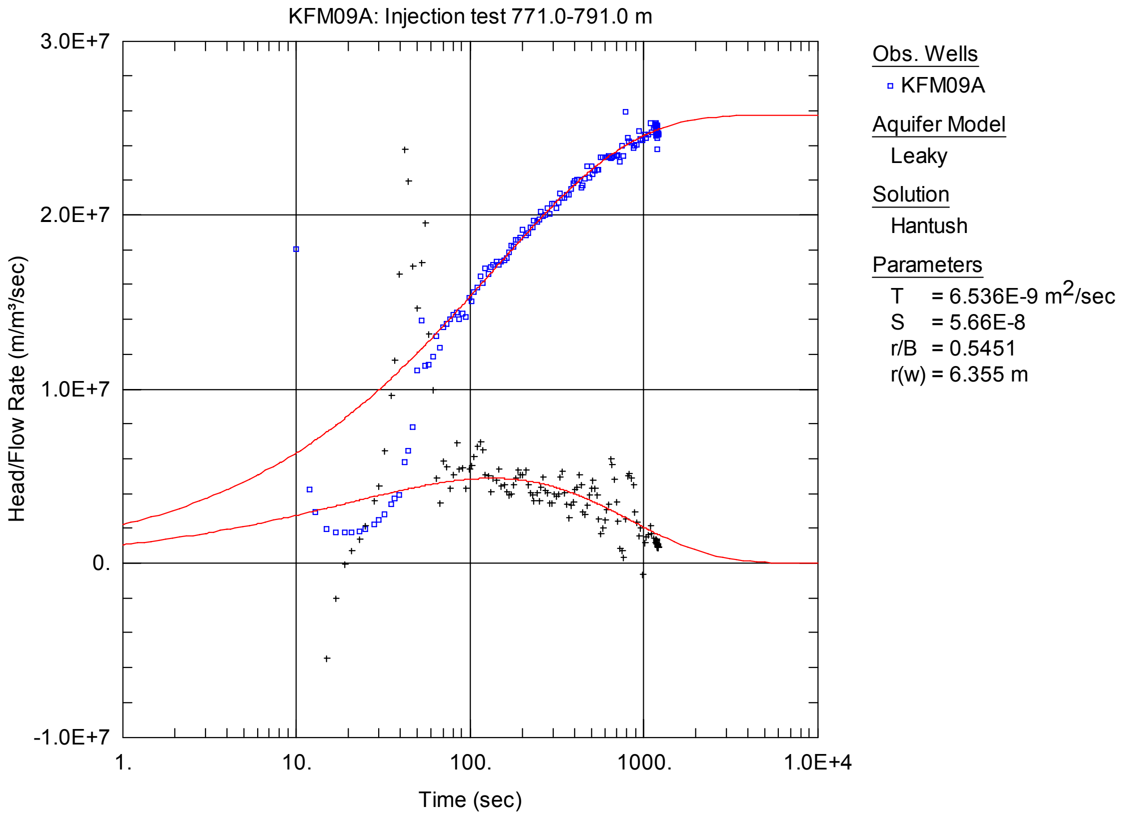


Figure A3-200. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 771.0-791.0 m in KFM09A.*

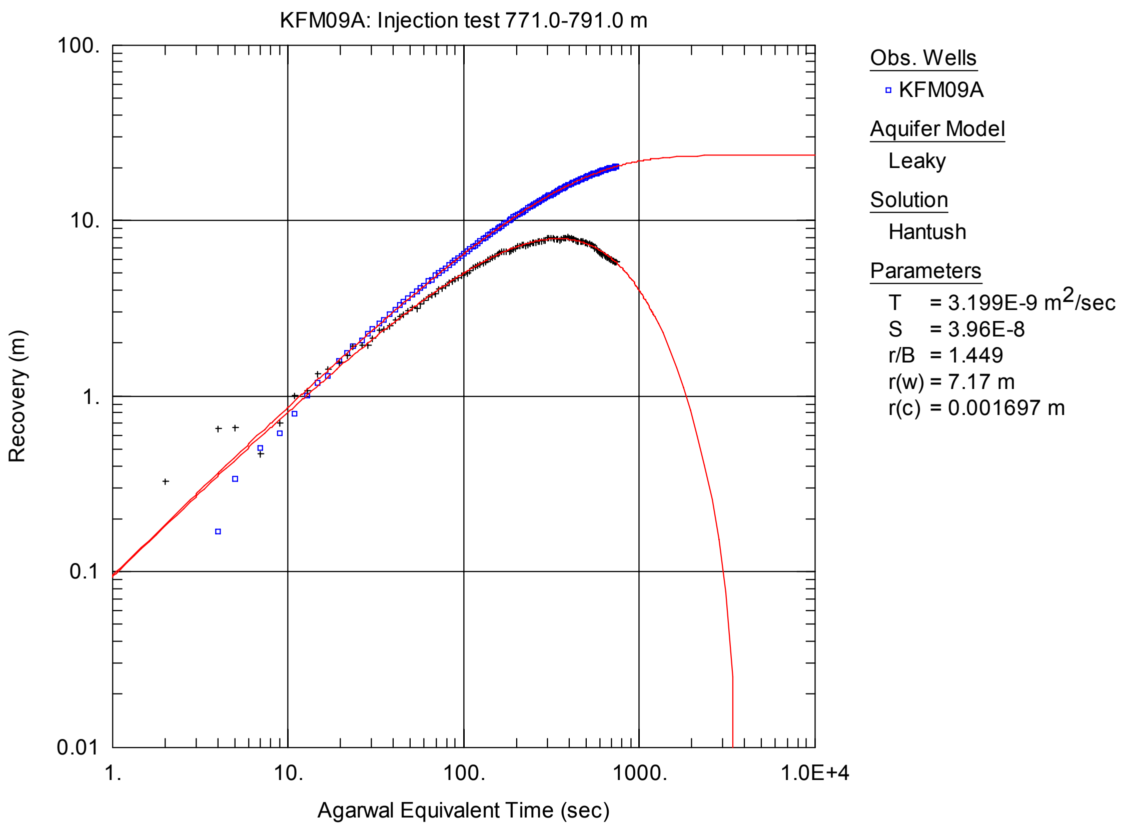


Figure A3-201. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 771.0-791.0 m in KFM09A.*

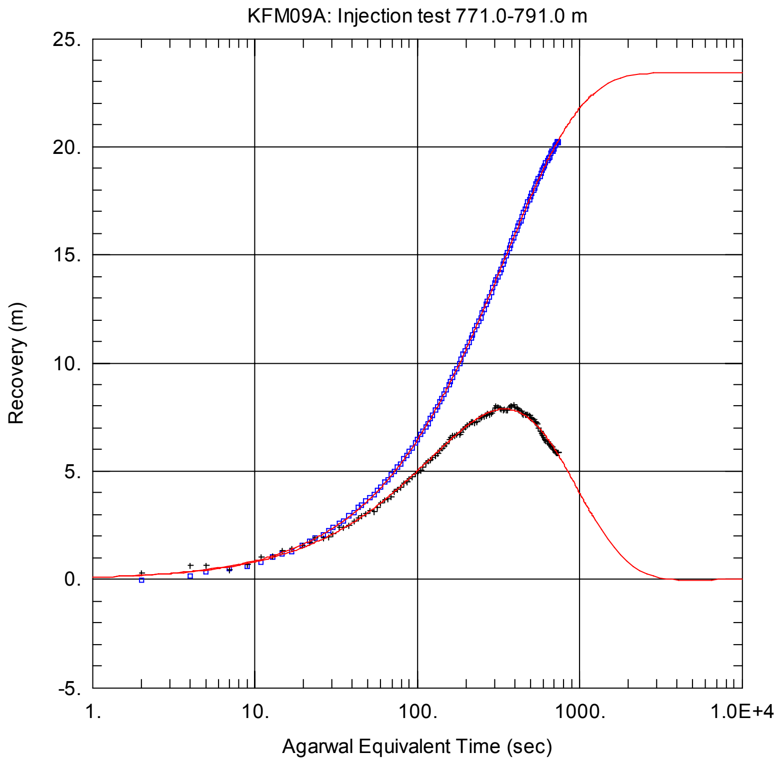


***Figure A3-202.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 771.0-791.0 m in KFM09A.*

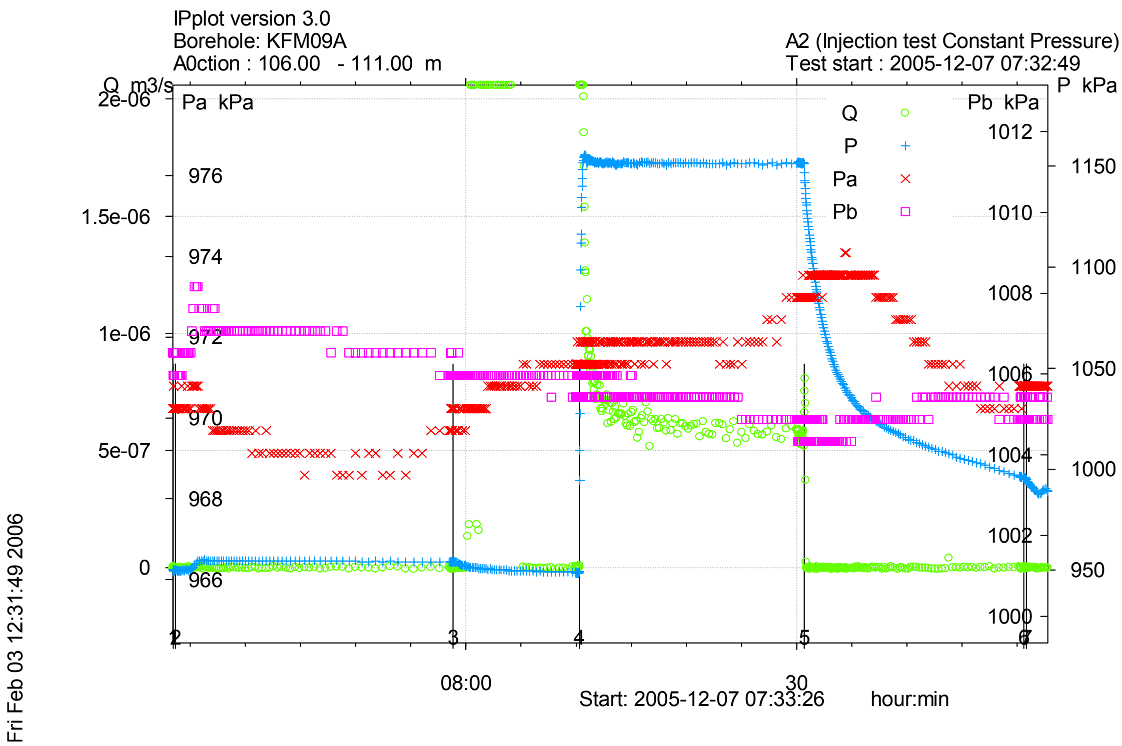


***Figure A3-203.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 106.0-111.0 m in borehole KFM09A.*

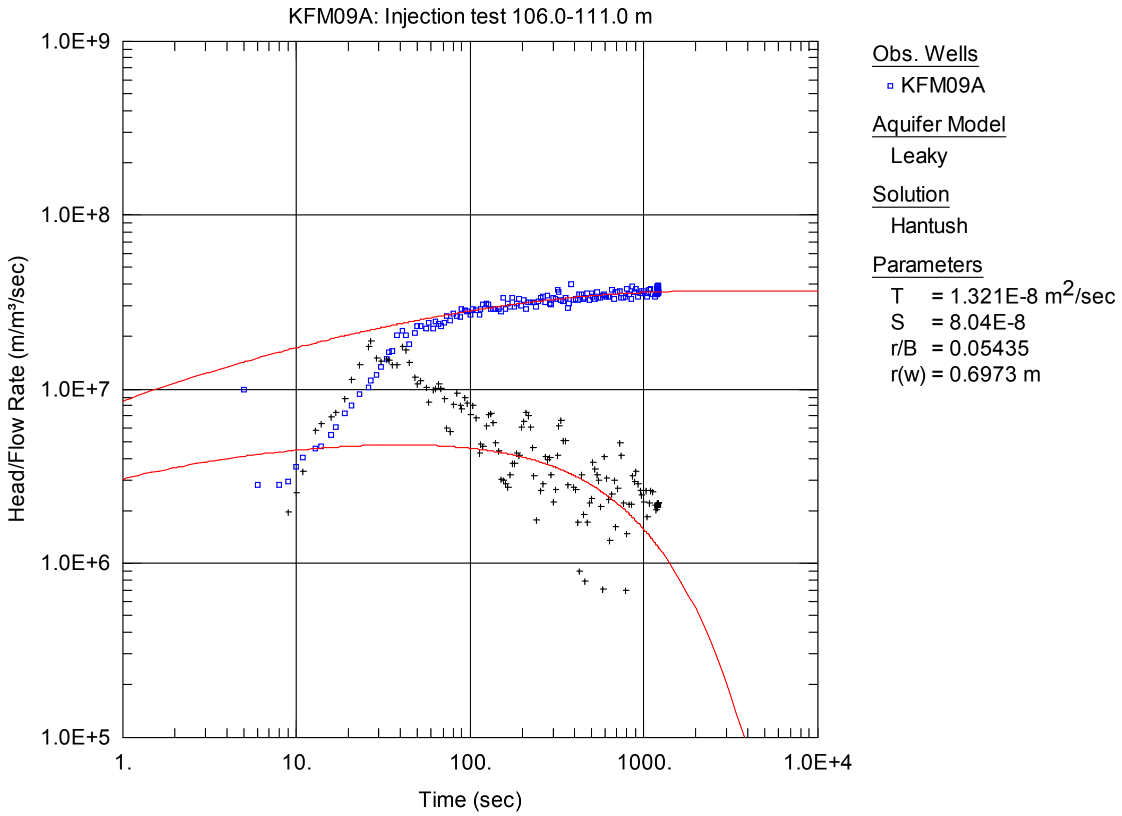


Figure A3-204. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 106.0-111.0 m in KFM09A.*

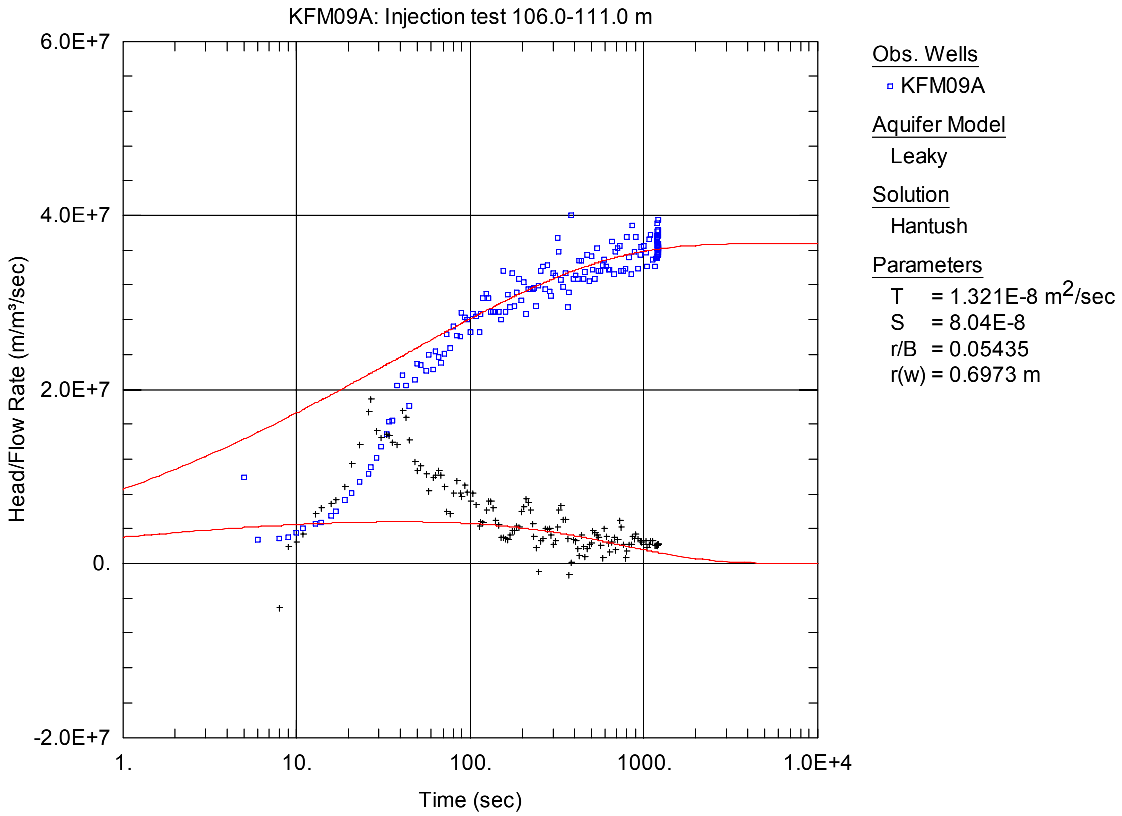


Figure A3-205. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 106.0-111.0 m in KFM09A.*

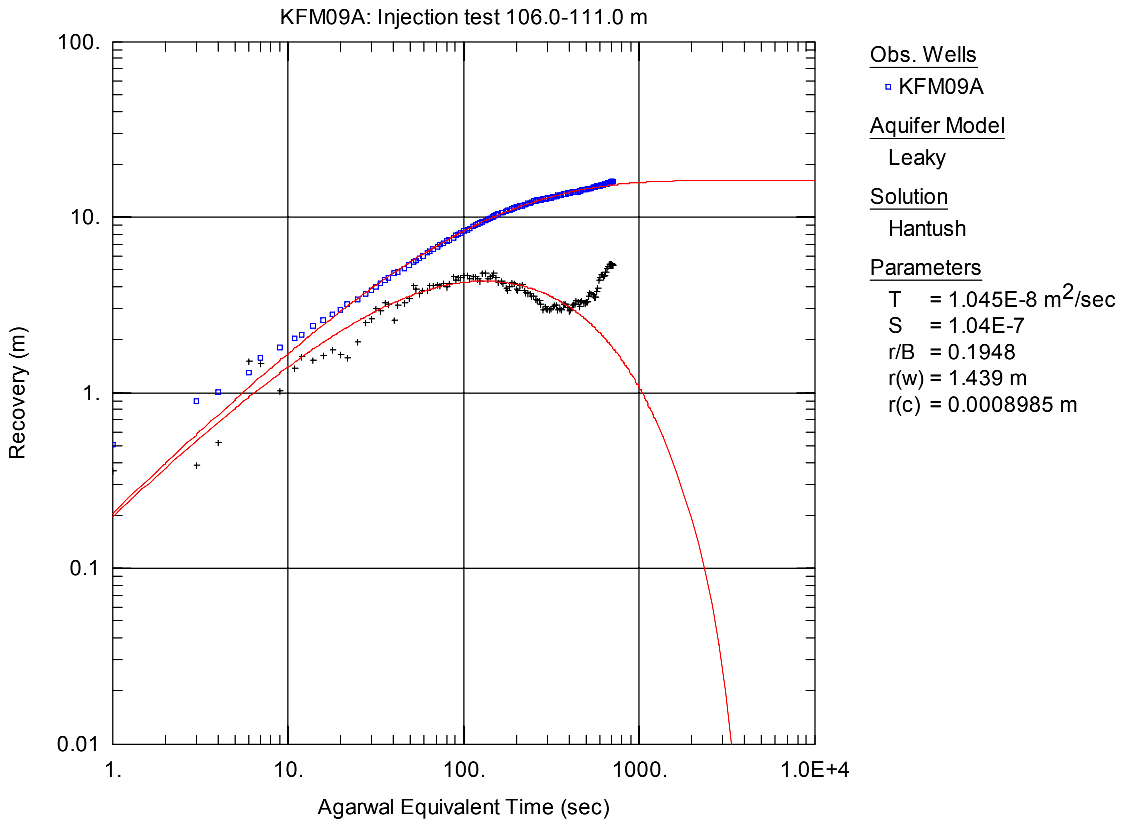


Figure A3-206. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 106.0-111.0 m in KFM09A.*

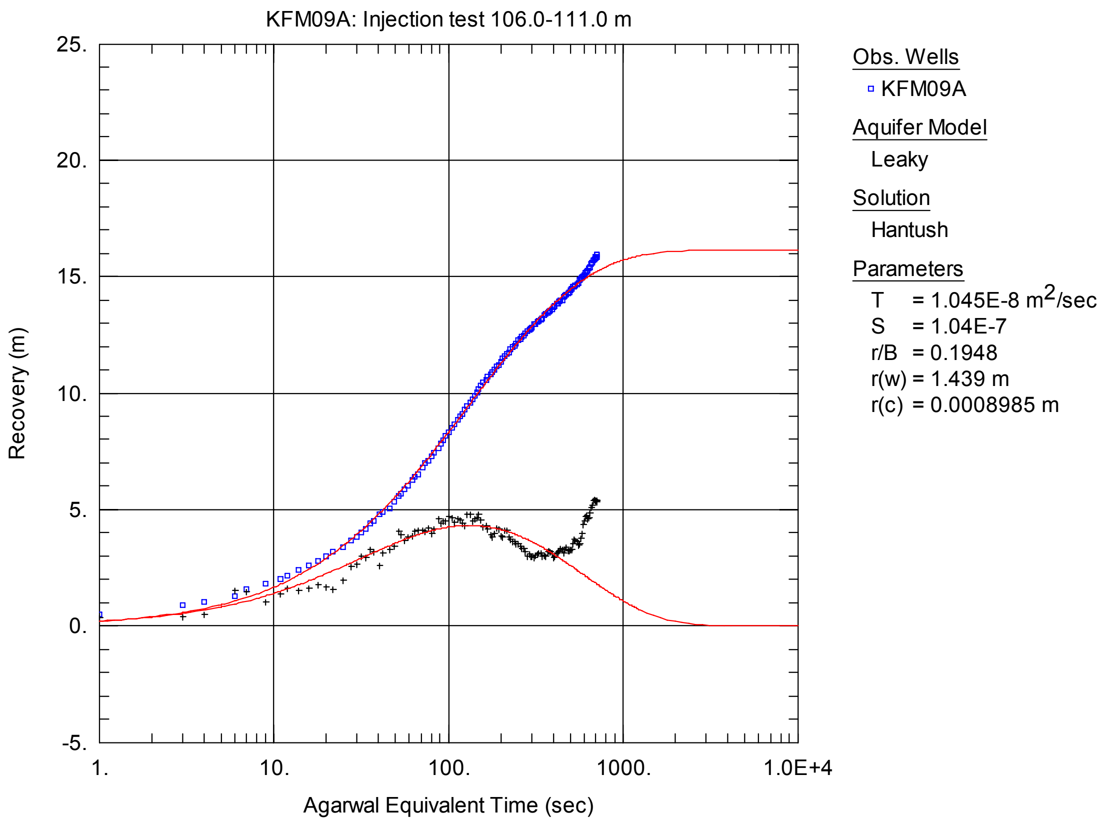


Figure A3-207. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 106.0-111.0 m in KFM09A.*

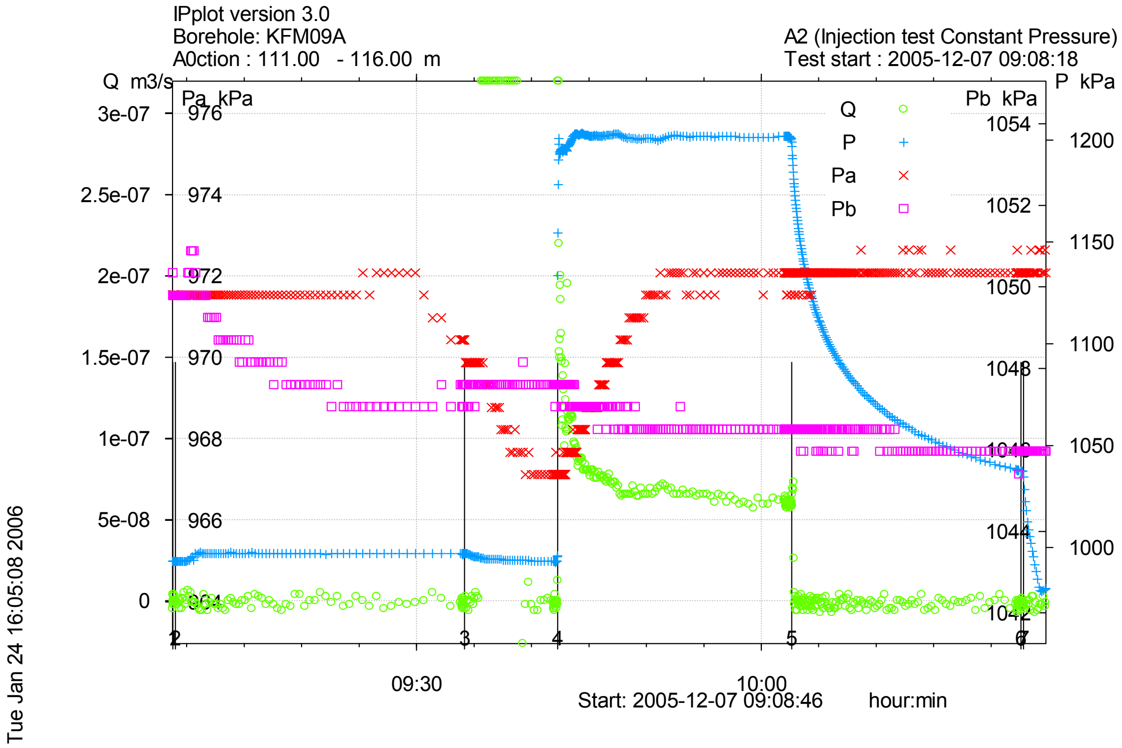


Figure A3-208. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 111.0-116.0 m in borehole KFM09A.*

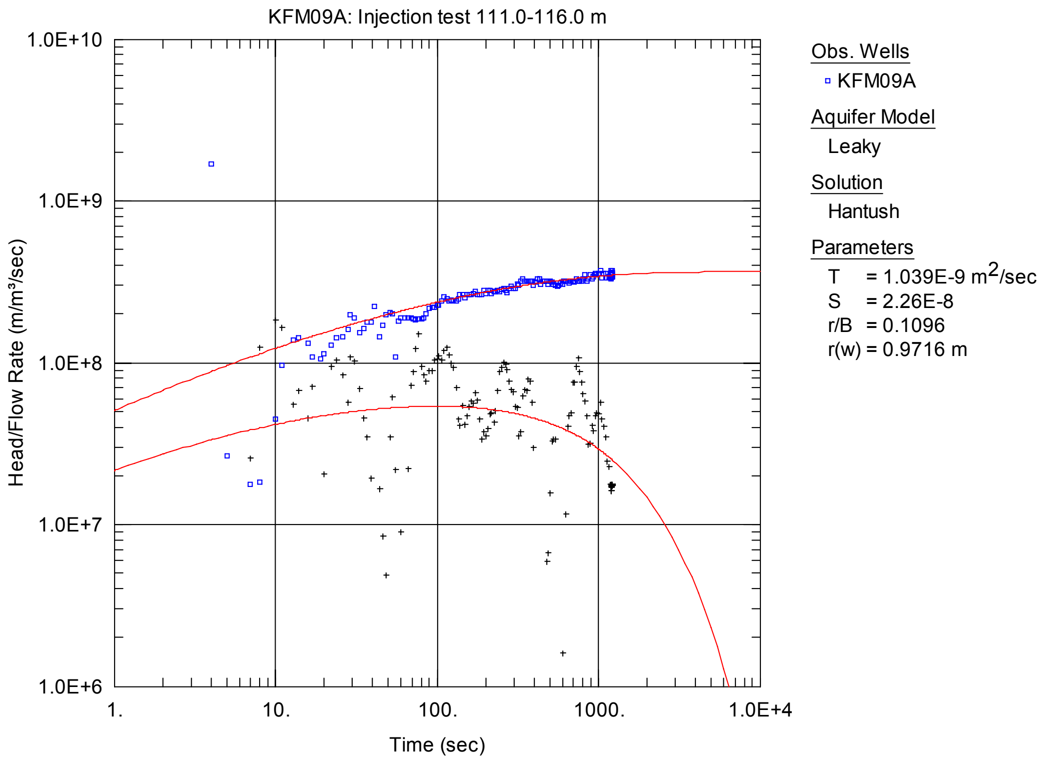


Figure A3-209. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 111.0-116.0 m in KFM09A.*

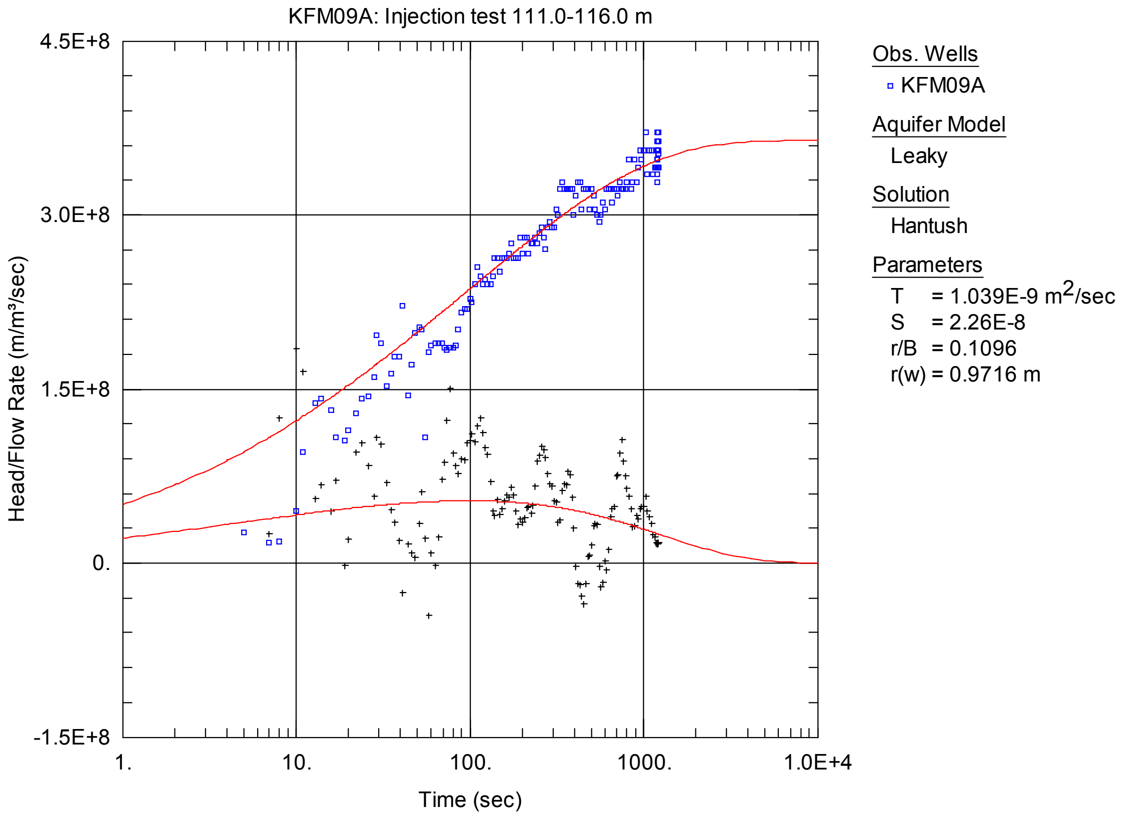


Figure A3-210. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 111.0-116.0 m in KFM09A.*

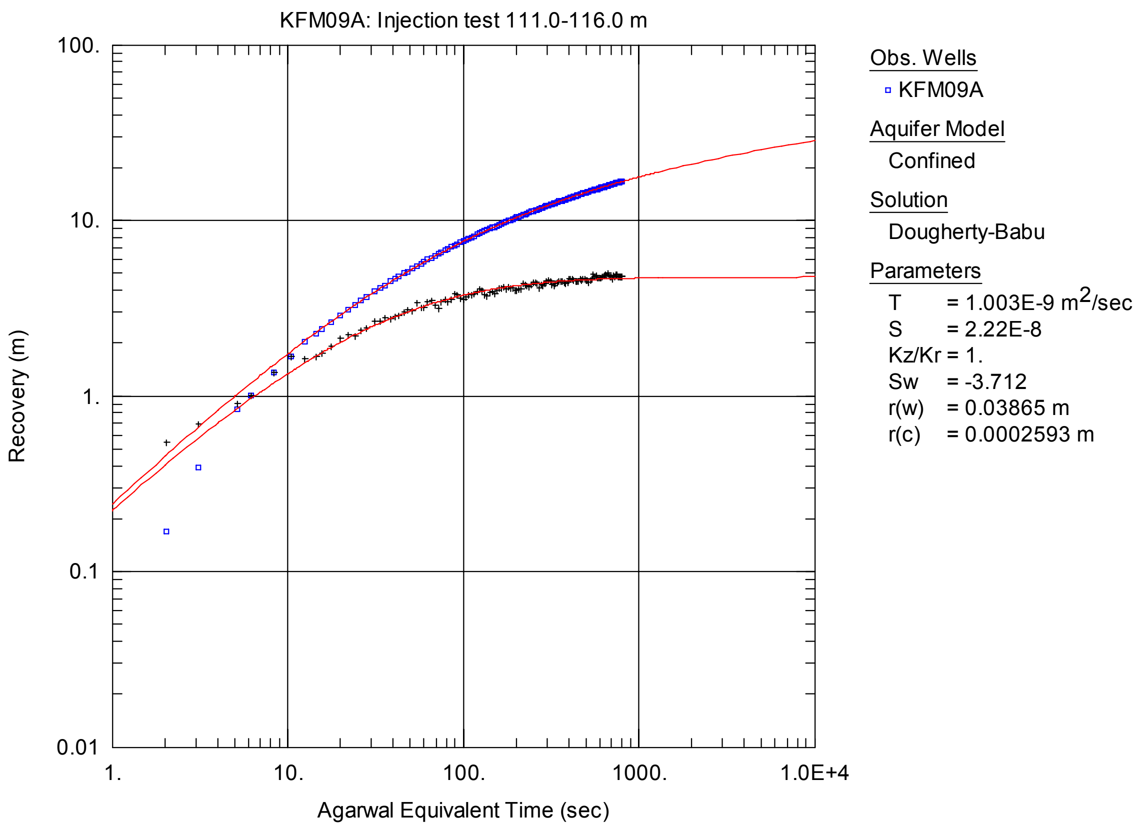


Figure A3-211. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 111.0-116.0 m in KFM09A.*

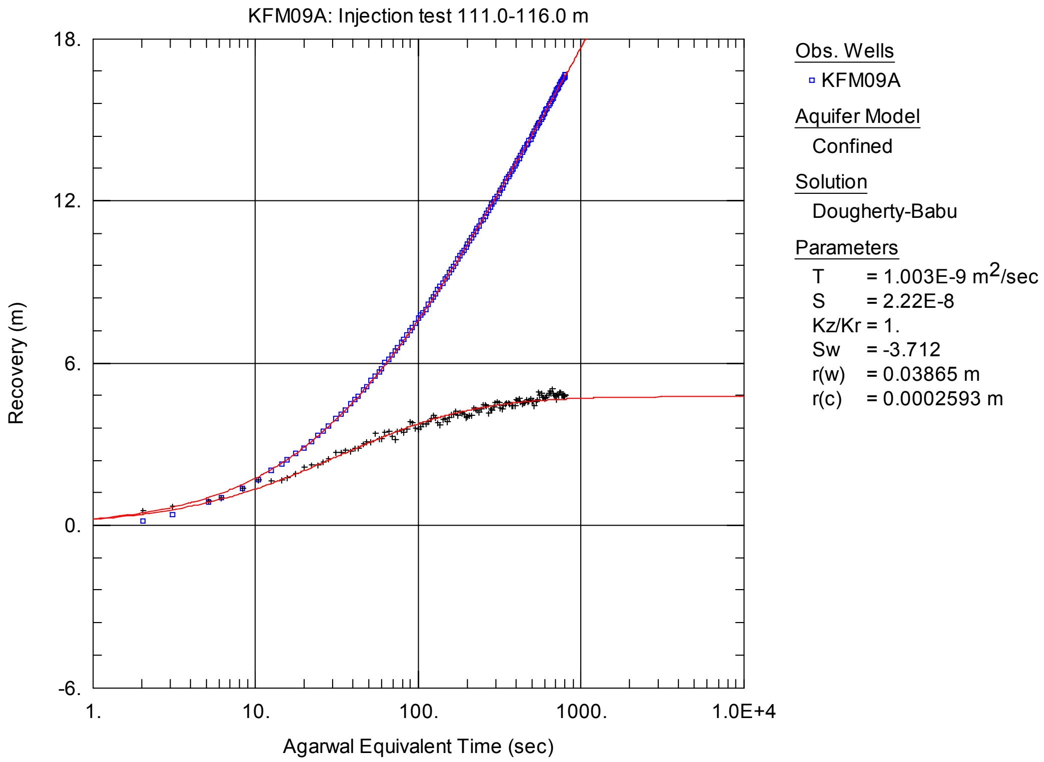


***Figure A3-212.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 111.0-116.0 m in KFM09A.*

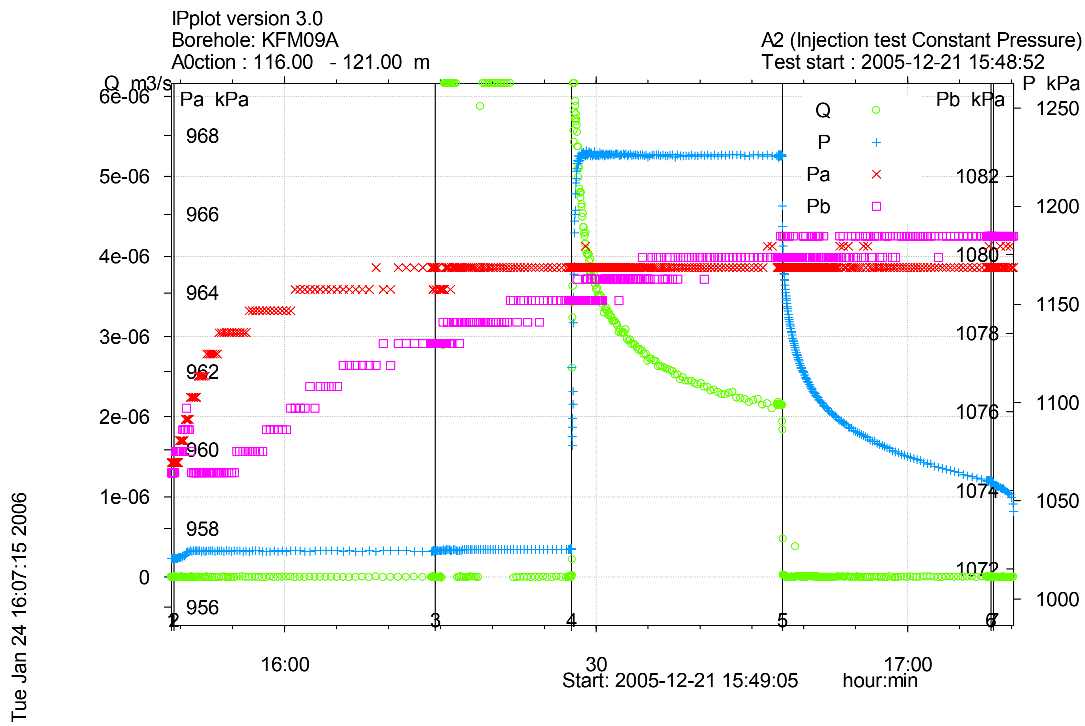


***Figure A3-213.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 116.0-121.0 m in borehole KFM09A.*

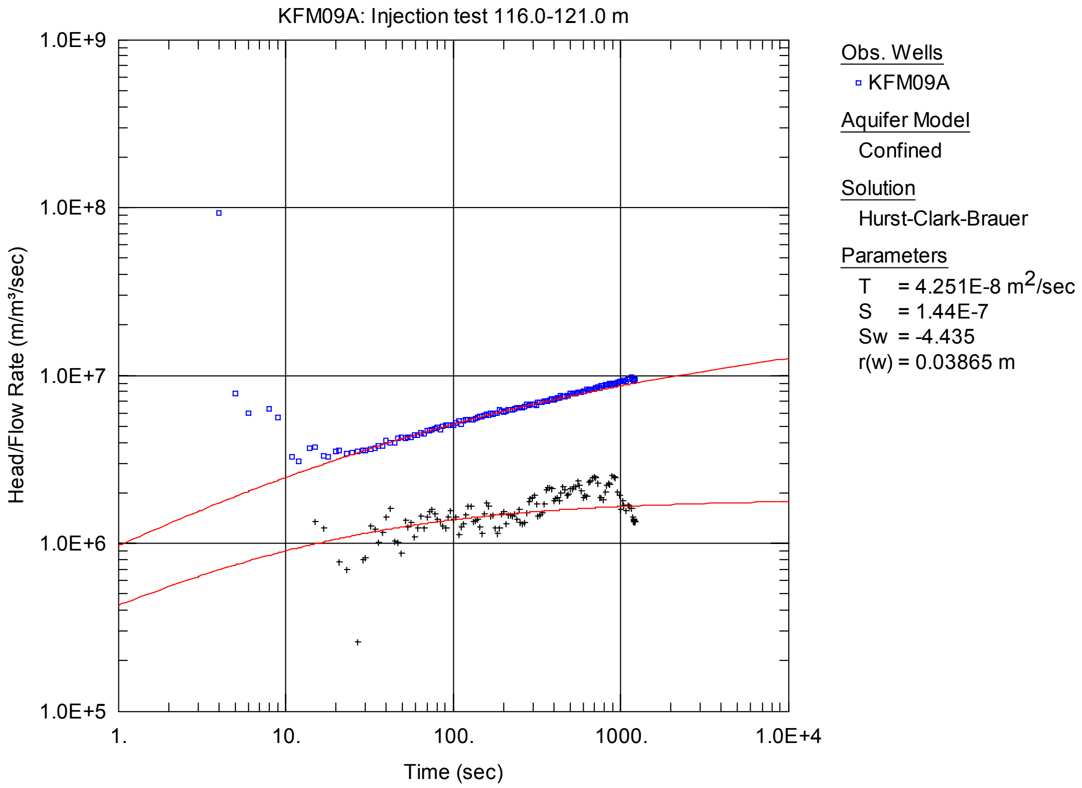


Figure A3-214. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 116.0-121.0 m in KFM09A. This plot shows the first of two different PRF:s during the injection period in this section.*

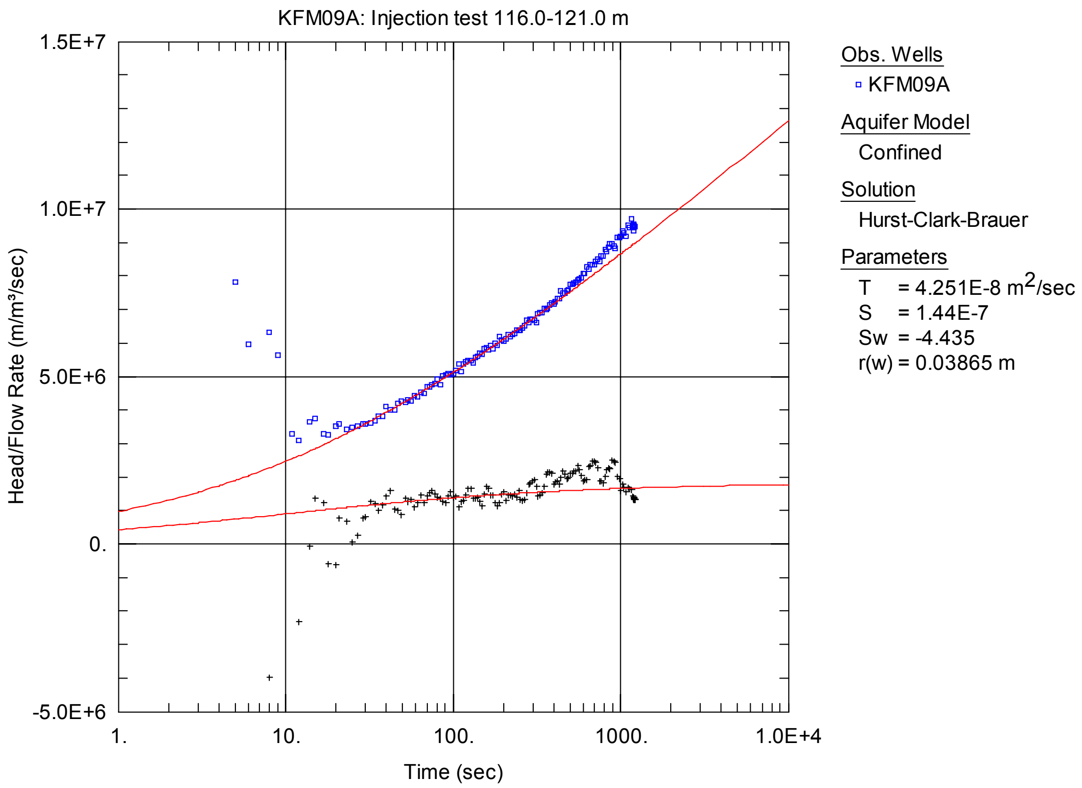


Figure A3-215. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 116.0-121.0 m in KFM09A. This plot shows the first of two different PRF:s during the injection period in this section.*

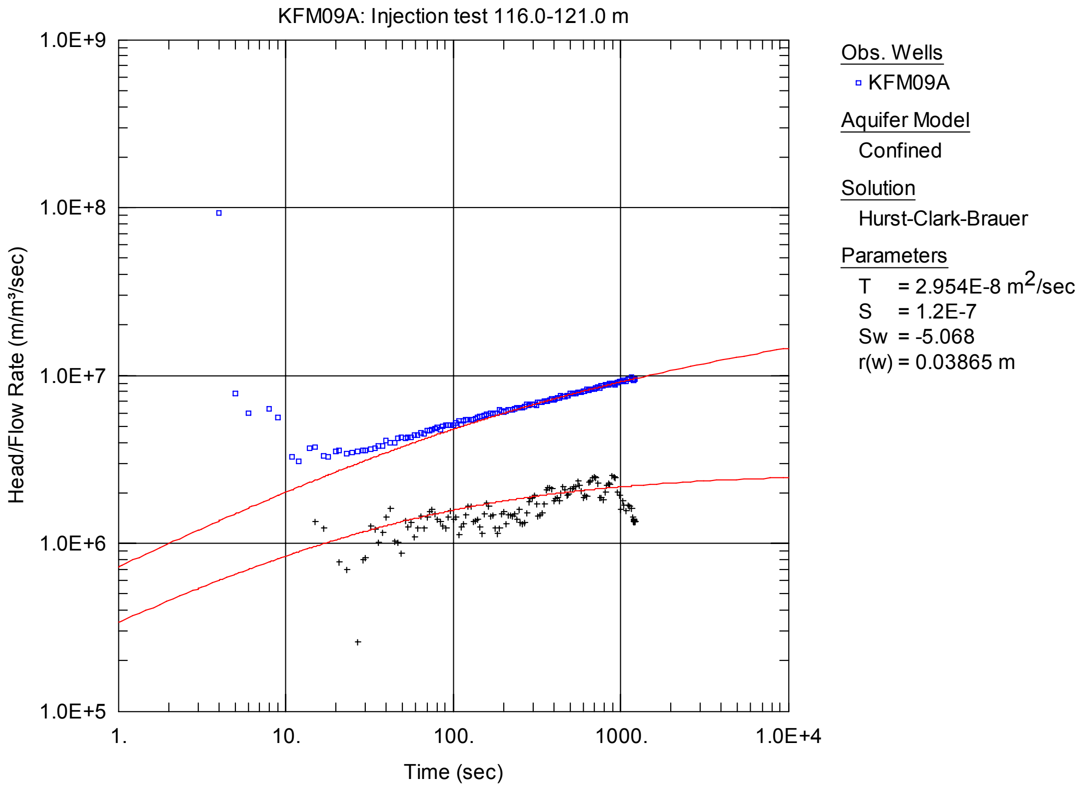


Figure A3-216. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 116.0-121.0 m in KFM09A. This plot shows a fit to the second of two different PRF:s during the injection period in this section.*

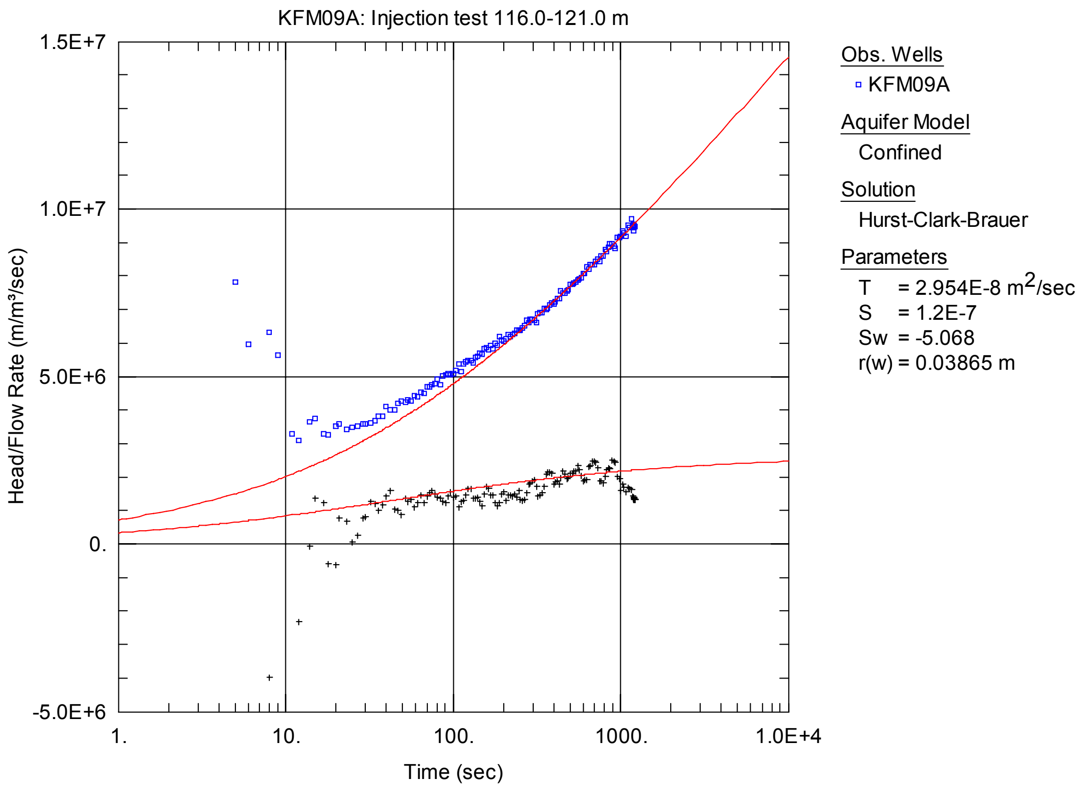


Figure A3-217. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 116.0-121.0 m in KFM09A. This plot shows a fit to the second of two different PRF:s during the injection period in this section.*

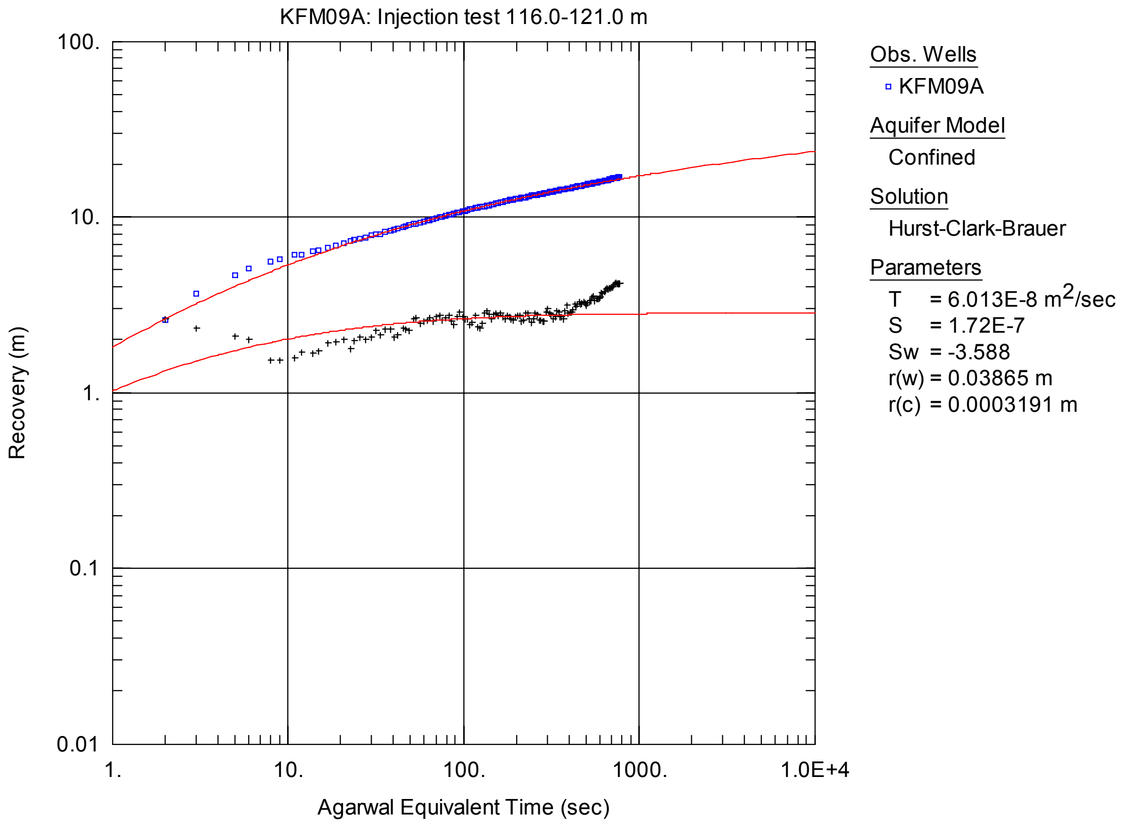


Figure A3-218. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 116.0-121.0 m in KFM09A.*

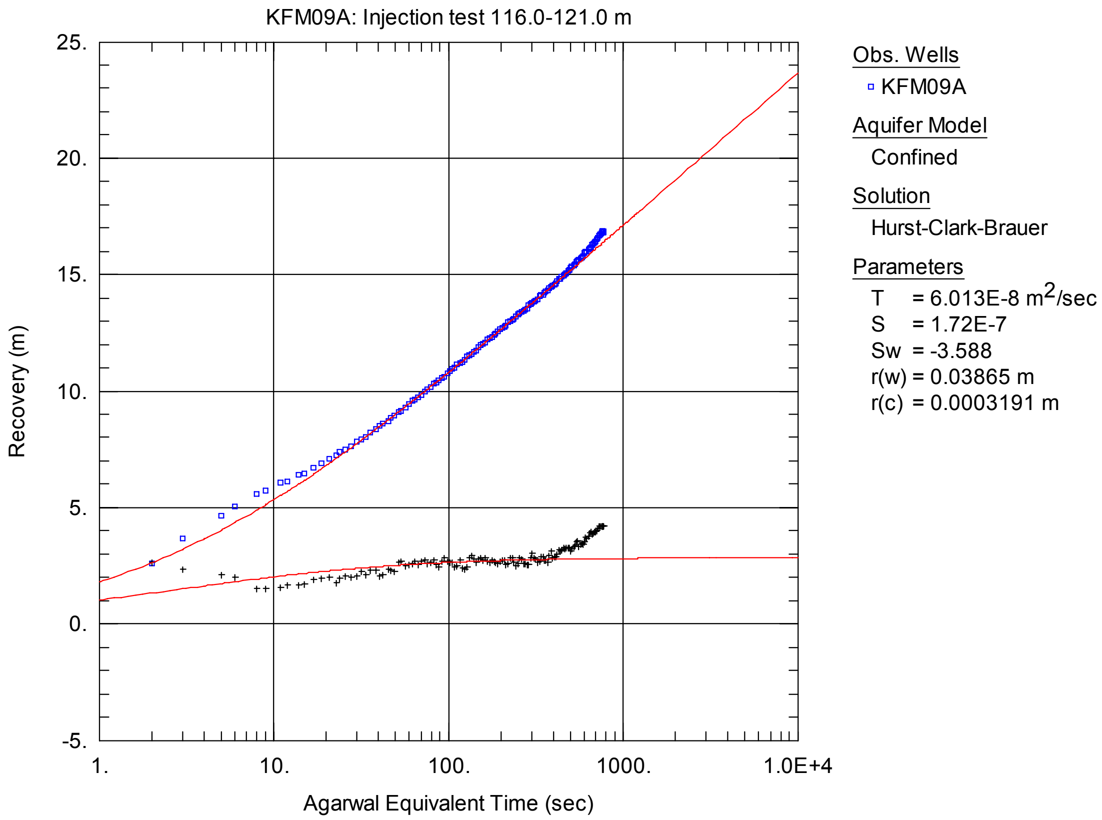


Figure A3-219. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 116.0-121.0 m in KFM09A.*

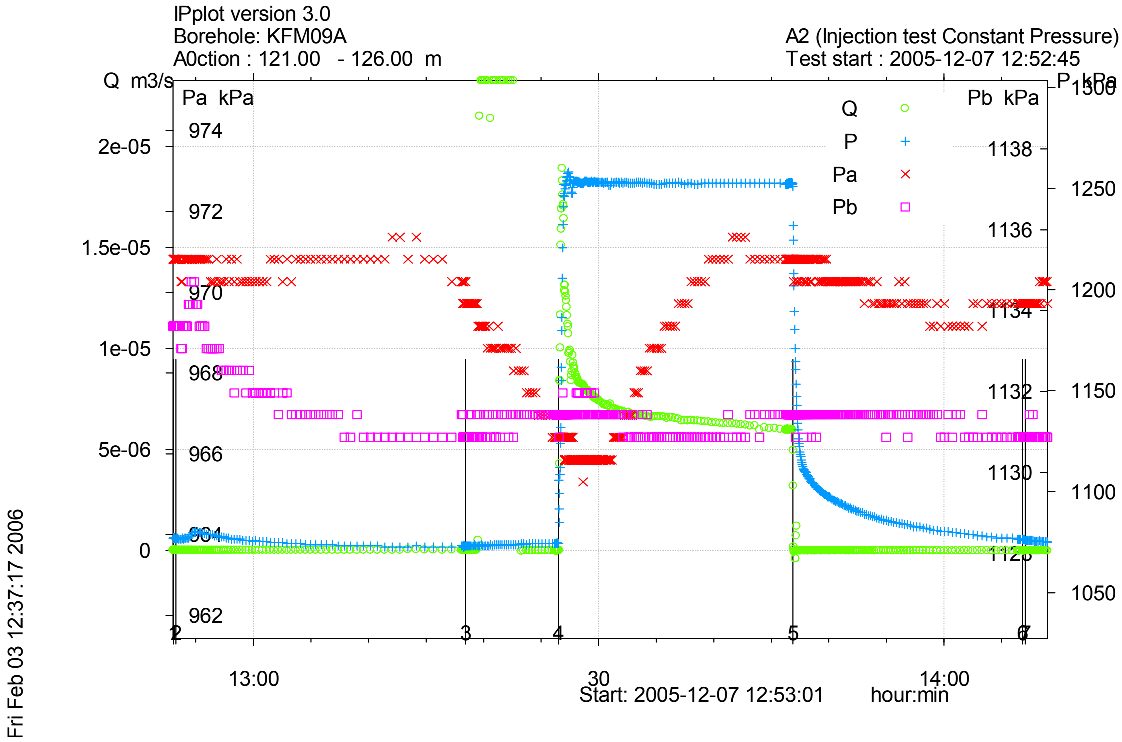


Figure A3-220. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 121.0-126.0 m in borehole KFM09A.*

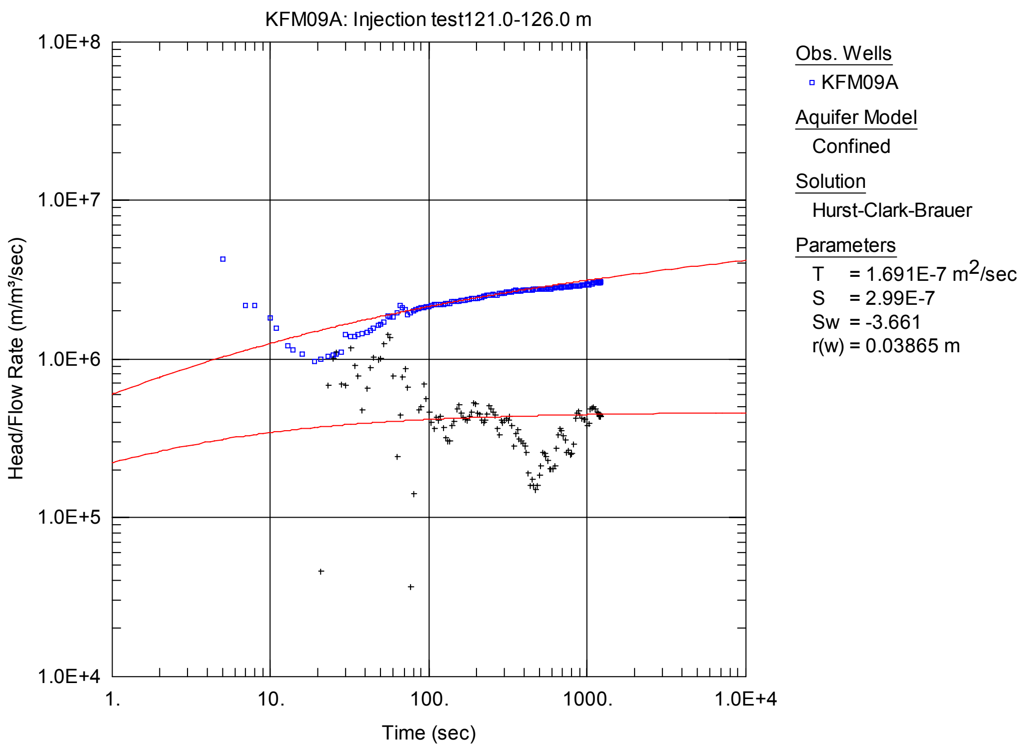


Figure A3-221. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 121.0-126.0 m in KFM09A. This plot shows a fit to the first of two different PRF:s during the injection period in this section.*

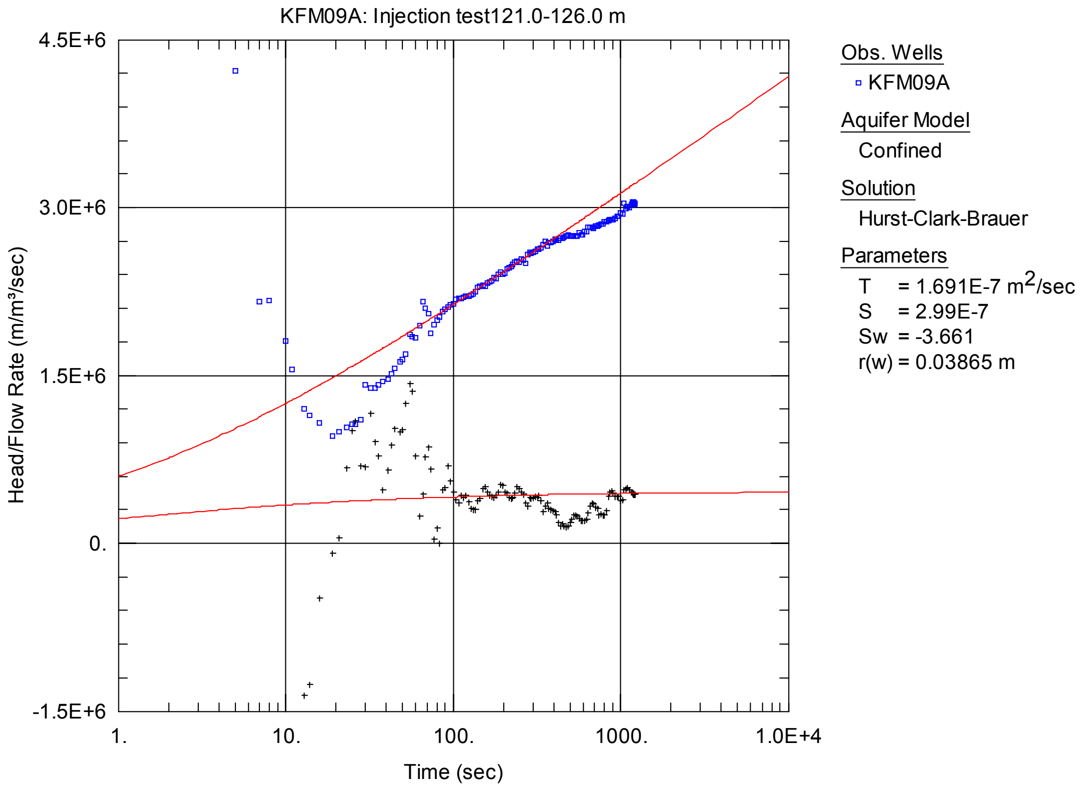


Figure A3-222. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 121.0-126.0 m in KFM09A. This plot shows a fit to the first of two different PRF:s during the injection period in this section.*

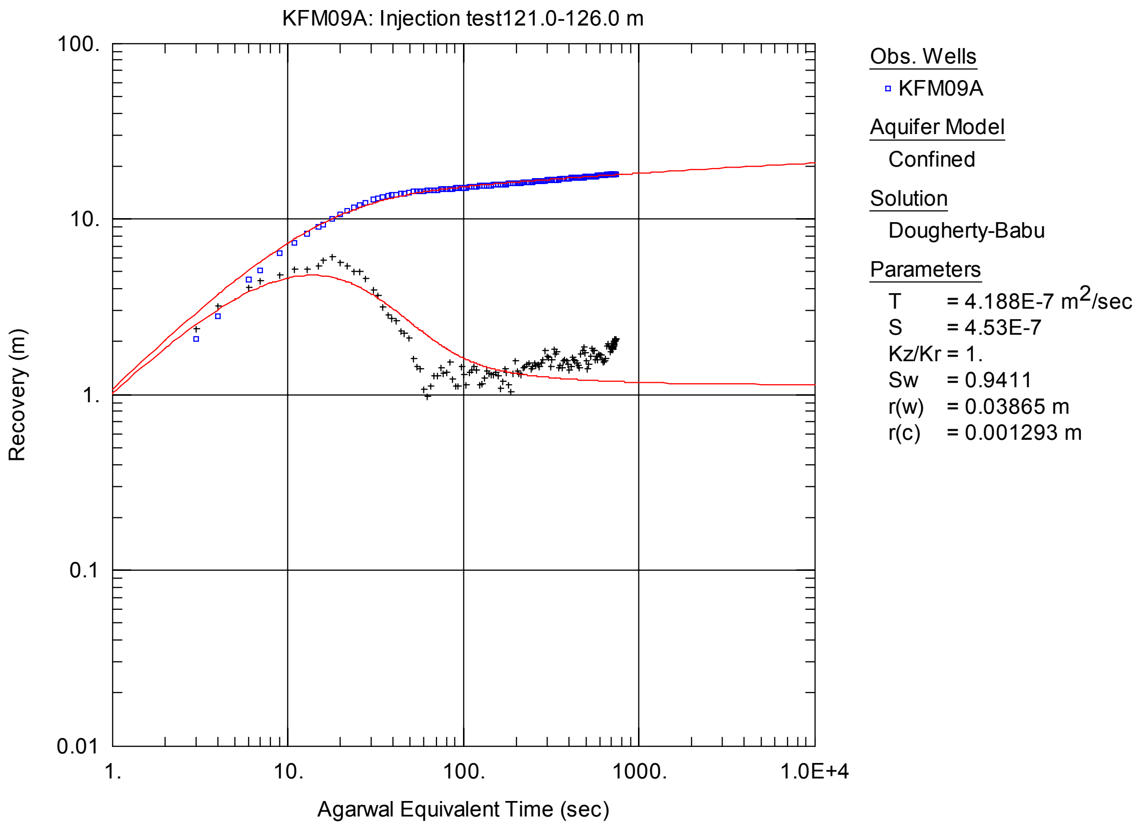


Figure A3-223. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 121.0-126.0 m in KFM09A.*

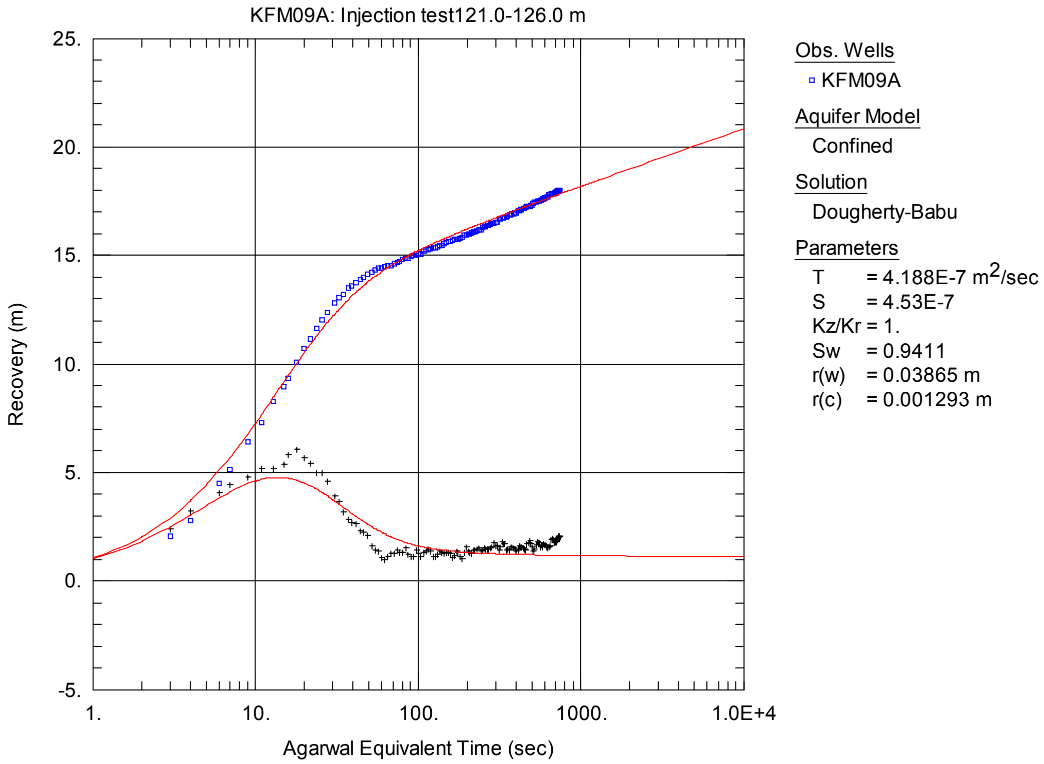


Figure A3-224. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 121.0-126.0 m in KFM09A.*

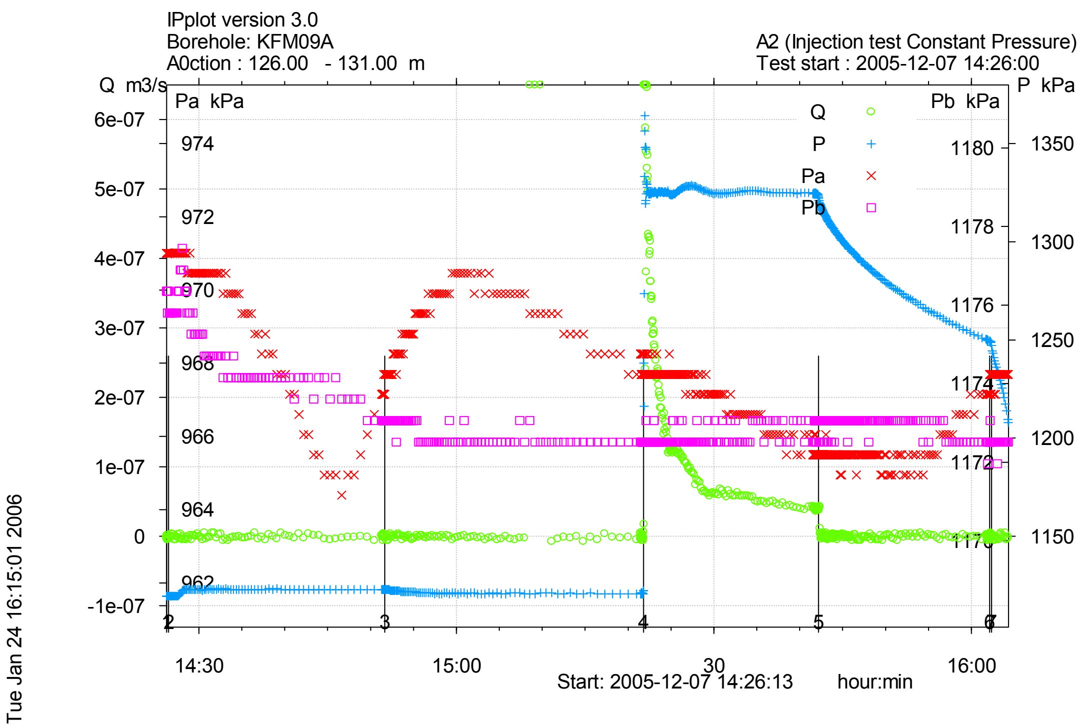


Figure A3-225. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 126.0-131.0 m in borehole KFM09A.*

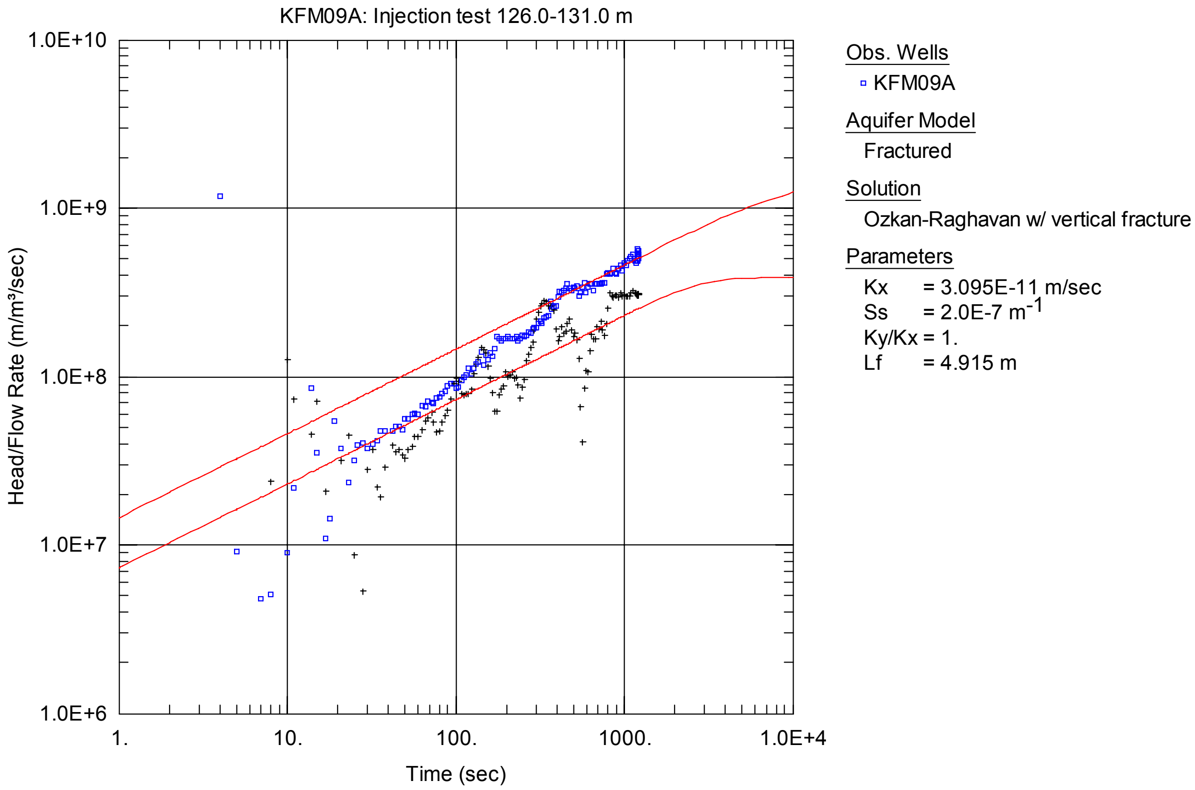


Figure A3-226. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 126.0-131.0 m in KFM09A. No unambiguous transient evaluation is possible on the injection period.*

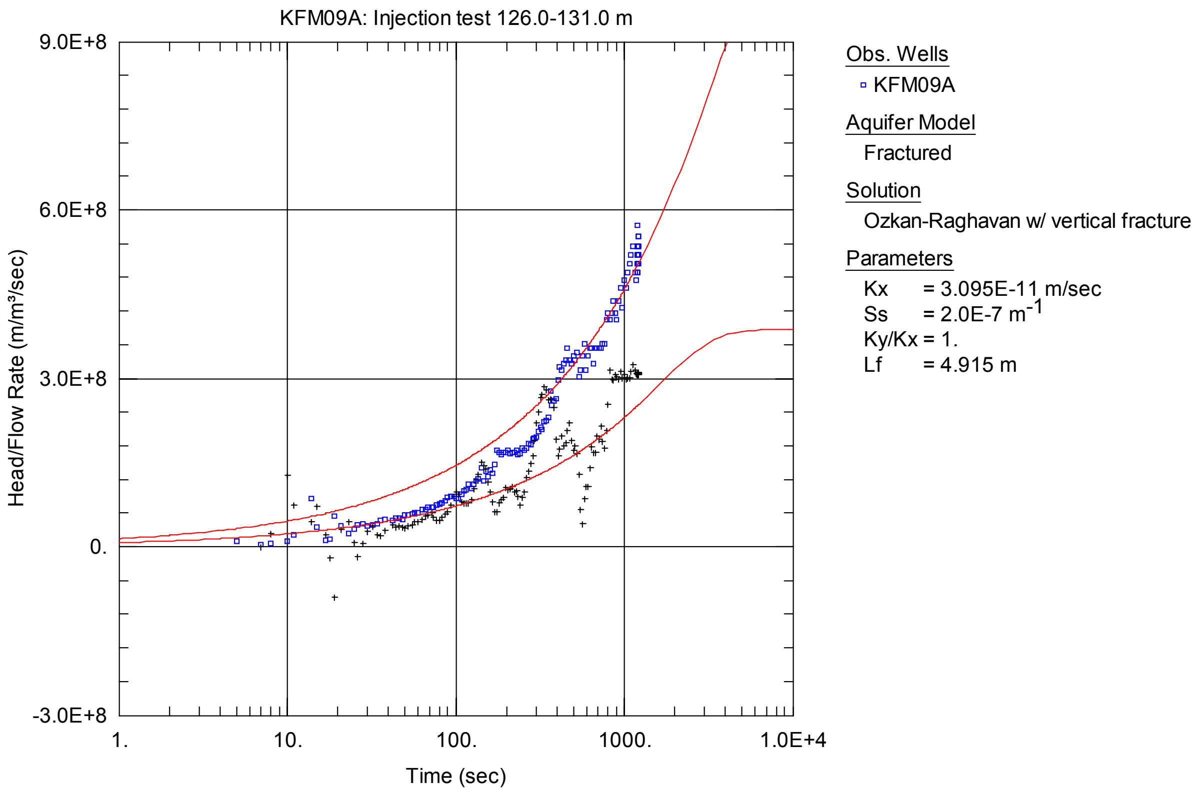


Figure A3-227. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 126.0-131.0 m in KFM09A. No unambiguous transient evaluation is possible on the injection period.*

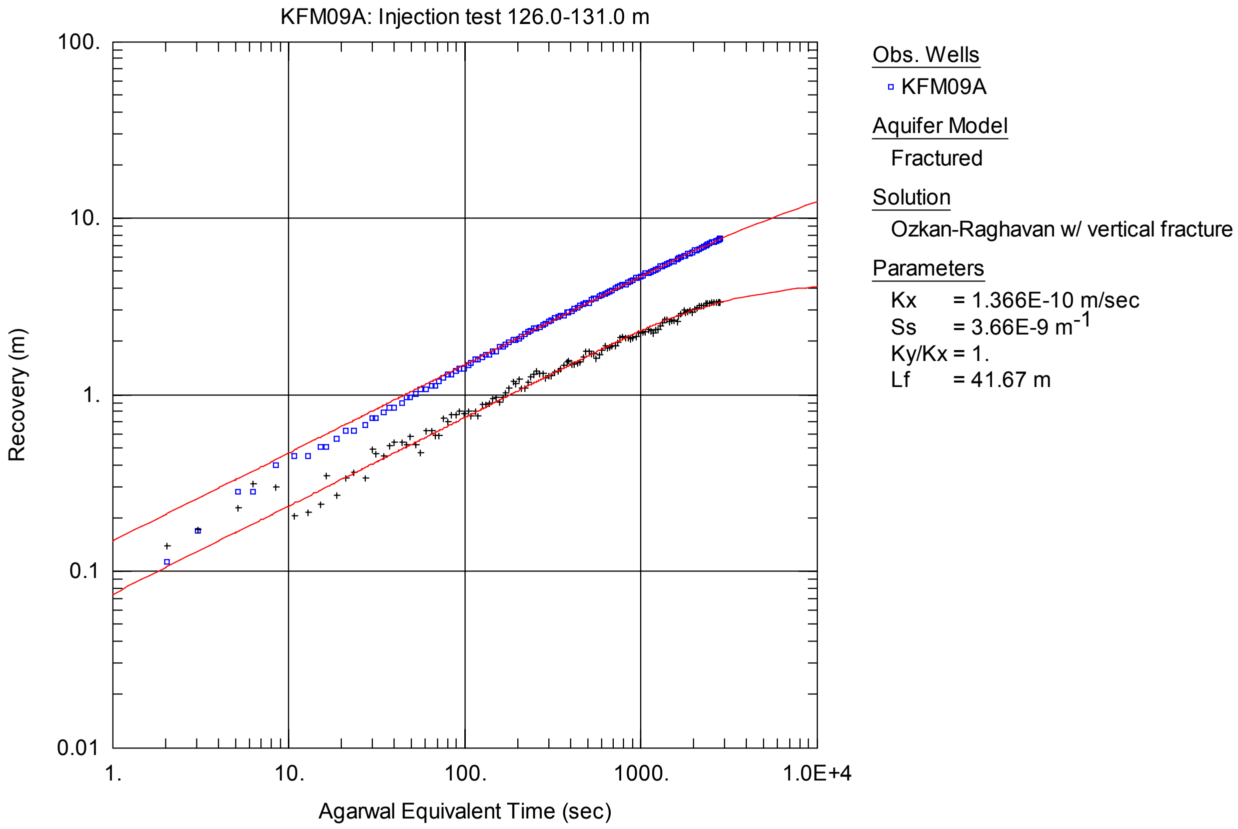


***Figure A3-228.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 126.0-131.0 m in KFM09A.*

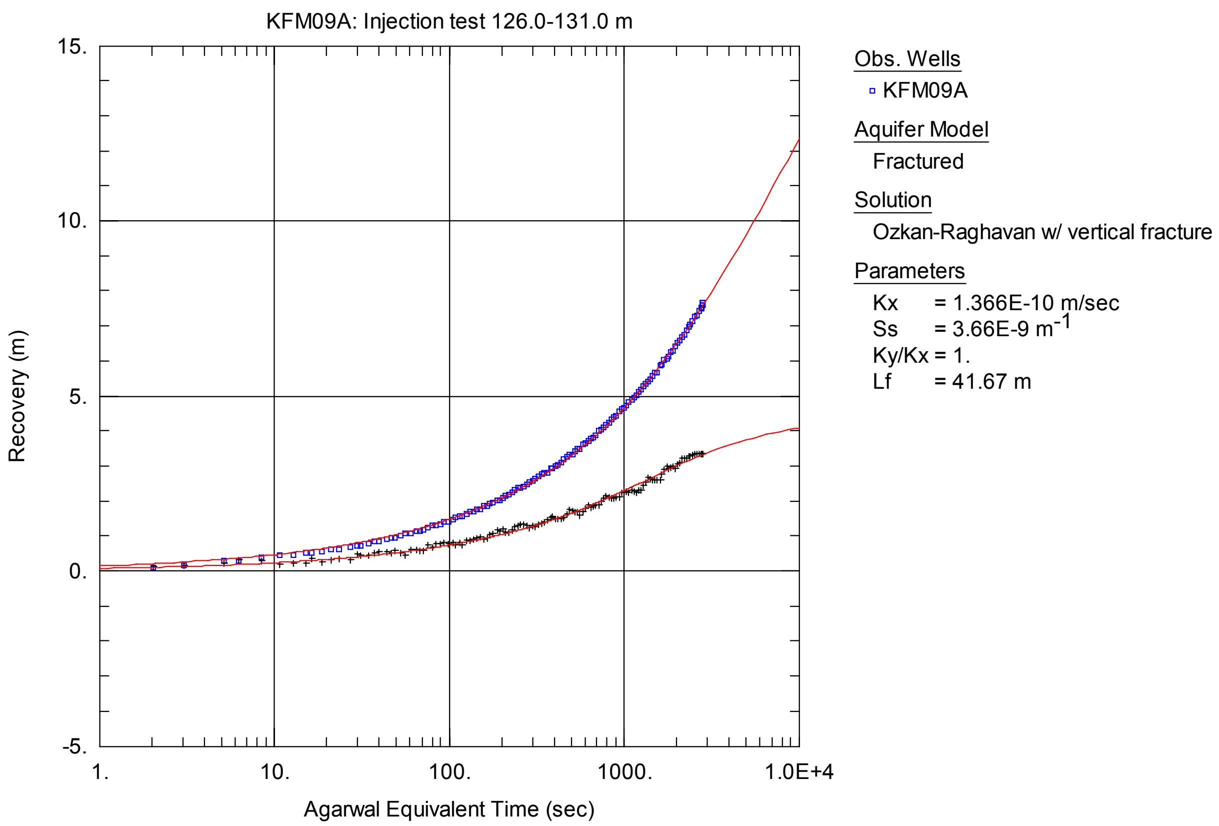


***Figure A3-229.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 126.0-131.0 m in KFM09A.*

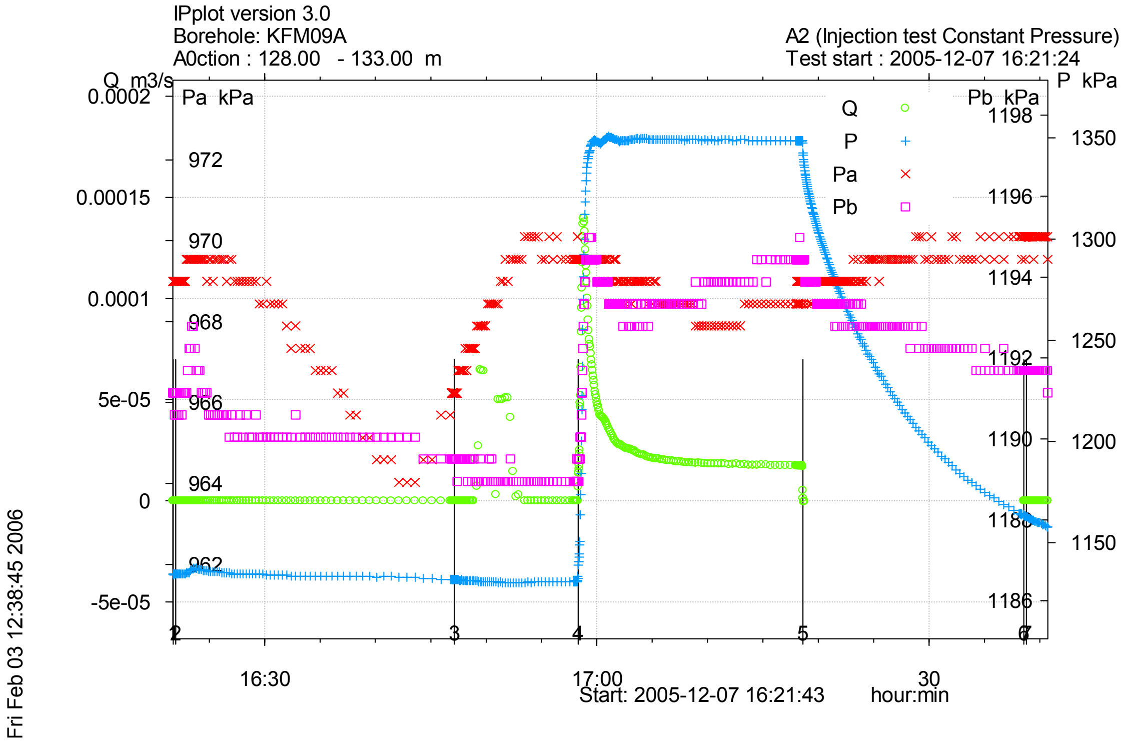


Figure A3-230. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 128.0-133.0 m in borehole KFM09A.*

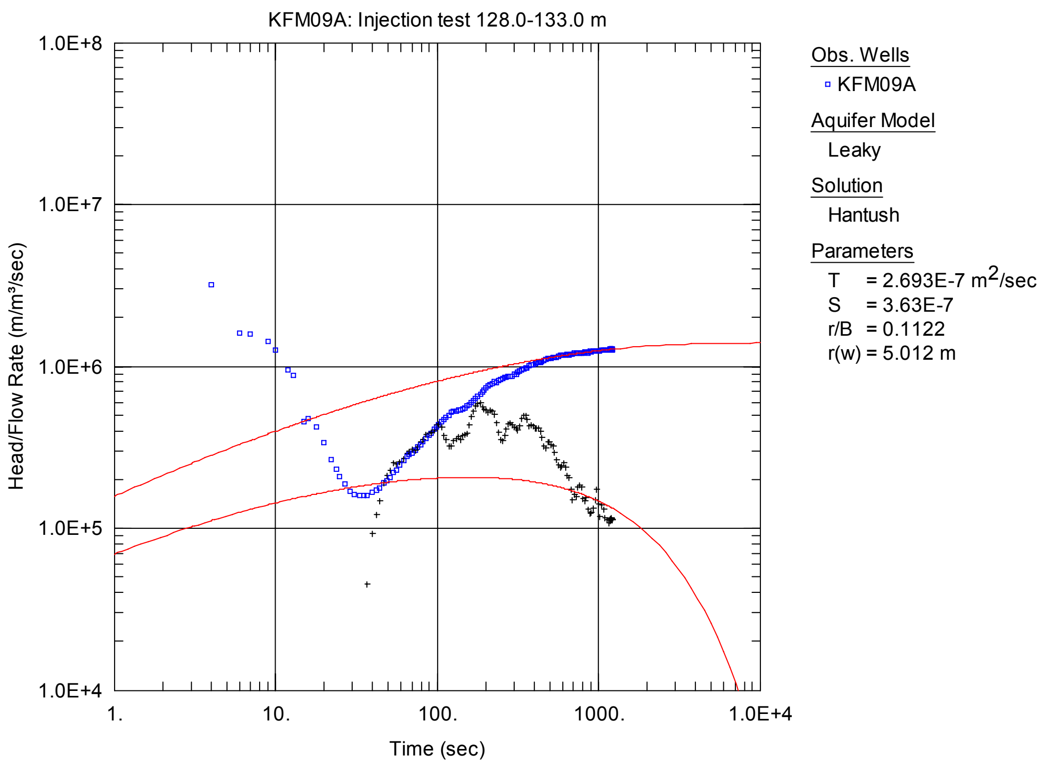


Figure A3-231. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 128.0-133.0 m in KFM09A.*

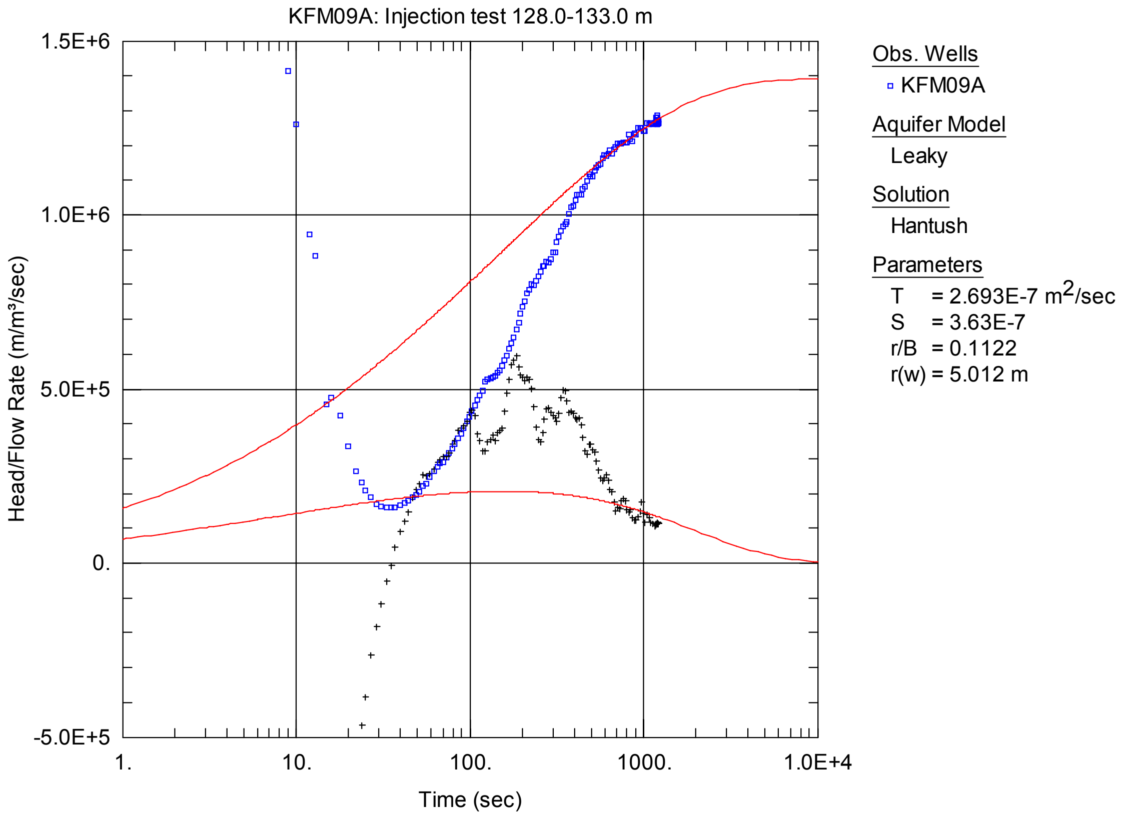


Figure A3-232. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 128.0-133.0 m in KFM09A.*

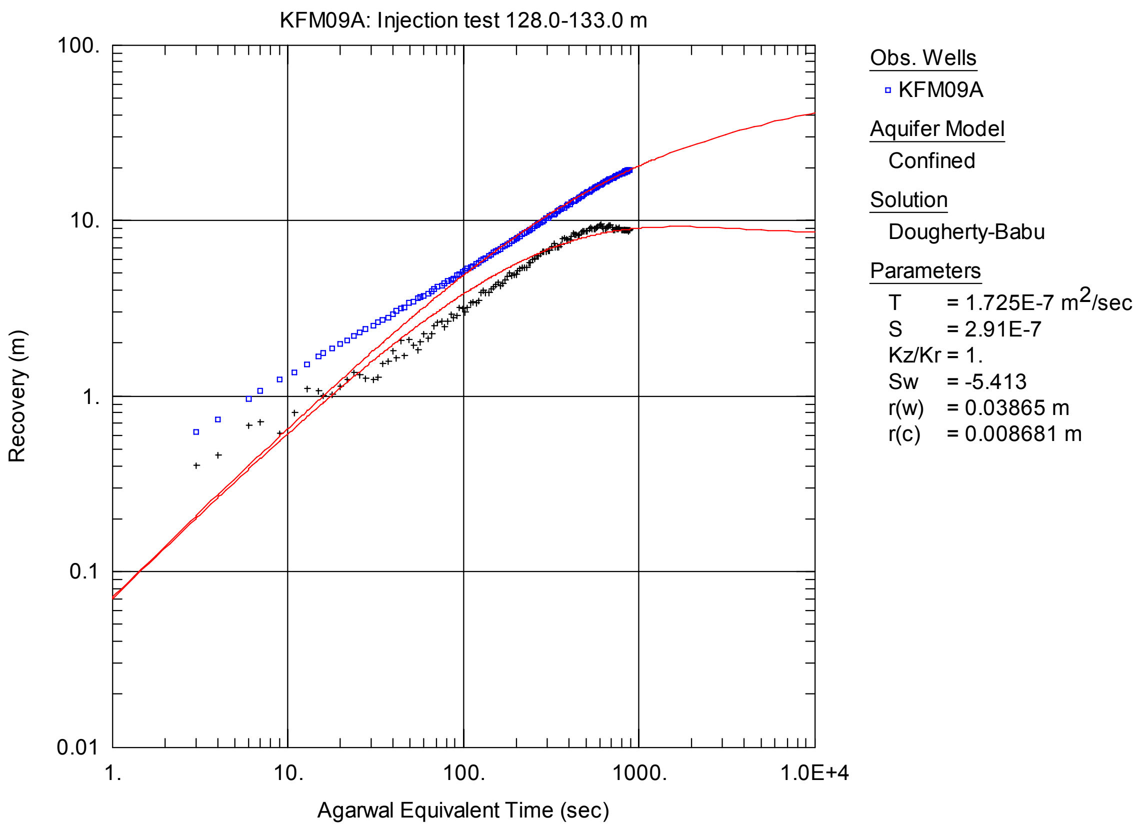


Figure A3-233. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 128.0-133.0 m in KFM09A.*

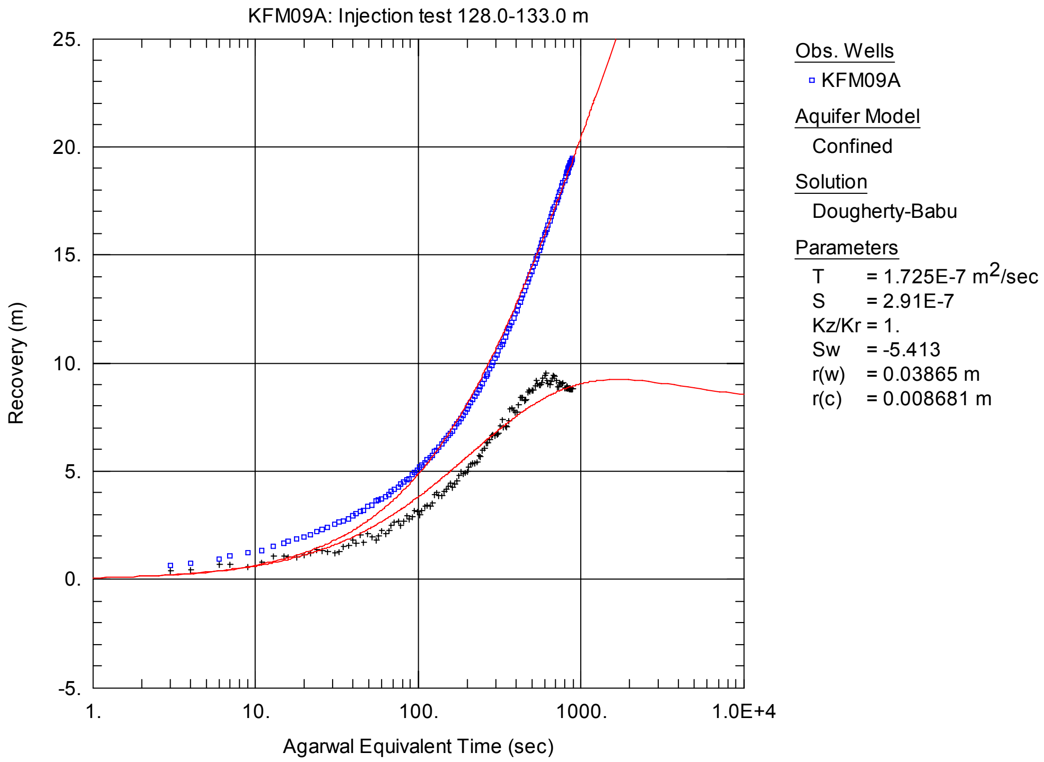


Figure A3-234. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 128.0-133.0 m in KFM09A.*

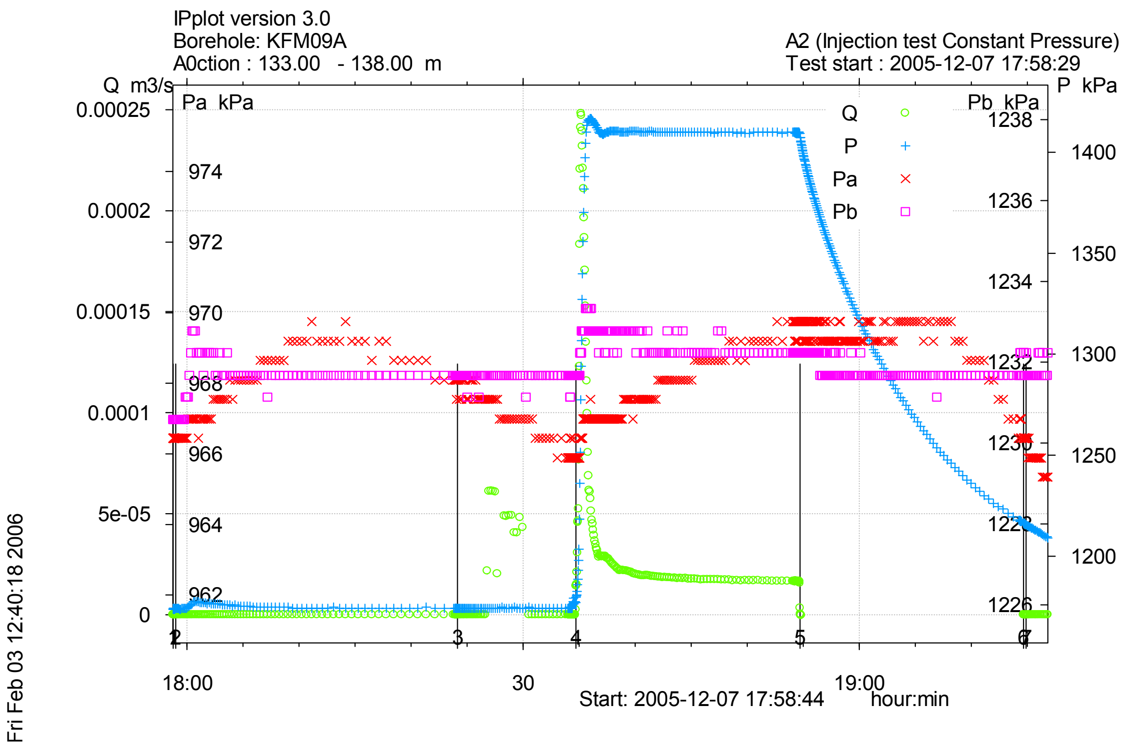


Figure A3-235. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 133.0-138.0 m in borehole KFM09A.*

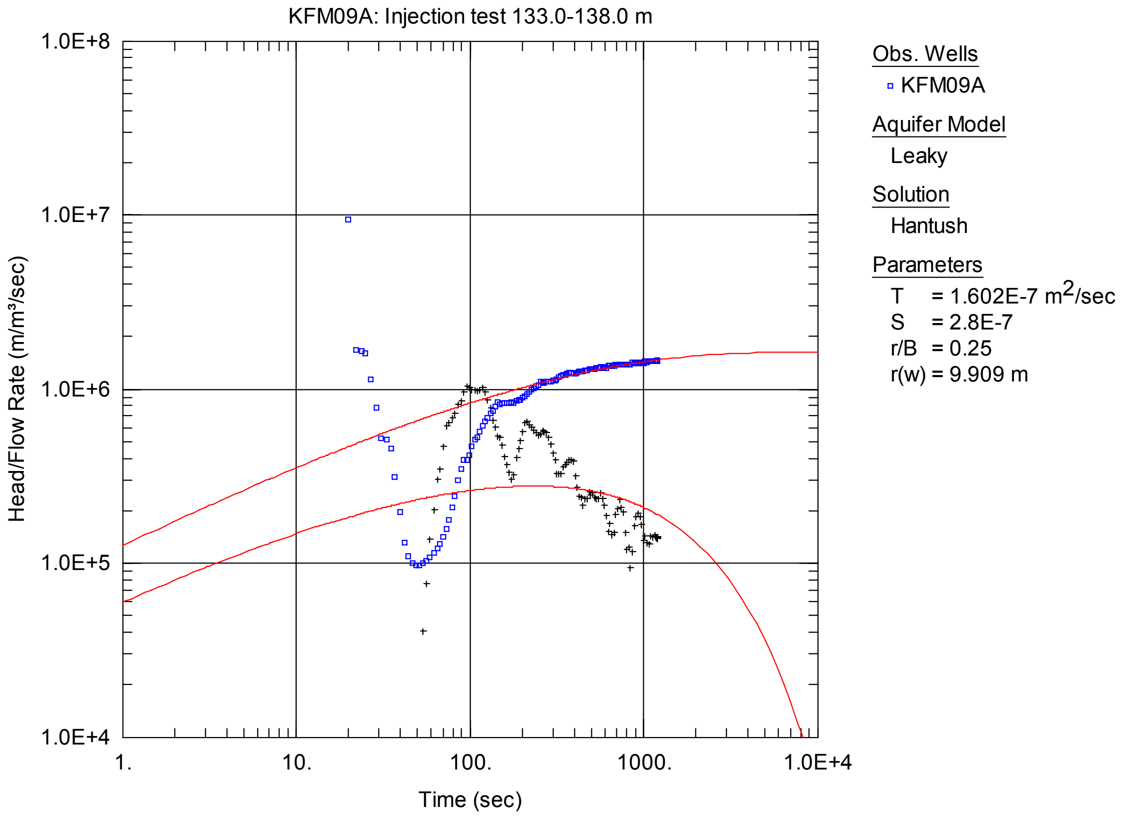


Figure A3-236. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 133.0-138.0 m in KFM09A.*

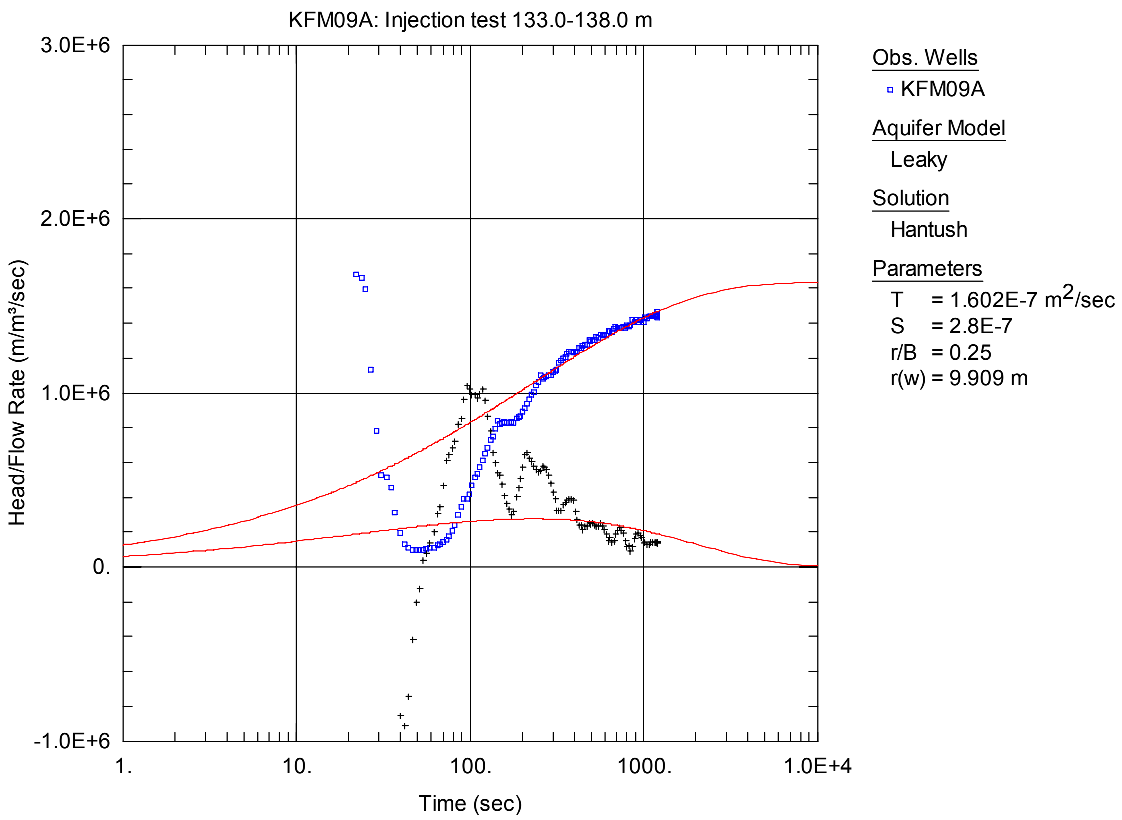


Figure A3-237. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 133.0-138.0 m in KFM09A.*

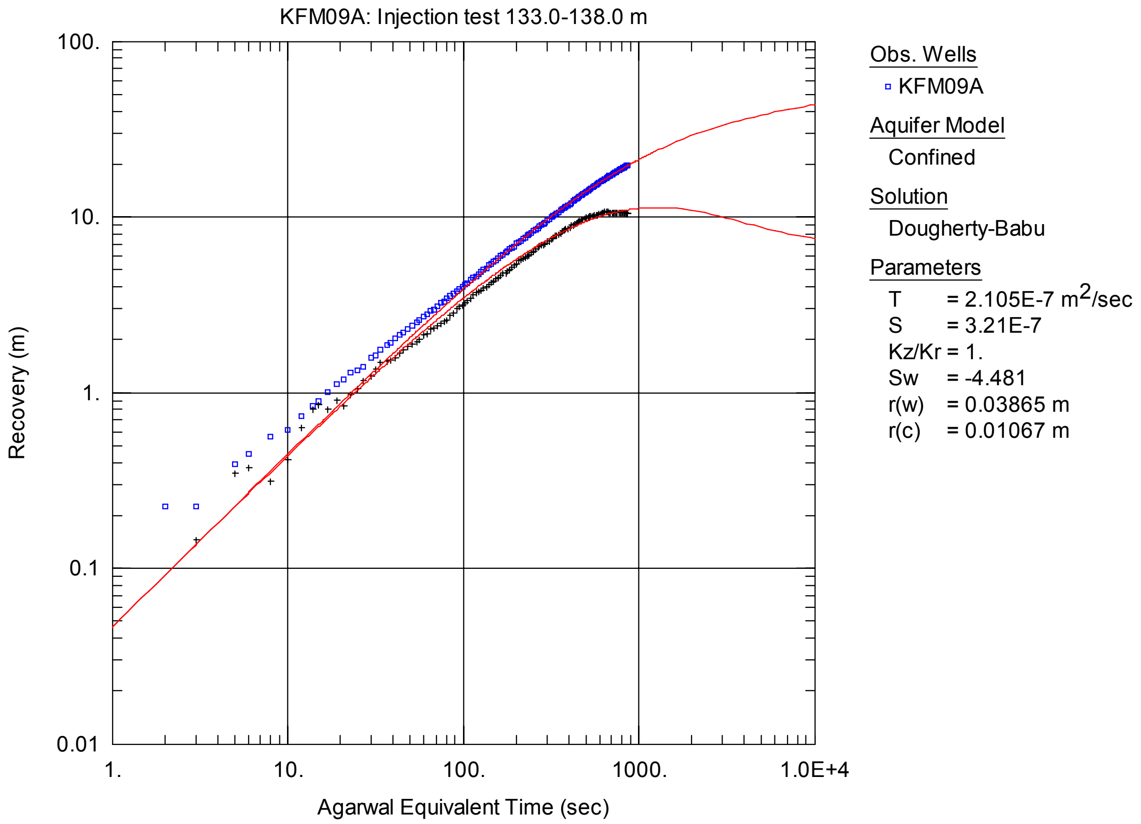


***Figure A3-238.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 133.0-138.0 m in KFM09A.*

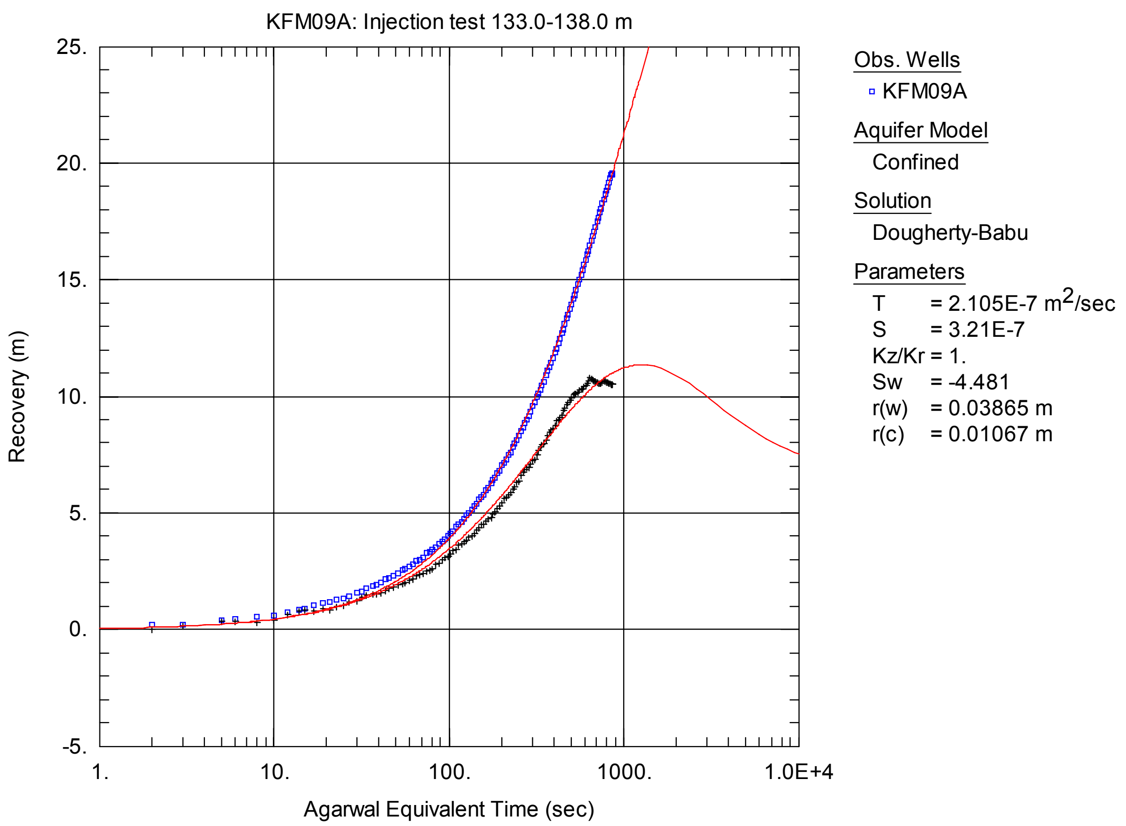


***Figure A3-239.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 133.0-138.0 m in KFM09A.*

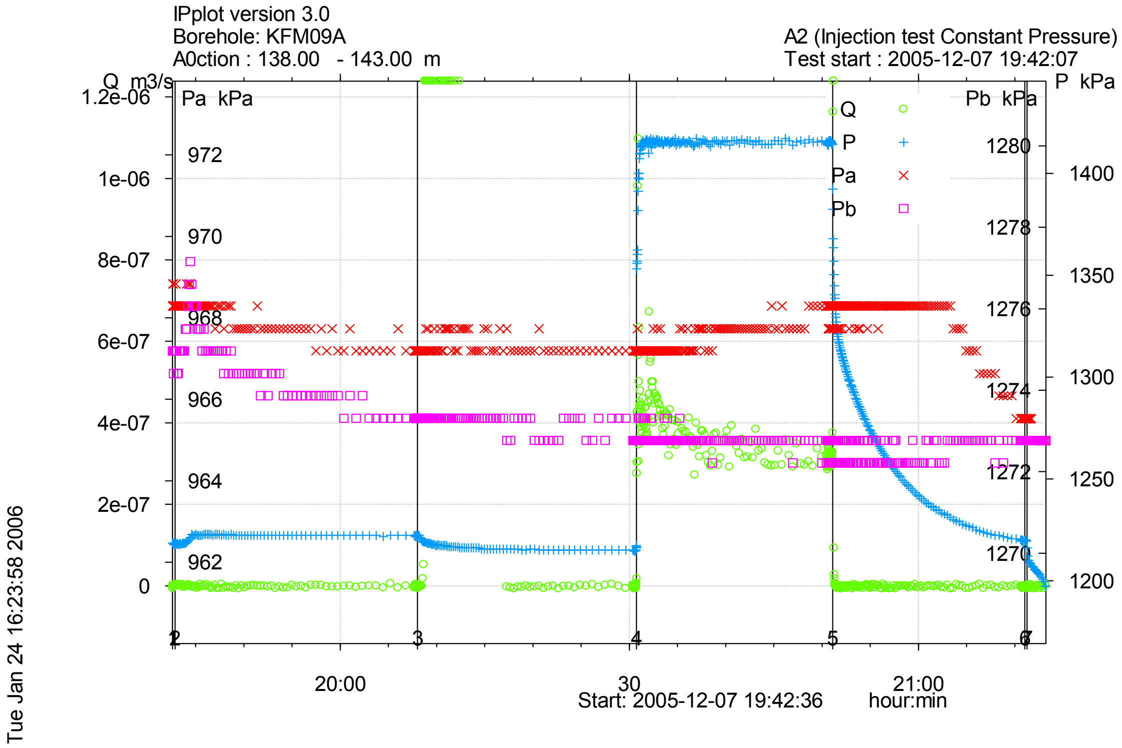


Figure A3-240. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 138.0-143.0 m in borehole KFM09A.*

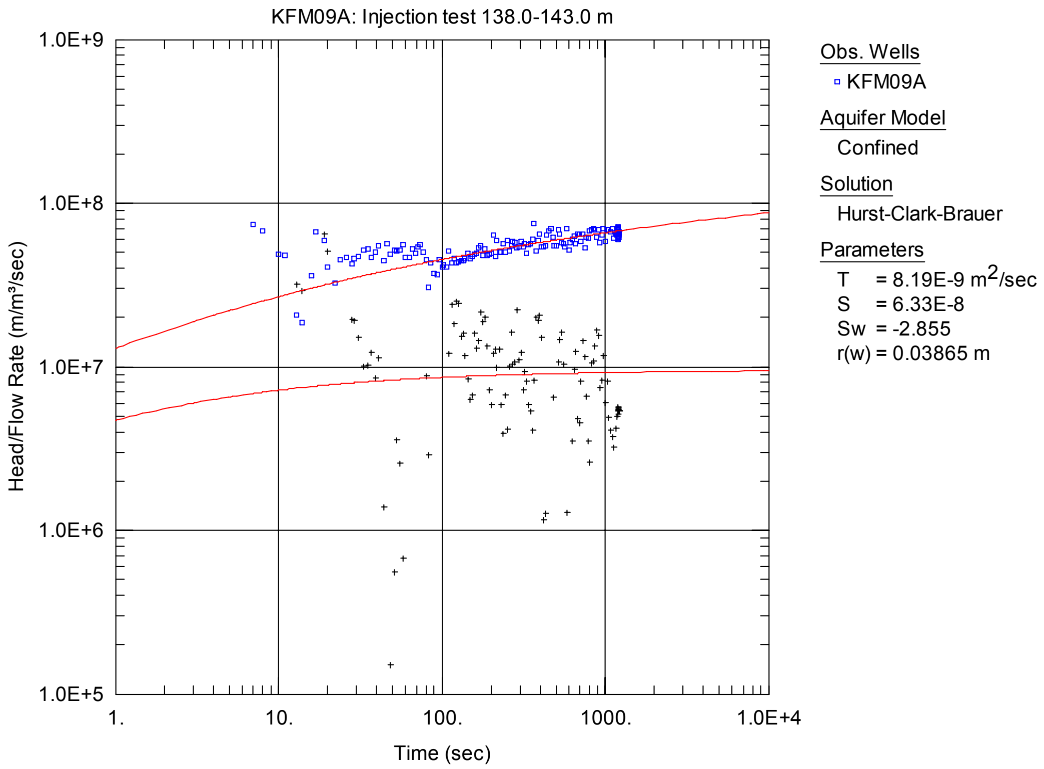


Figure A3-241. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 138.0-143.0 m in KFM09A.*

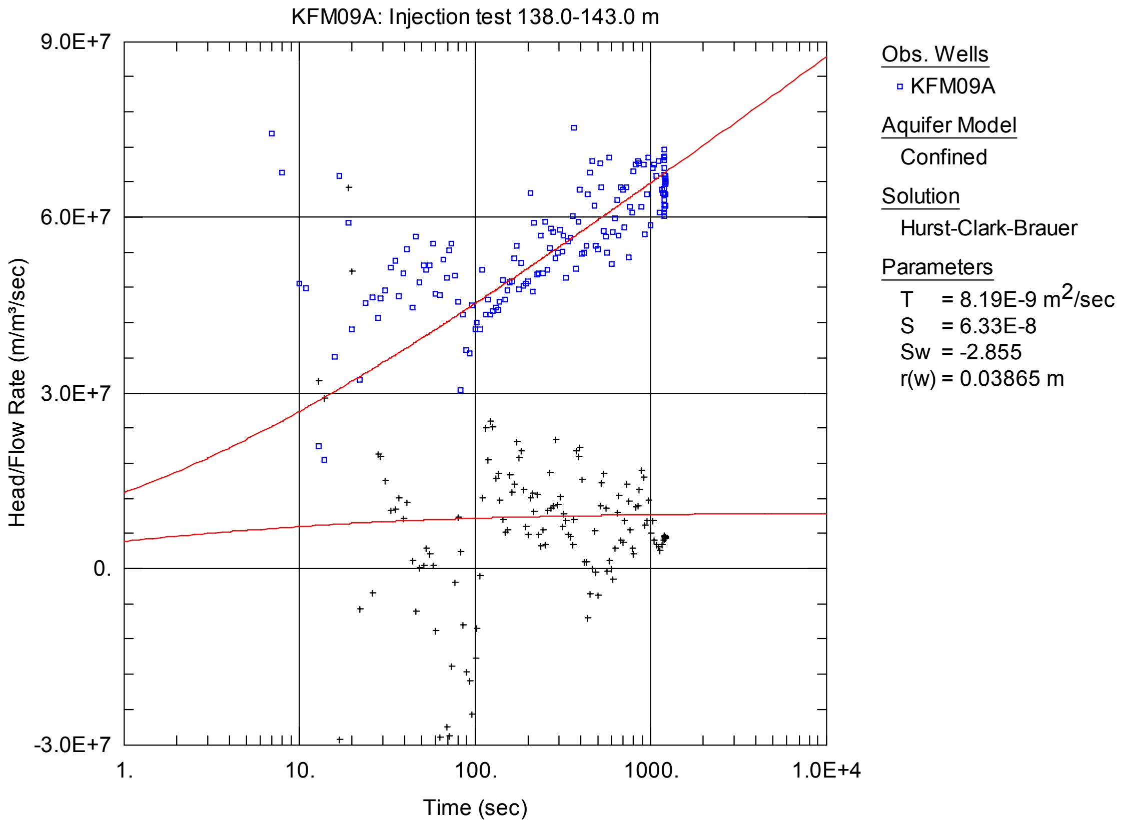


Figure A3-242. Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 138.0-143.0 m in KFM09A.

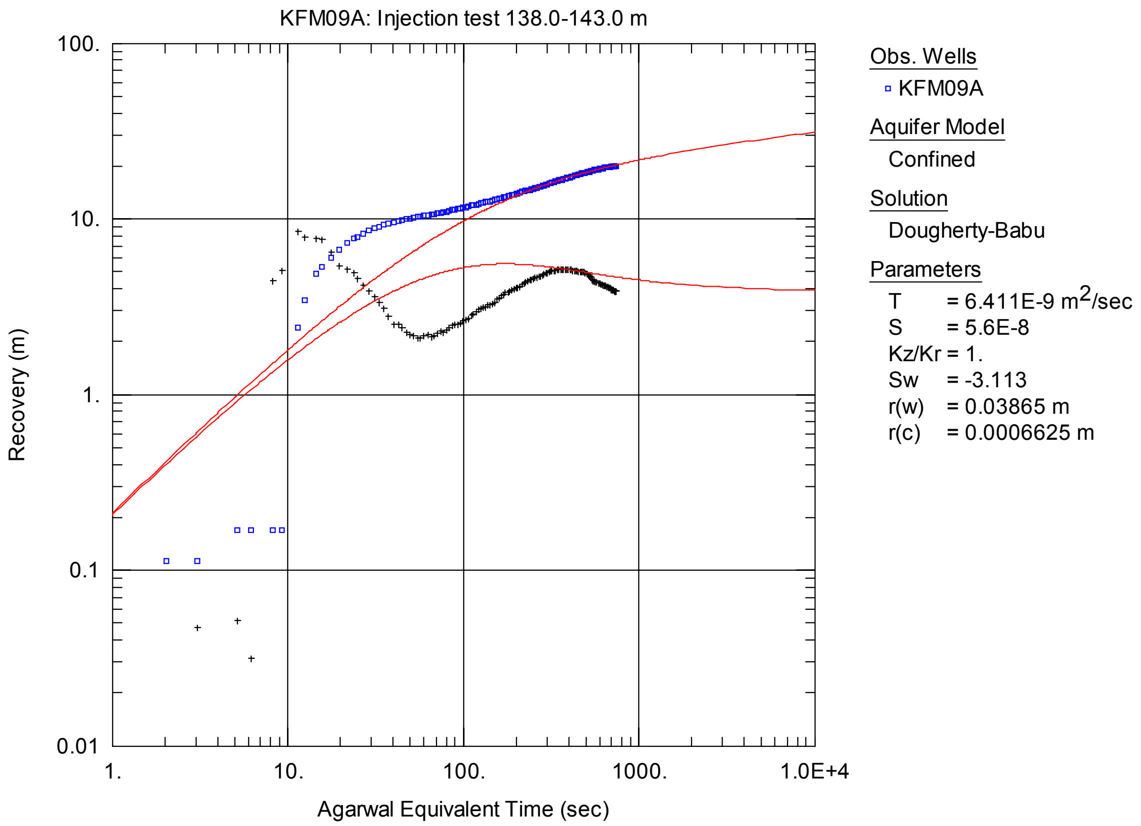


Figure A3-243. Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 138.0-143.0 m in KFM09A.

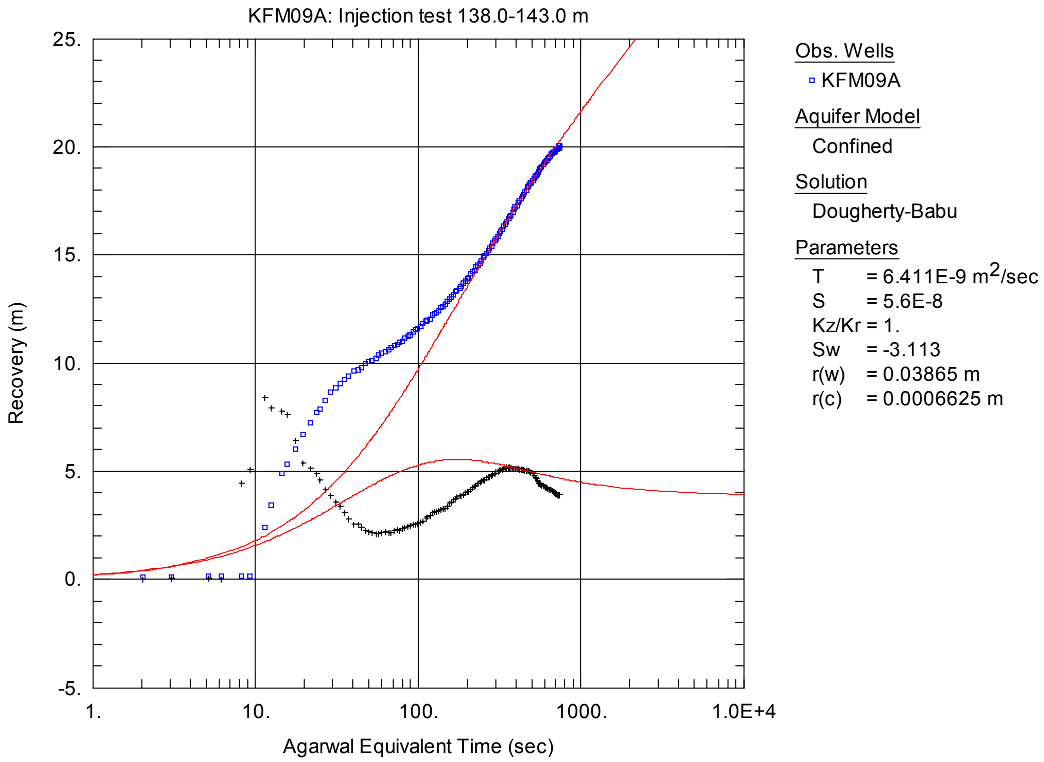


***Figure A3-244.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 138.0-143.0 m in KFM09A.*

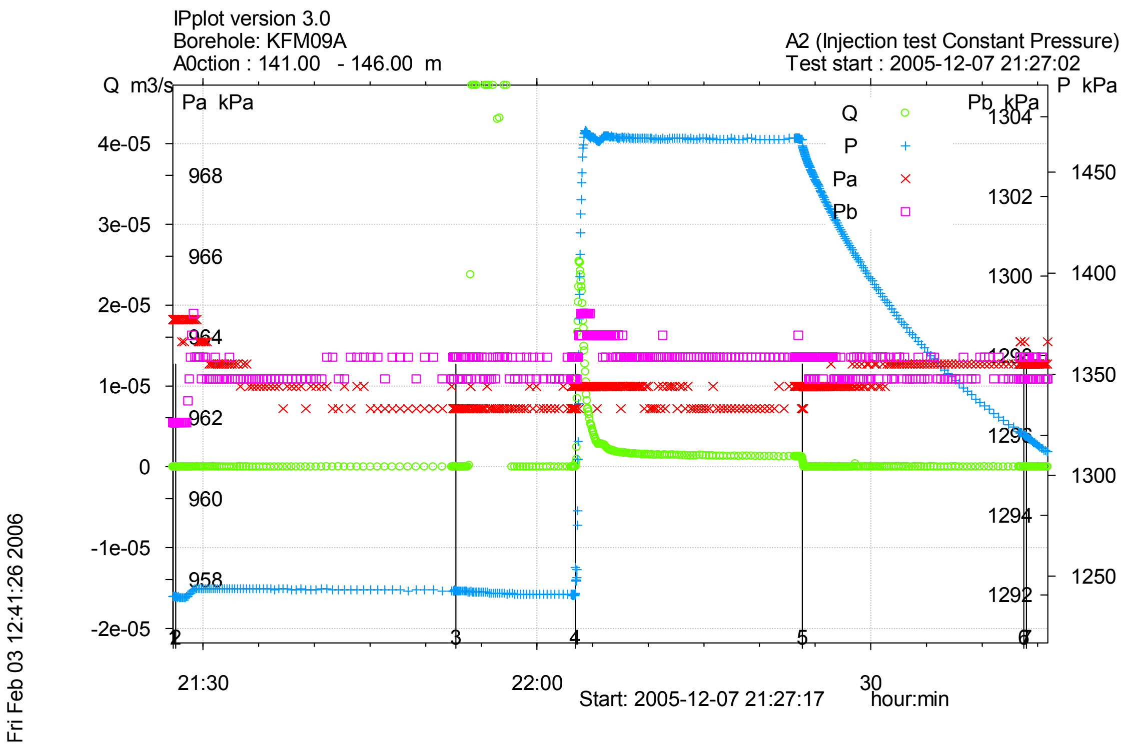


***Figure A3-245.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 141.0-146.0 m in borehole KFM09A.*

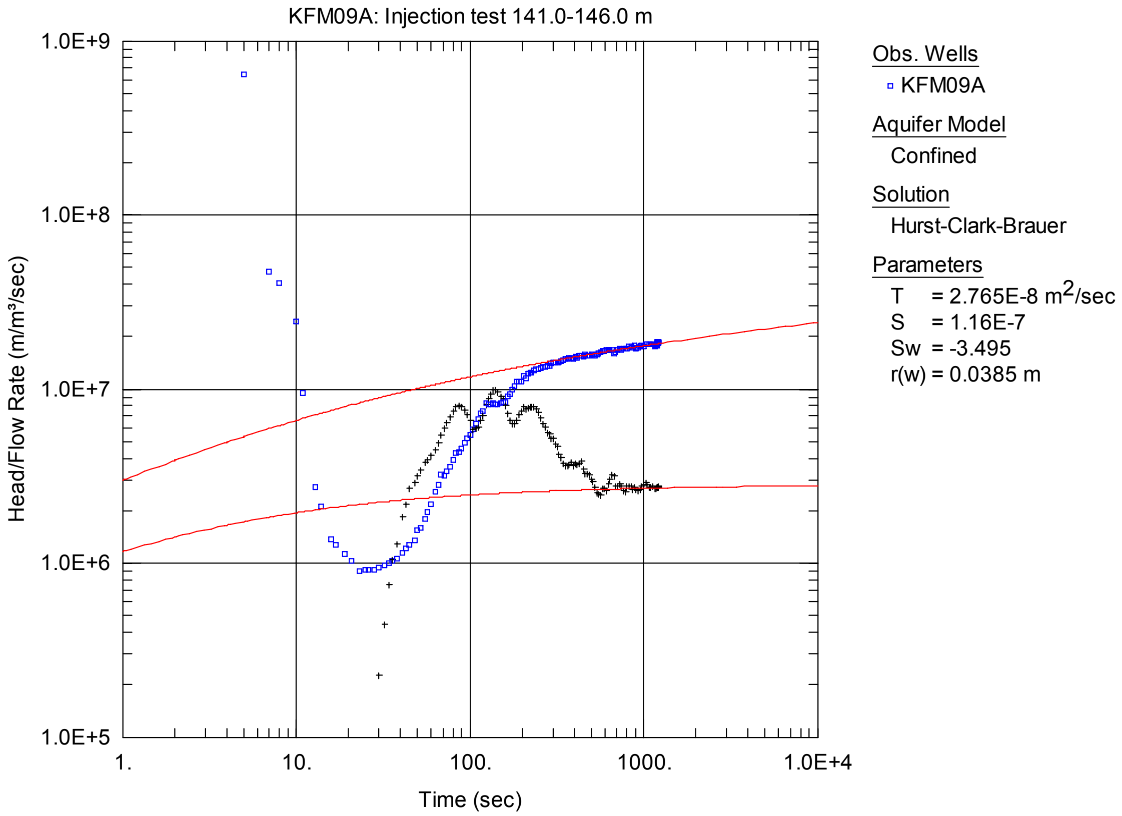


Figure A3-246. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 141.0-146.0 m in KFM09A.*

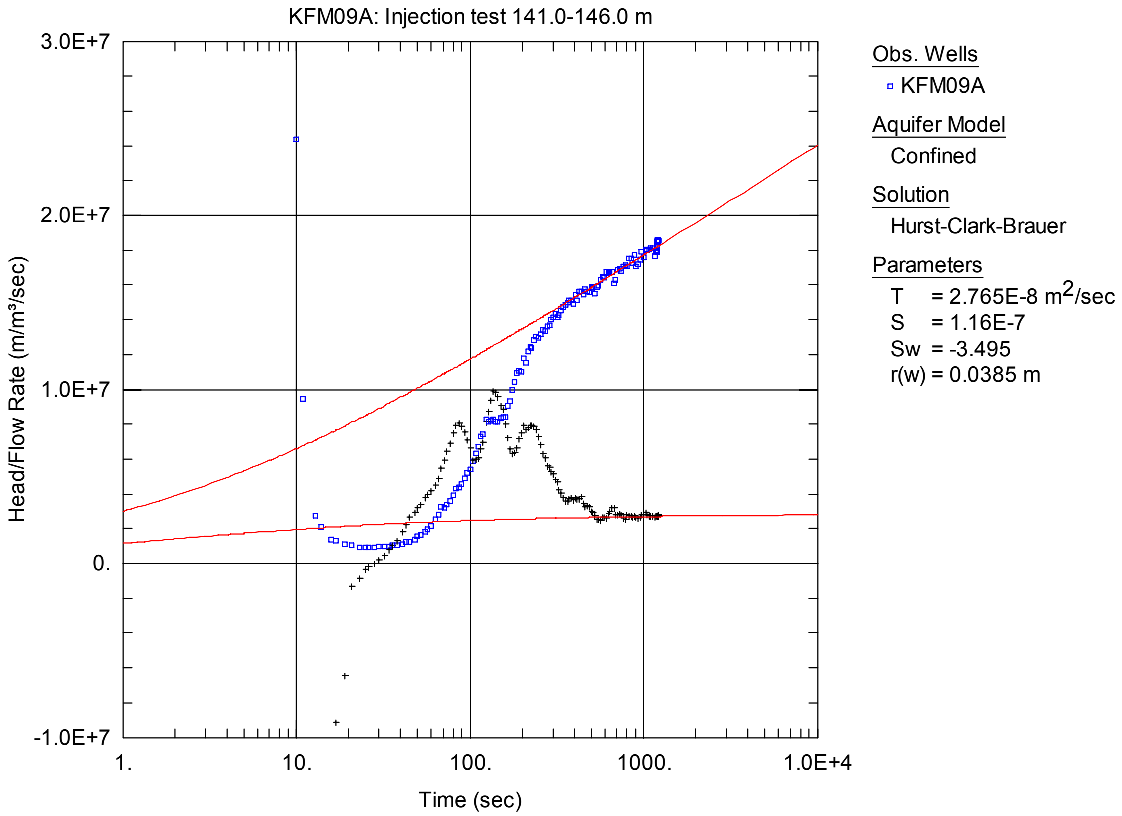


Figure A3-247. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 141.0-146.0 m in KFM09A.*

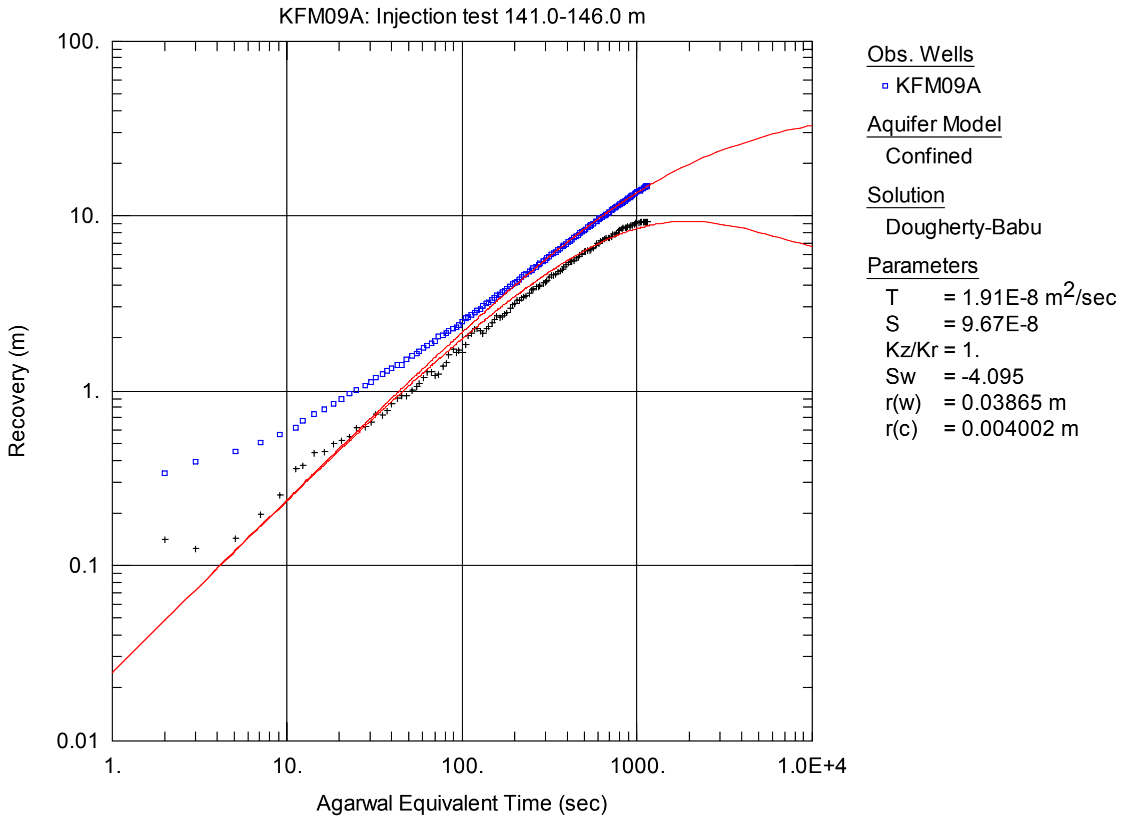


Figure A3-248. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 141.0-146.0 m in KFM09A.*

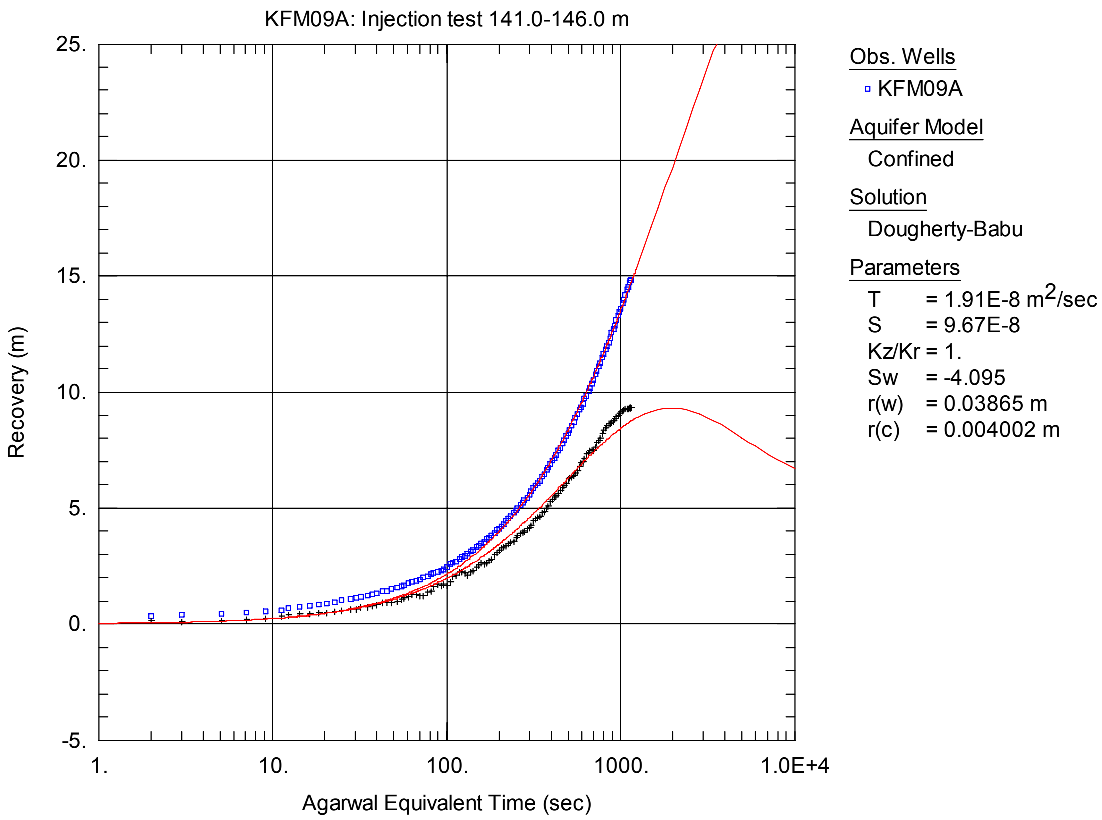


Figure A3-249. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 141.0-146.0 m in KFM09A.*

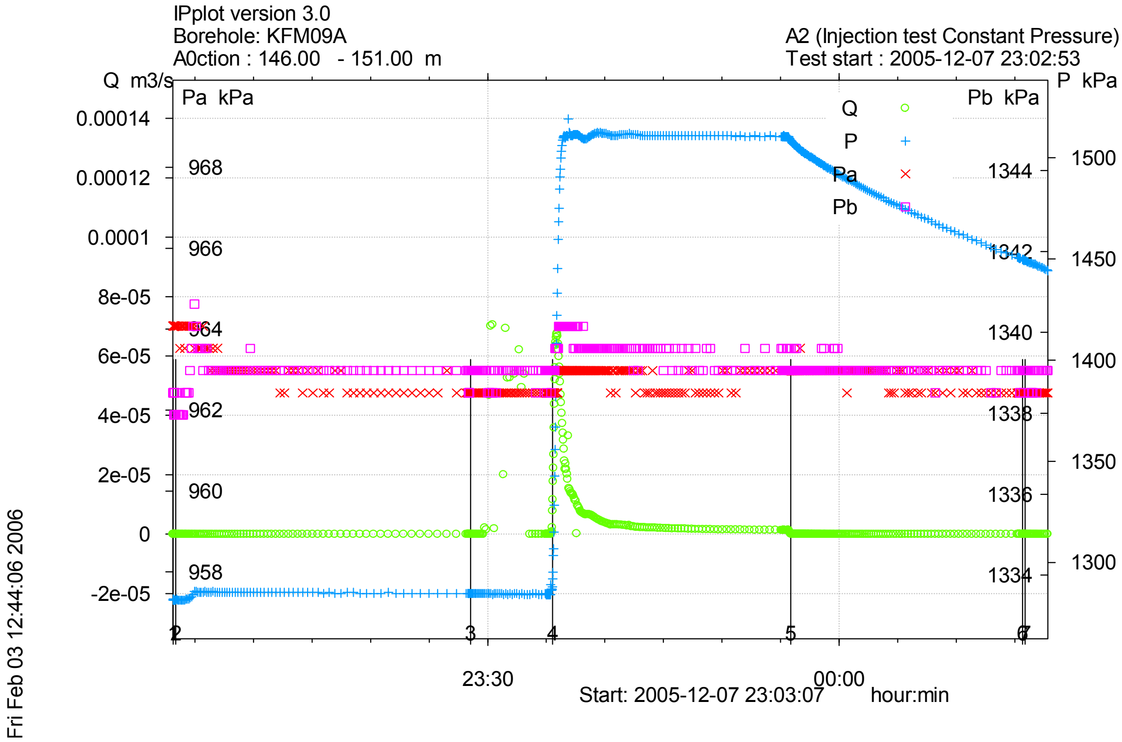


Figure A3-250. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 146.0-151.0 m in borehole KFM09A.*

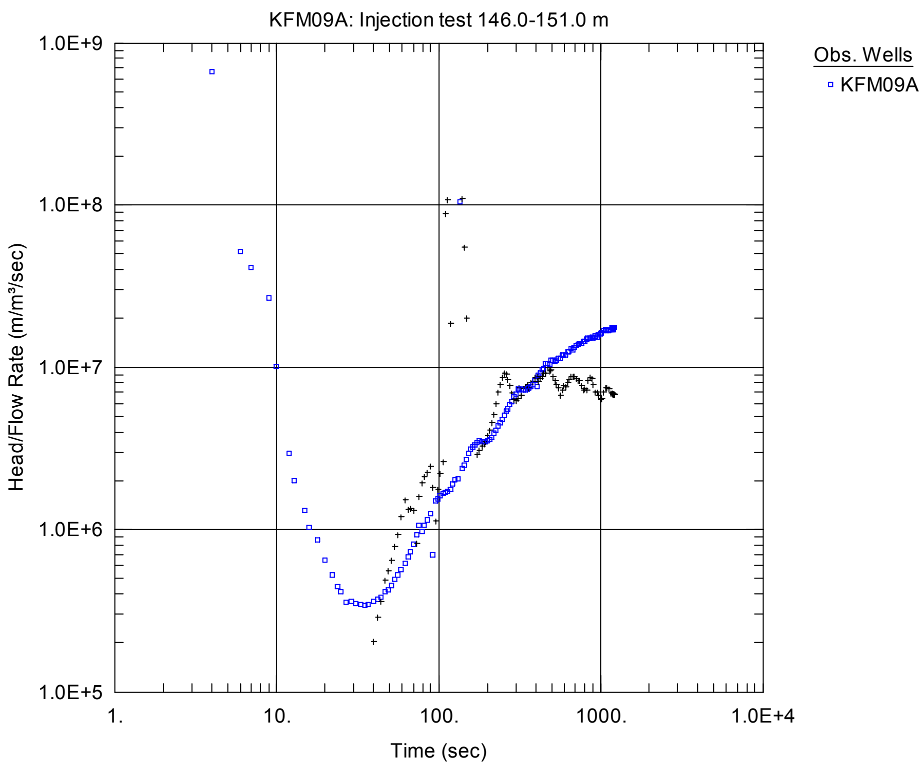


Figure A3-251. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 146.0-151.0 m in KFM09A.*

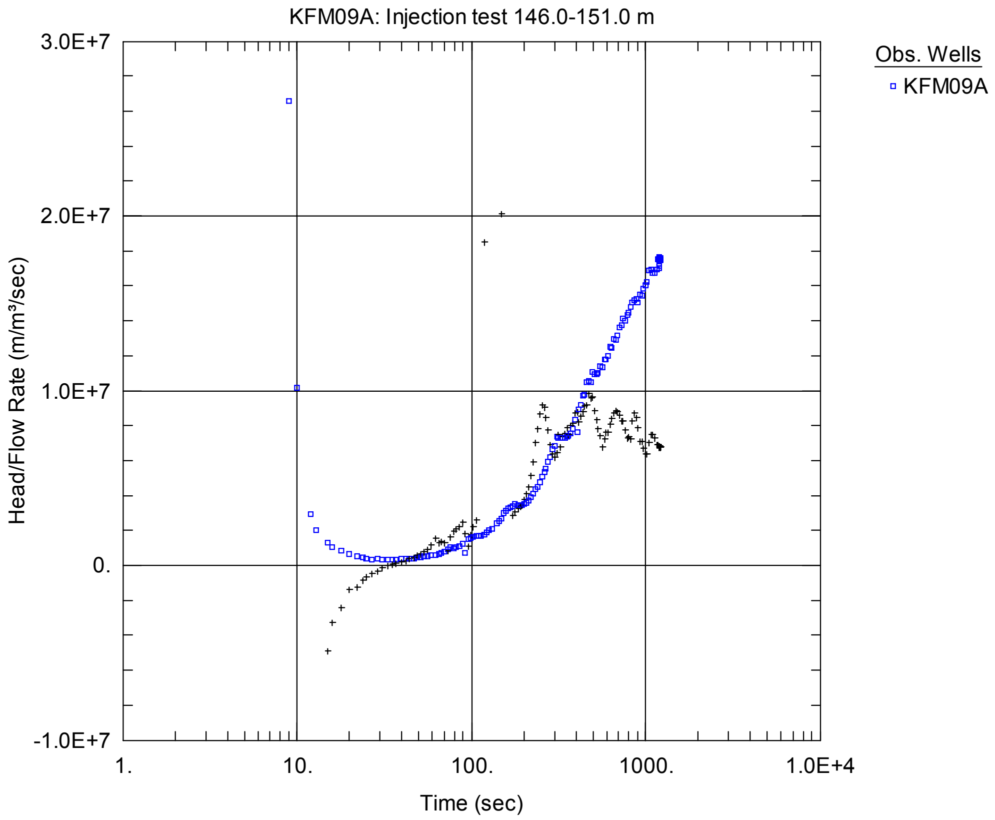


Figure A3-252. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 146.0-151.0 m in KFM09A.*

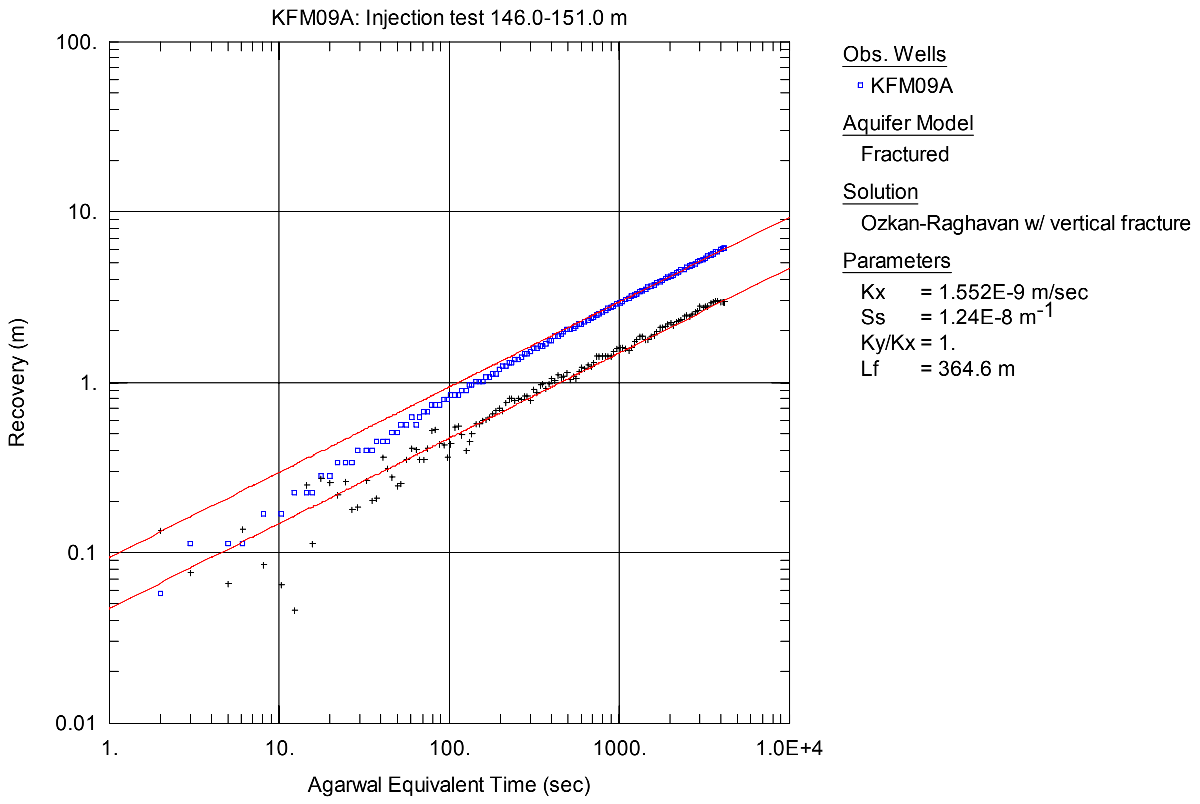


Figure A3-253. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 146.0-151.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

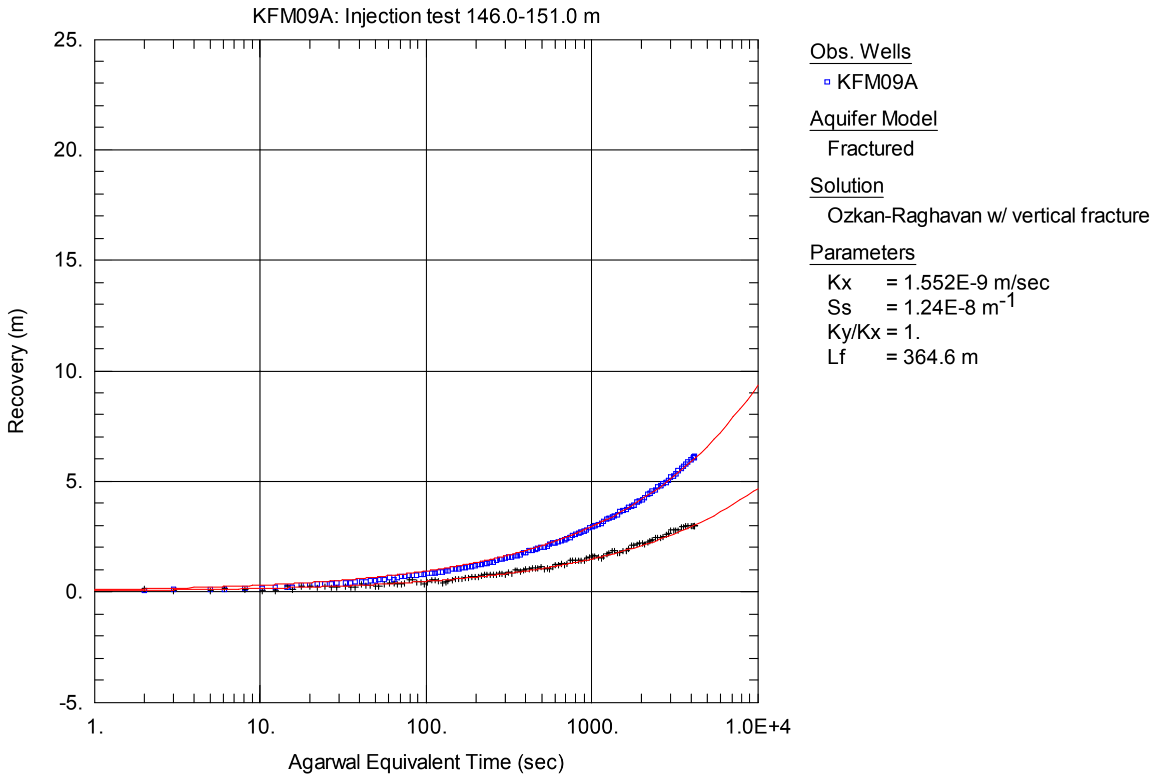


Figure A3-254. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 146.0-151.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

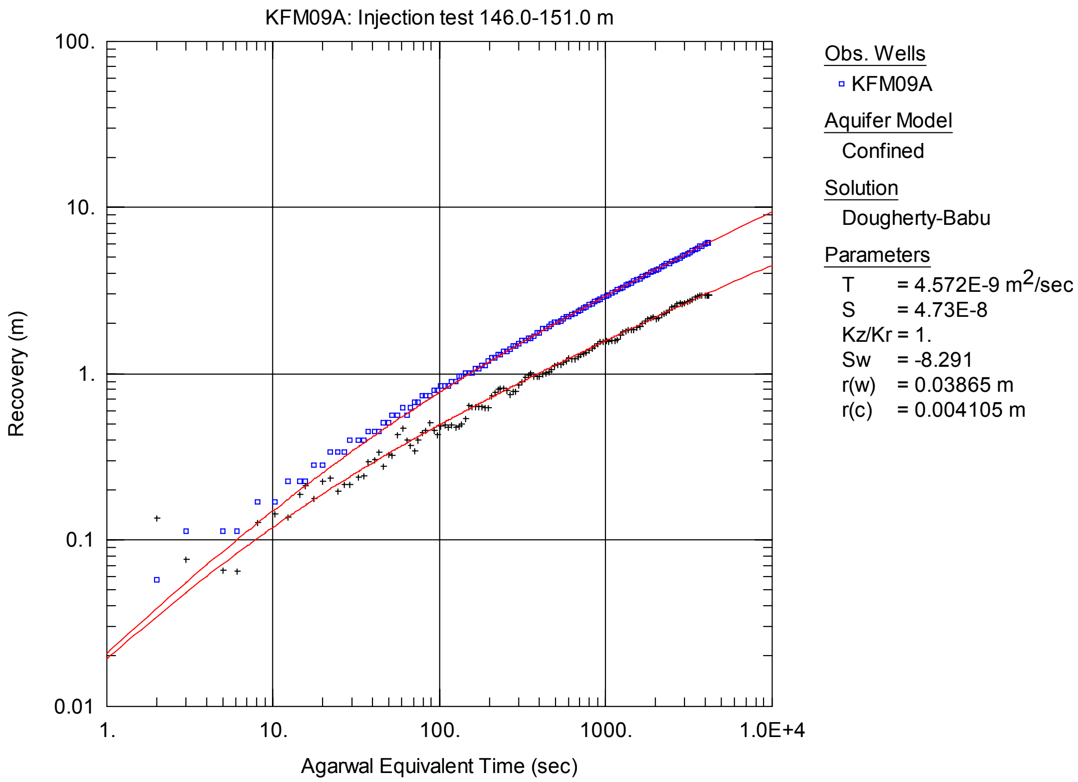


Figure A3-255. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 146.0-151.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

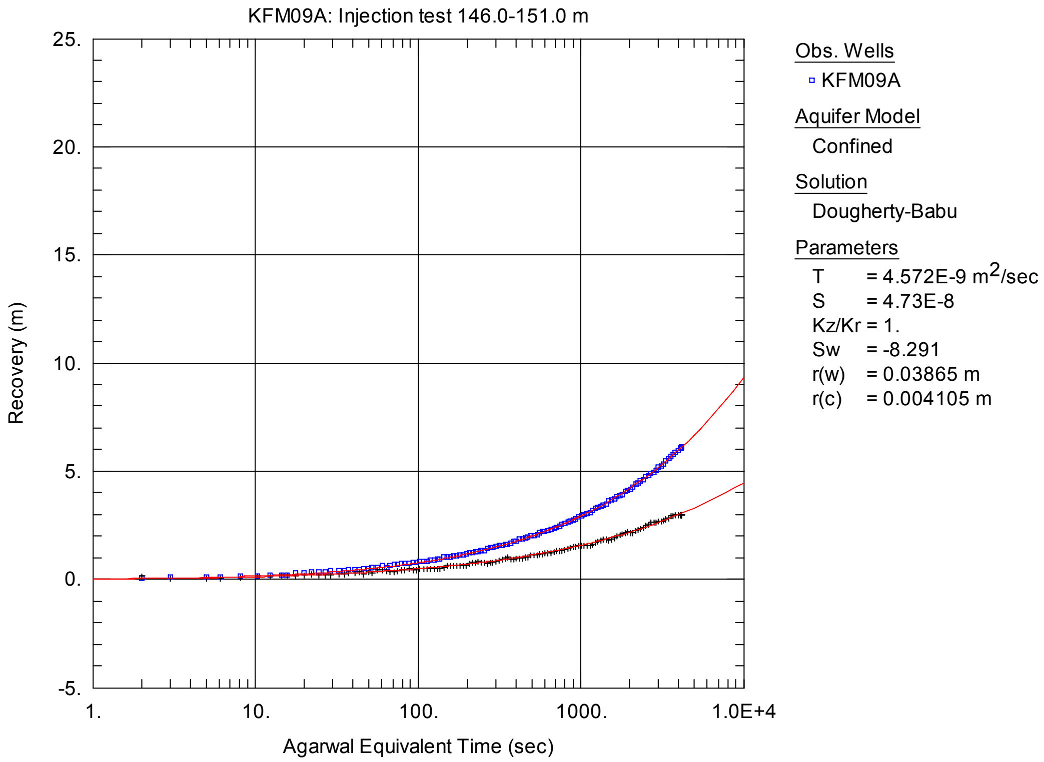


Figure A3-256. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 146.0-151.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

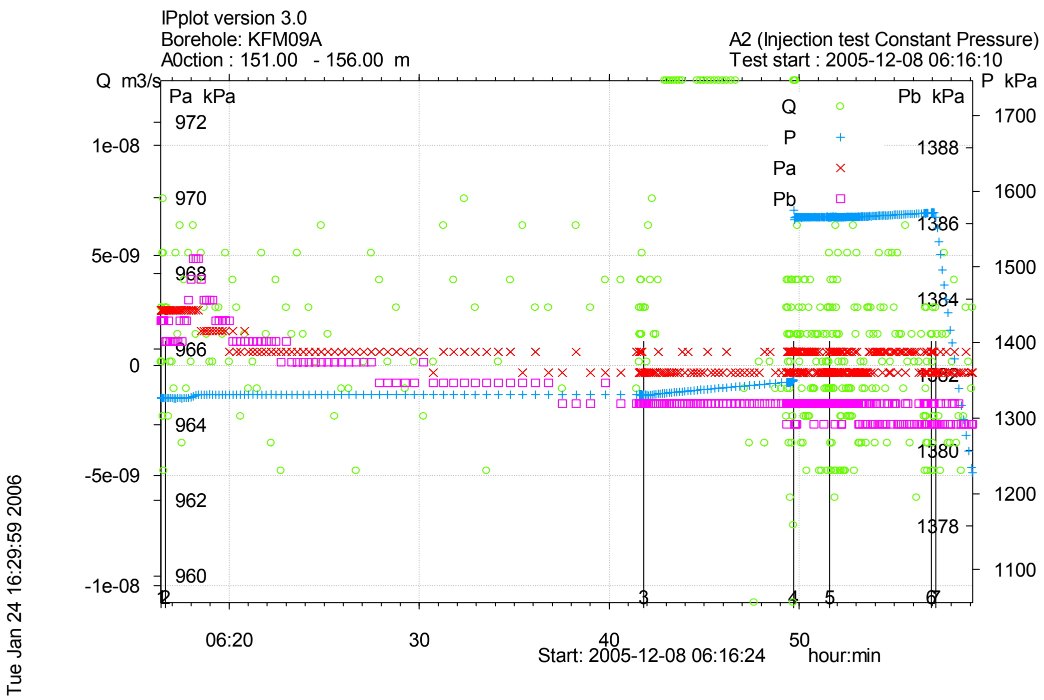


Figure A3-257. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 151.0-156.0 m in borehole KFM09A.*

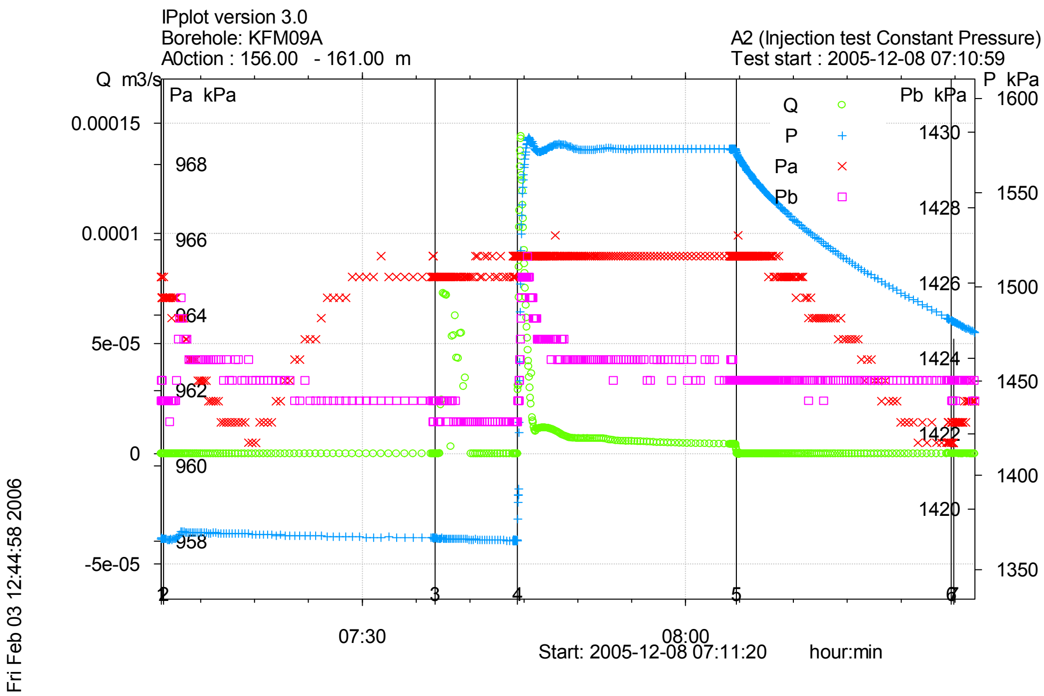


Figure A3-258. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 156.0-161.0 m in borehole KFM09A.

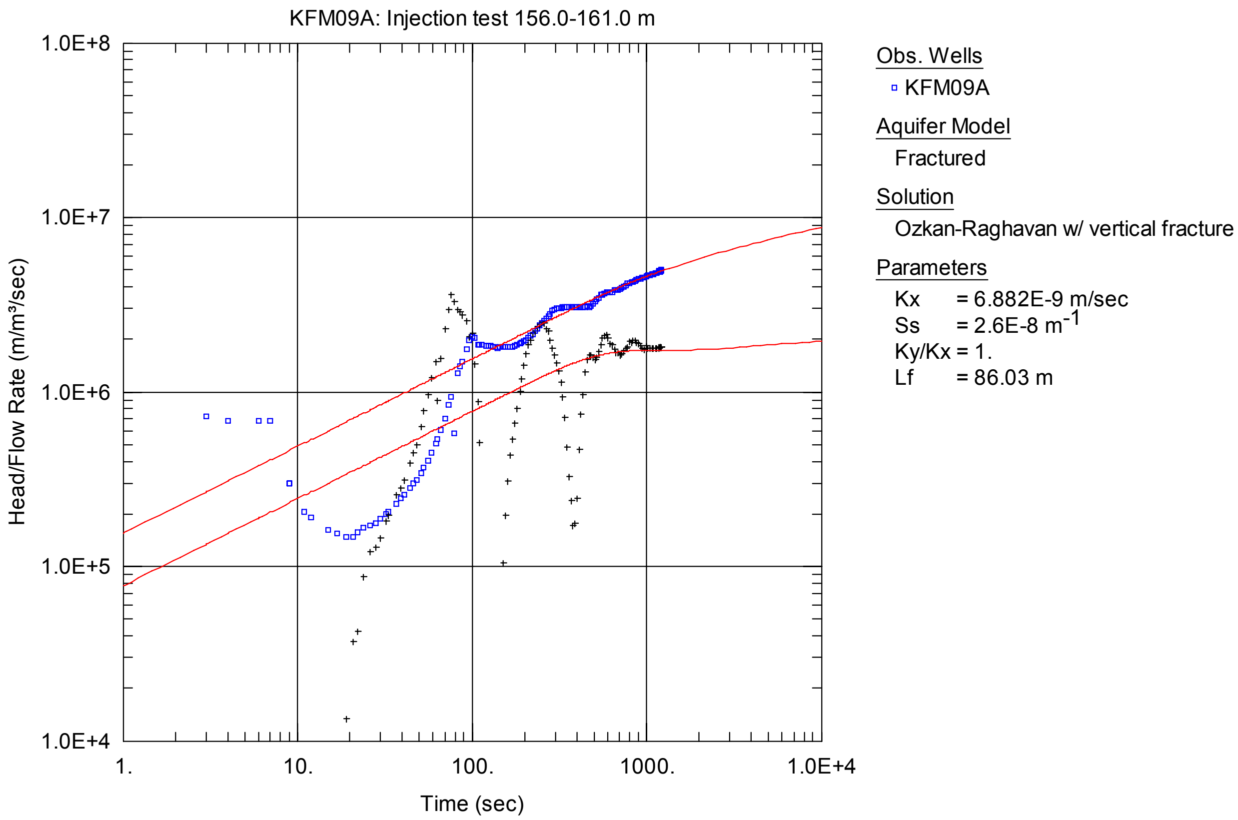


Figure A3-259. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 156.0-161.0 m in KFM09A.

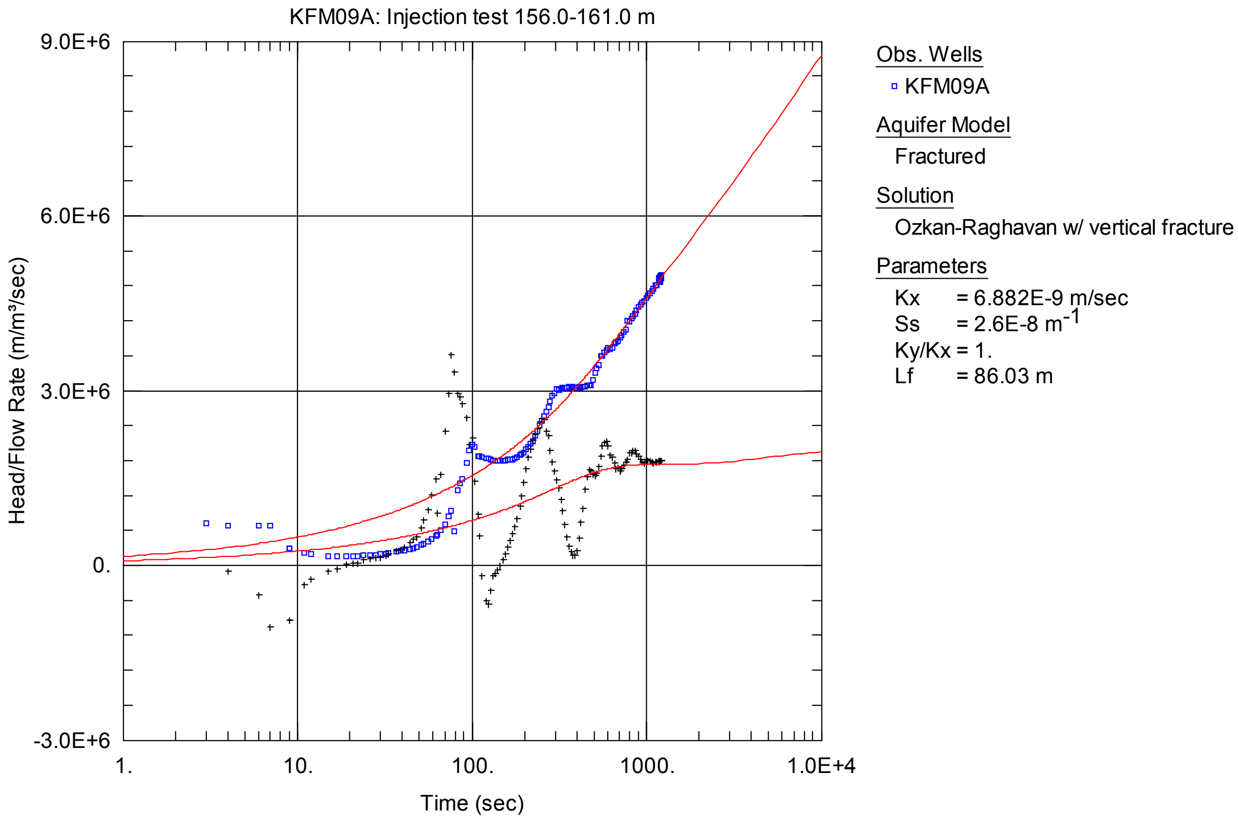


Figure A3-260. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 156.0-161.0 m in KFM09A.*

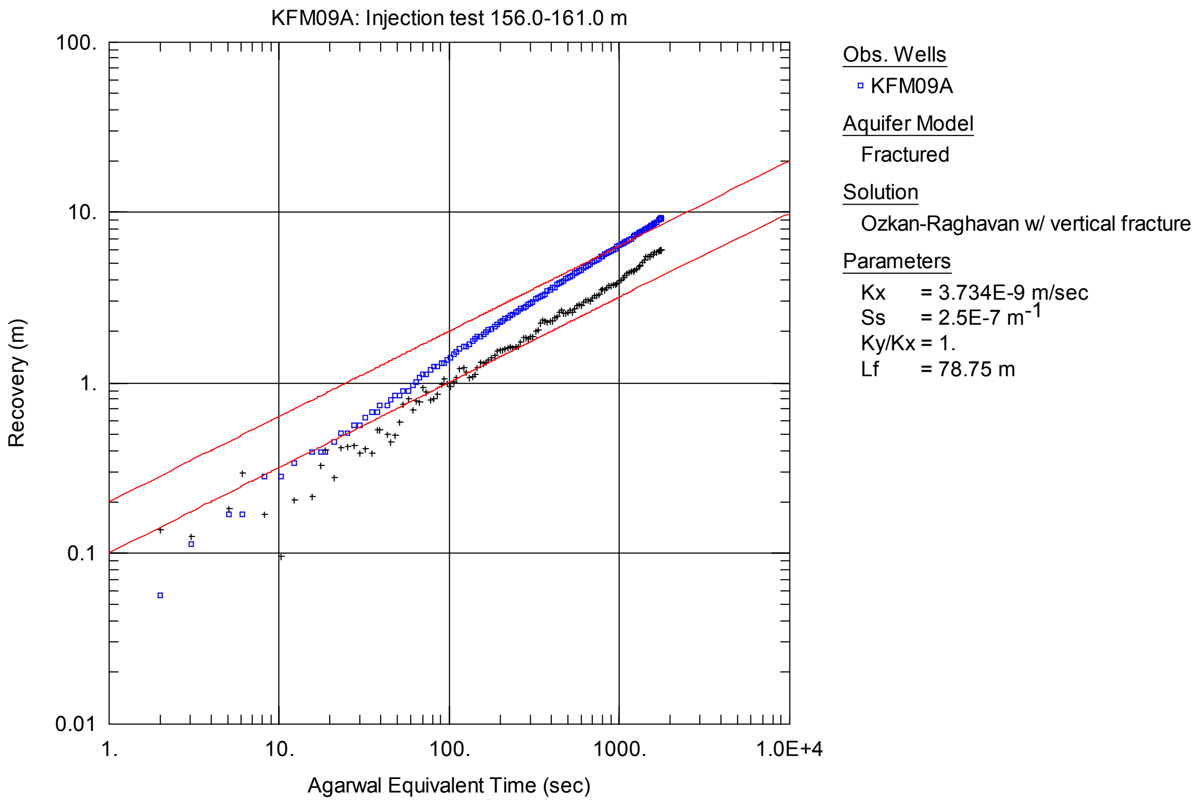


Figure A3-261. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 156.0-161.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.*

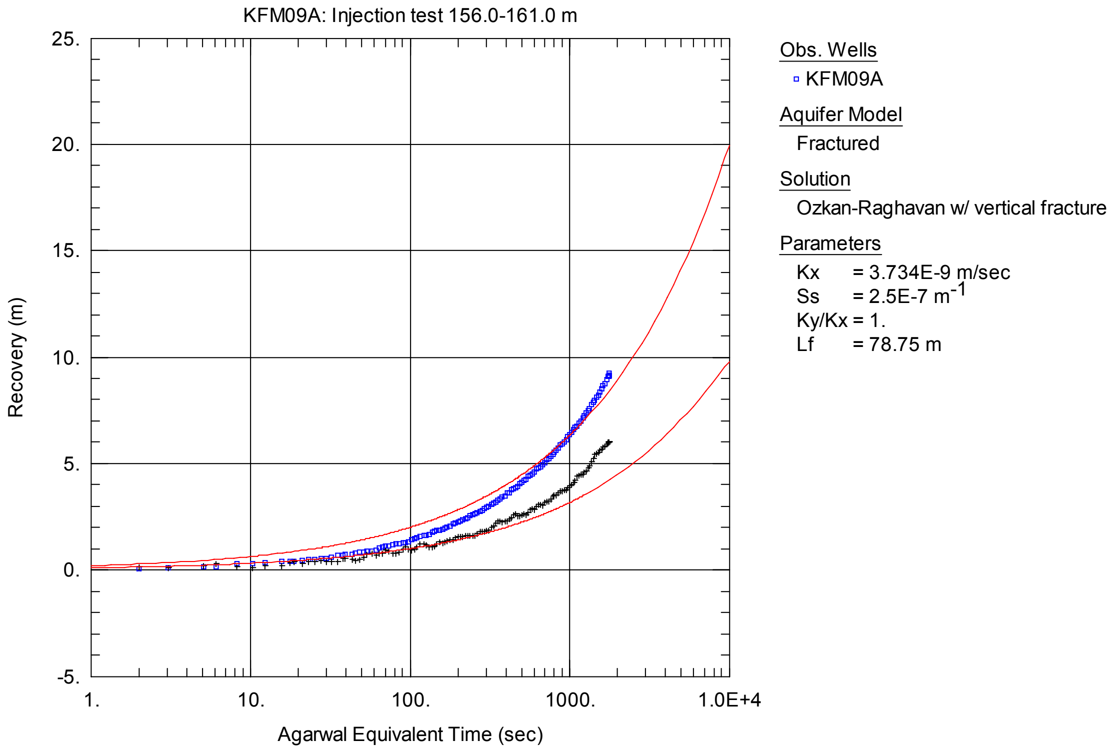


Figure A3-262. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 156.0-161.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.*

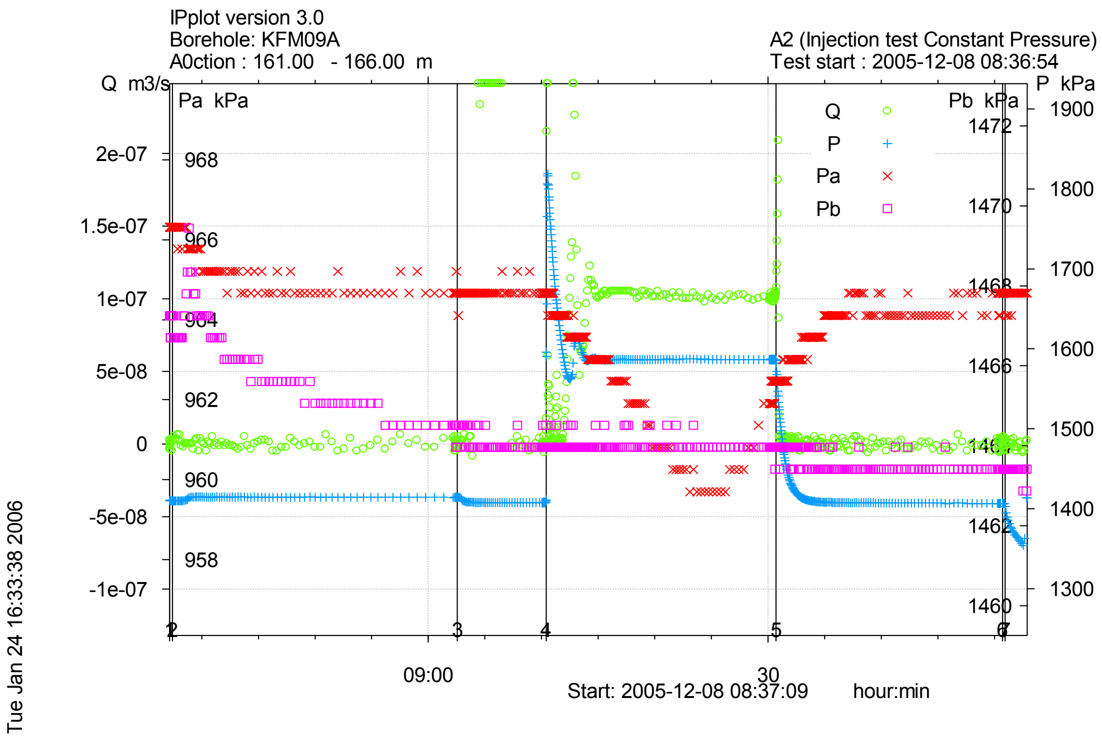


Figure A3-263. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 161.0-166.0 m in borehole KFM09A.*

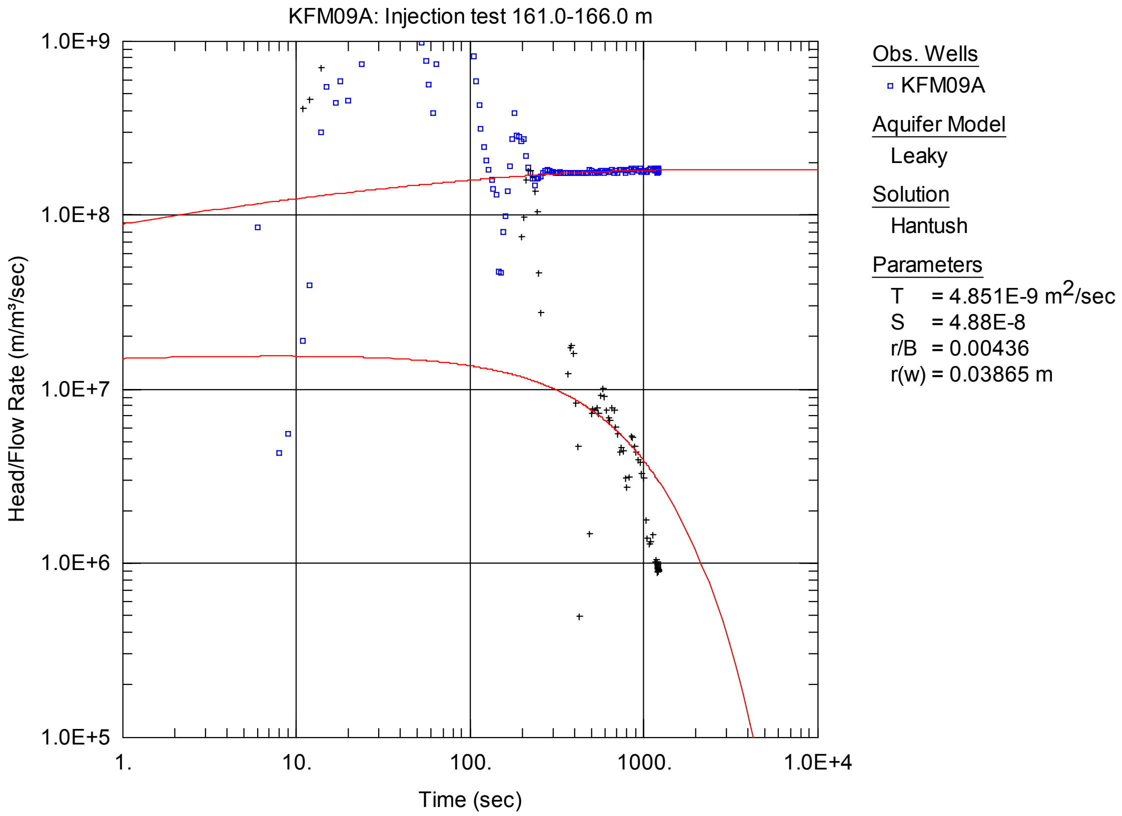


Figure A3-264. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 161.0-166.0 m in KFM09A.*

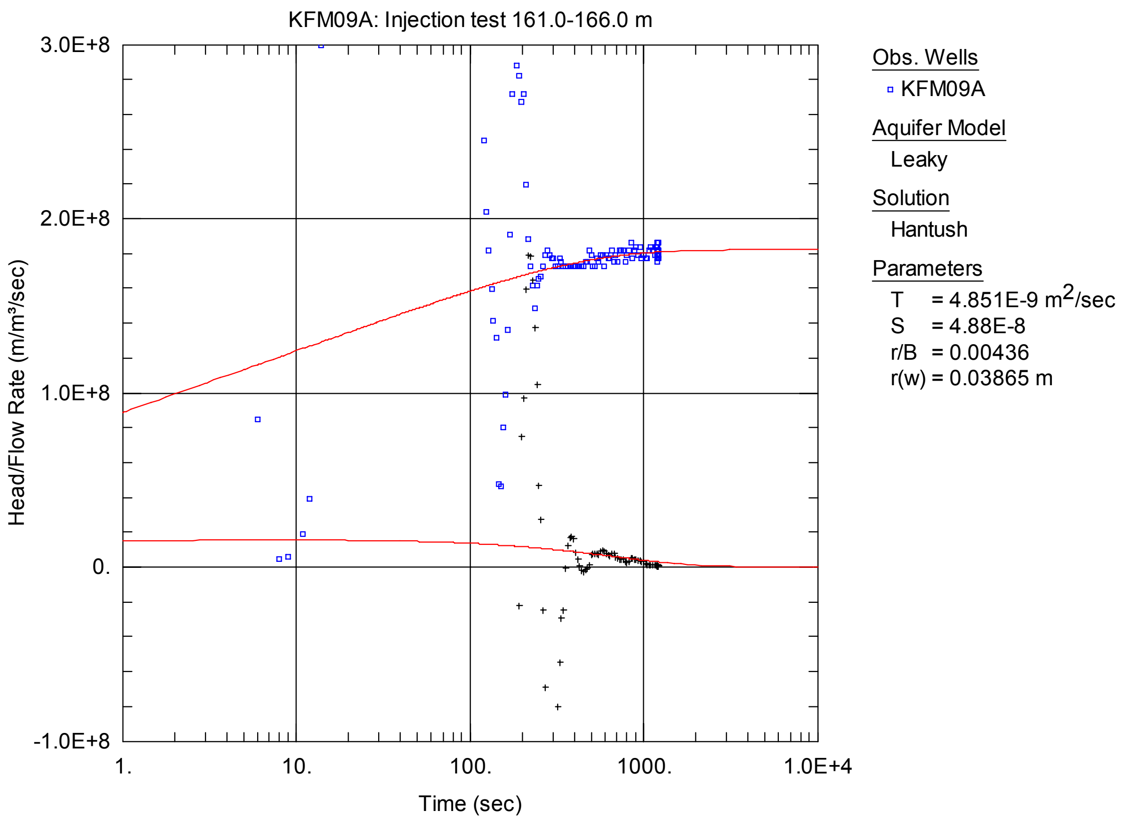


Figure A3-265. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 161.0-166.0 m in KFM09A.*

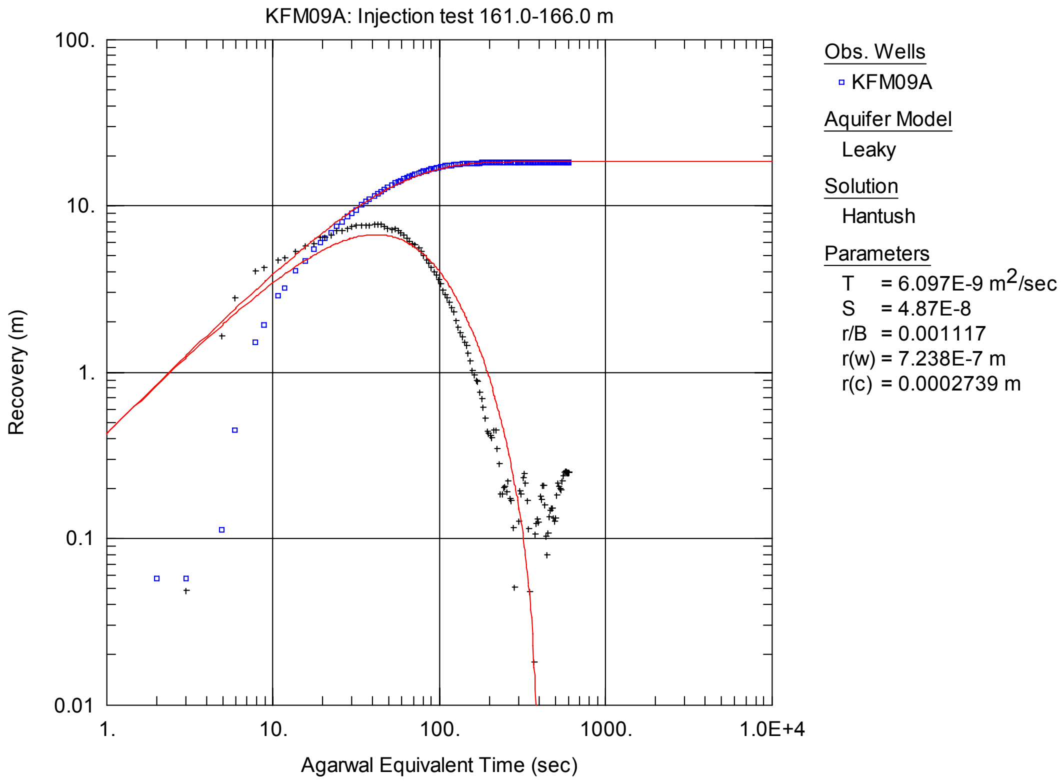


***Figure A3-266.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 161.0-166.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.*

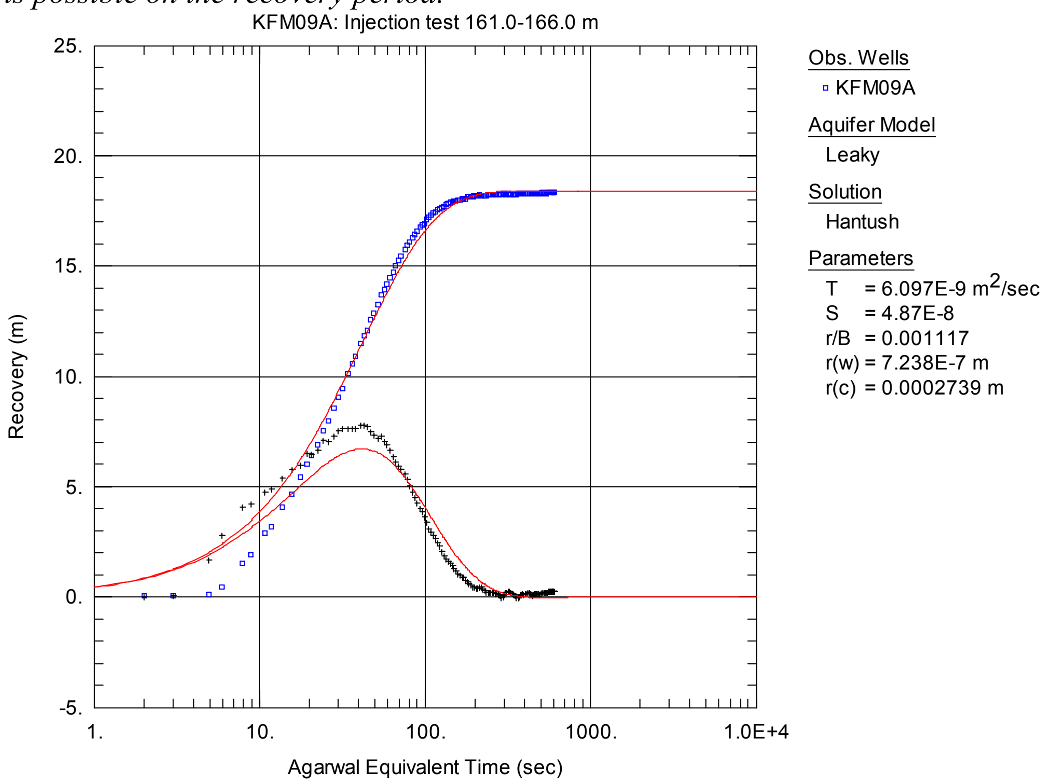


***Figure A3-267.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 161.0-166.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.*

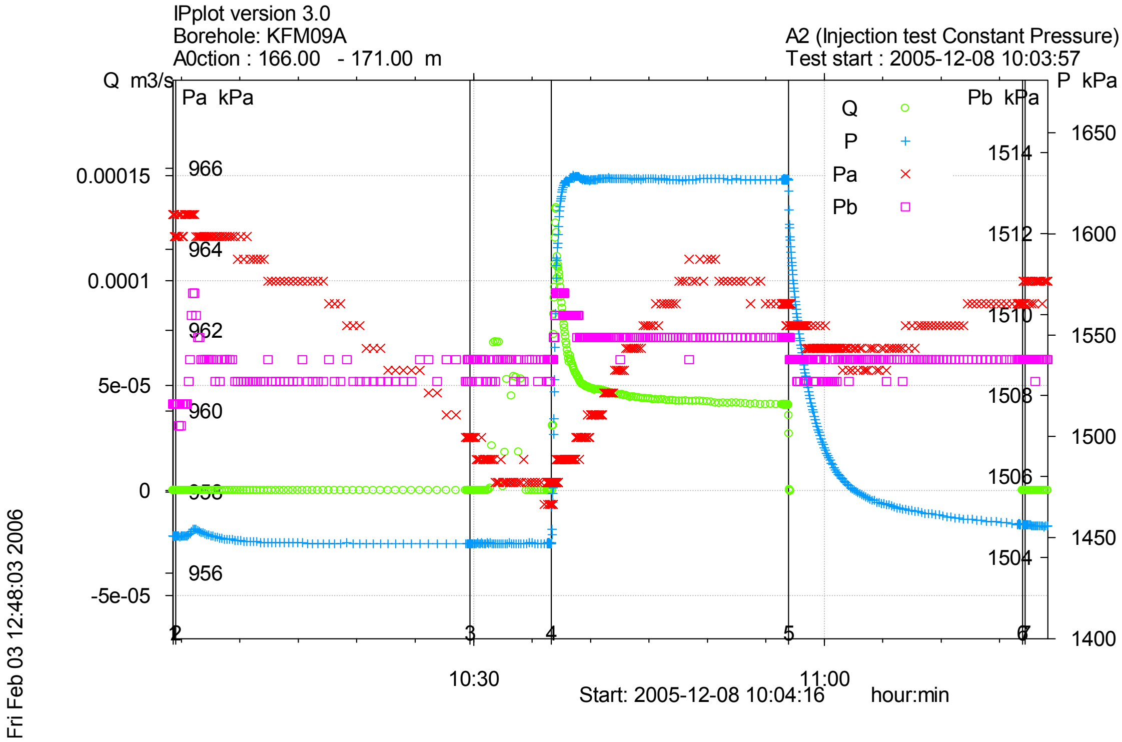


***Figure A3-268.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 166.0-171.0 m in borehole KFM09A.*

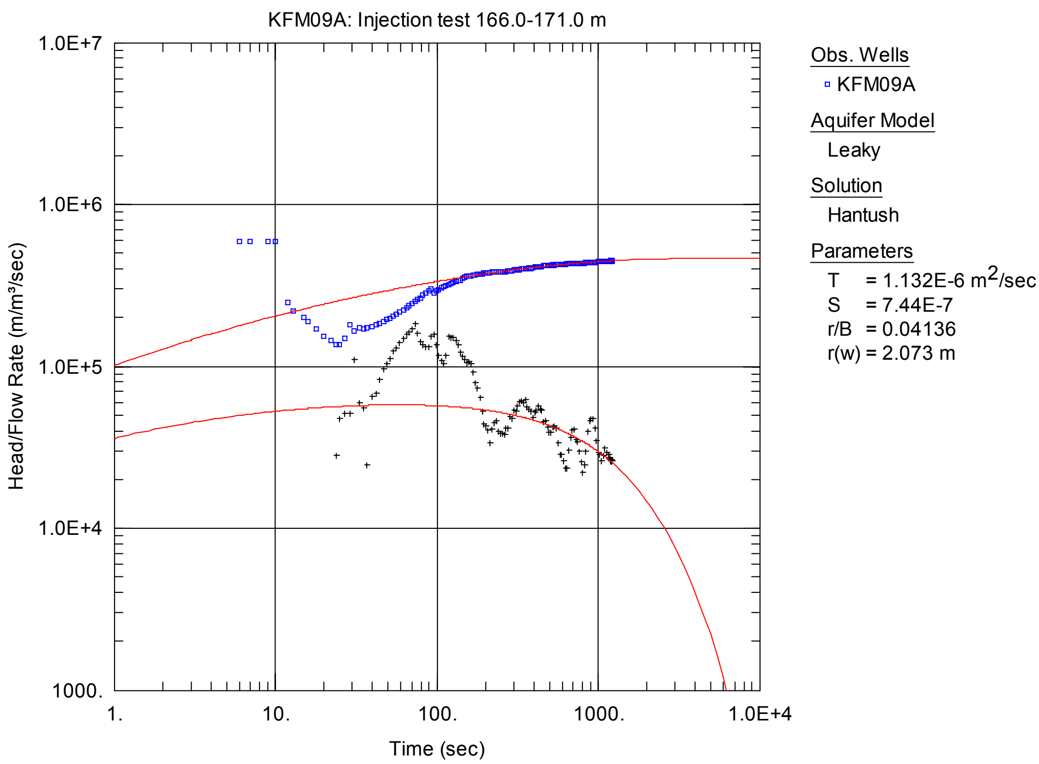


***Figure A3-269.** Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 166.0-171.0 m in KFM09A.*

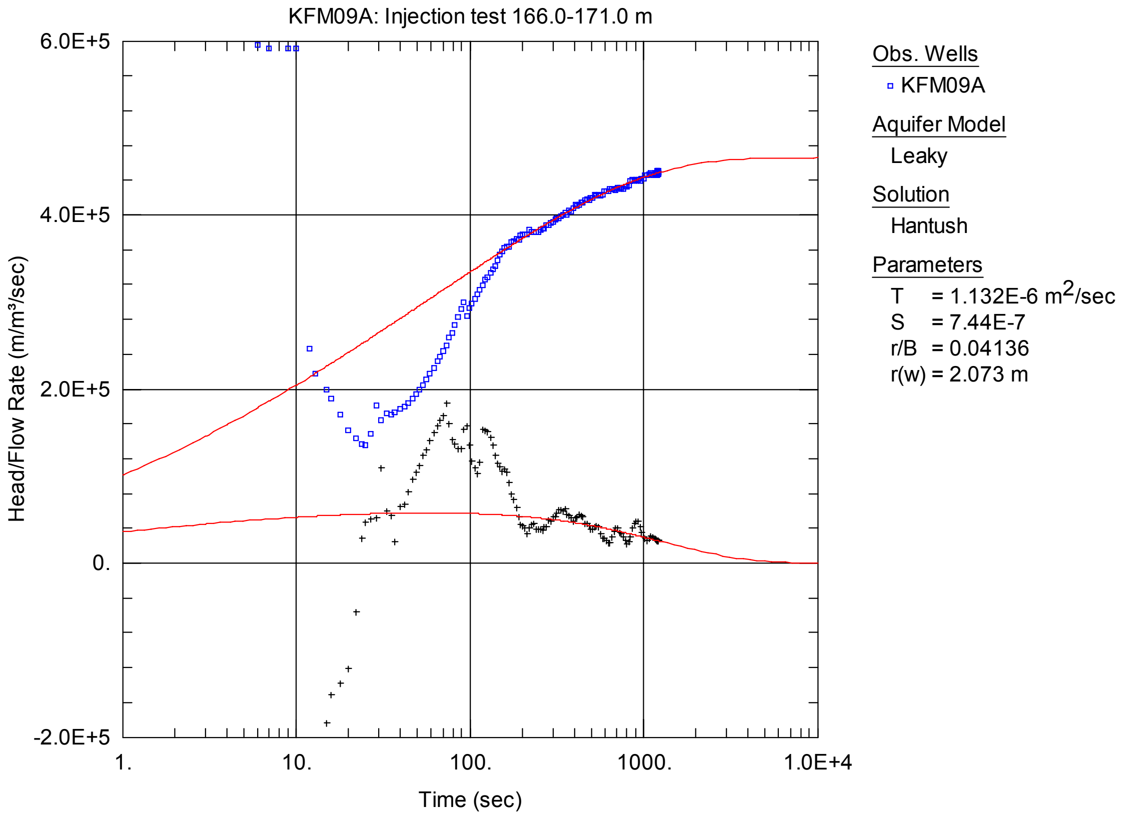


Figure A3-270. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 166.0-171.0 m in KFM09A.*

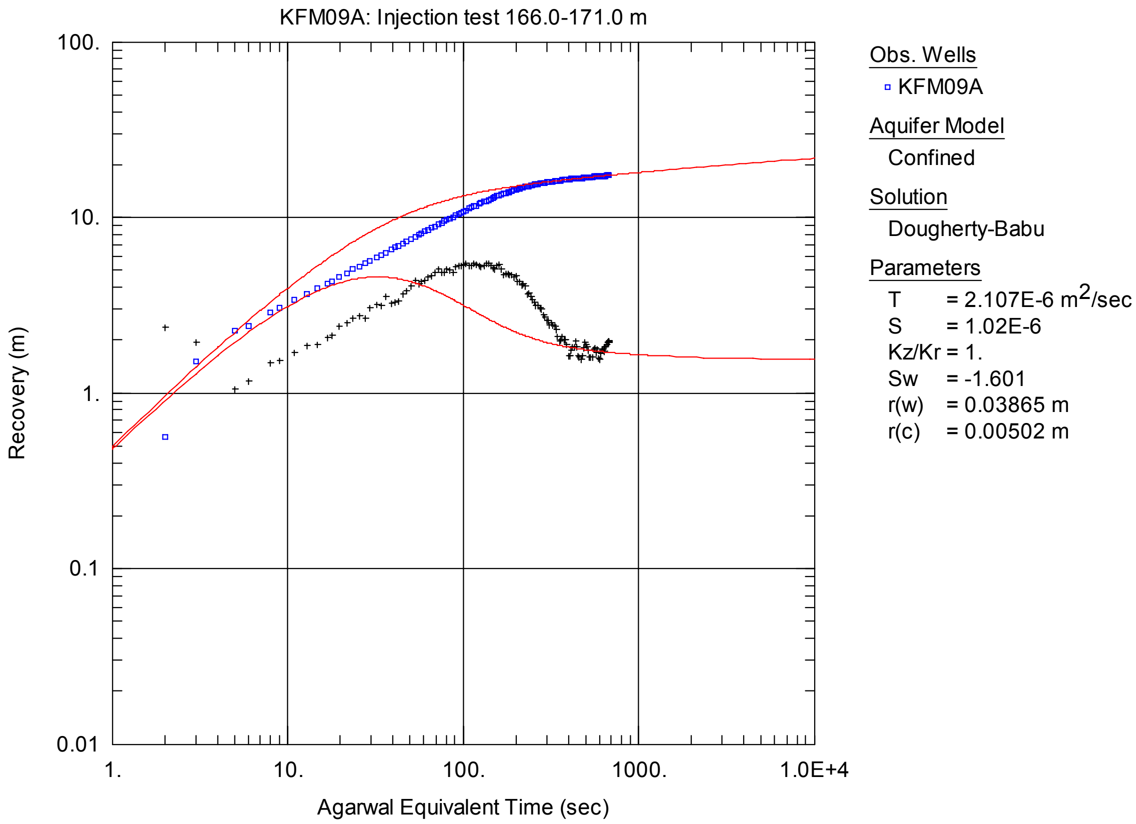


Figure A3-271. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 166.0-171.0 m in KFM09A.*

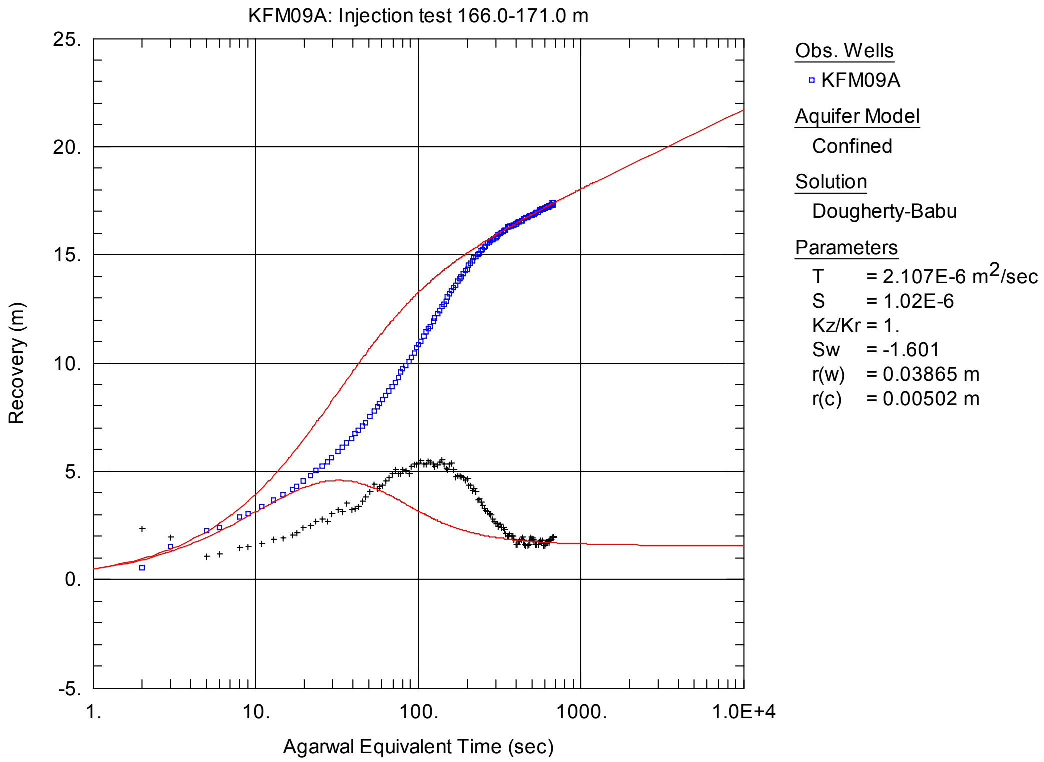


Figure A3-272. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 166.0-171.0 m in KFM09A.*

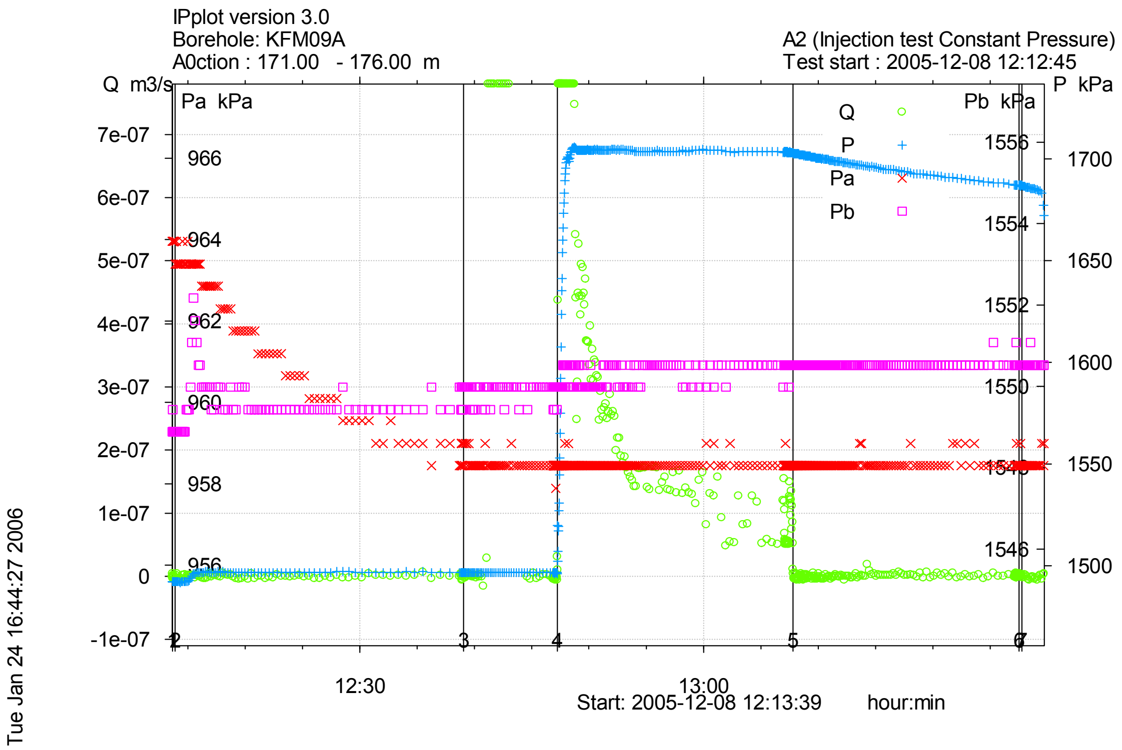


Figure A3-273. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 171.0-176.0 m in borehole KFM09A*

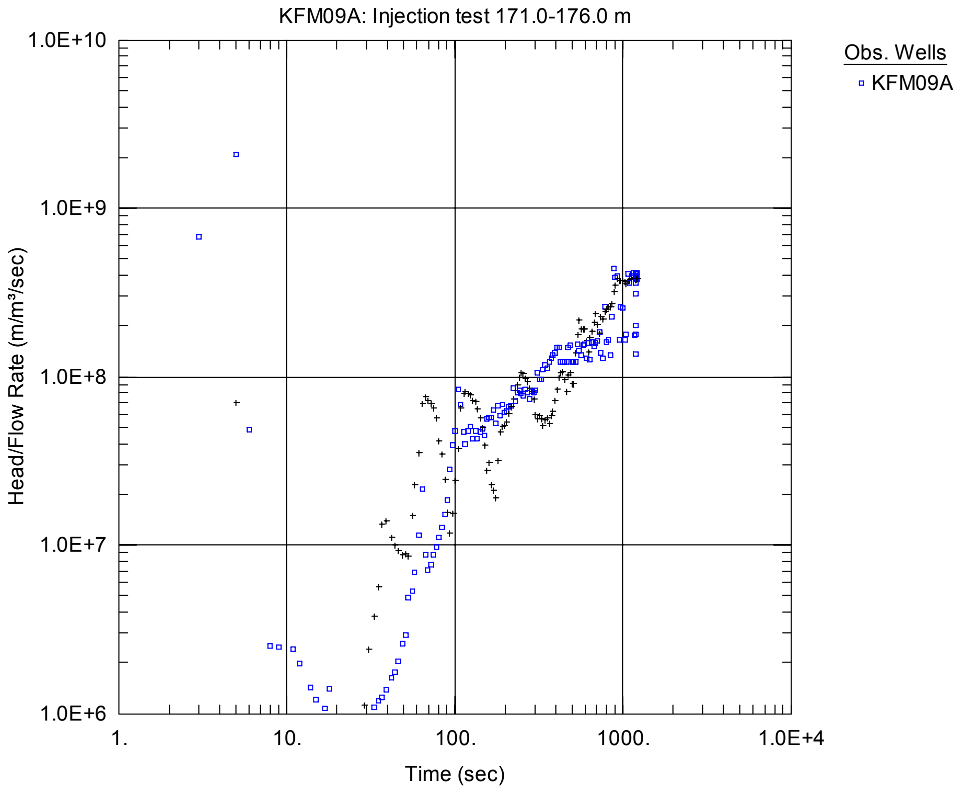


Figure A3-274. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 171.0-176.0 m in KFM09A.*

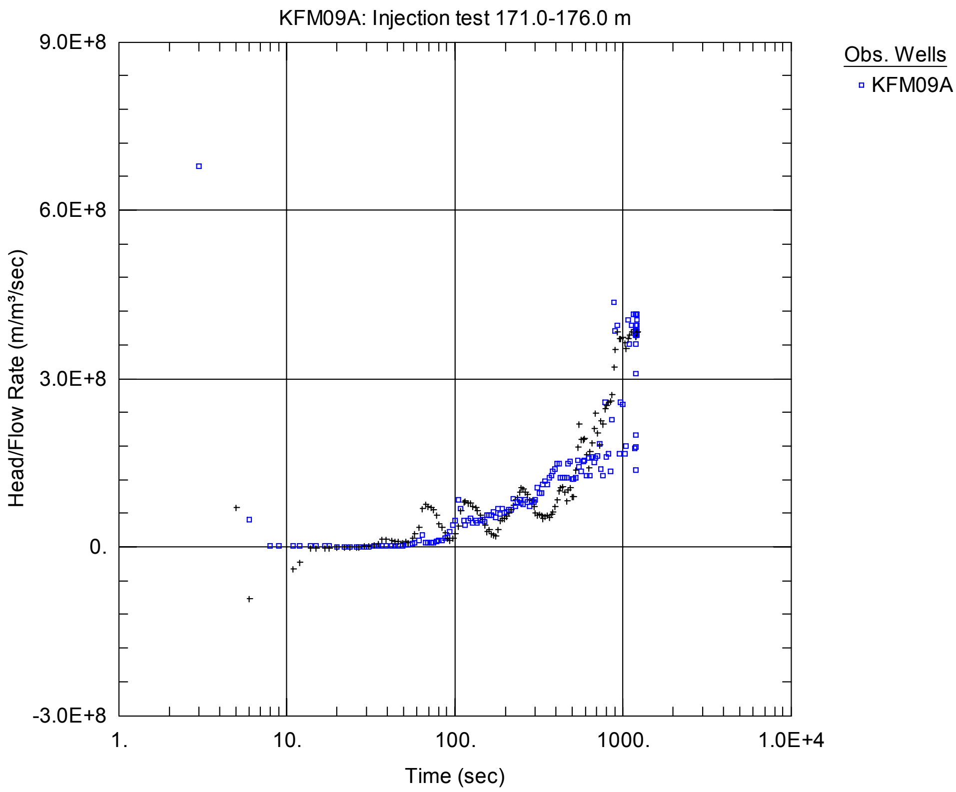


Figure A3-275. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 171.0-176.0 m in KFM09A.*

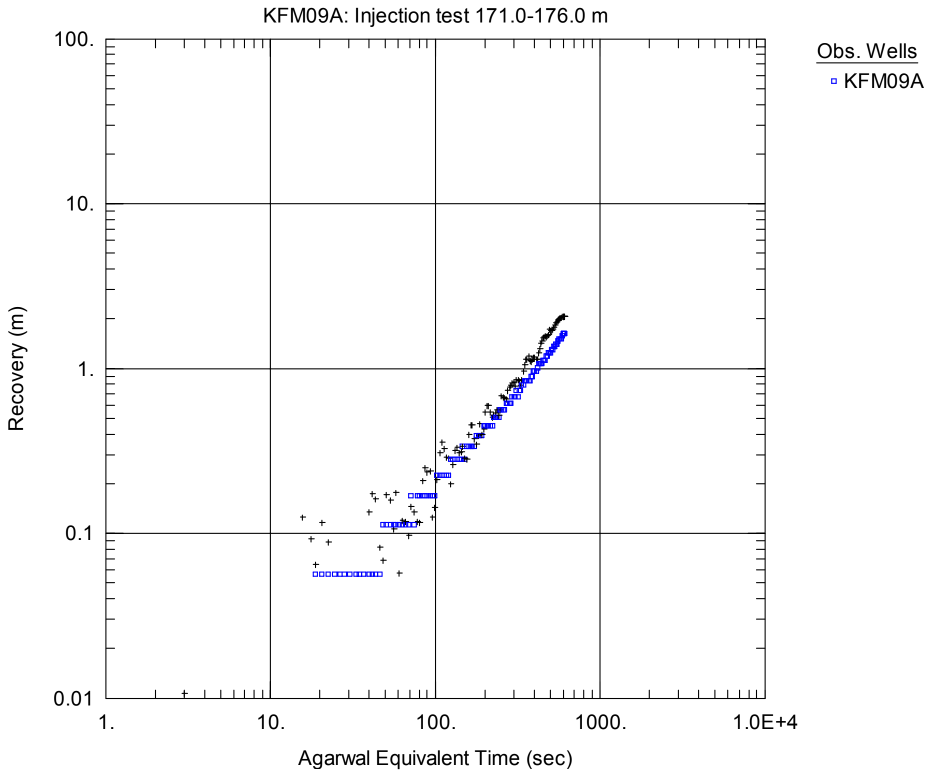


Figure A3-276. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 171.0-176.0 m in KFM09A.*

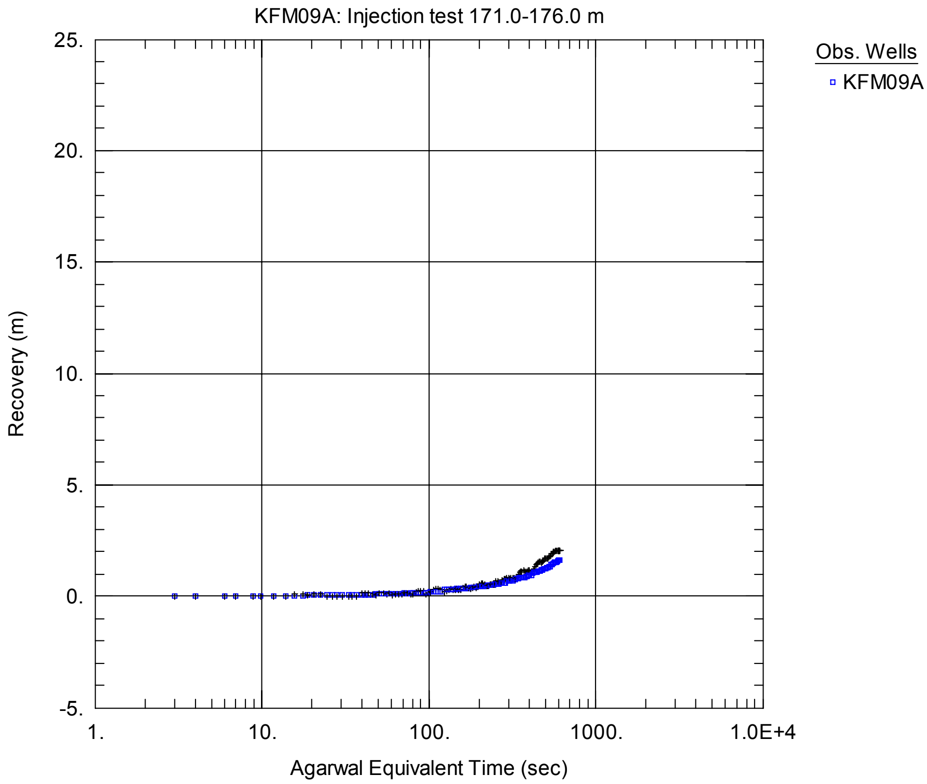


Figure A3-277. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 171.0-176.0 m in KFM09A.*

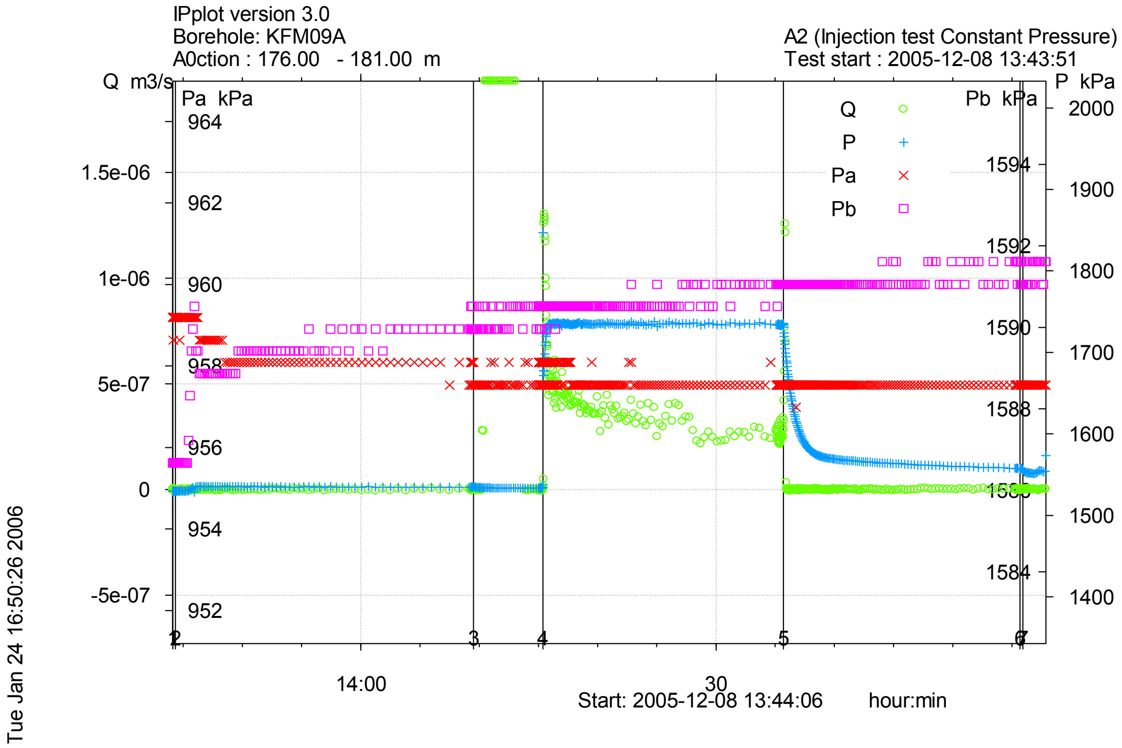


Figure A3-278. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 176.0-181.0 m in borehole KFM09A.*

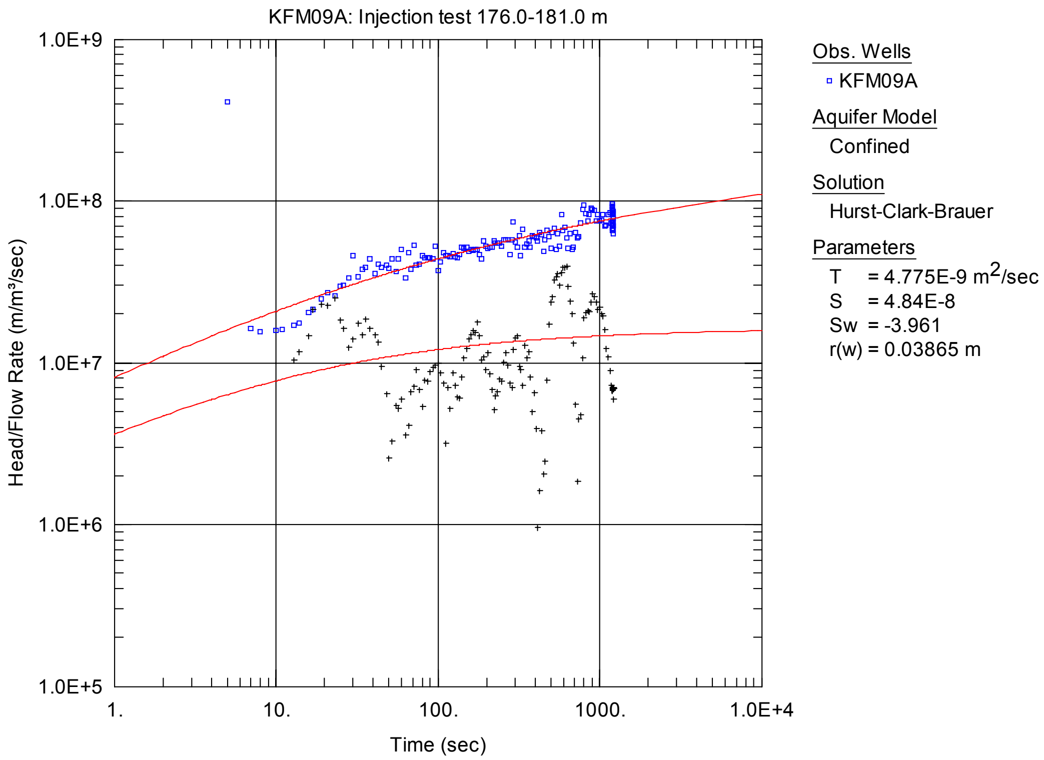


Figure A3-279. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 176.0-181.0 m in KFM09A.*

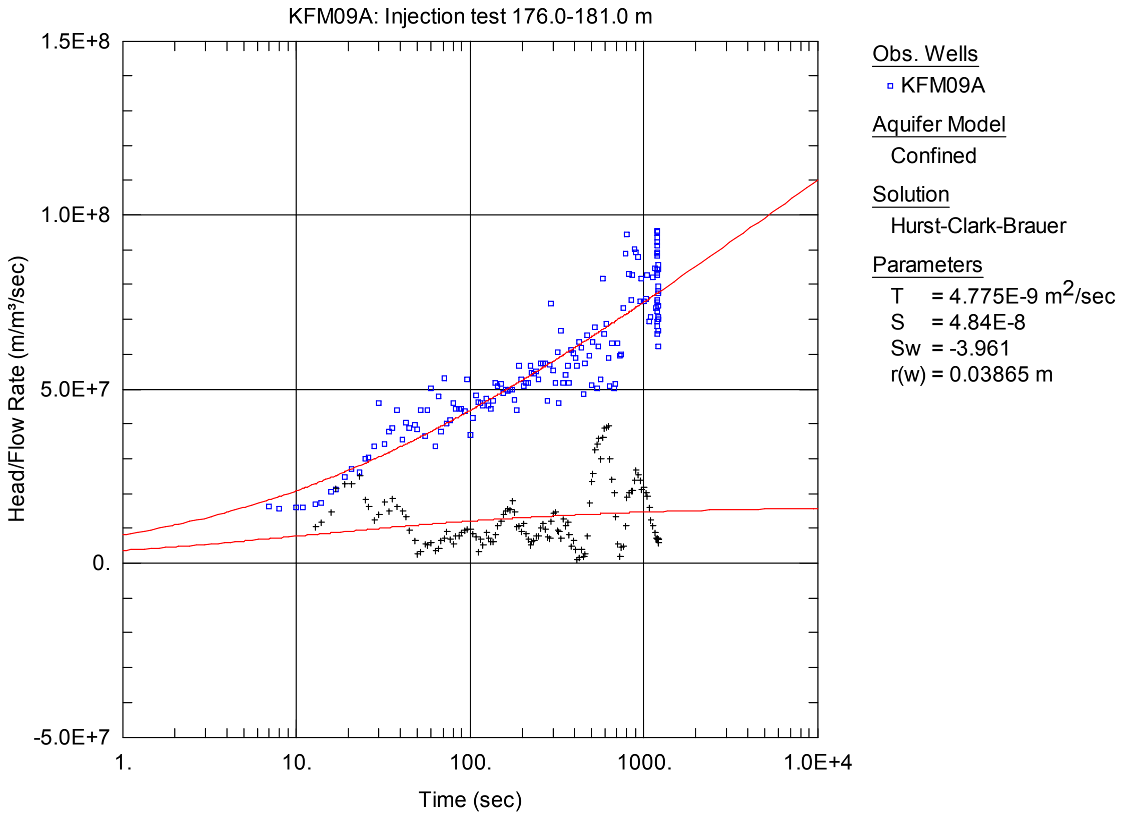


Figure A3-280. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 176.0-181.0 m in KFM09A.*

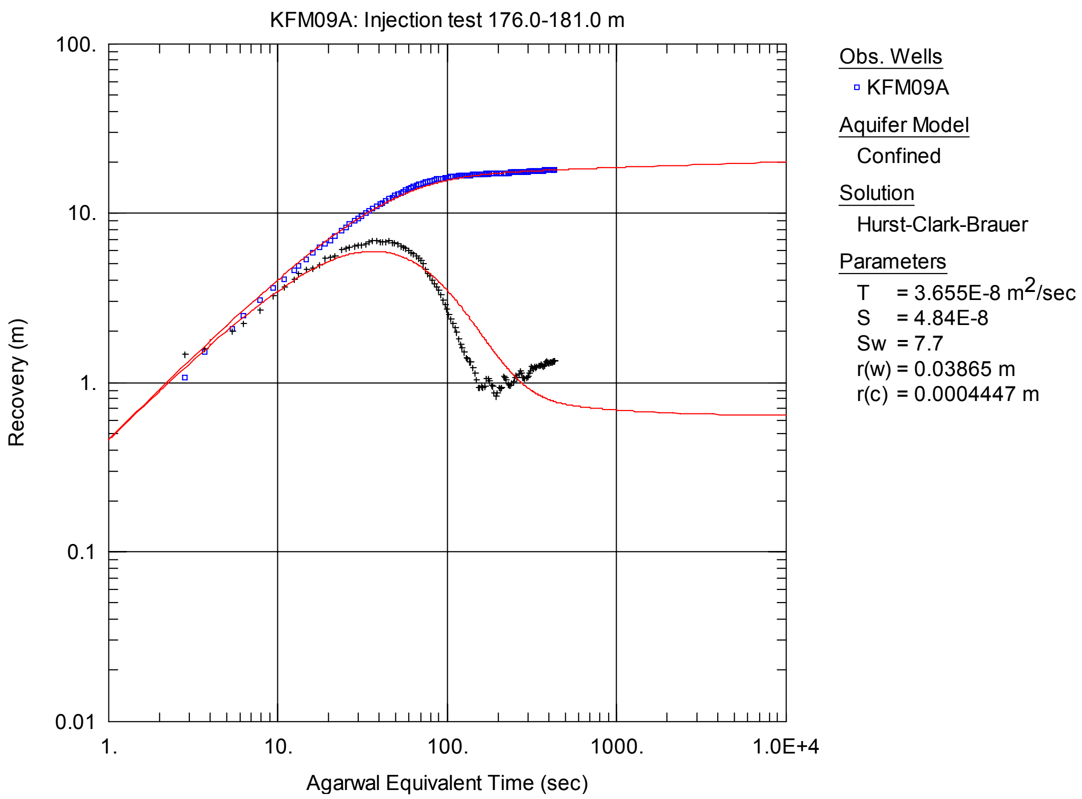


Figure A3-281. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 176.0-181.0 m in KFM09A No unambiguous transient evaluation is possible on the recovery period.*

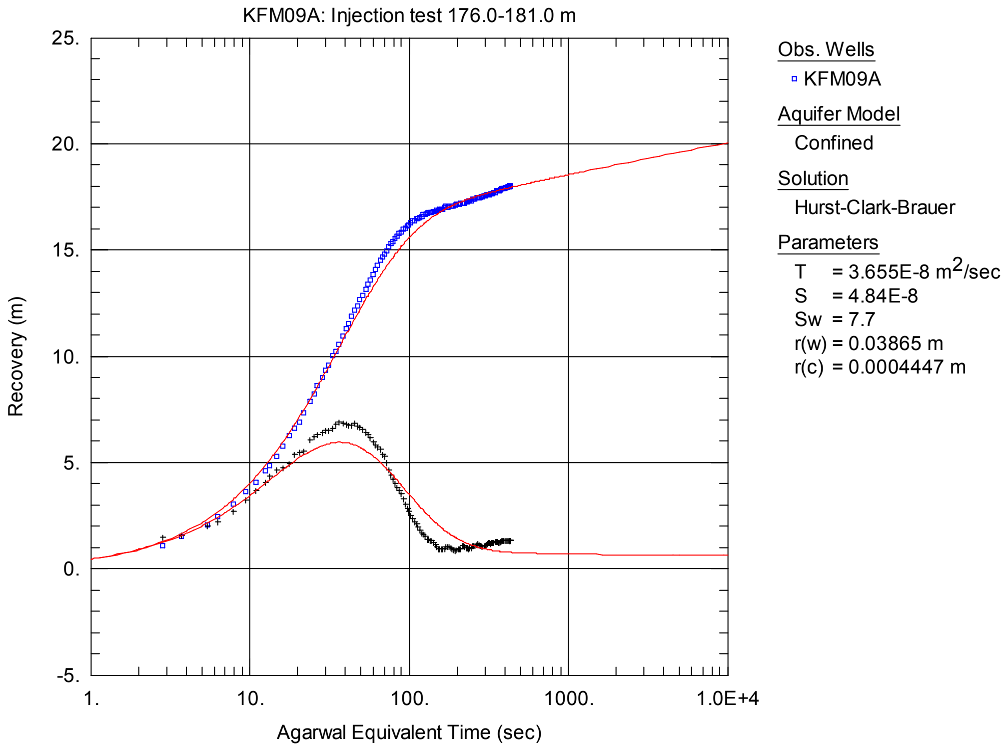


***Figure A3-282.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 176.0-181.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.*

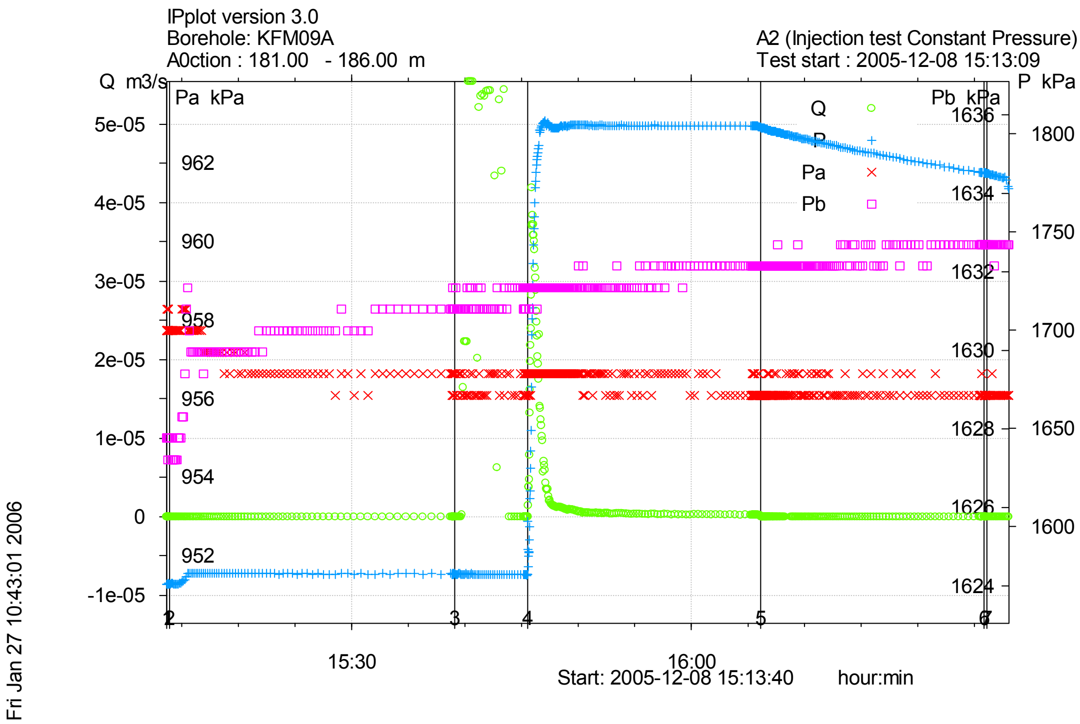


***Figure A3-283.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 181.0-186.0 m in borehole KFM09A.*

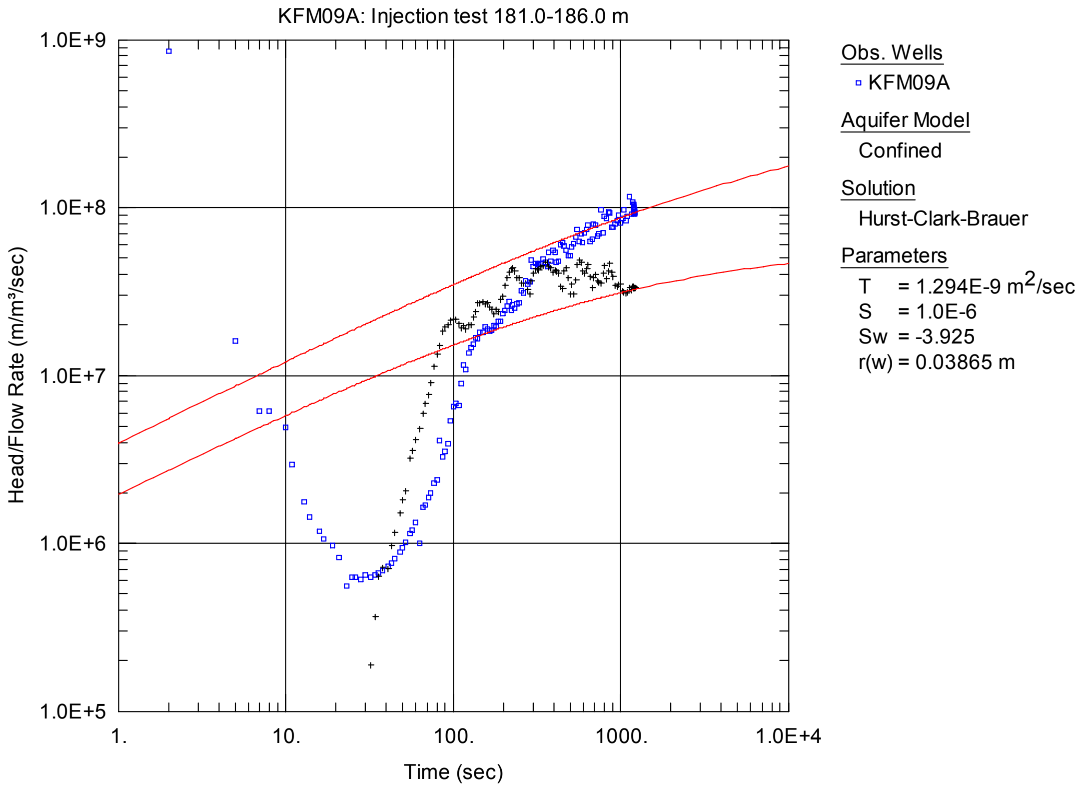


Figure A3-284. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 181.0-186.0 m in KFM09A. A fit with Hurst-Clark-Brauer is not possible and no transient evaluation is possible on the injection.*

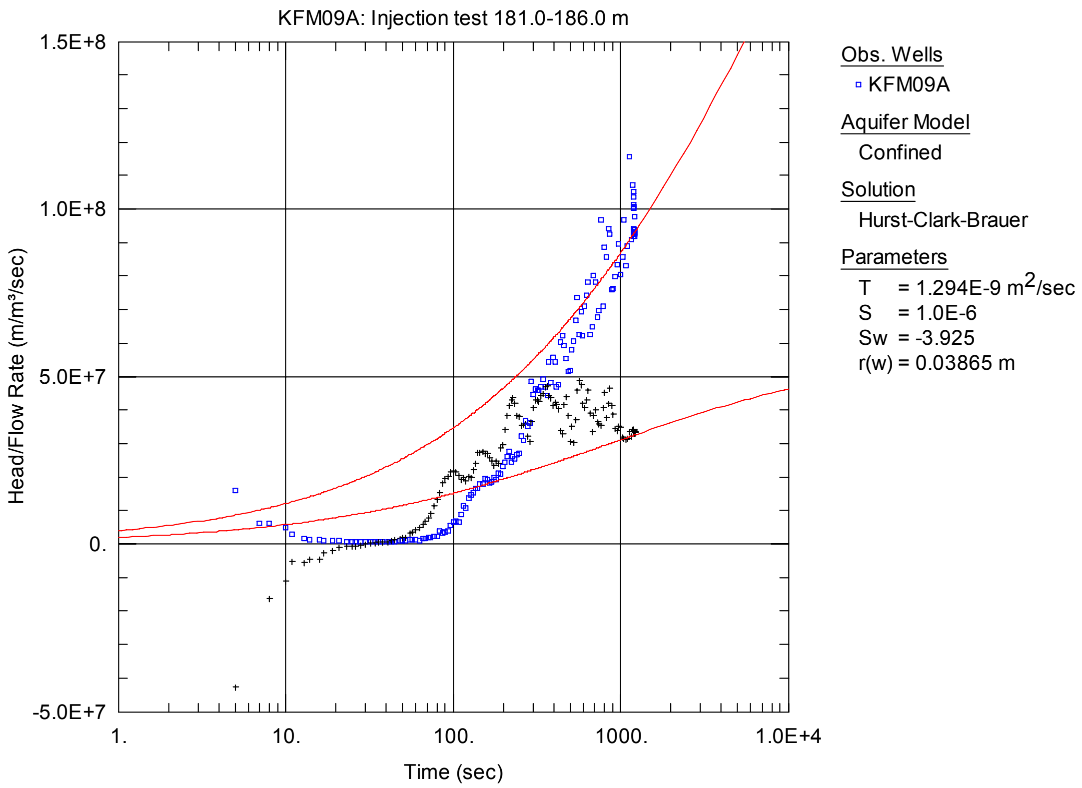


Figure A3-285. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 181.0-186.0 m in KFM09A. A fit with Hurst-Clark-Brauer is not possible and no transient evaluation is possible on the injection.*

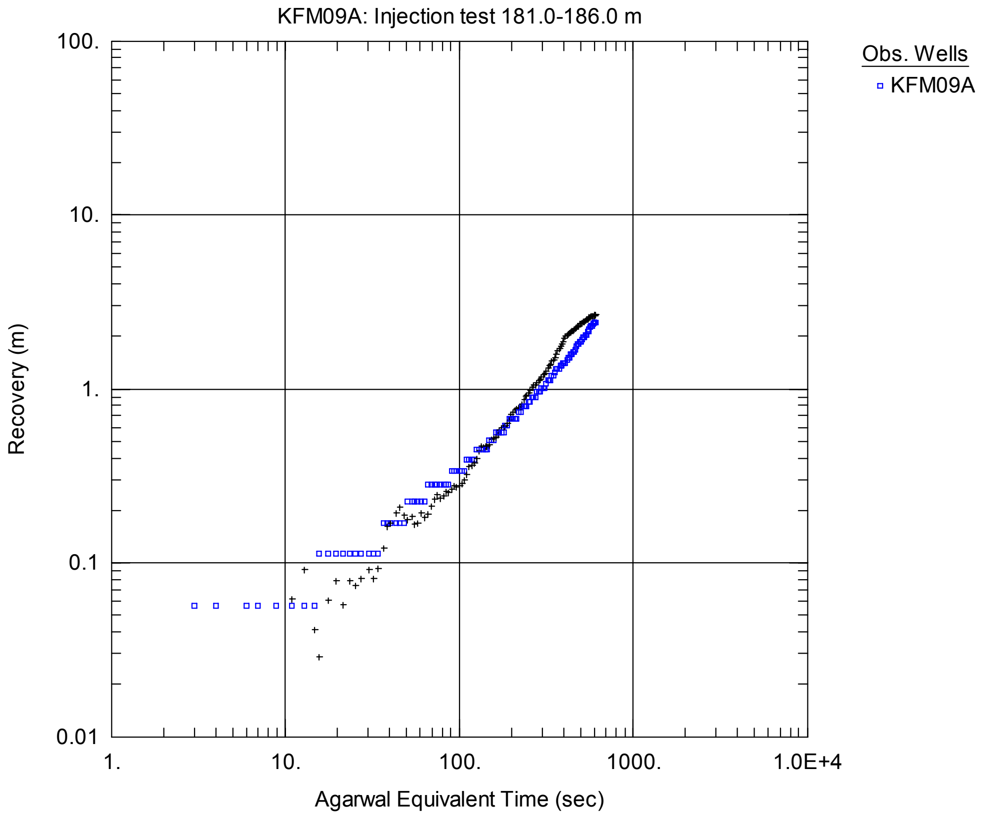


Figure A3-286. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 181.0-186.0 m in KFM09A.*

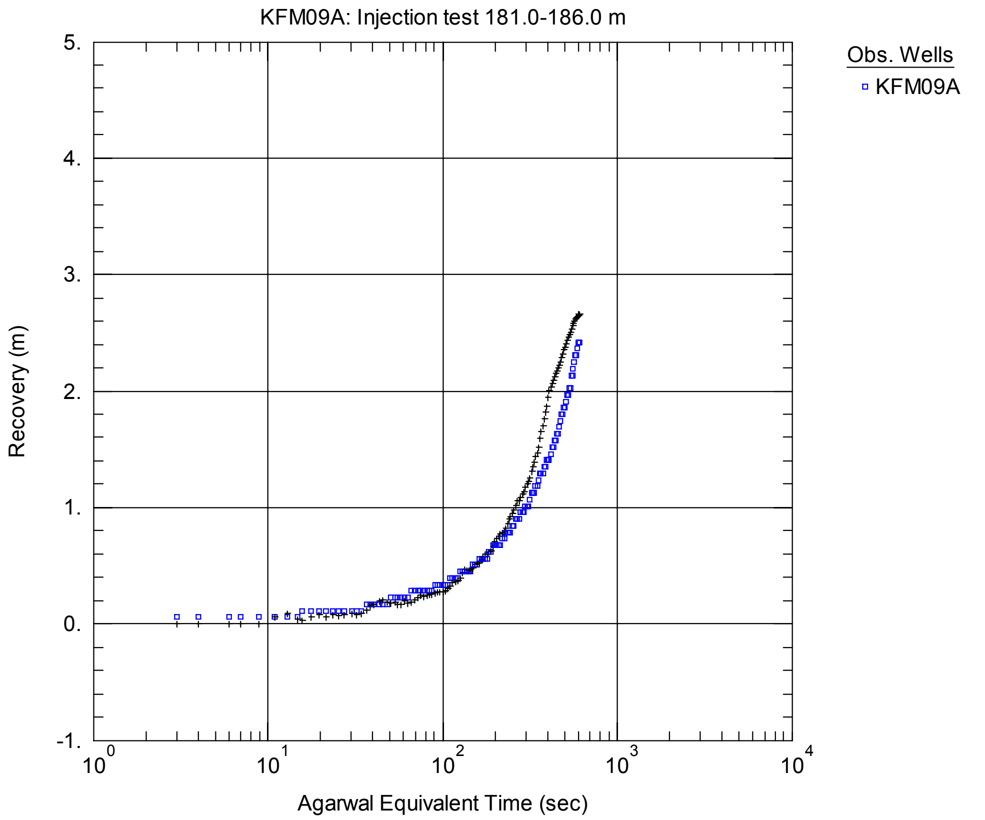


Figure A3-287. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 181.0-186.0 m in KFM09A.*

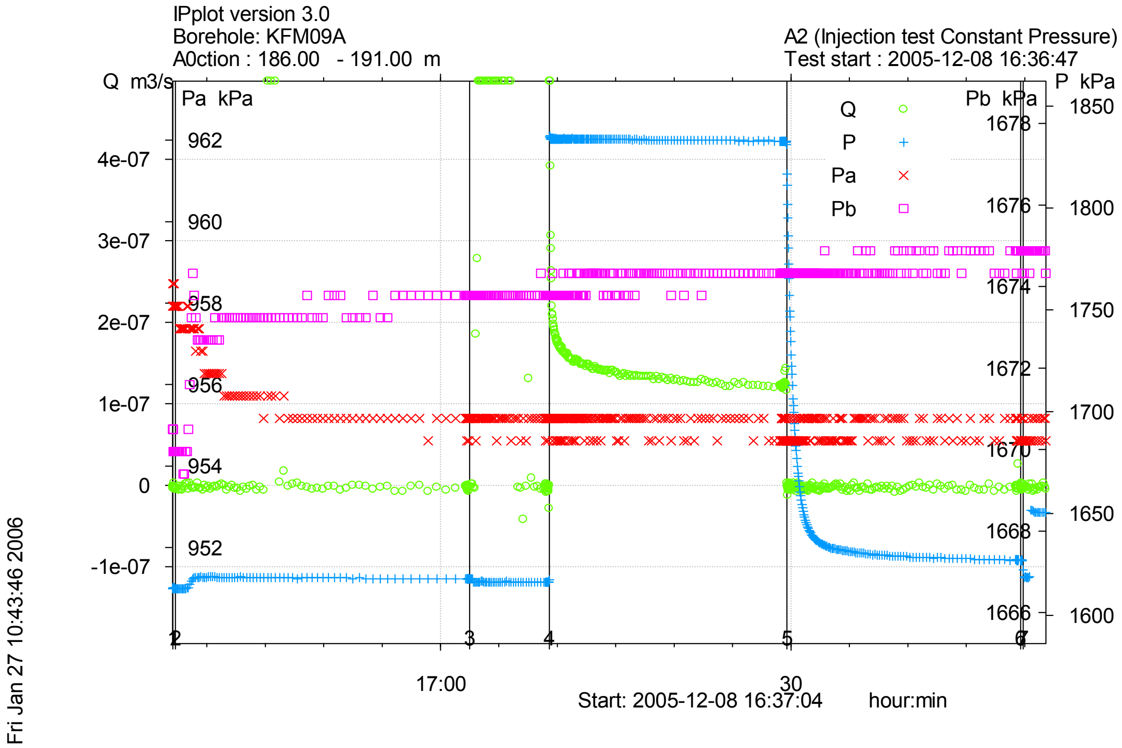


Figure A3-288. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 186.0-191.0 m in borehole KFM09A.*

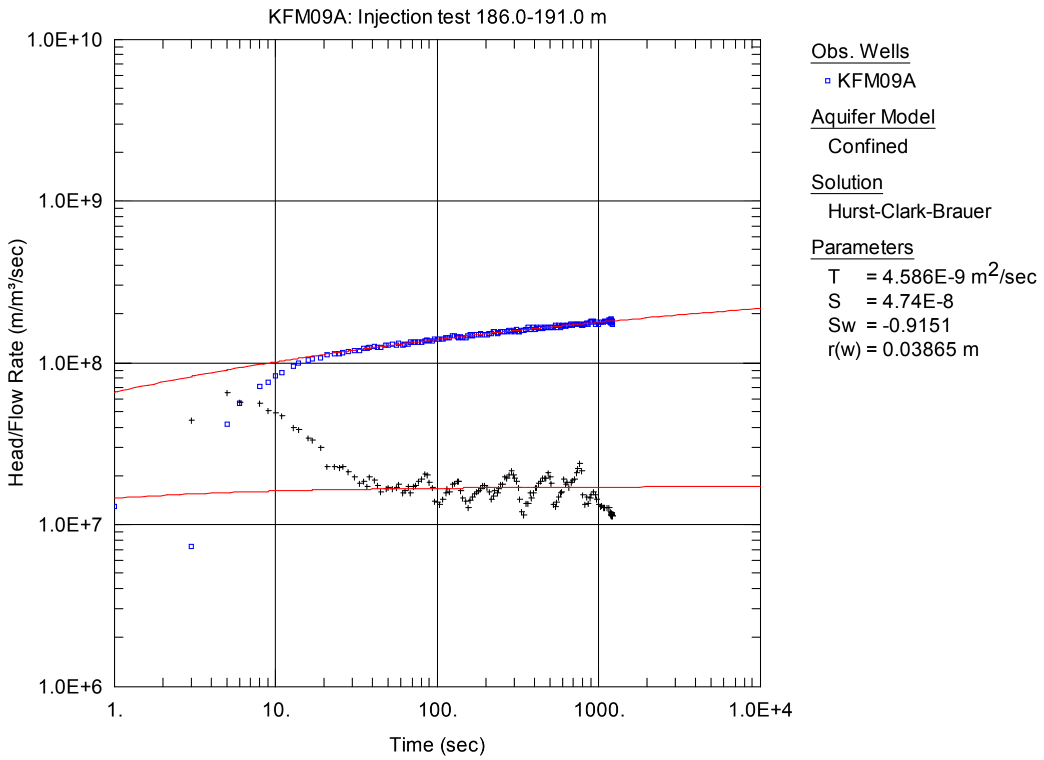


Figure A3-289. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 186.0-191.0 m in KFM09A.*

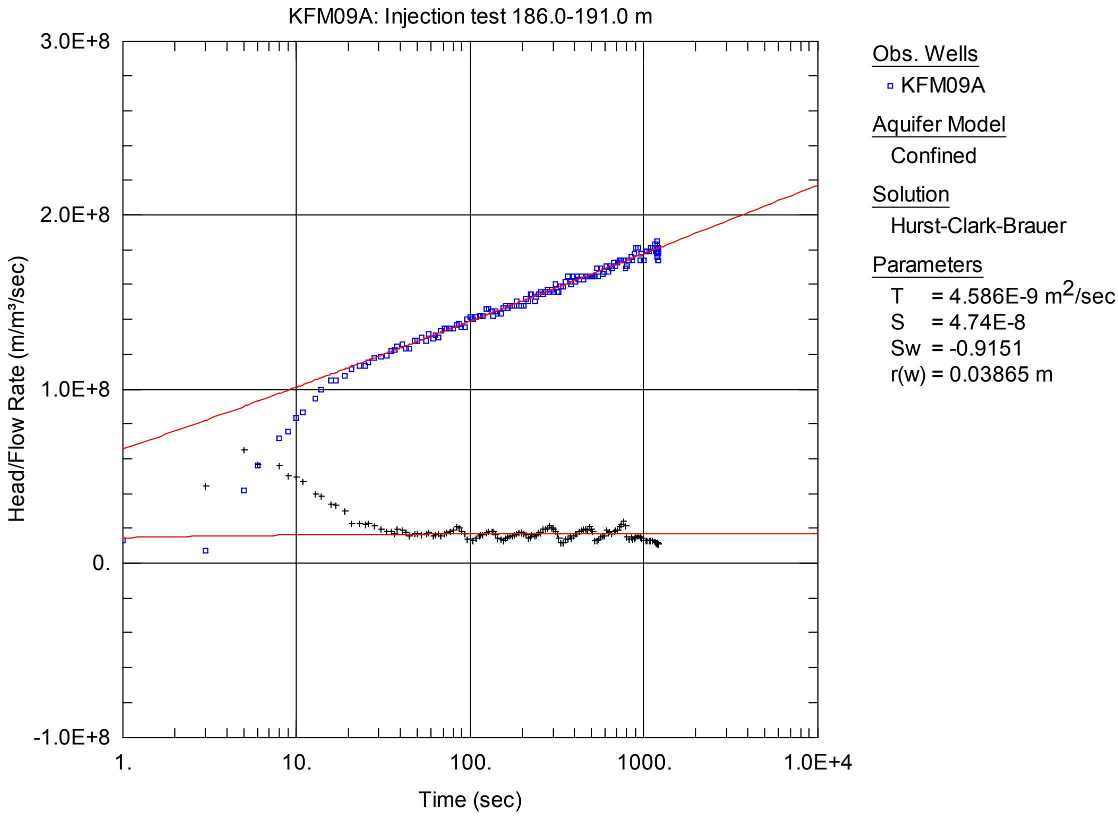


Figure A3-290. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 186.0-191.0 m in KFM09A.*

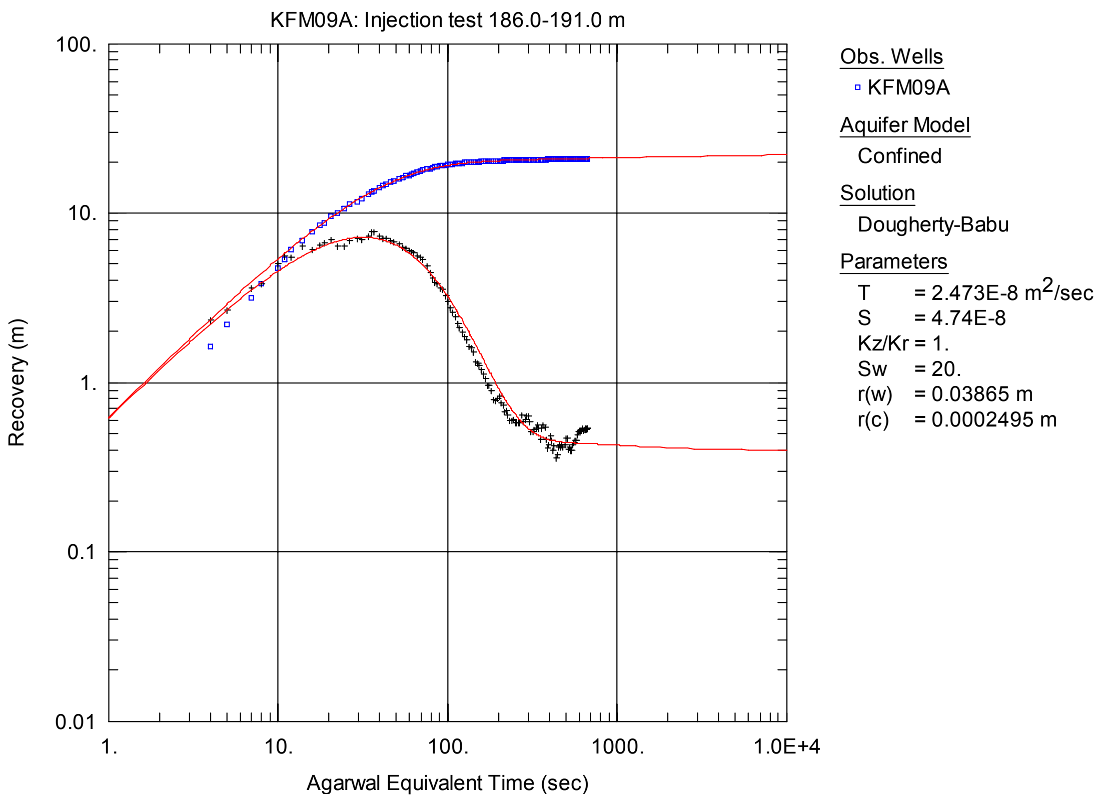


Figure A3-291. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 186.0-191.0 m in KFM09A. The transient evaluation on the recovery period is not regarded as representative.*

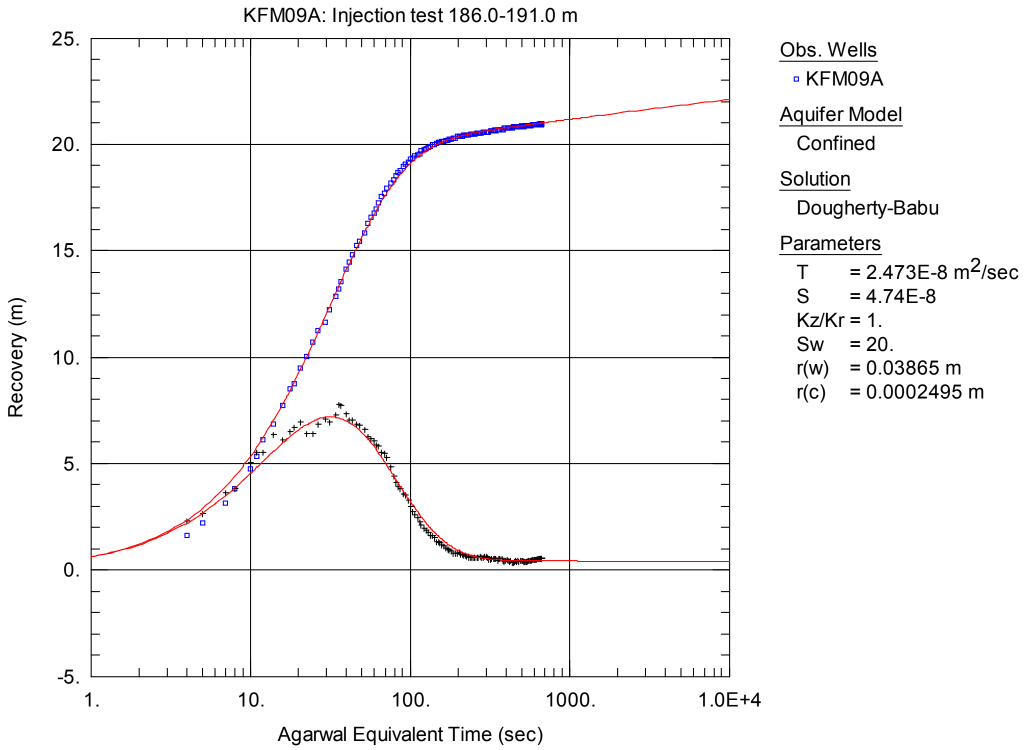


***Figure A3-292.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 186.0-191.0 m in KFM09A. The transient evaluation on the recovery period is not regarded as representative.*

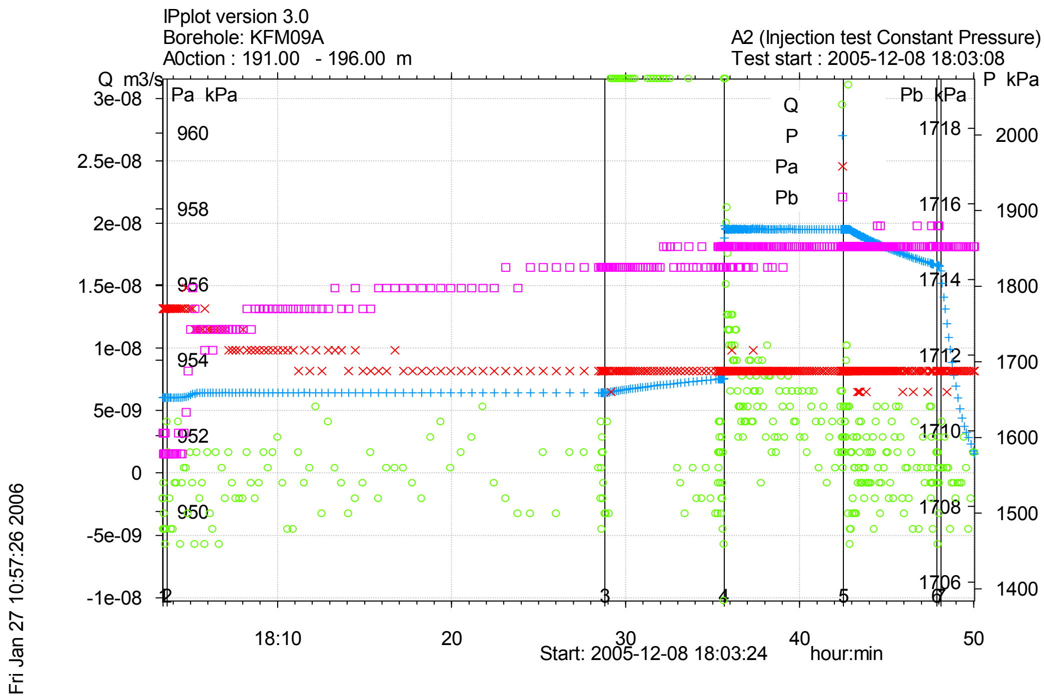


***Figure A3-293.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 191.0-196.0 m in borehole KFM09A.*

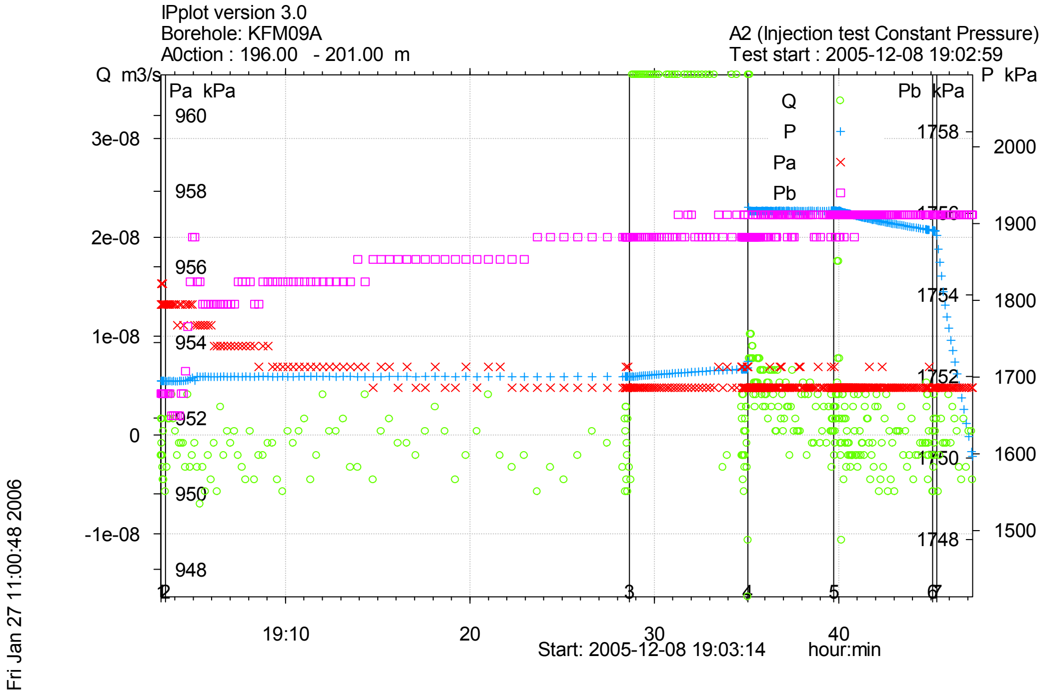


Figure A3-294. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 196.0-201.0 m in borehole KFM09A.*

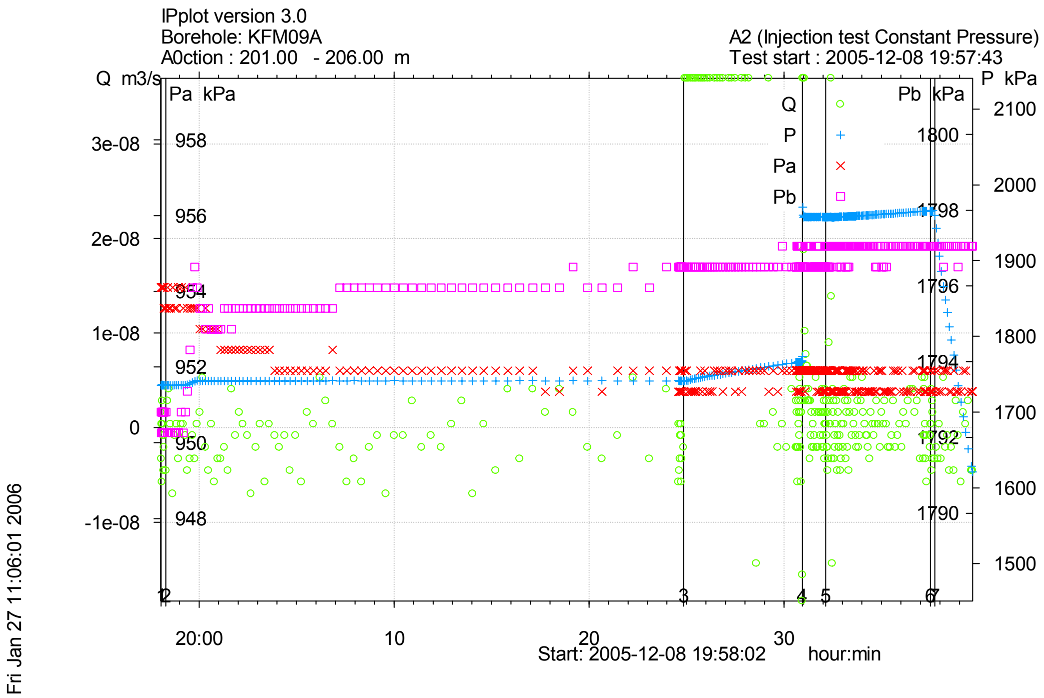


Figure A3-295. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 201.0-206.0 m in borehole KFM09A.*

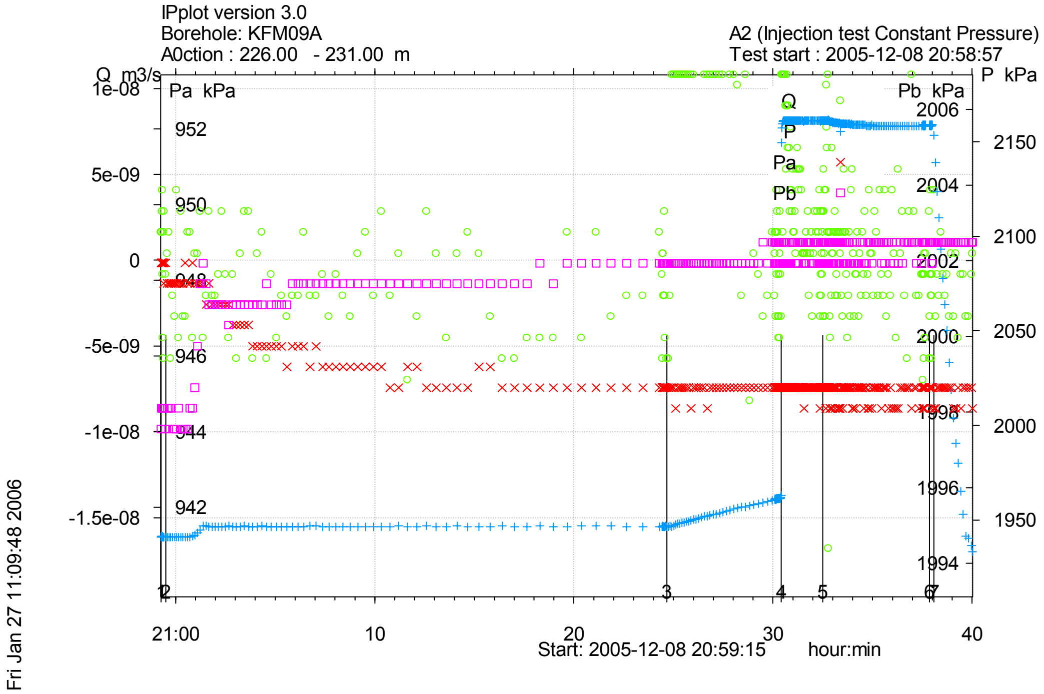


Figure A3-296. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 226.0-231.0 m in borehole KFM09A.*

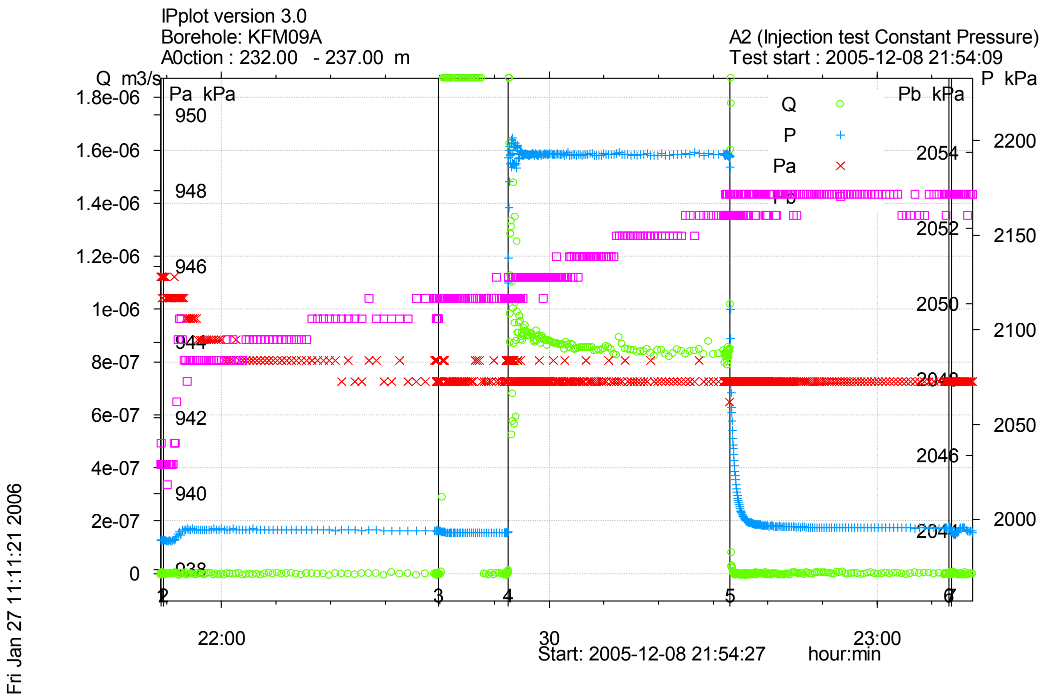


Figure A3-297. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 232.0-237.0 m in borehole KFM09A.*

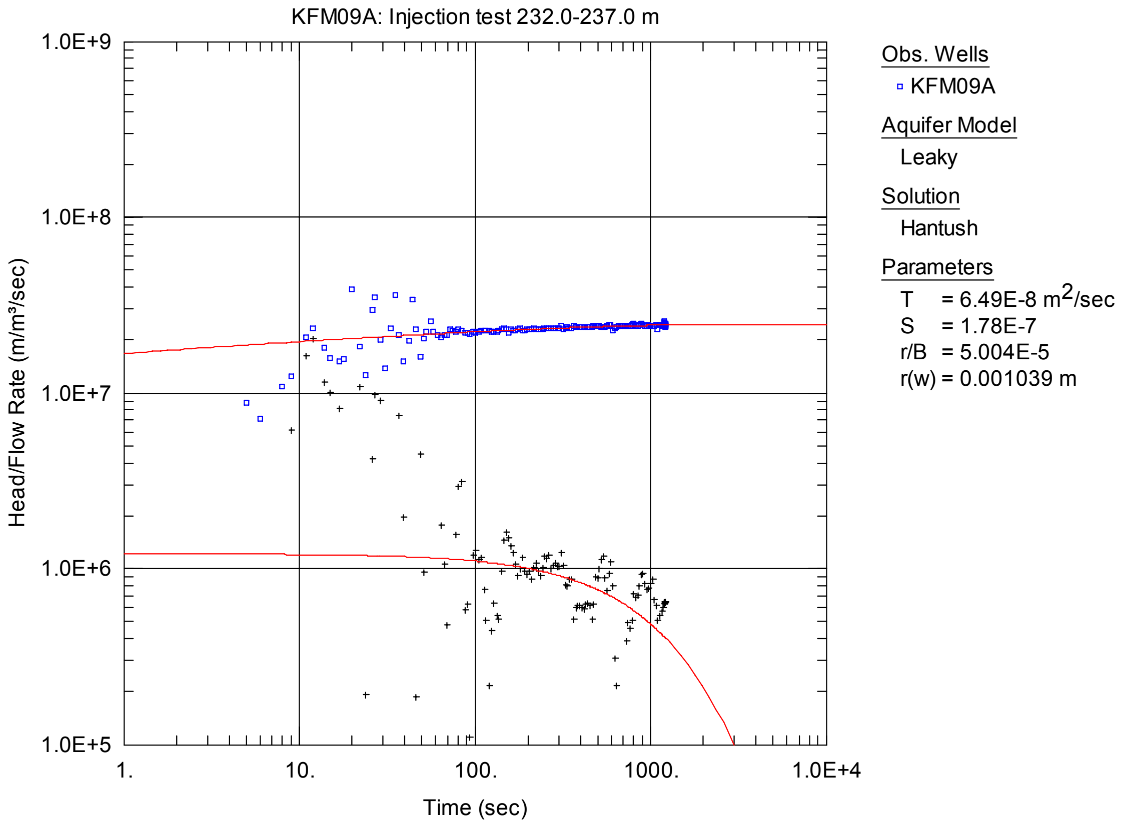


Figure A3-298. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 232.0-237.0 m in KFM09A.*

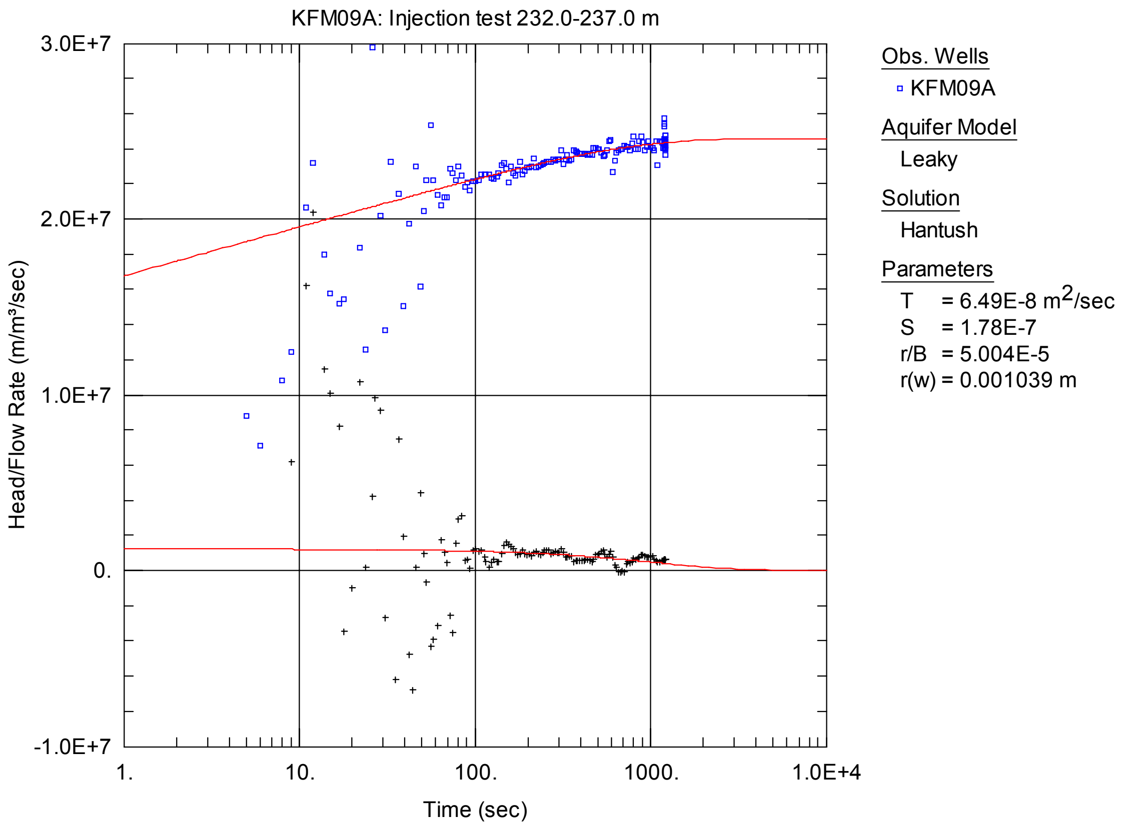


Figure A3-299. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 232.0-237.0 m in KFM09A.*

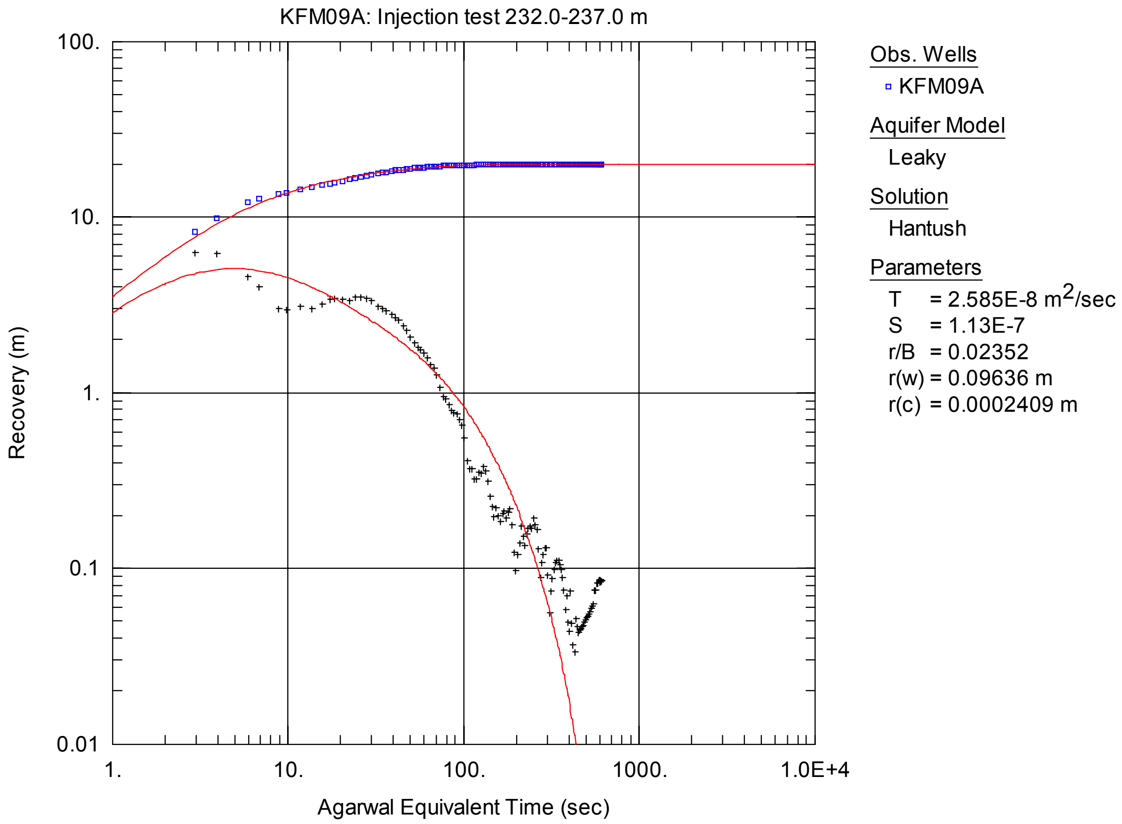


***Figure A3-300.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 232.0-237.0 m in KFM09A.*

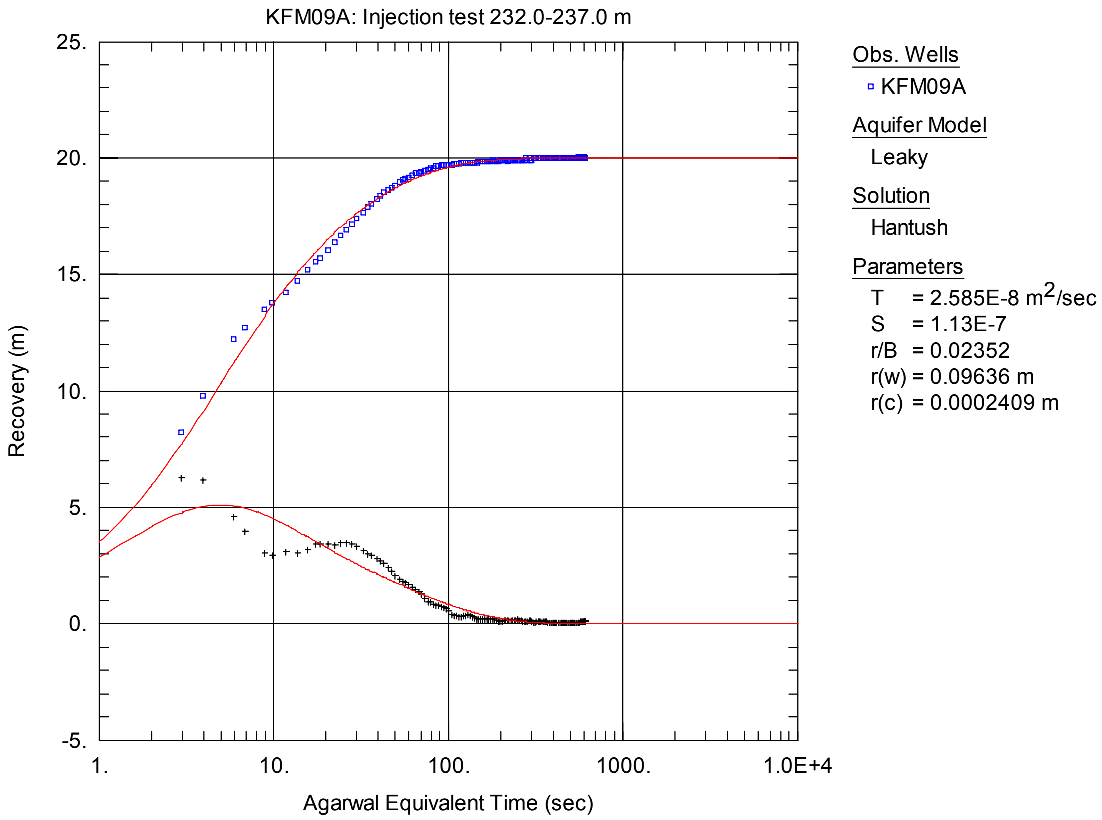


***Figure A3-301.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 232.0-237.0 m in KFM09A.*

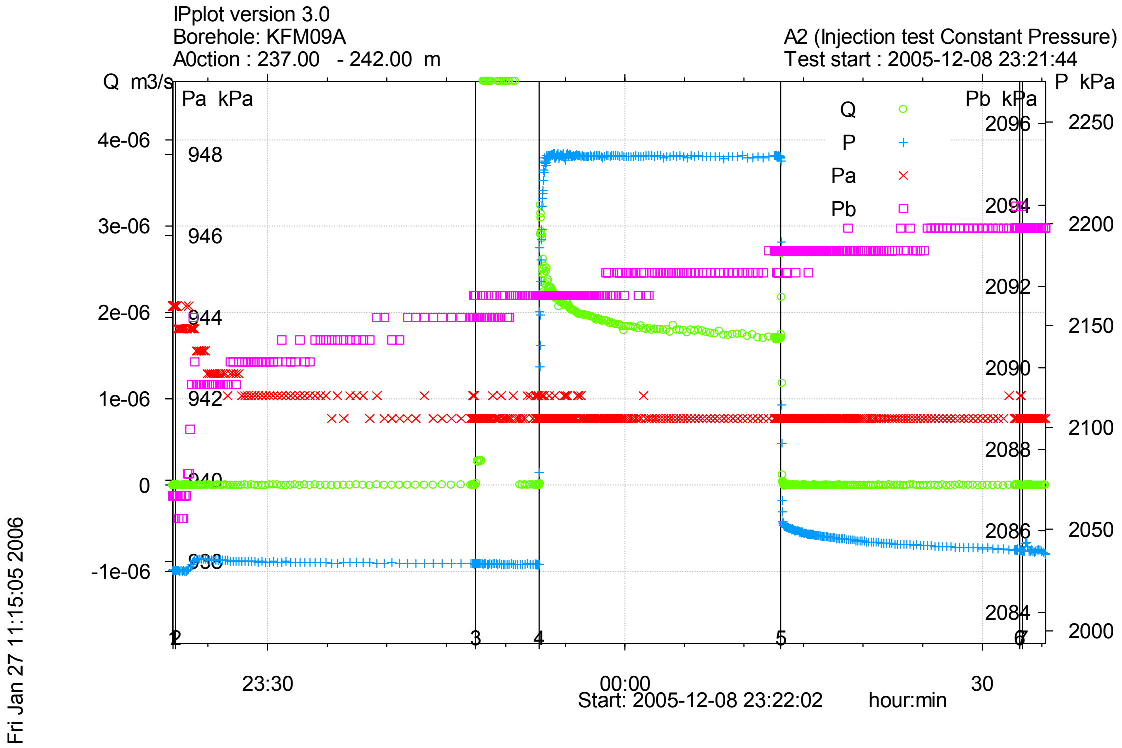


Figure A3-302. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 237.0-242.0 m in borehole KFM09A.*

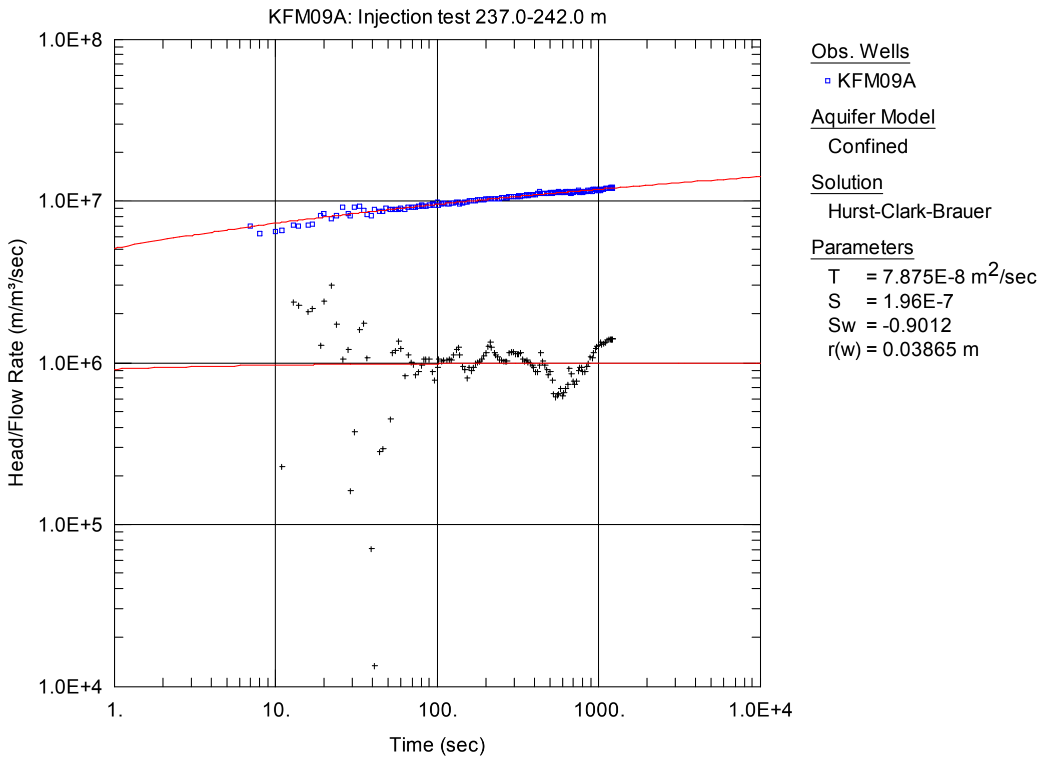


Figure A3-303. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 237.0-242.0 m in KFM09A.*

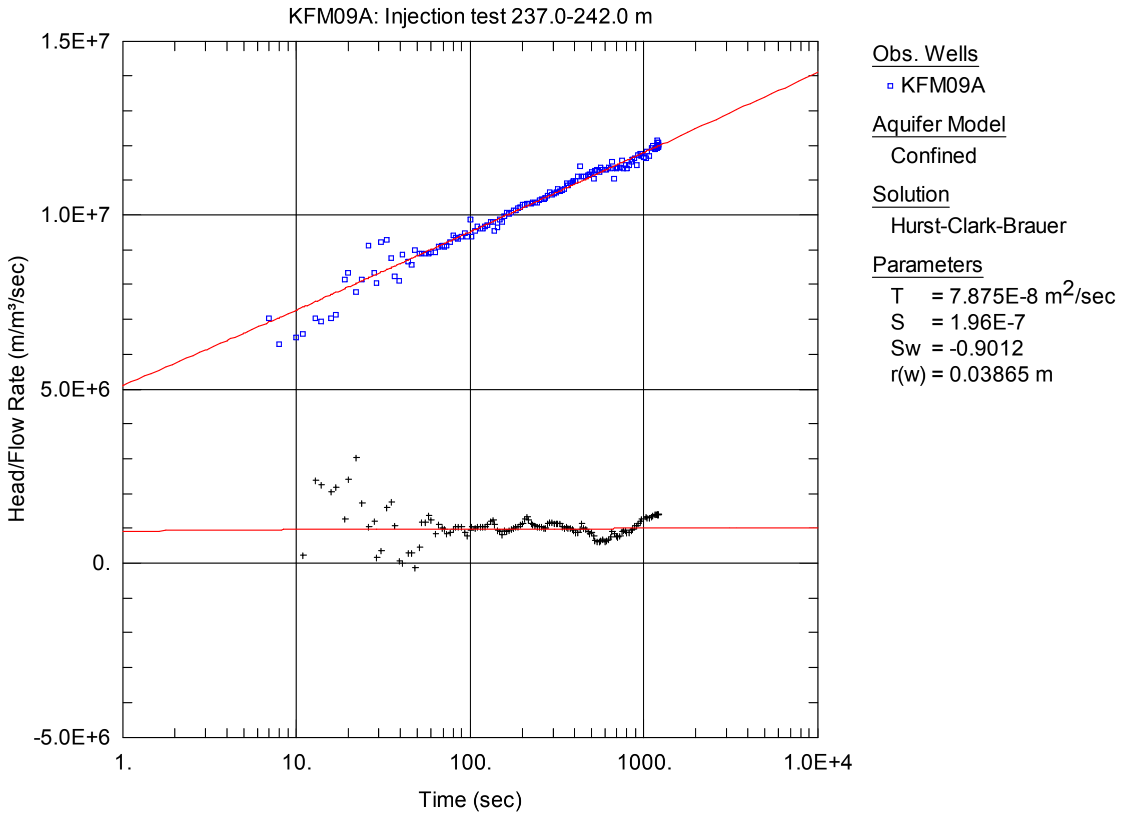


Figure A3-304. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 237.0-242.0 m in KFM09A.*

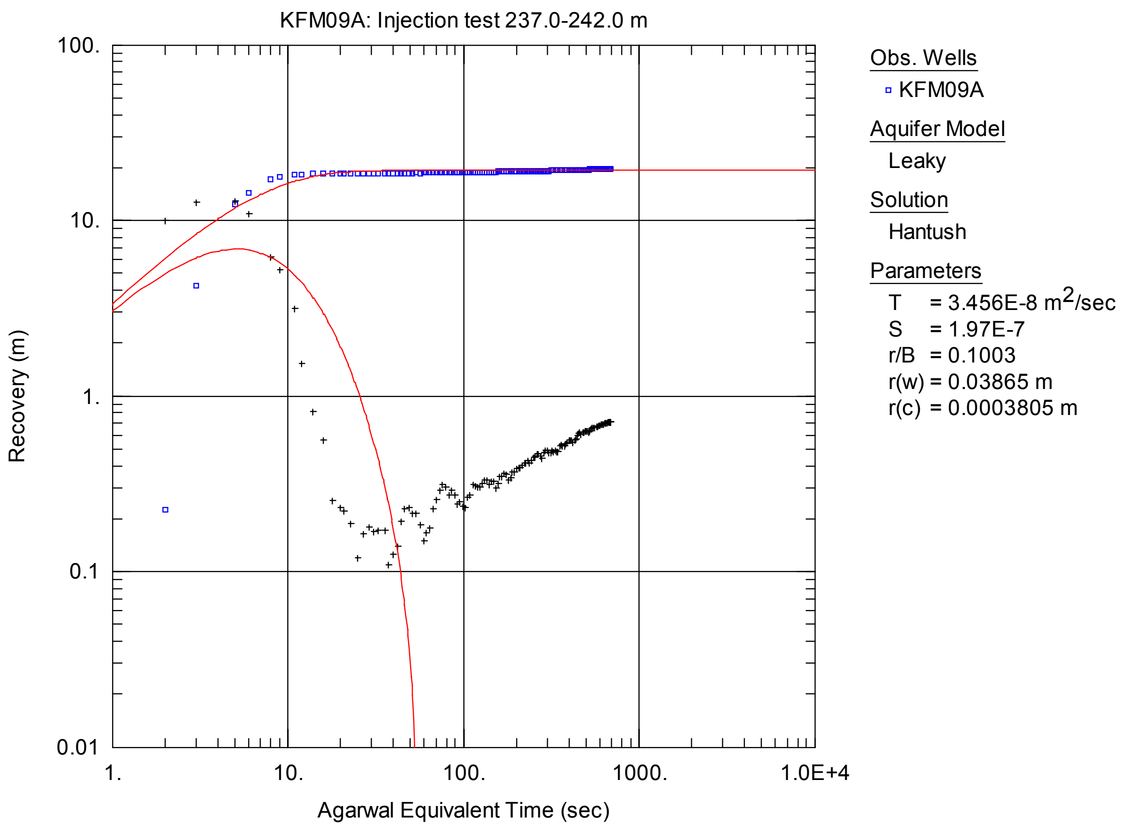


Figure A3-305. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 237.0-242.0 m in KFM09A.*

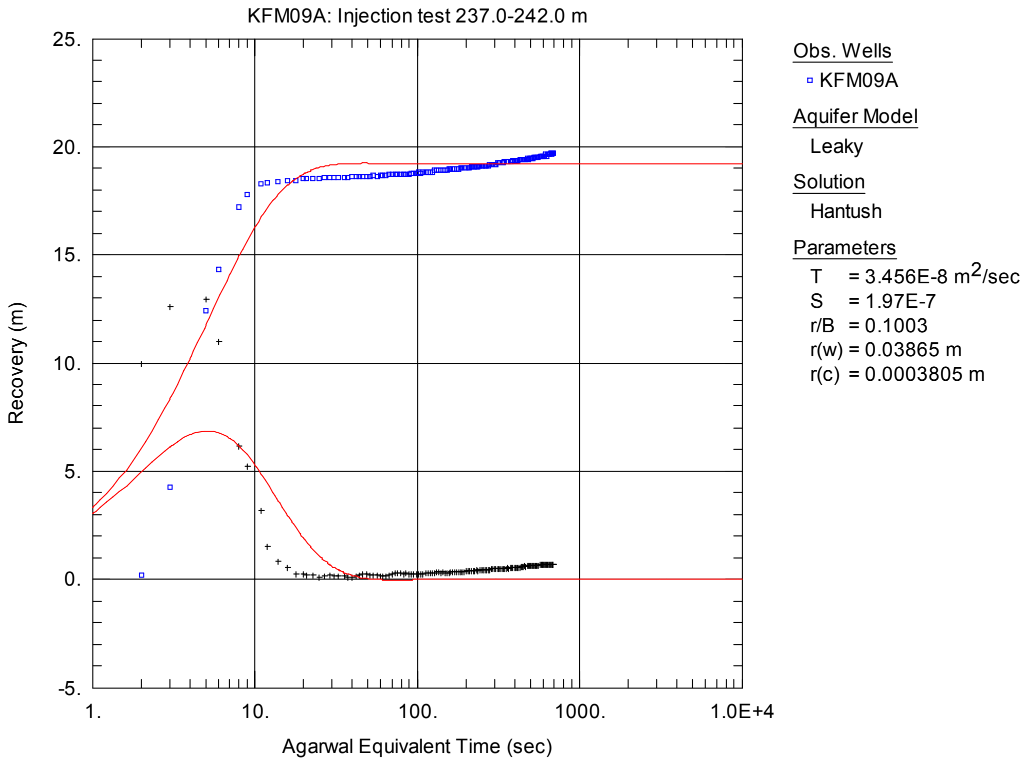


Figure A3-306. Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 237.0-242.0 m in KFM09A.

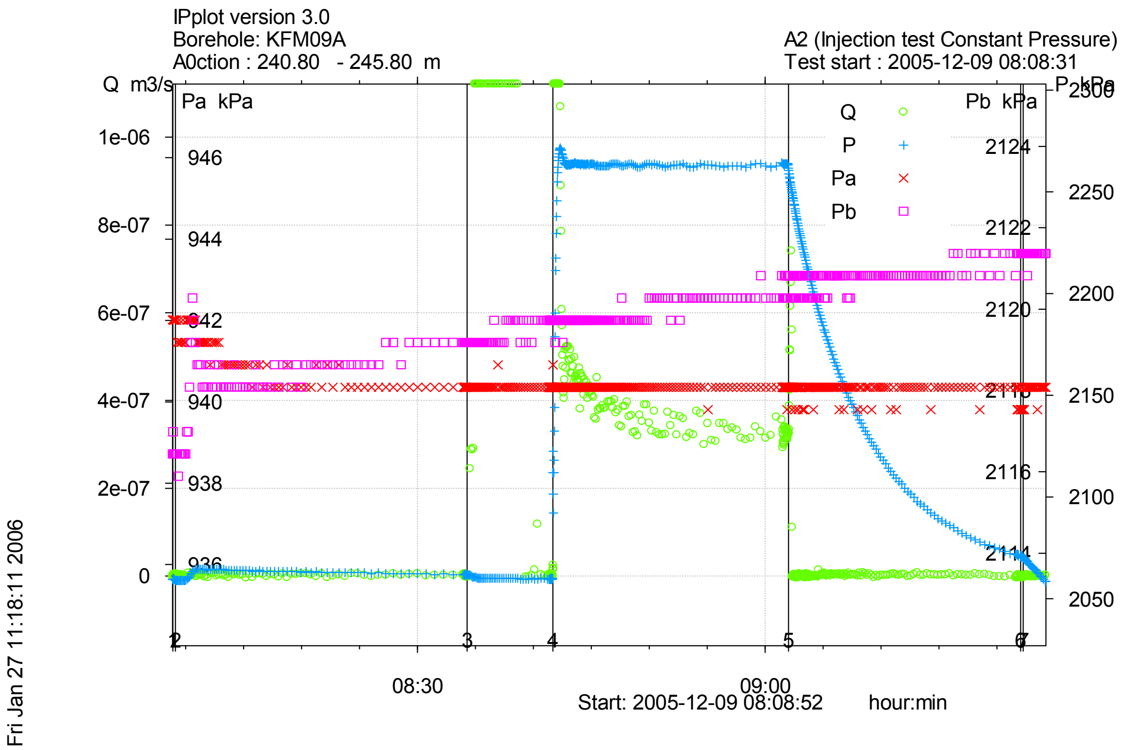


Figure A3-307. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 240.80-245.80 m in borehole KFM09A.

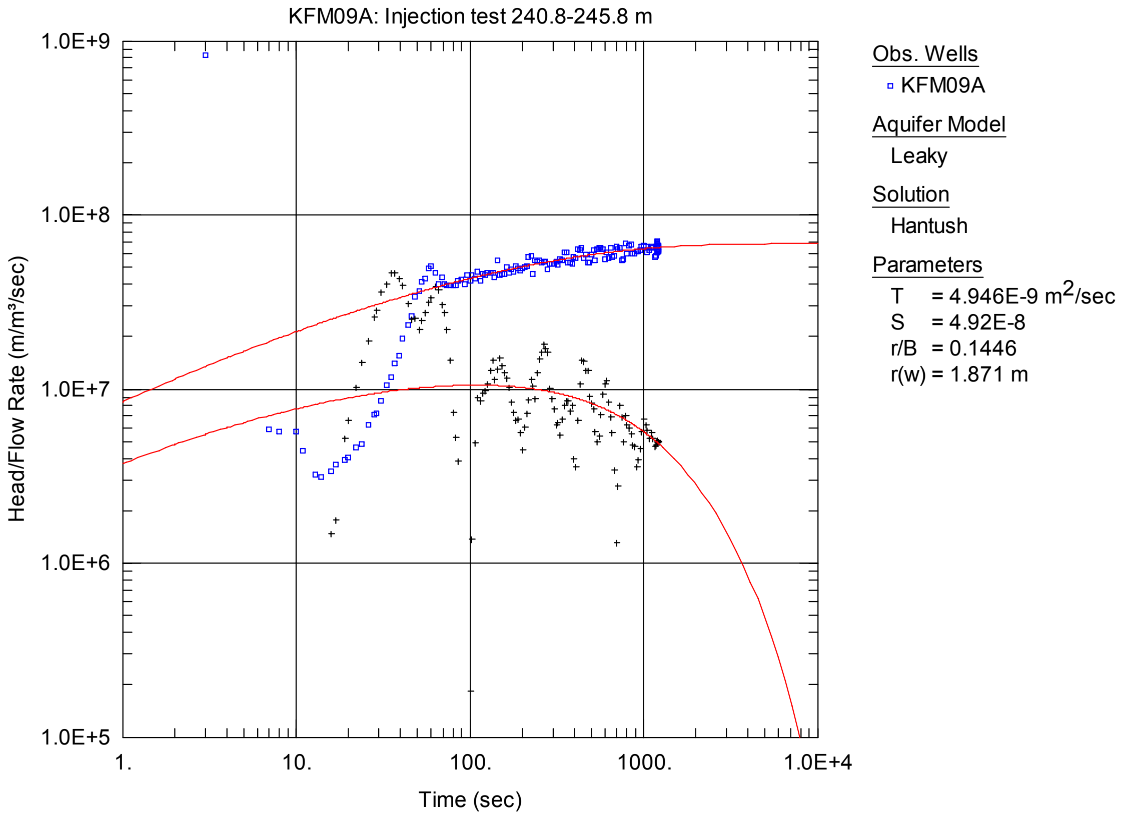


Figure A3-308. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 240.80-245.80 m in KFM09A.*

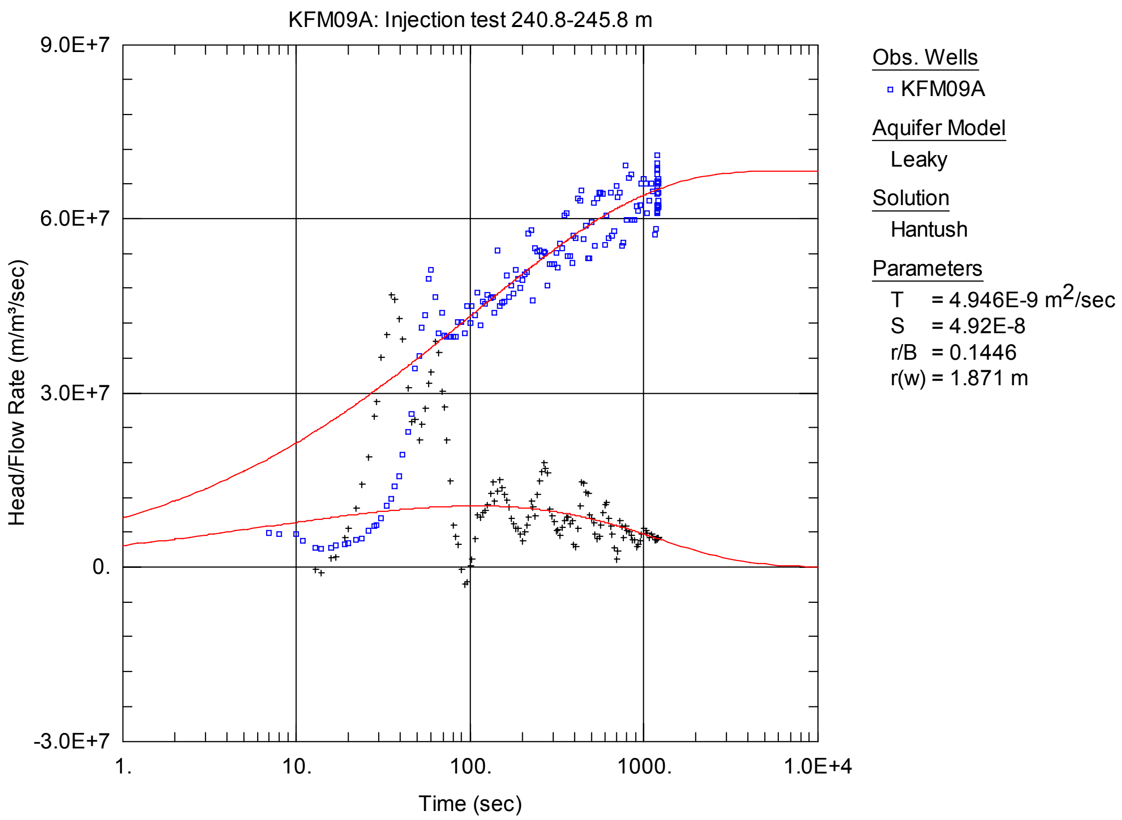


Figure A3-309. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 240.80-245.80 m in KFM09A.*

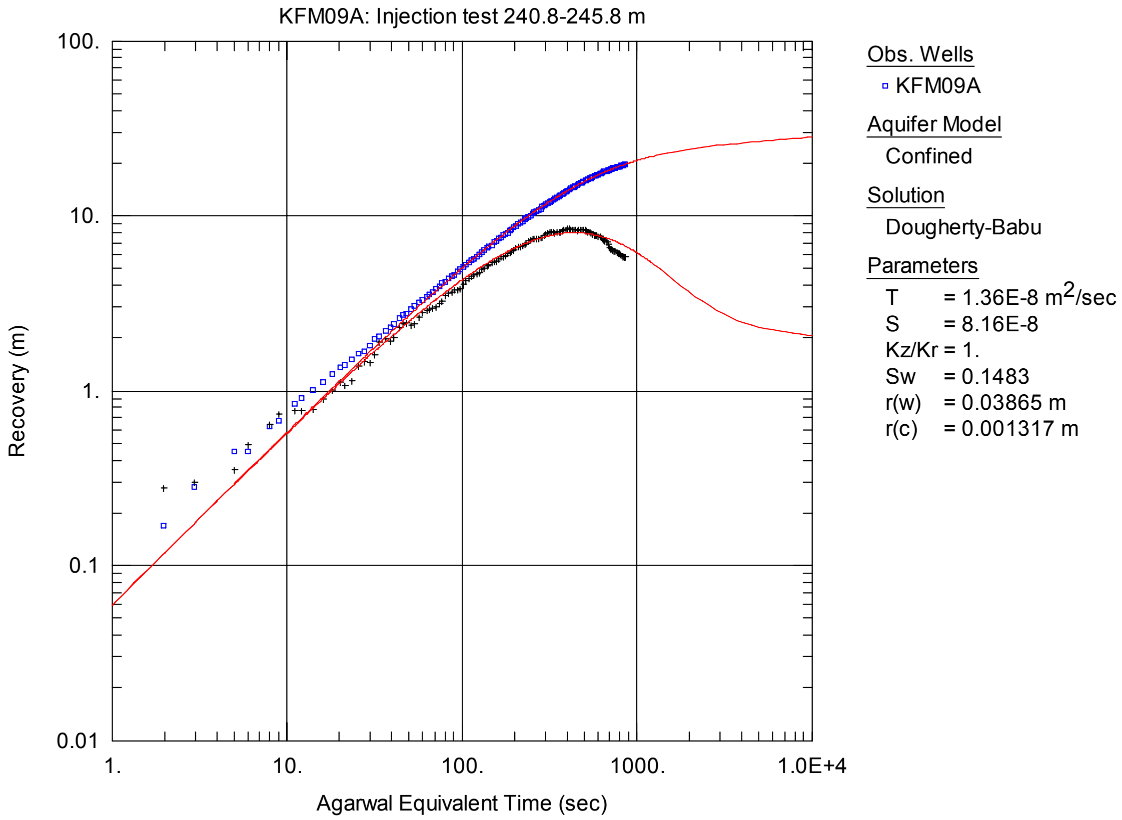


Figure A3-310. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 240.80-245.80 m in KFM09A.*

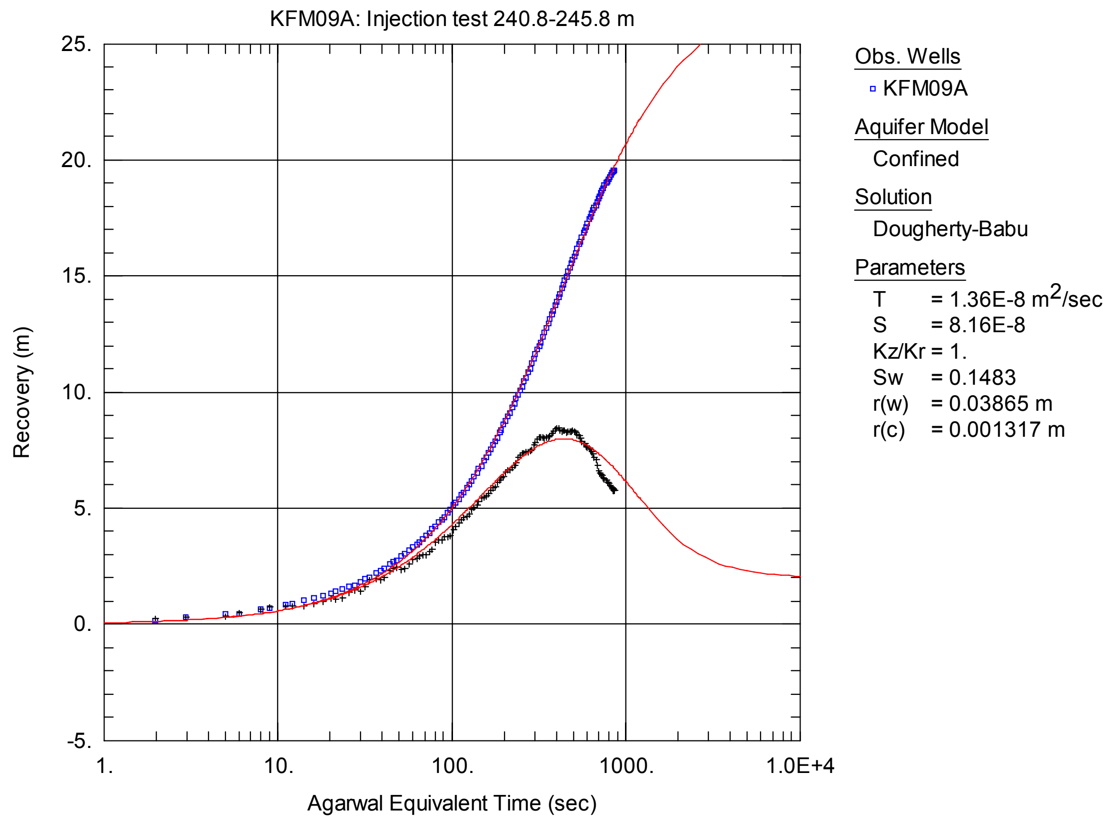


Figure A3-311. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 240.80-245.80 m in KFM09A.*

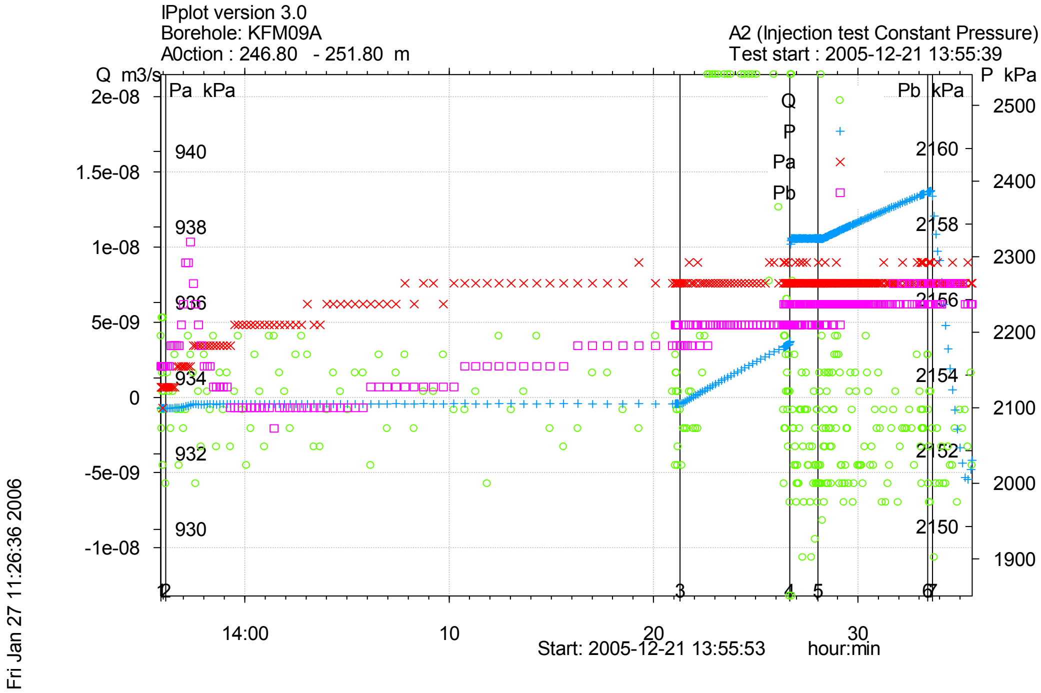


Figure A3-312. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 246.80-251.80 m in borehole KFM09A.*

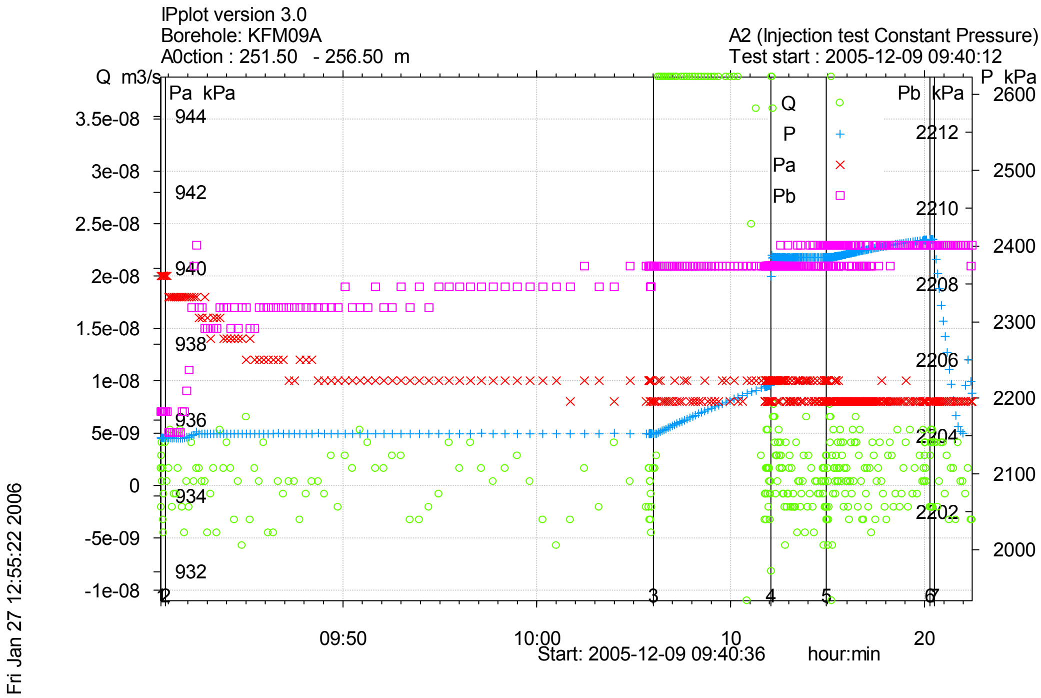


Figure A3-313. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 251.50-256.50 m in borehole KFM09A.*

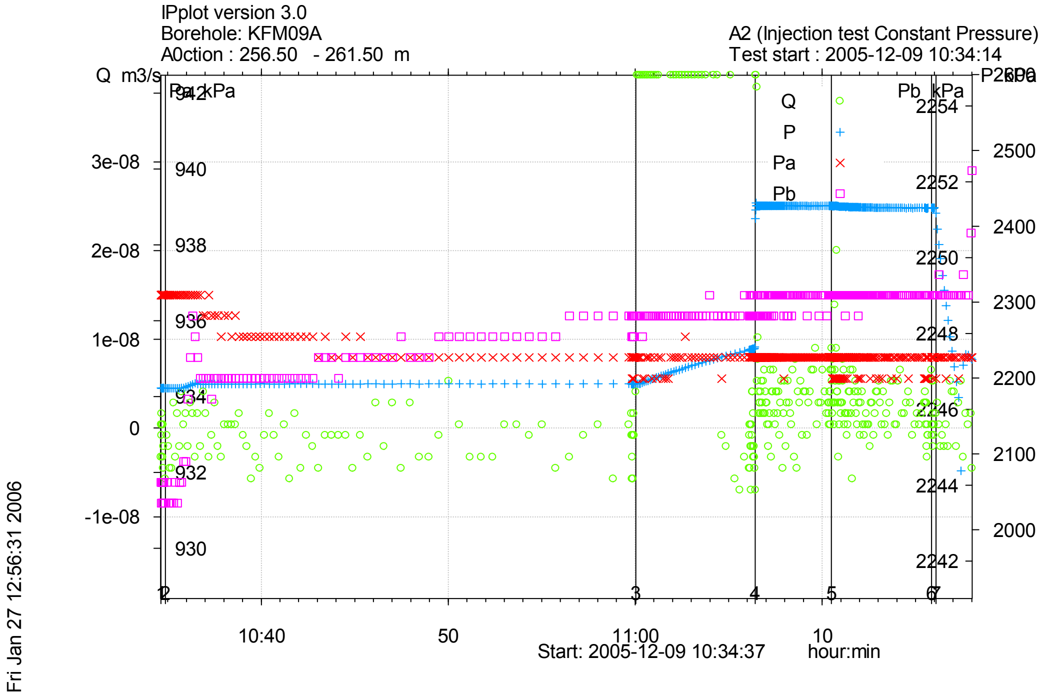


***Figure A3-314.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 256.50-261.50 m in borehole KFM09A.*

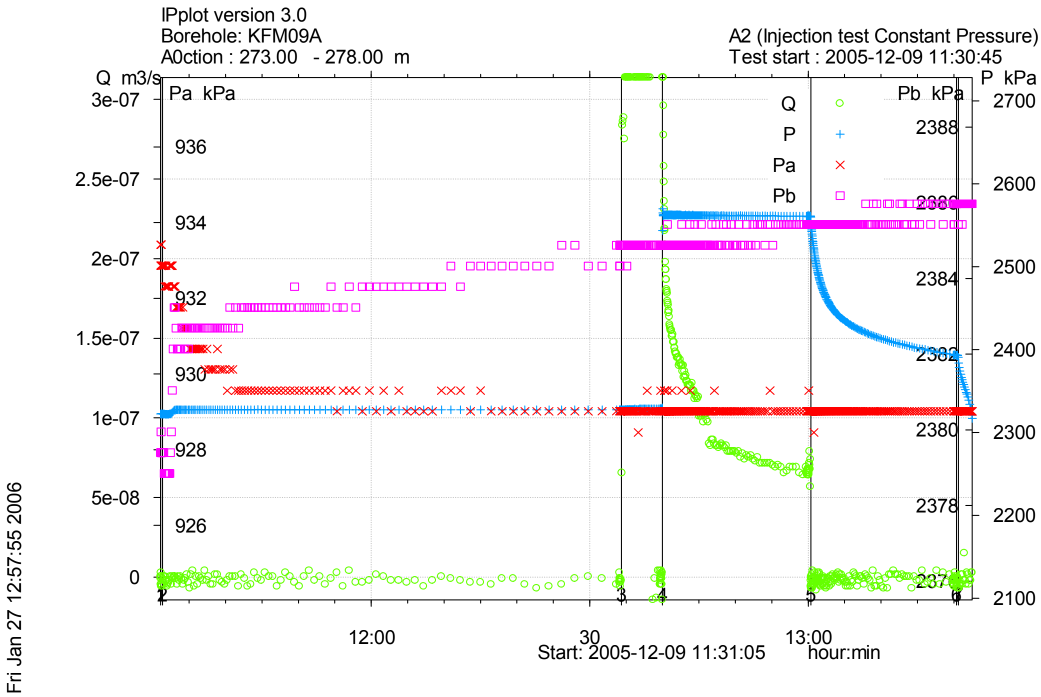


***Figure A3-315.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 273.0-278.0 m in borehole KFM09A.*

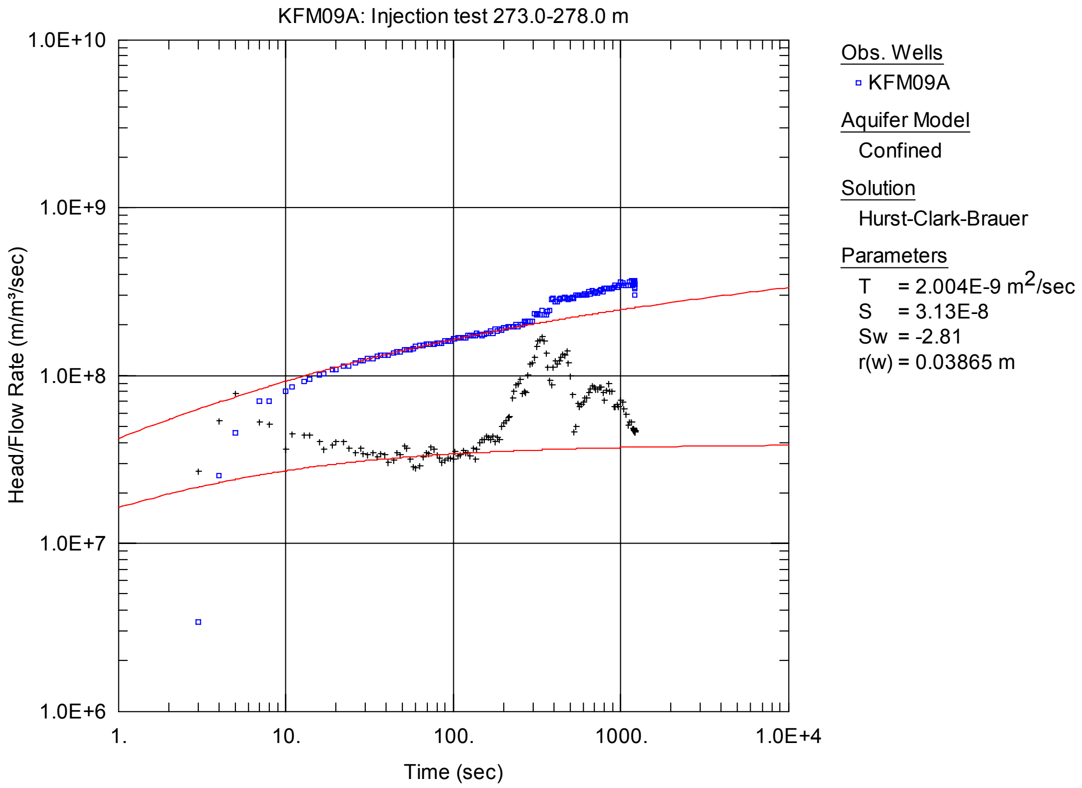


Figure A3-316. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 273.0-278.0 m in KFM09A. This plot shows a fit to the first of two different PRF:s during the injection period in this section.*

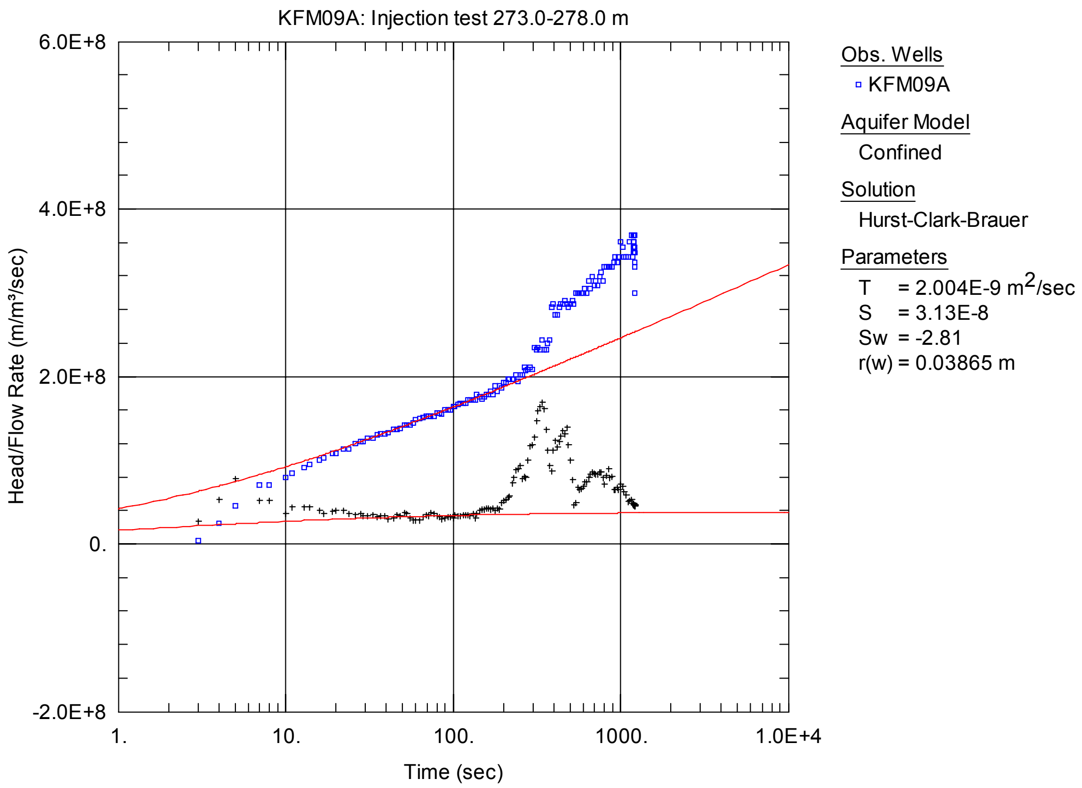


Figure A3-317. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 273.0-278.0 m in KFM09A. This plot shows a fit to the first of two different PRF:s during the injection period in this section.*

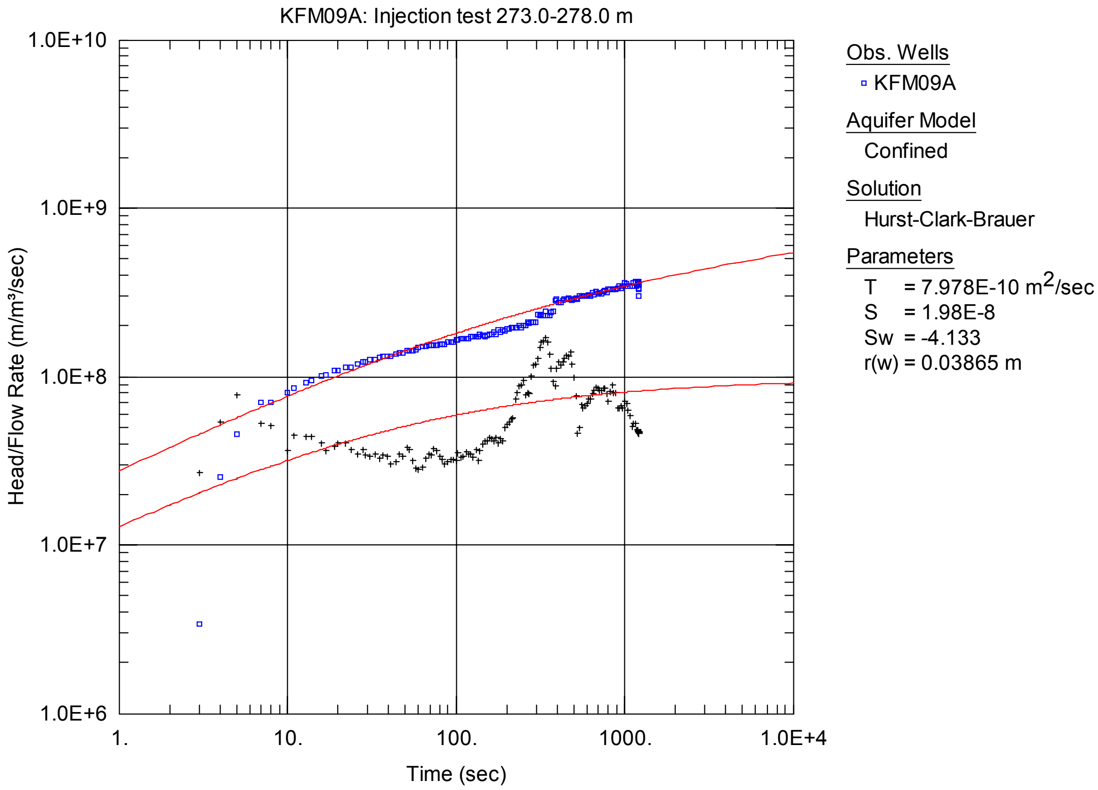


Figure A3-318. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 273.0-278.0 m in KFM09A. This plot shows a fit to the second of two different PRF:s during the injection period in this section.*

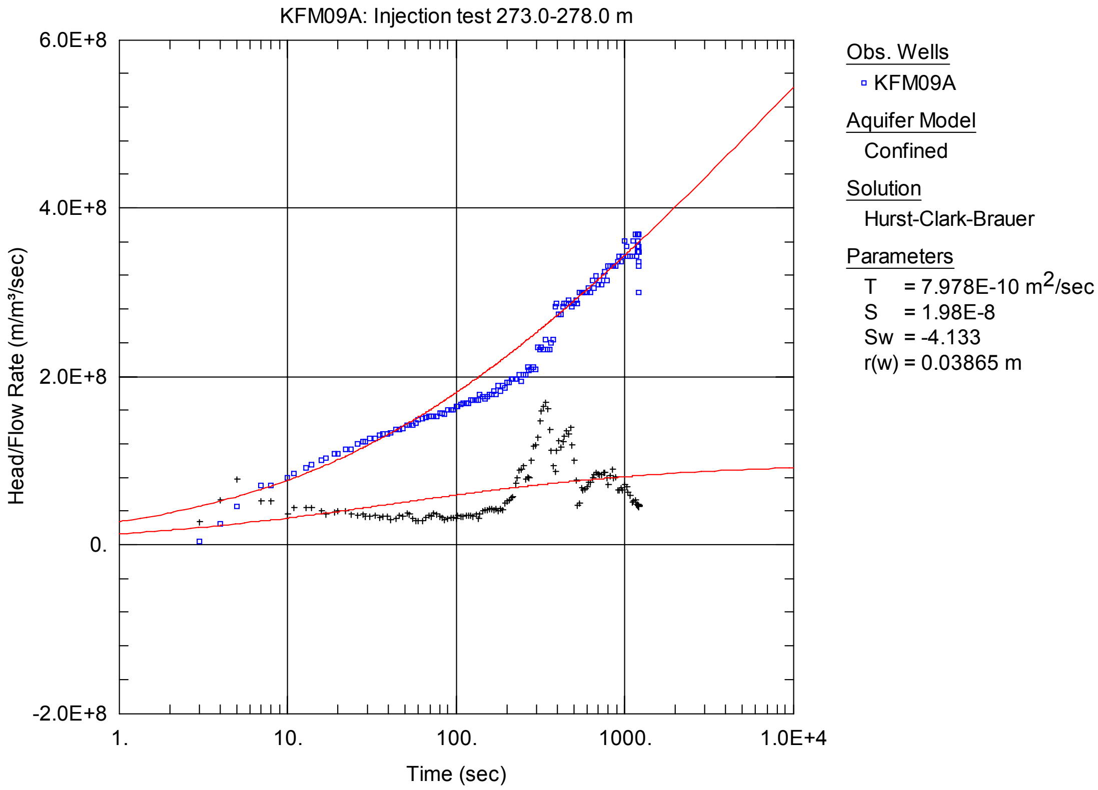


Figure A3-319. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 273.0-278.0 m in KFM09A. This plot shows a fit to the second of two different PRF:s during the injection period in this section.*

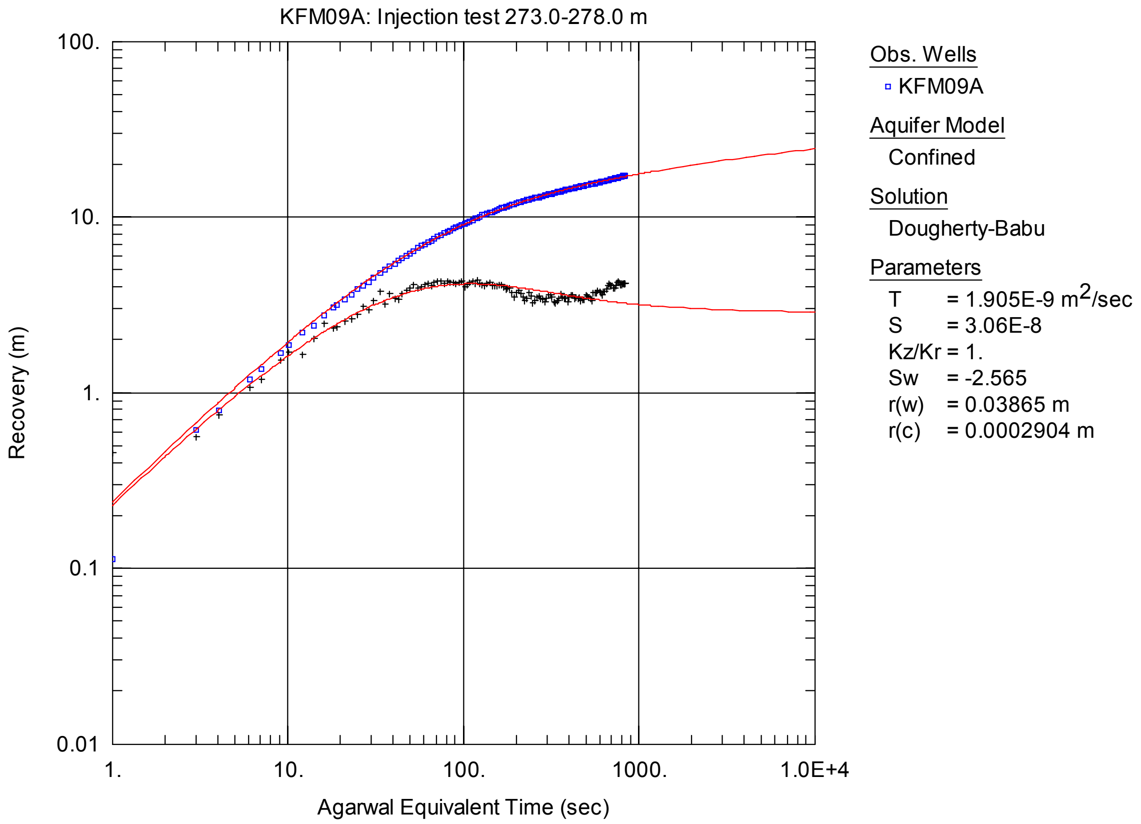


Figure A3-320. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 273.0-278.0 m in KFM09A.*

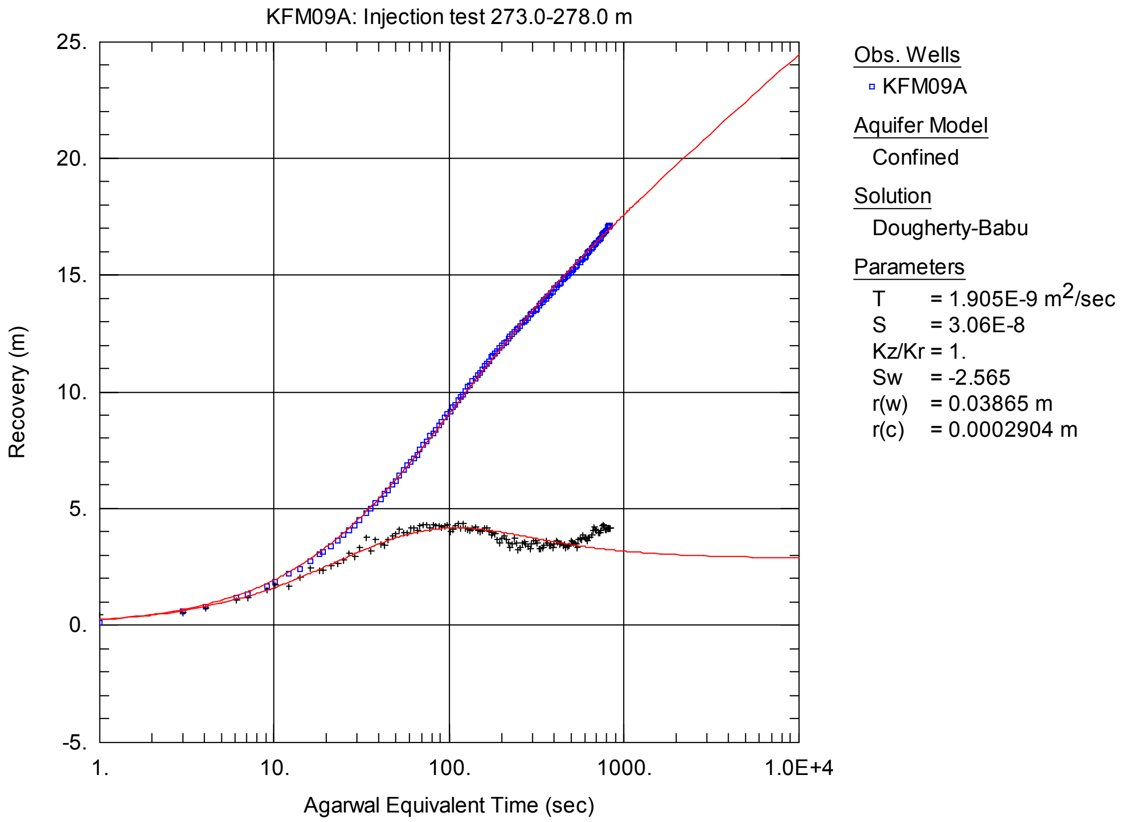


Figure A3-321. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 273.0-278.0 m in KFM09A.*

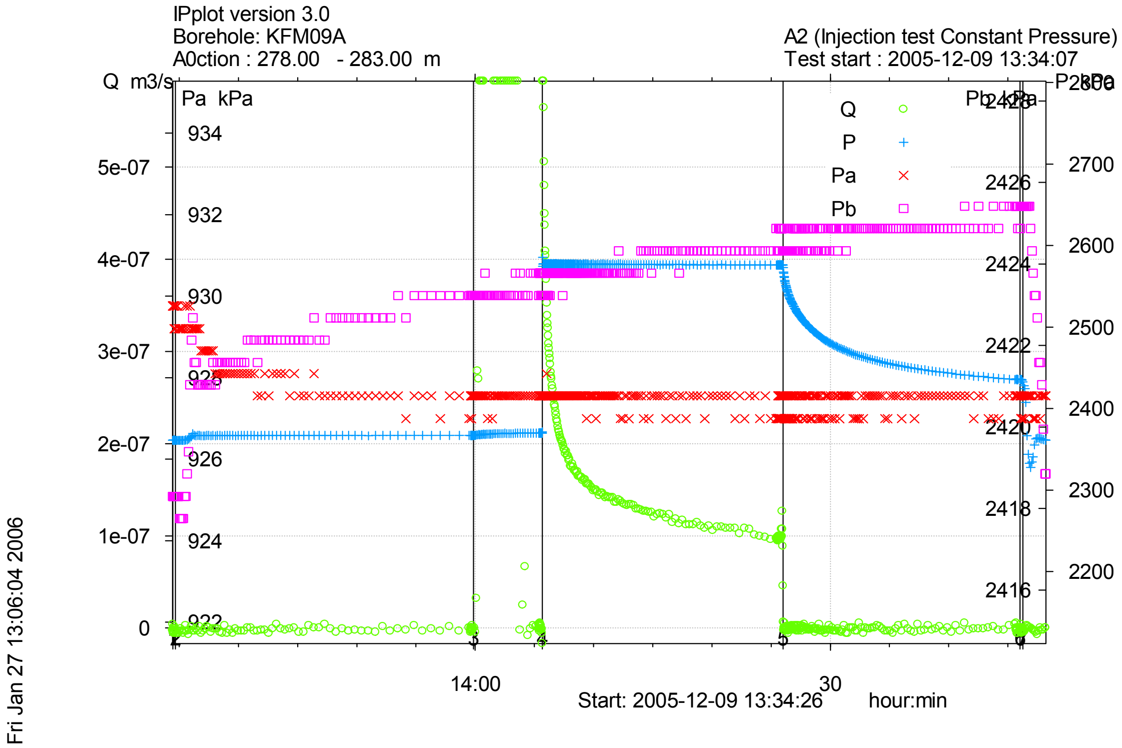


Figure A3-322. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in 278.0-283.0 m in borehole KFM09A.*

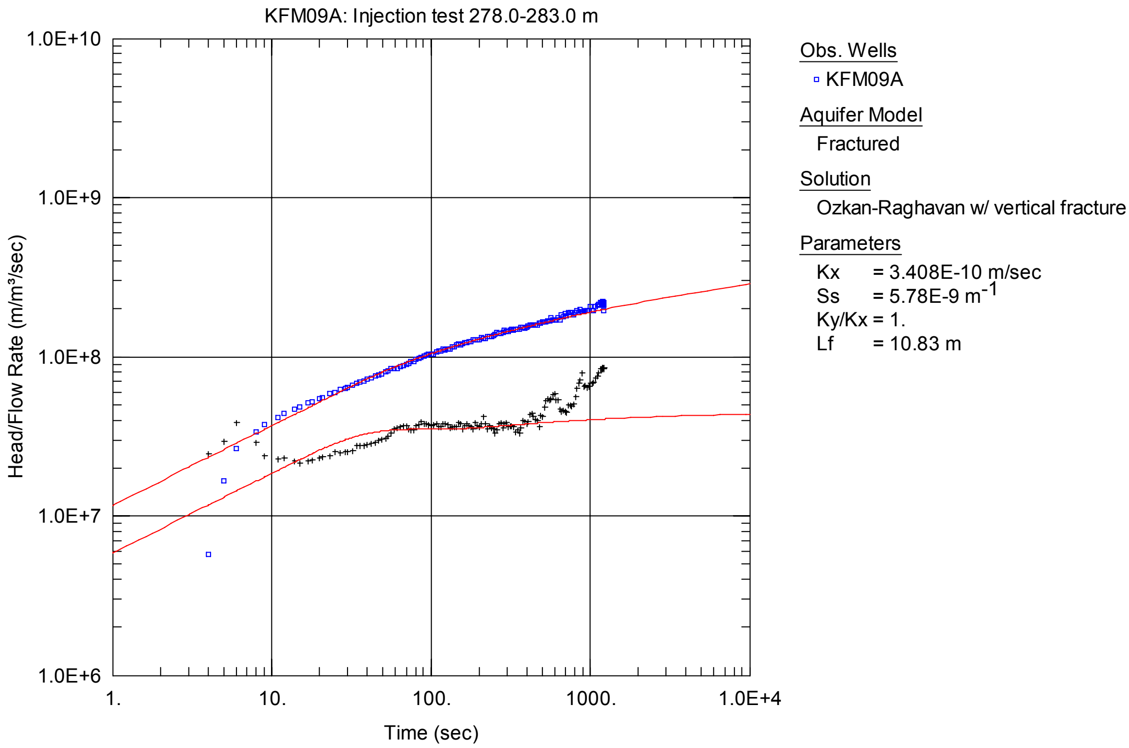


Figure A3-323. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 278.0-283.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

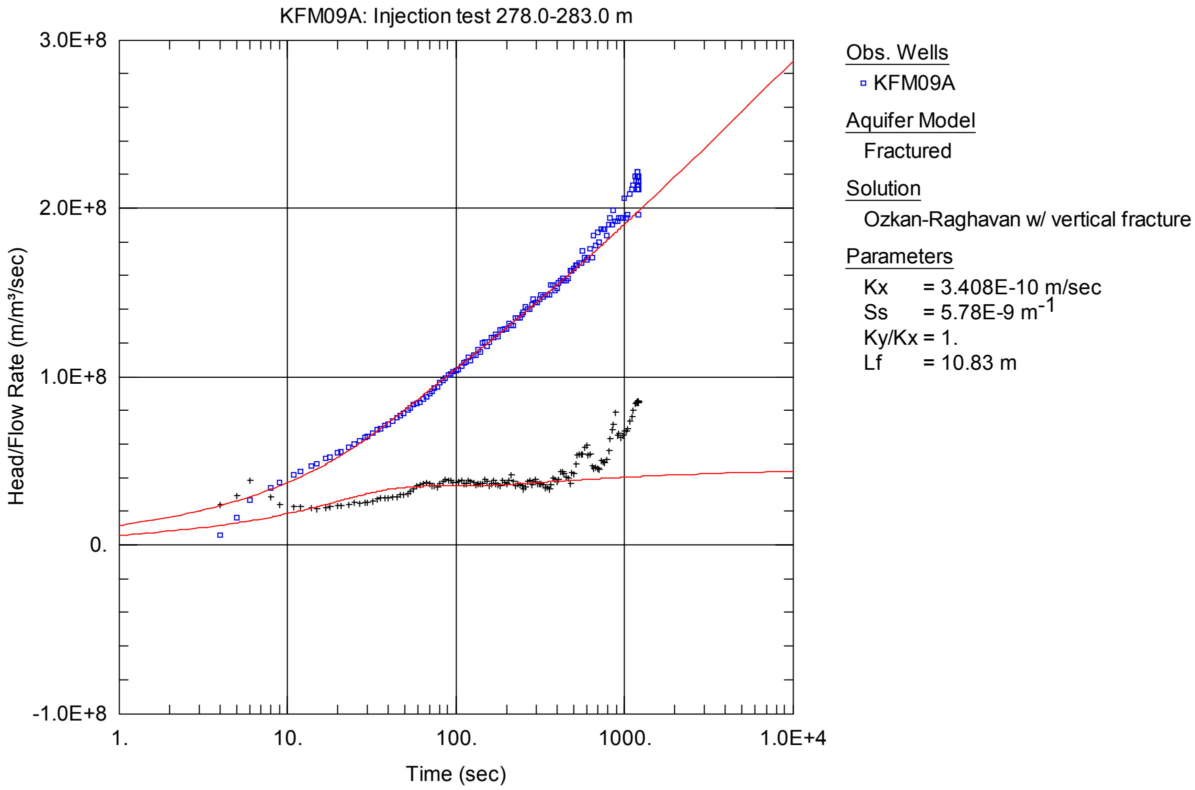


Figure A3-324. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 278.0-283.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

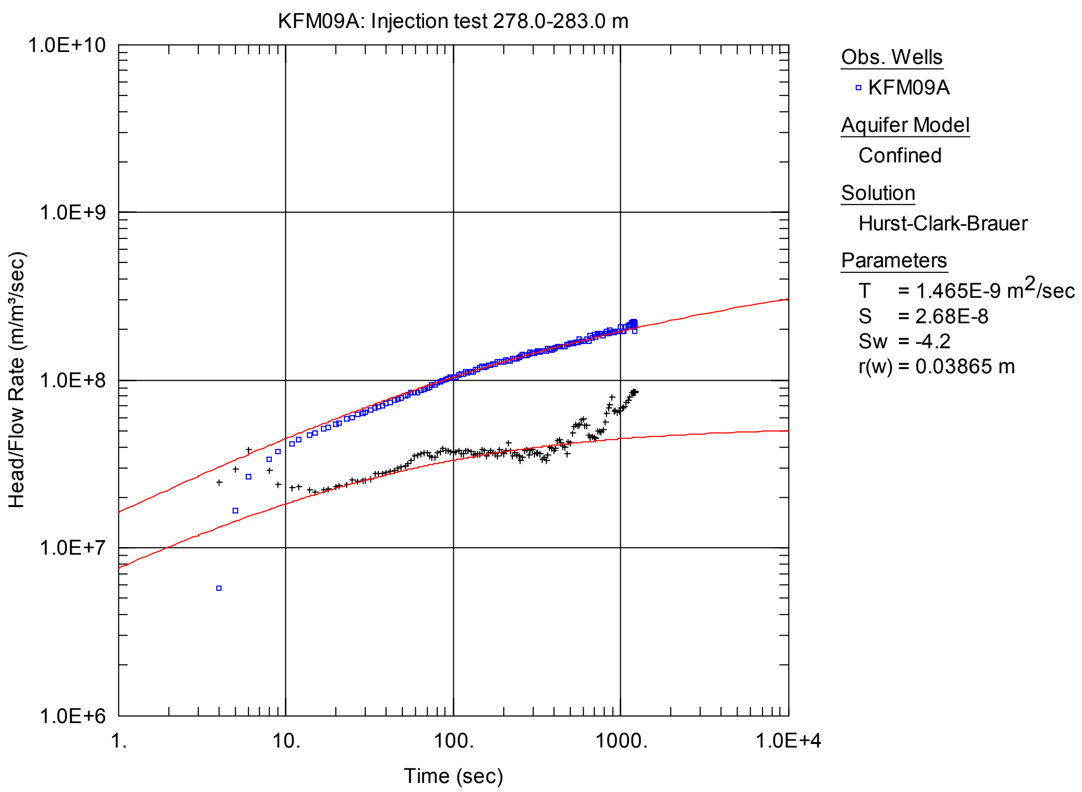


Figure A3-325. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 278.0-283.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for a pseudo-radial response.*

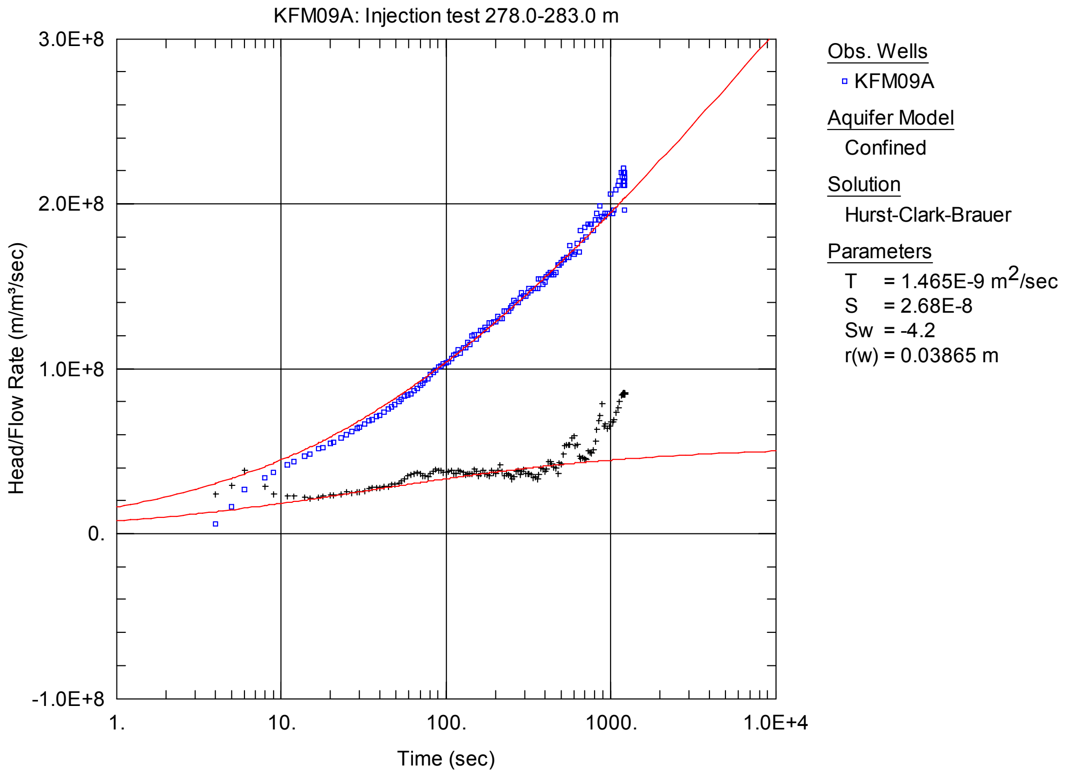


Figure A3-326. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 278.0-283.0 m in KFM09A This evaluation is made with the Hurst-Clark-Brauer model for a pseudo-radial response.*

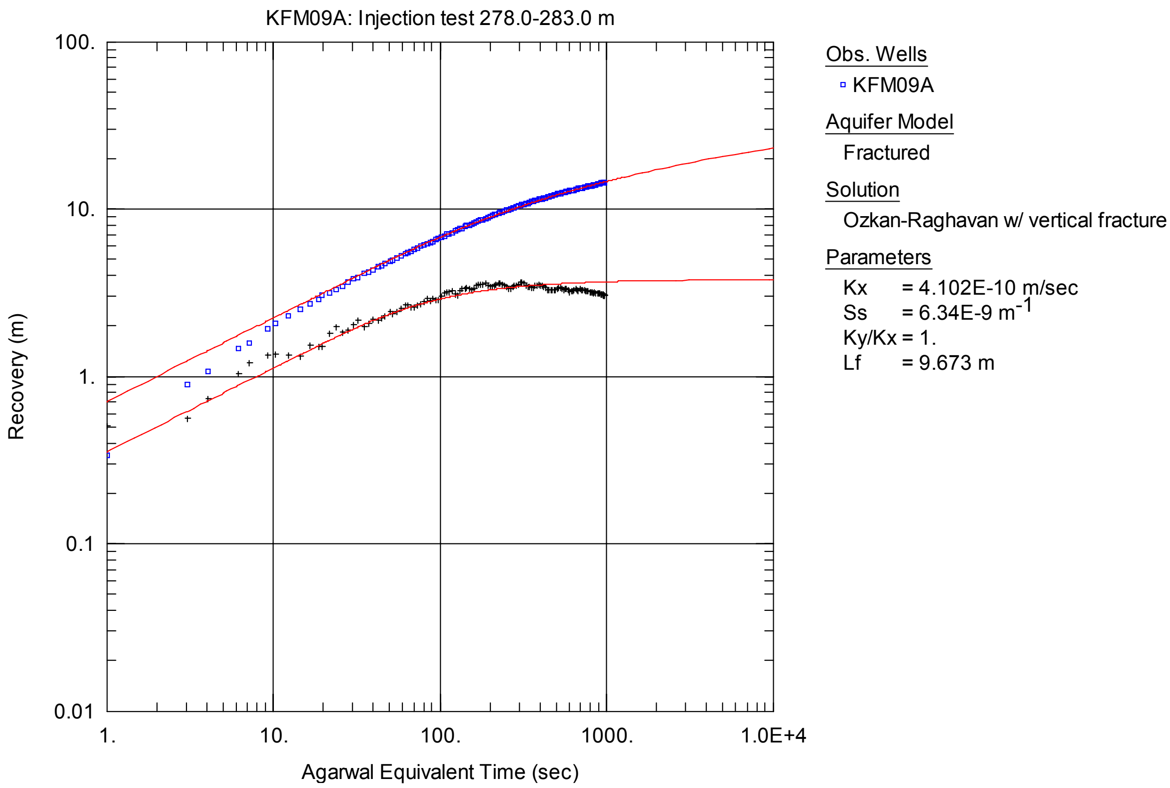


Figure A3-327. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 278.0-283.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

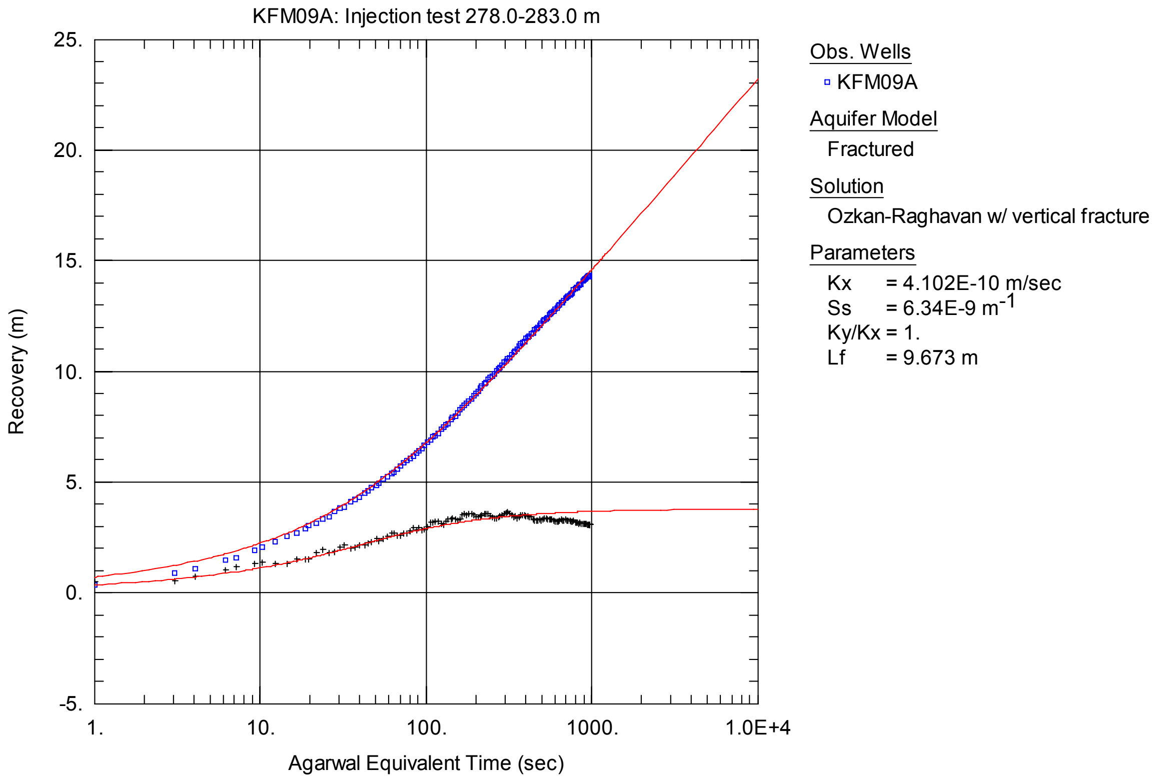


Figure A3-328. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 278.0-283.0 m in KFM09A This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

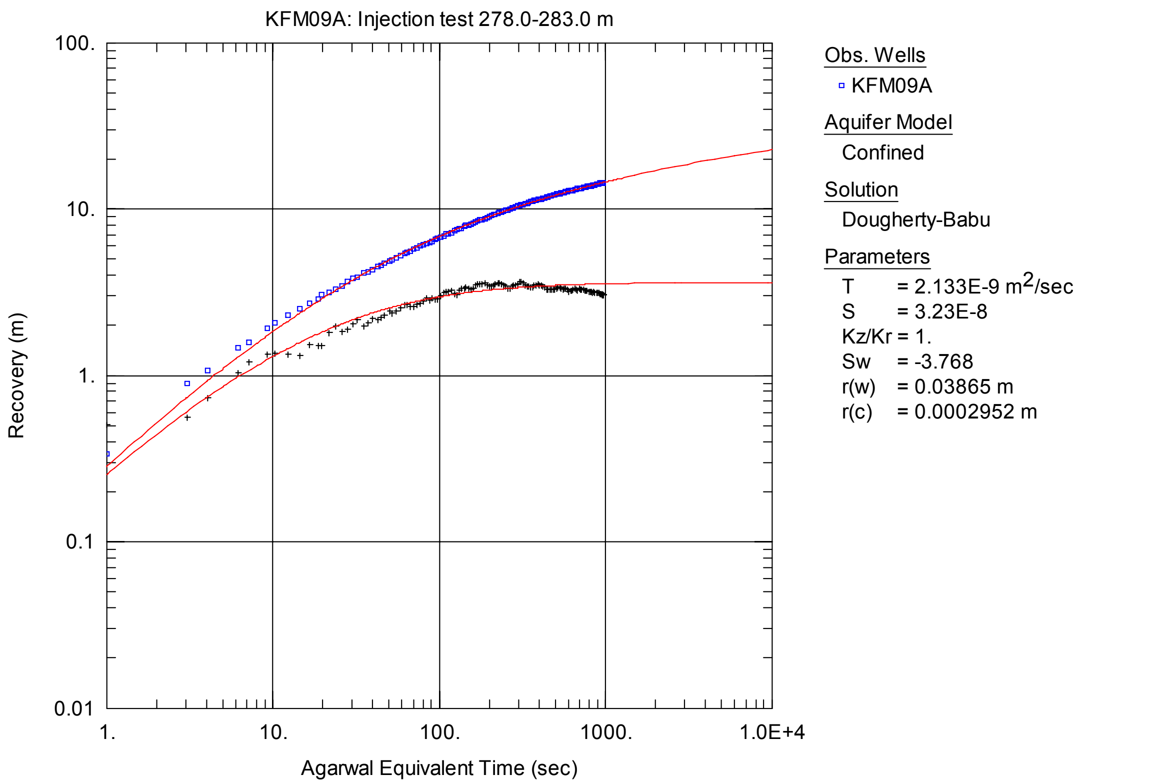


Figure A3-329. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 278.0-283.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for pseudo-radial response during recovery.*

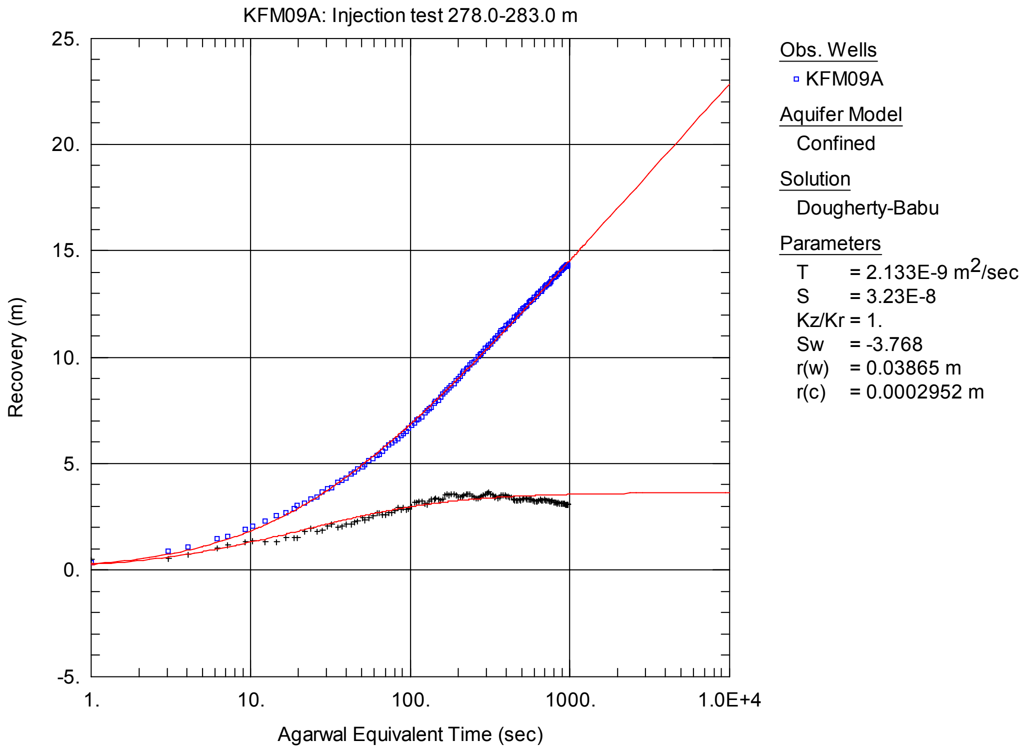


Figure A3-330. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 278.0-283.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for pseudo-radial response during recovery.*

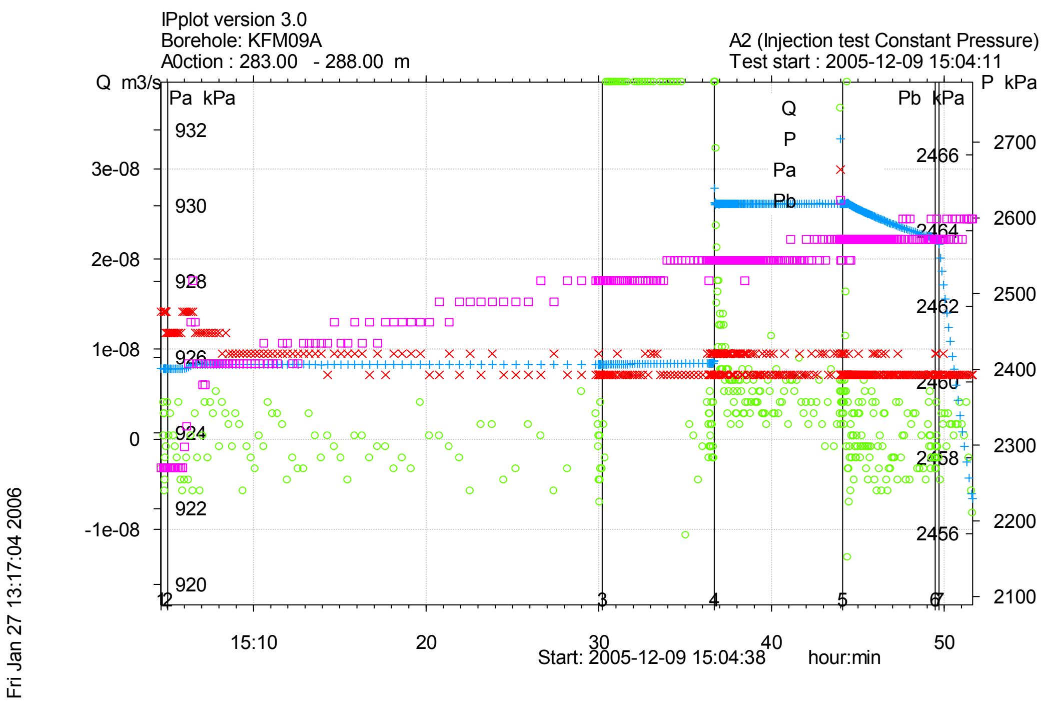


Figure A3-331. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 283.0-288.0 m in borehole KFM09A.*

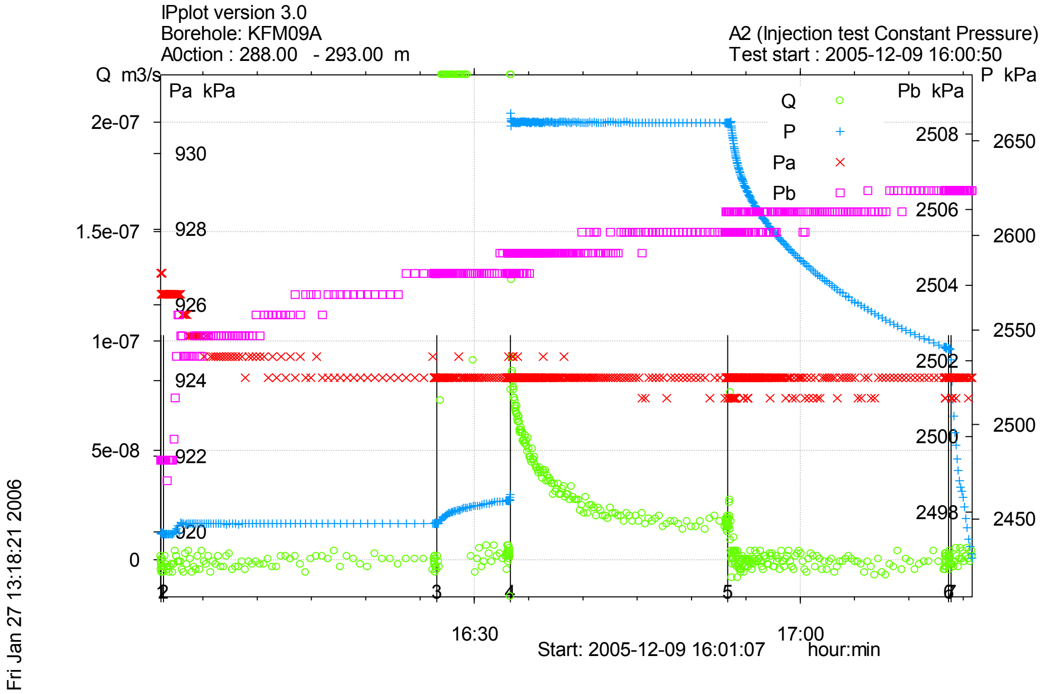


Figure A3-332. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 288.0-293.0 m in borehole KFM09A.

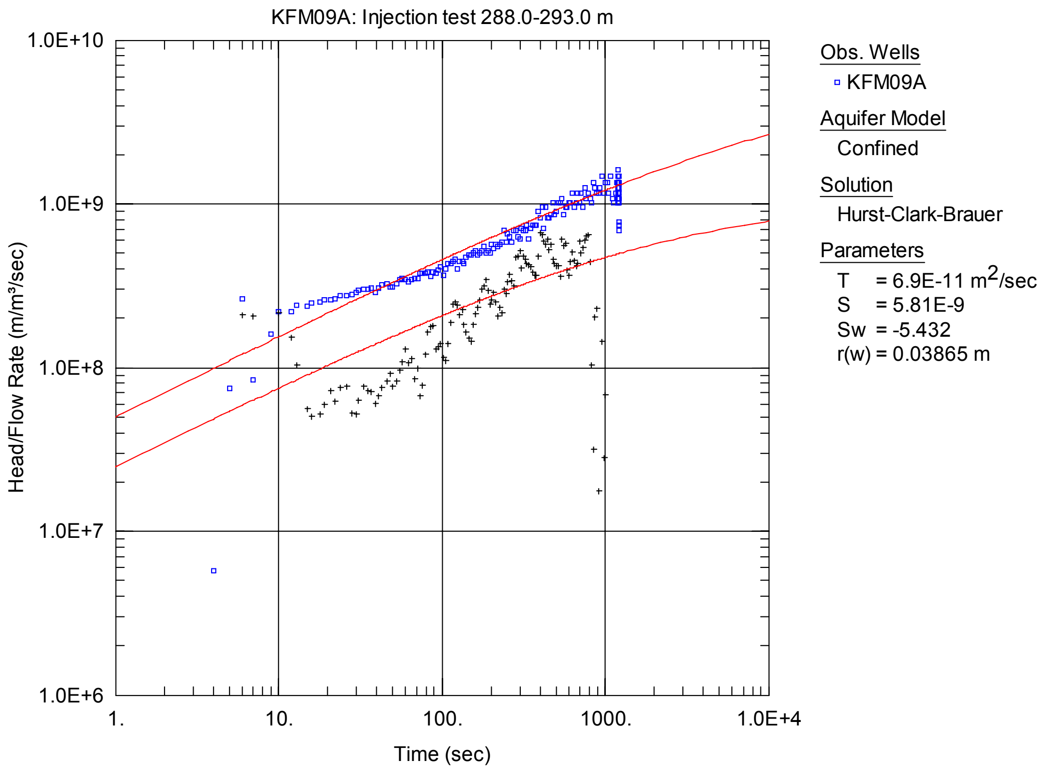


Figure A3-333. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 288.0-293.0 m in KFM09A.

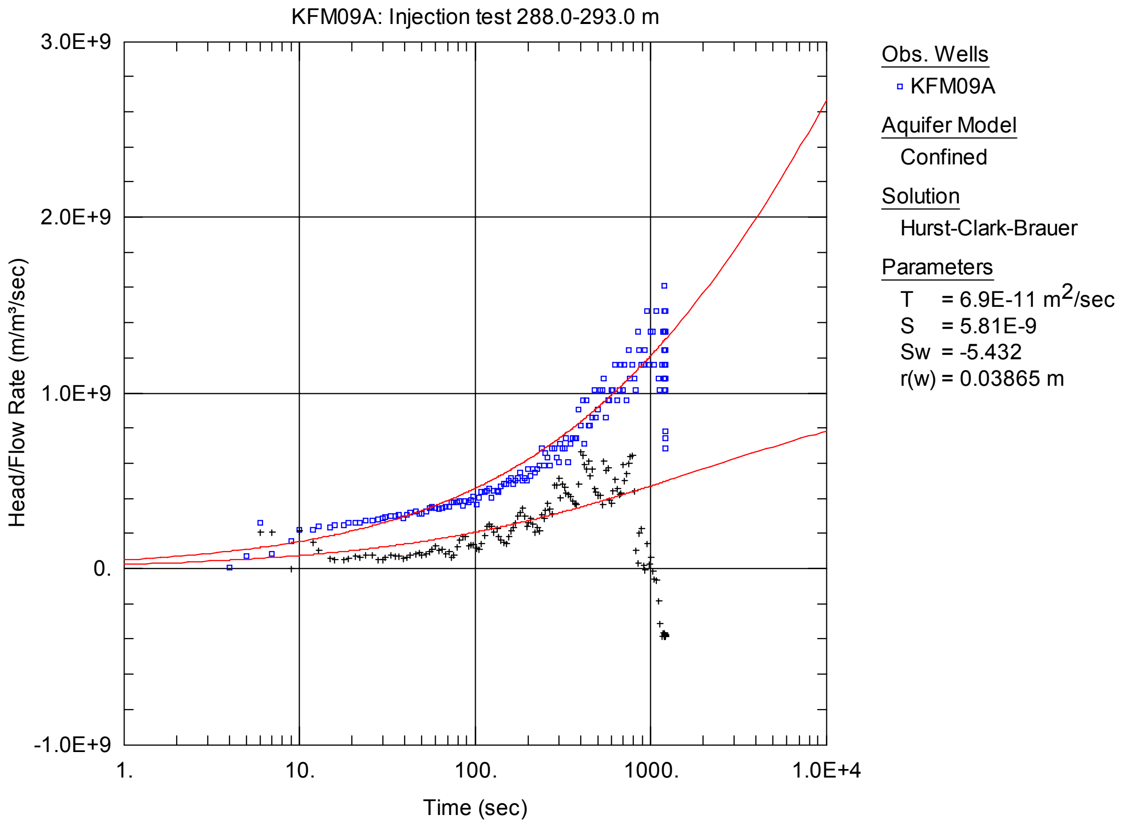


***Figure A3-334.** Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 288.0-293.0 m in KFM09A.*

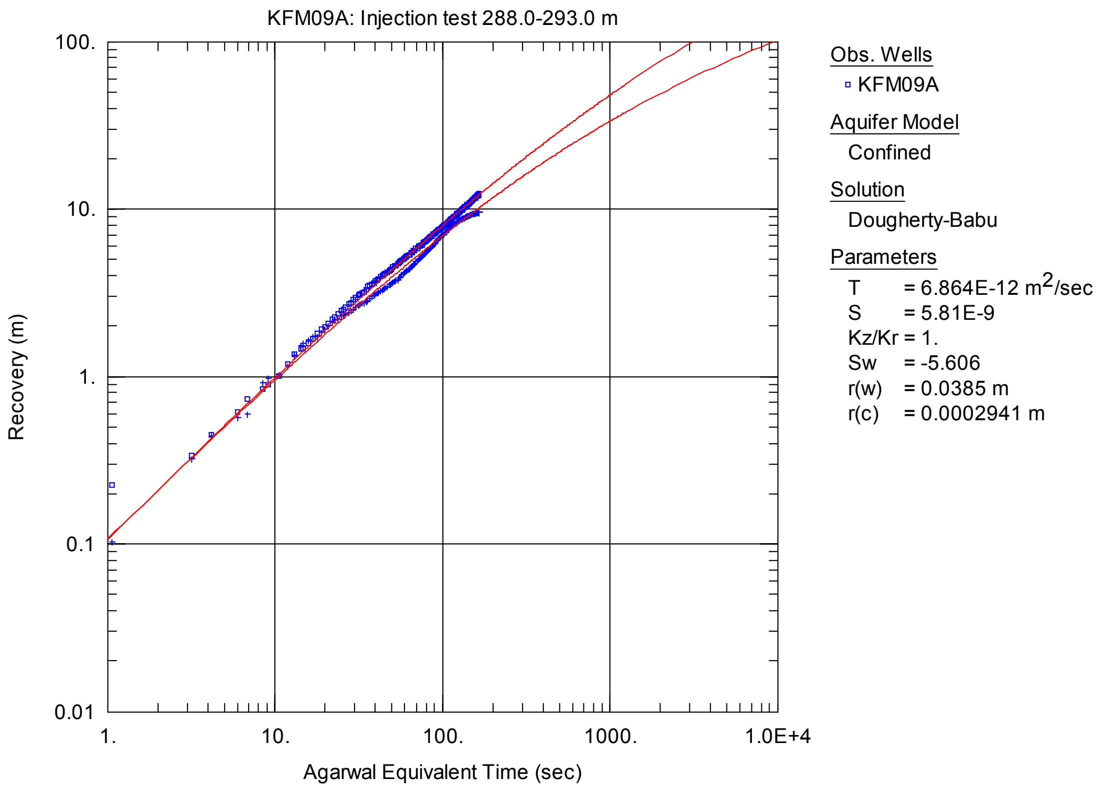


***Figure A3-335.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 288.0-293.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.*

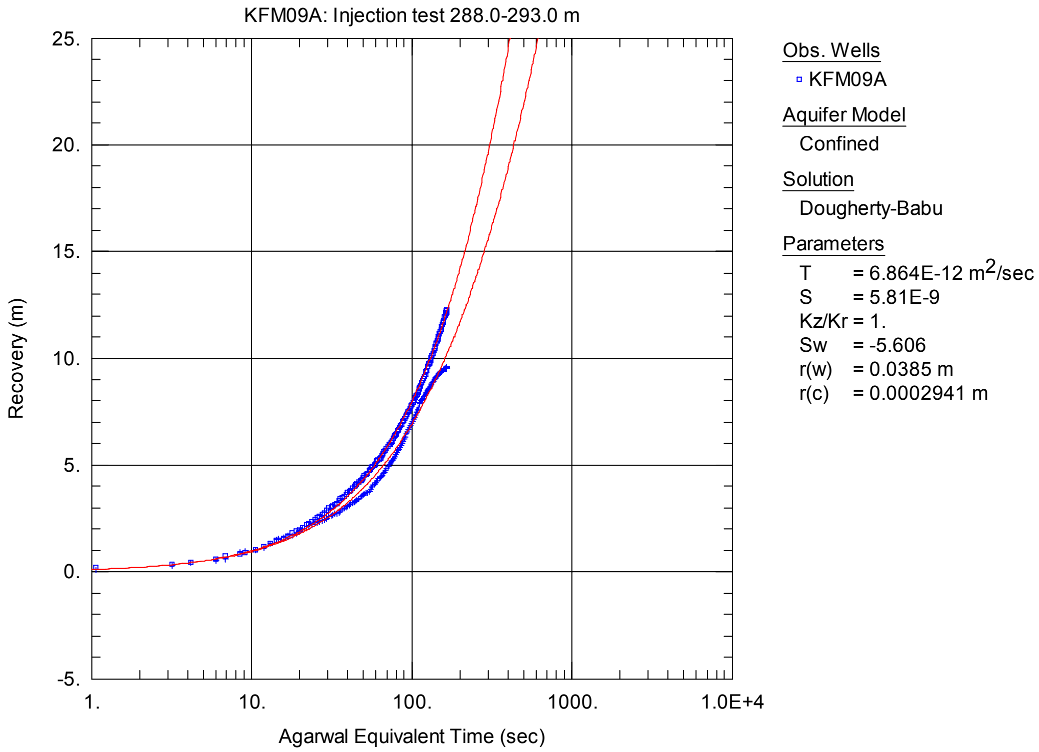


Figure A3-336. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 288.0-293.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.*

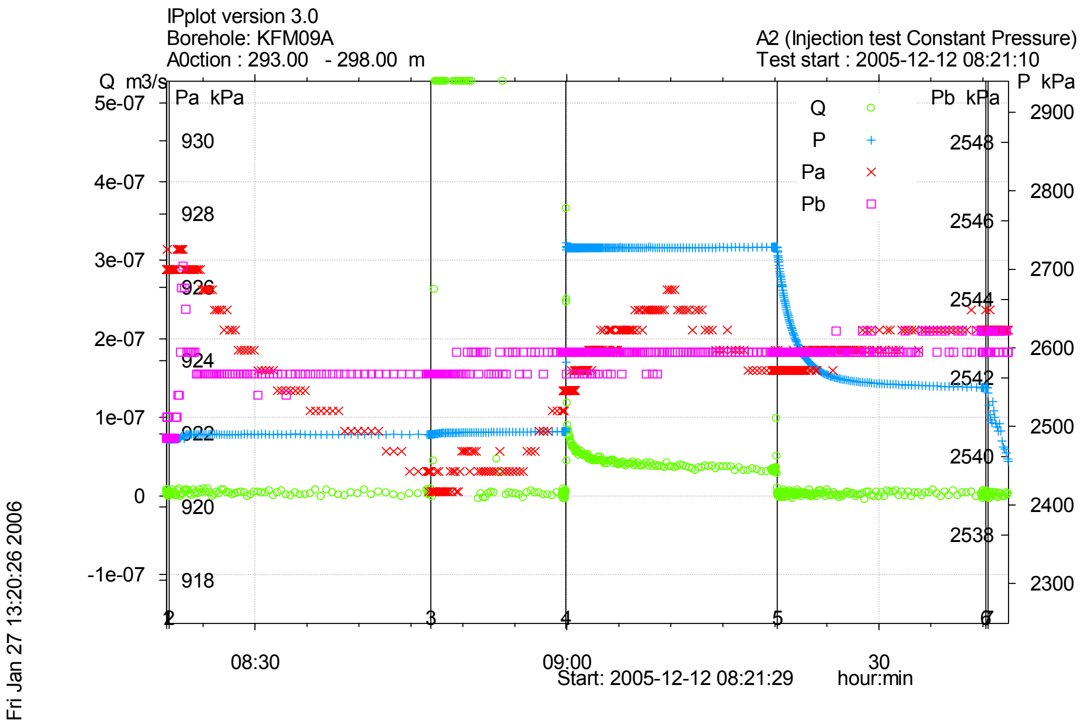


Figure A3-337. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 293.0-298.0 m in borehole KFM09A.*

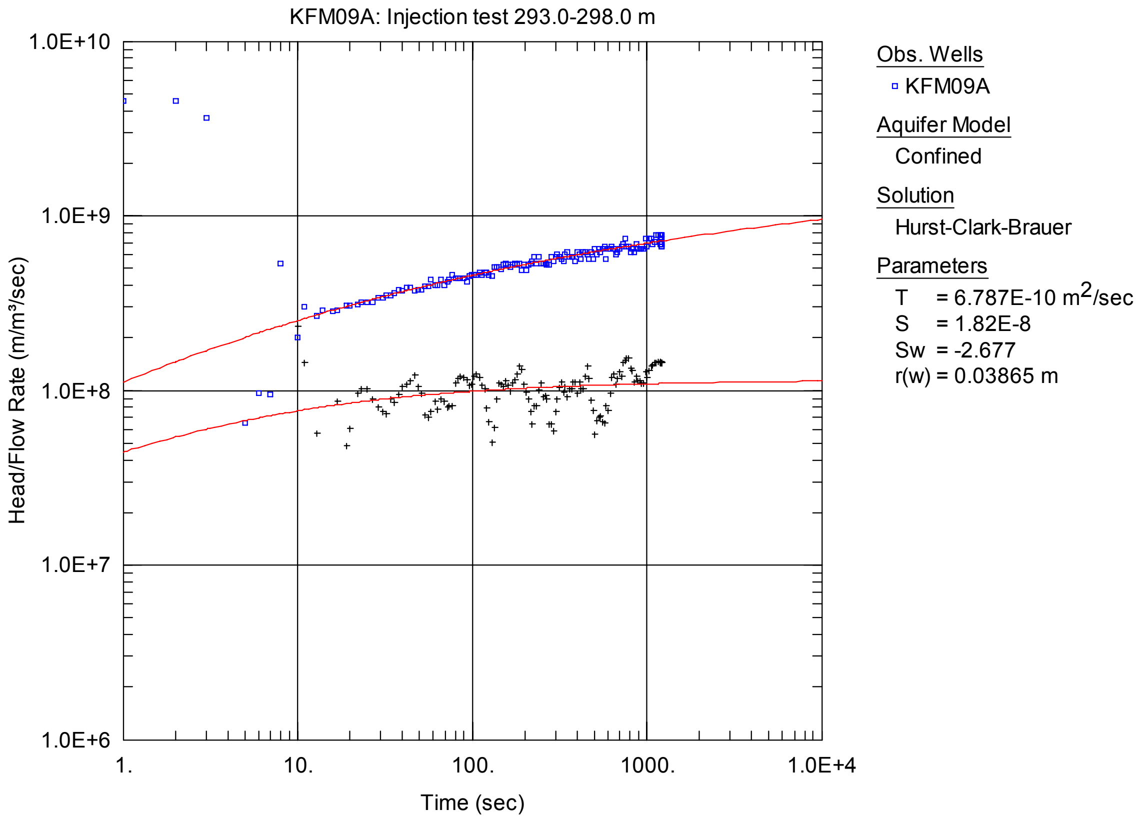


Figure A3-338. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 293.0-298.0 m in KFM09A.*

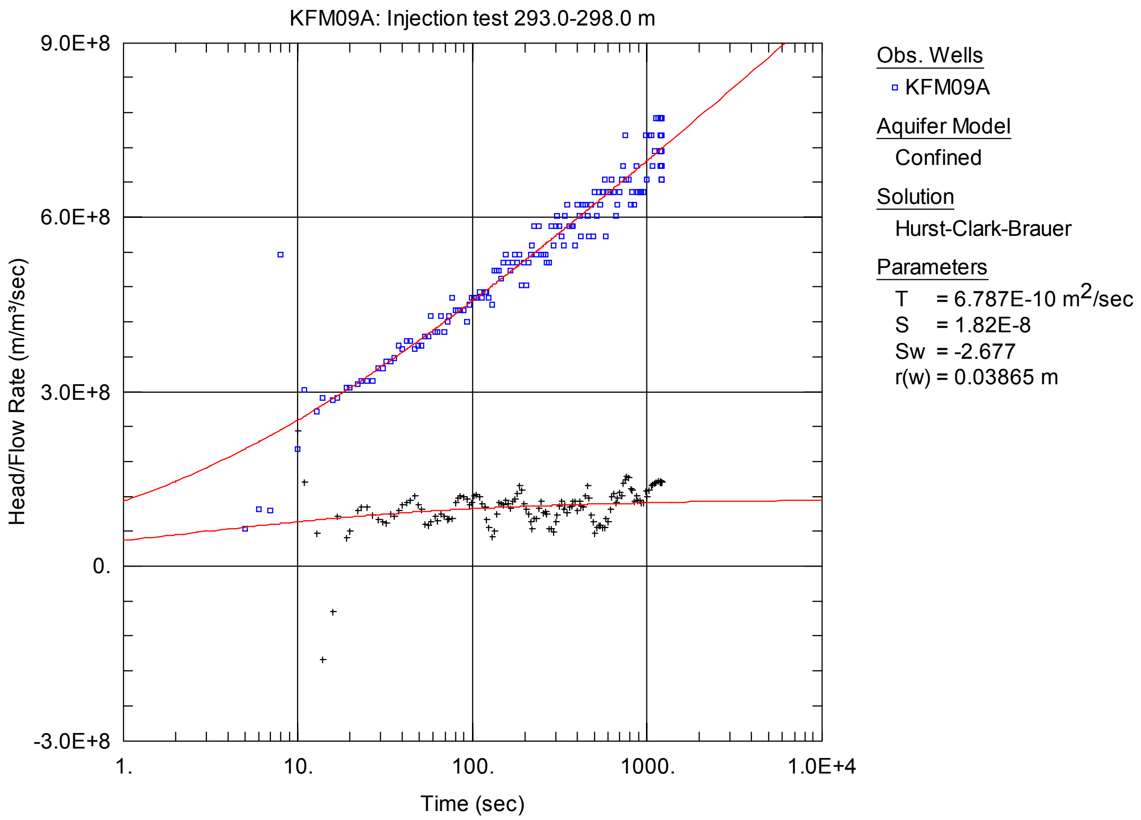


Figure A3-339. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 293.0-298.0 m in KFM09A.*

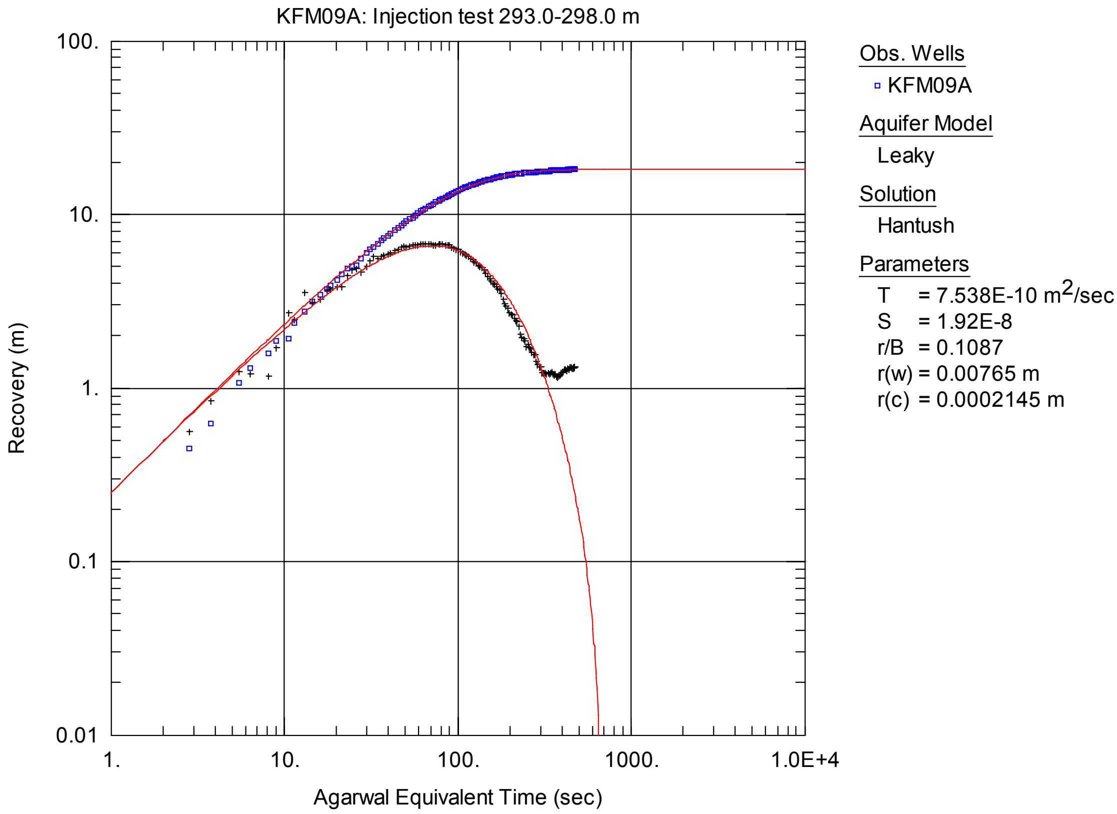


Figure A3-340. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 293.0-298.0 m in KFM09A.*

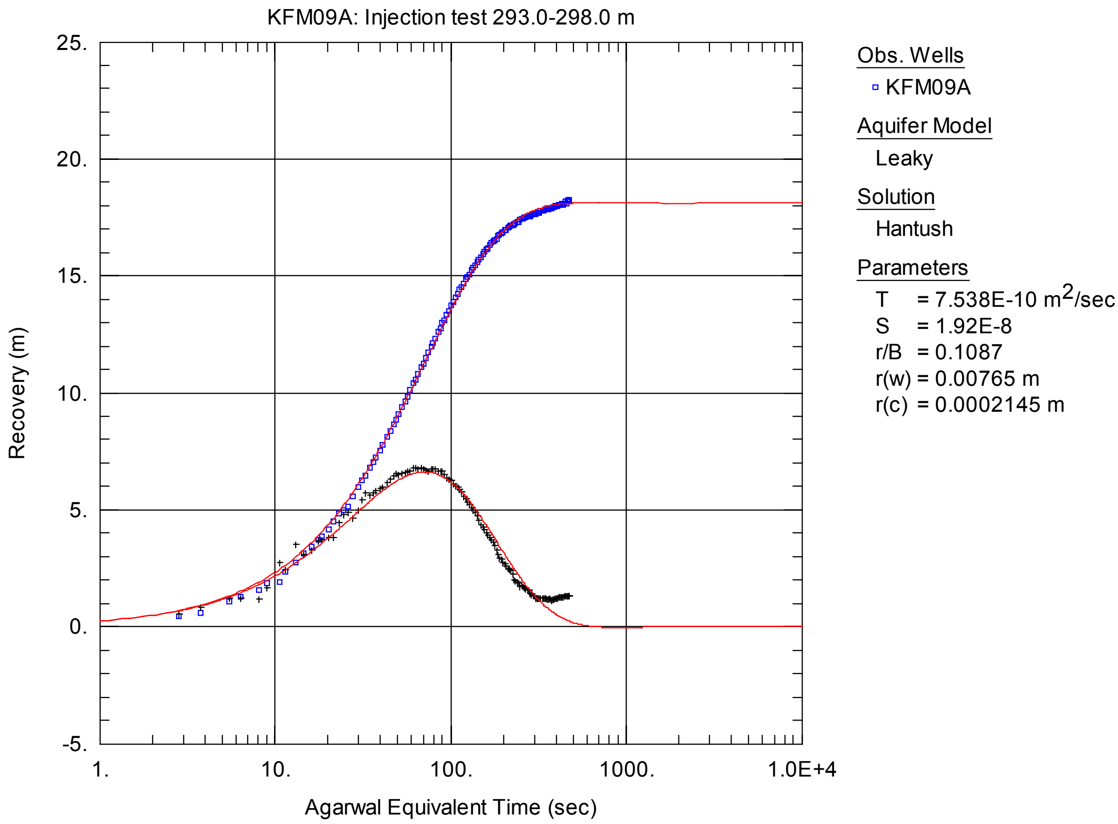


Figure A3-341. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 293.0-298.0 m in KFM09A.*

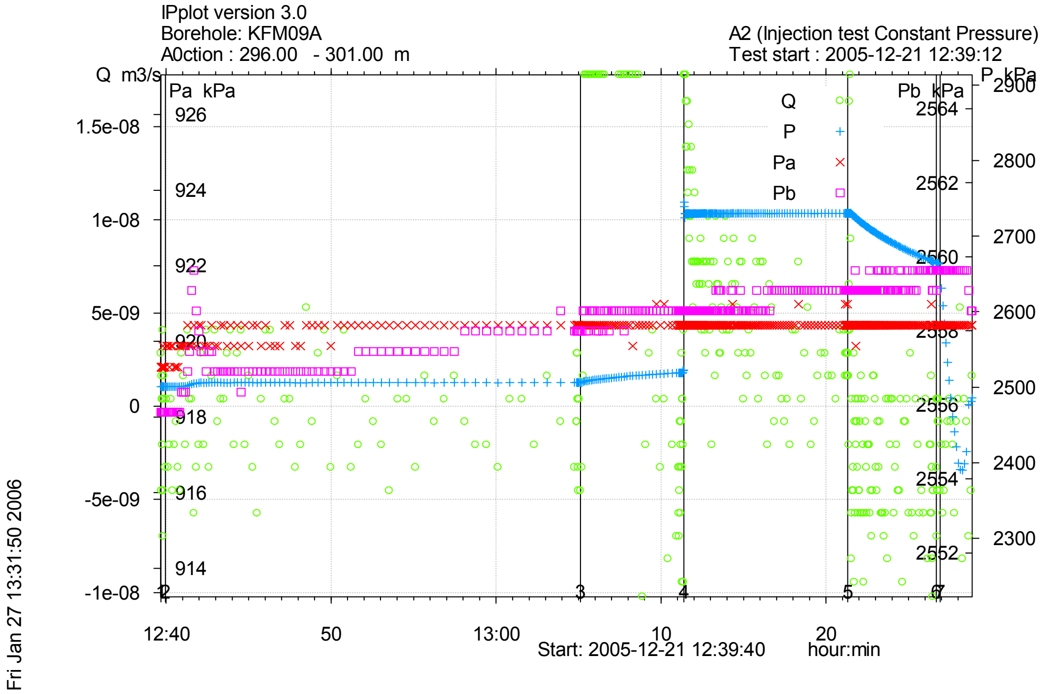


Figure A3-342. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 296.0-301.0 m in borehole KFM09A.*

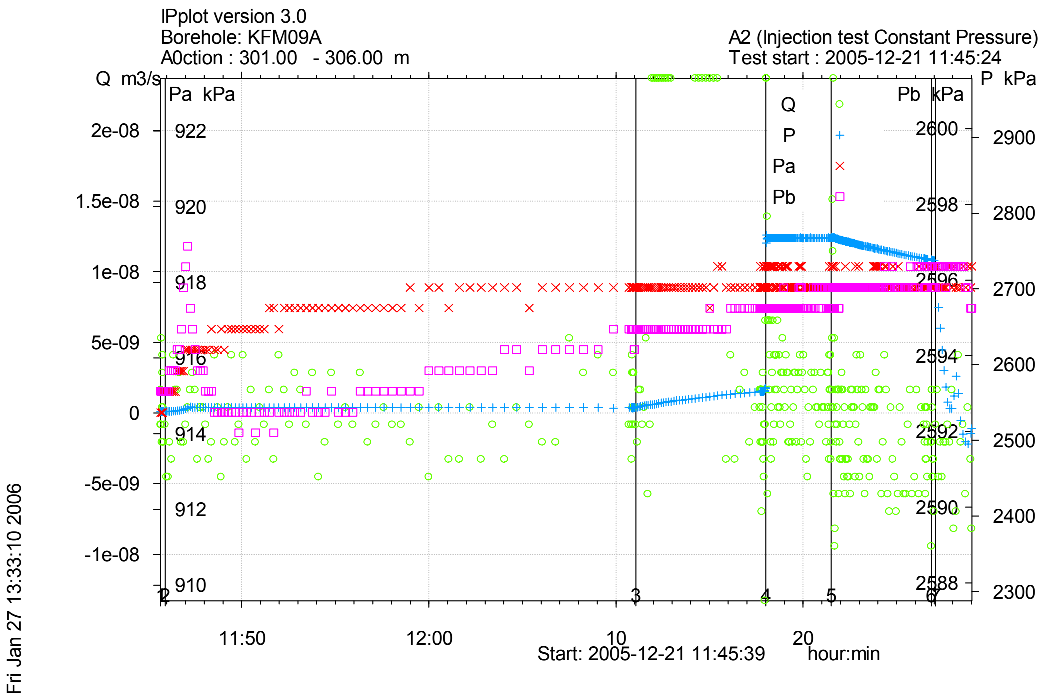


Figure A3-343. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 301.0-306.0 m in borehole KFM09A.*

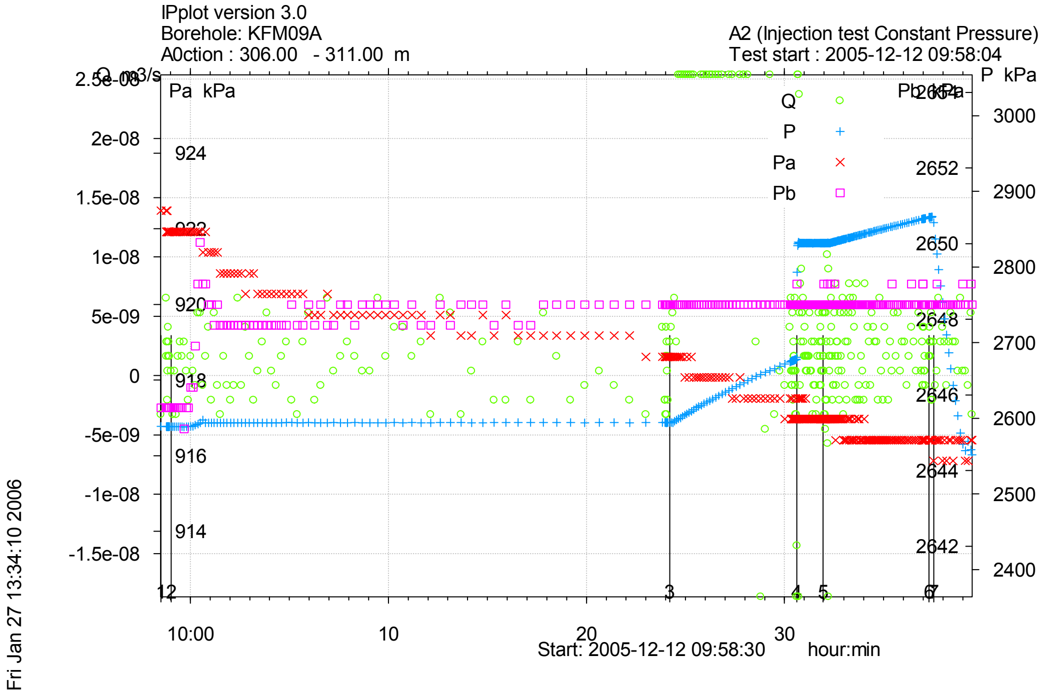


Figure A3-344. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 306.0-311.0 m in borehole KFM09A.*

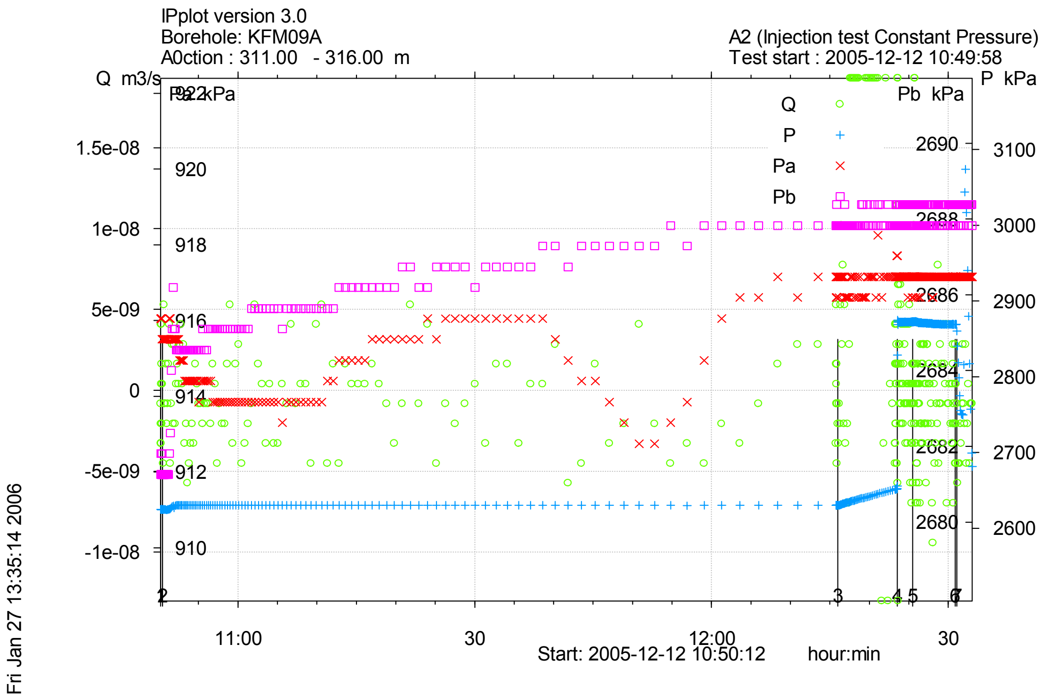


Figure A3-345. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 311.0-316.0 m in borehole KFM09A.*

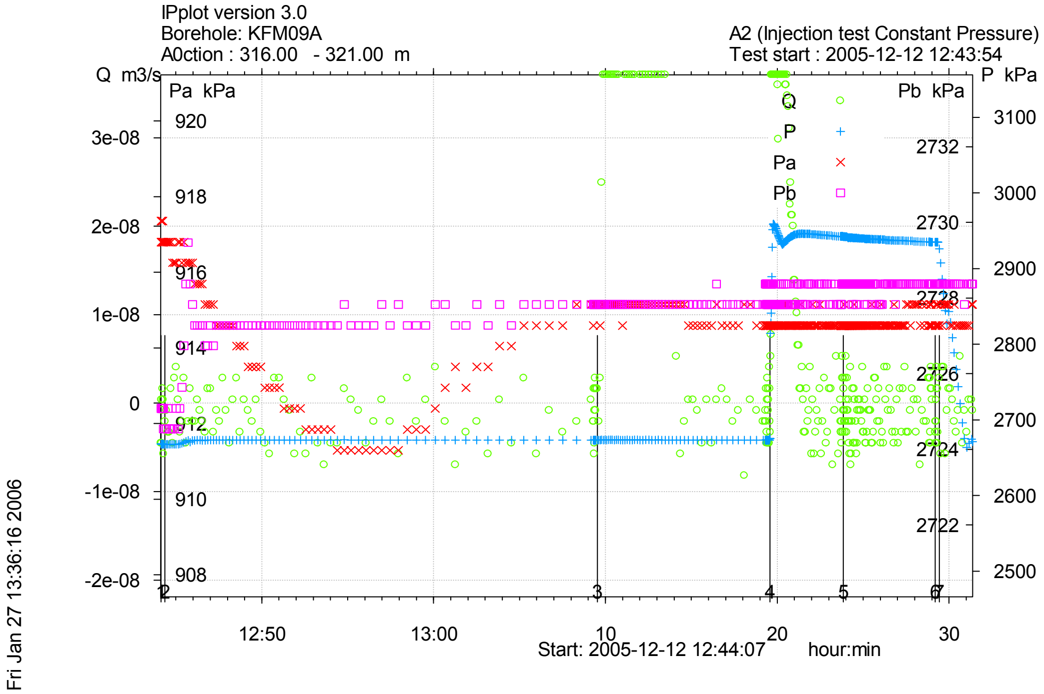


Figure A3-346. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 316.0-321.0 m in borehole KFM09A.*

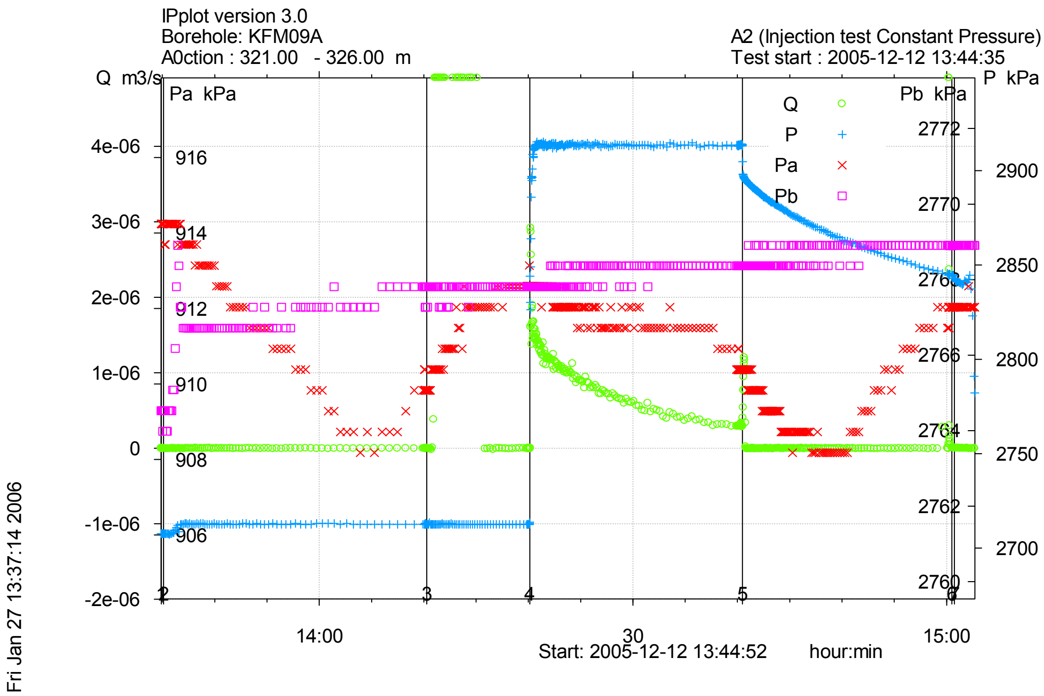


Figure A3-347. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 321.0-326.0 m in borehole KFM09A.*

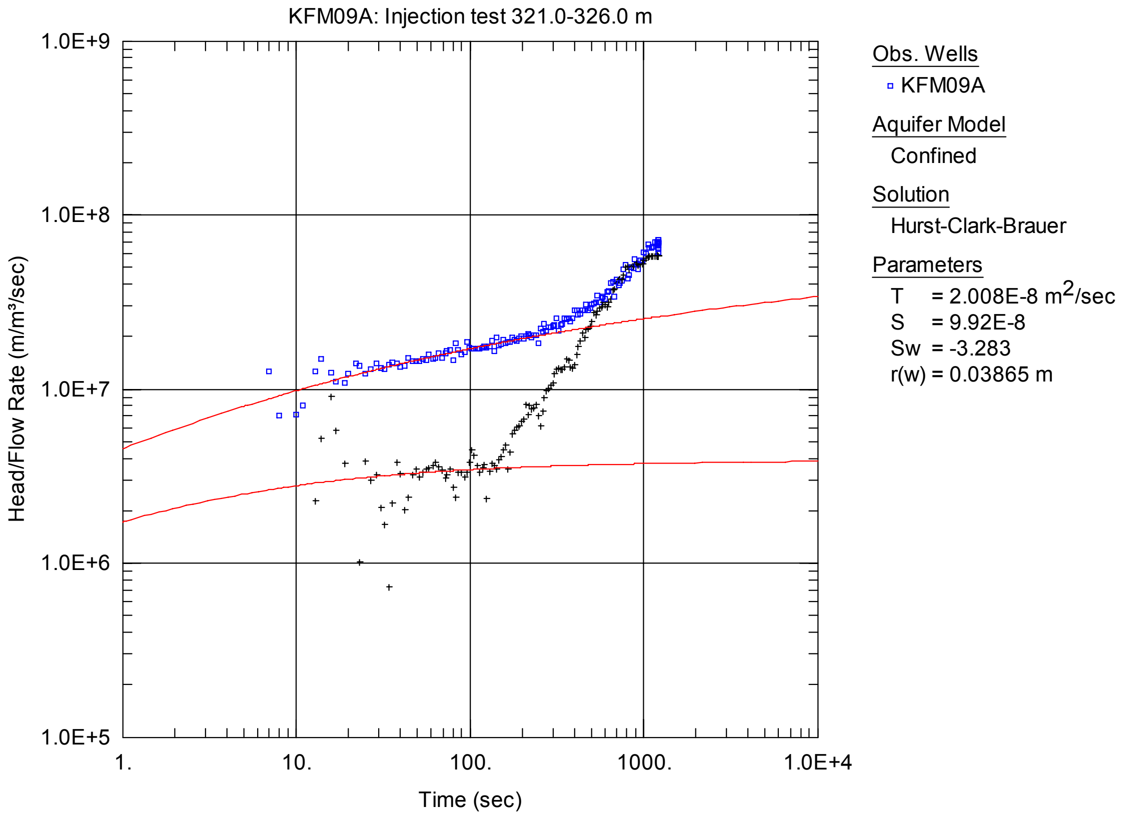


Figure A3-348. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 321.0-326.0 m in KFM09A.*

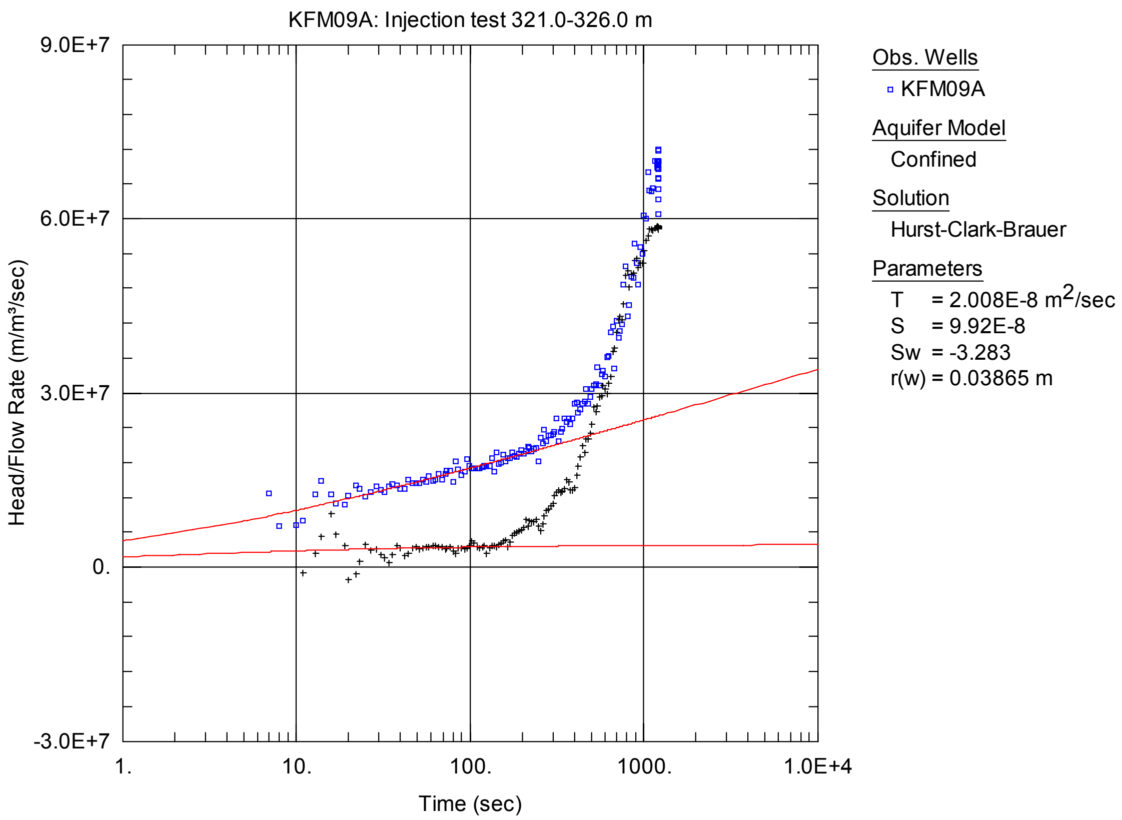


Figure A3-349. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 321.0-326.0 m in KFM09A.*

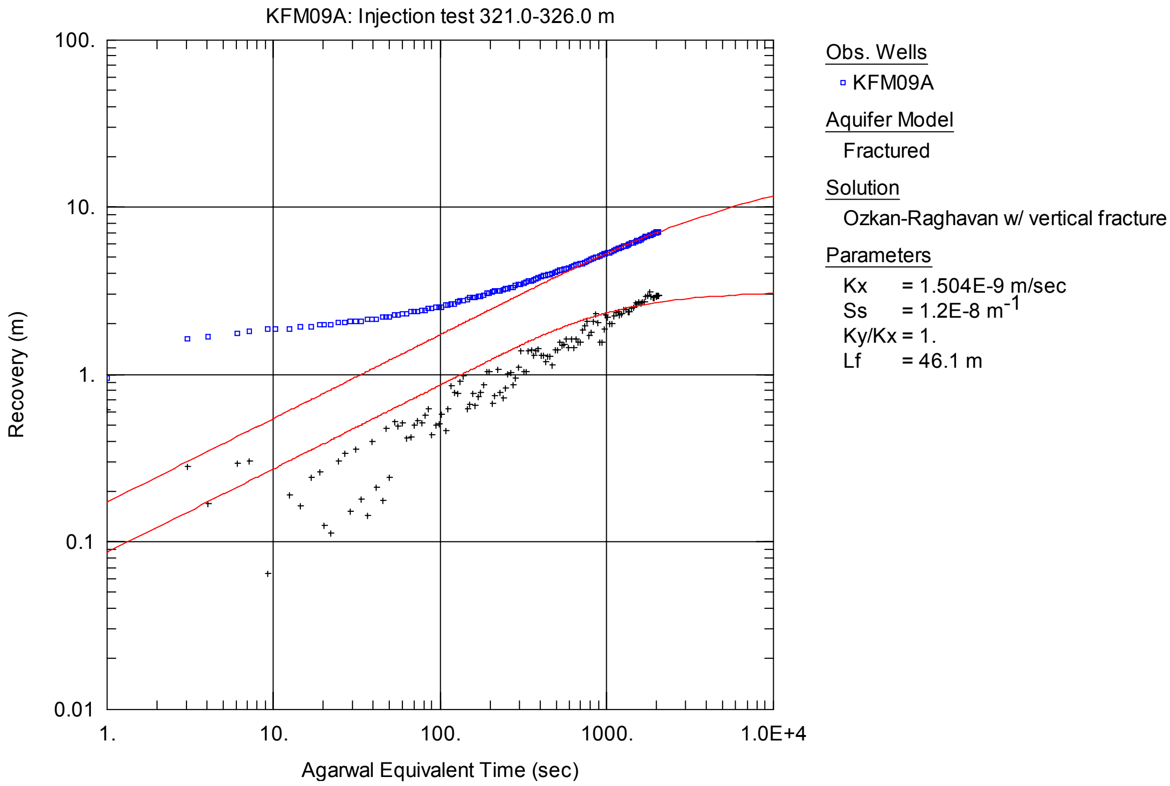


Figure A3-350. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 321.0-326.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.*

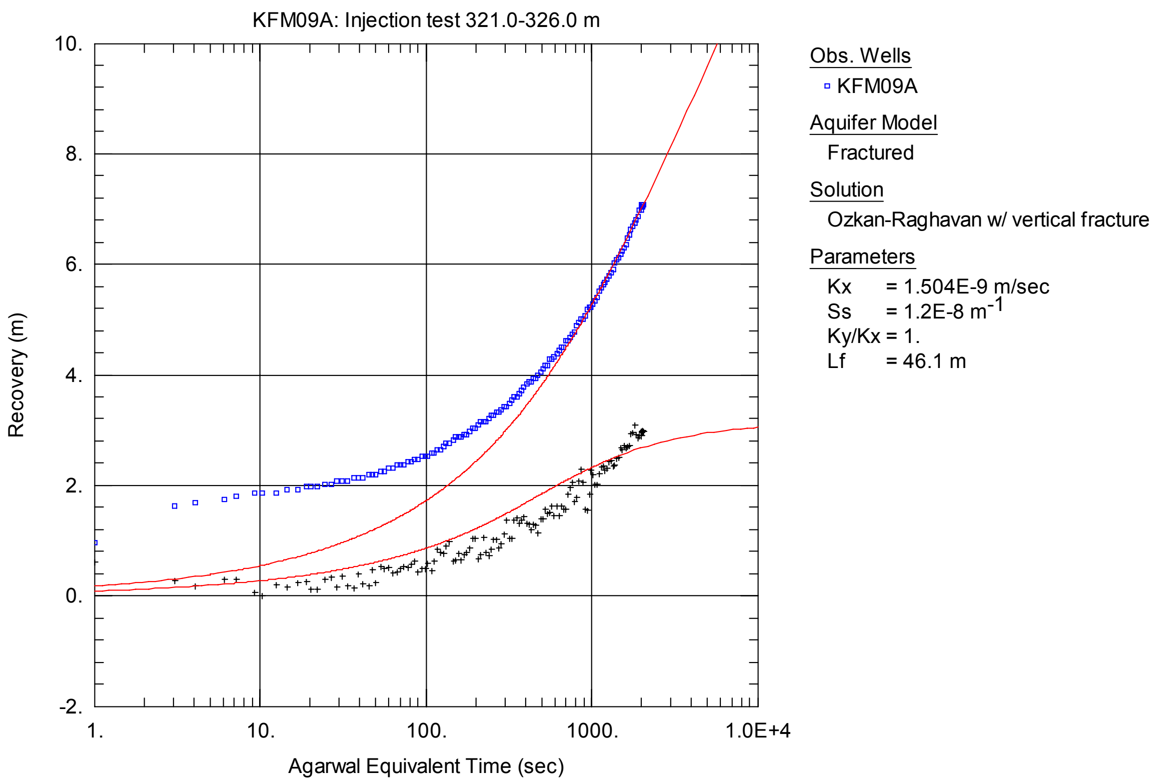


Figure A3-351. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 321.0-326.0 m in KFM09A No unambiguous transient evaluation is possible on the recovery period.*

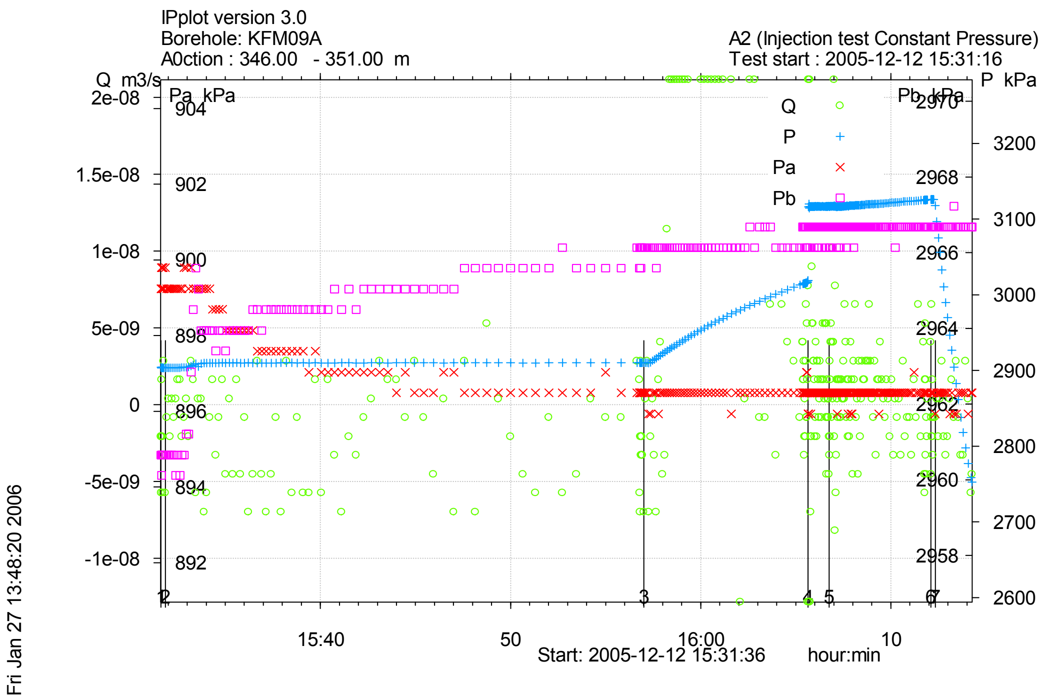


__Figure A3-352.__ Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 346.0-351.0 m in borehole KFM09A.

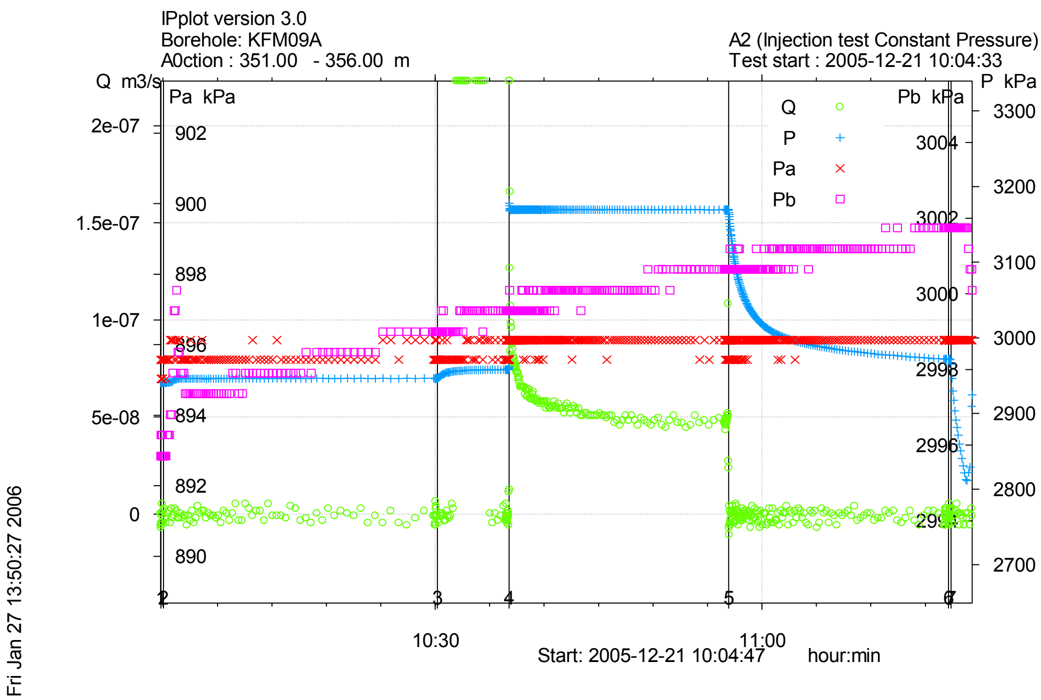


Figure A3-353. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 351.0-356.0 m in borehole KFM09A.*

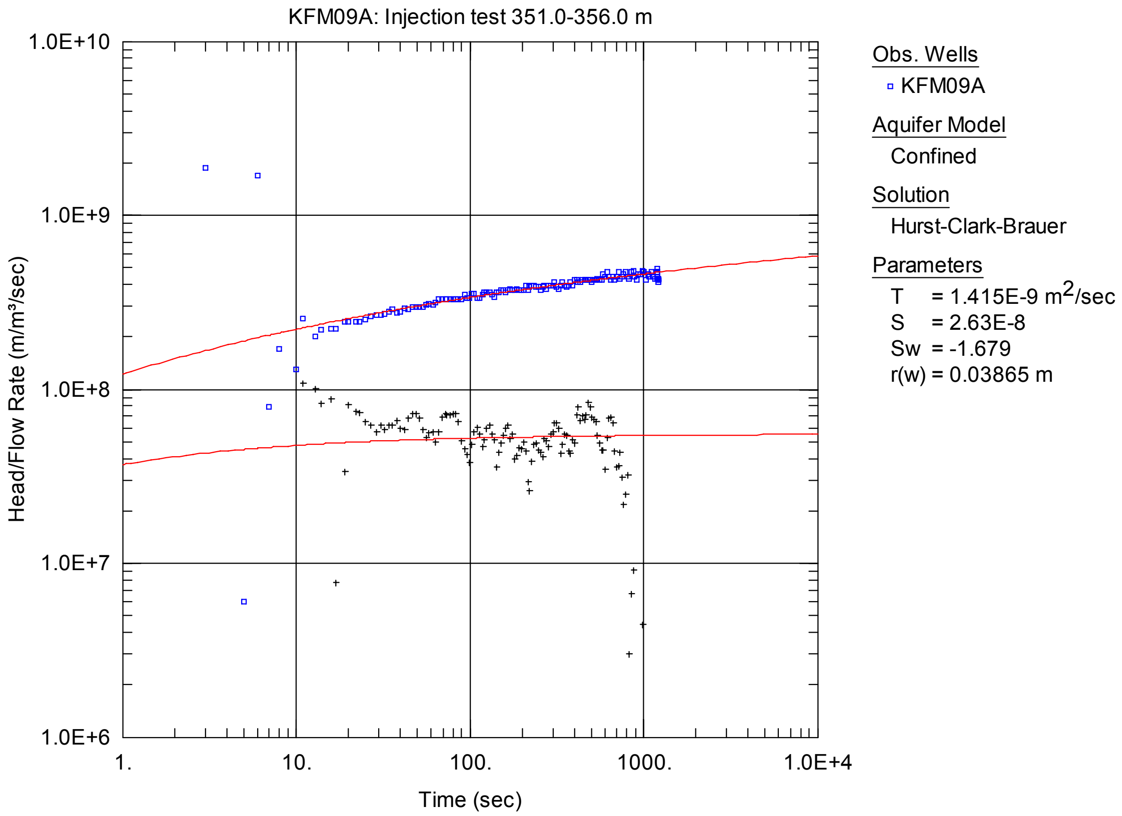


Figure A3-354. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 351.0-356.0 m in KFM09A.*

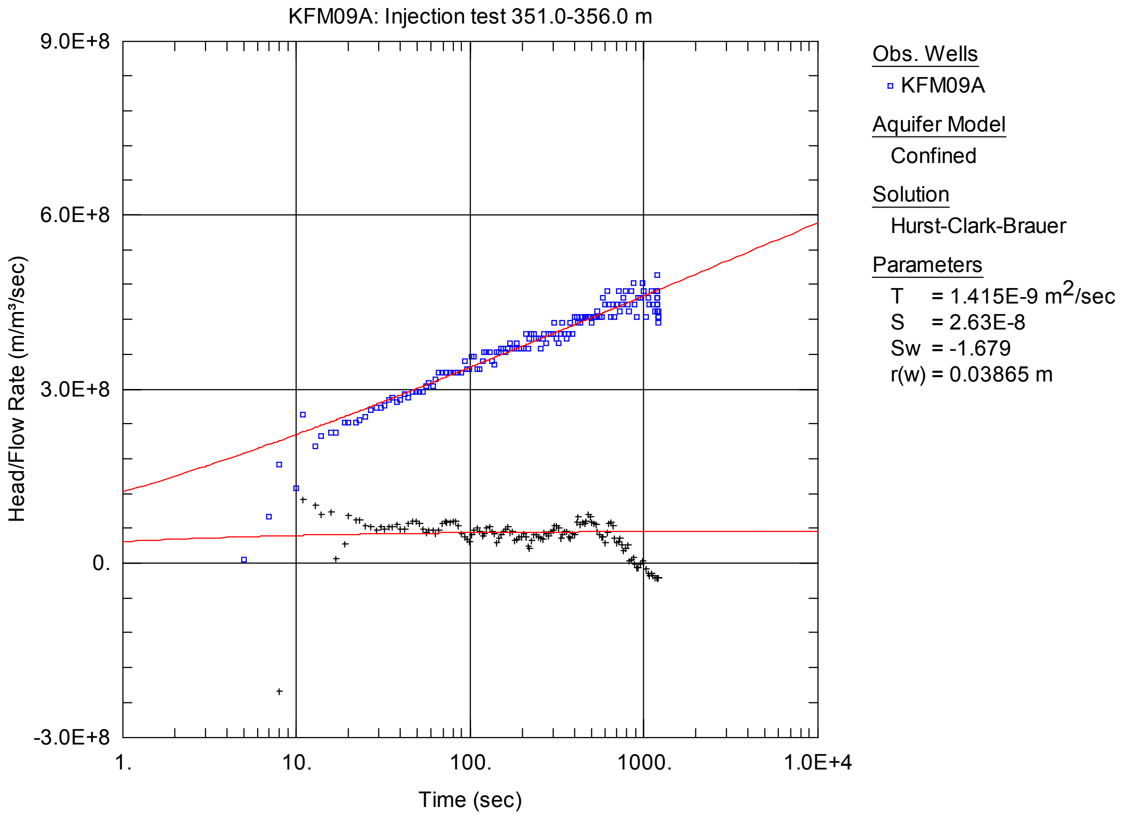


Figure A3-355. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 351.0-356.0 m in KFM09A.*

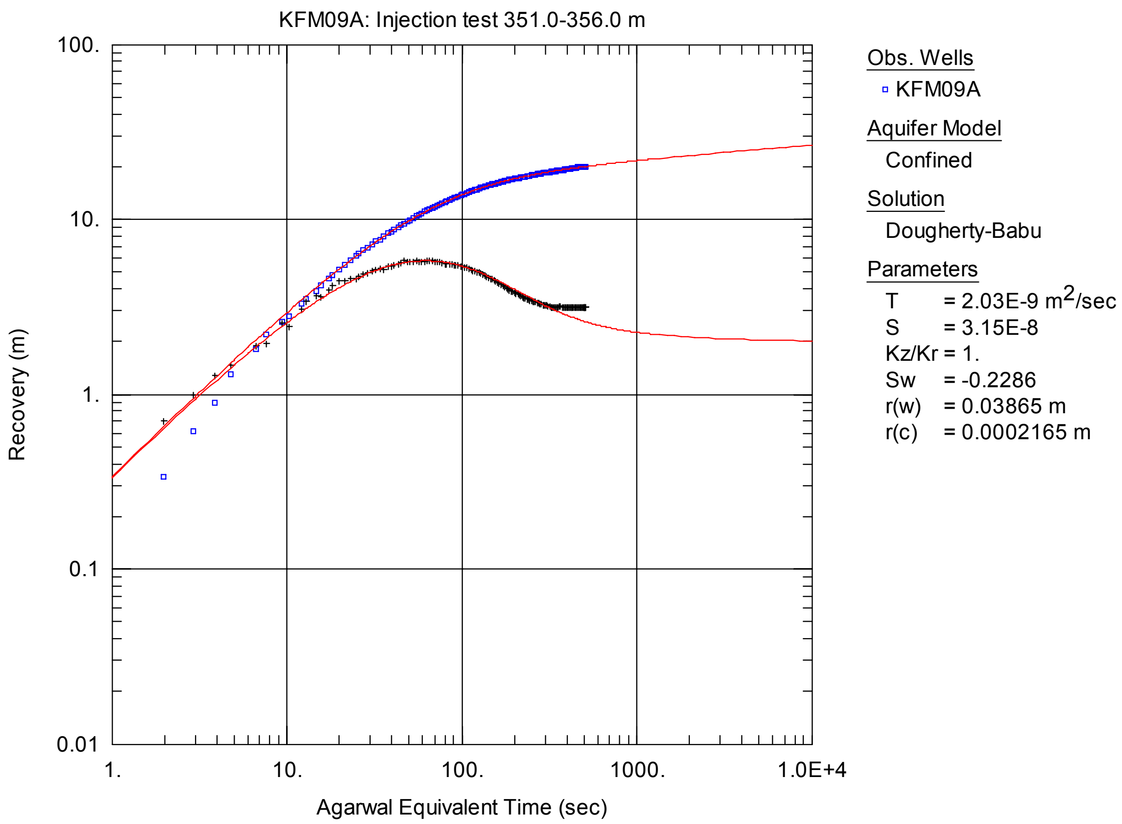


Figure A3-356. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 351.0-356.0 m in KFM09A.*

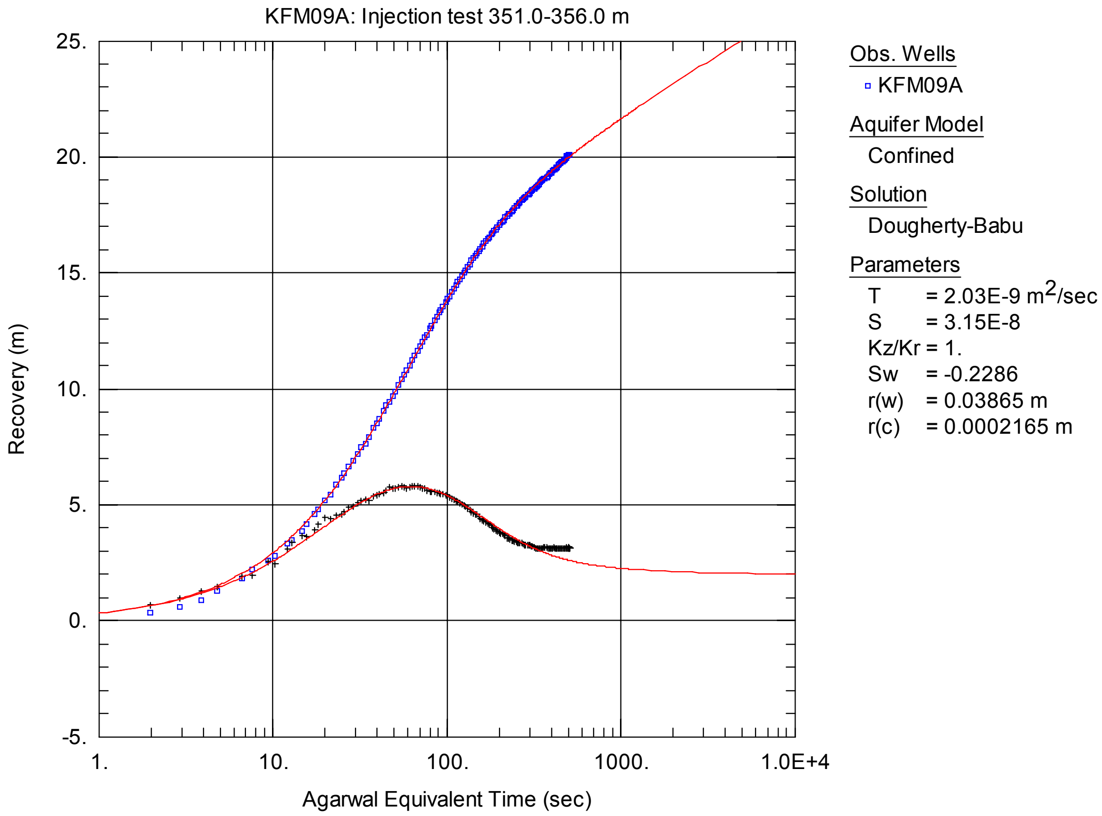


Figure A3-357. Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 351.0-356.0 m in KFM09A.

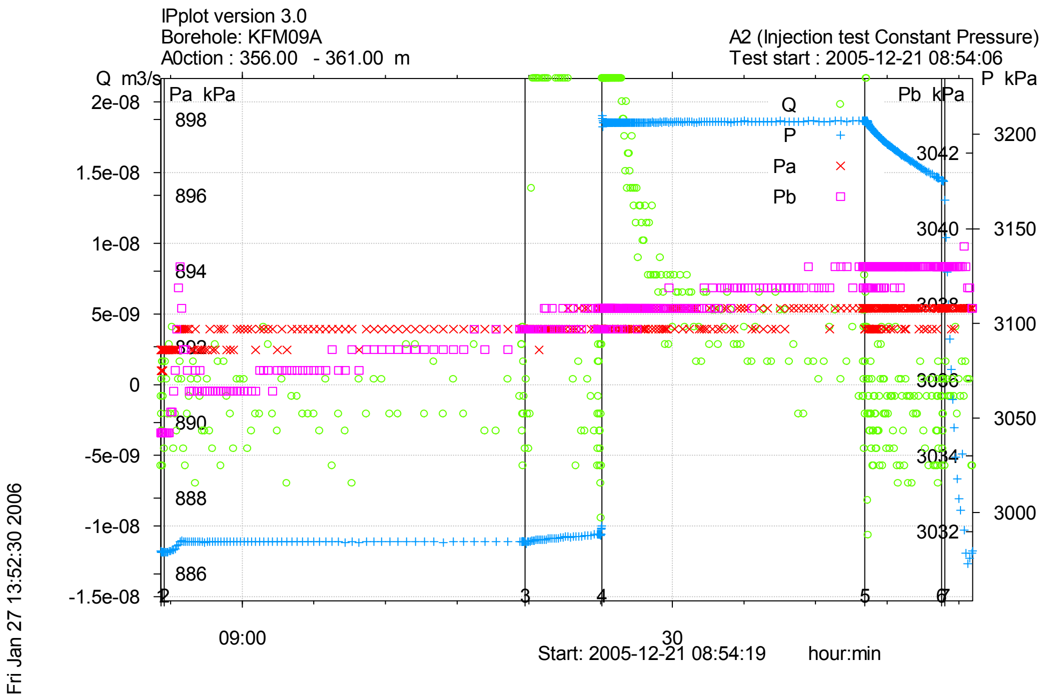


Figure A3-358. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 356.0-361.0 m in borehole KFM09A.

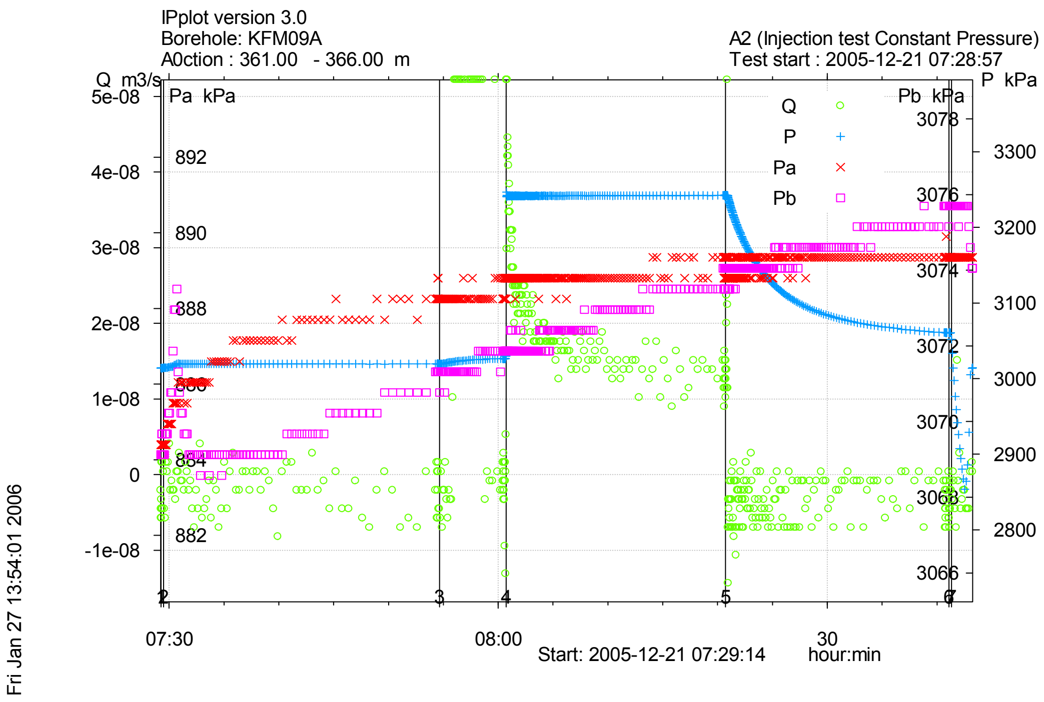


Figure A3-359. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 361.0-366.0 m in borehole KFM09A.*

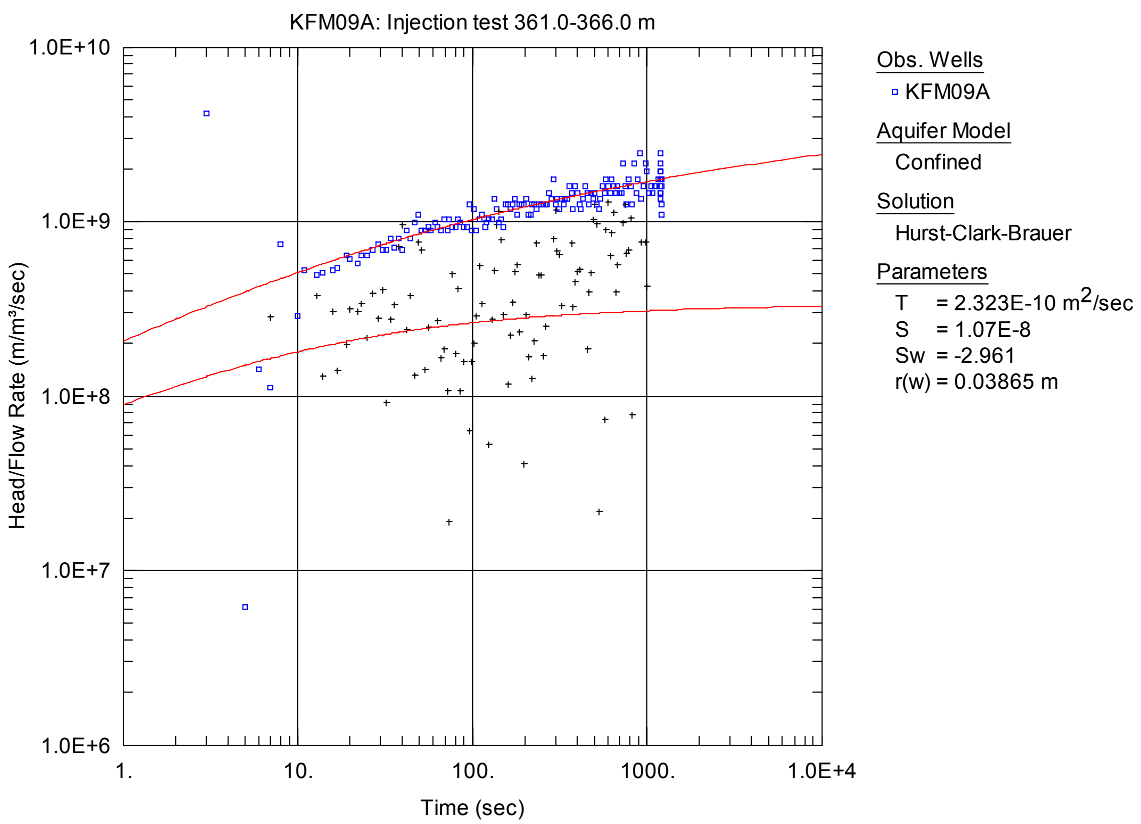


Figure A3-360. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 361.0-366.0 m in KFM09A.*

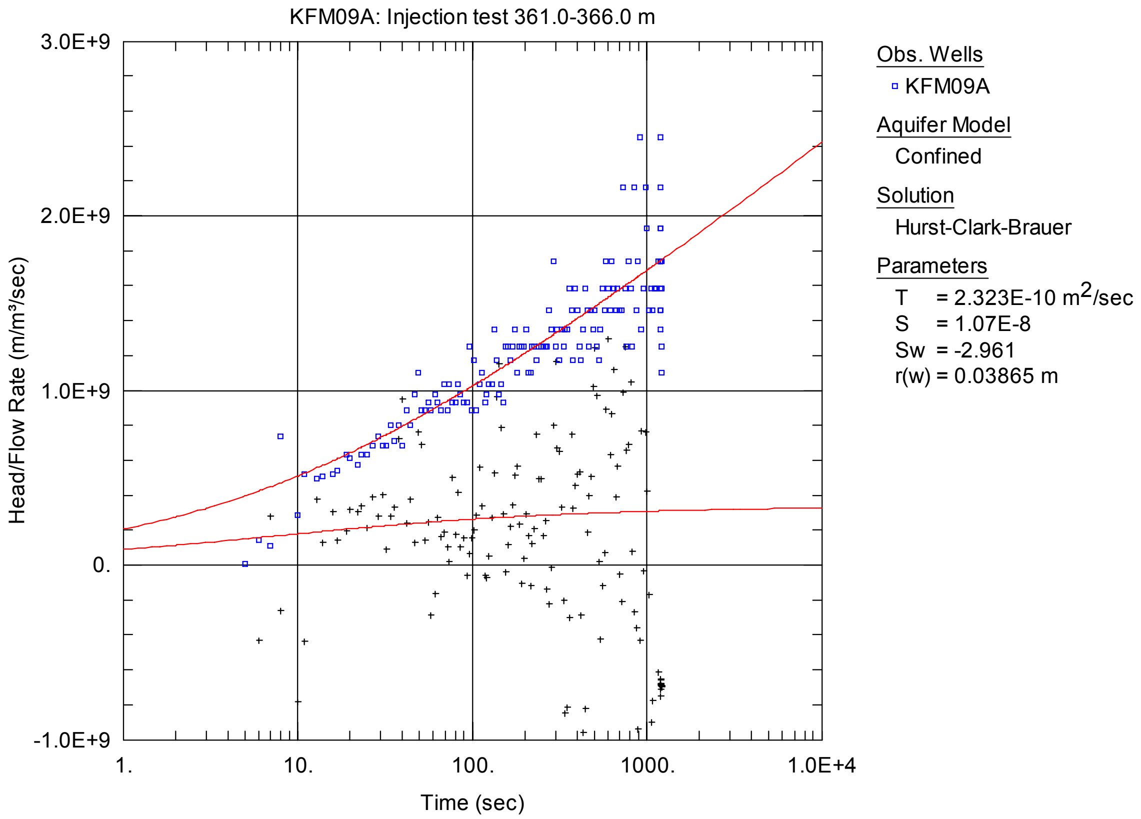


***Figure A3-361.** Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 361.0-366.0 m in KFM09A.*

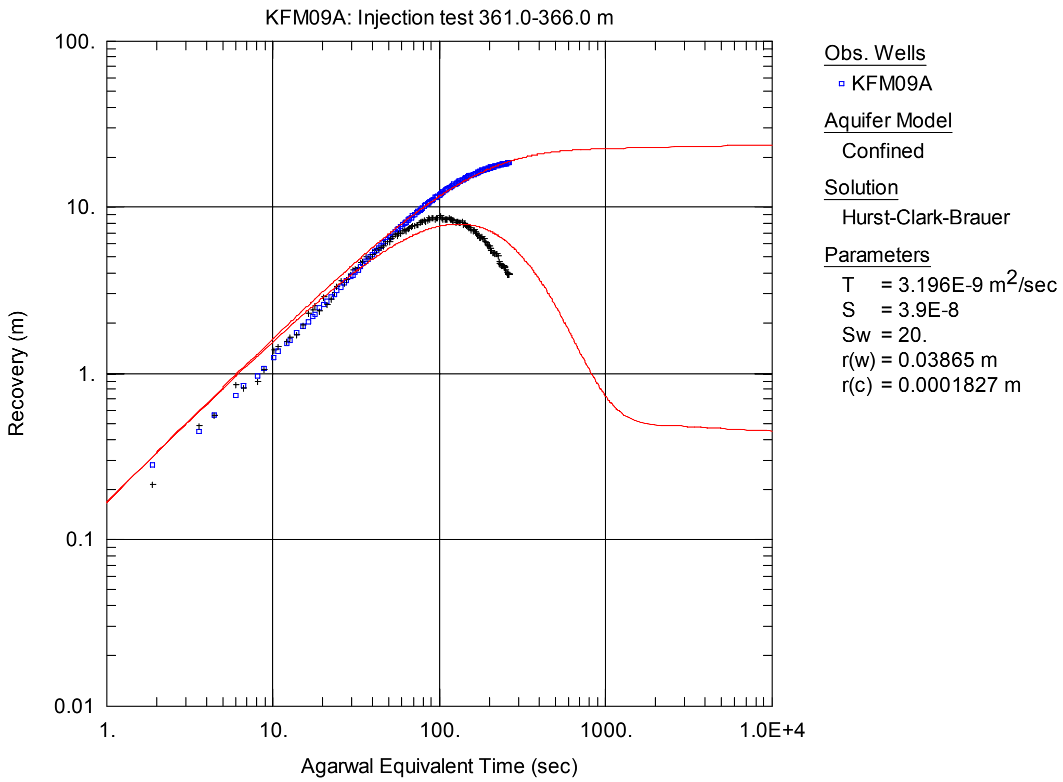


***Figure A3-362.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 361.0-366.0 m in KFM09A. No unambiguous transient evaluation could be made from the recovery period.*

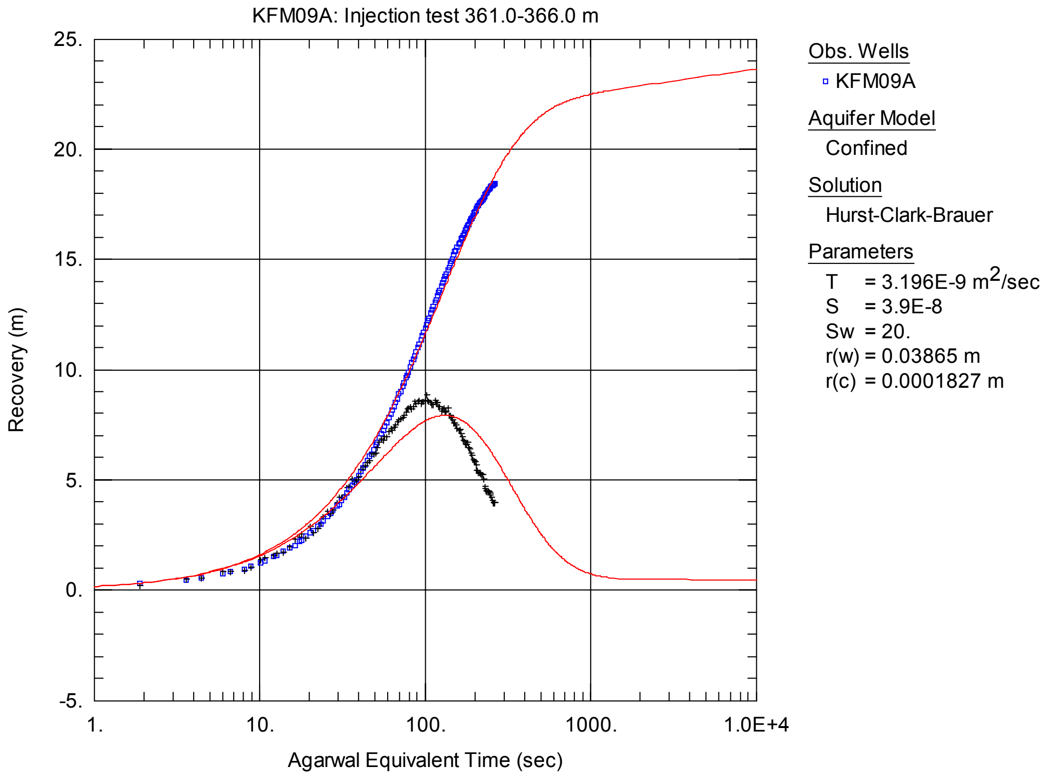


Figure A3-363. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 361.0-366.0 m in KFM09A. No unambiguous transient evaluation could be made from the recovery period.*

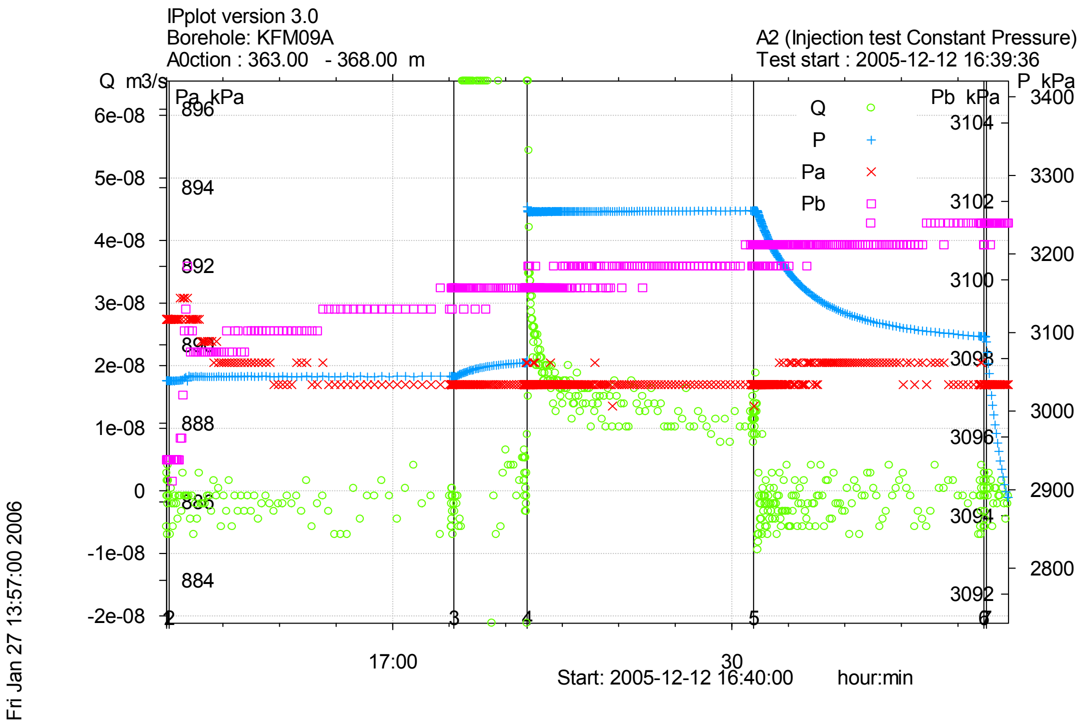


Figure A3-364. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 363.0-368.0 m in borehole KFM09A.*

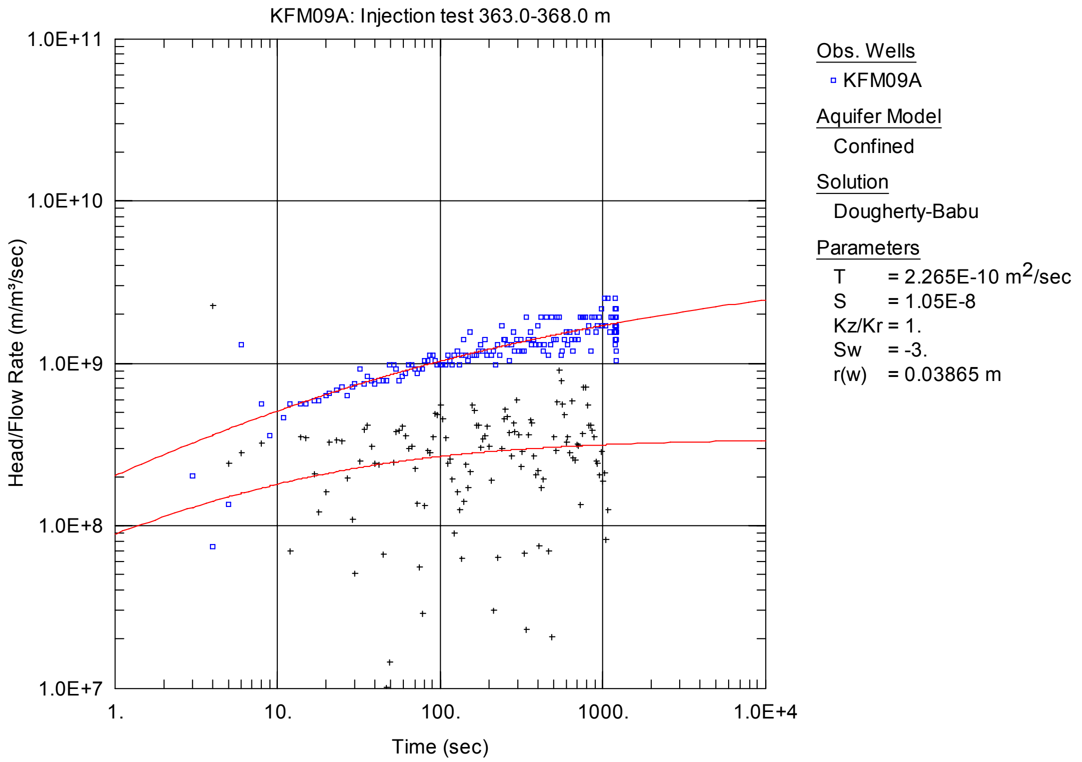


Figure A3-365. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 363.0-368.0 m in KFM09A.*

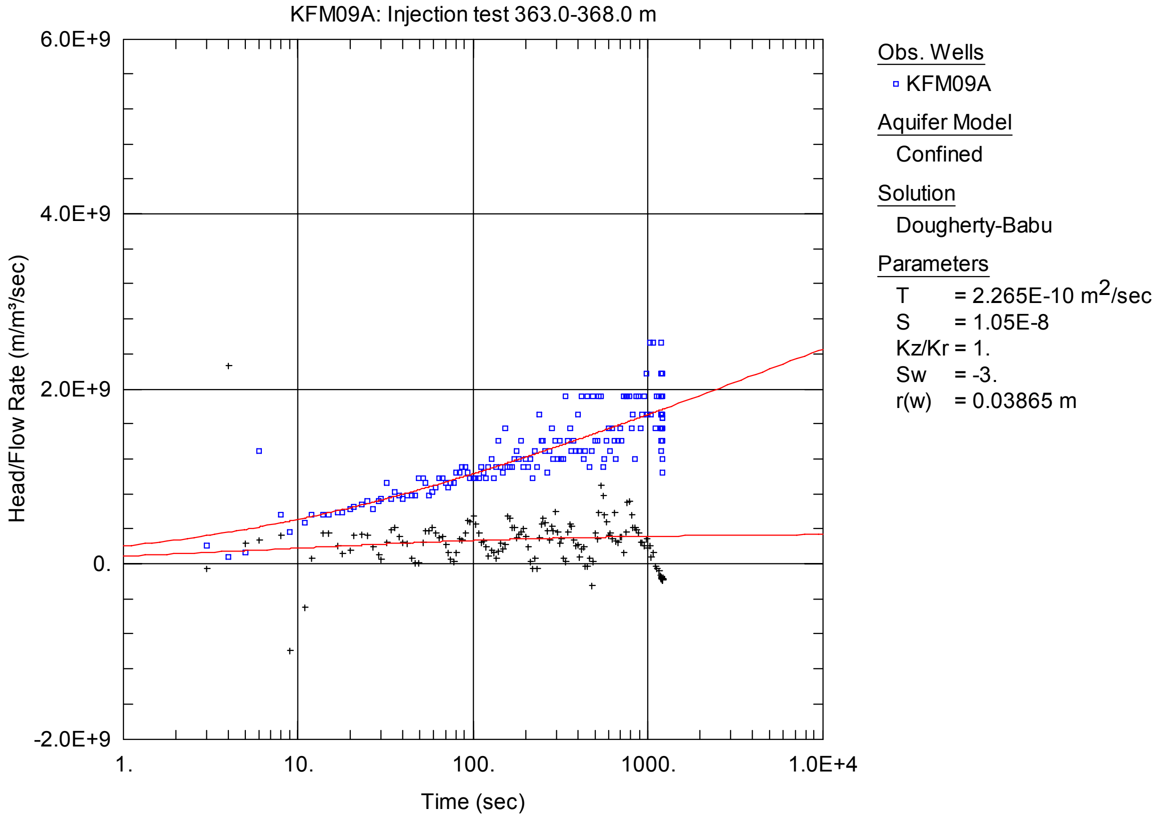


Figure A3-366. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 363.0-368.0 m in KFM09A.*

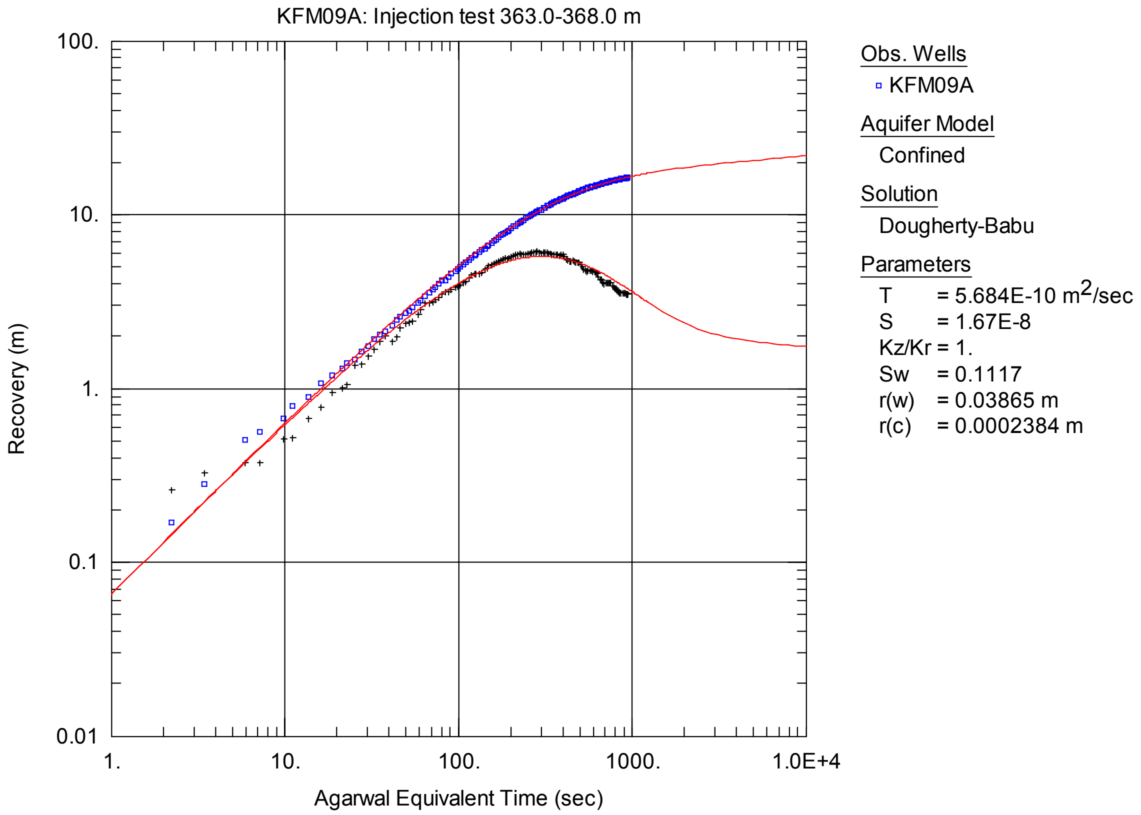


***Figure A3-367.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 363.0-368.0 m in KFM09A.*

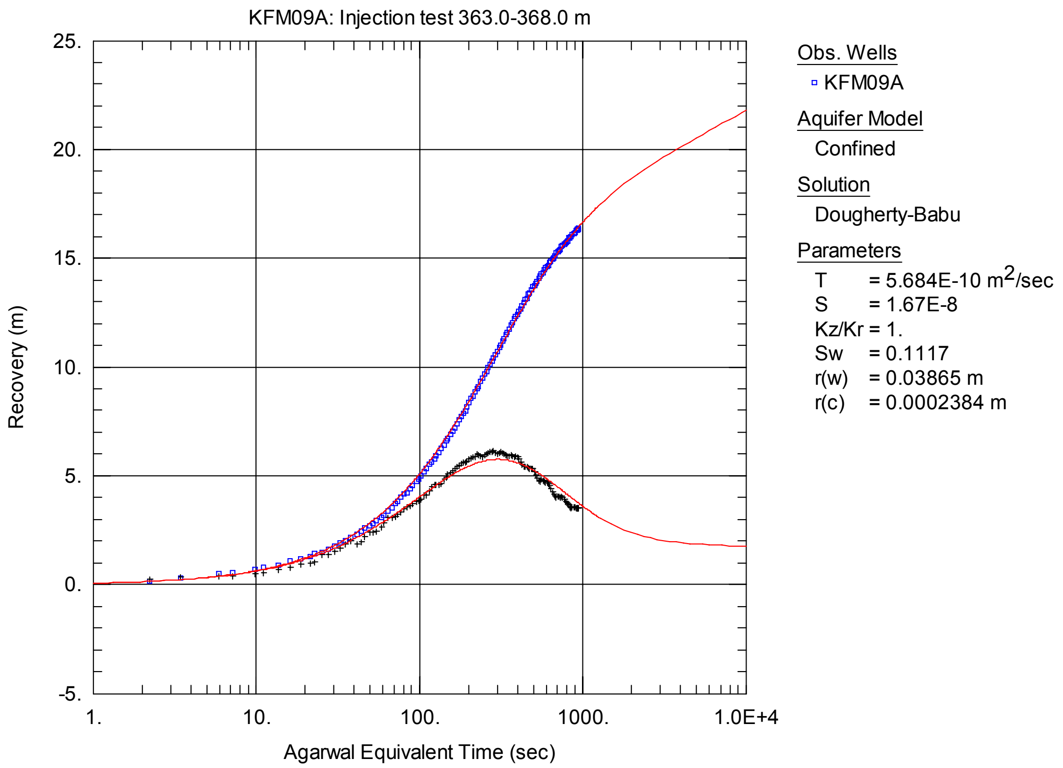


***Figure A3-368.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 363.0-368.0 m in KFM09A.*

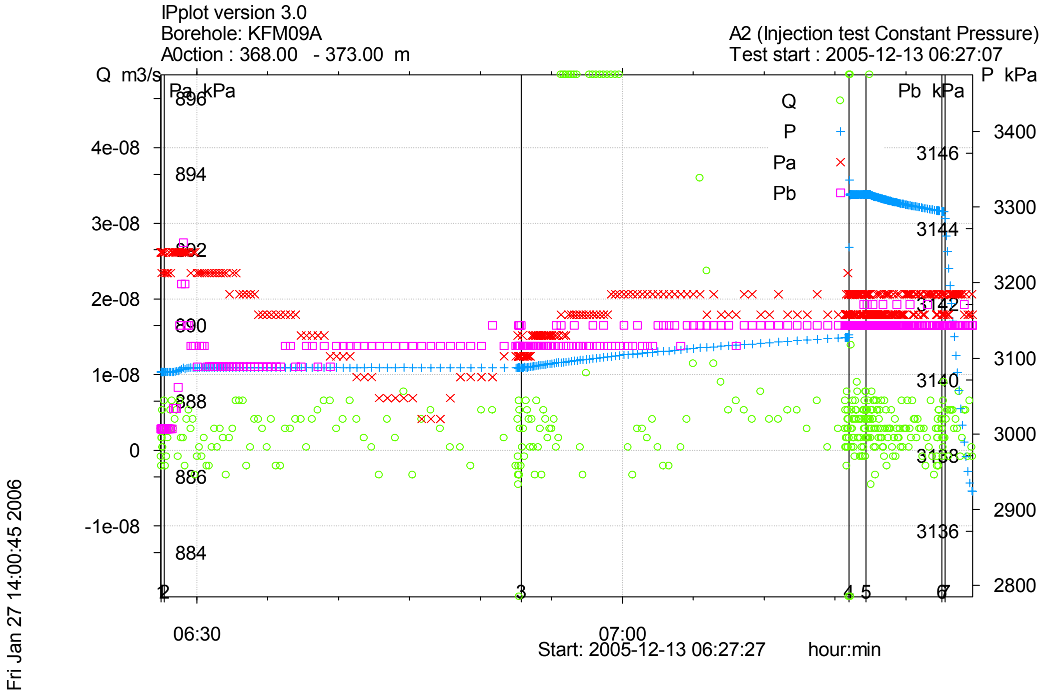


Figure A3-369. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 368.0-373.0 m in borehole KFM09A.*

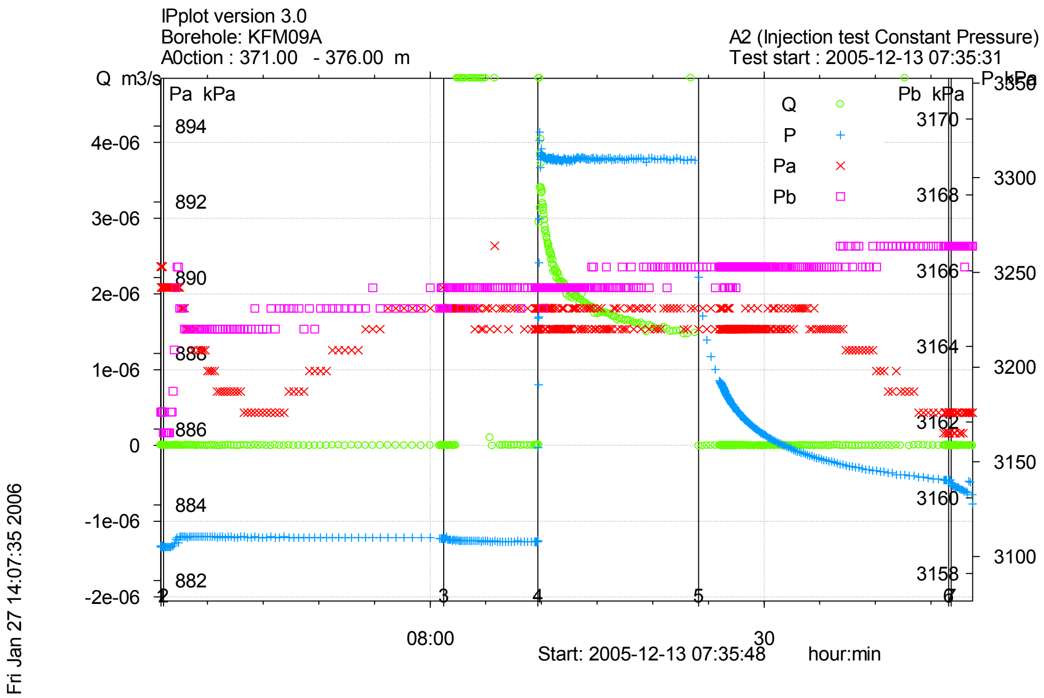


Figure A3-370. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 371.0-376.0 m in borehole KFM09A.*

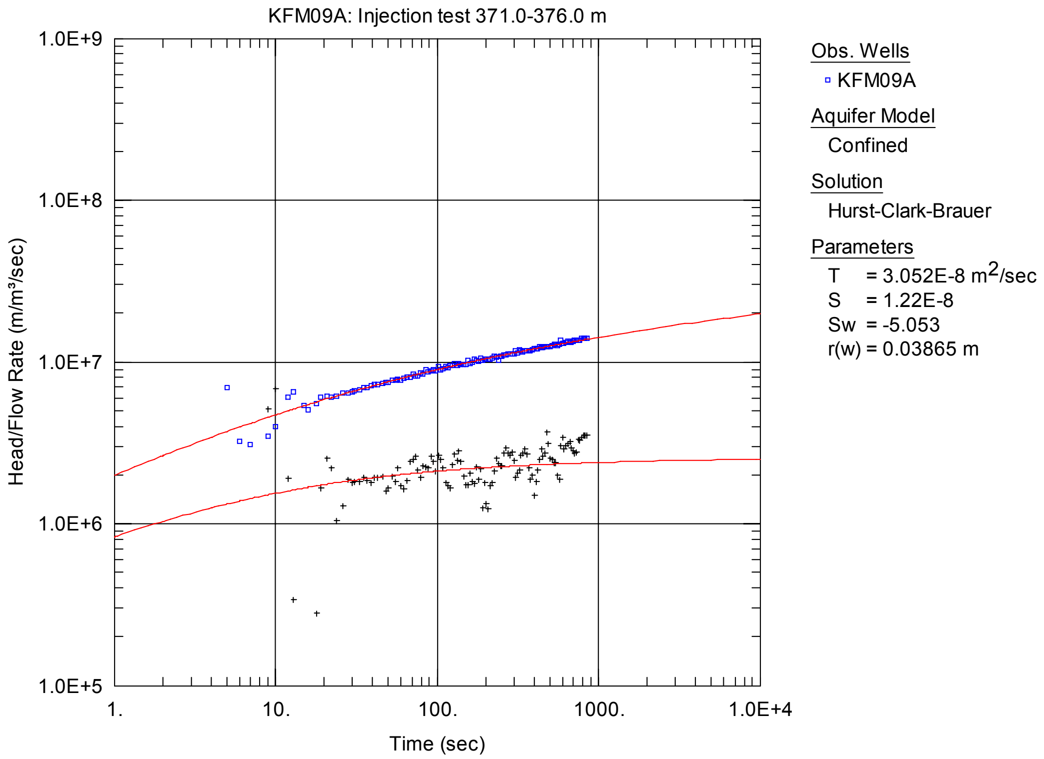


Figure A3-371. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 371.0-376.0 m in KFM09A.*

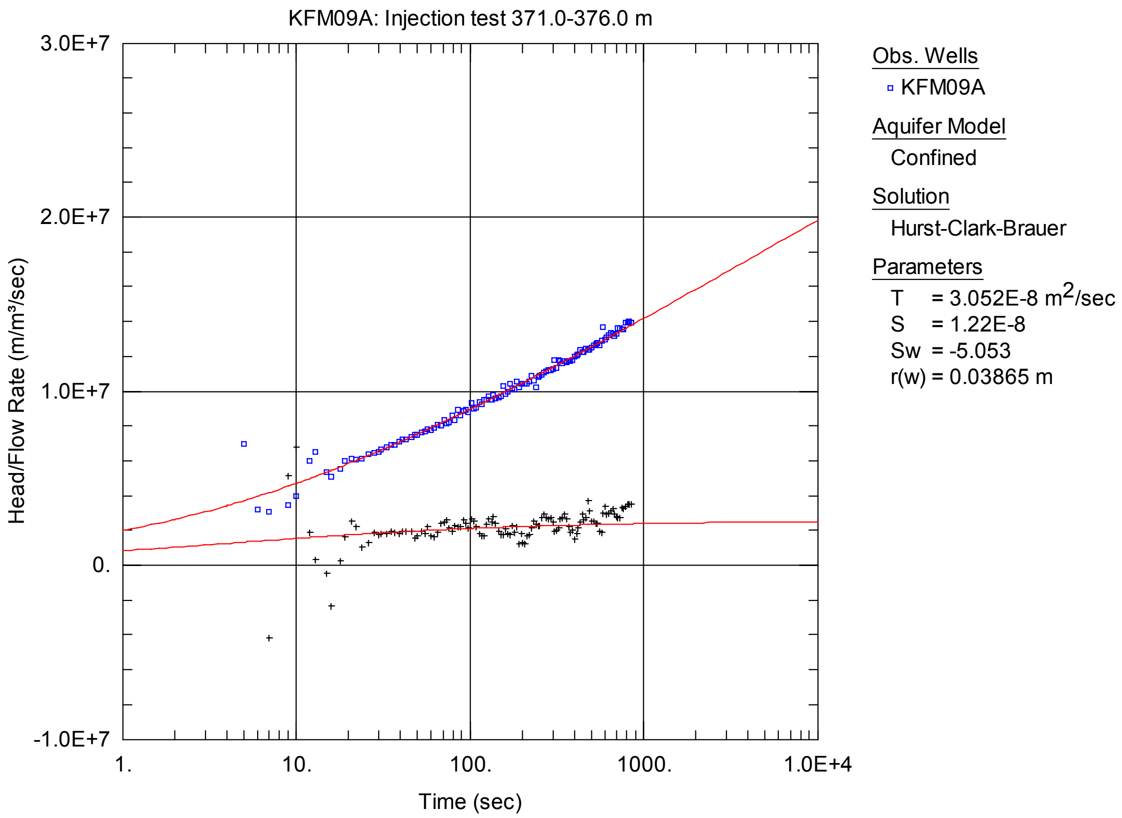


Figure A3-372. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 371.0-376.0 m in KFM09A.*

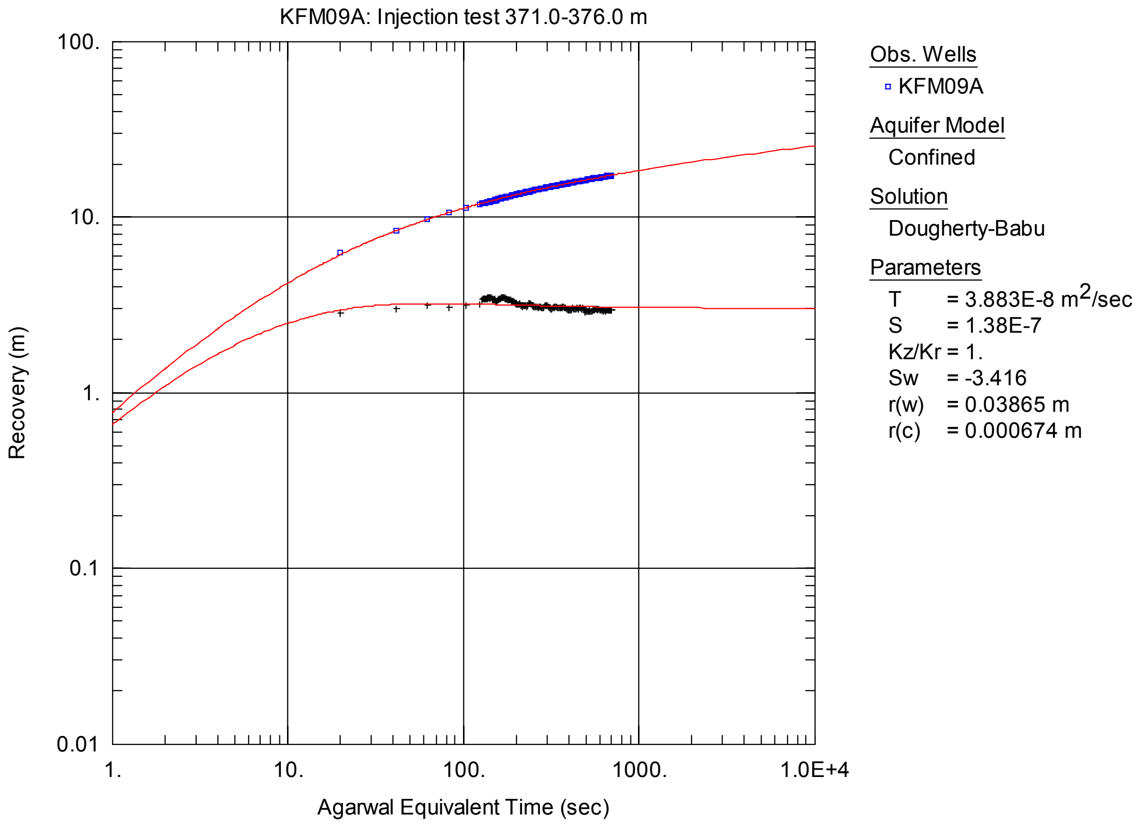


Figure A3-373. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 371.0-376.0 m in KFM09A.*

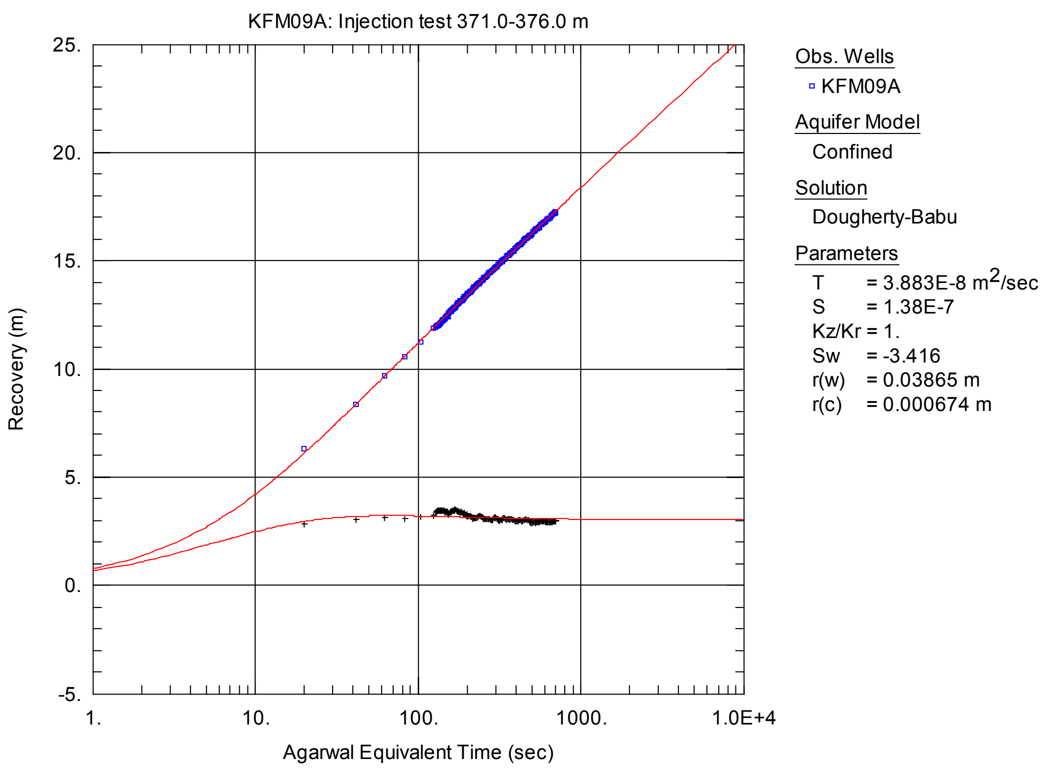


Figure A3-374. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 371.0-376.0 m in KFM09A.*

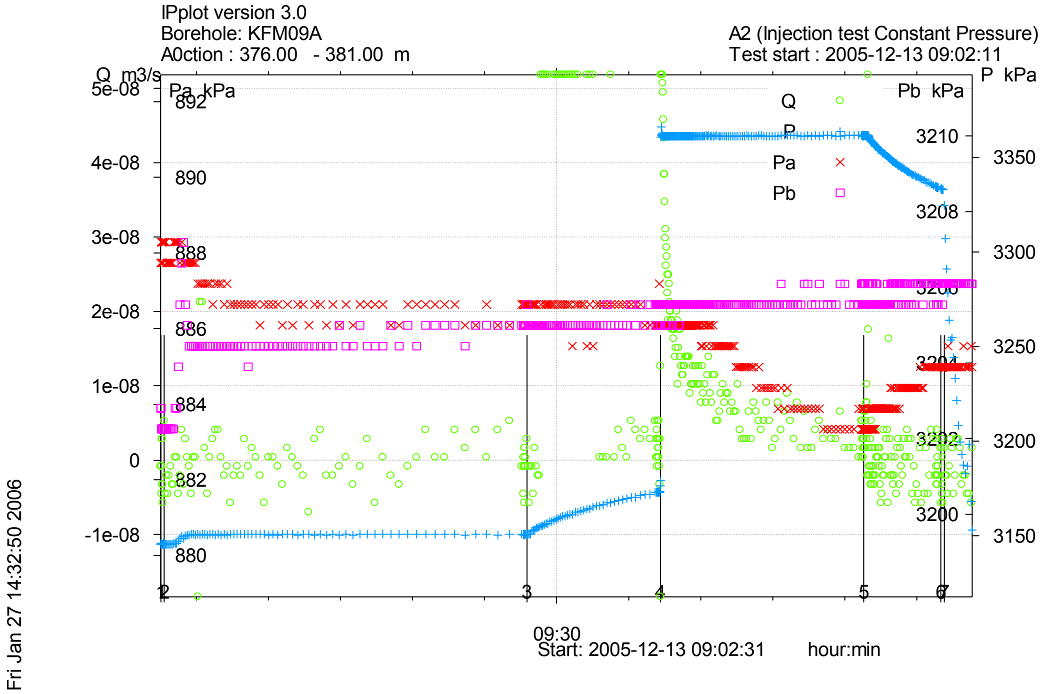


Figure A3-375. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 376.0-381.0 m in borehole KFM09A.*

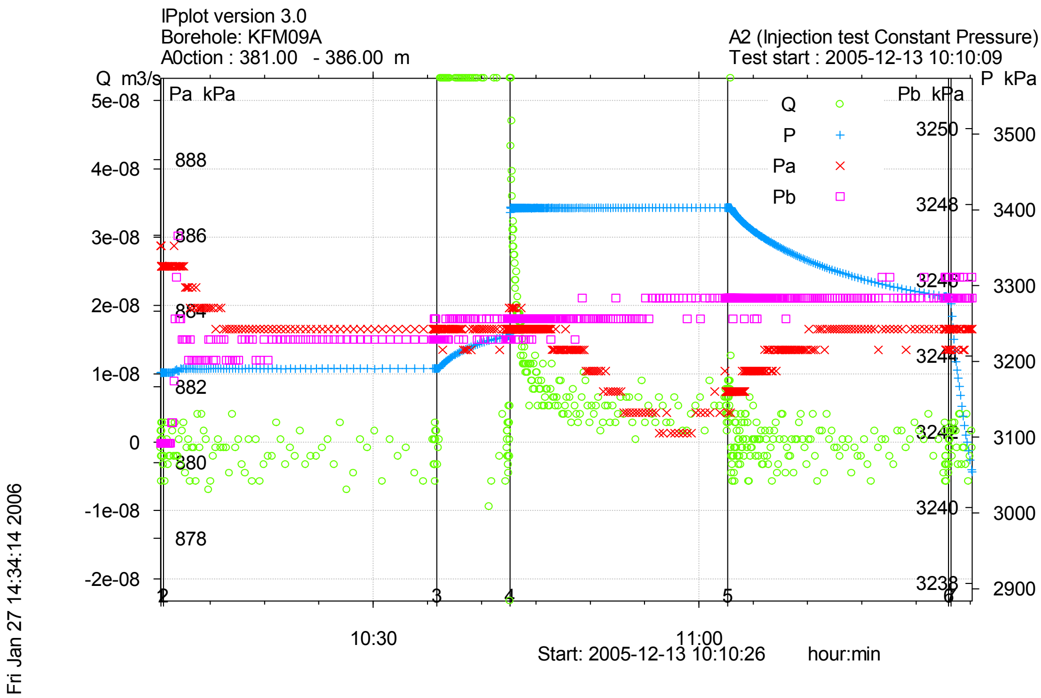


Figure A3-376. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 381.0-386.0 m in borehole KFM09A.*

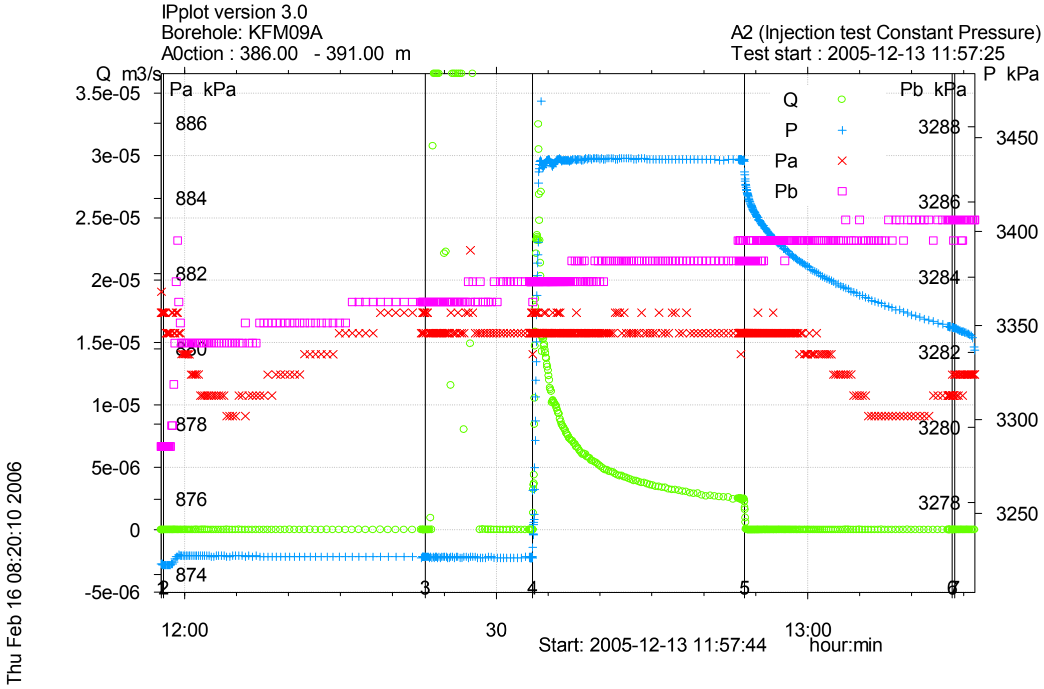


Figure A3-377. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 386.0-391.0 m in borehole KFM09A.*

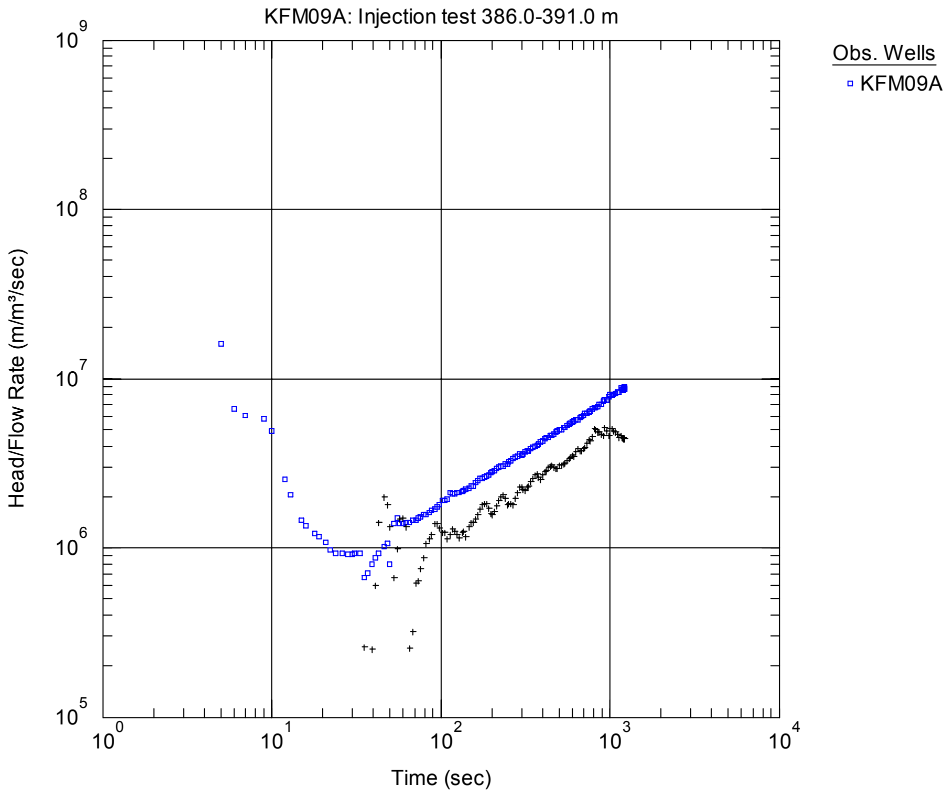


Figure A3-378. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 386.0-391.0 m in KFM09A*

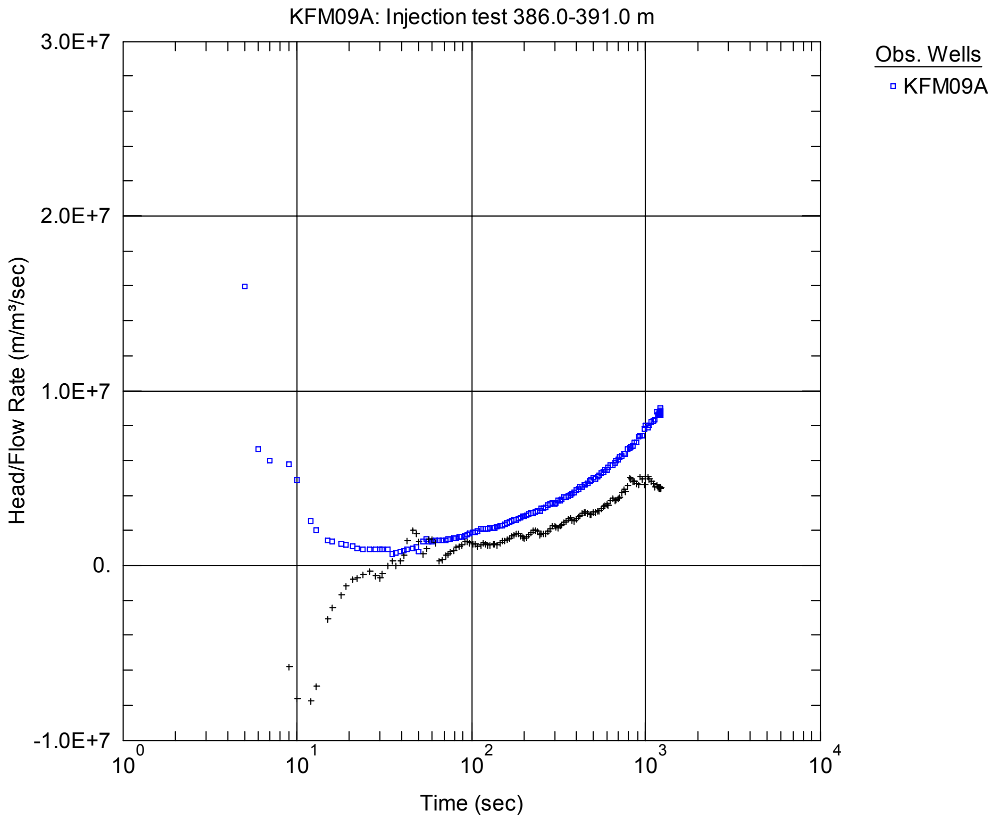


Figure A3-379. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 386.0-391.0 m in KFM09A.*

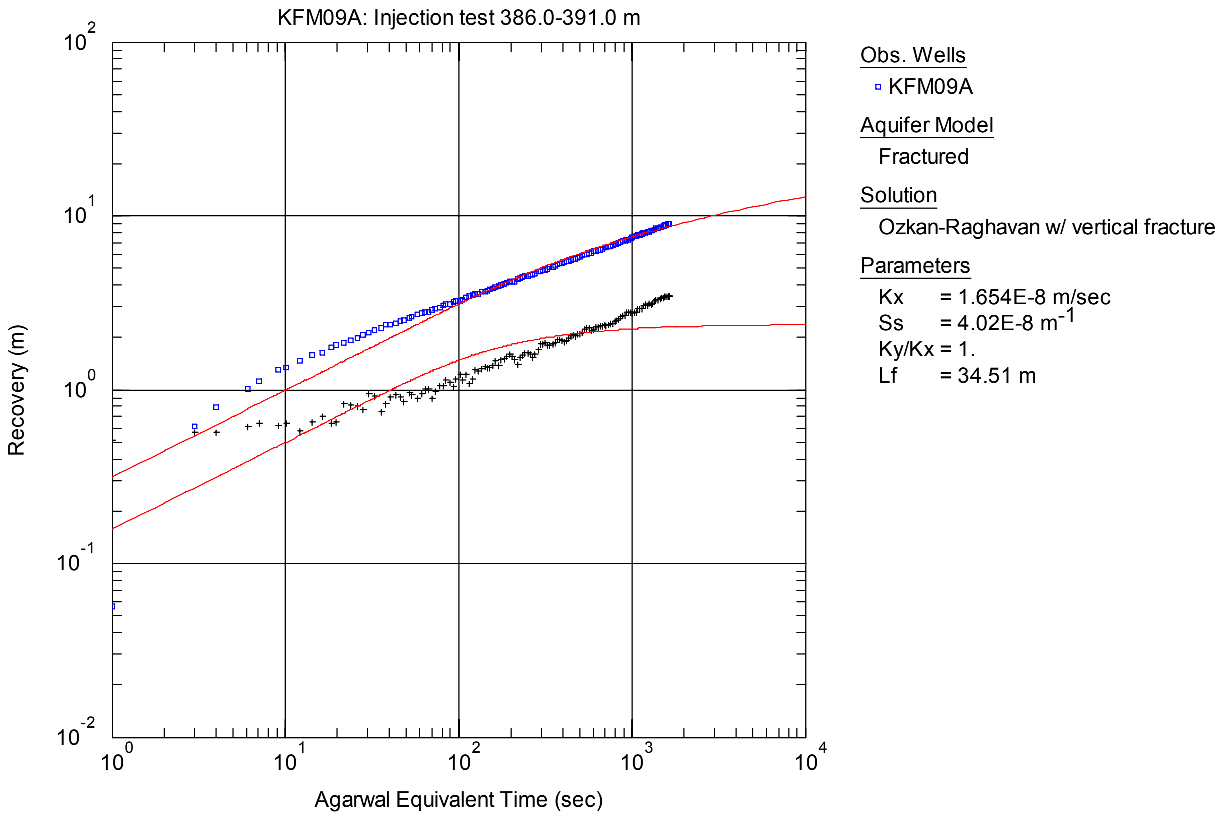


Figure A3-380. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 386.0-391.0 m in KFM09A.*

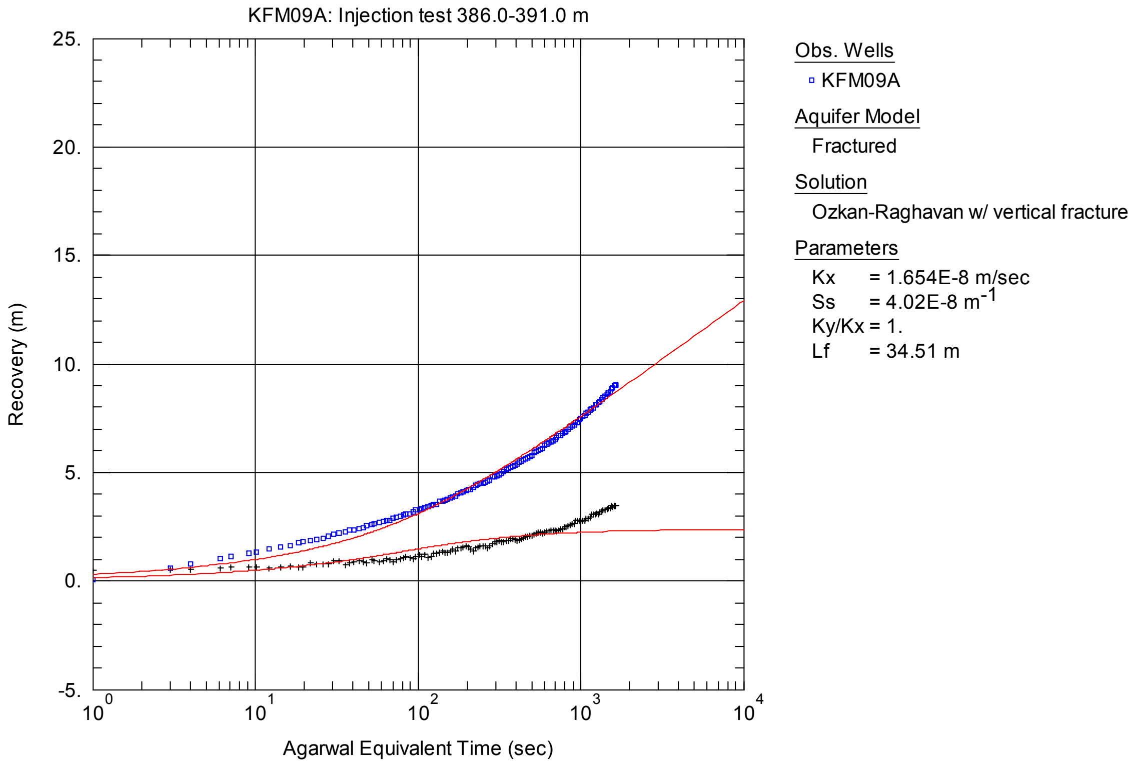


Figure A3-381. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 386.0-391.0 m in KFM09A.*

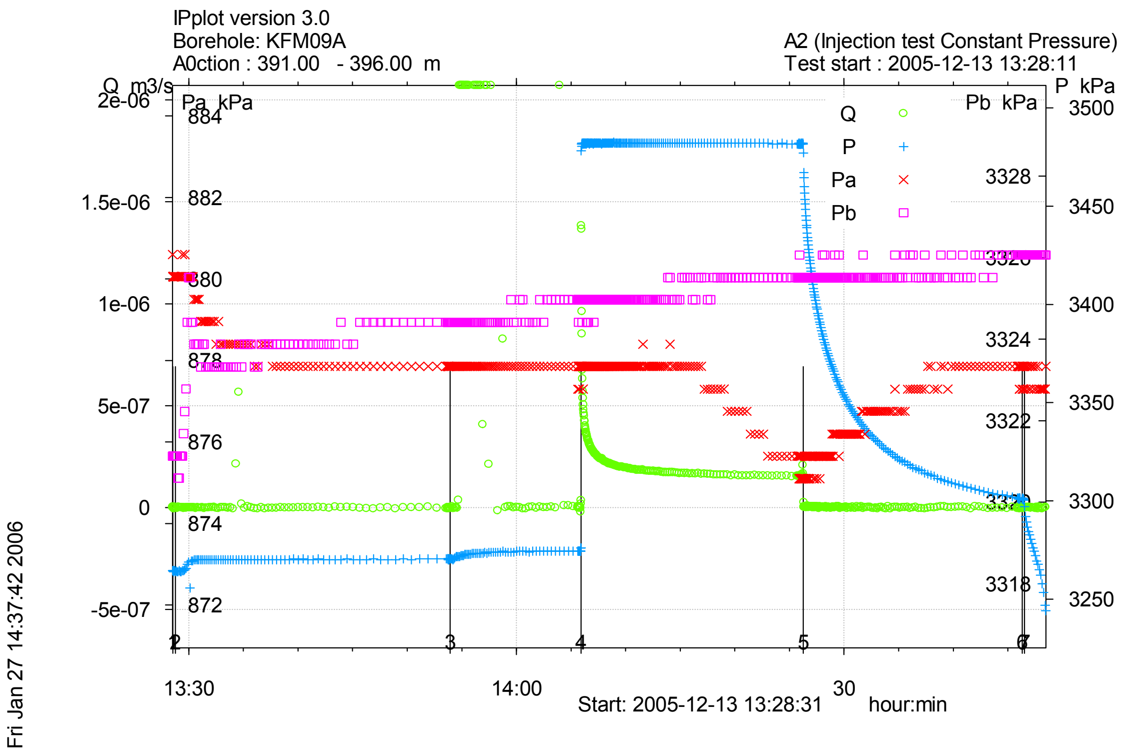


Figure A3-382. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 391.0-396.0 m in borehole KFM09A.*

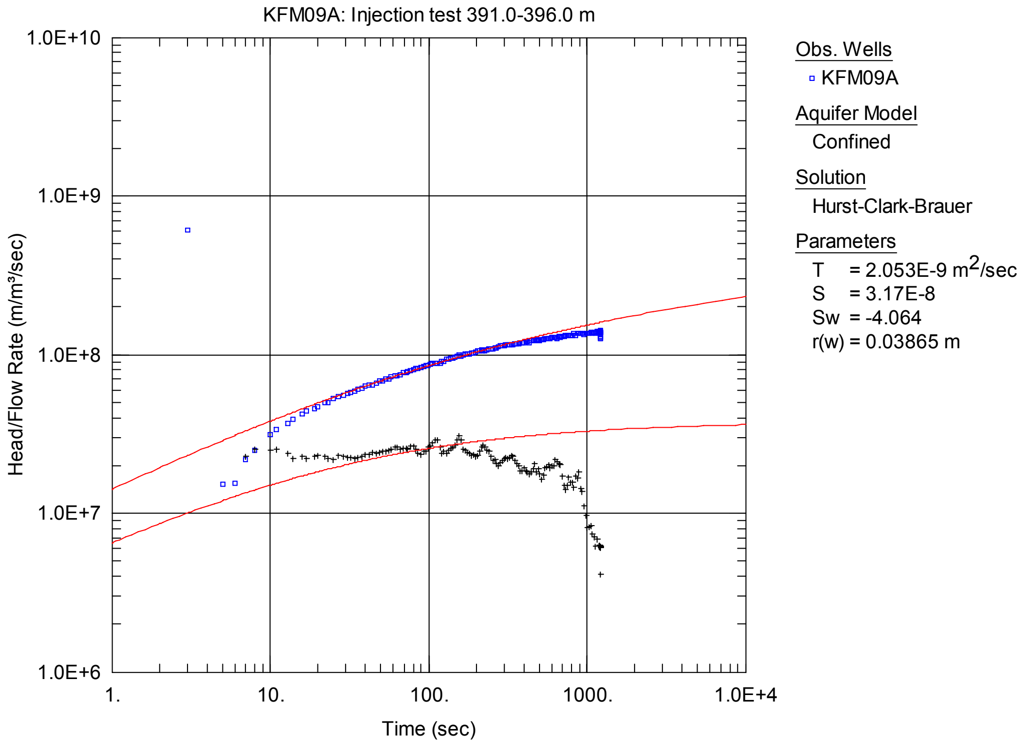


Figure A3-383. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 391.0-396.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for a pseudo-radial response.*

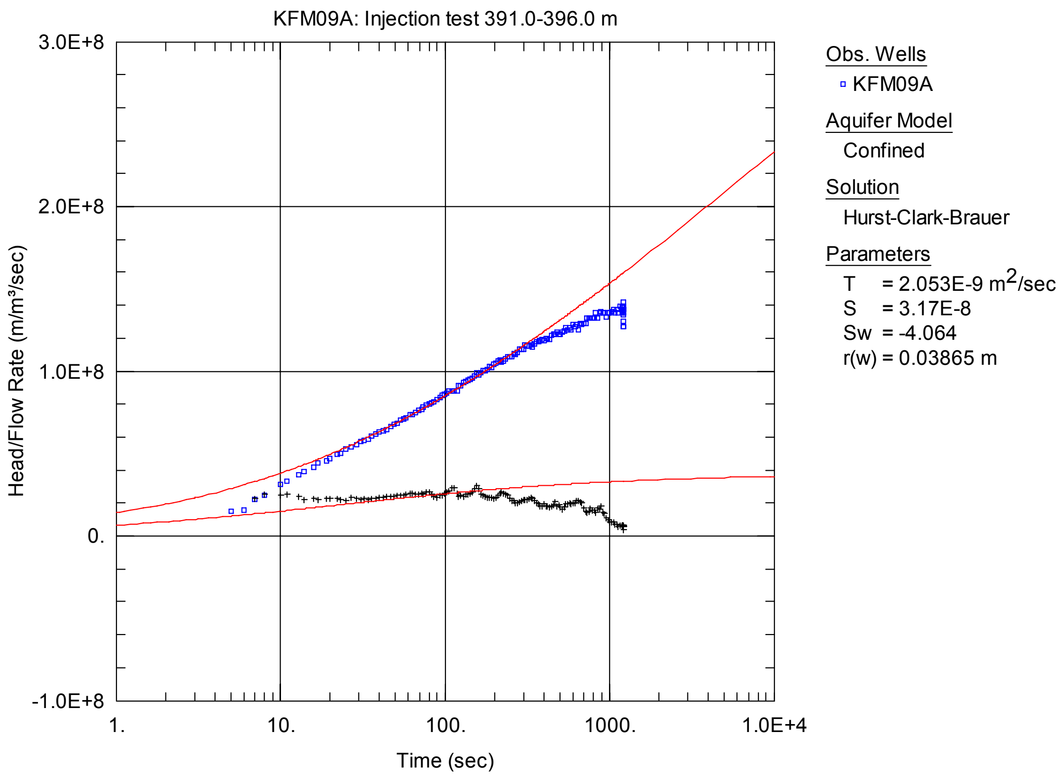


Figure A3-384. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 391.0-396.0 m in KFM09A This evaluation is made with the Hurst-Clark-Brauer model for a pseudo-radial response.*

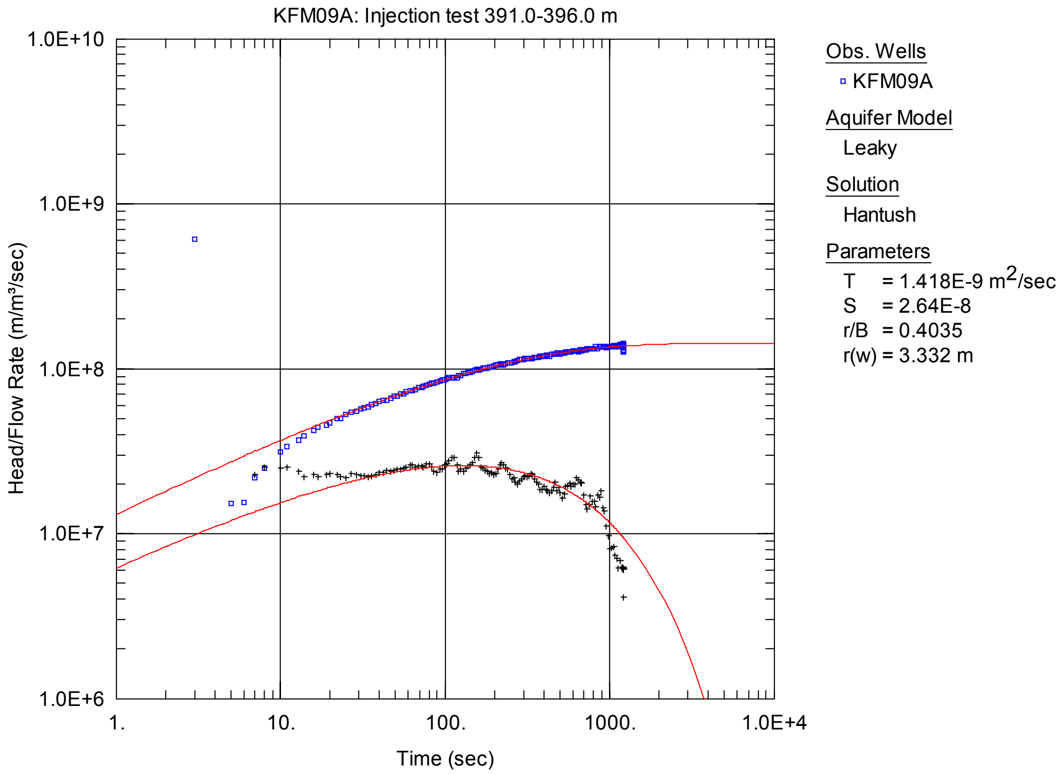


Figure A3-385. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 391.0-396.0 m in KFM09A This evaluation is made with the Hantush model for a pseudo-spherical response.*

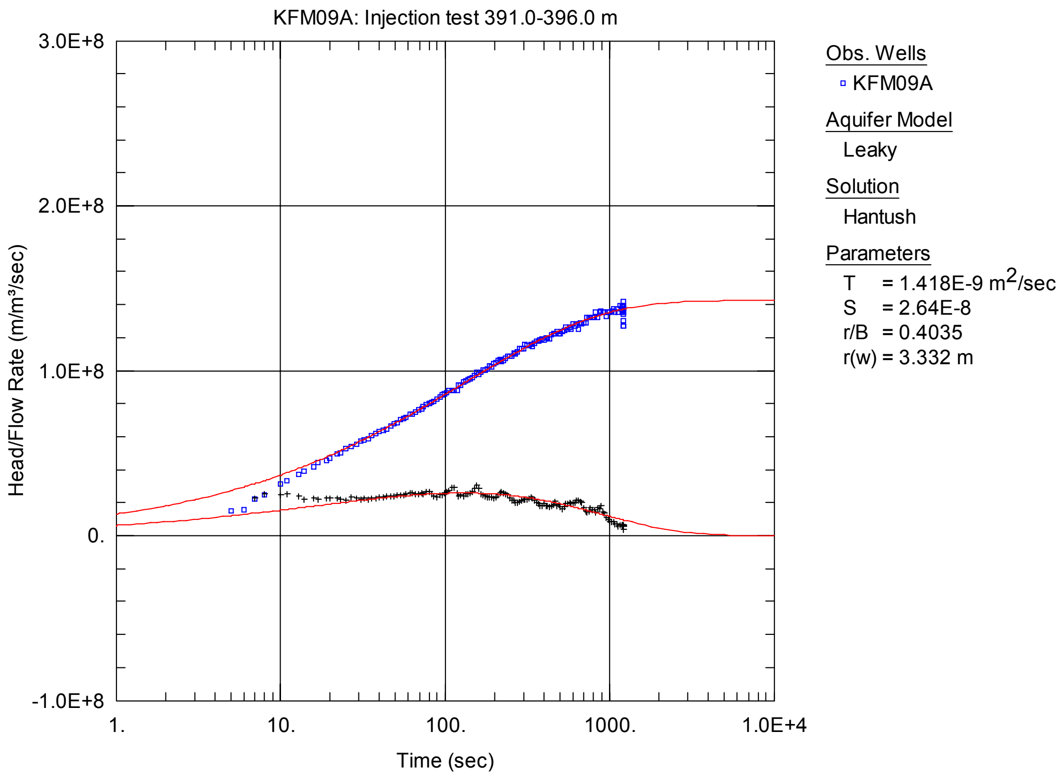


Figure A3-386. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 391.0-396.0 m in KFM09A This evaluation is made with the Hantush model for a pseudo-spherical response.*

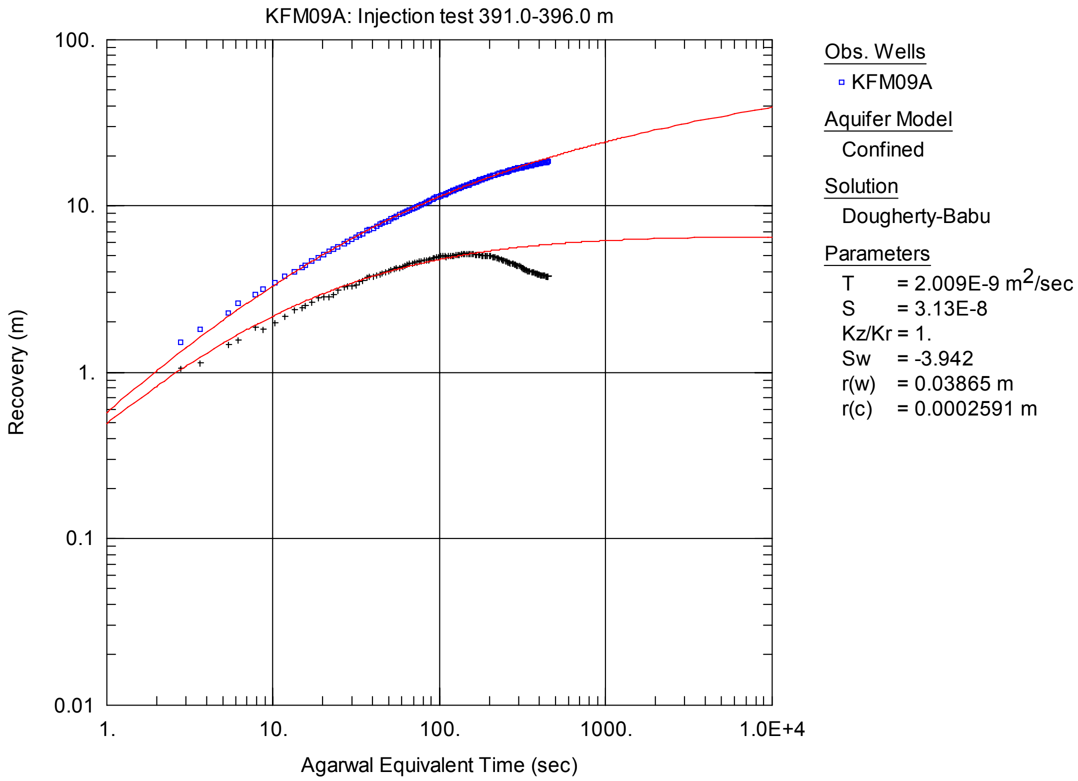


Figure A3-387. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 391.0-396.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

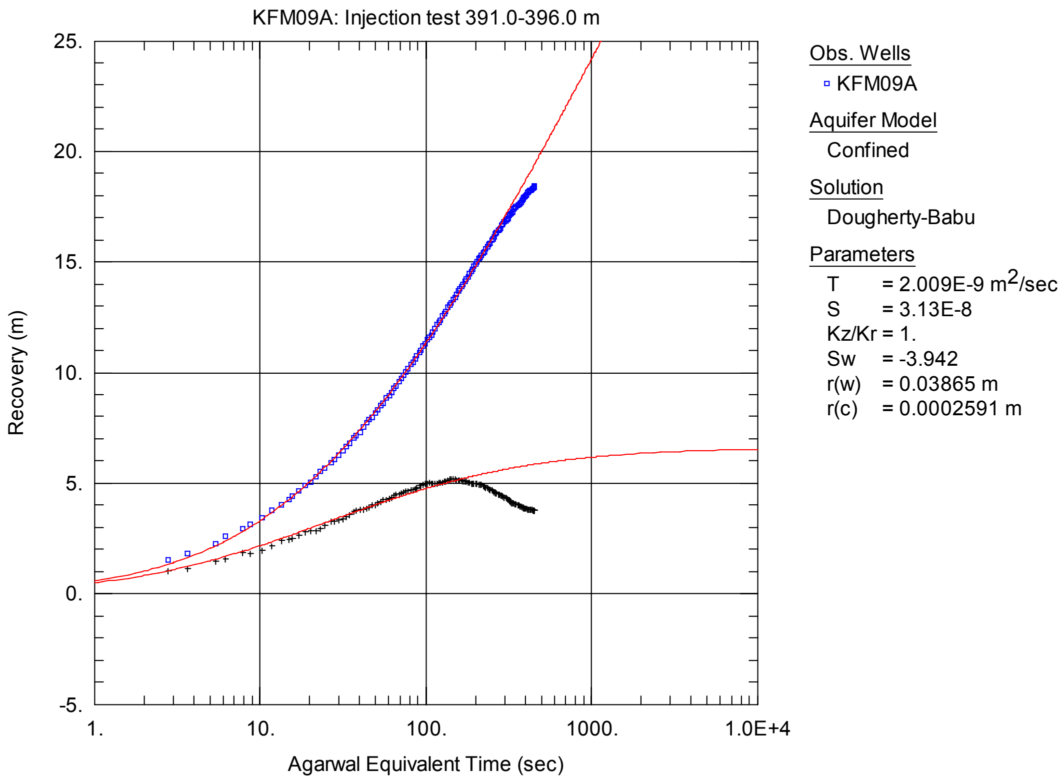


Figure A3-388. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 391.0-396.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

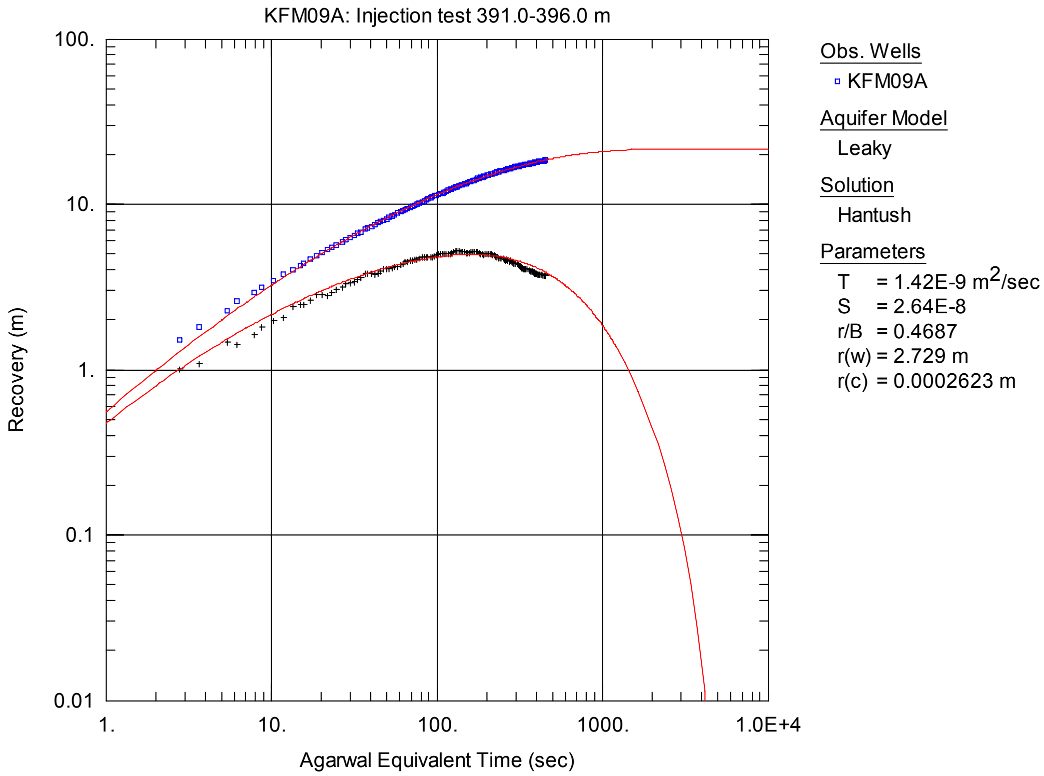


Figure A3-389. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 391.0-396.0 m in KFM09A. This evaluation is made with the Hantush model for a pseudo-spherical response.*

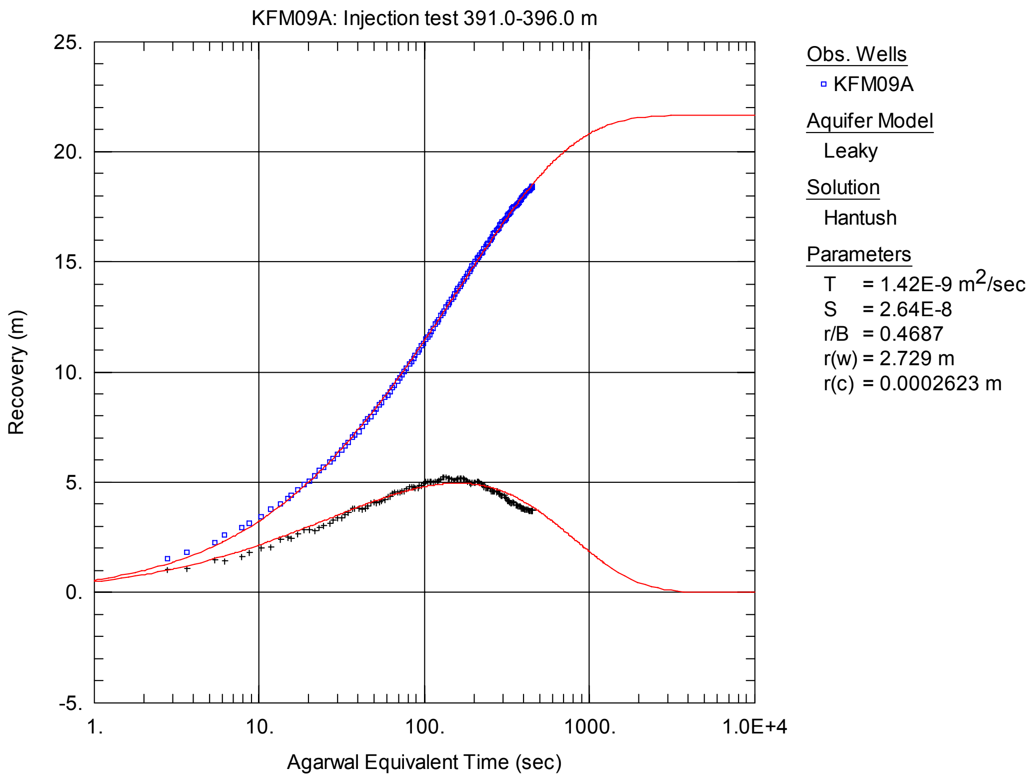


Figure A3-390. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 391.0-396.0 m in KFM09A. This evaluation is made with the Hantush model for a pseudo-spherical response.*

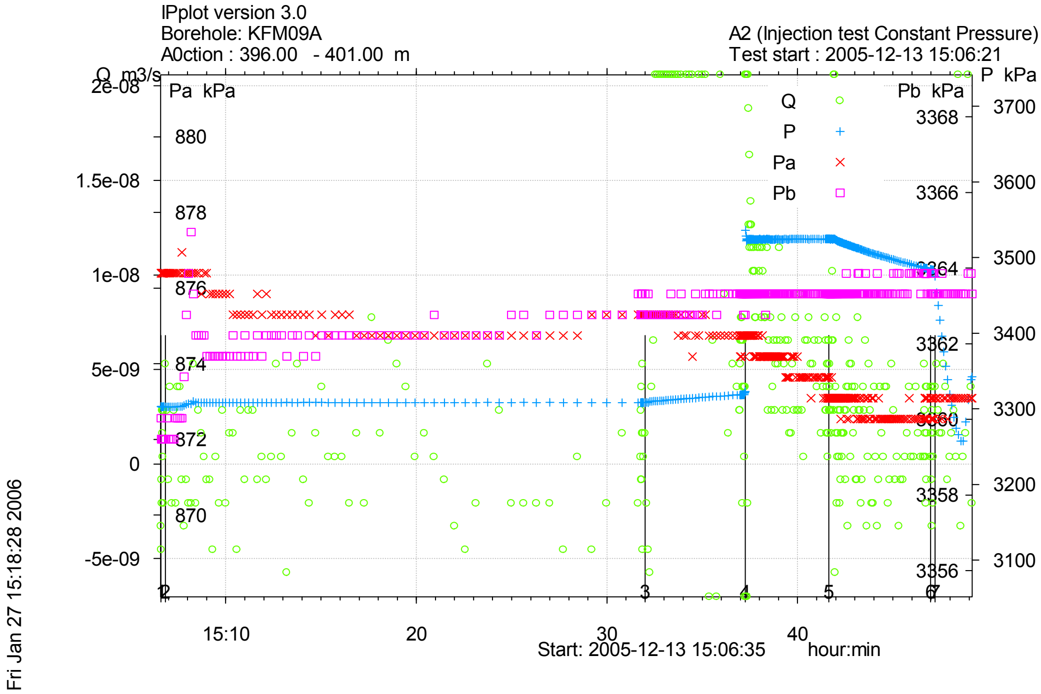


Figure A3-391. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 396.0-401.0 m in borehole KFM09A.*

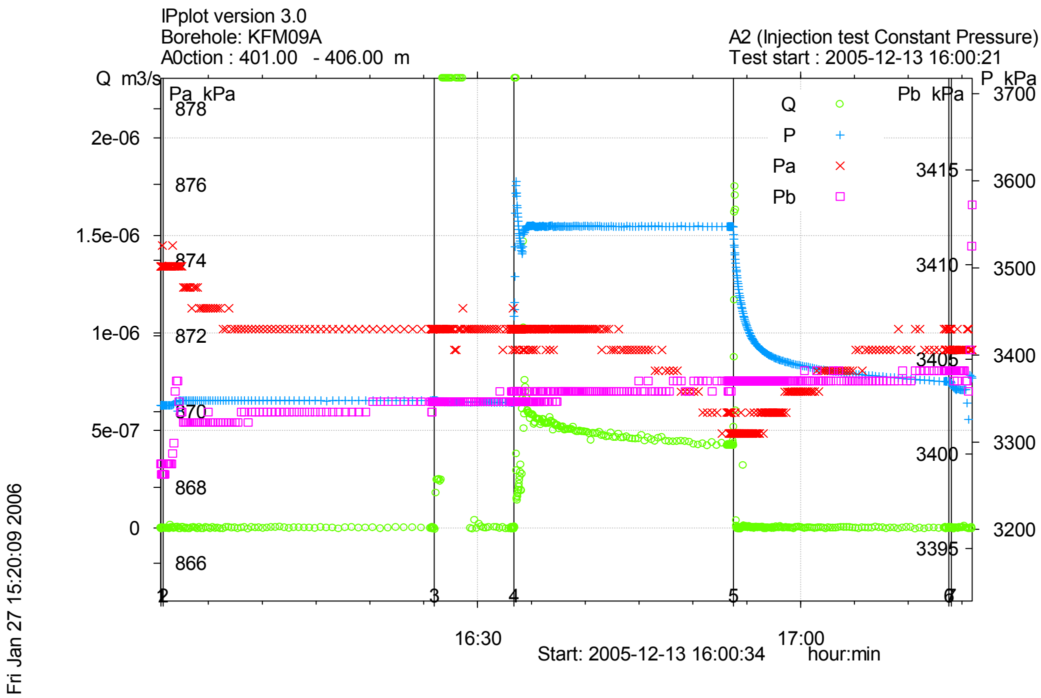


Figure A3-392. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 401.0-406.0 m in borehole KFM09A.*

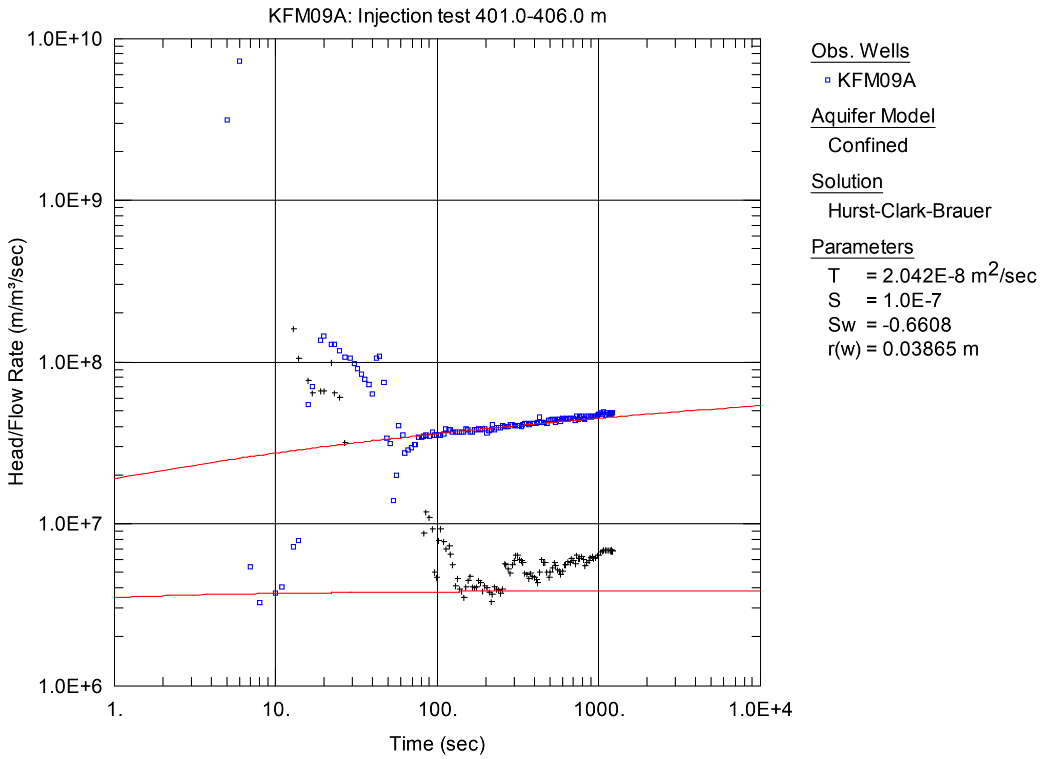


Figure A3-393. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 401.0-406.0 m in KFM09A.*

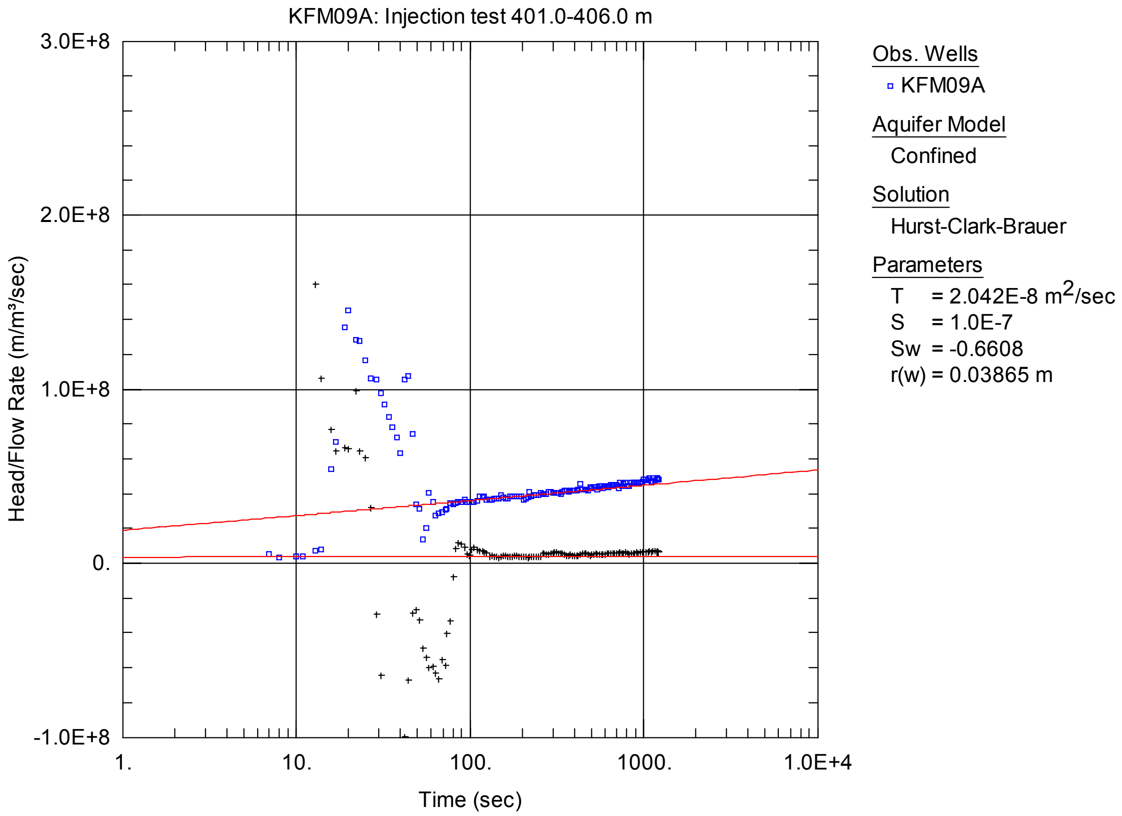


Figure A3-394. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 401.0-406.0 m in KFM09A.*

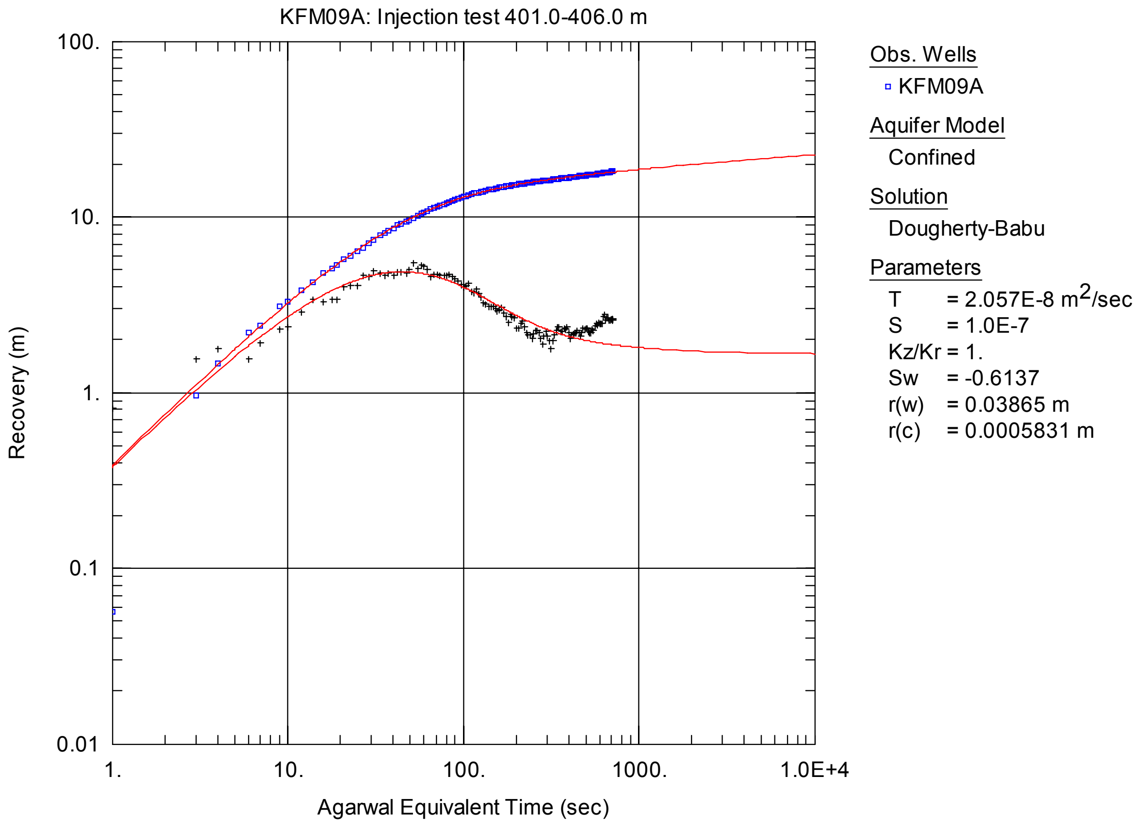


Figure A3-395. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 401.0-406.0 m in KFM09A.*

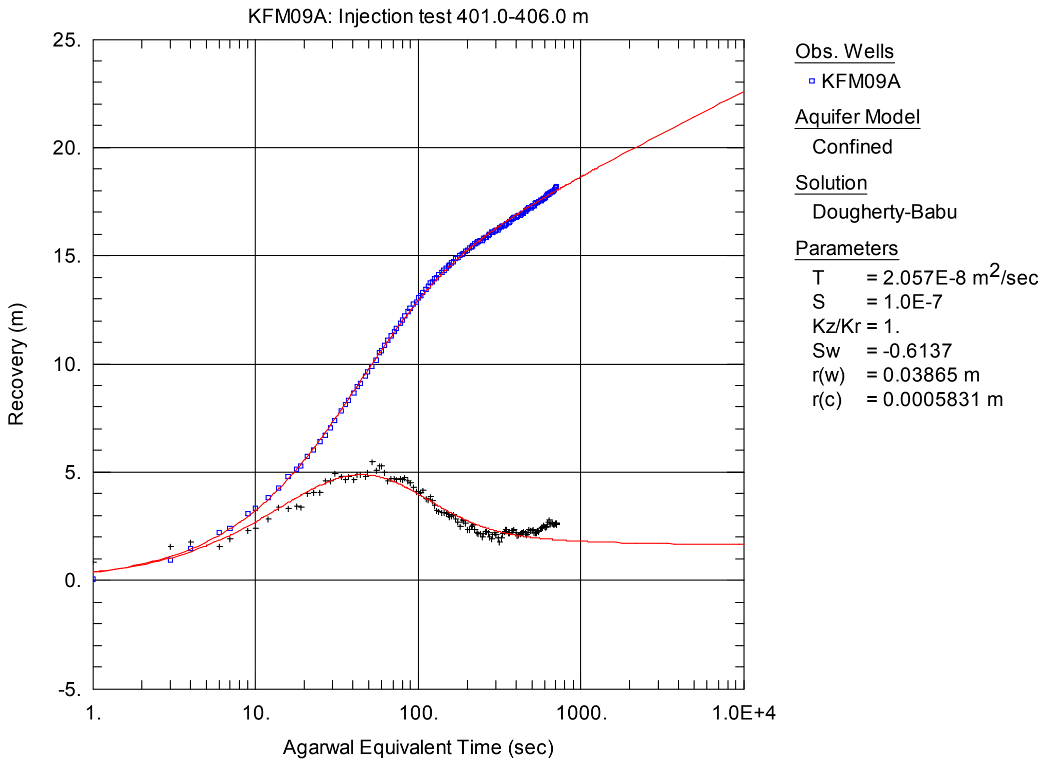


Figure A3-396. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 401.0-406.0 m in KFM09A.*

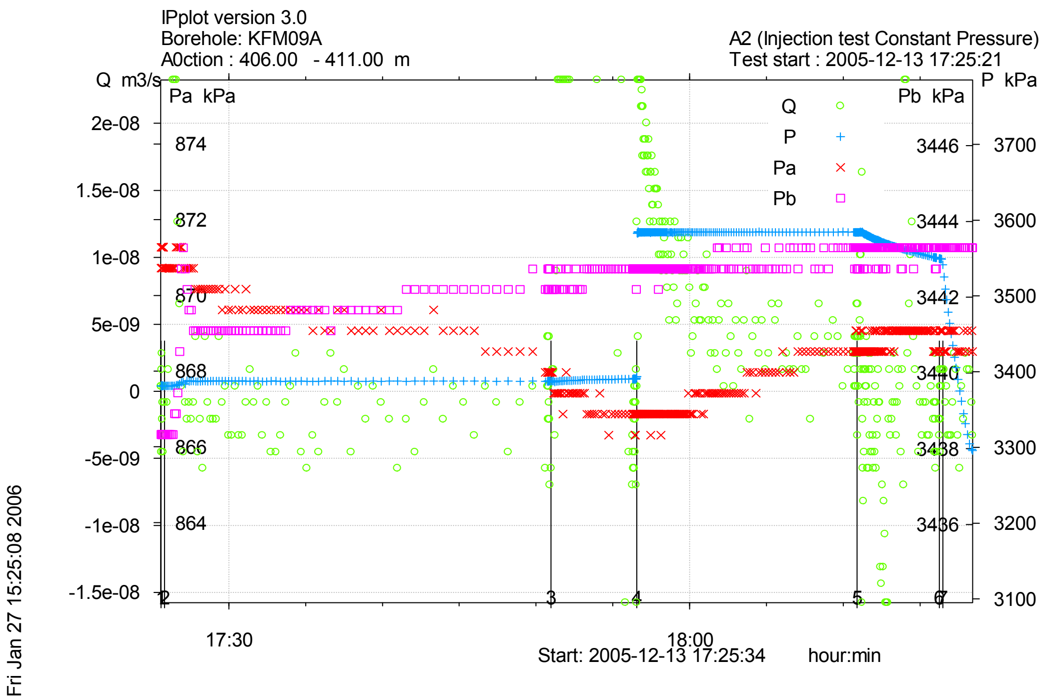


Figure A3-397. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 406.0-411.0 m in borehole KFM09A.*

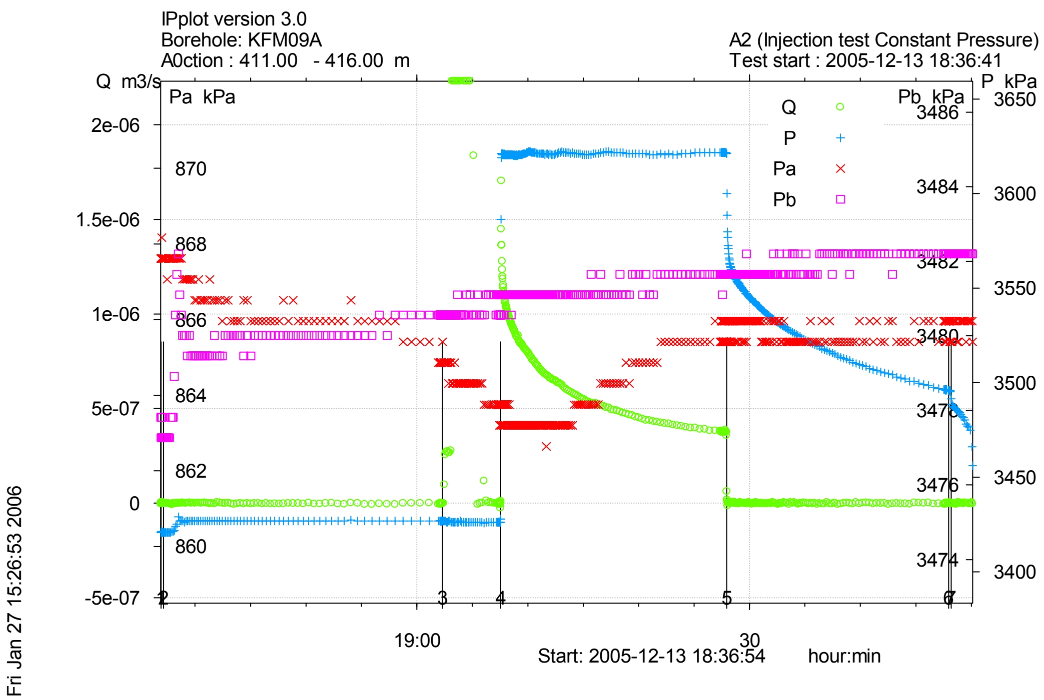


Figure A3-398. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 411.0-416.0 m in borehole KFM09A.*

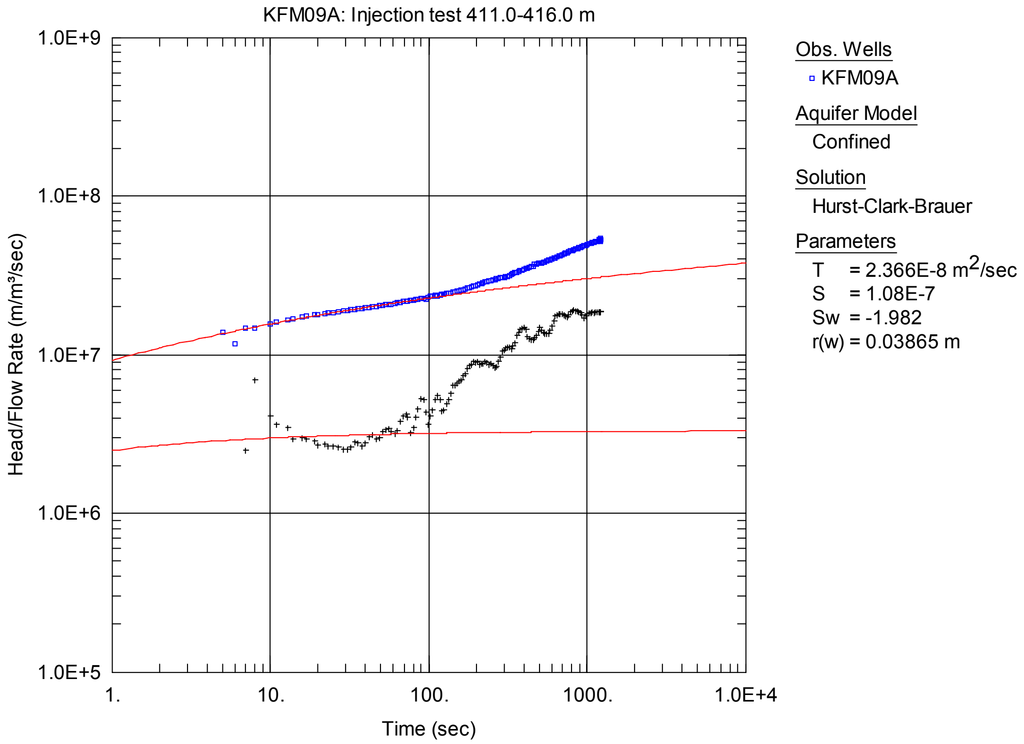


Figure A3-399. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 411.0-416.0 m in KFM09A. This plot shows a fit to the first of two different PRF:s during the injection period in this section.*

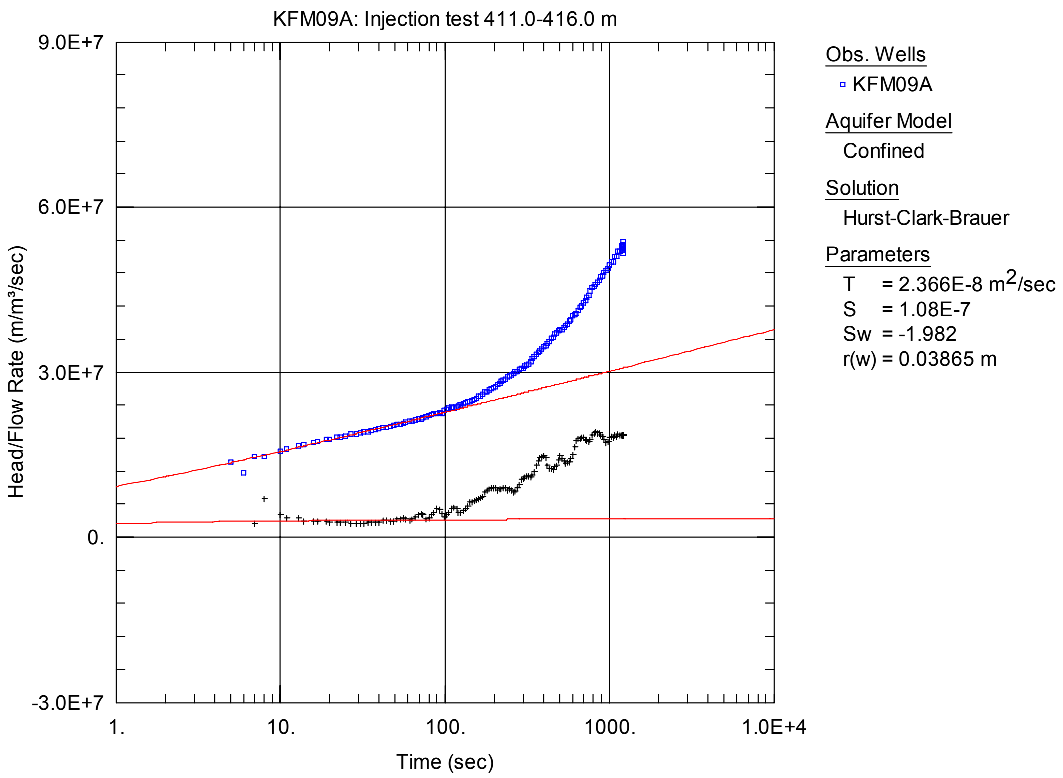


Figure A3-400. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 411.0-416.0 m in KFM09A. This plot shows a fit to the first of two different PRF:s during the injection period in this section.*

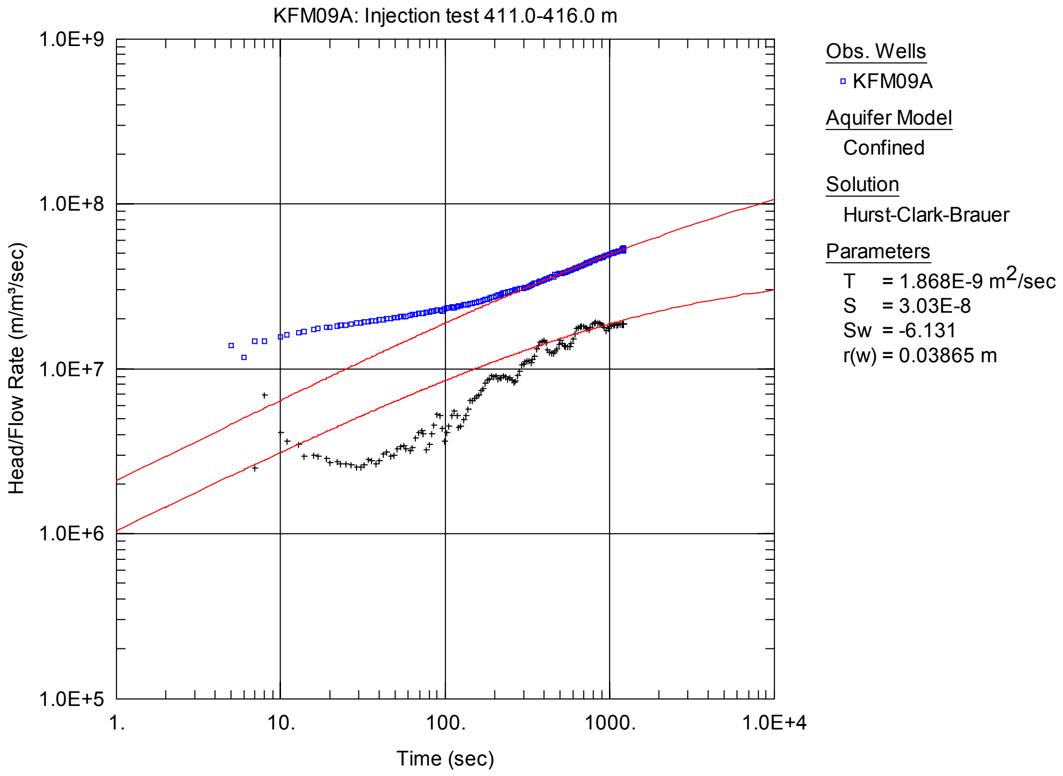


Figure A3-401. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 411.0-416.0 m in KFM09A. This plot shows a fit to the second of two different PRF:s during the injection period in this section.*

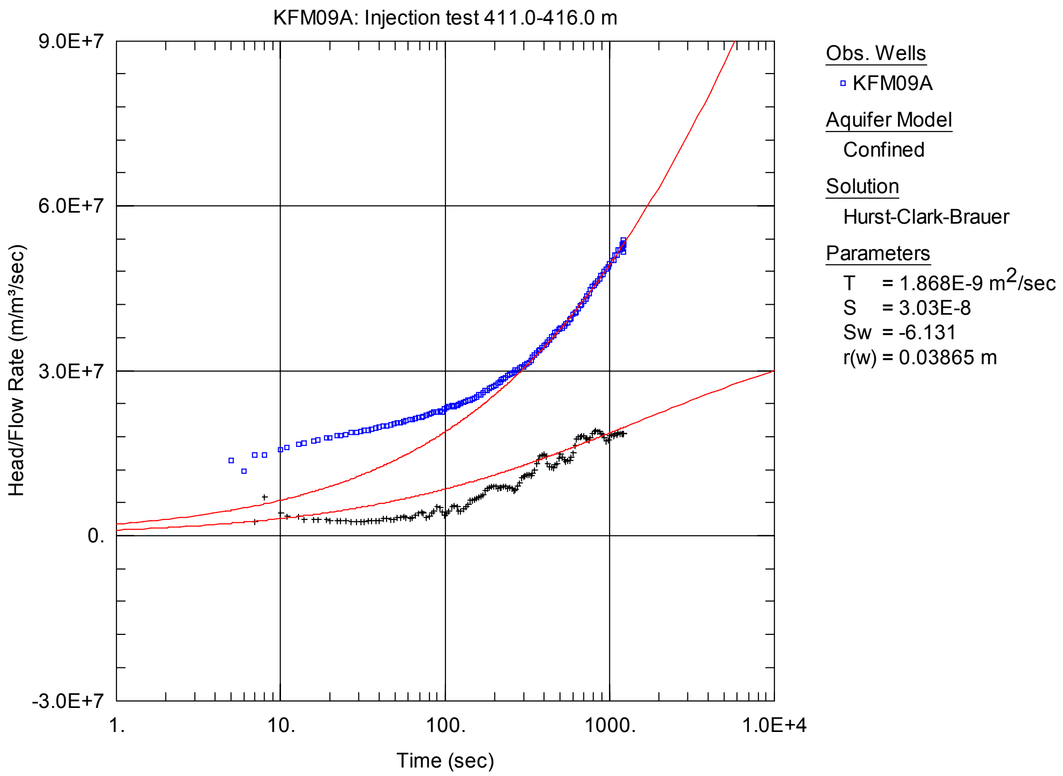


Figure A3-402. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 411.0-416.0 m in KFM09A. This plot shows a fit to the second of two different PRF:s during the injection period in this section.*

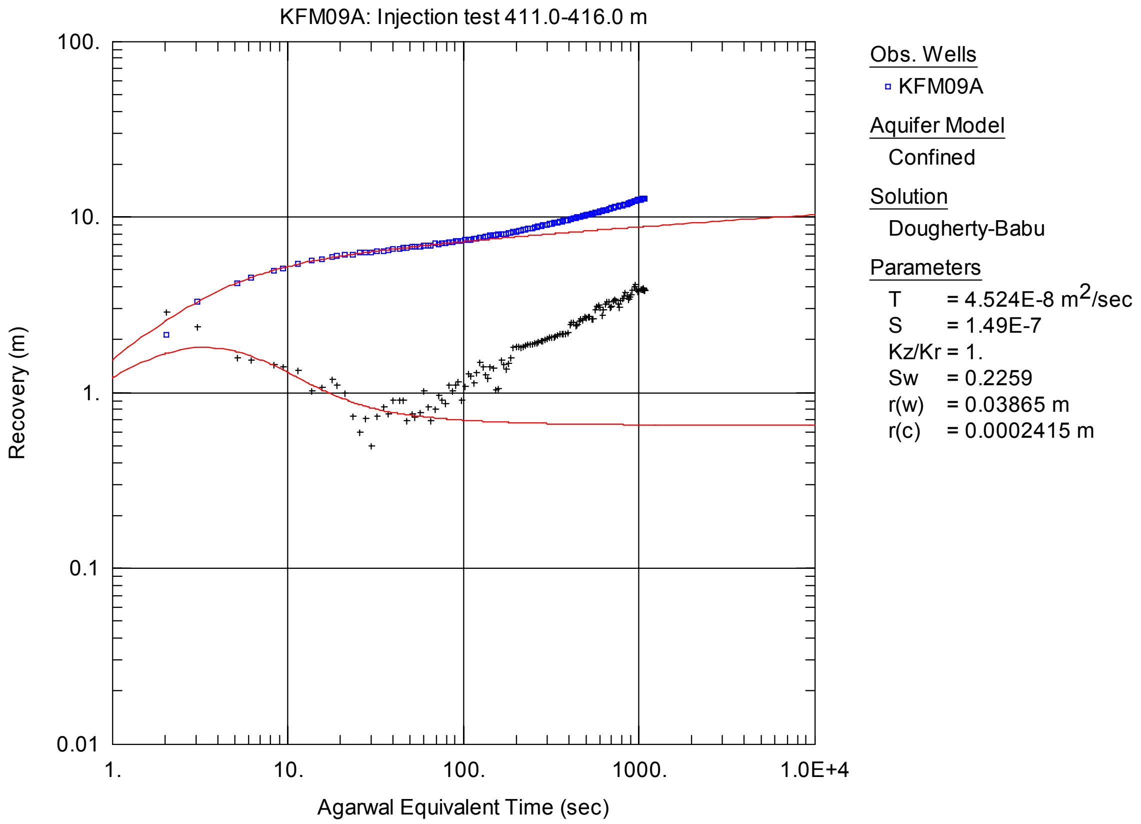


Figure A3-403. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 411.0-416.0 x m in KFM09A.*

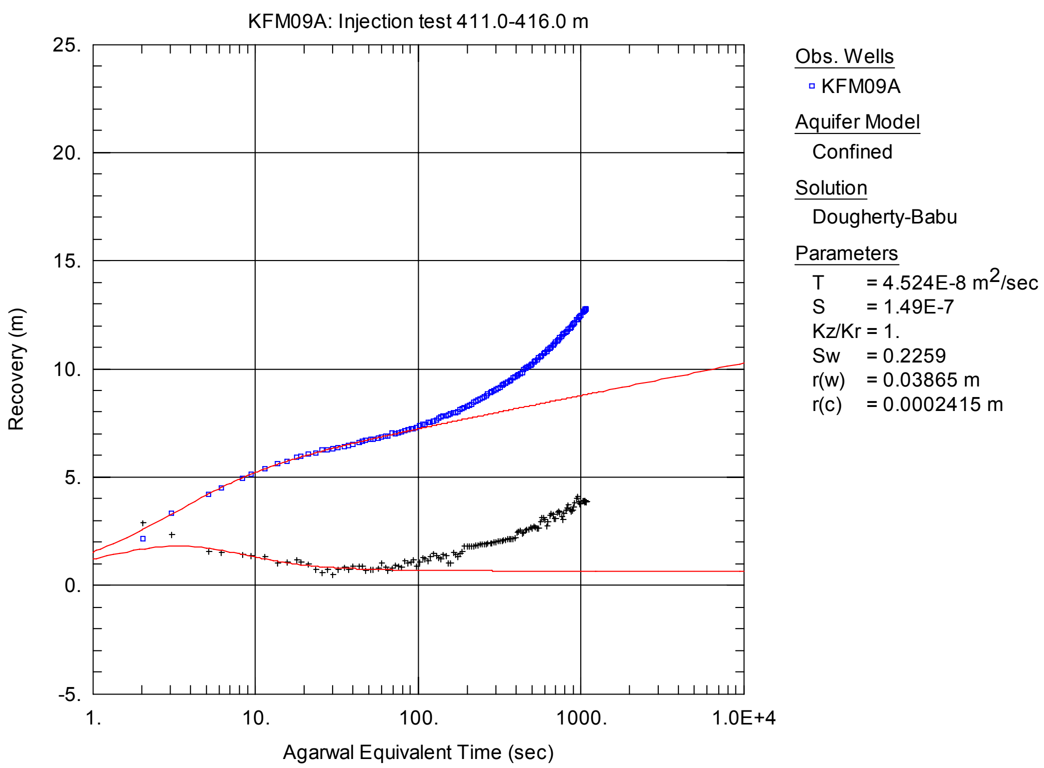


Figure A3-404. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 411.0-416.0 m in KFM09A.*

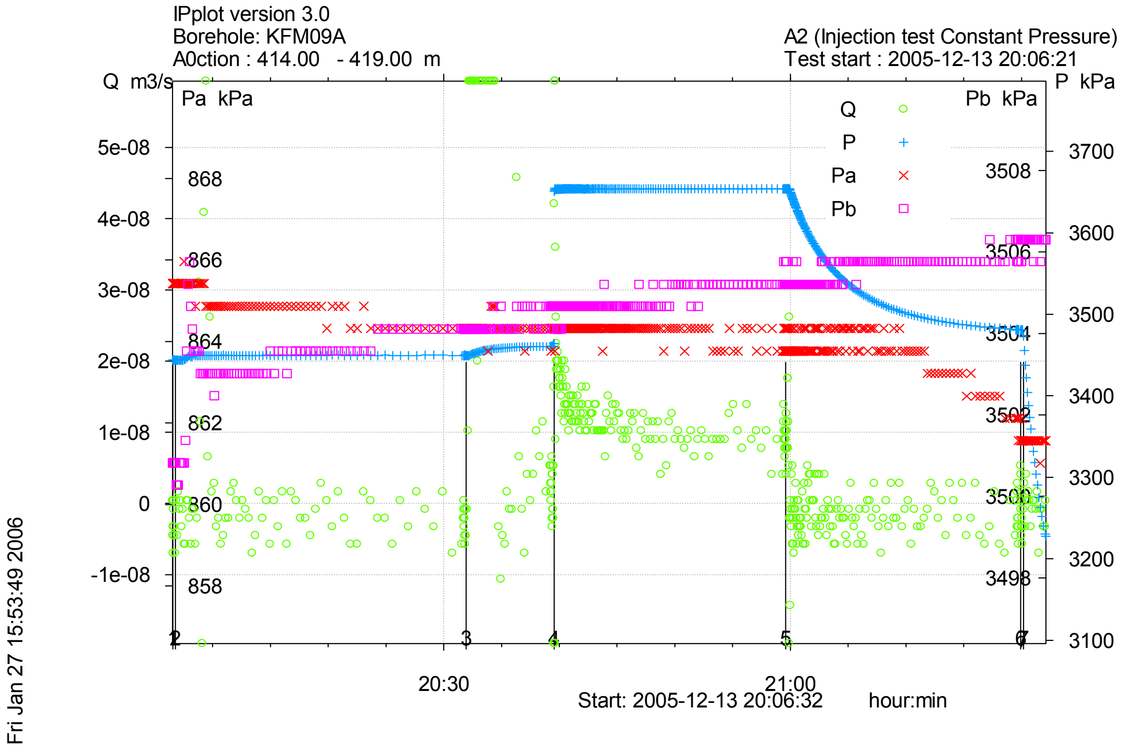


Figure A3-405. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 414.0-419.0 m in borehole KFM09A.

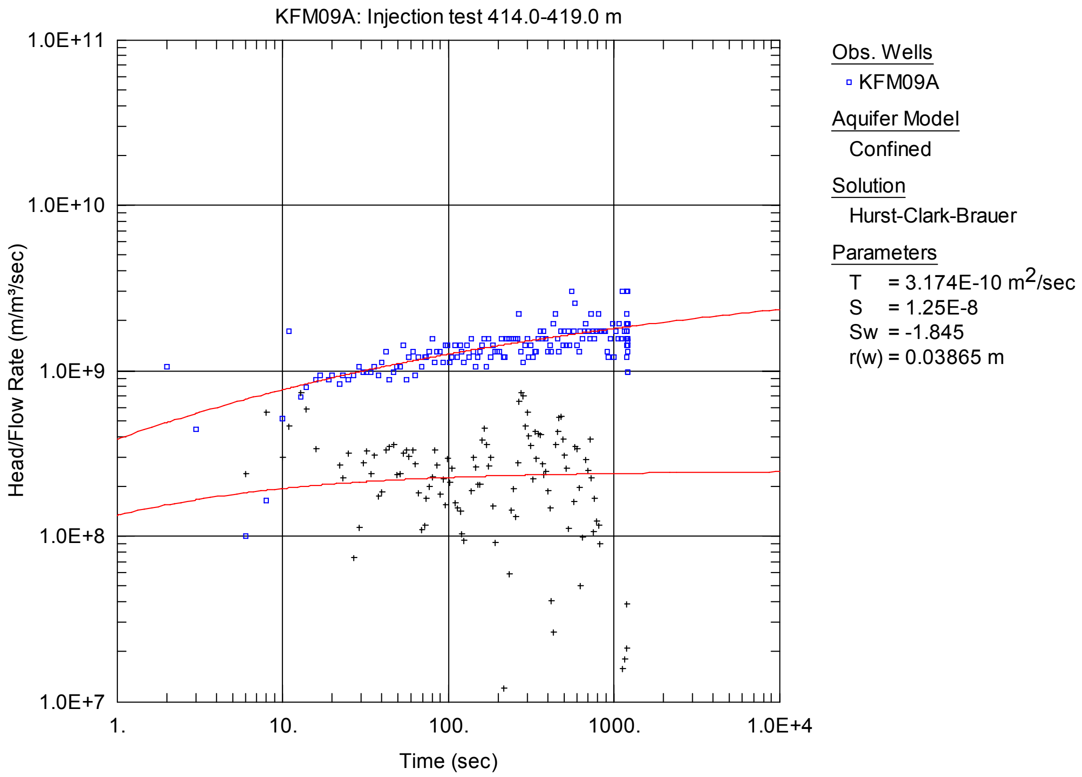


Figure A3-406. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 414.0-419.0 m in KFM09A.

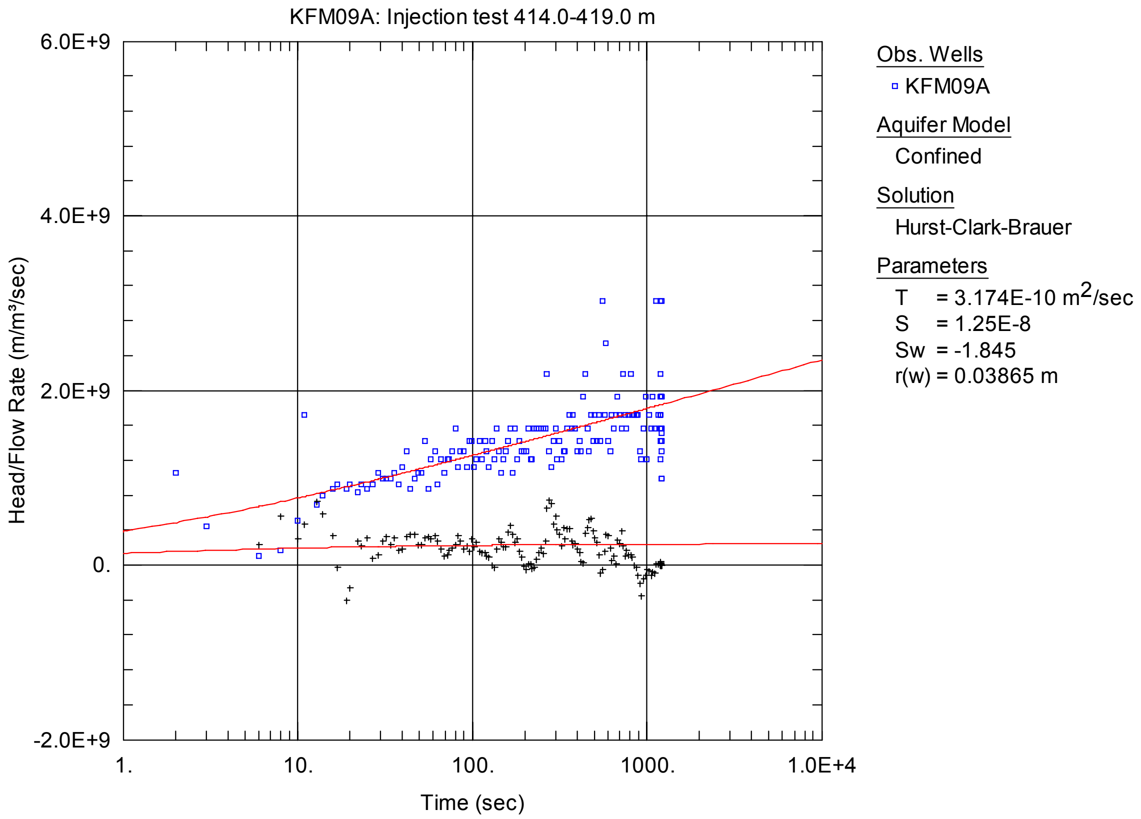


__Figure A3-407.__ Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 414.0-419.0 m in KFM09A.

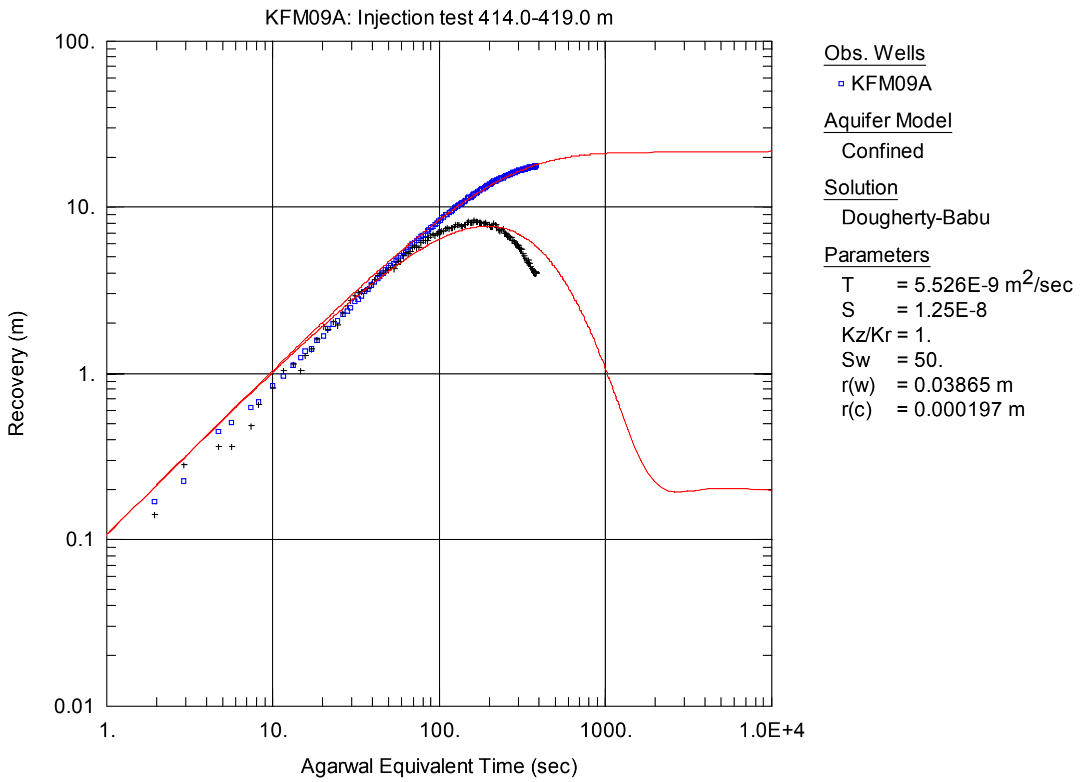


__Figure A3-408.__ Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 414.0-419.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.

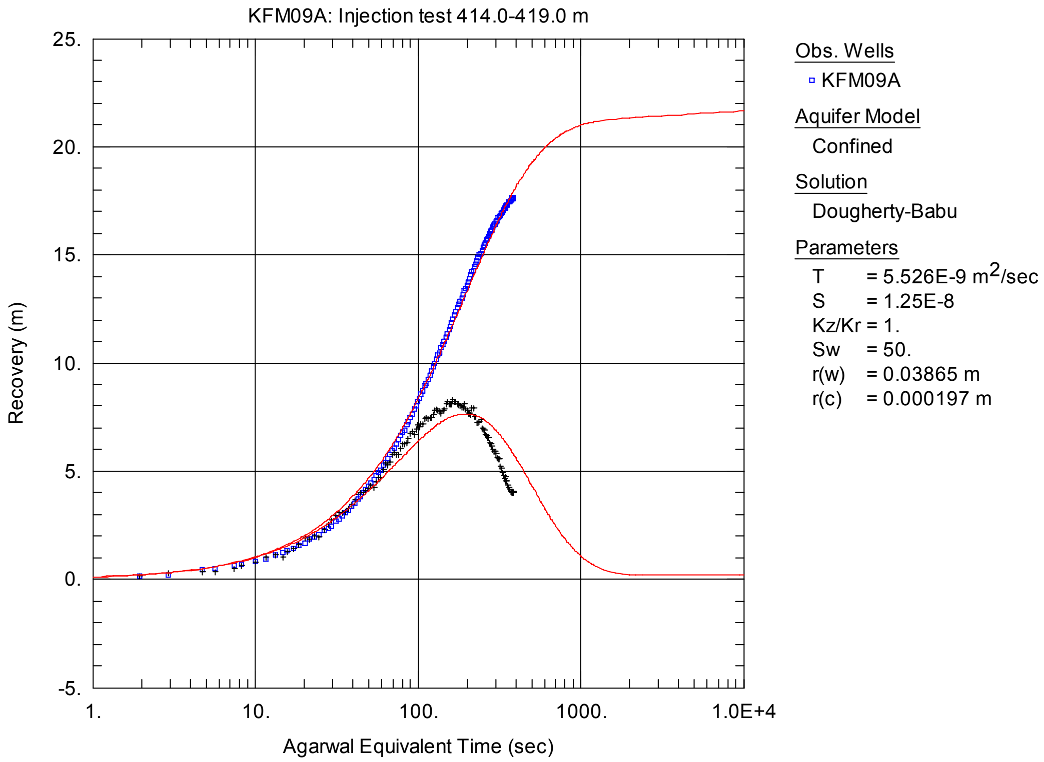


Figure A3-409. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 414.0-419.0 m in KFM09A. No unambiguous transient evaluation is possible on the recovery period.*

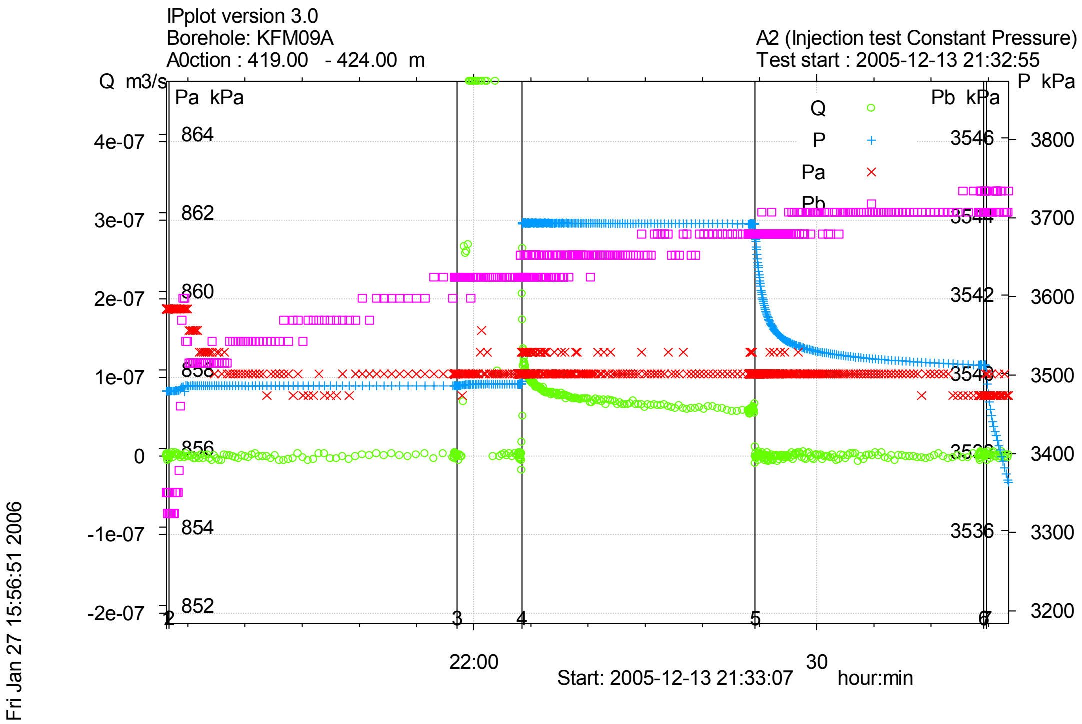


Figure A3-410. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 419.0-424.0 m in borehole KFM09A.*

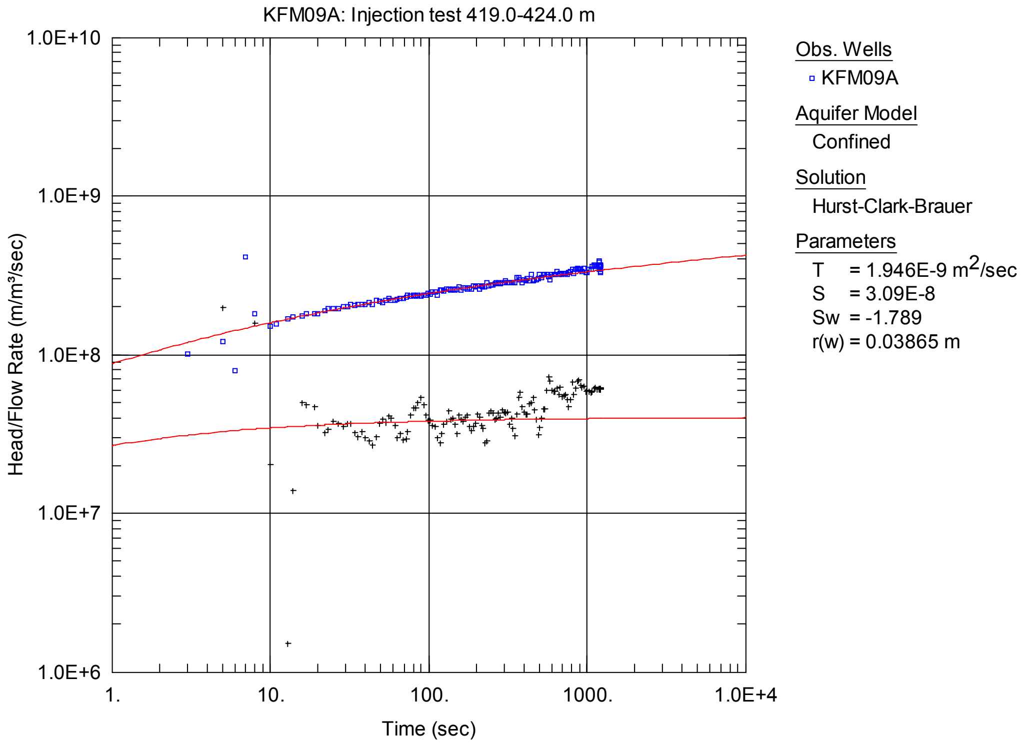


Figure A3-411. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 419.0-424.0 m in KFM09A. This plot shows a fit to the first of two different PRF:s during the injection period in this section.*

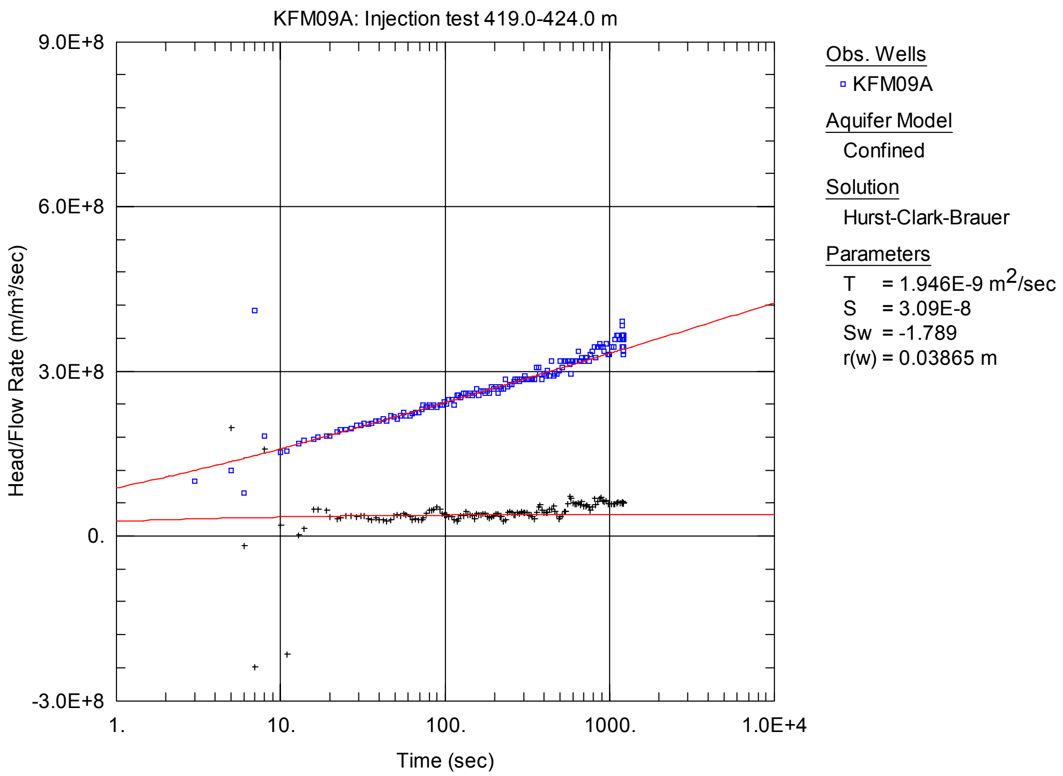


Figure A3-412. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 419.0-424.0 m in KFM09A. This plot shows a fit to the first of two different PRF:s during the injection period in this section.*

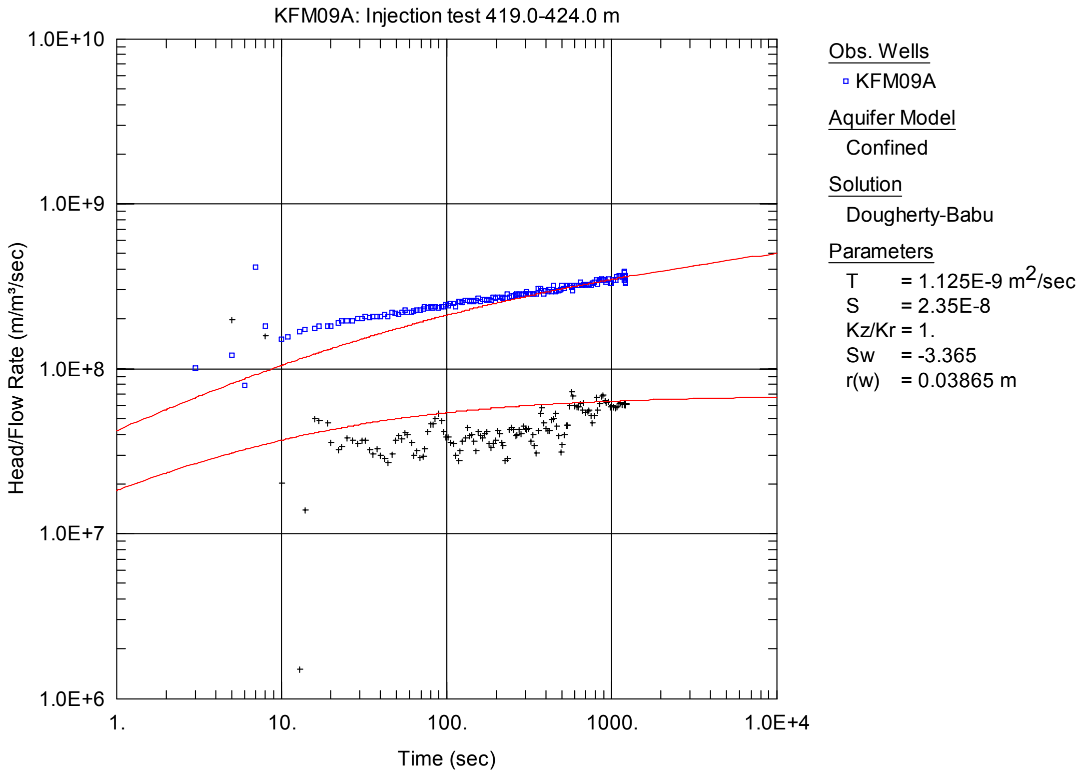


Figure A3-413. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 419.0-424.0 m in KFM09A. This plot shows a fit to the second of two different PRF:s during the injection period in this section.*

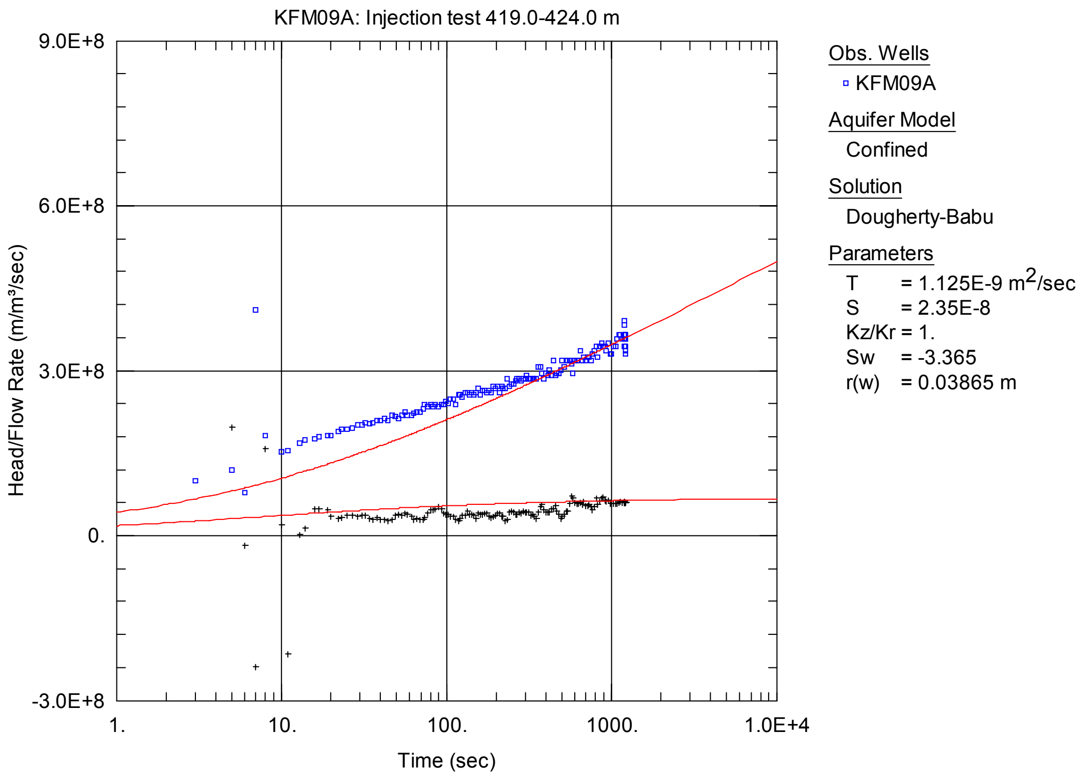


Figure A3-414. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 419.0-424.0 m in KFM09A. This plot shows a fit to the second of two different PRF:s during the injection period in this section.*

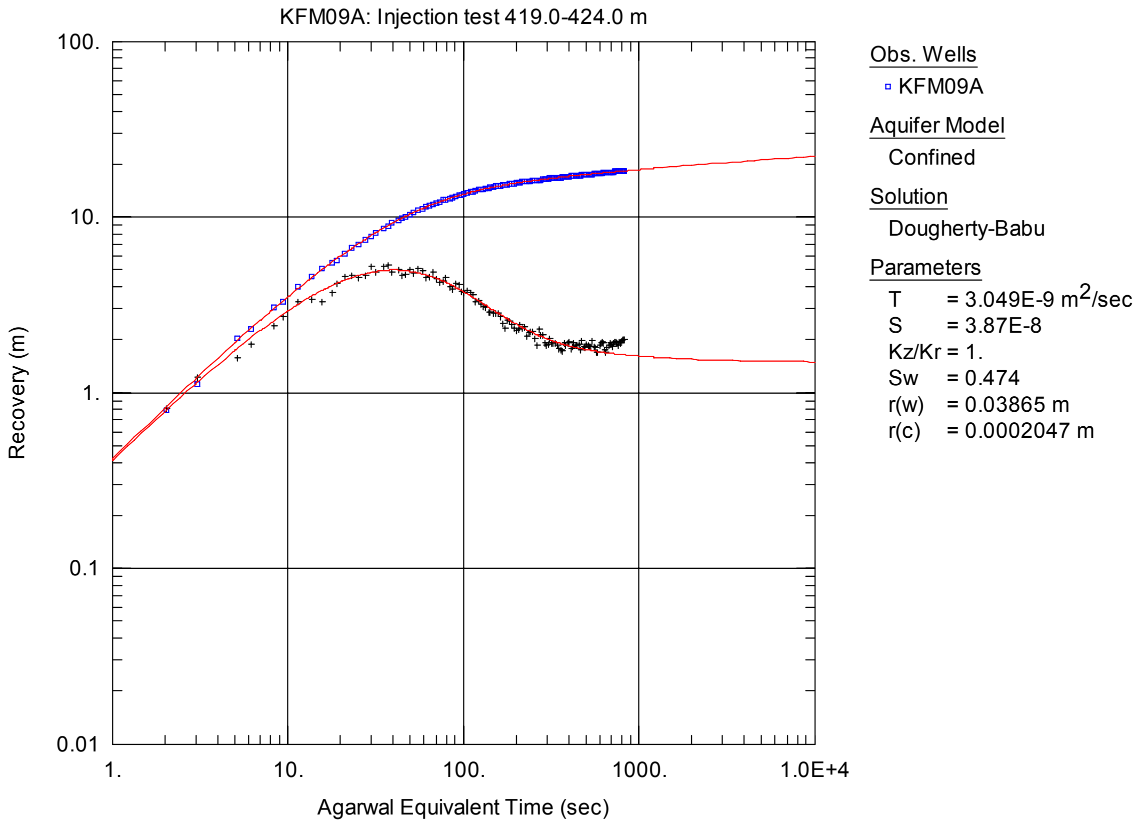


Figure A3-415. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 419.0-424.0 m in KFM09A.*

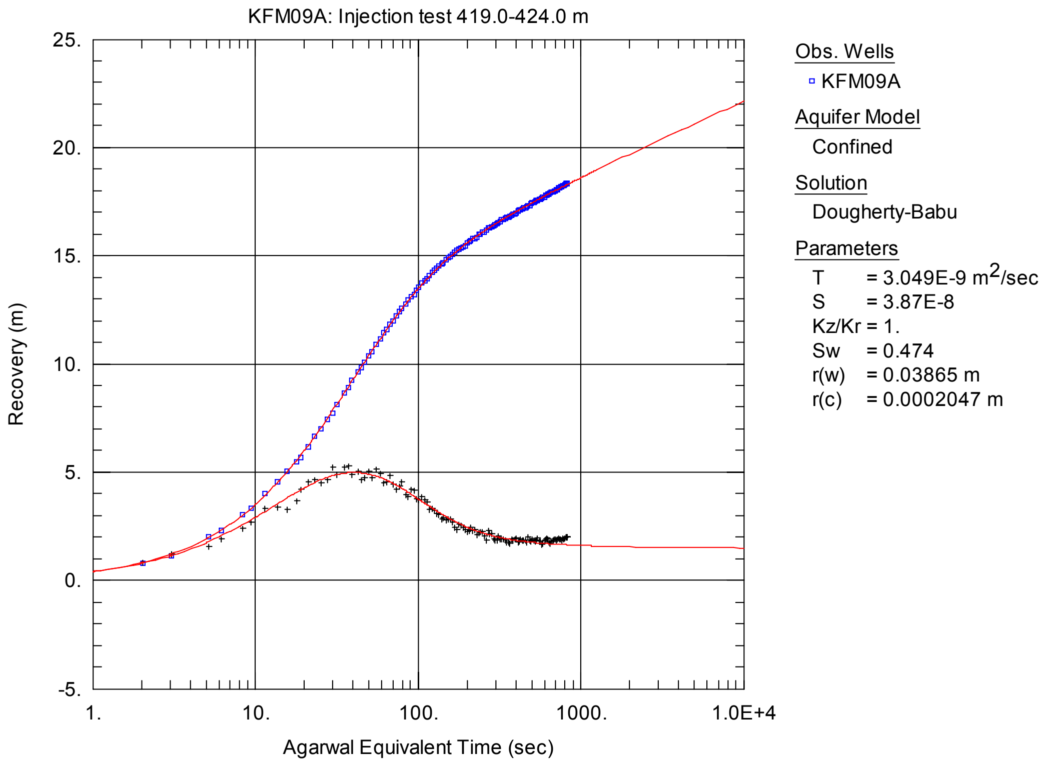


Figure A3-416. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 419.0-424.0 m in KFM09A.*

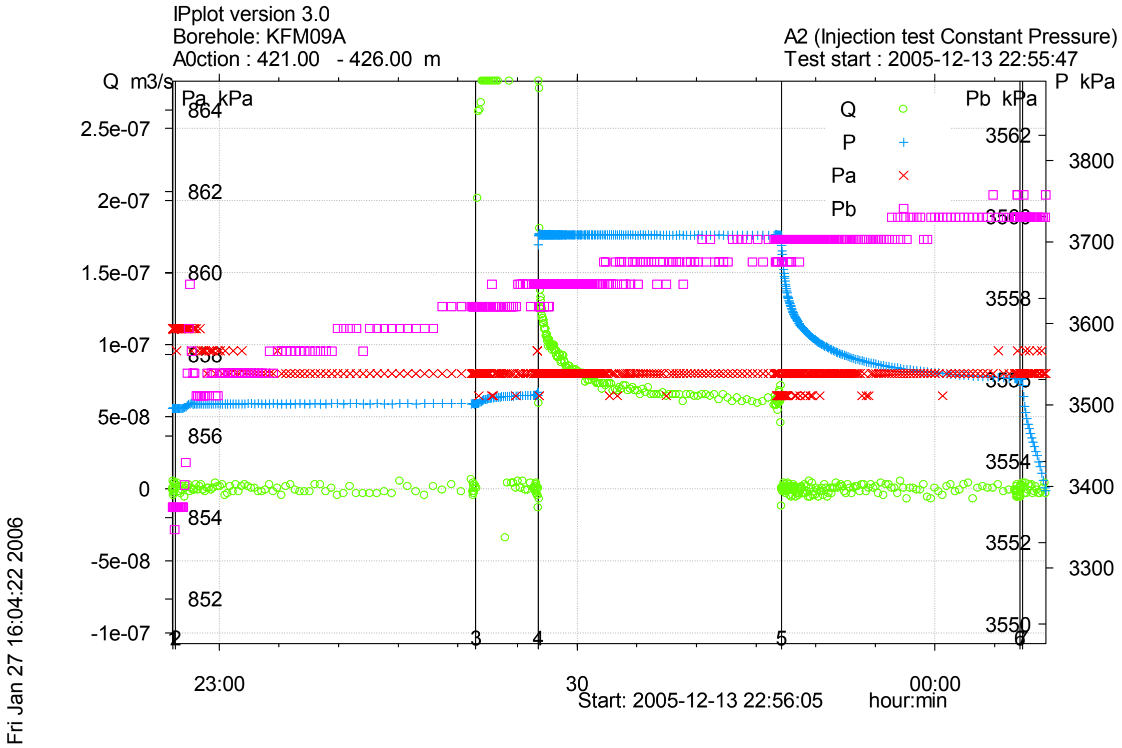


Figure A3-417. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 421.0-426.0 m in borehole KFM09A.

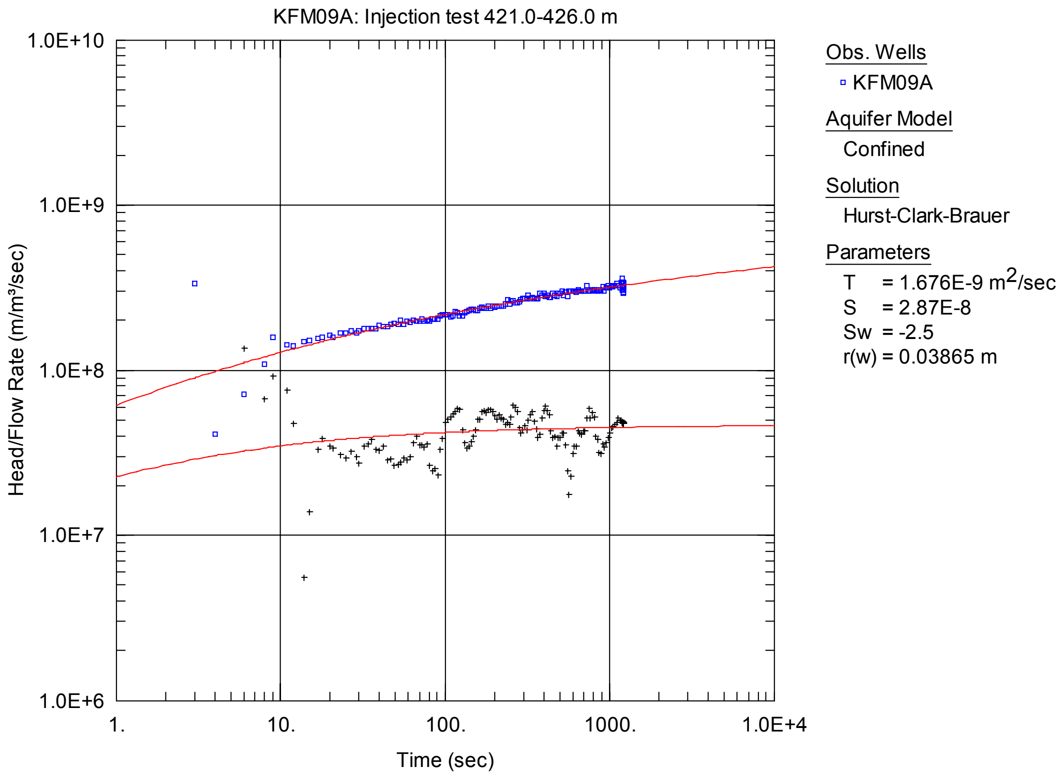


Figure A3-418. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 421.0-426.0 m in KFM09A.

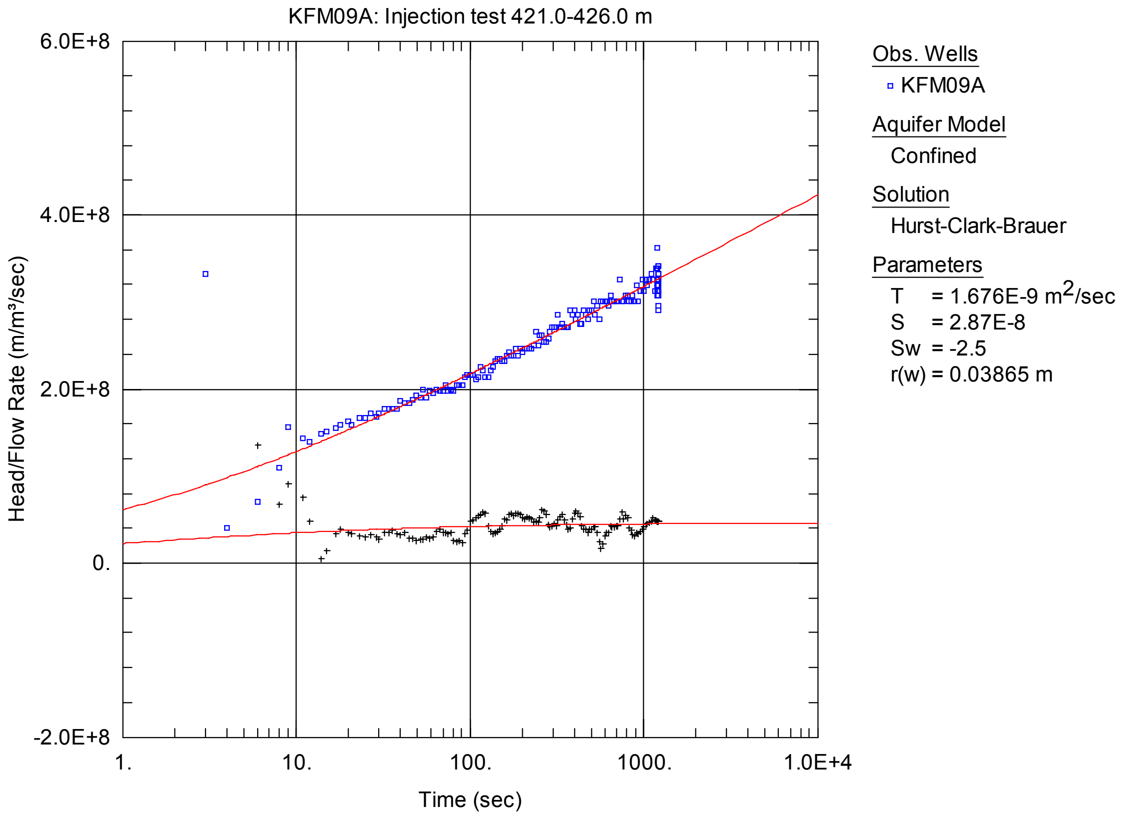


Figure A3-419. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 421.0-426.0 m in KFM09A.*

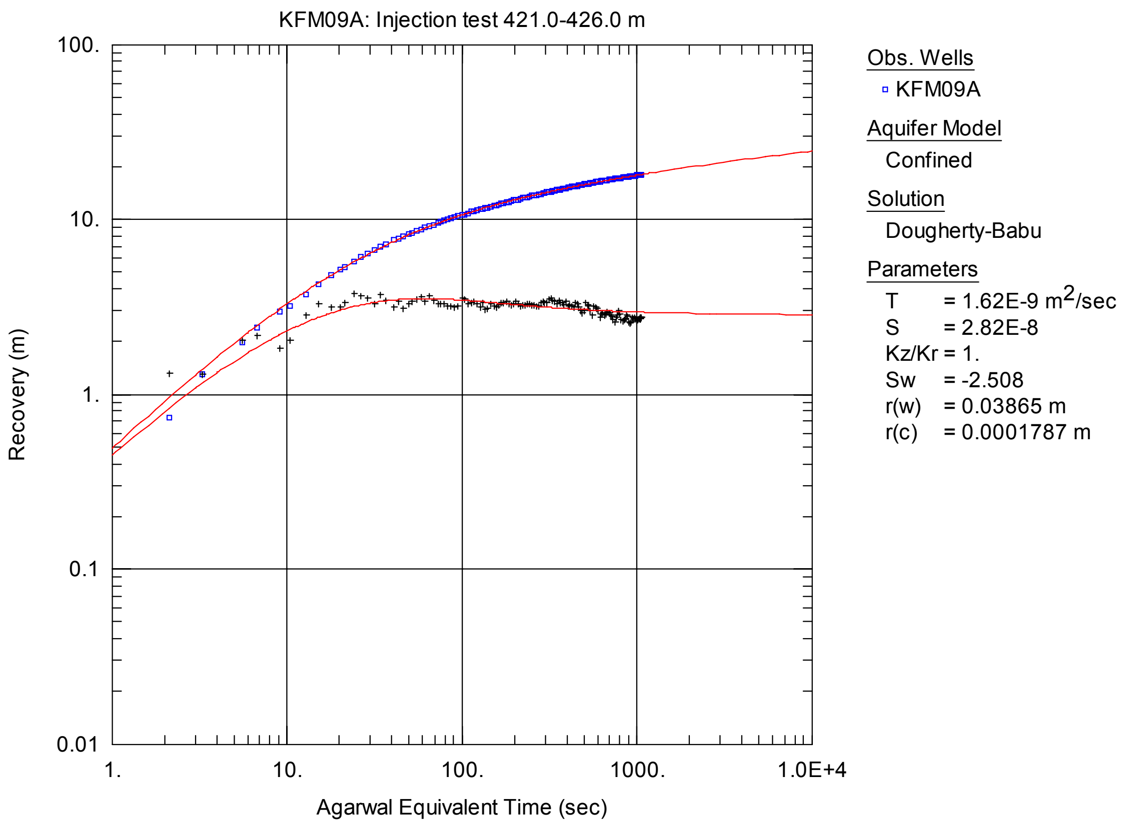


Figure A3-420. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 421.0-426.0 m in KFM09A.*

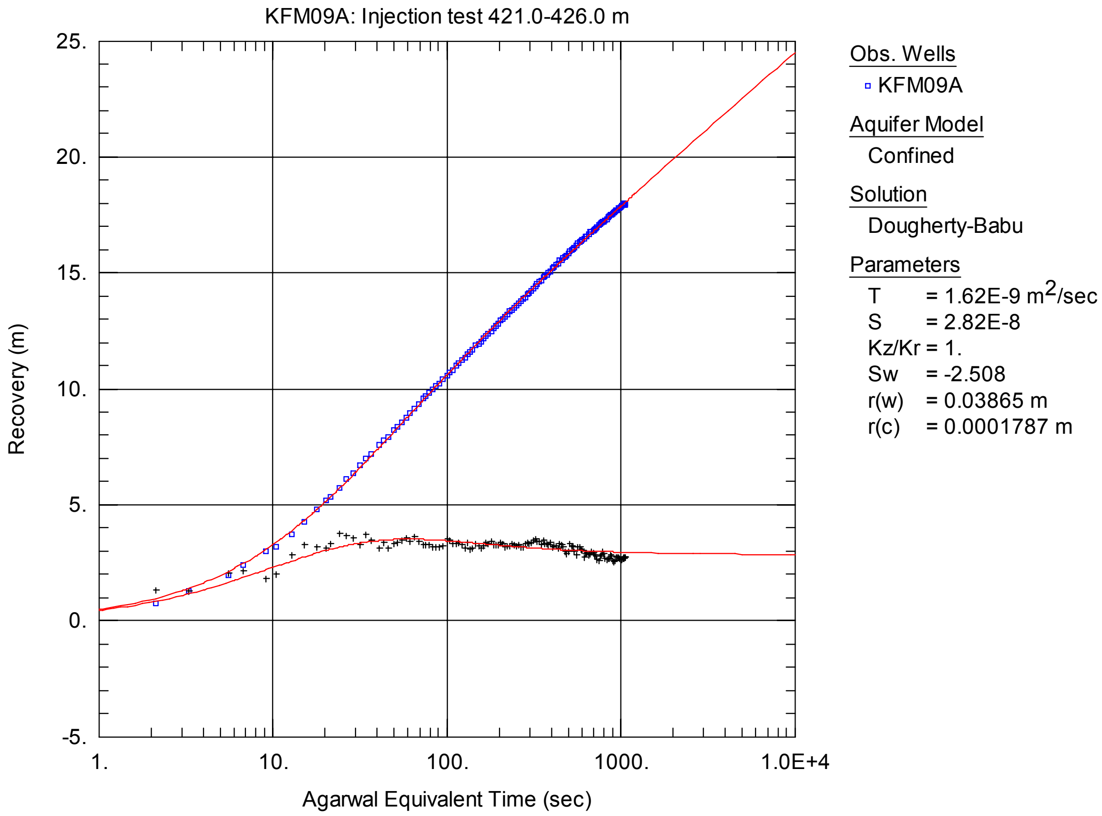


Figure A3-421. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 421.0-426.0 m in KFM09A.*

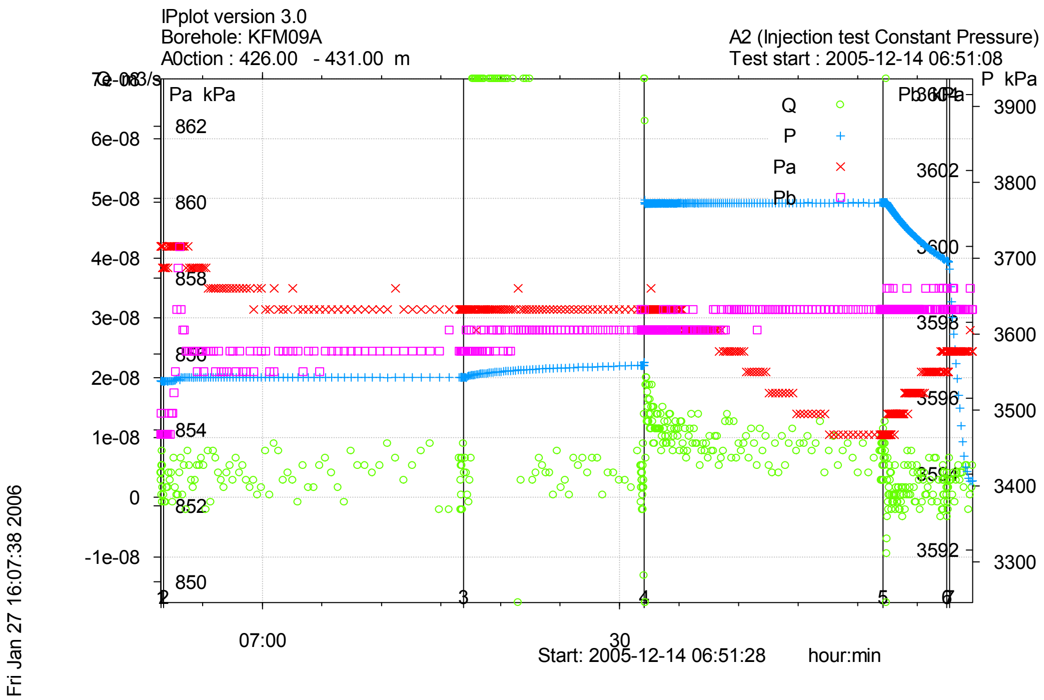


Figure A3-422. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 426.0-431.0 m in borehole KFM09A.*

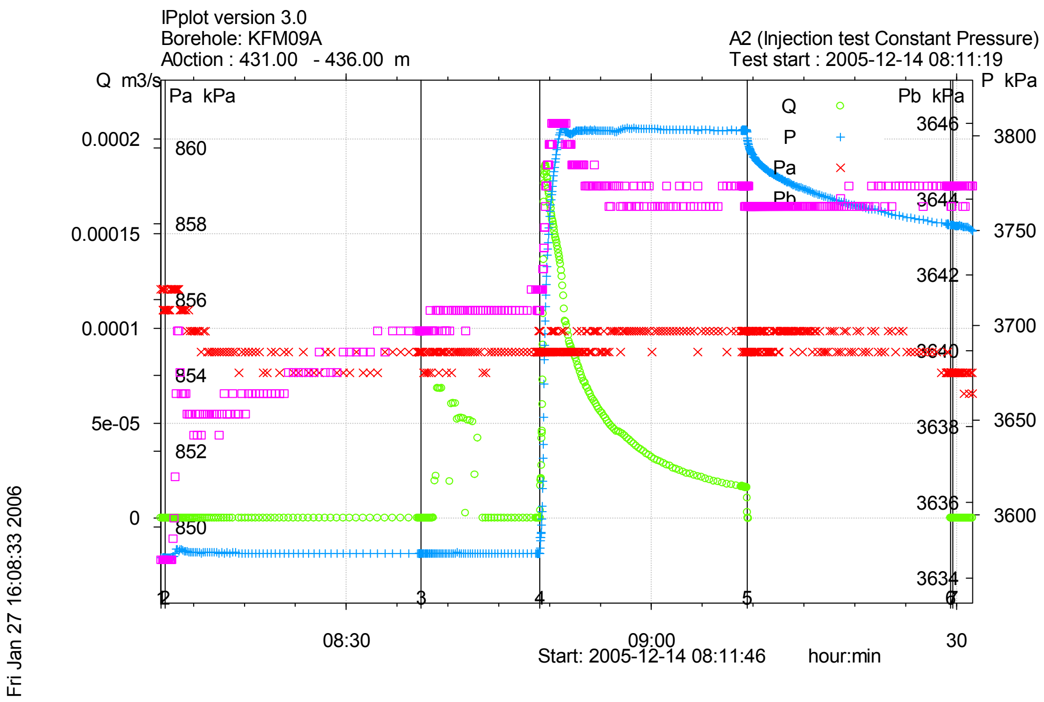


Figure A3-423. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 431.0-436.0 m in borehole KFM09A.*

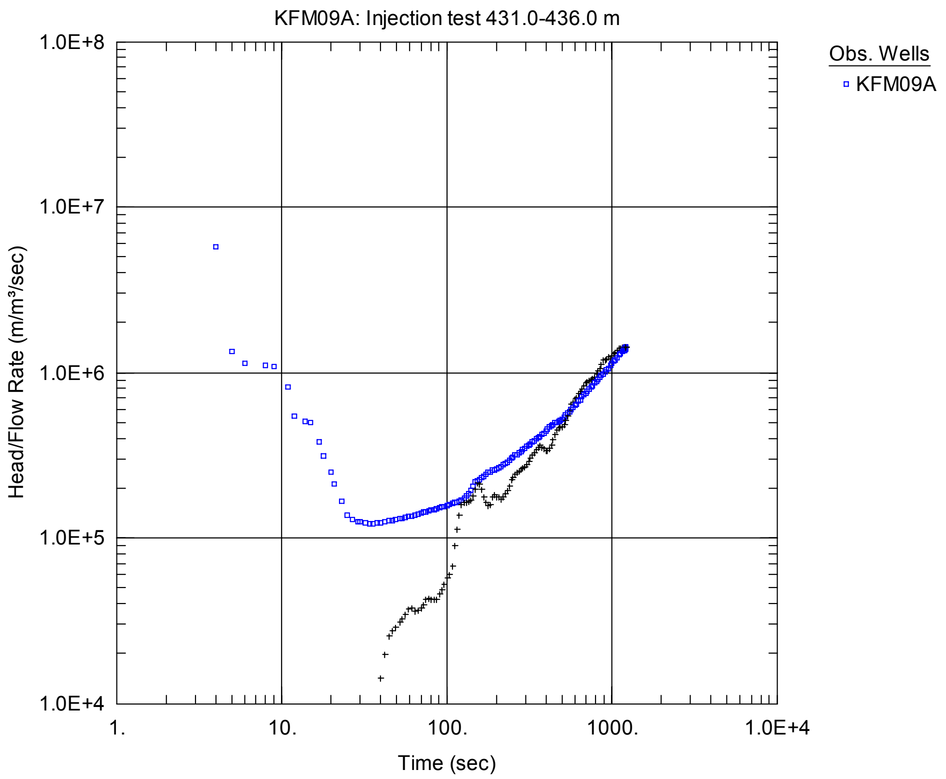


Figure A3-424. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 431.0-436.0 m in KFM09A.*

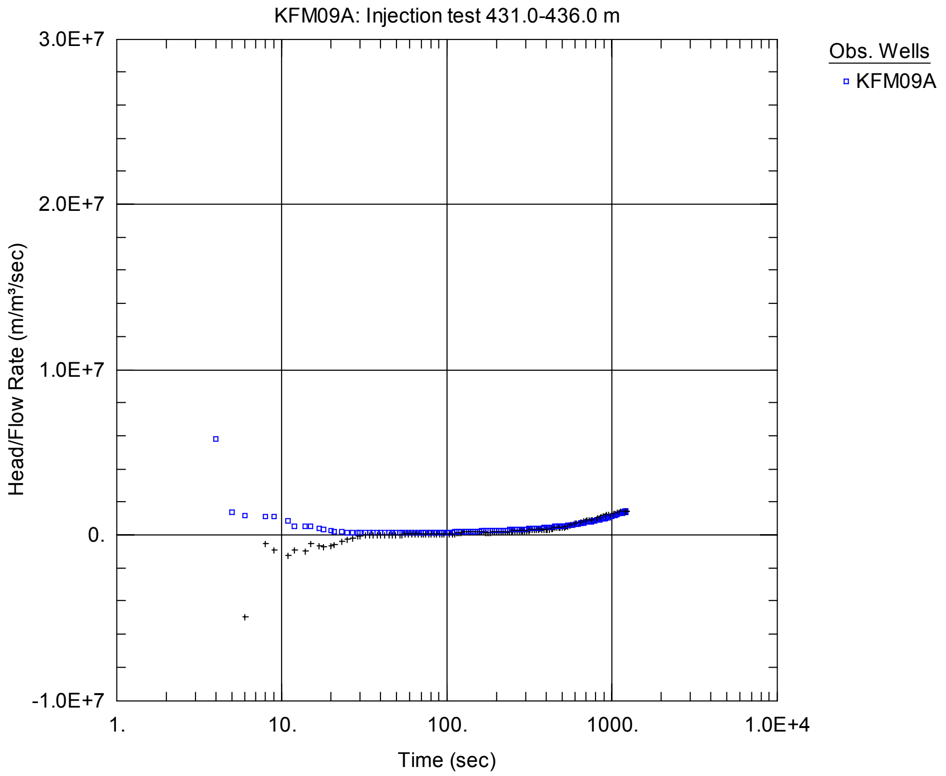


Figure A3-425. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 431.0-436.0 m in KFM09A.*

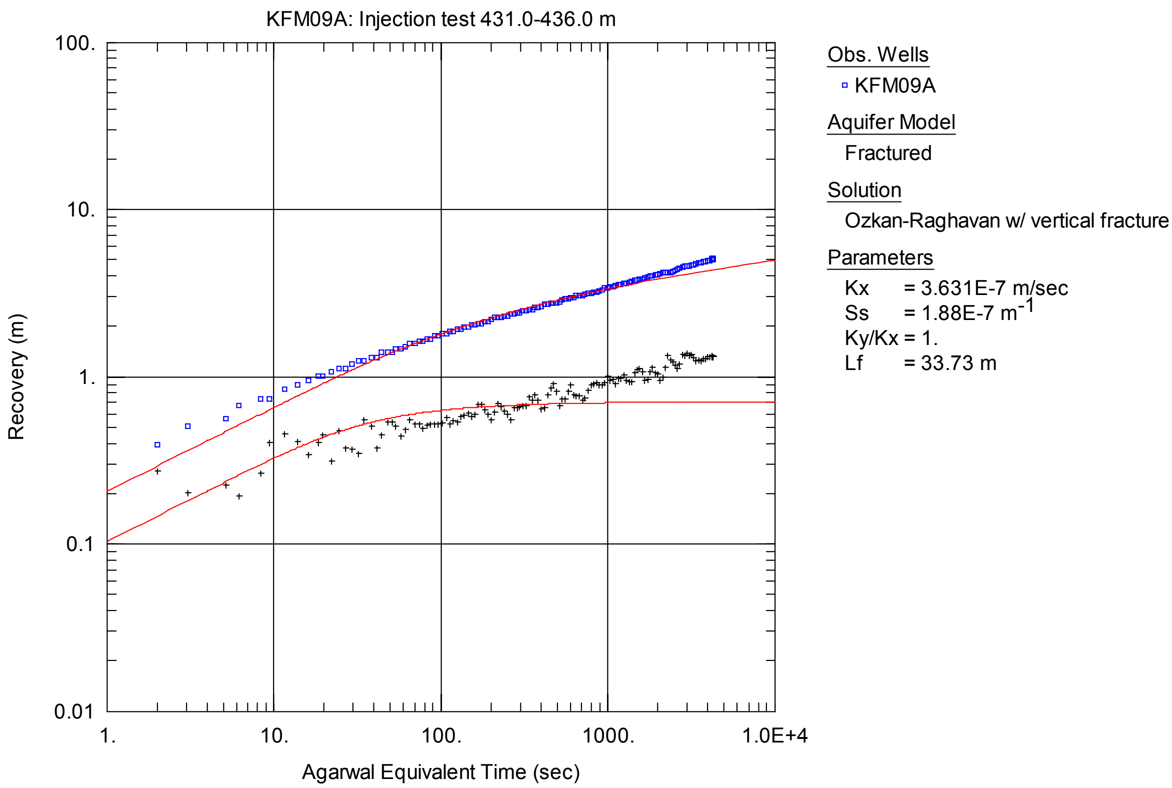


Figure A3-426. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 431.0-436.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

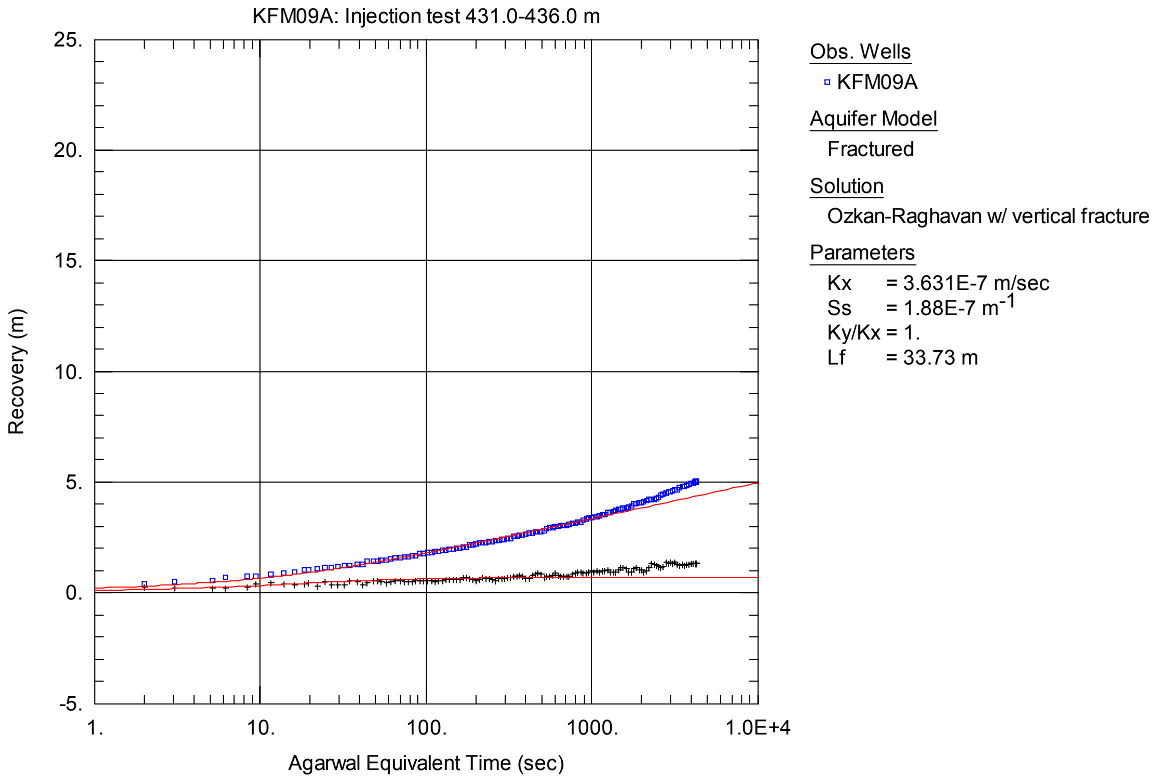


Figure A3-427. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 431.0-436.0 m in KFM09A.This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

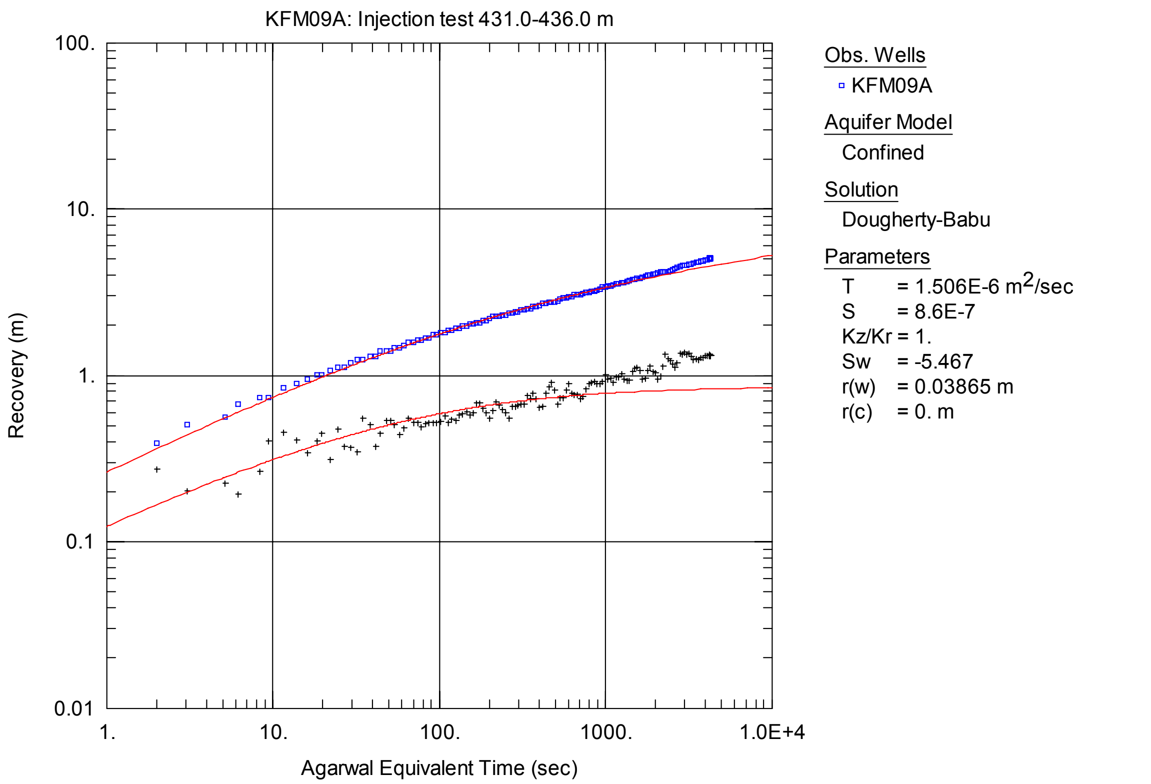


Figure A3-428. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 431.0-436.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

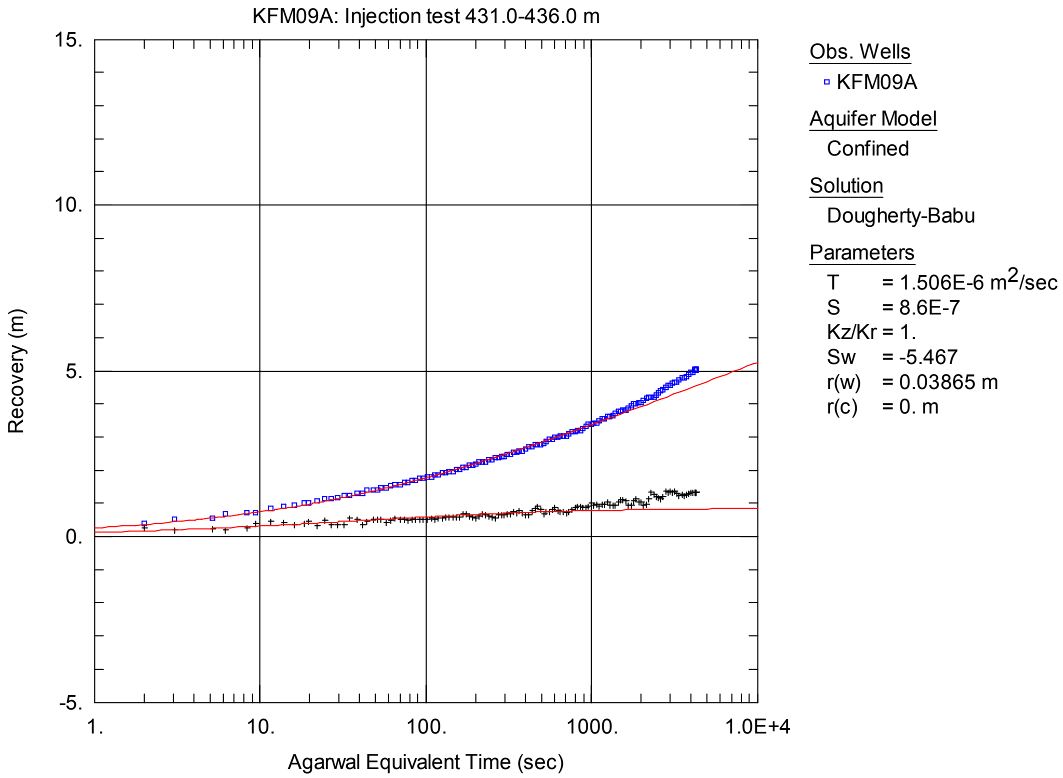


***Figure A3-429.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 431.0-436.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

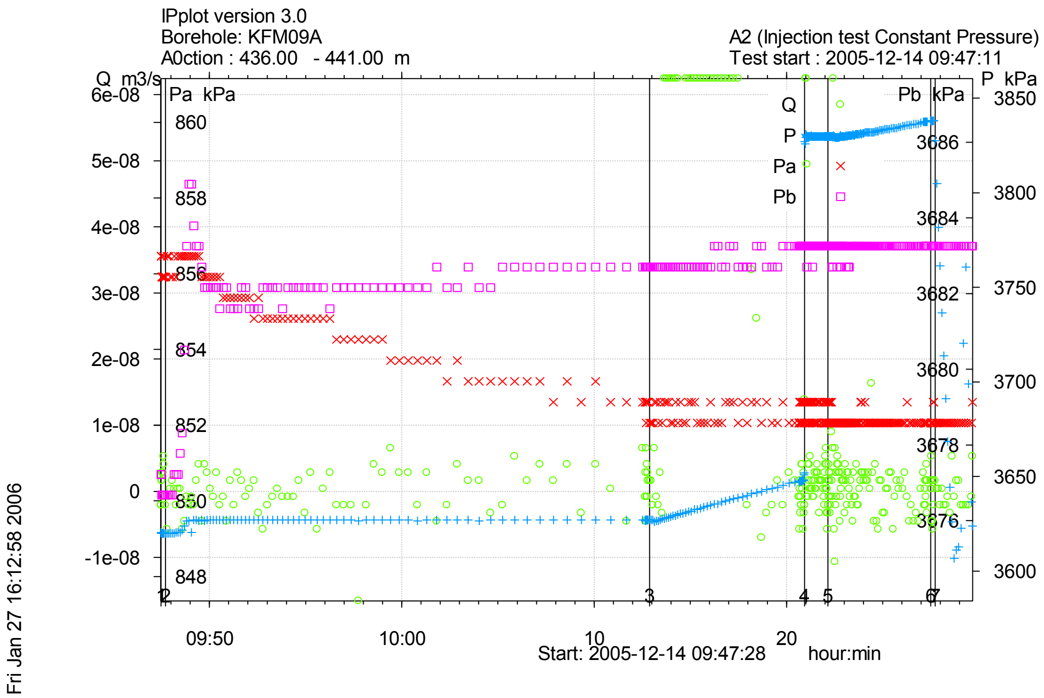


***Figure A3-430.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 436.0-441.0 m in borehole KFM09A.*

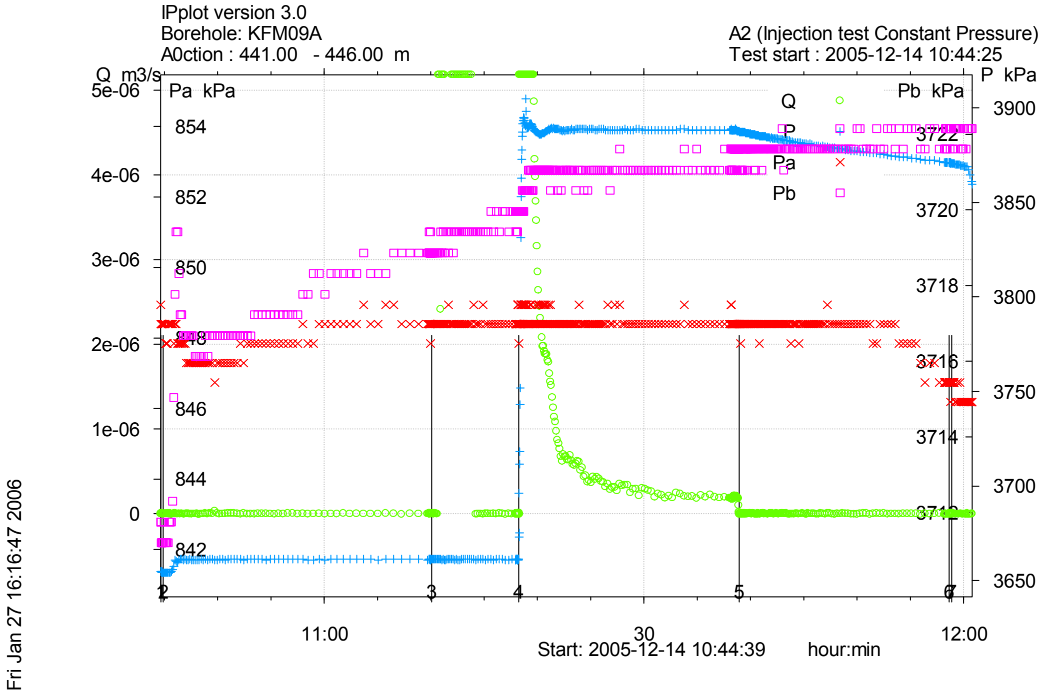


Figure A3-431. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in 441.0-446.0 m in borehole KFM09A.*

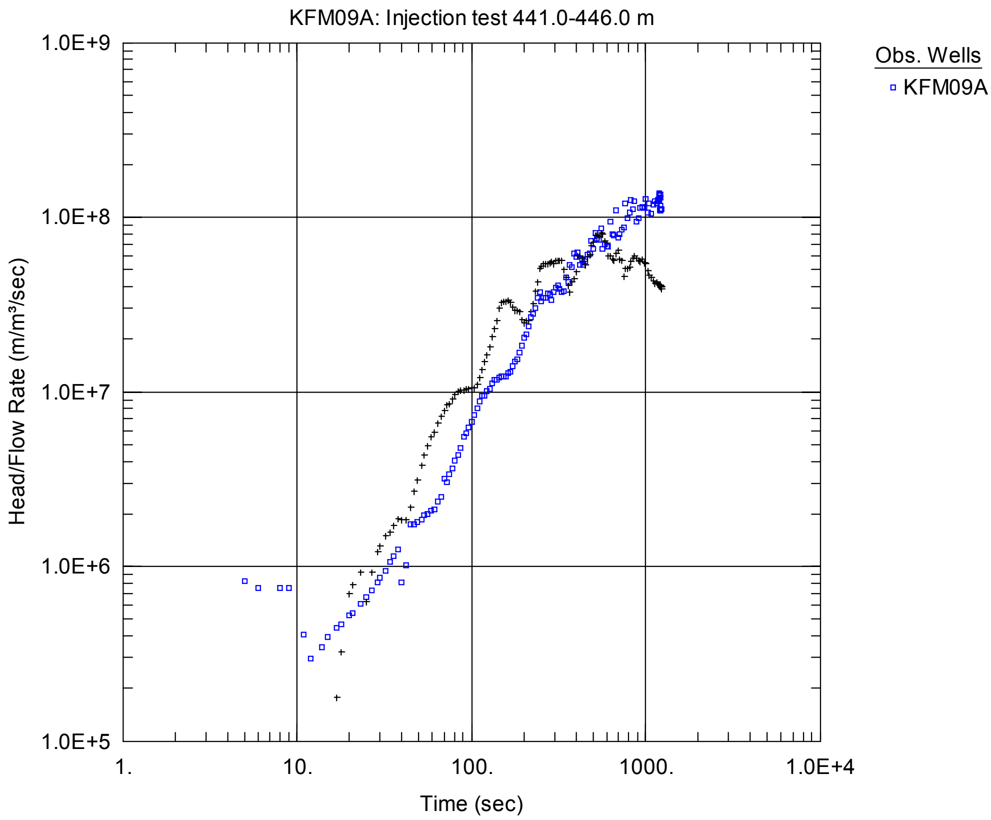


Figure A3-432. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 441.0-446.0 m in KFM09A.*

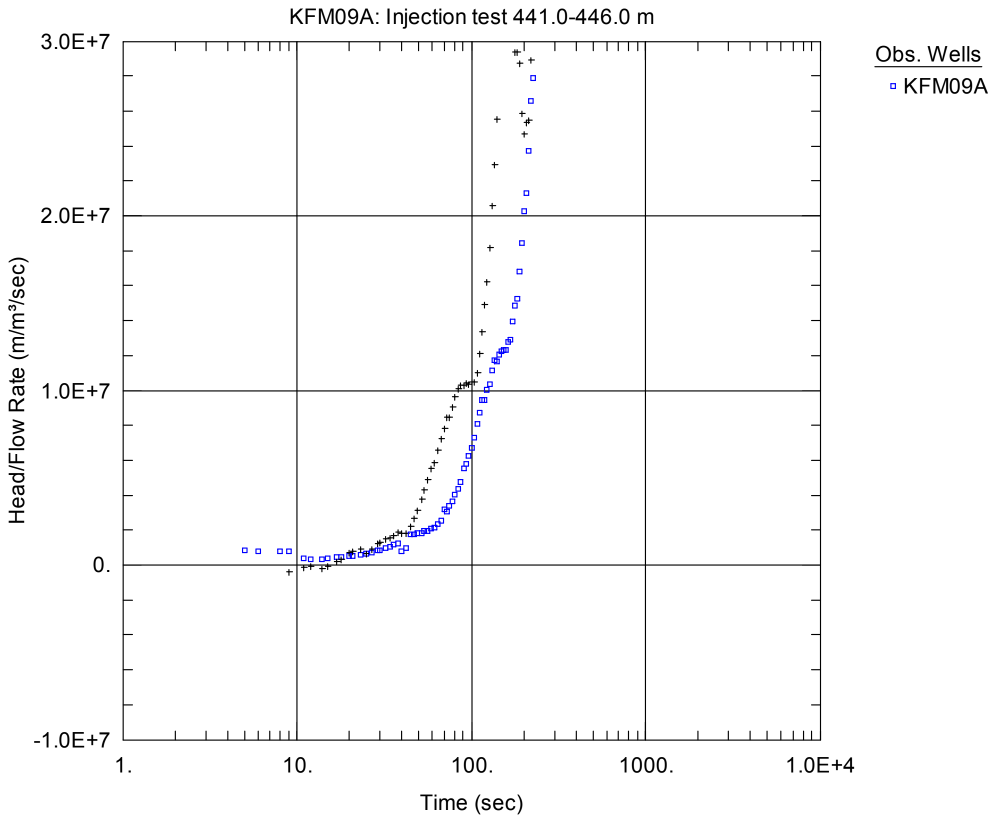


Figure A3-433. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 441.0-446.0 m in KFM09A.*

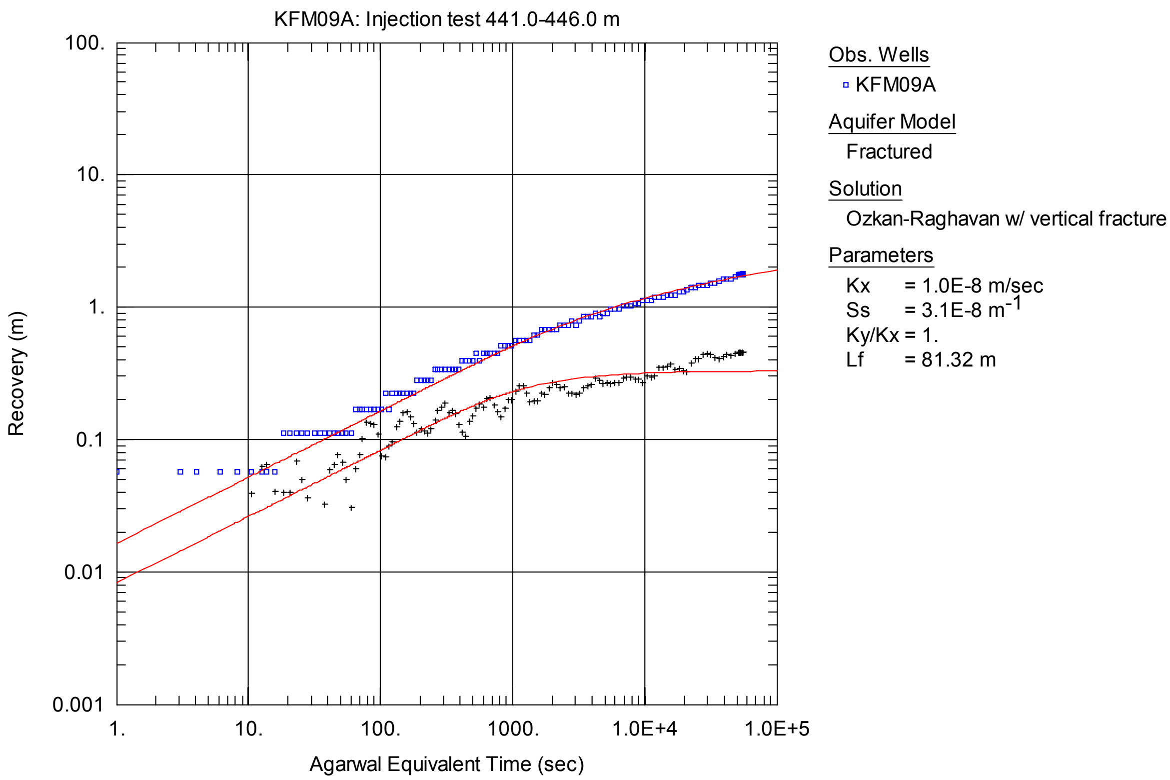


Figure A3-434. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 441.0-446.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

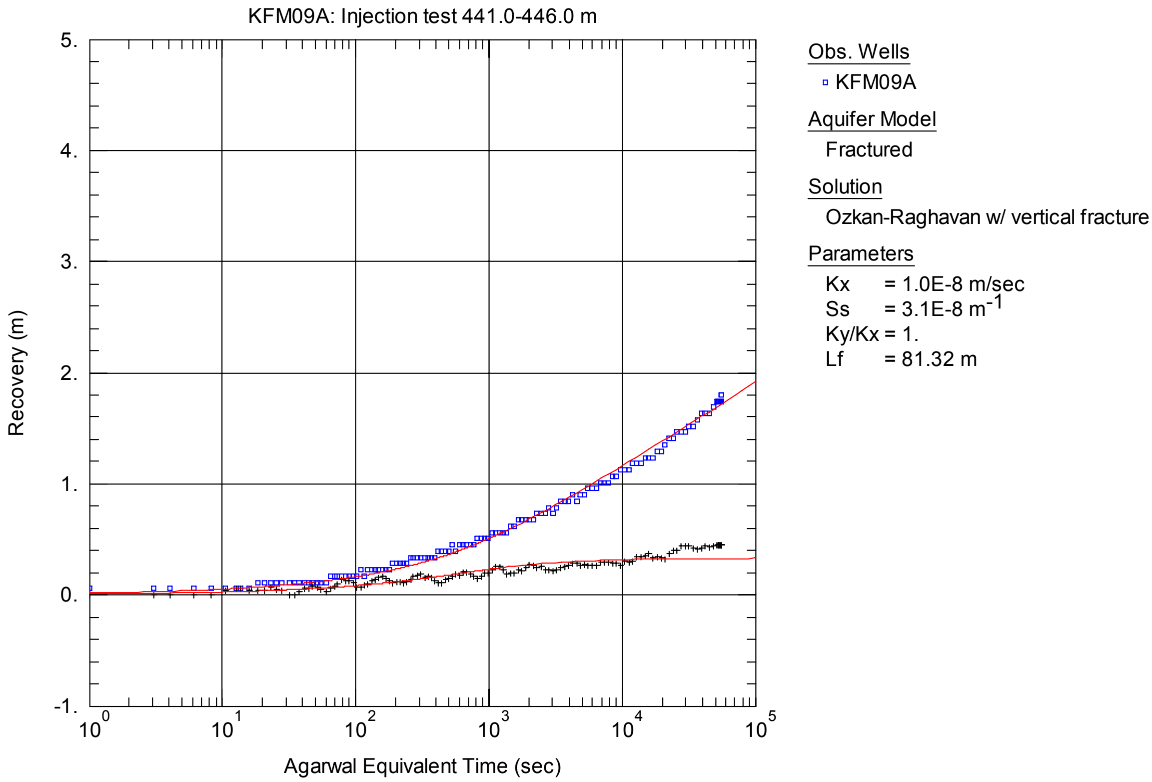


__Figure A3-435.__ Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 441.0-446.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.

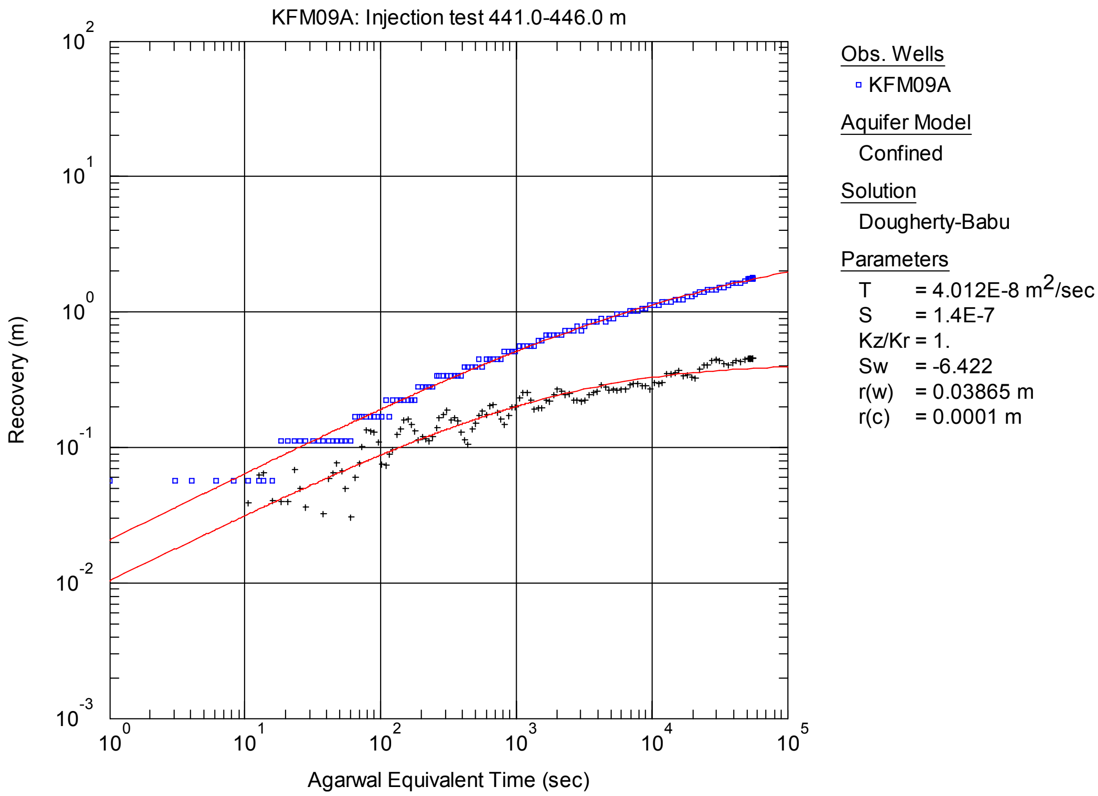


__Figure A3-436.__ Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 441.0-446.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.

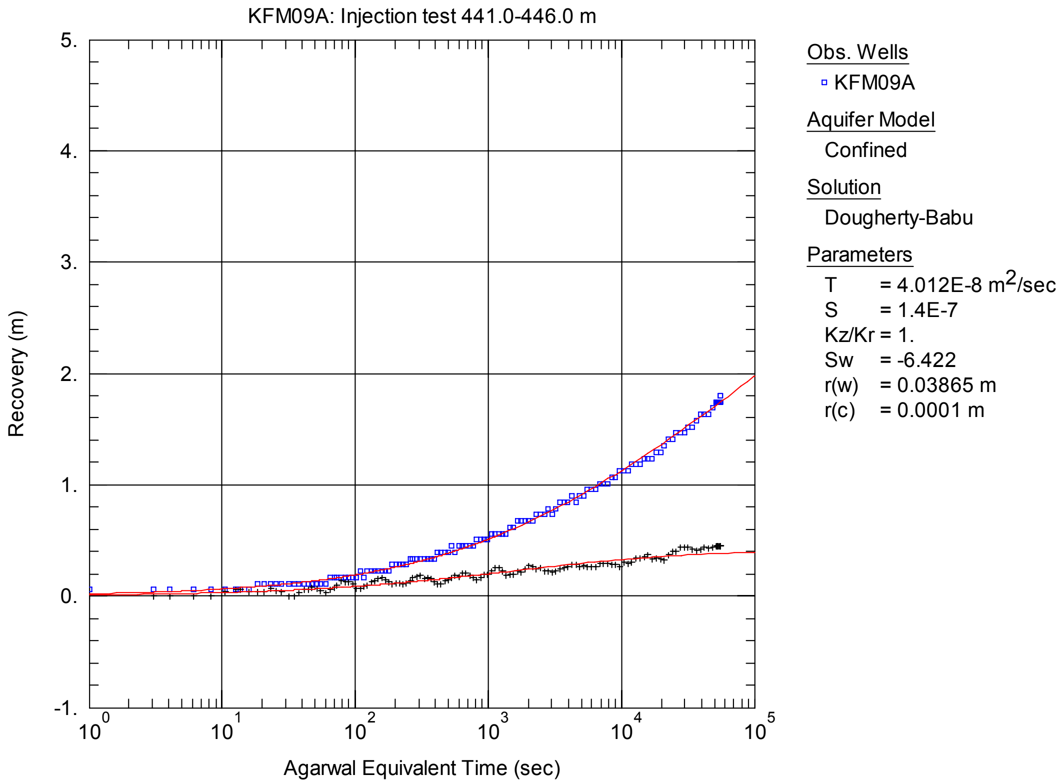


Figure A3-437. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 441.0-446.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

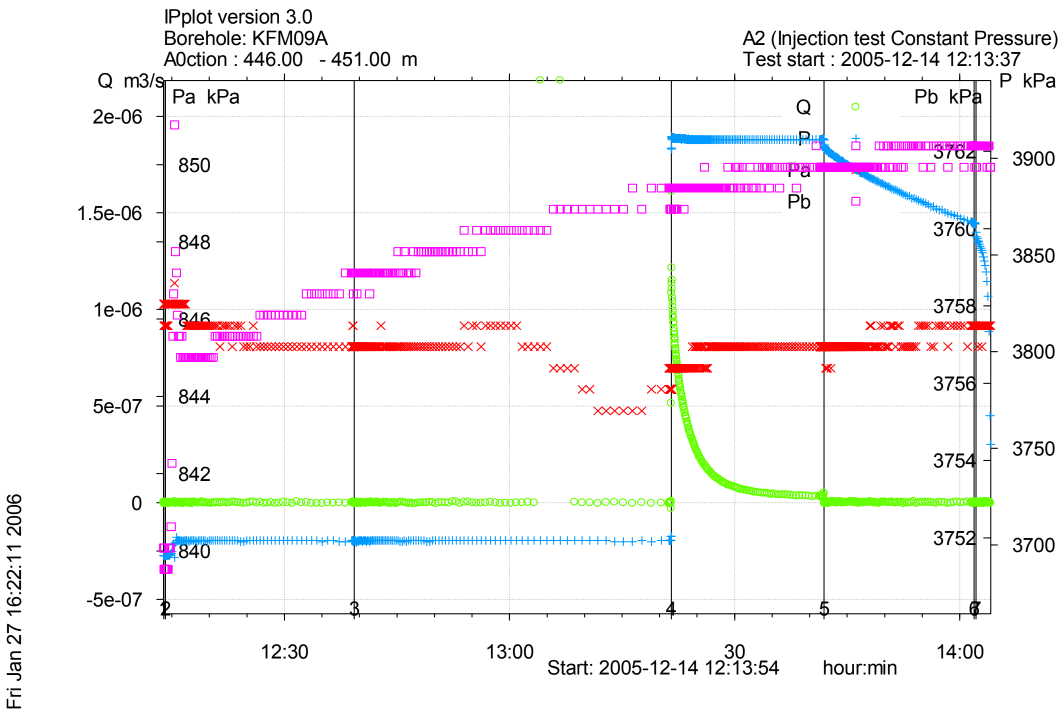


Figure A3-438. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 446.0-451.0 m in borehole KFM09A.*

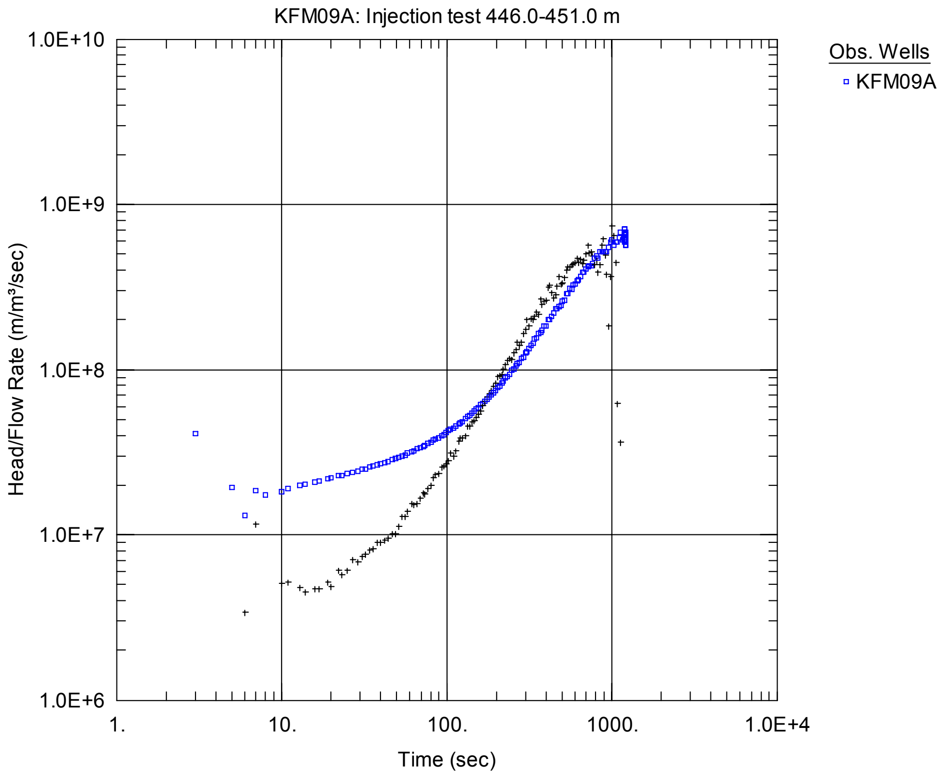


Figure A3-439. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 446.0-451.0 m in KFM09A.*

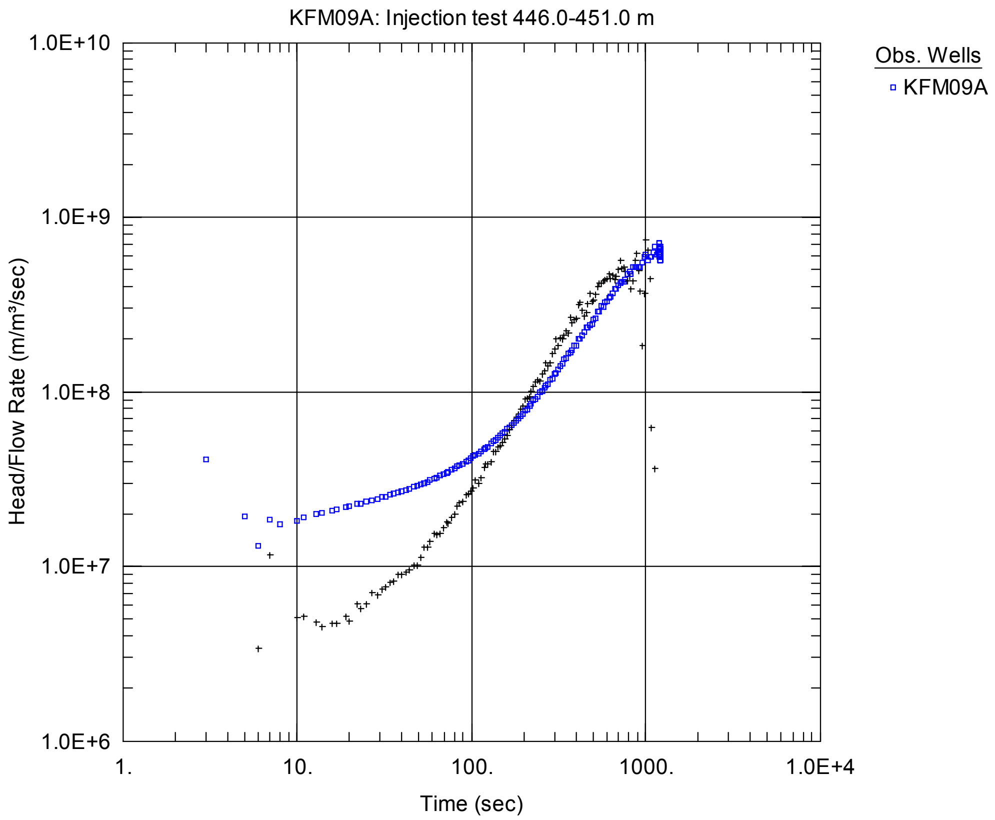


Figure A3-440. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 446.0-451.0 m in KFM09A.*

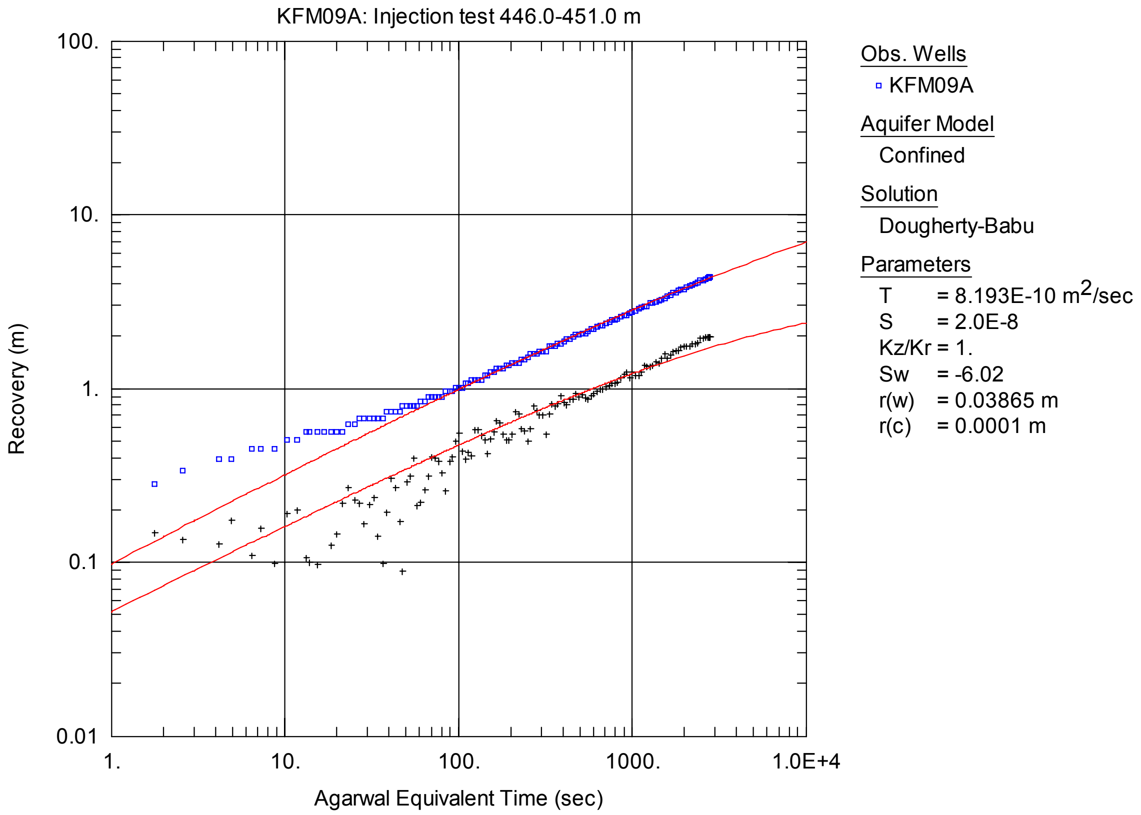


***Figure A3-441.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 446.0-451.0 m in KFM09A.*

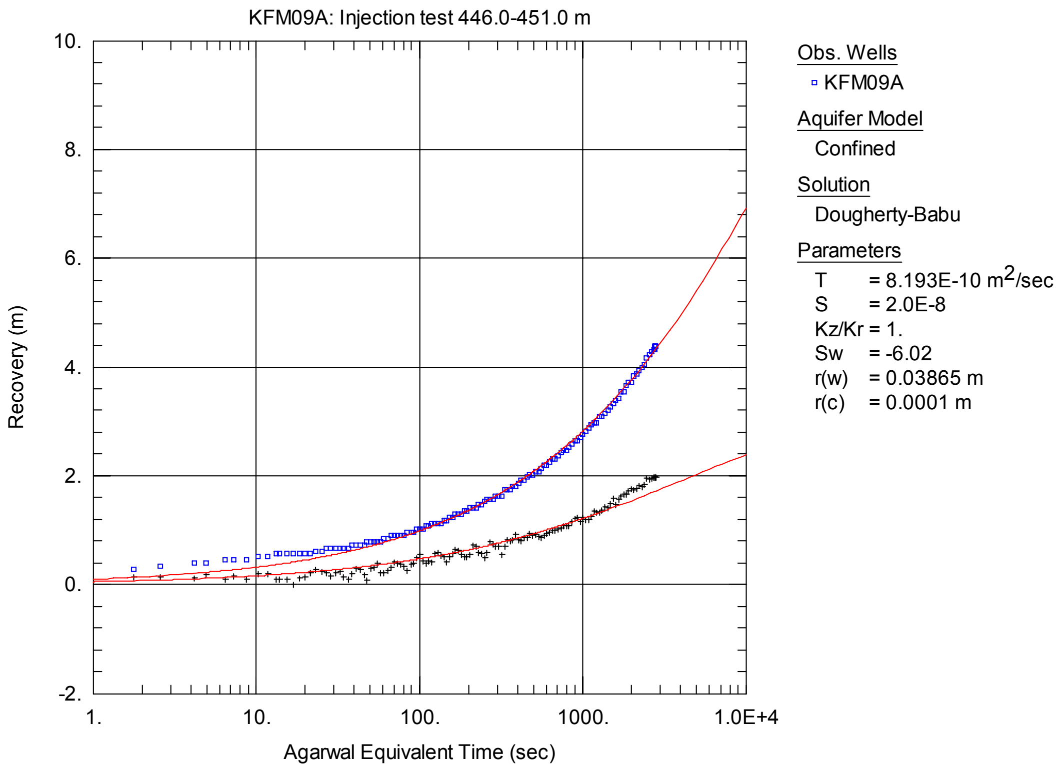


***Figure A3-442.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 446.0-451.0 m in KFM09A.*

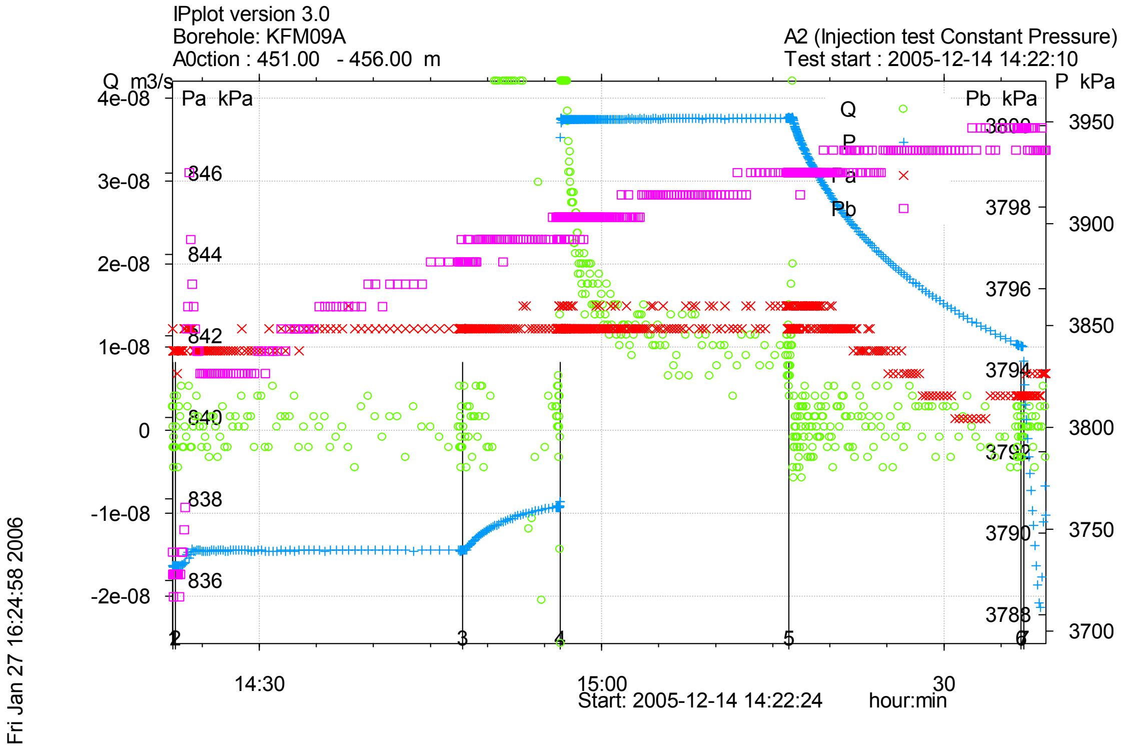


Figure A3-443. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 451.0-456.0 m in borehole KFM09A.

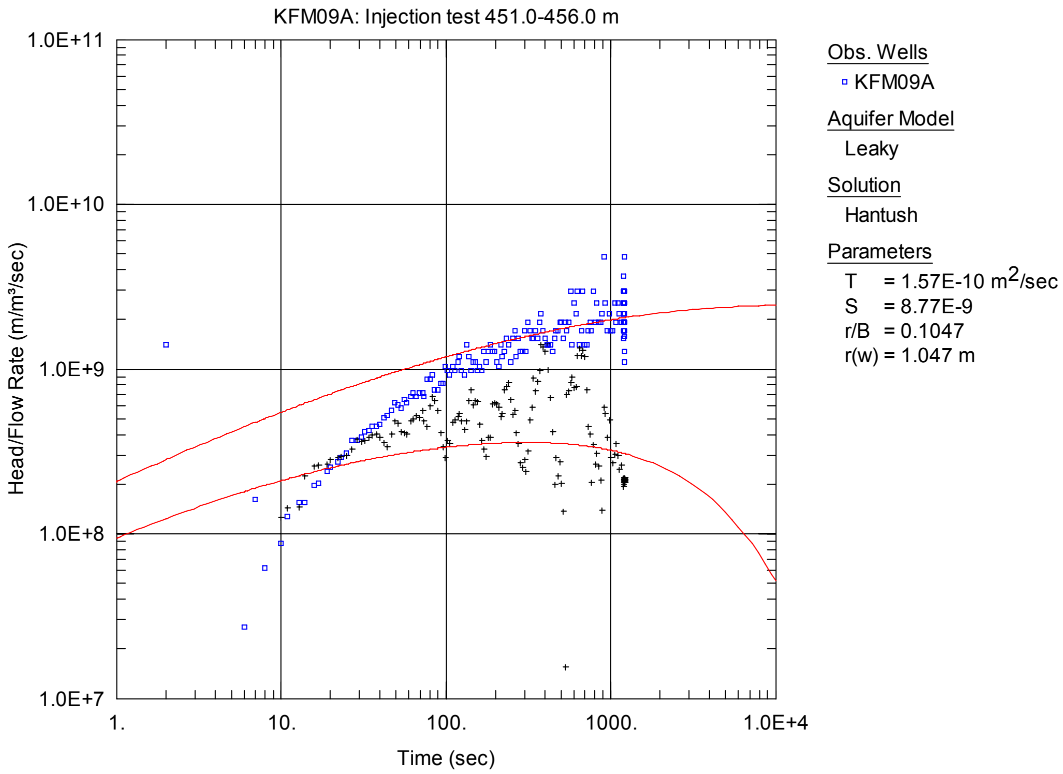


Figure A3-444. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 451.0-456.0 m in KFM09A.

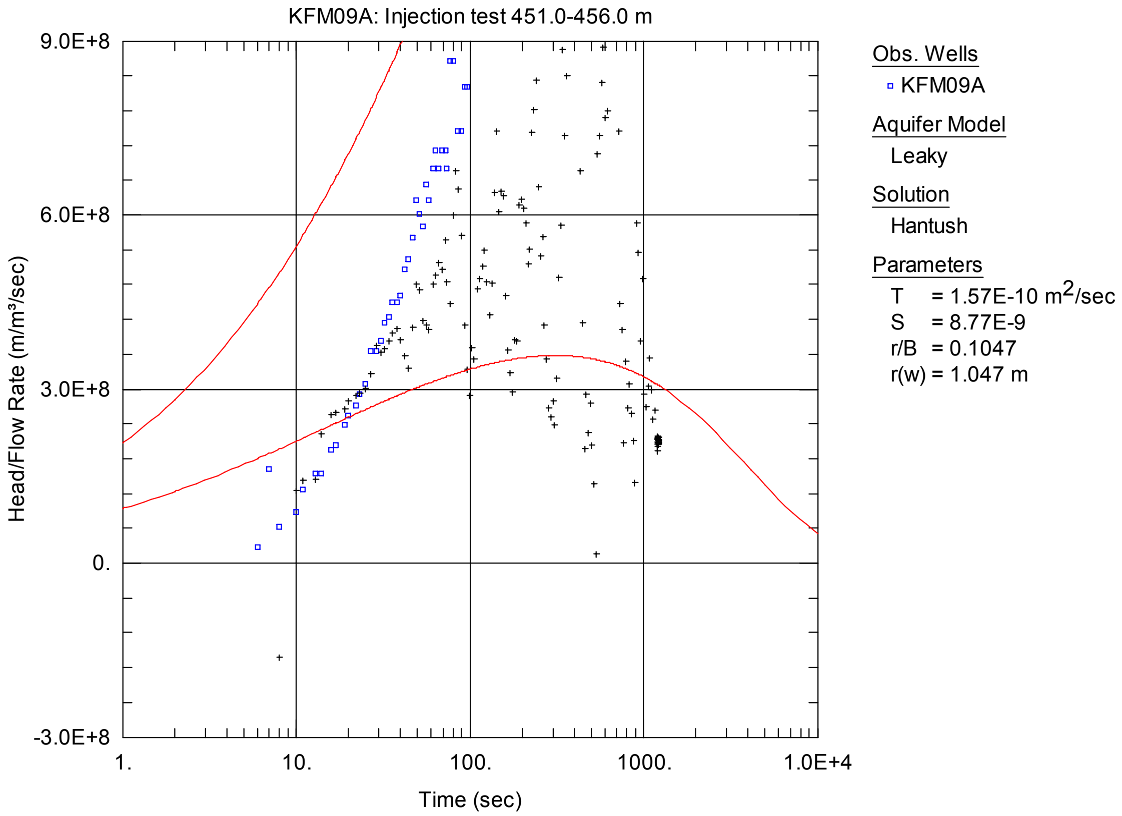


***Figure A3-445.** Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 451.0-456.0 m in KFM09A.*

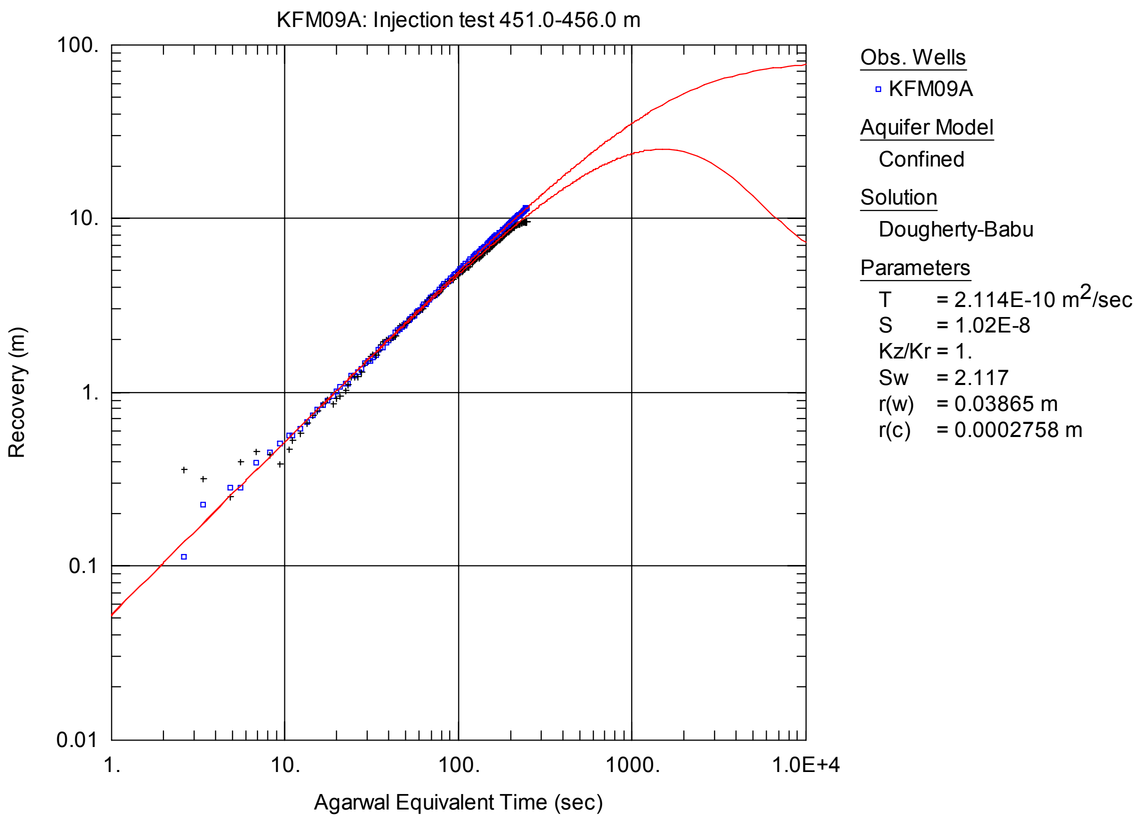


***Figure A3-446.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 451.0-456.0 m in KFM09A.*

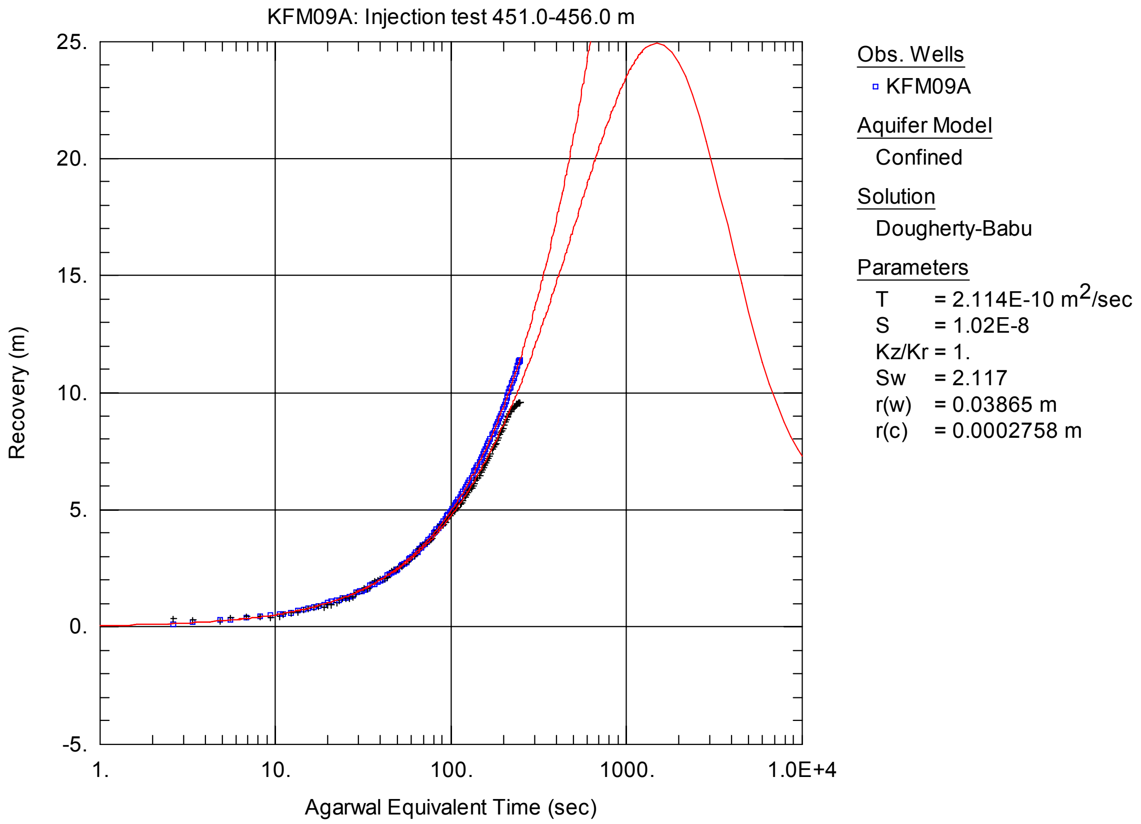


Figure A3-447. Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 451.0-456.0 m in KFM09A.

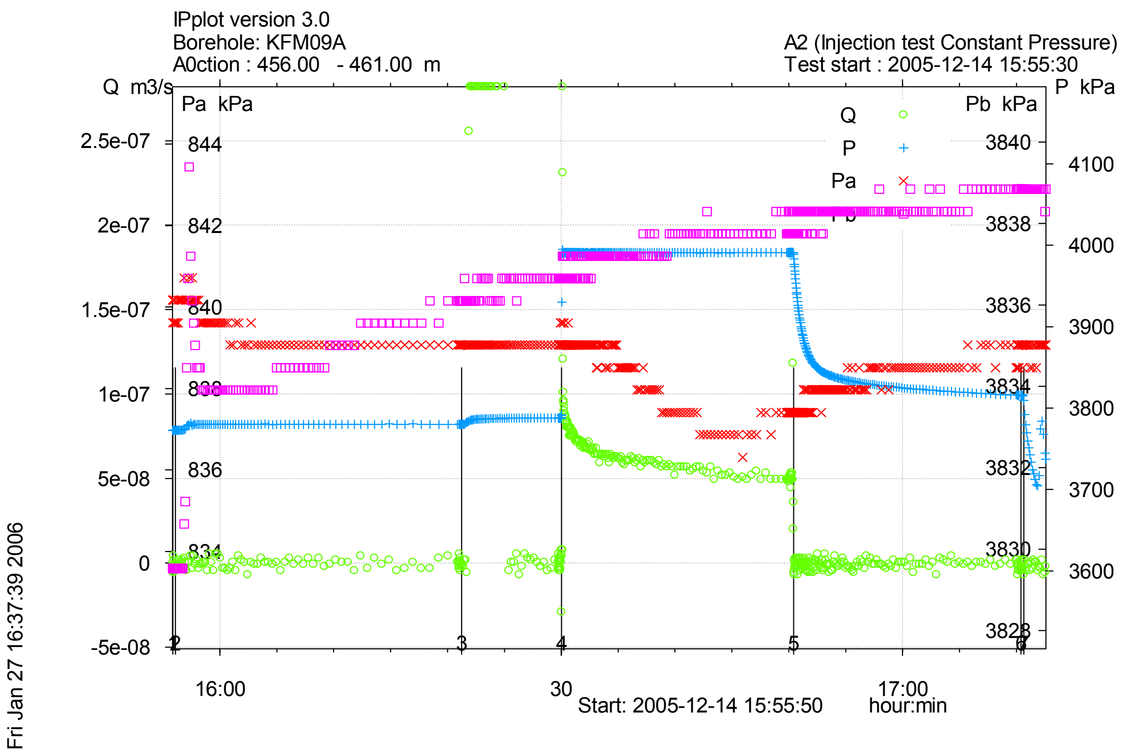


Figure A3-448. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 456.0-461.0 m in borehole KFM09A.*

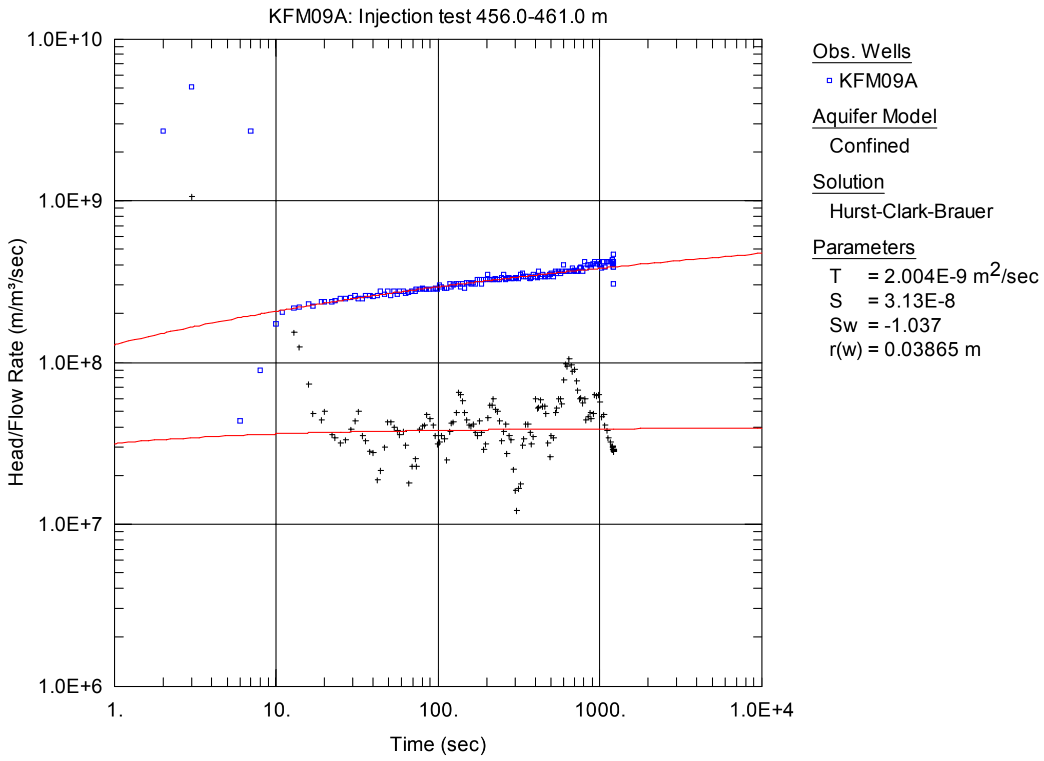


Figure A3-449. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 456.0-461.0 m in KFM09A.*

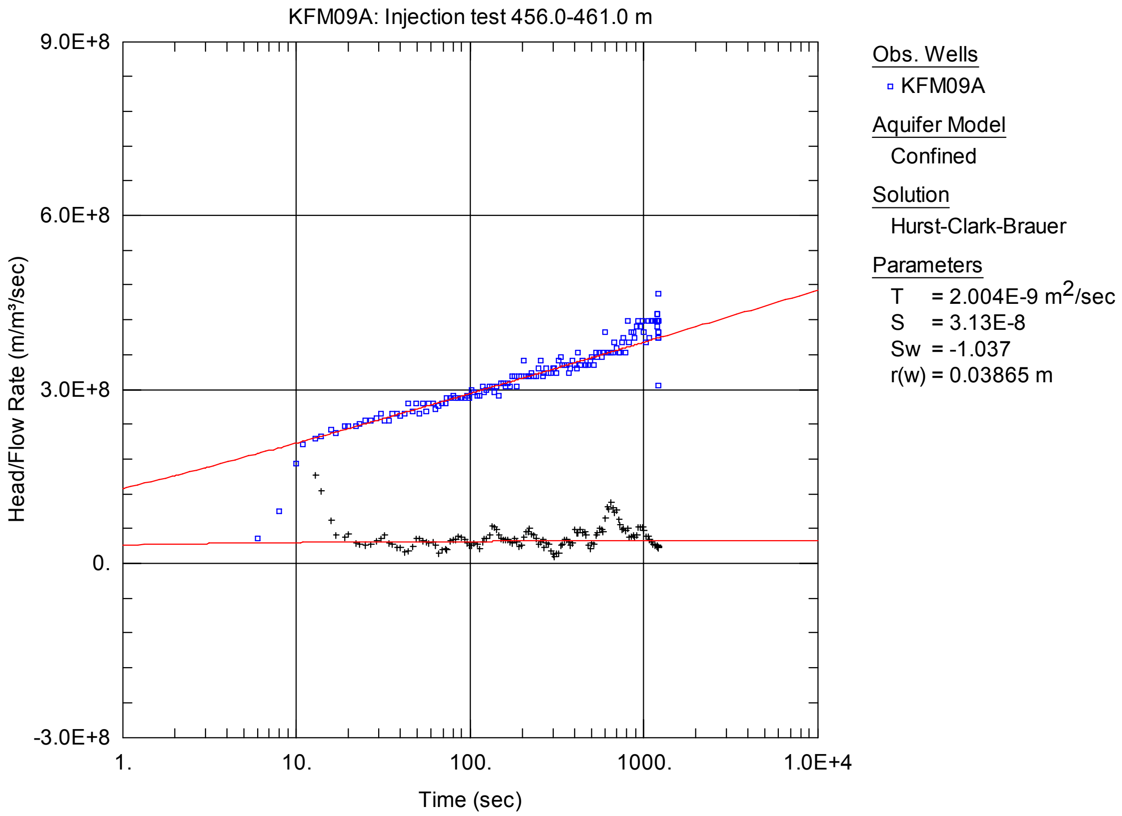


Figure A3-450. Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 456.0-461.0 m in KFM09A.

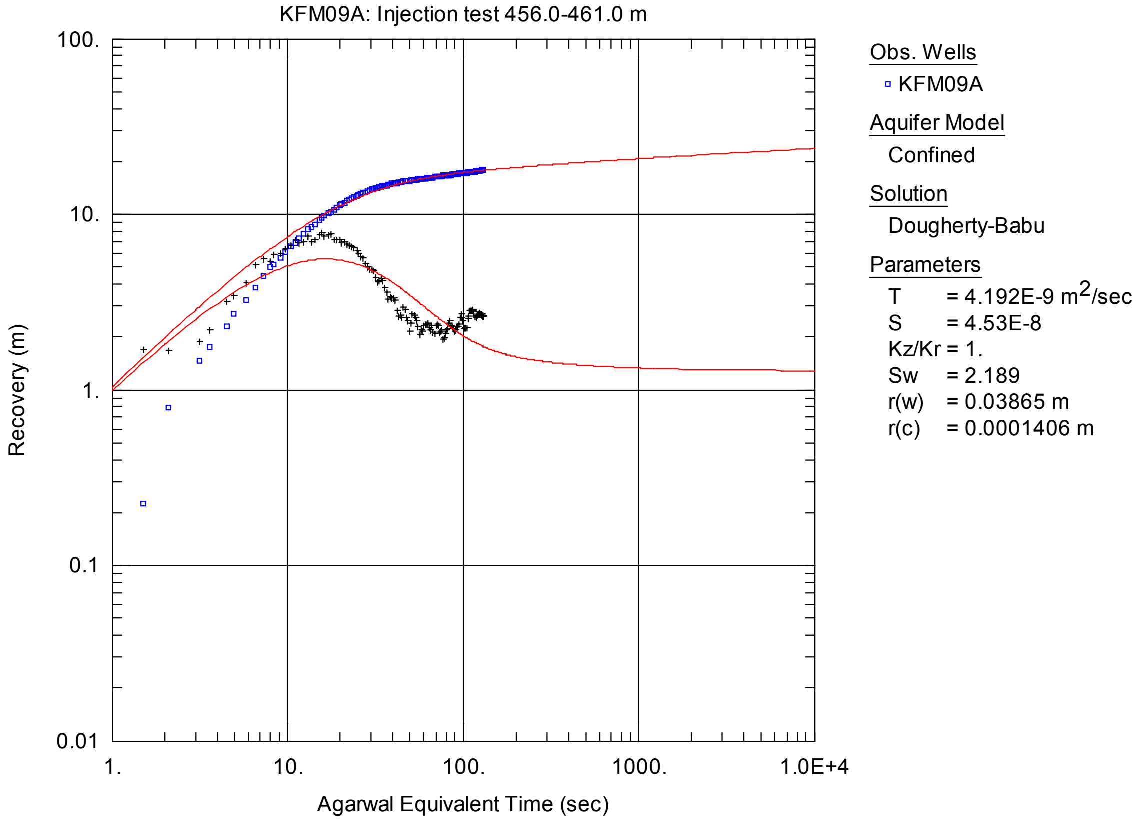


Figure A3-451. Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 456.0-461.0 m in KFM09A.

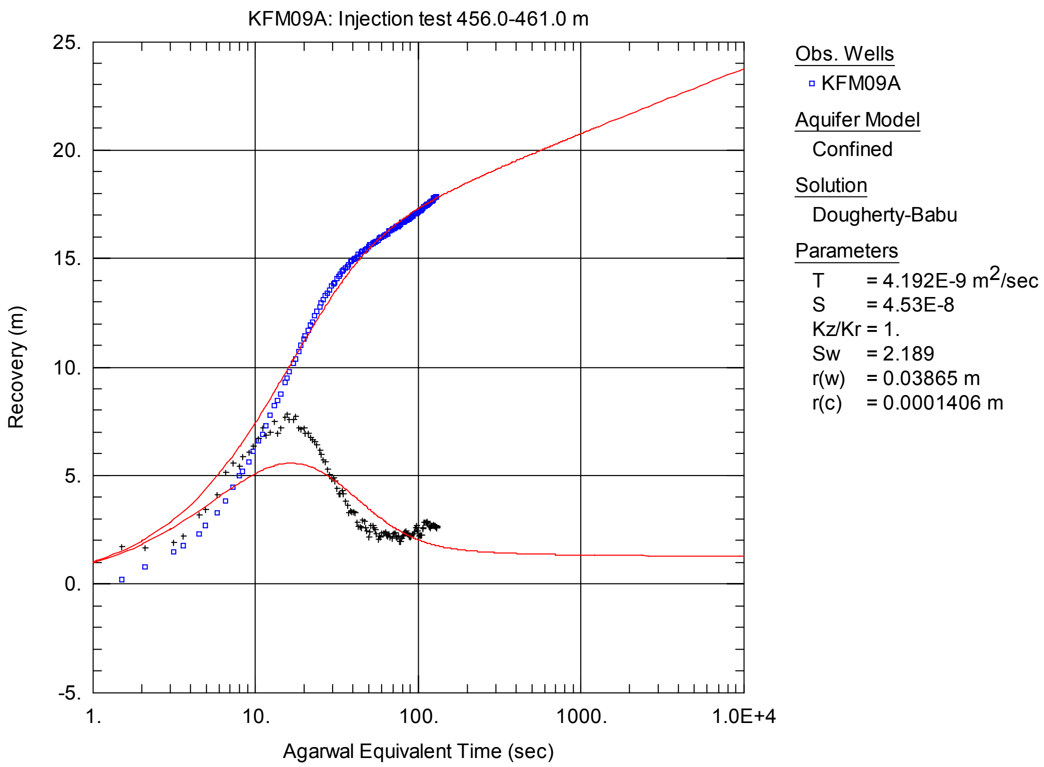


***Figure A3-452.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 456.0-461.0 m in KFM09A.*

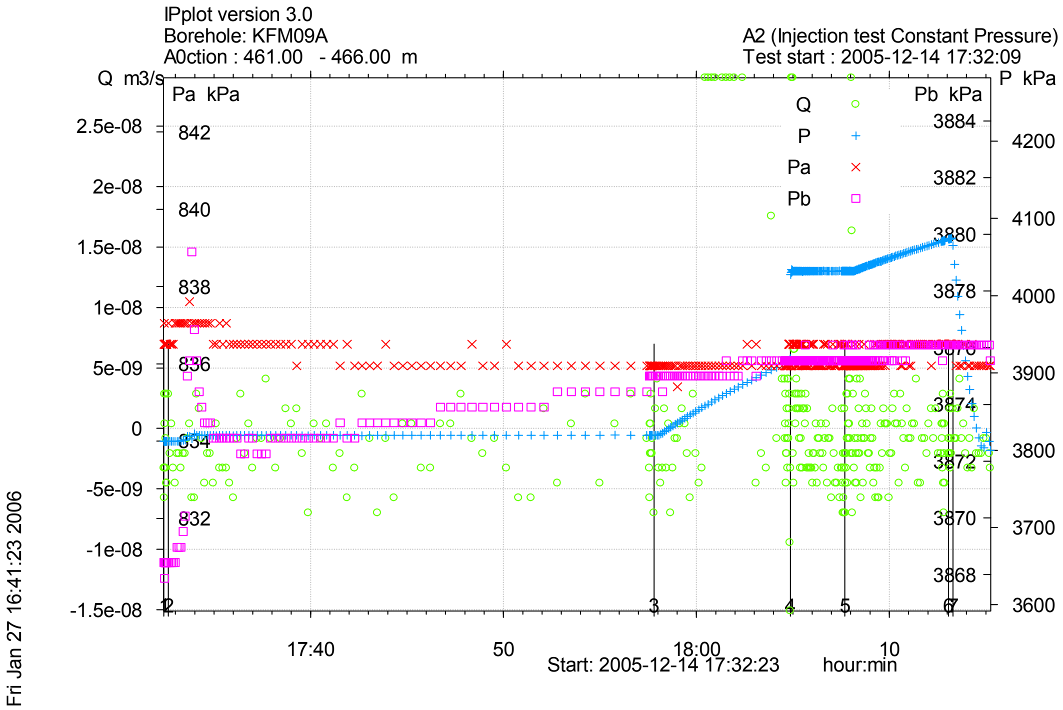


***Figure A3-453.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 461.0-466.0 m in borehole KFM09A.*

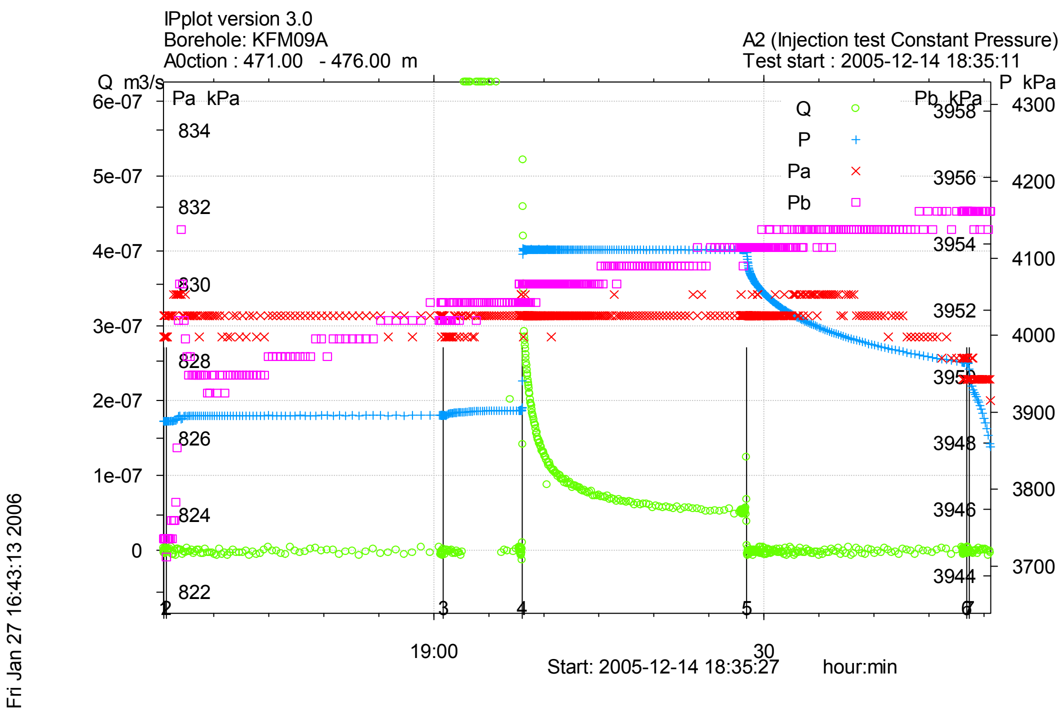


Figure A3-454. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 471.0-476.0 m in borehole KFM09A.*

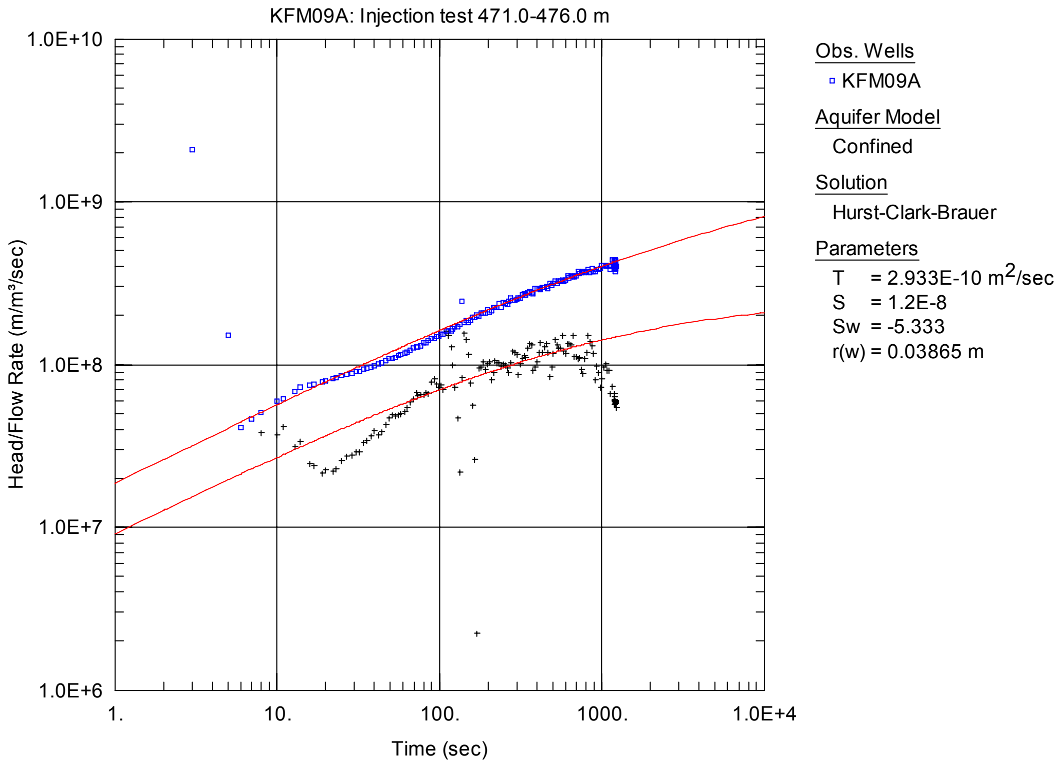


Figure A3-455. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 471.0-476.0 m in KFM09A.*

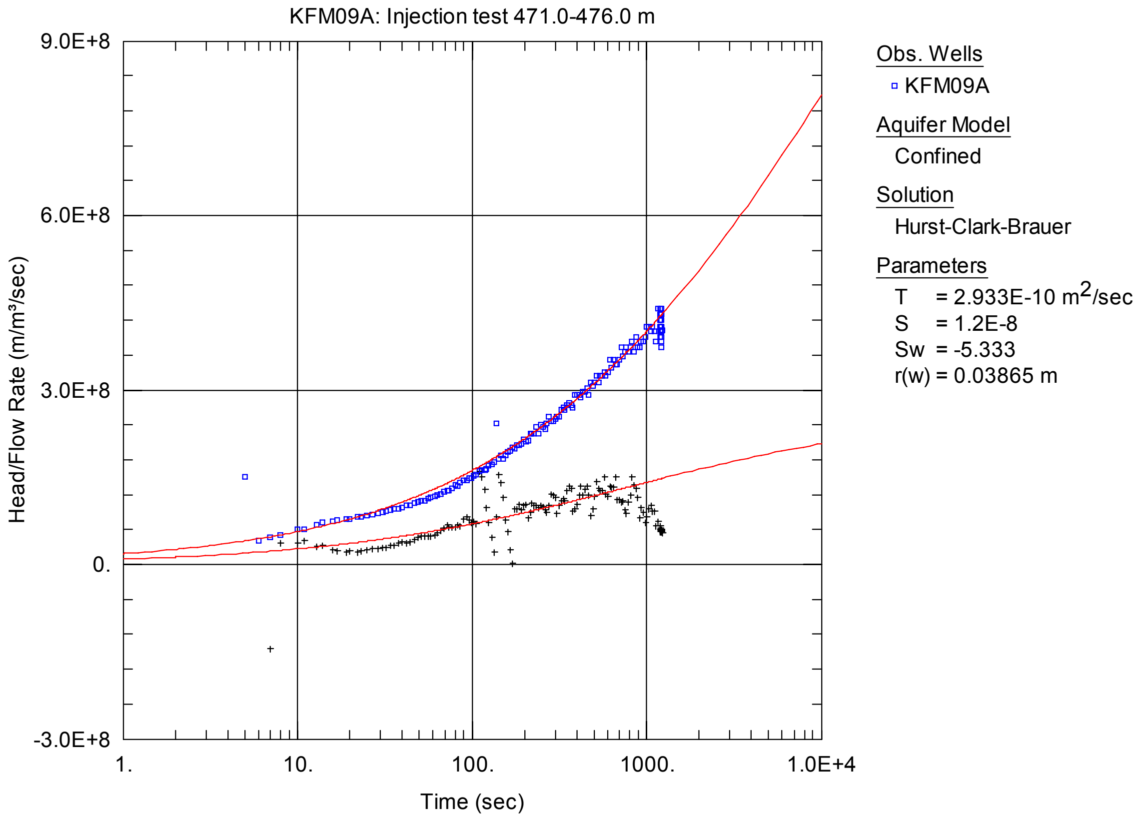


Figure A3-456. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 471.0-476.0 m in KFM09A.*

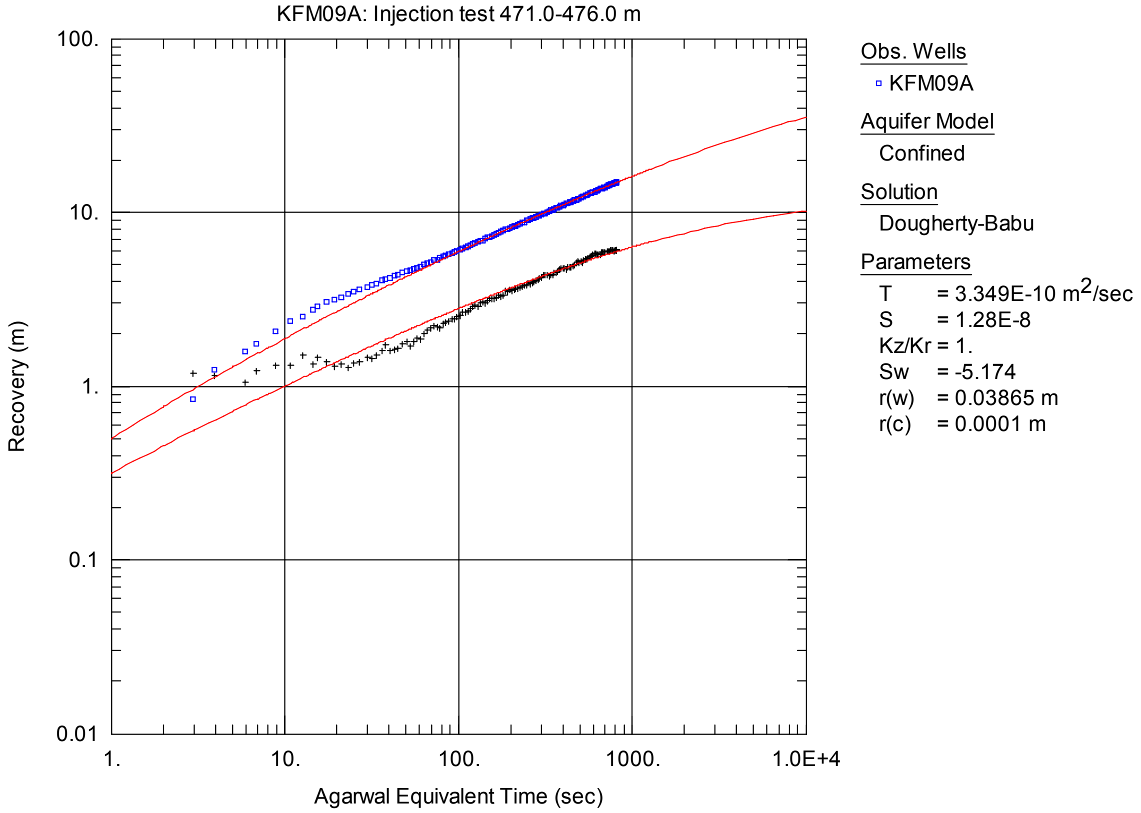


Figure A3-457. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 471.0-476.0 m in KFM09A.*

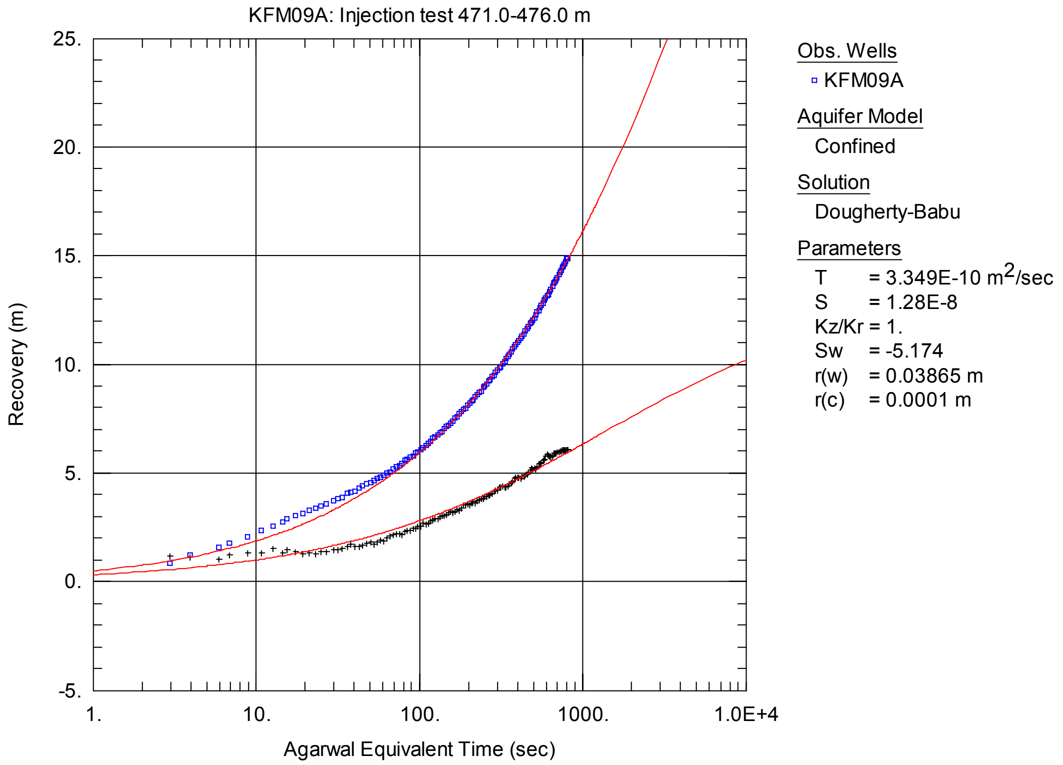


Figure A3-458. Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 471.0-476.0 m in KFM09A.

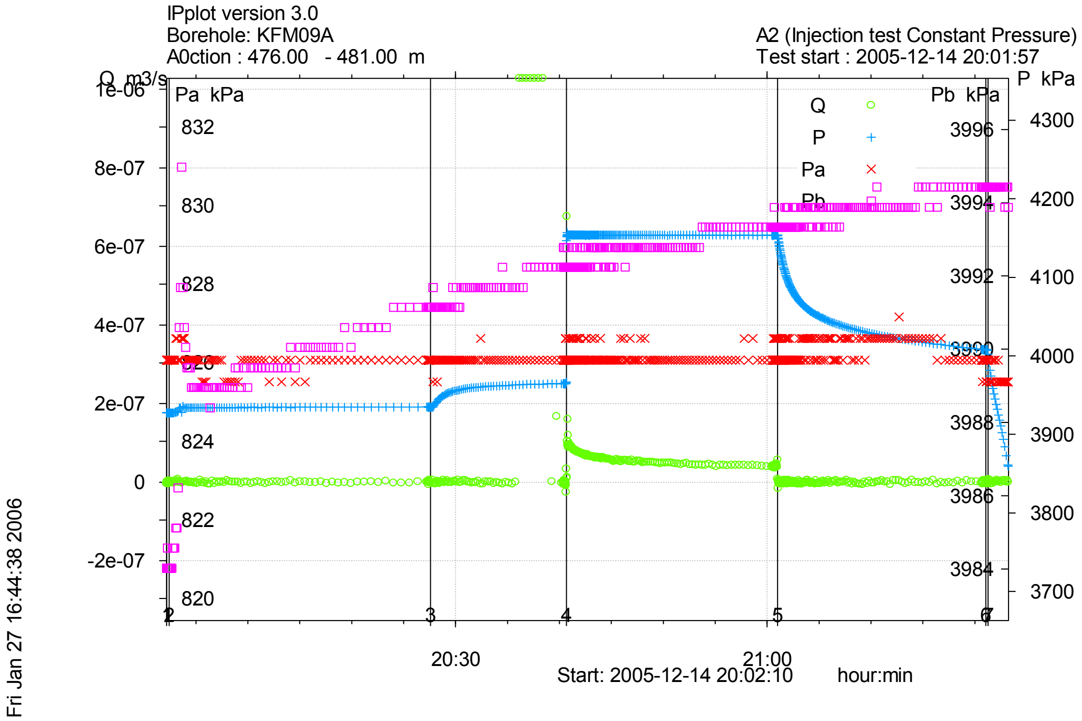


Figure A3-459. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 476.0-481.0 m in borehole KFM09A.

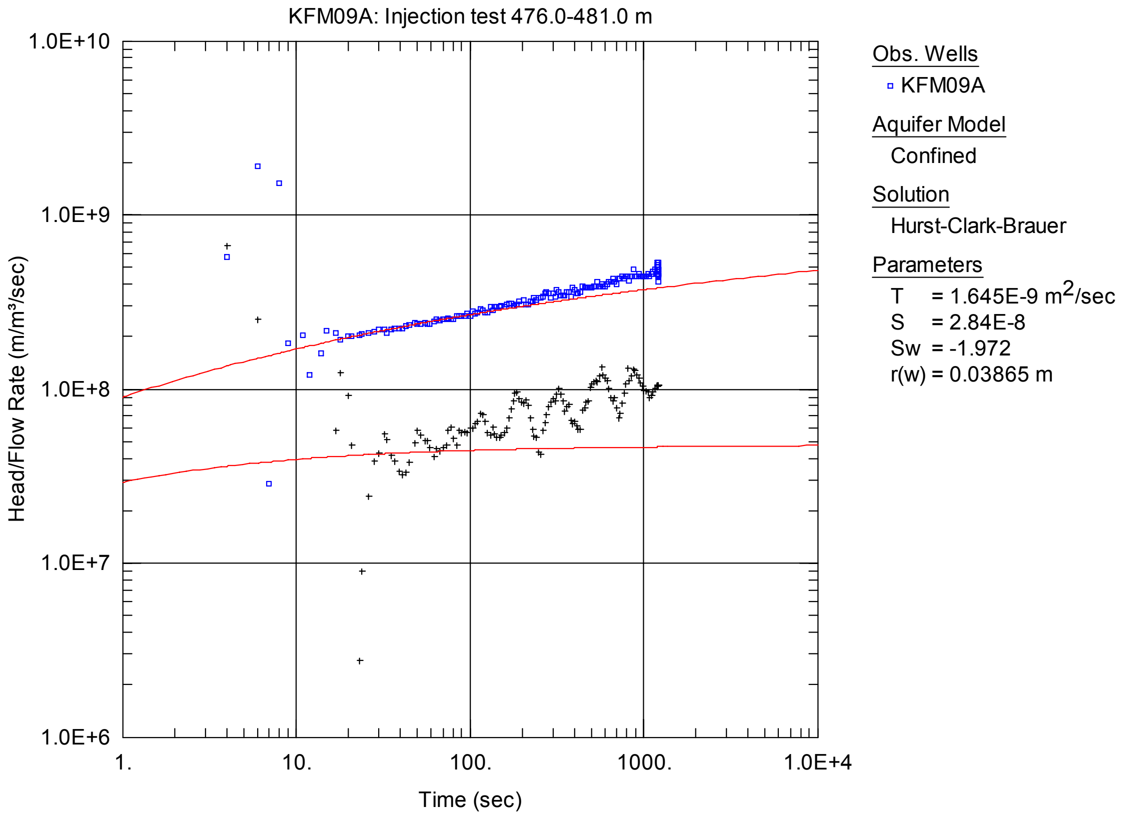


Figure A3-460. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 476.0-481.0 m in KFM09A.*

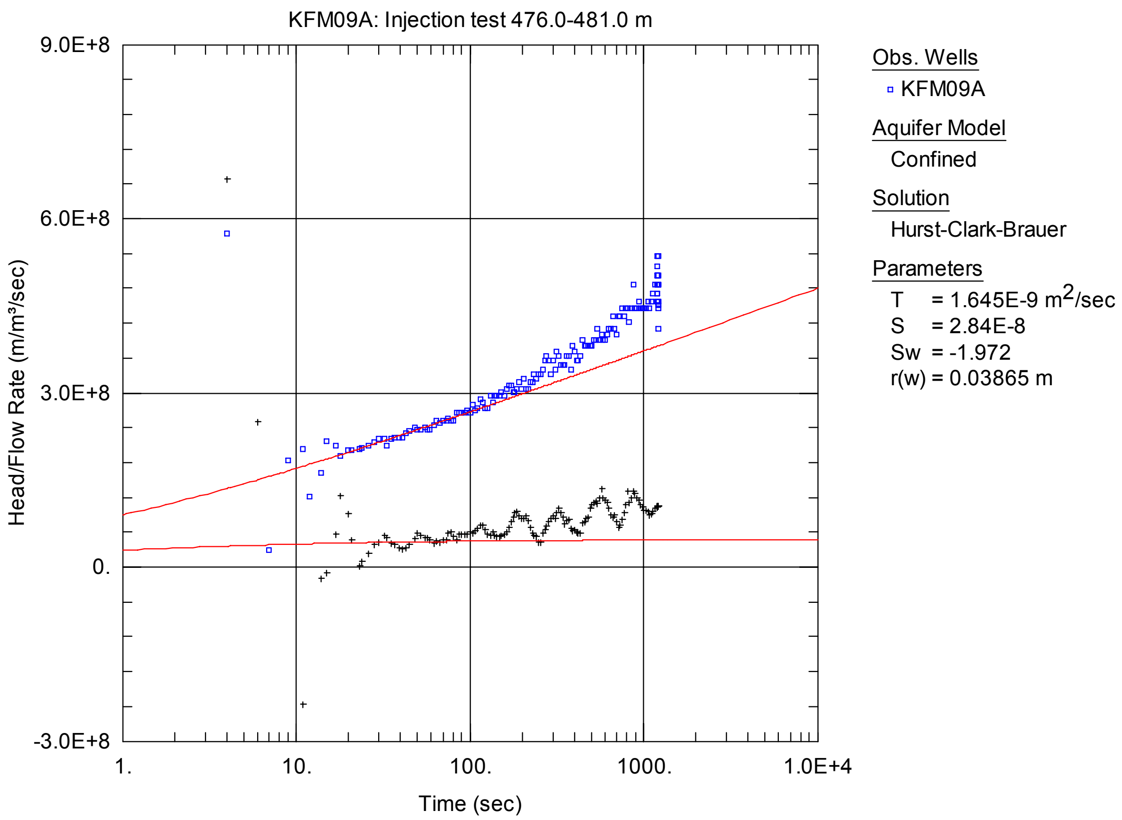


Figure A3-461. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 476.0-481.0 m in KFM09A.*

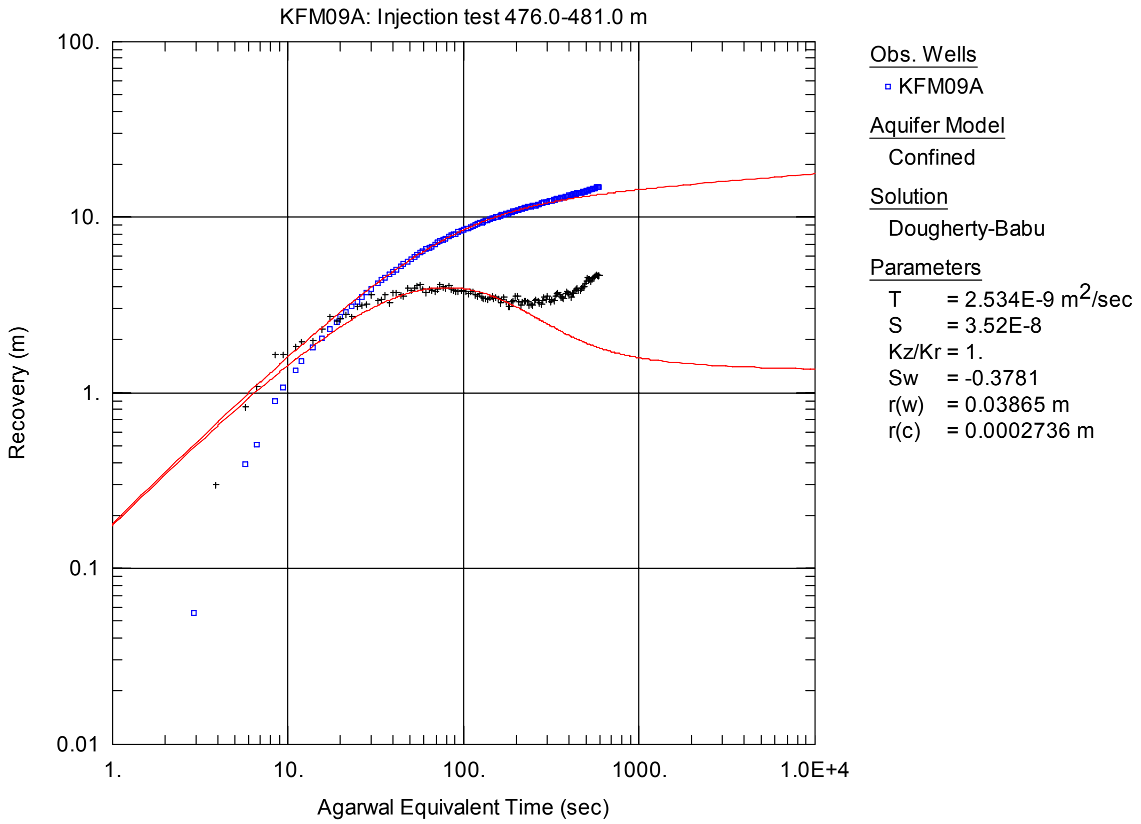


***Figure A3-462.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 476.0-481.0 m in KFM09A.*

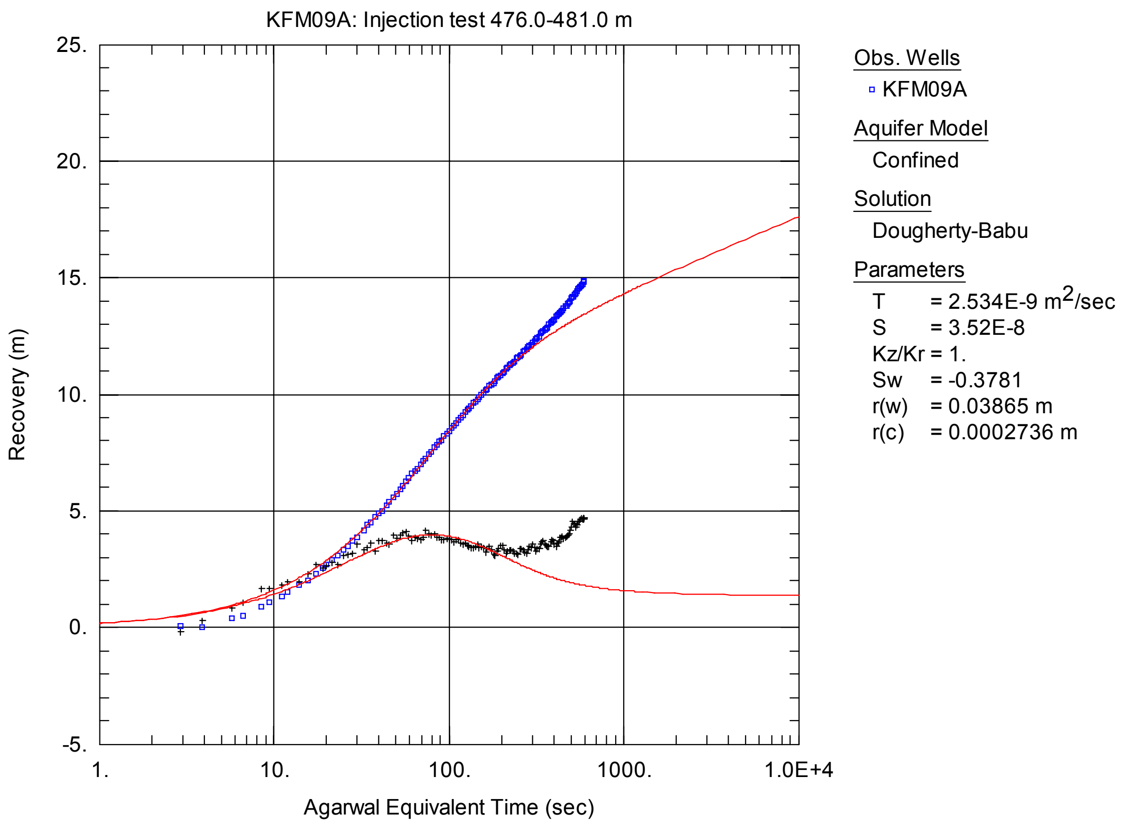


***Figure A3-463.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 476.0-481.0 m in KFM09A.*

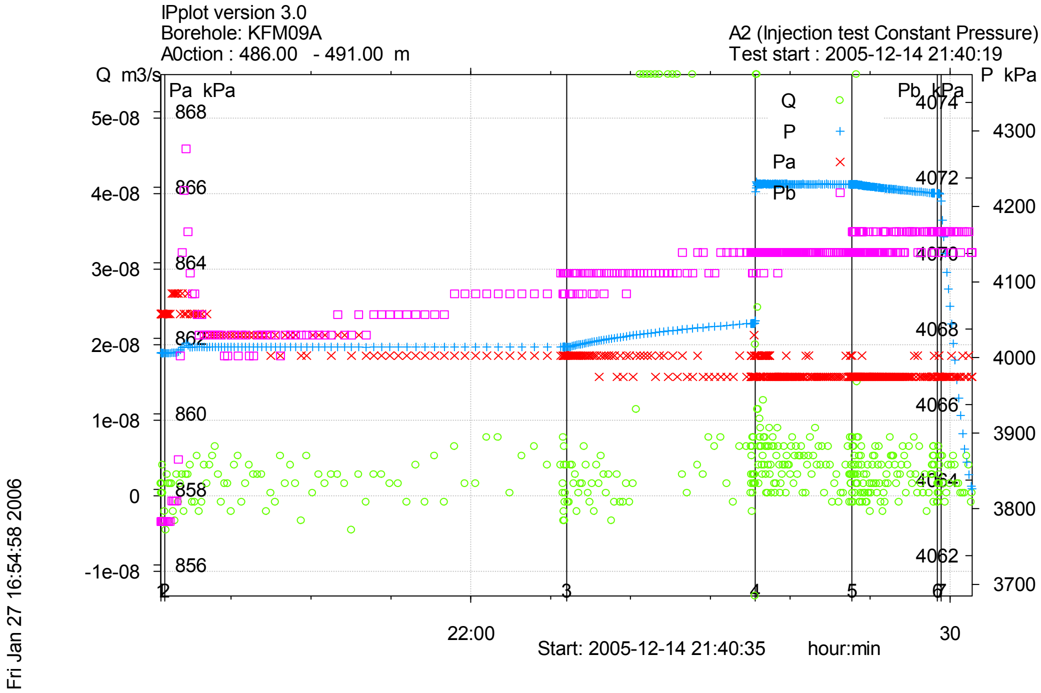


Figure A3-464. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 486.0-491.0 m in borehole KFM09A.*

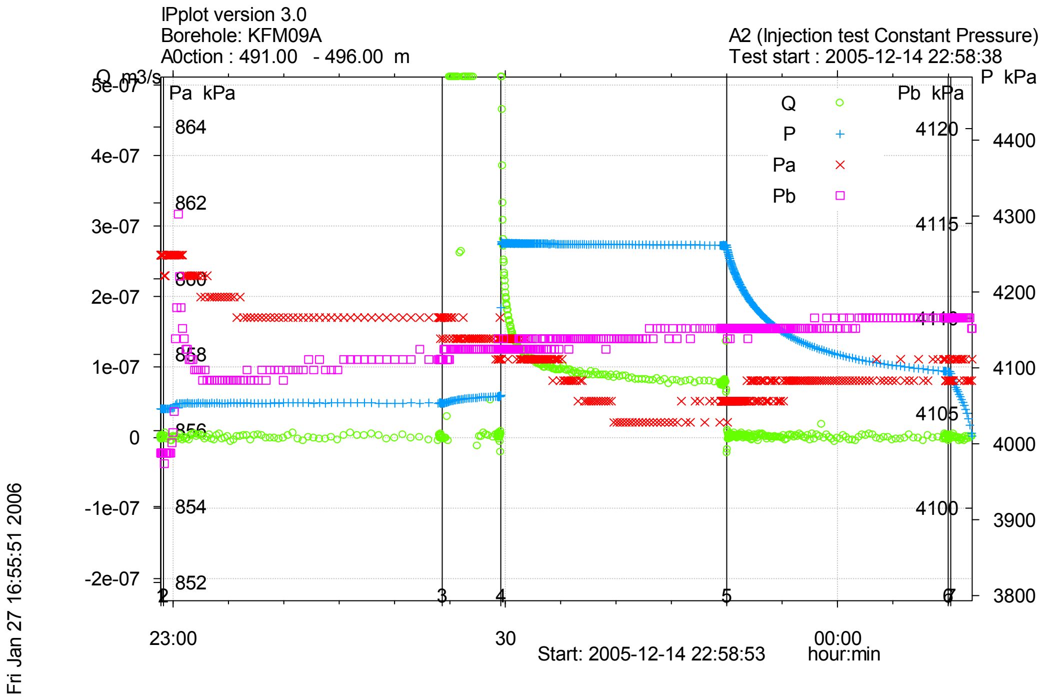


Figure A3-465. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 491.0-496.0 m in borehole KFM09A.*

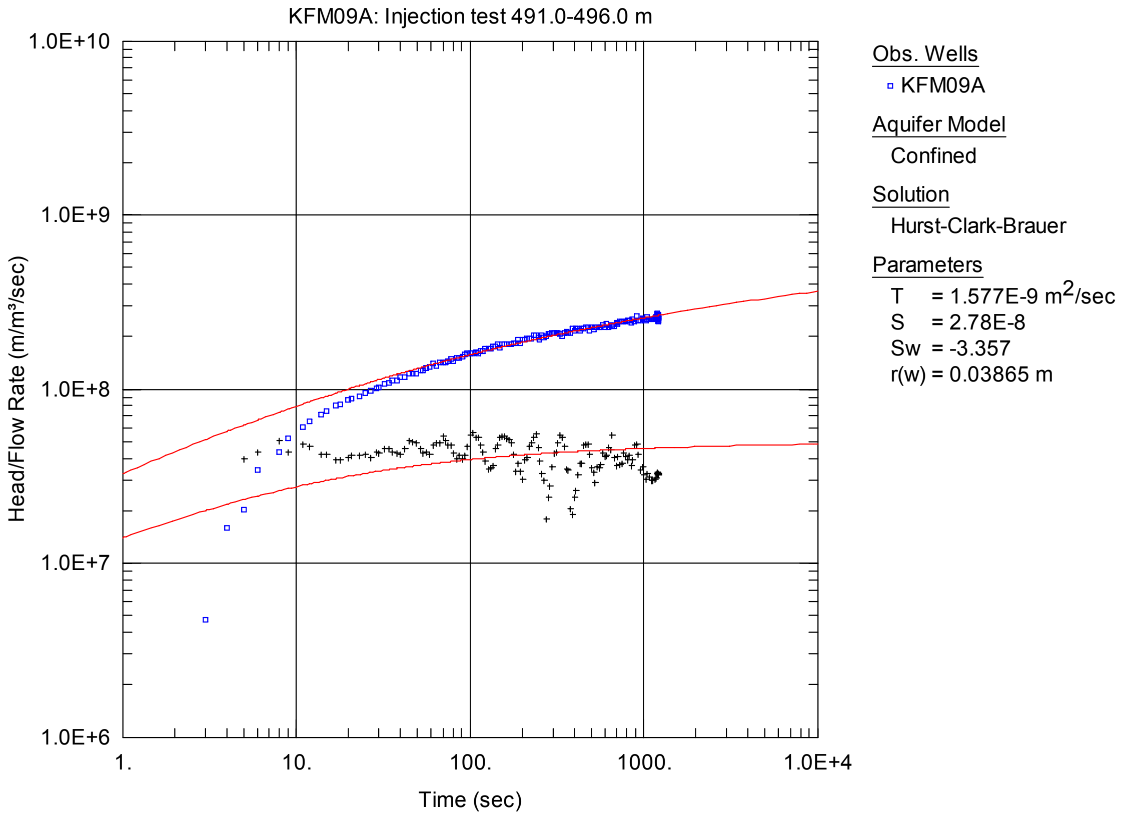


Figure A3-466. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 491.0-496.0 m in KFM09A.*

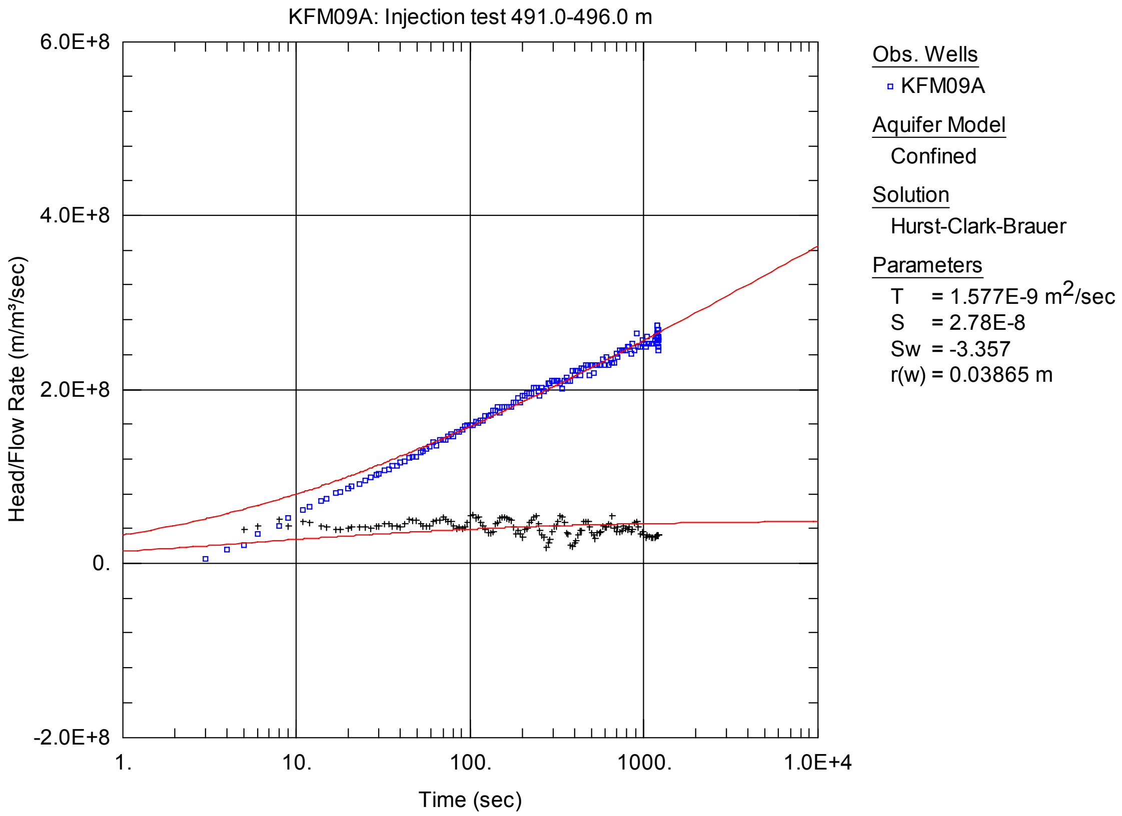


Figure A3-467. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 491.0-496.0 m in KFM09A.*

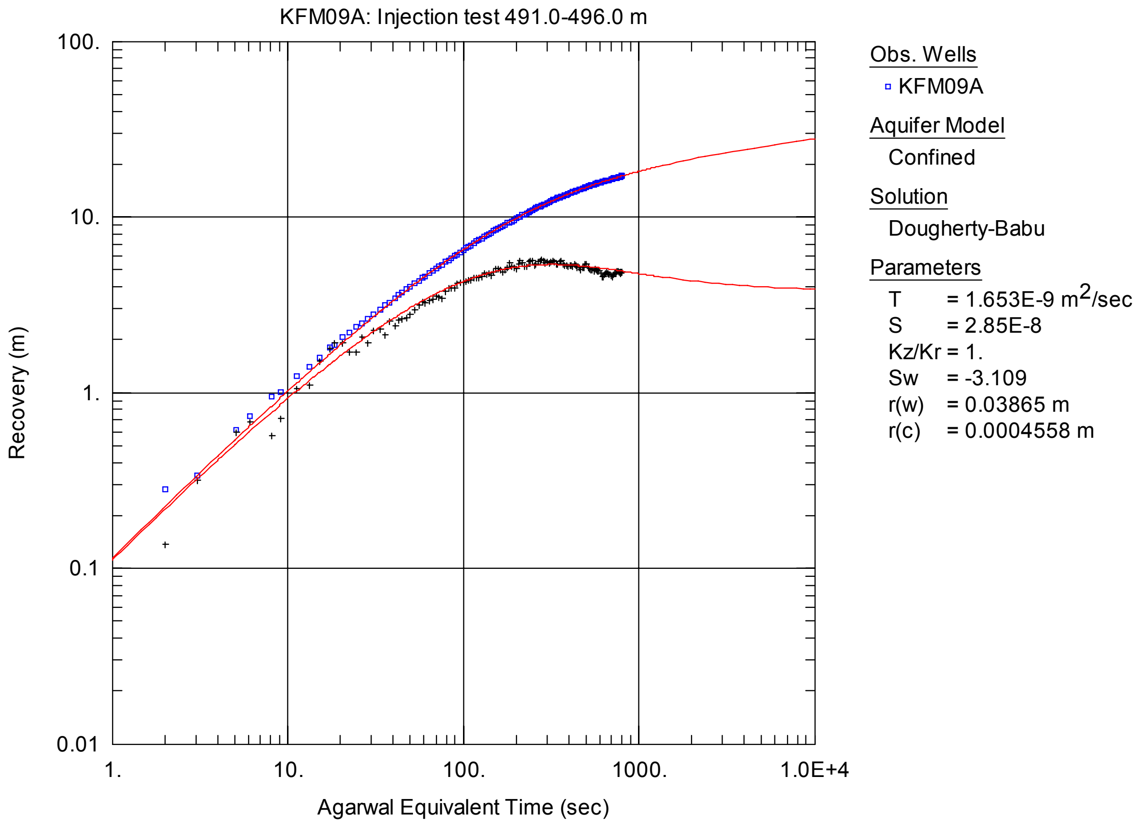


Figure A3-468. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 491.0-496.0 m in KFM09A.*

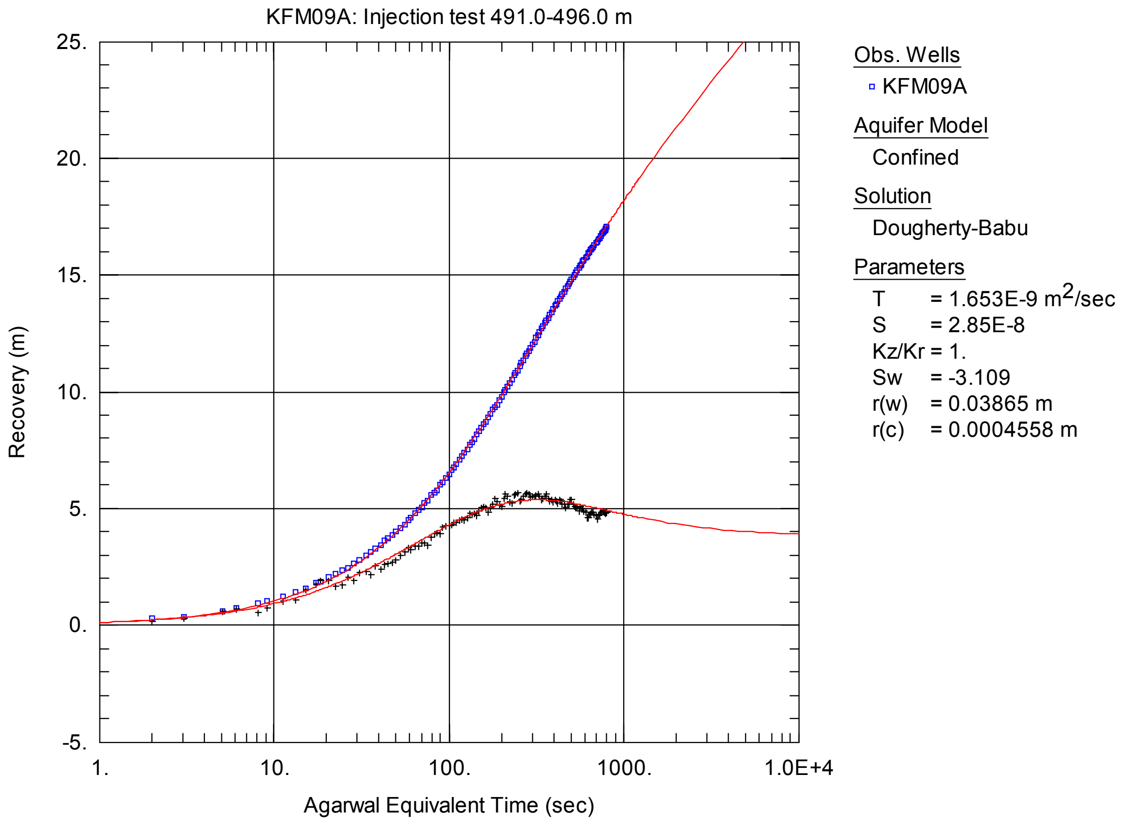


Figure A3-469. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 491.0-496.0 m in KFM09A.*

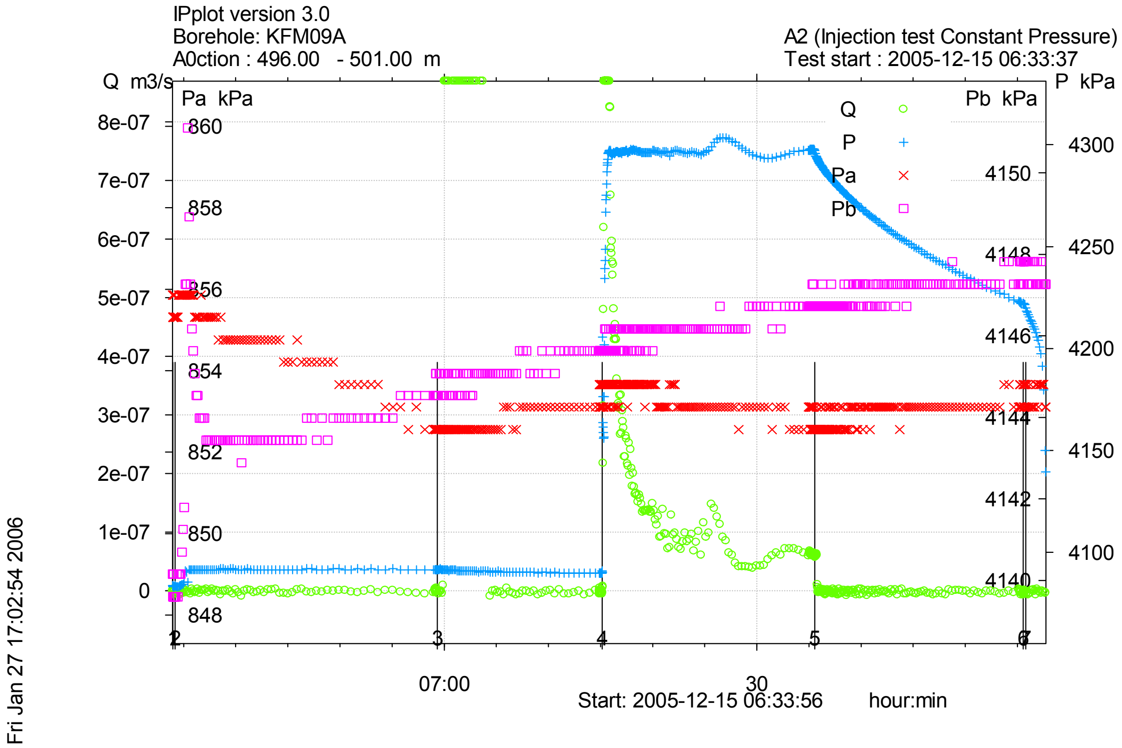


Figure A3-470. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 496.0-501.0 m in borehole KFM09A.*

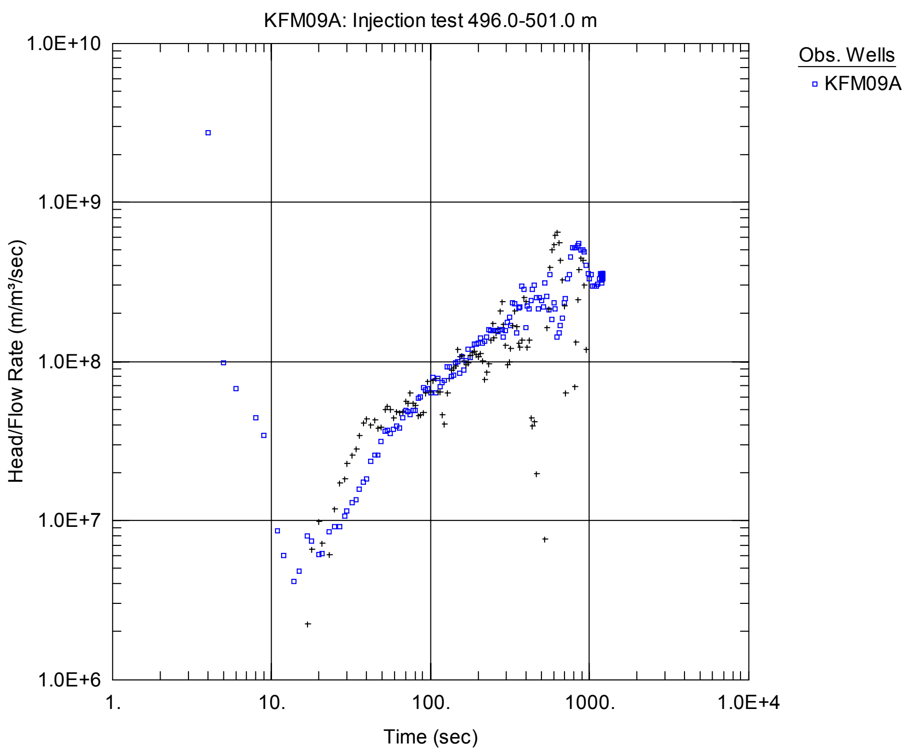


Figure A3-471. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 496.0-501.0 m in KFM09A.*

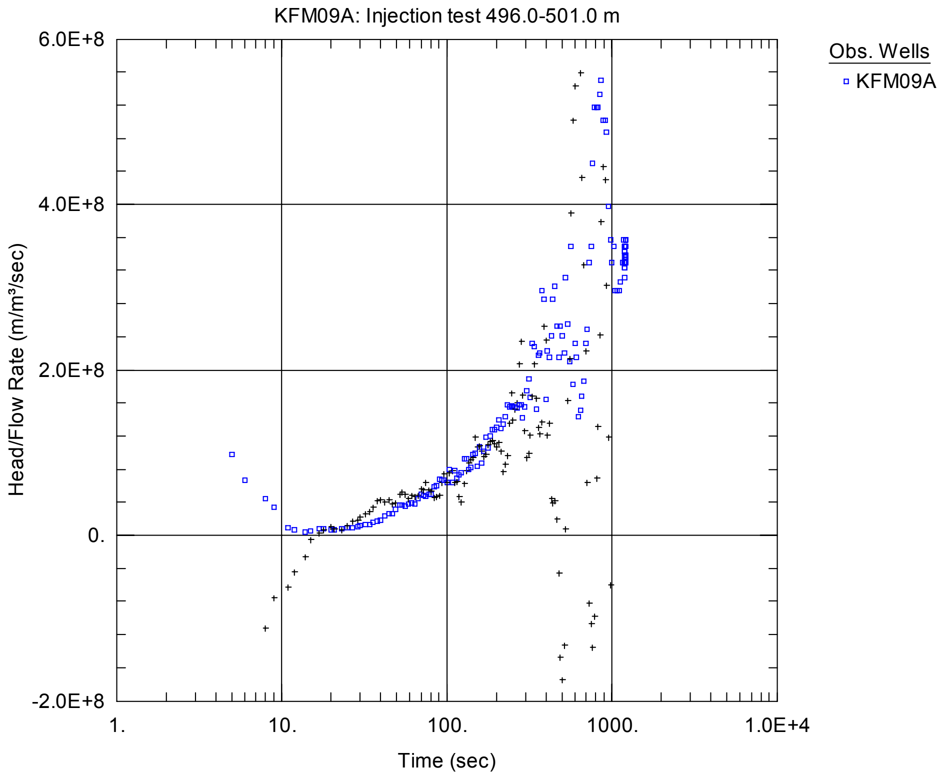


Figure A3-472. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 496.0-501.0 m in KFM09A.*

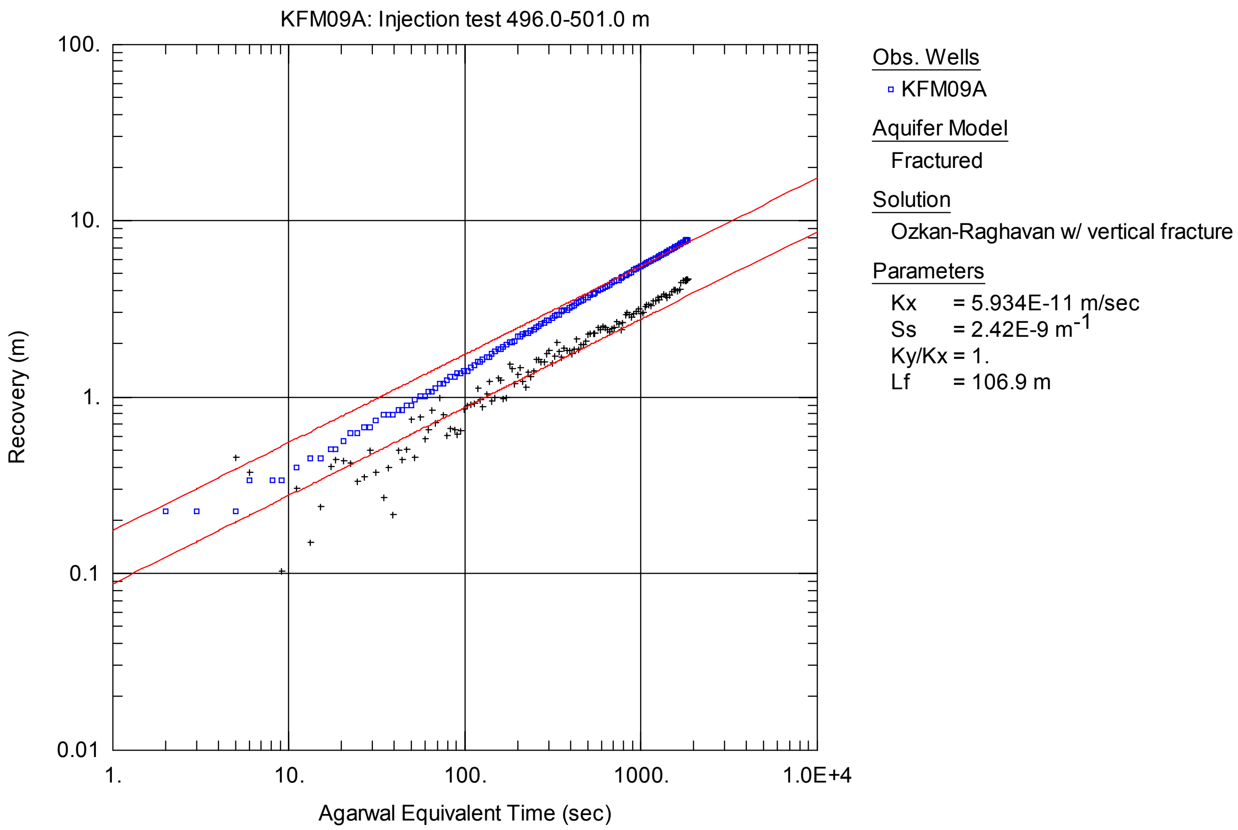


Figure A3-473. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 496.0-501.0 m in KFM09A.*

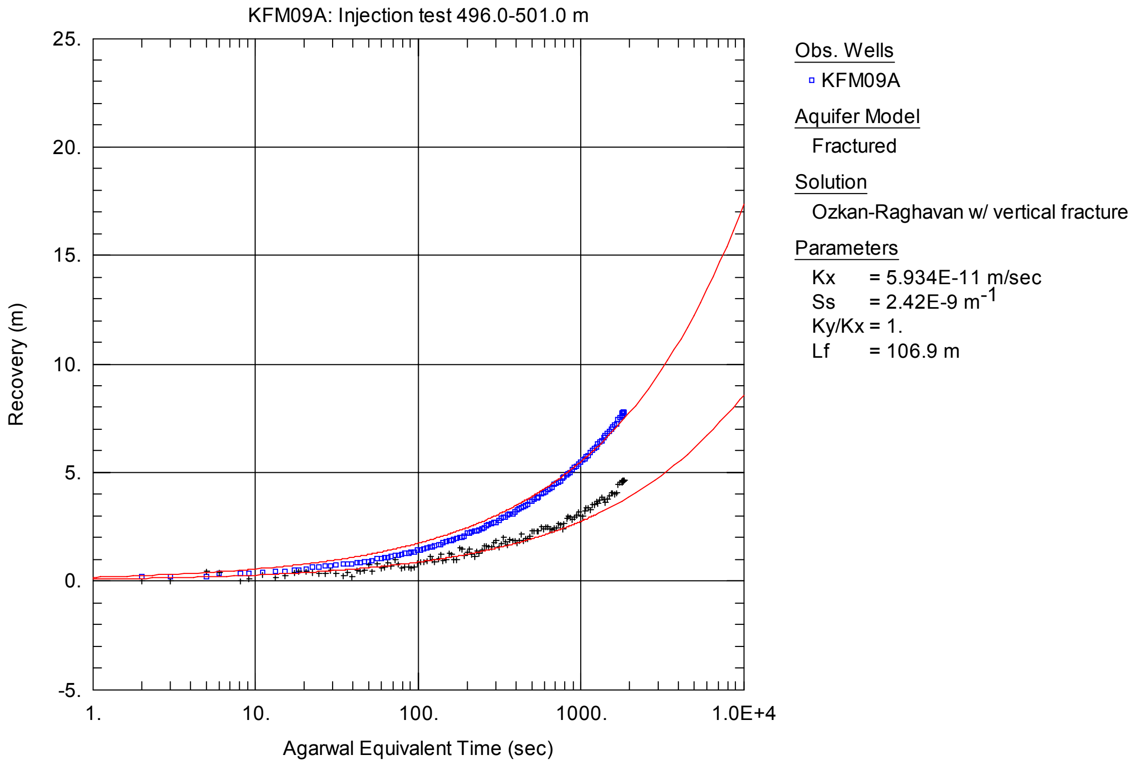


Figure A3-474. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 496.0-501.0 m in KFM09A.*

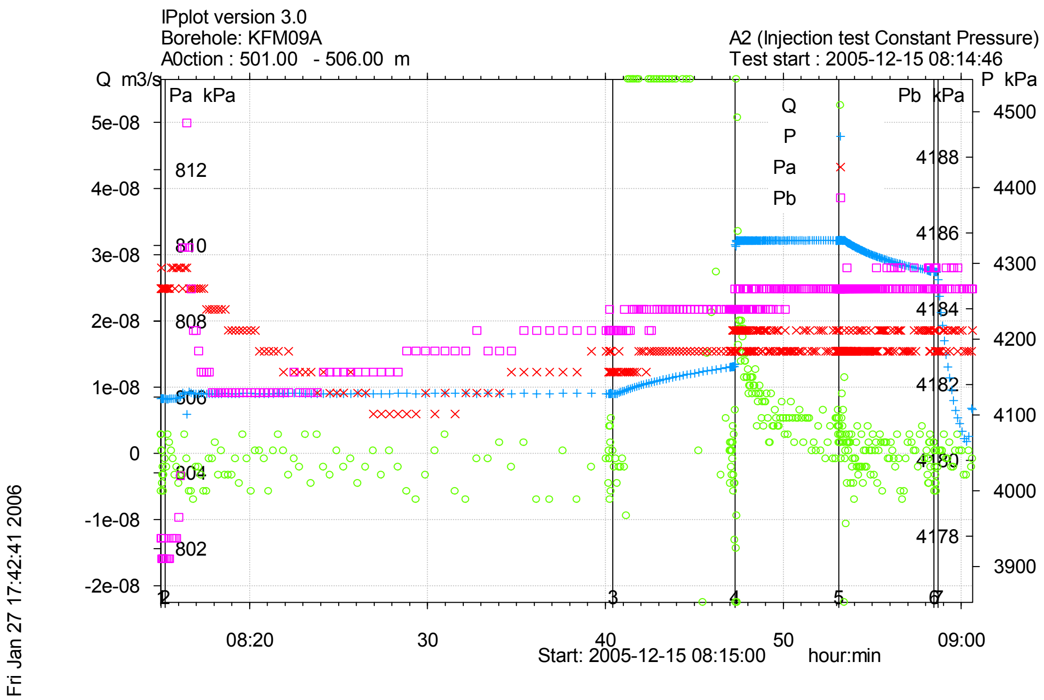


Figure A3-475. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 501.0-506.0 m in borehole KFM09A.*

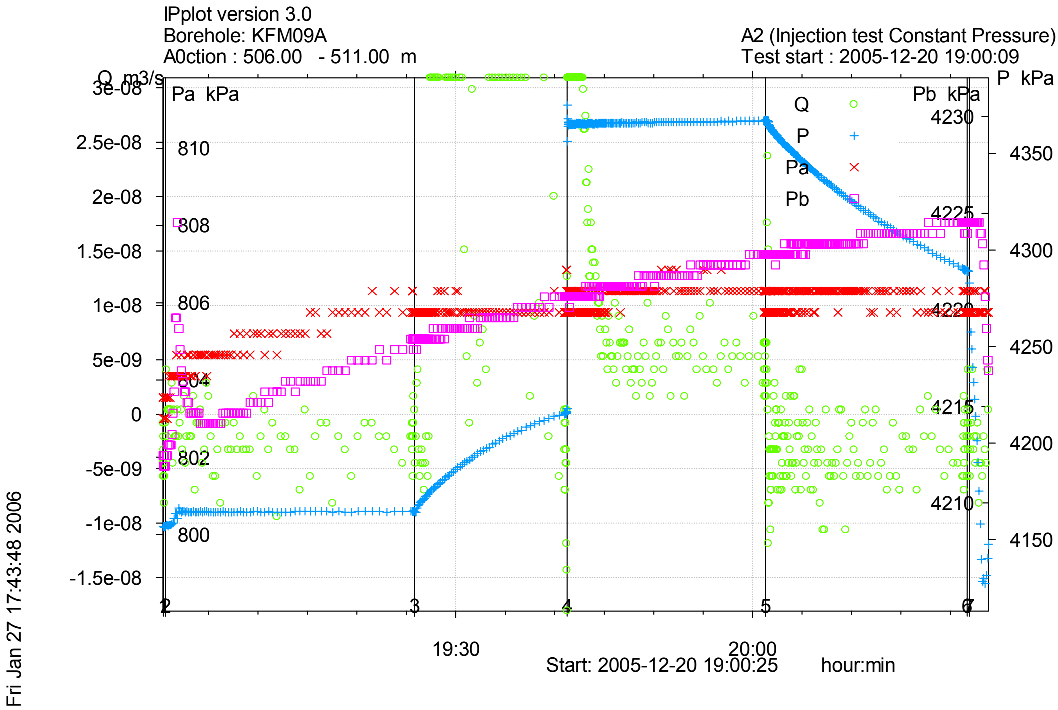


Figure A3-476. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 506.0-511.0 m in borehole KFM09A.*

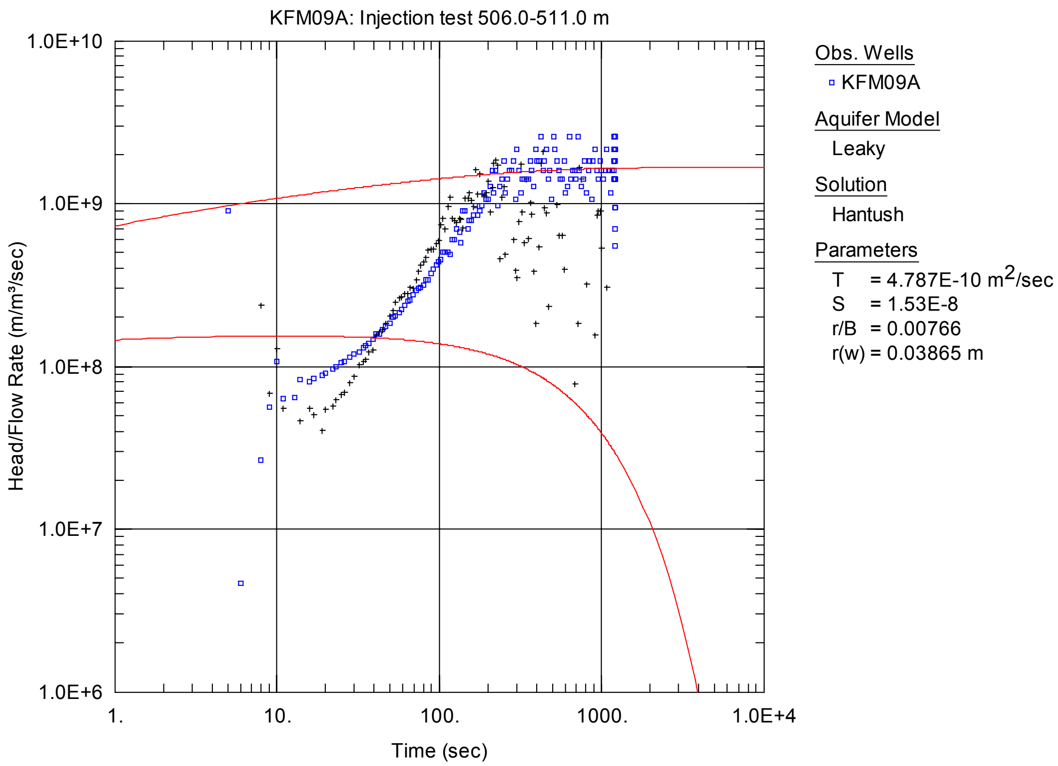


Figure A3-477. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 506.0-511.0 m in KFM09A.*

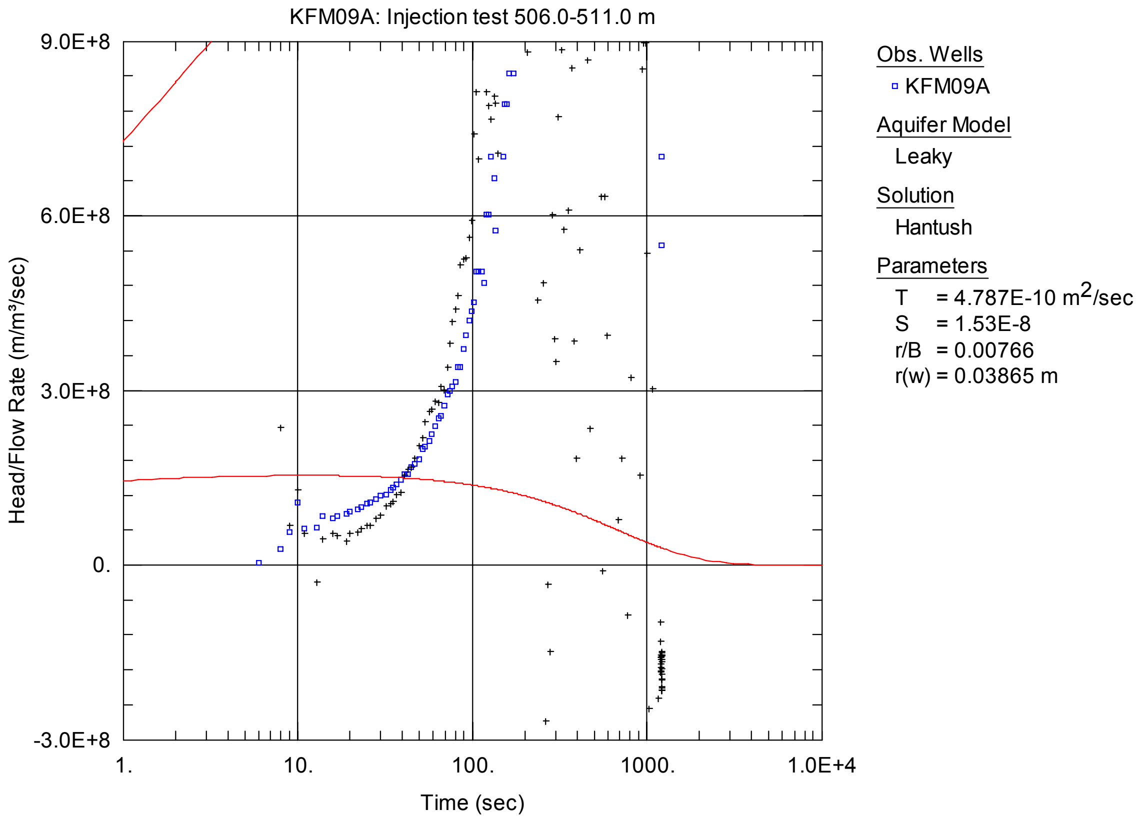


Figure A3-478. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 506.0-511.0 m in KFM09A.*

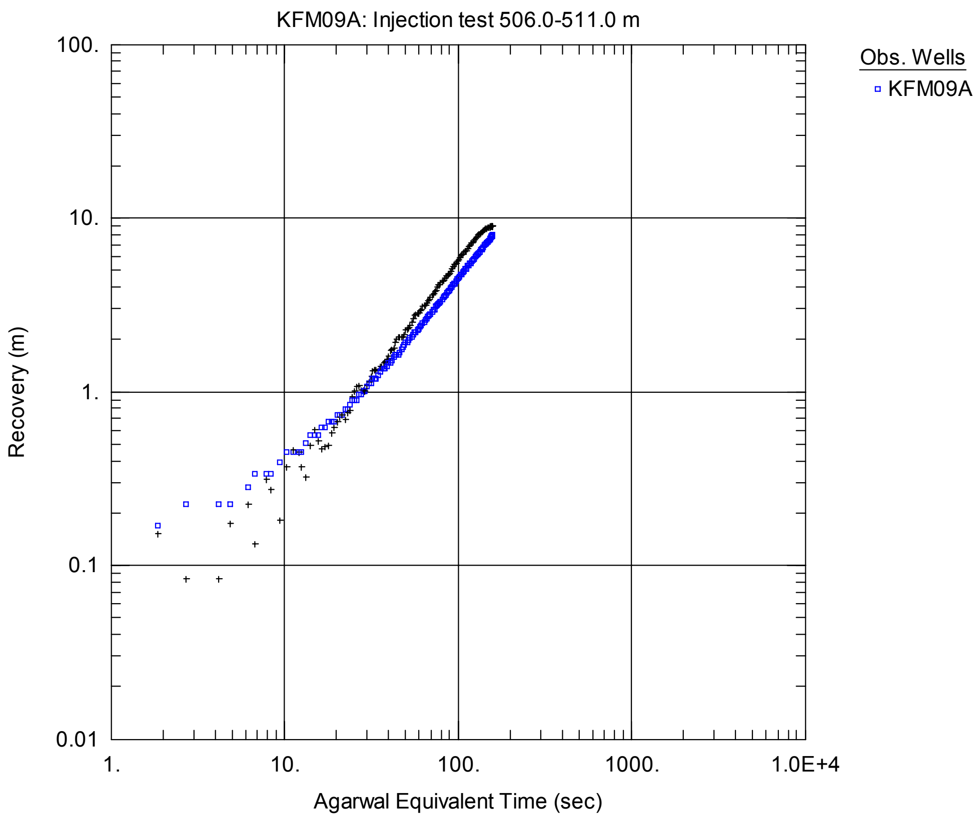


Figure A3-479. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 506.0-511.0 m in KFM09A.*

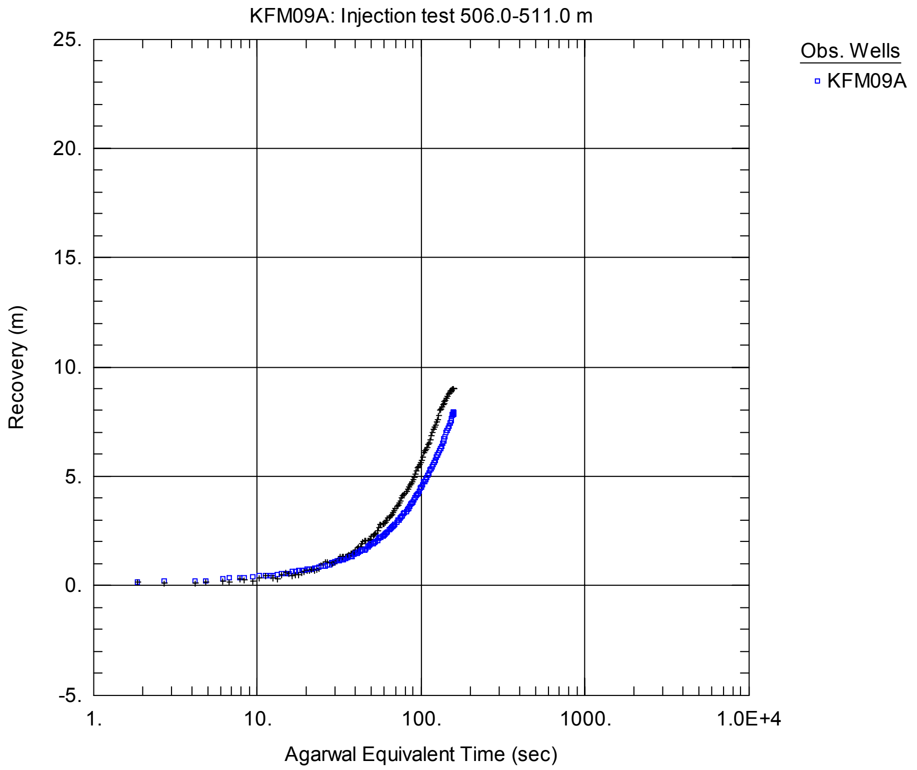


***Figure A3-480.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 506.0-511.0 m in KFM09A.*

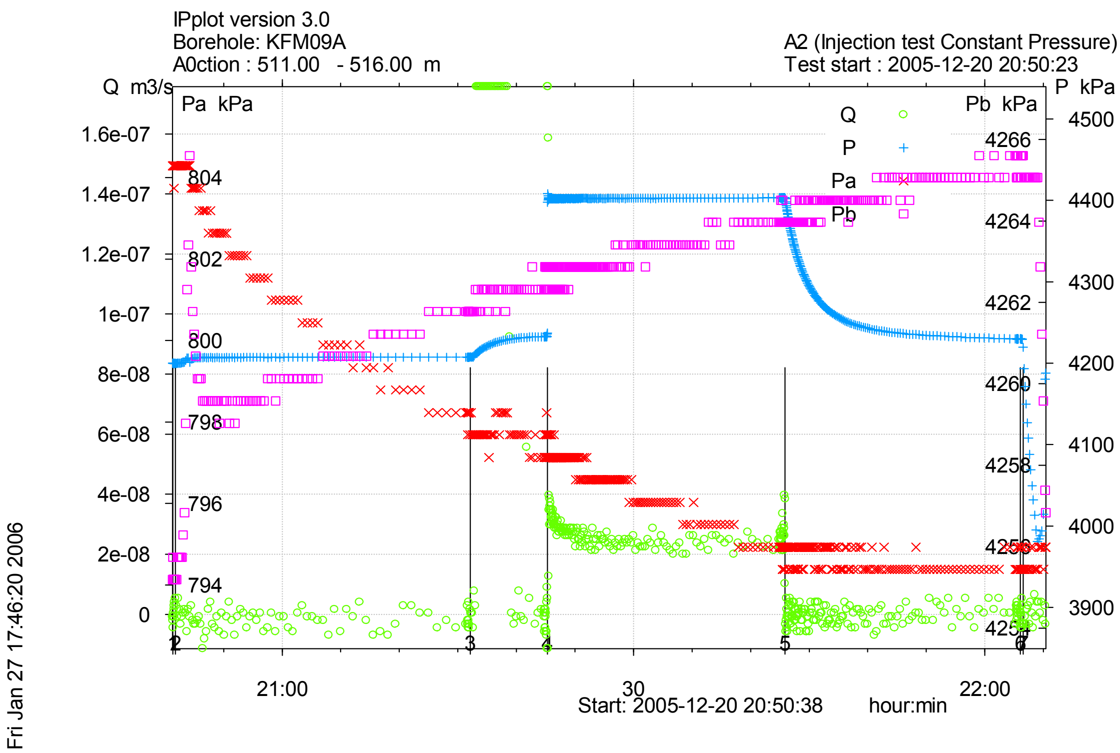


***Figure A3-481.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 511.0-516.0 m in borehole KFM09A.*

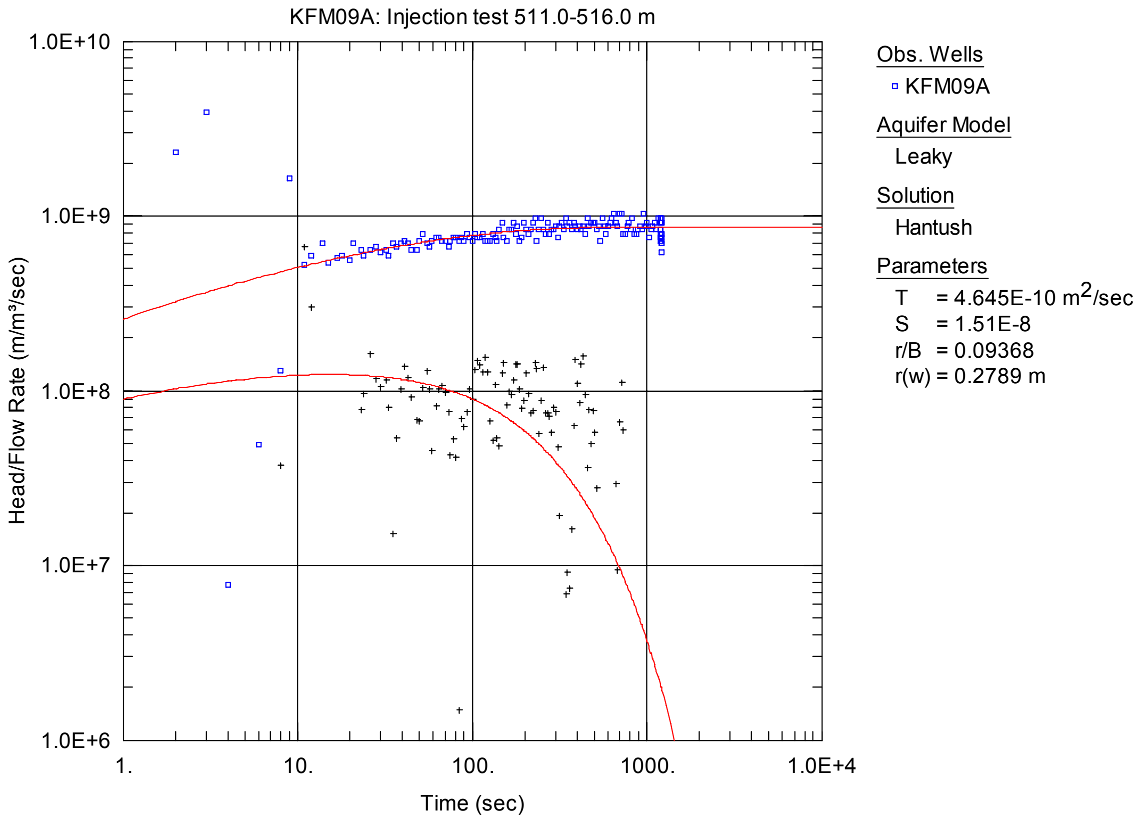


Figure A3-482. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 511.0-516.0 m in KFM09A.*

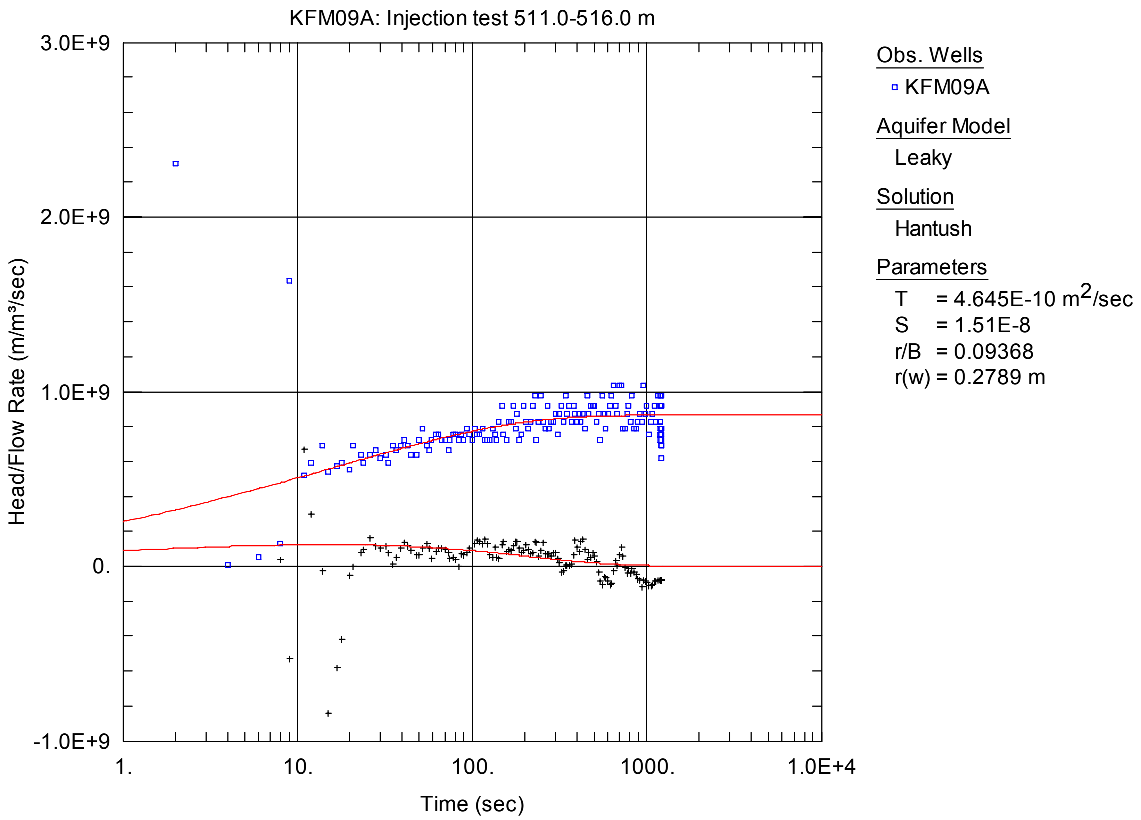


Figure A3-483. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 511.0-516.0 m in KFM09A.*

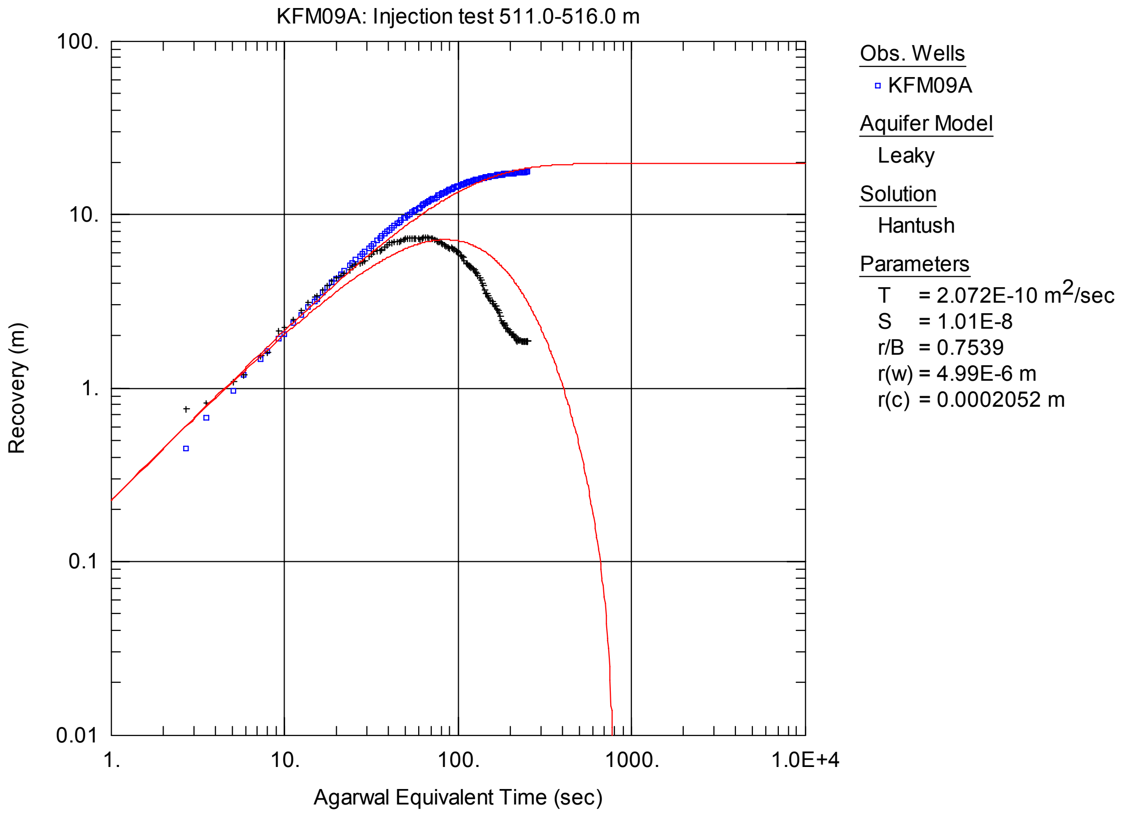


Figure A3-484. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 511.0-516.0 m in KFM09A.*

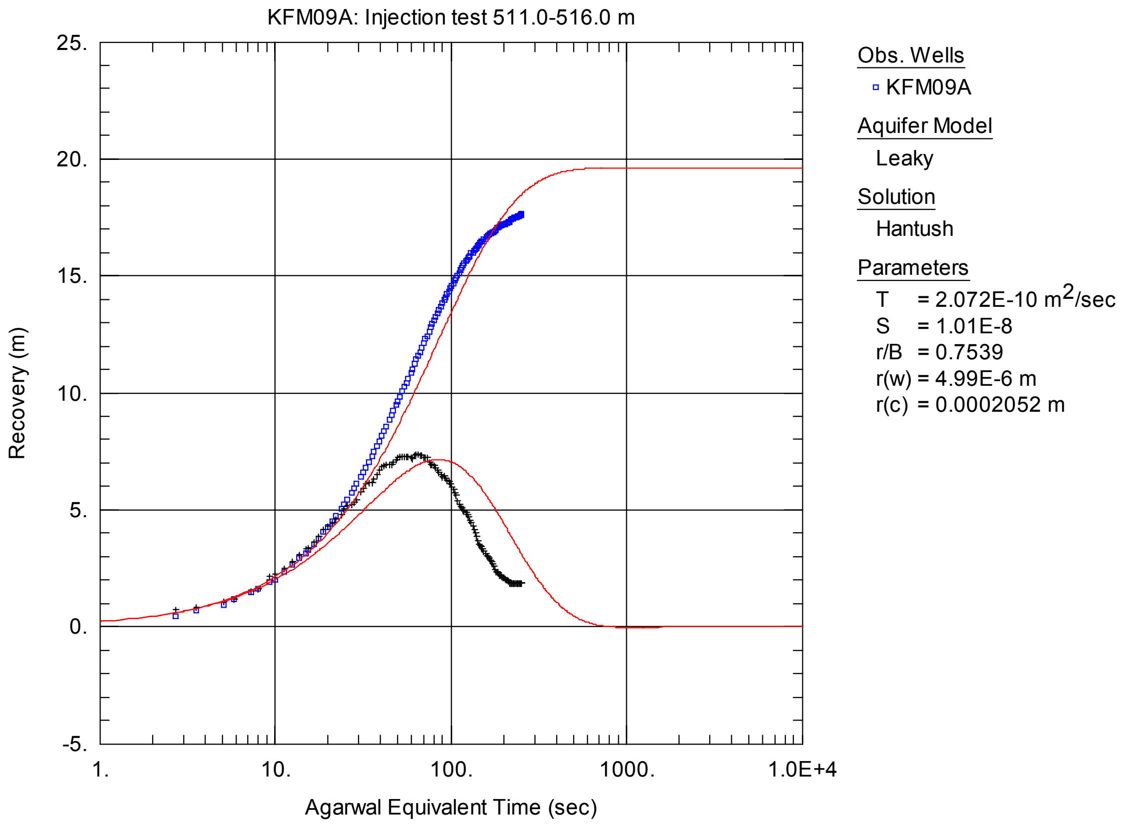


Figure A3-485. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 511.0-516.0 m in KFM09A.*

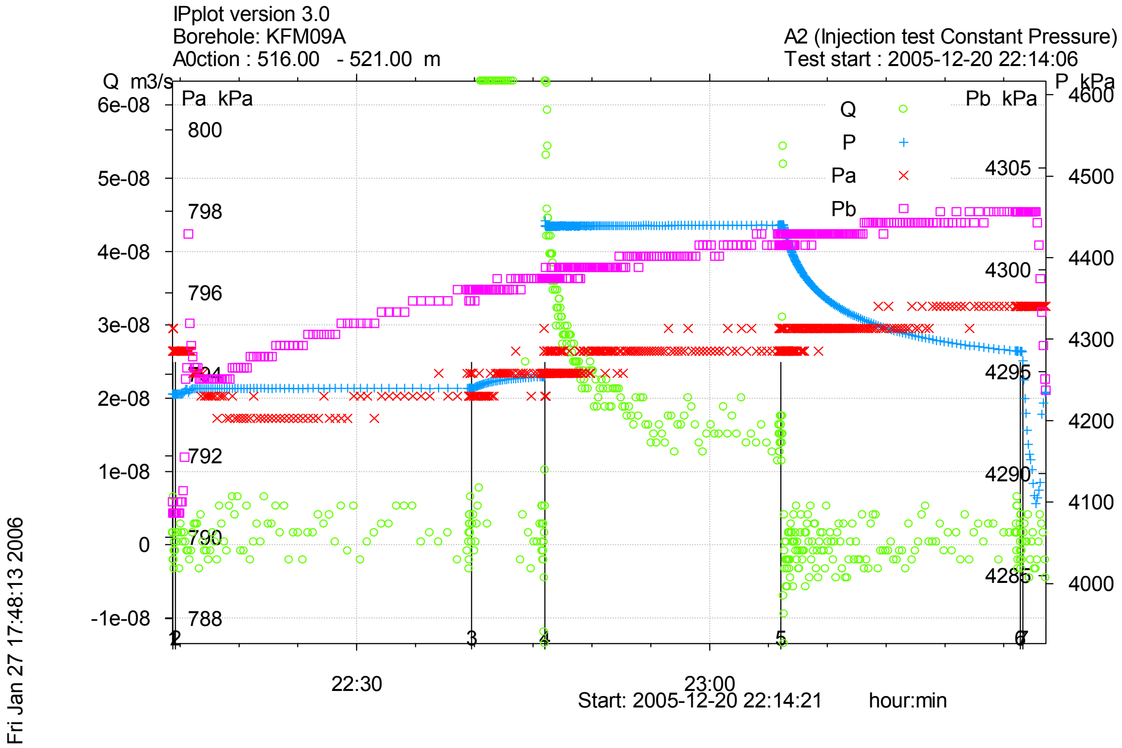


Figure A3-486. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 516.0-521.0 m in borehole KFM09A.*

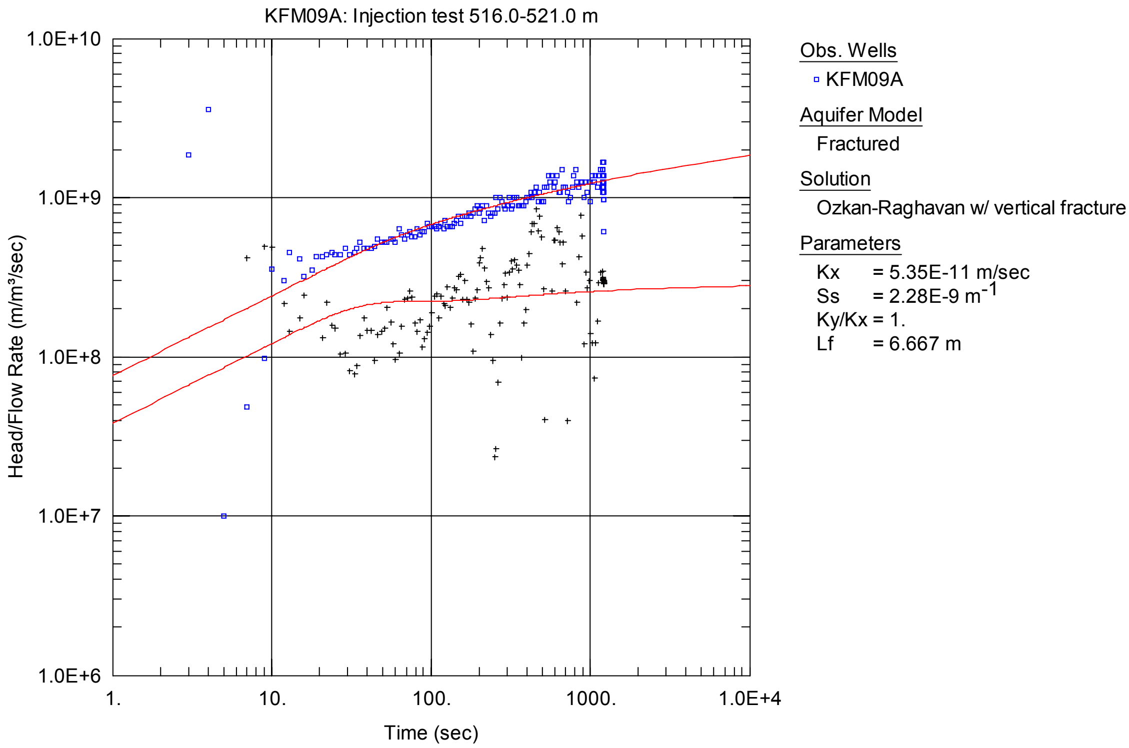


Figure A3-487. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 516.0-521.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

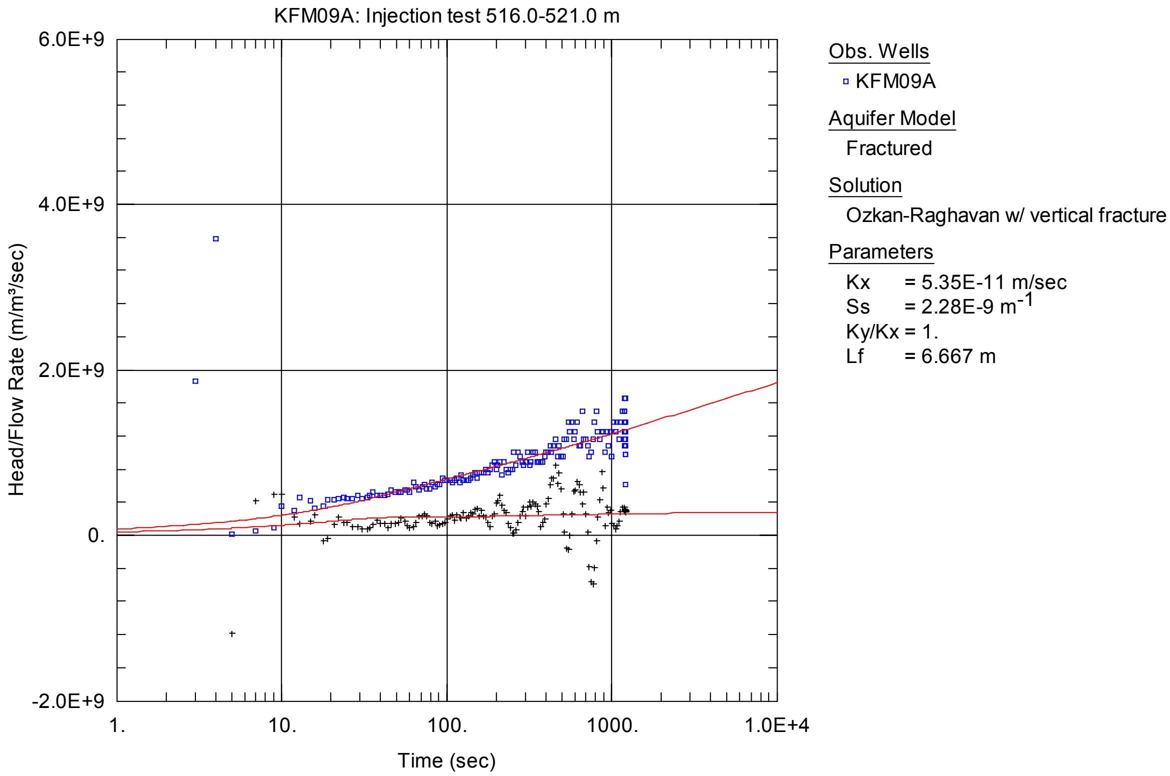


Figure A3-488. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 516.0-521.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

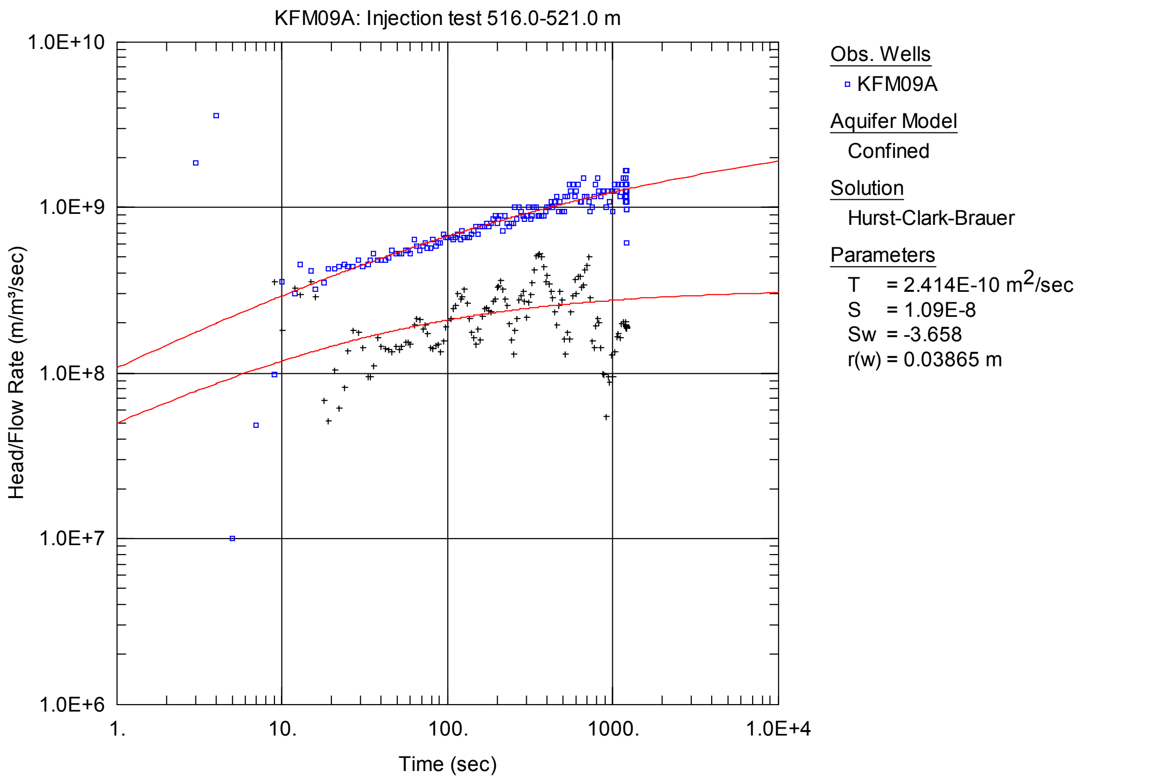


Figure A3-489. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 516.0-521.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for a pseudo-radial response.*

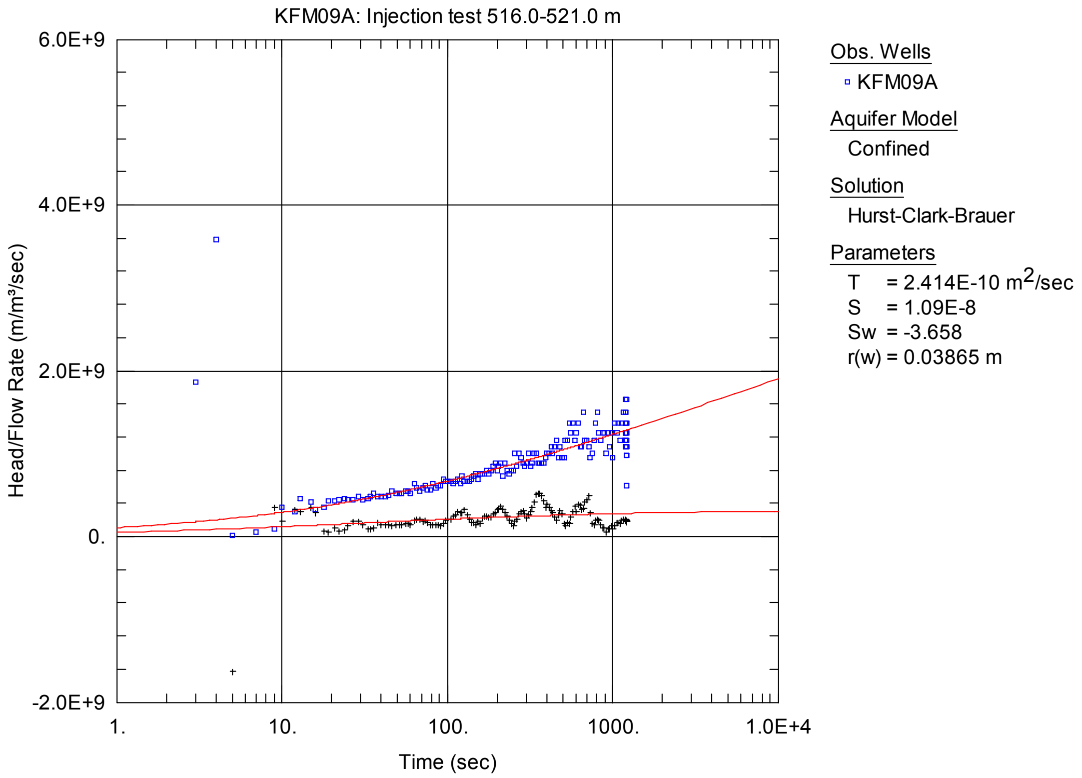


Figure A3-490. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 516.0-521.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for a pseudo-radial response.*

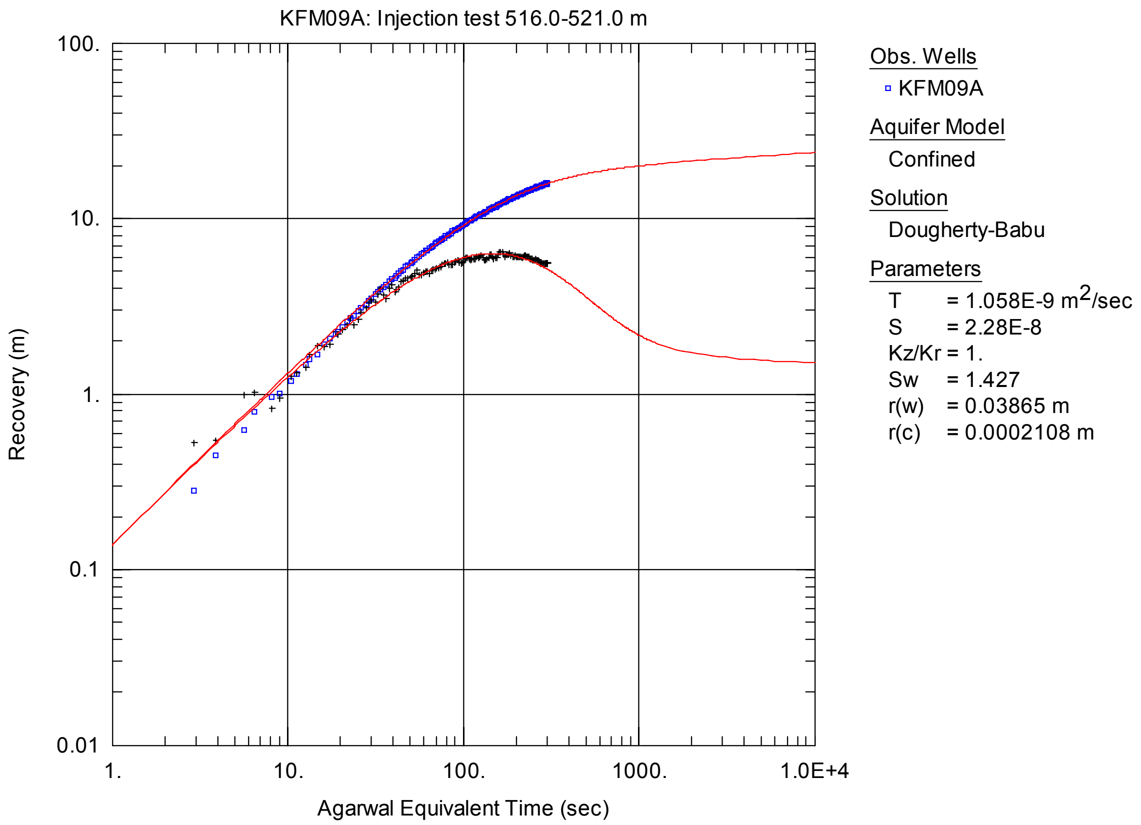


Figure A3-491. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 516.0-521.0 m in KFM09A.*

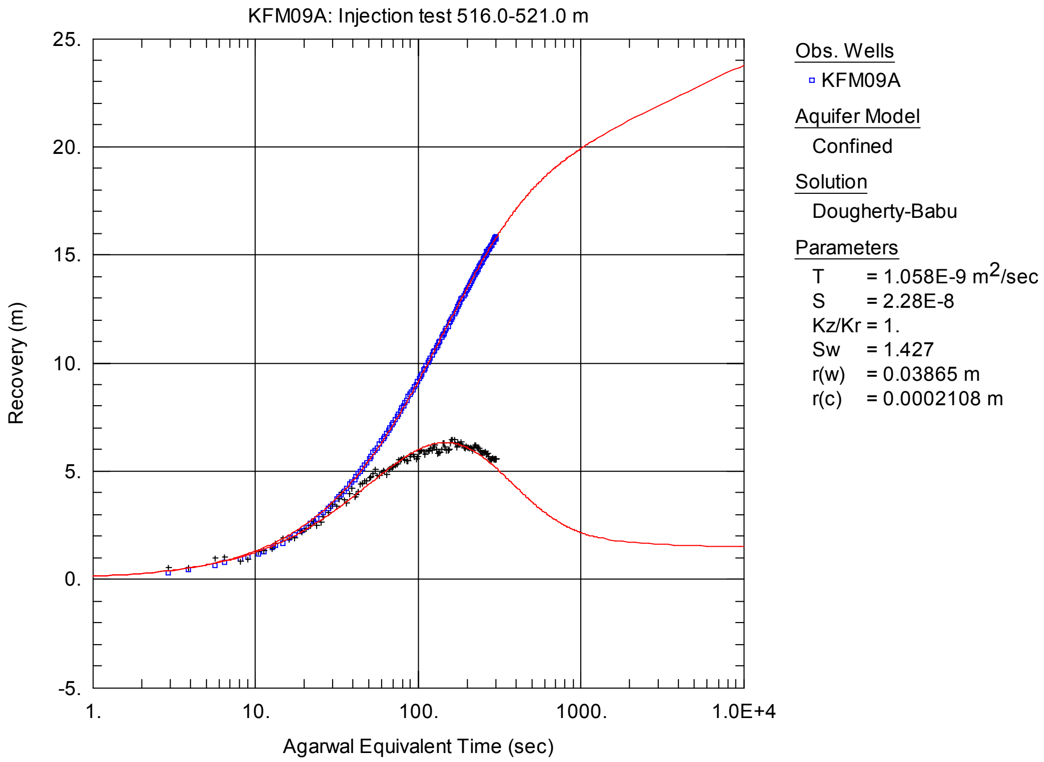


Figure A3-492. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 516.0-521.0 m in KFM09A.*

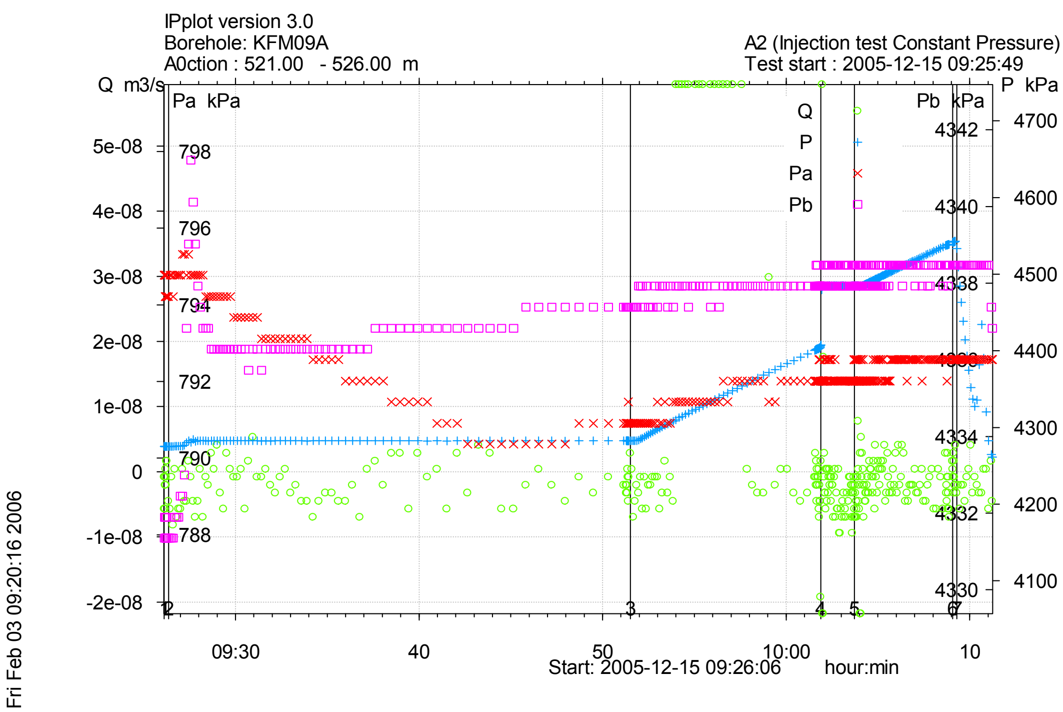


Figure A3-493. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 521.0-526.0 m in borehole KFM09A.*

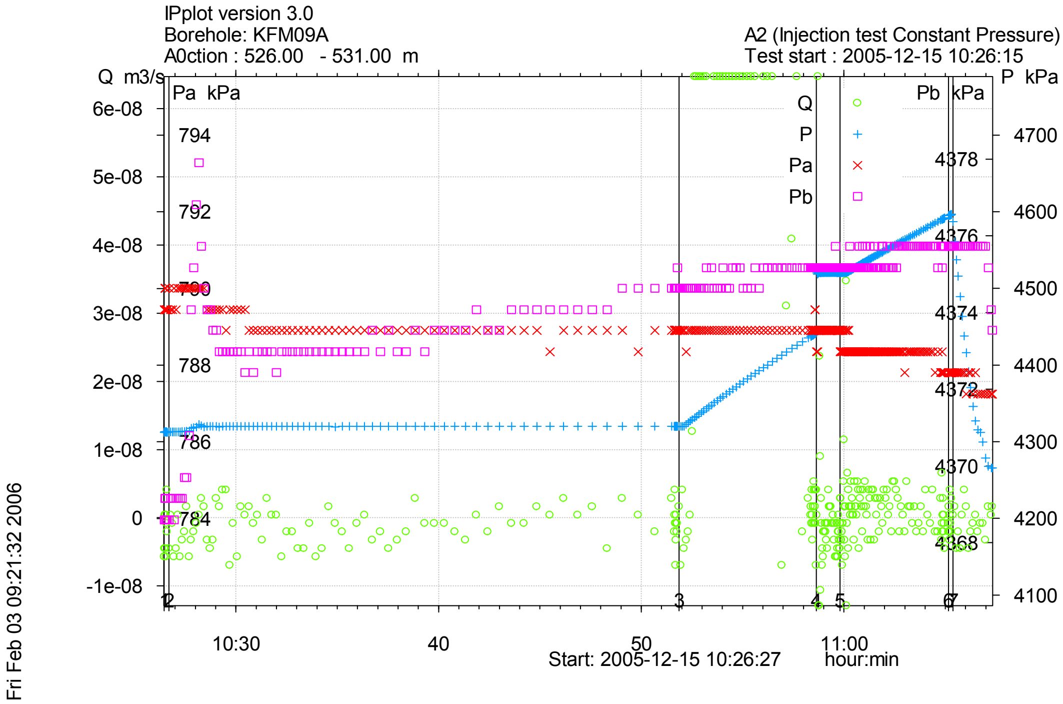


Figure A3-494. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 526.0-531.0 m in borehole KFM09A.*

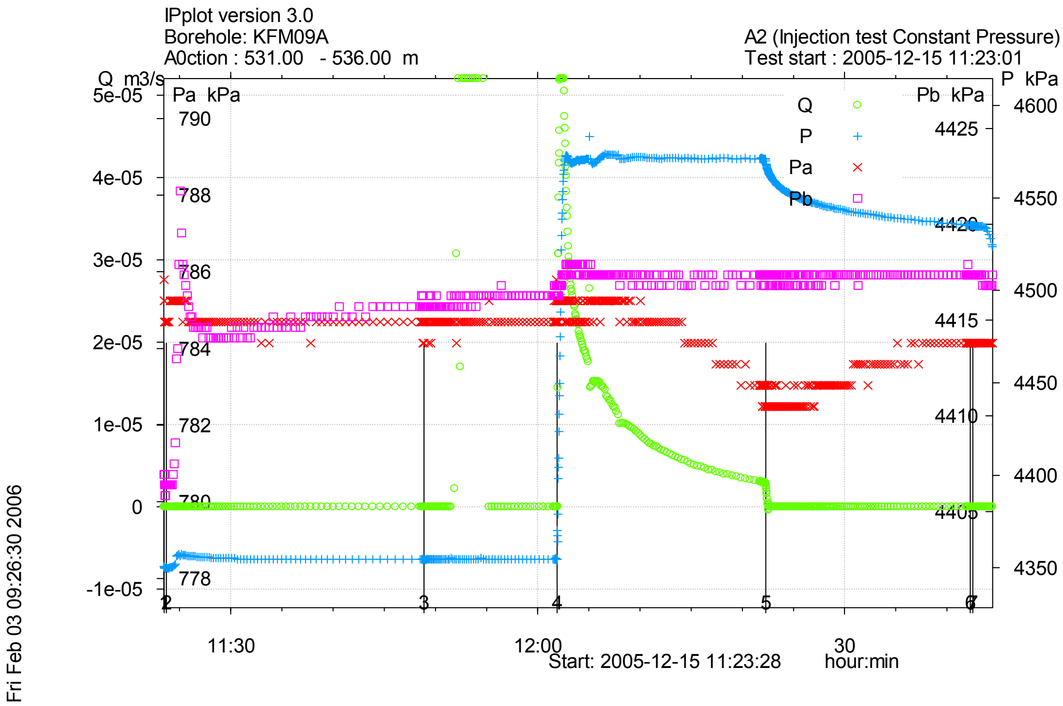


Figure A3-495. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 531.0-536.0 m in borehole KFM09A.*

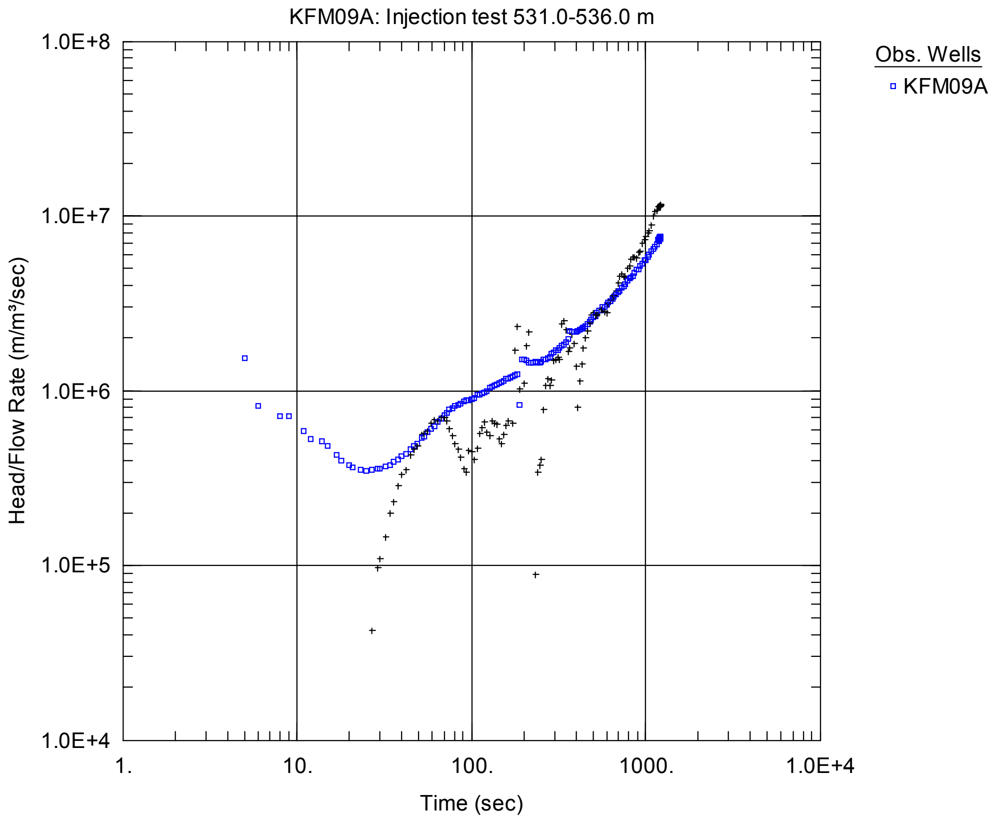


***Figure A3-496.** Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 531.0-536.0 m in KFM09A.*

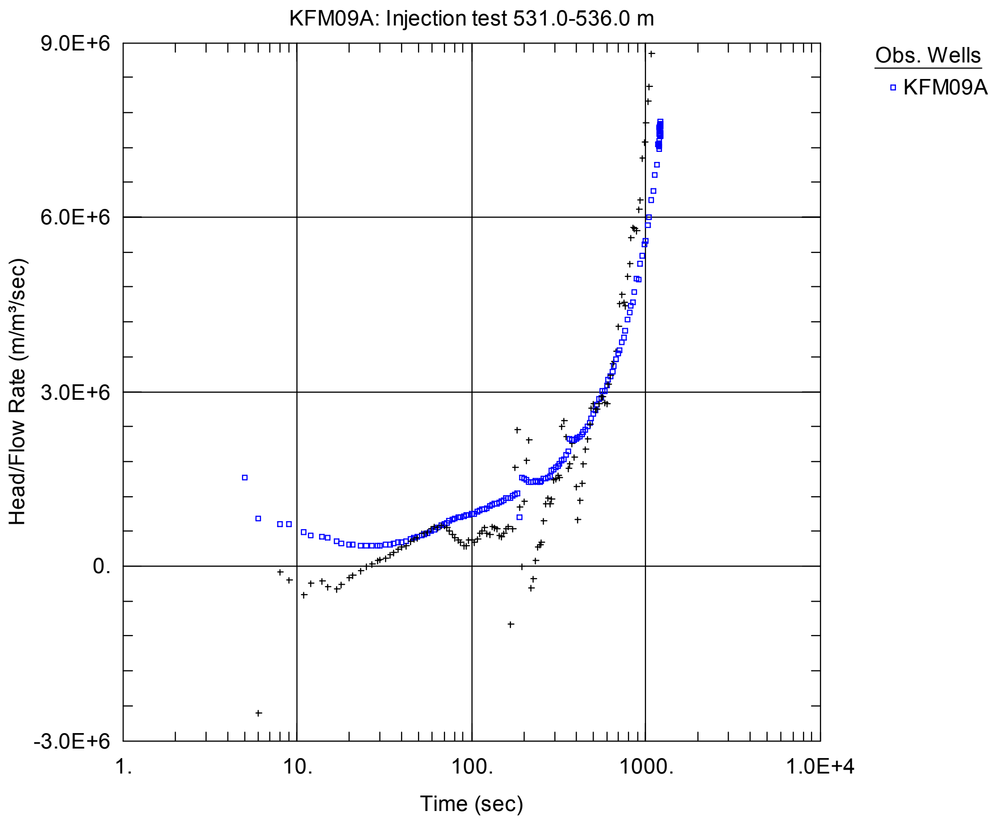


***Figure A3-497.** Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 531.0-536.0 m in KFM09A.*

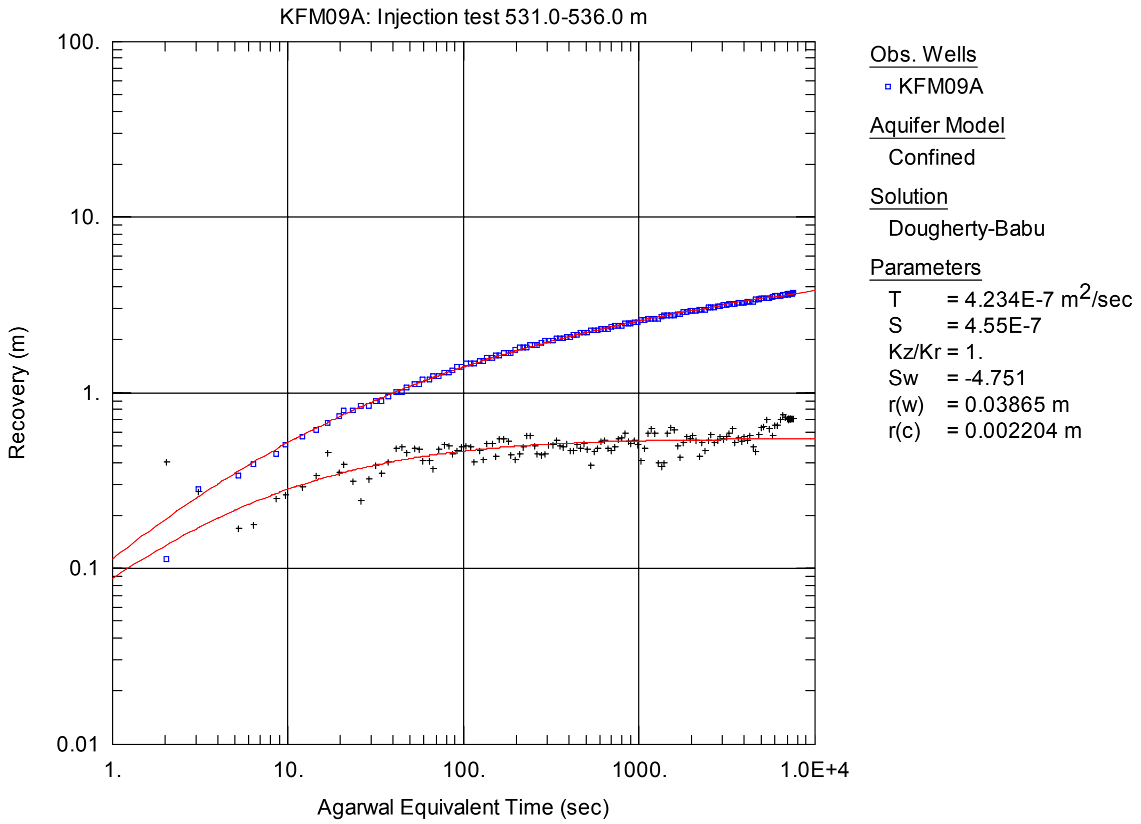


Figure A3-498. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 531.0-536.0 m in KFM09A.*

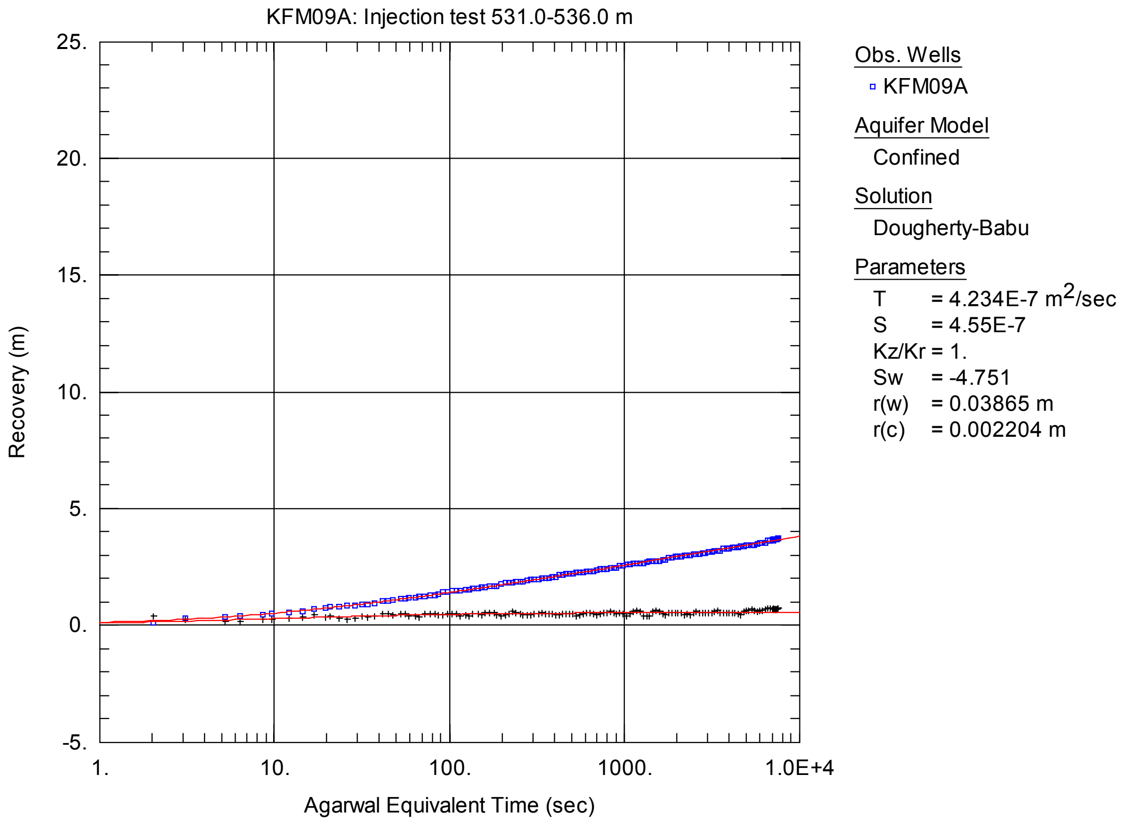


Figure A3-499. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 531.0-536.0 m in KFM09A.*

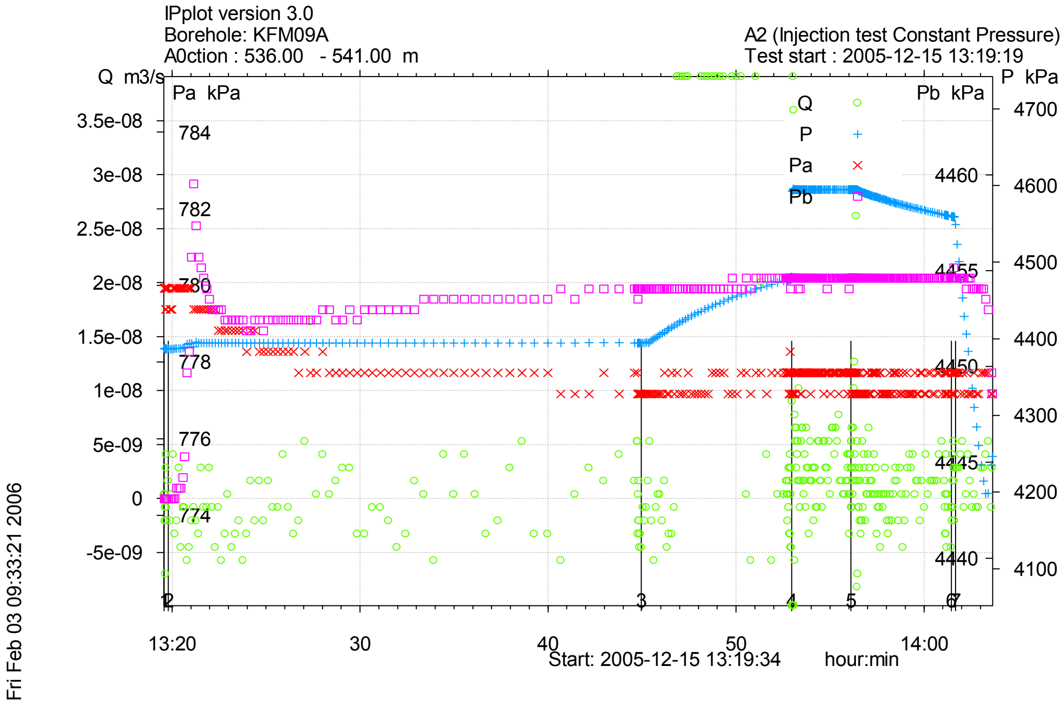


Figure A3-500. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 536.0-541.0 m in borehole KFM09A.

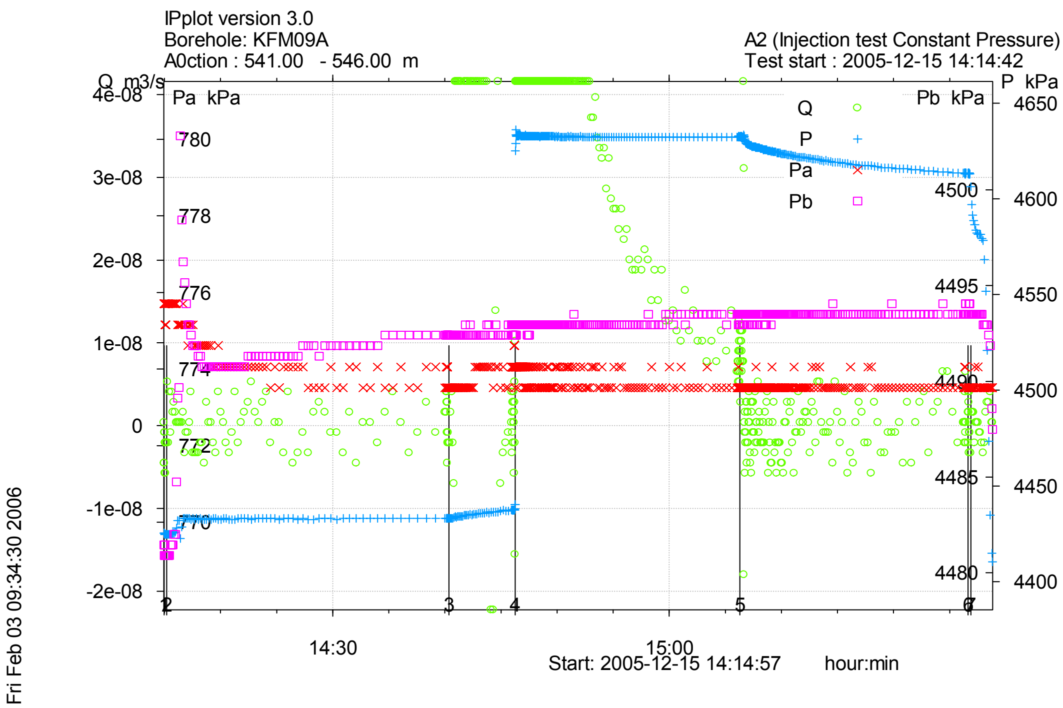


Figure A3-501. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 541.0-546.0 m in borehole KFM09A.

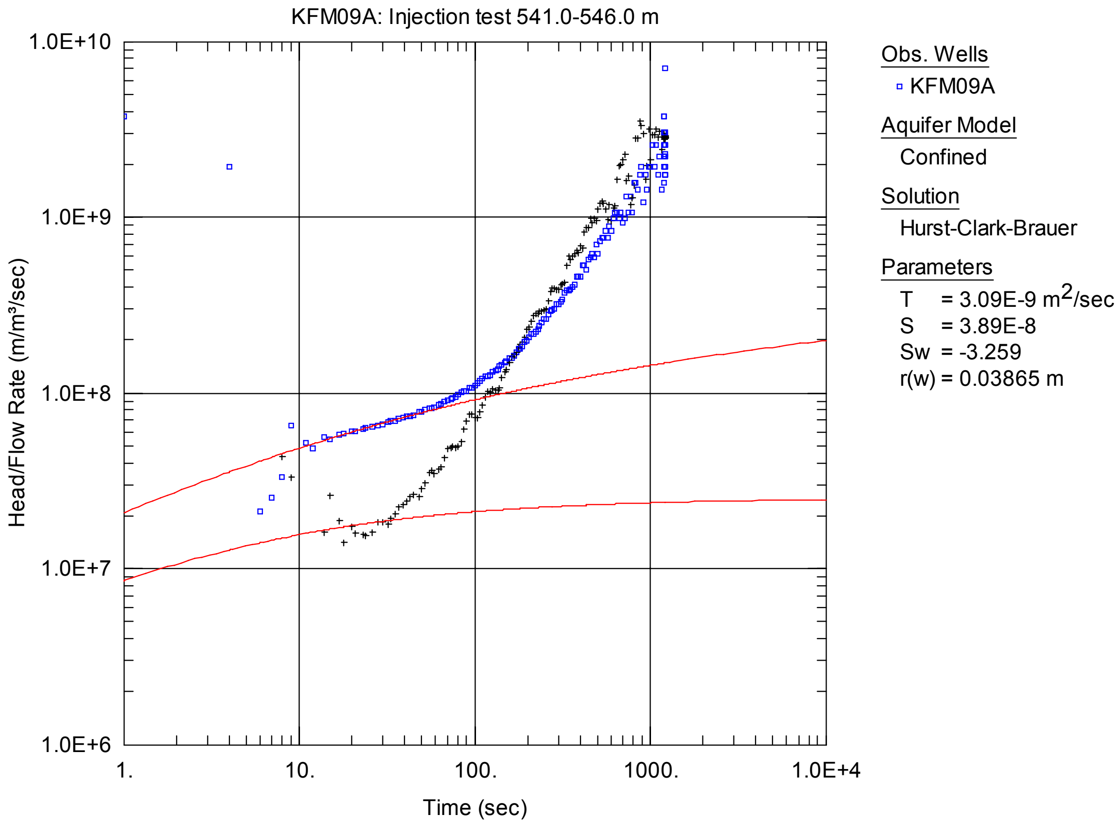


Figure A3-502. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 541.0-546.0 m in KFM09A.*

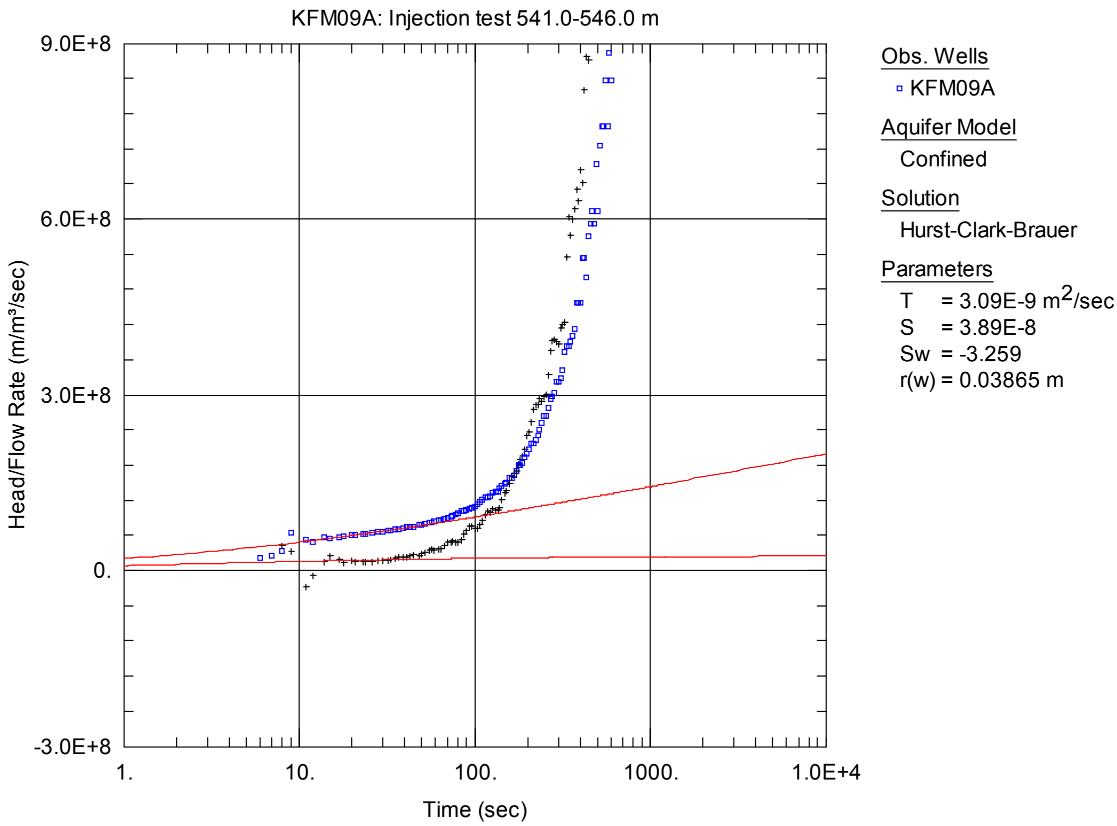


Figure A3-503. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 541.0-546.0 m in KFM09A.*

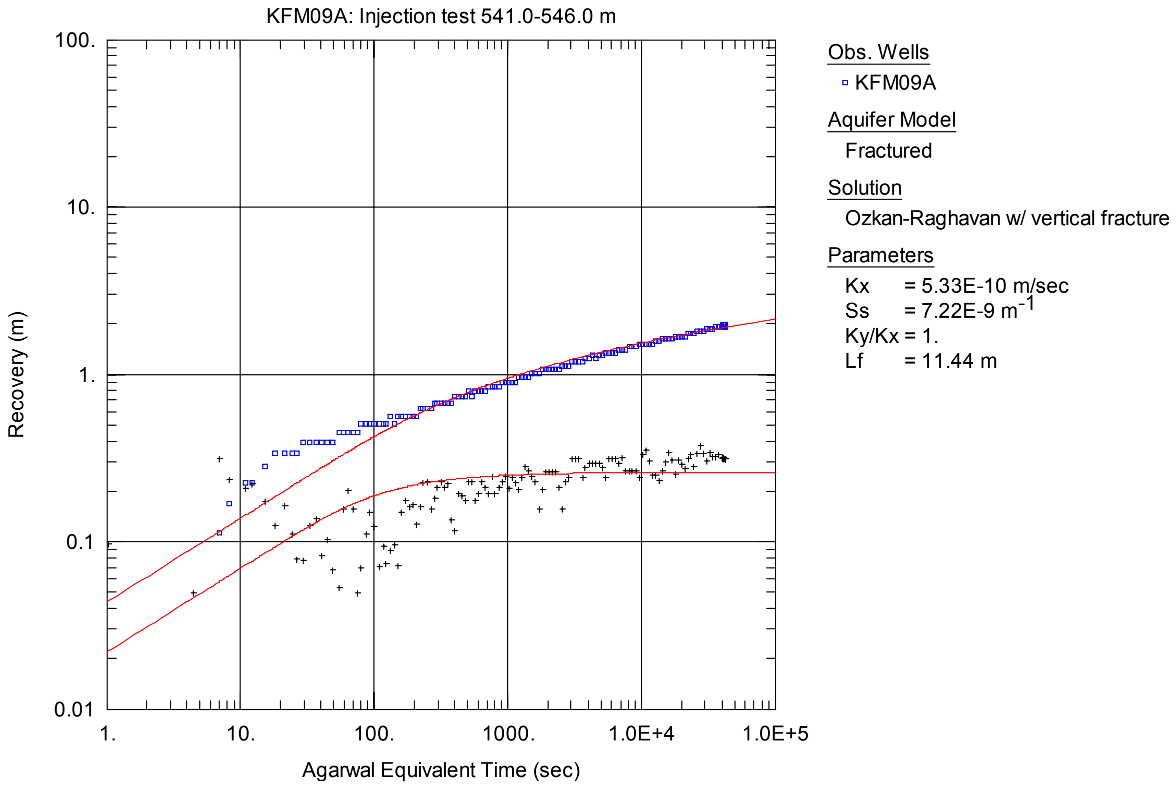


Figure A3-504. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 541.0-546.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

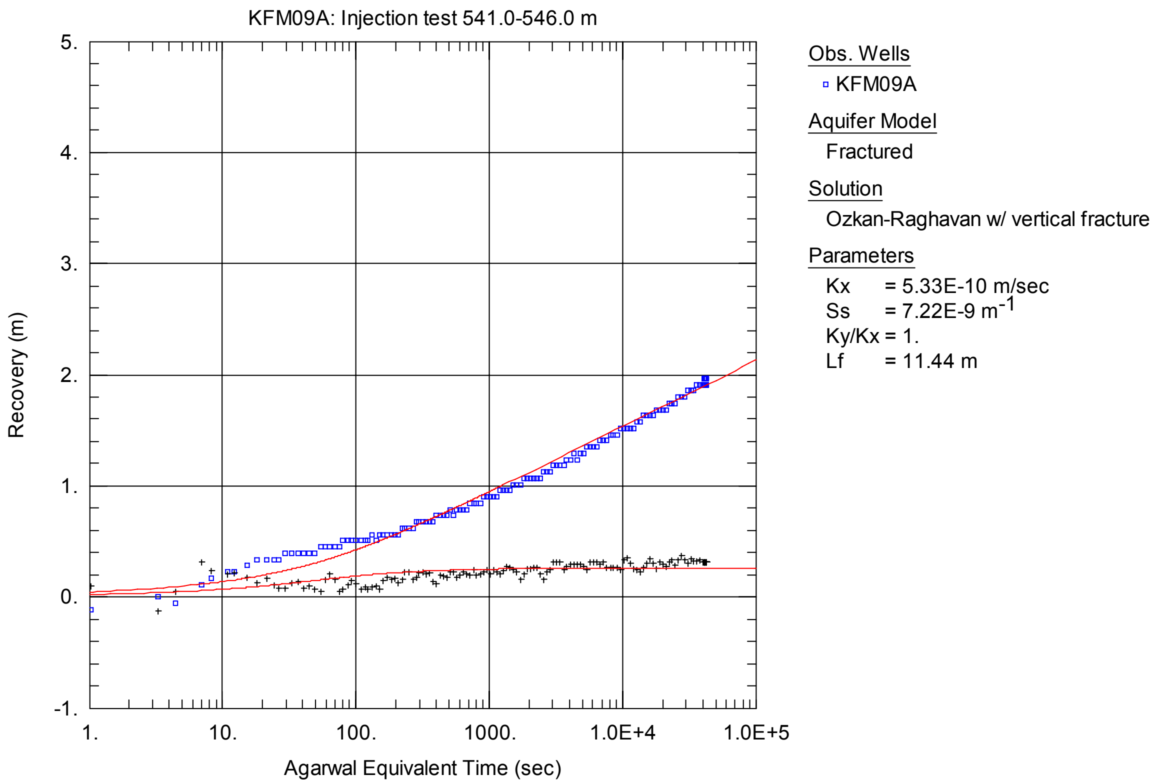


Figure A3-505. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 541.0-546.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

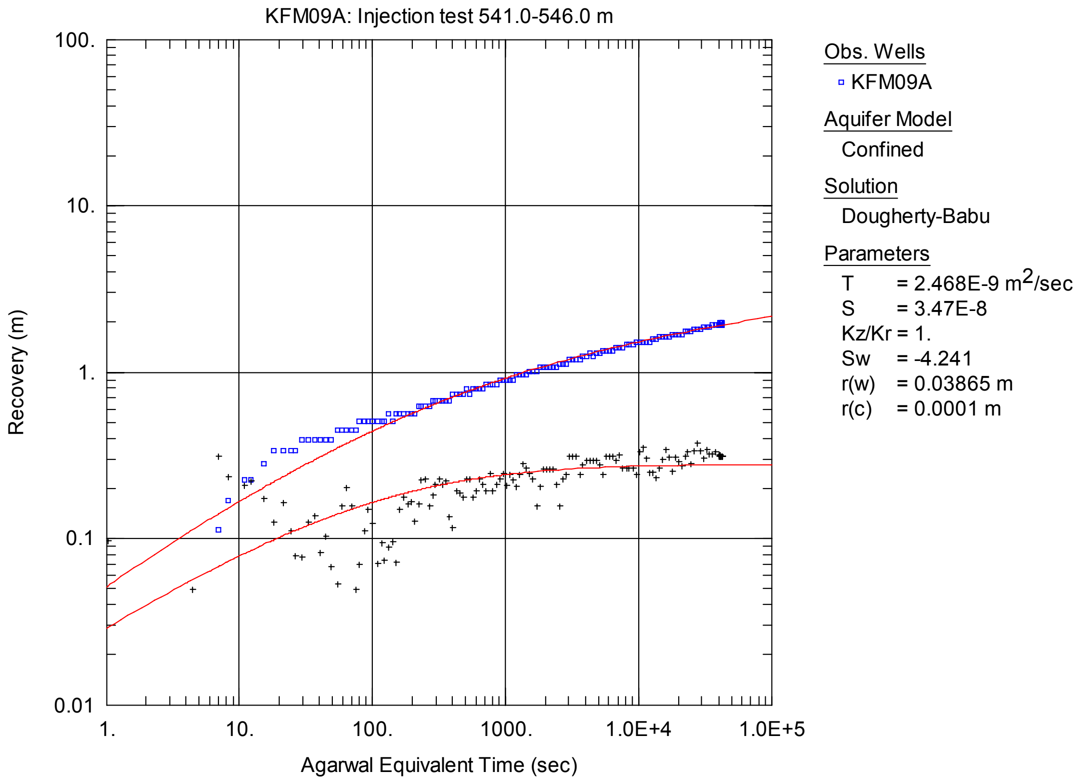


Figure A3-506. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 541.0-546.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

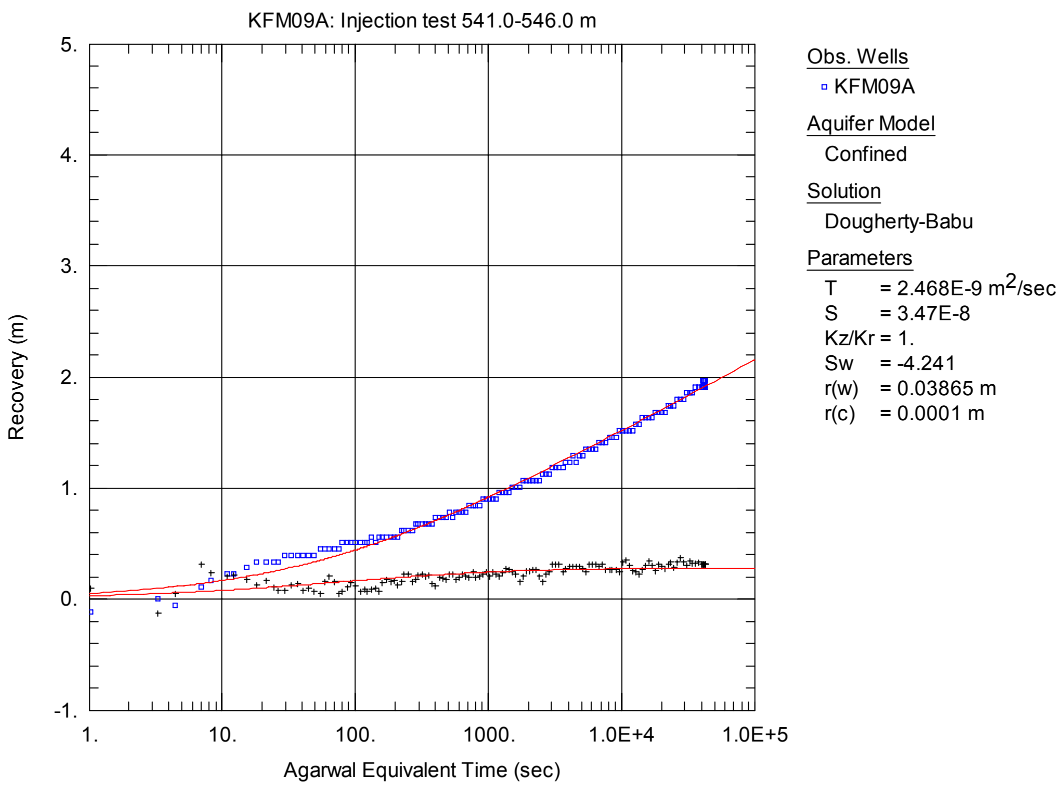


Figure A3-507. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 541.0-546.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

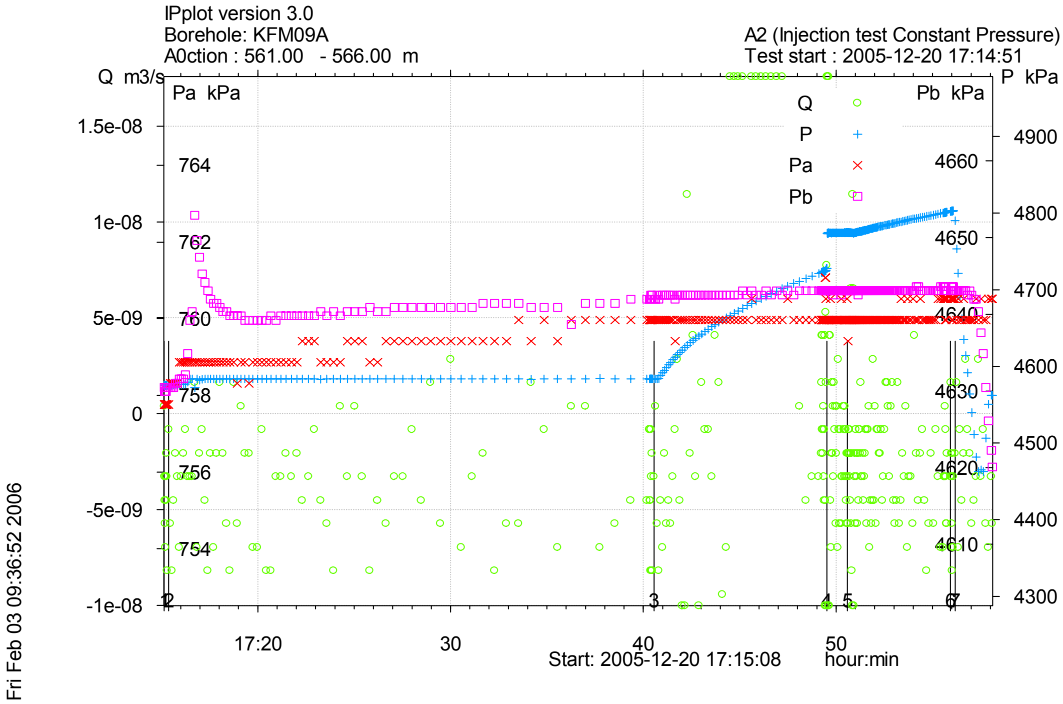


Figure A3-508. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 561.0-566.0 m in borehole KFM09A.*

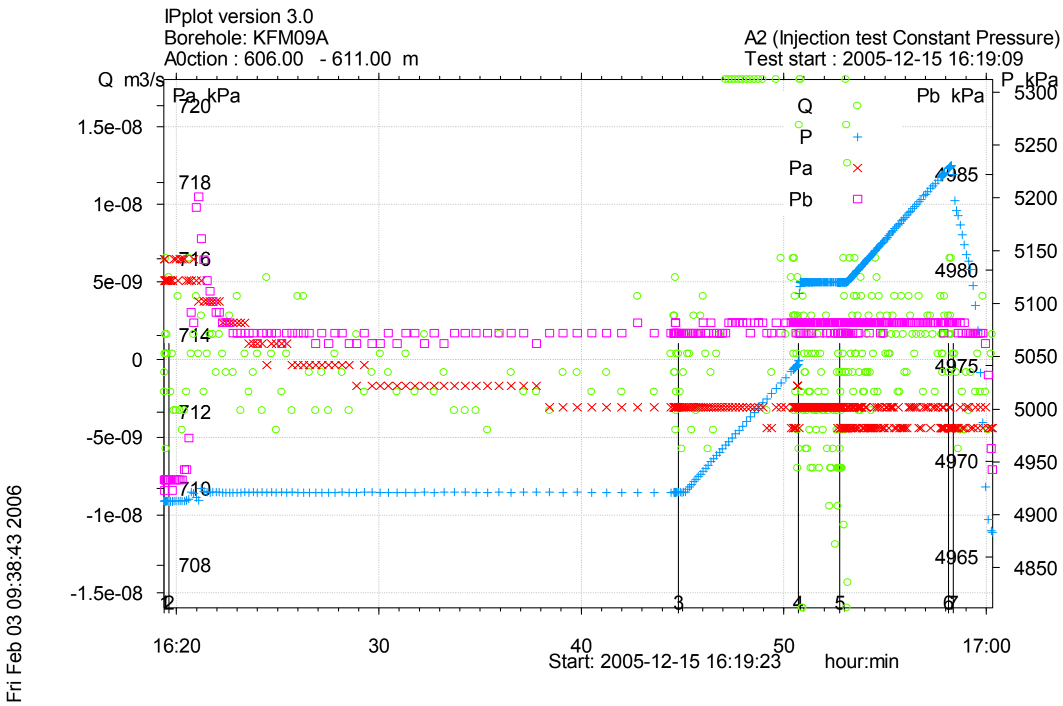


Figure A3-509. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 606.0-611.0 m in borehole KFM09A.*

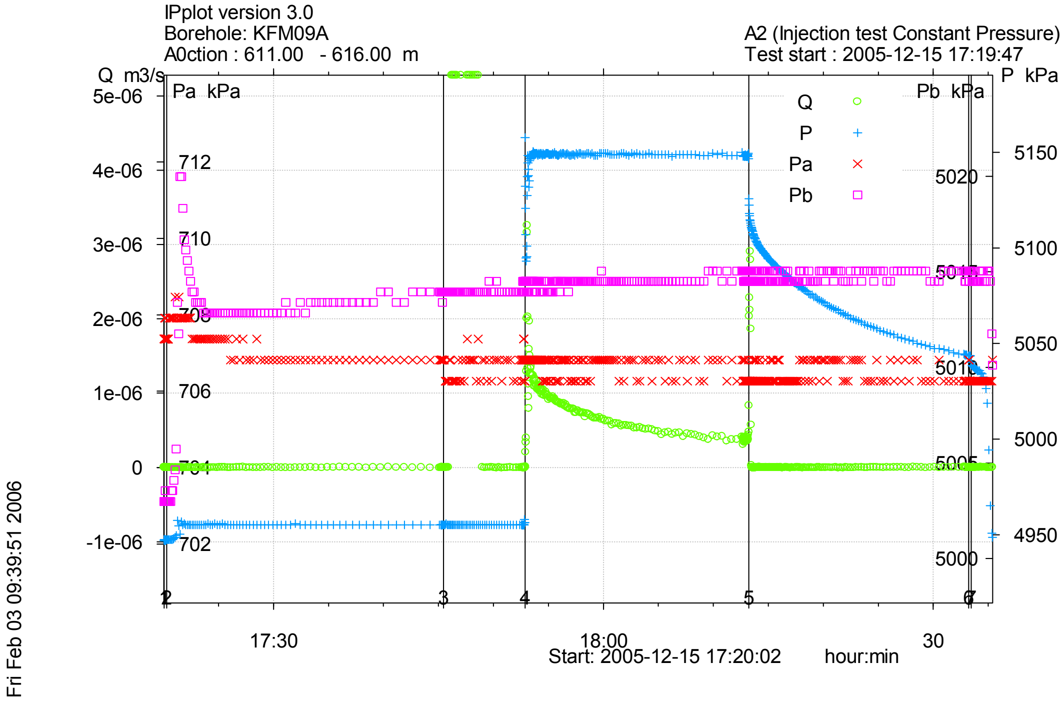


__Figure A3-510.__ Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 611.0-616.0 m in borehole KFM09A.

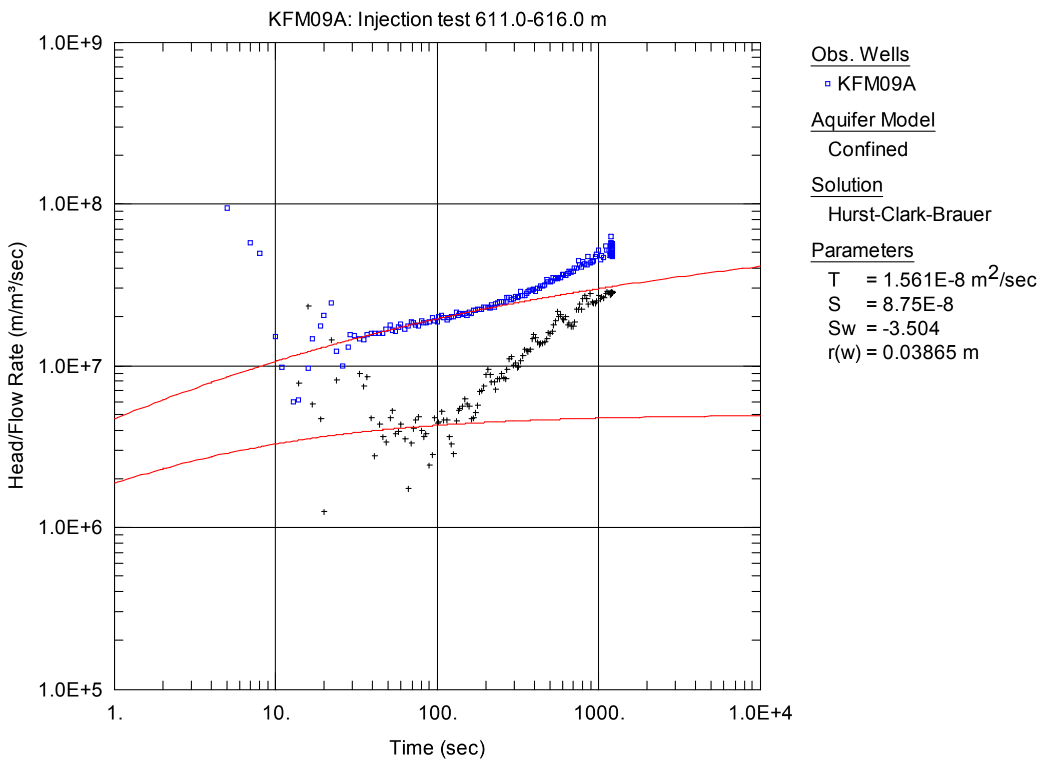


__Figure A3-511.__ Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 611.0-616.0 m in KFM09A.

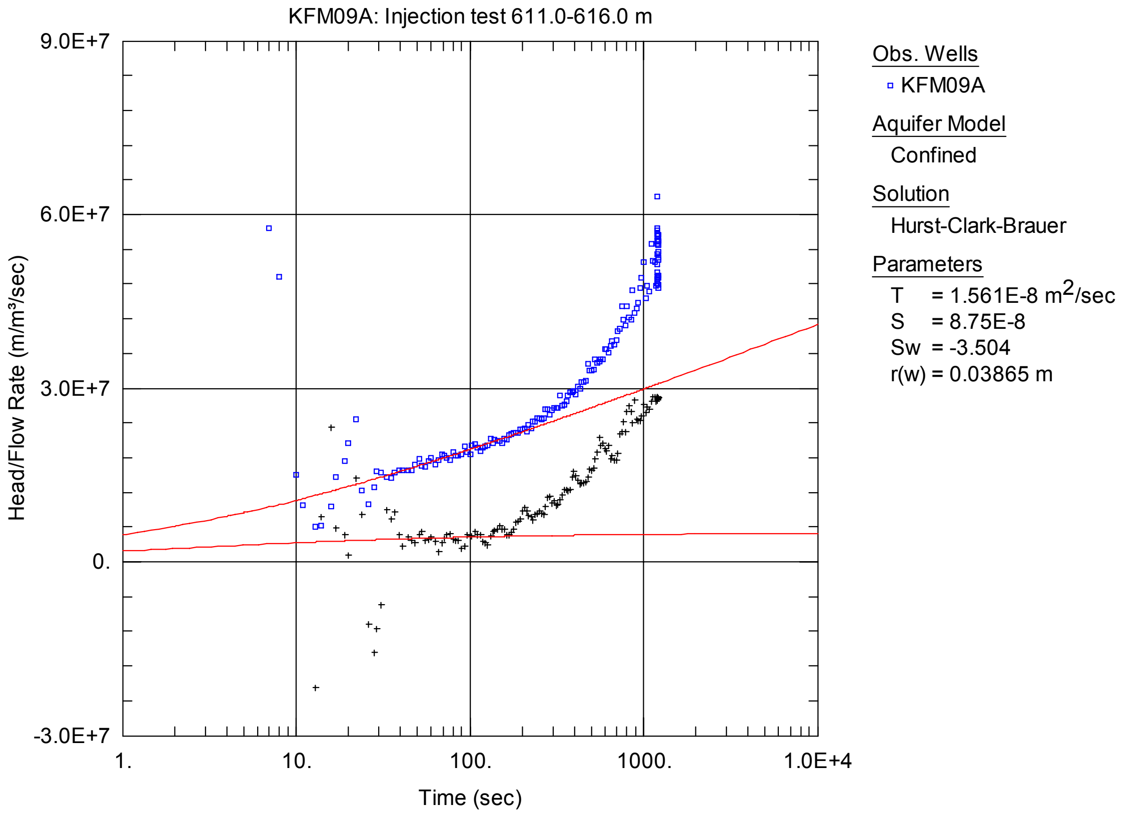


***Figure A3-512.** Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 611.0-616.0 m in KFM09A.*

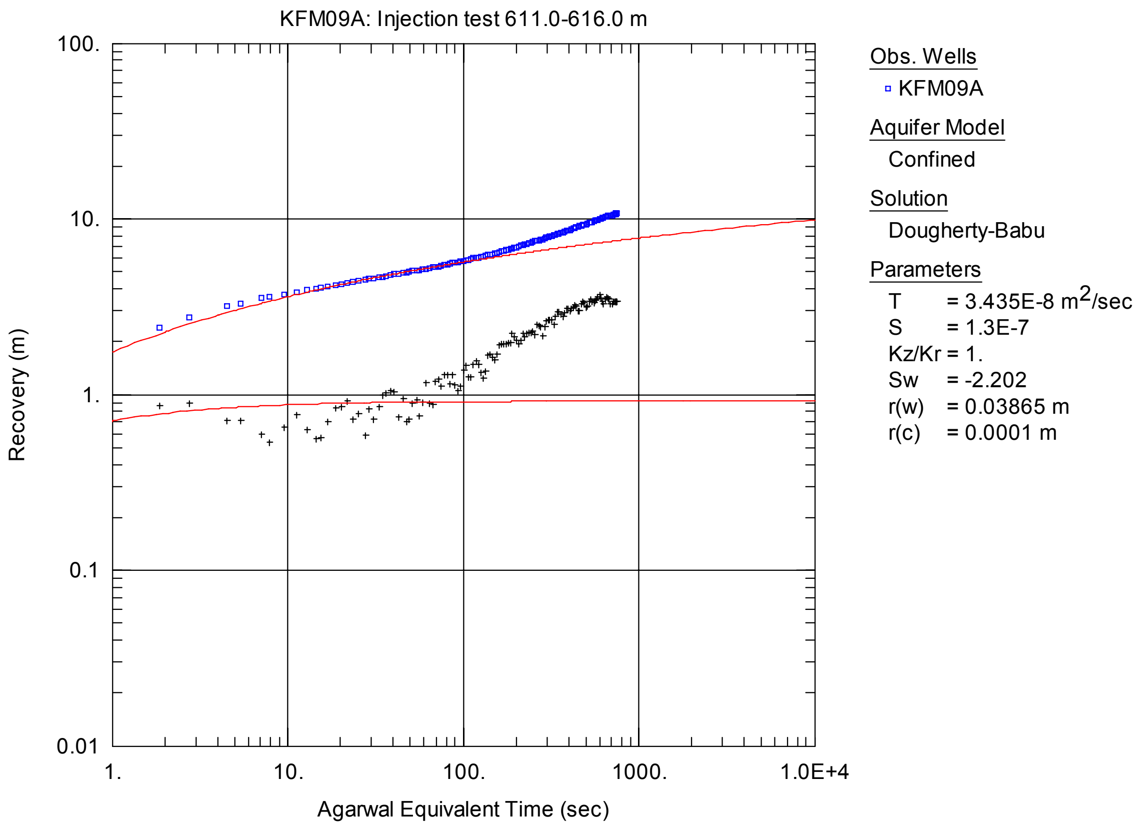


***Figure A3-513.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 611.0-616.0 m in KFM09A.*

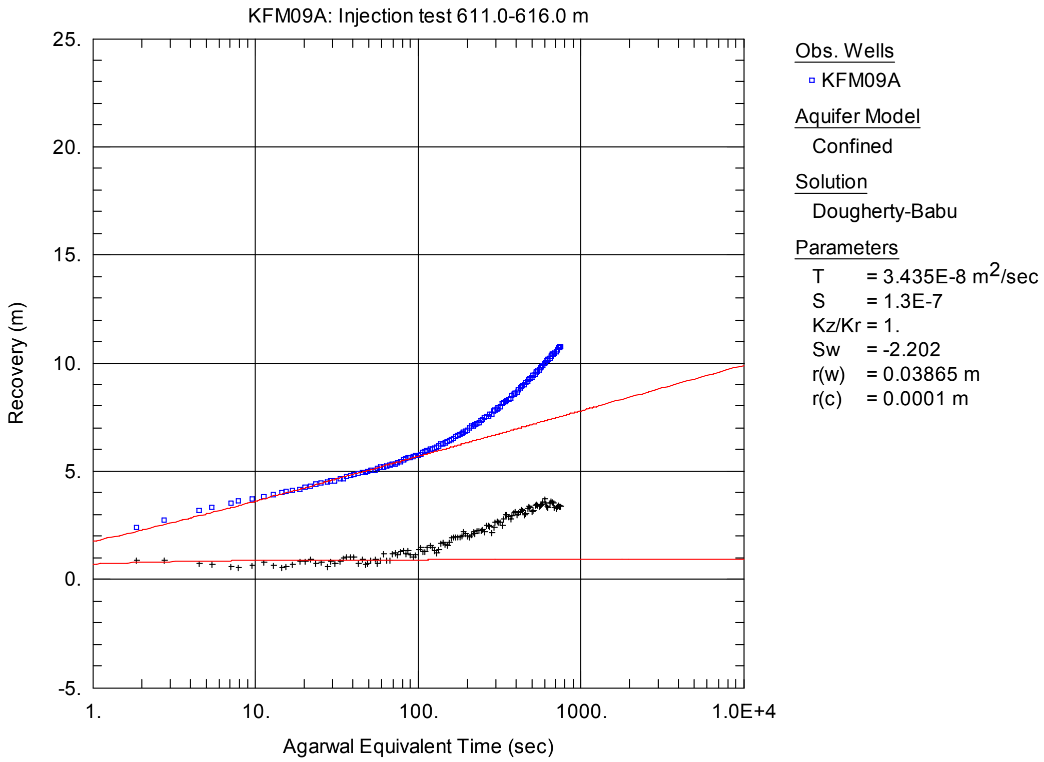


Figure A3-514. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 611.0-616.0 m in KFM09A.*

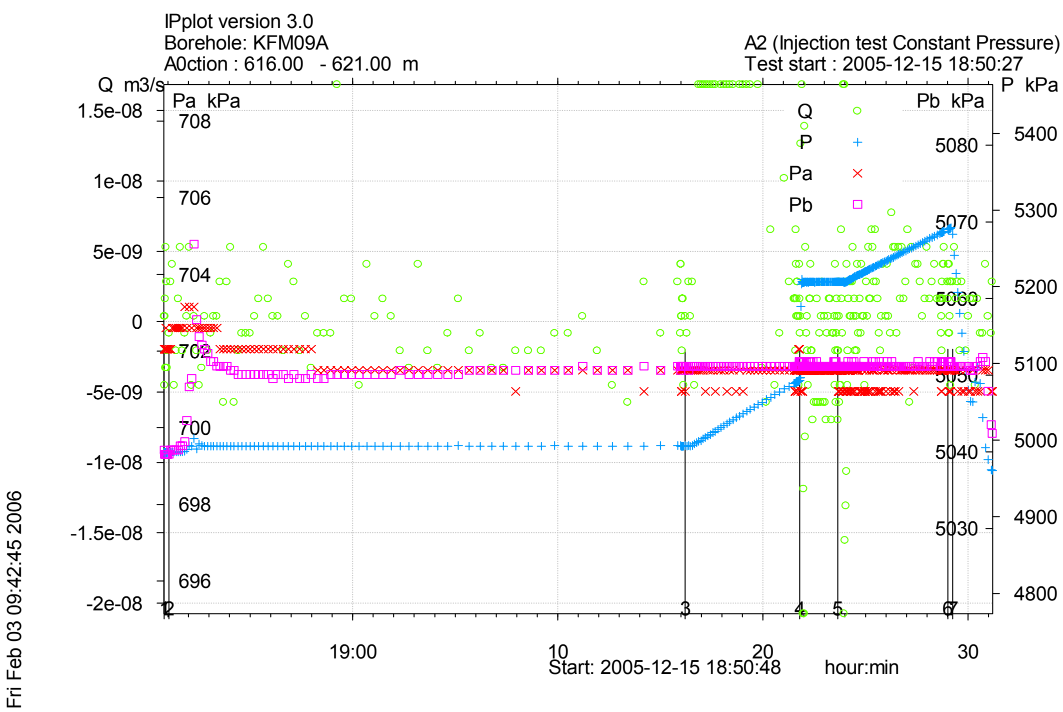


Figure A3-515. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 616.0-621.0 m in borehole KFM09A.*

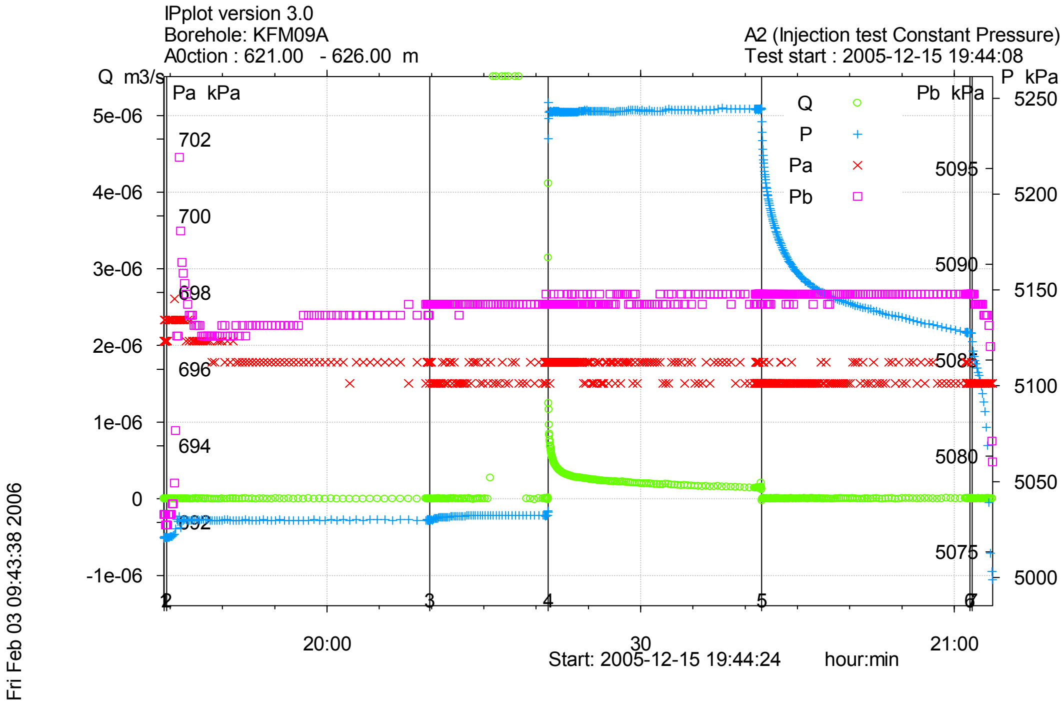


Figure A3-516. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 621.0-626.0 m in borehole KFM09A.*

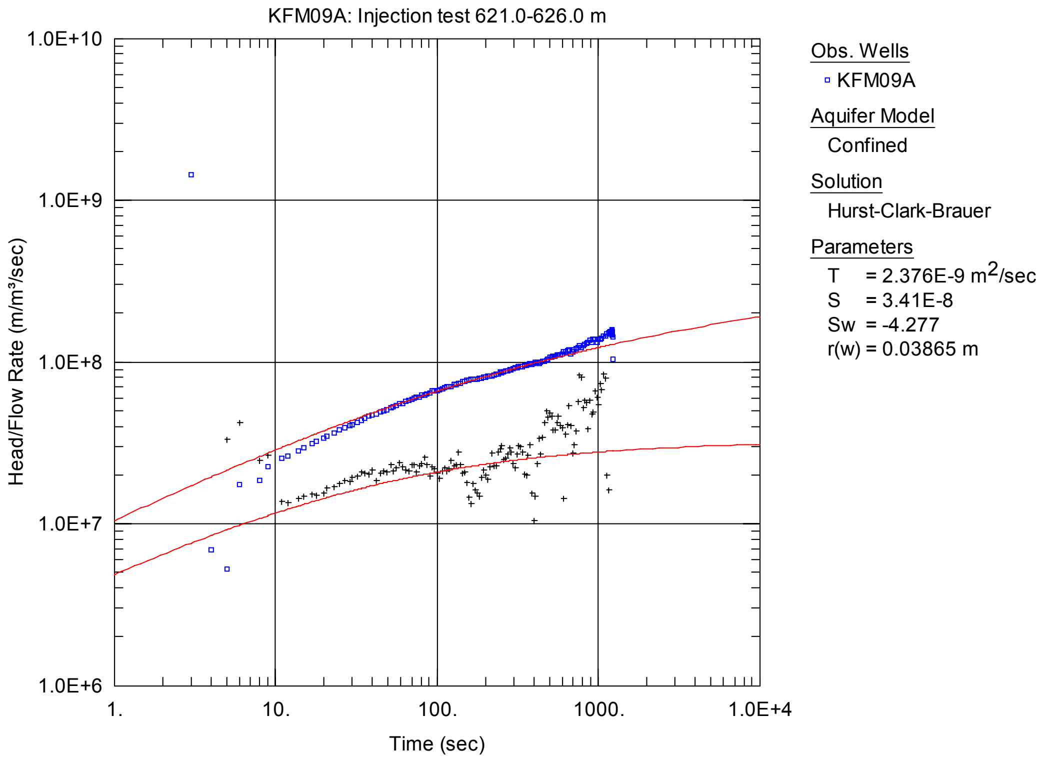


Figure A3-517. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 621.0-626.0 m in KFM09A.*

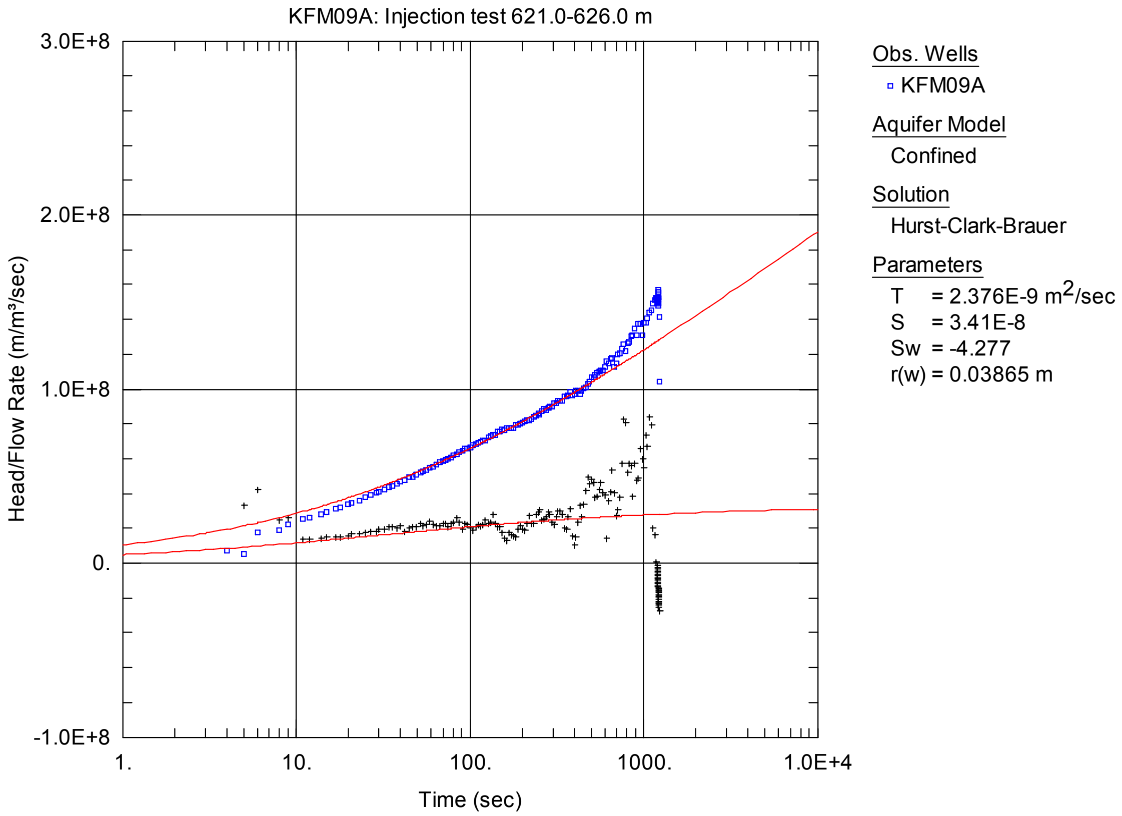


Figure A3-518. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 621.0-626.0 m in KFM09A.*

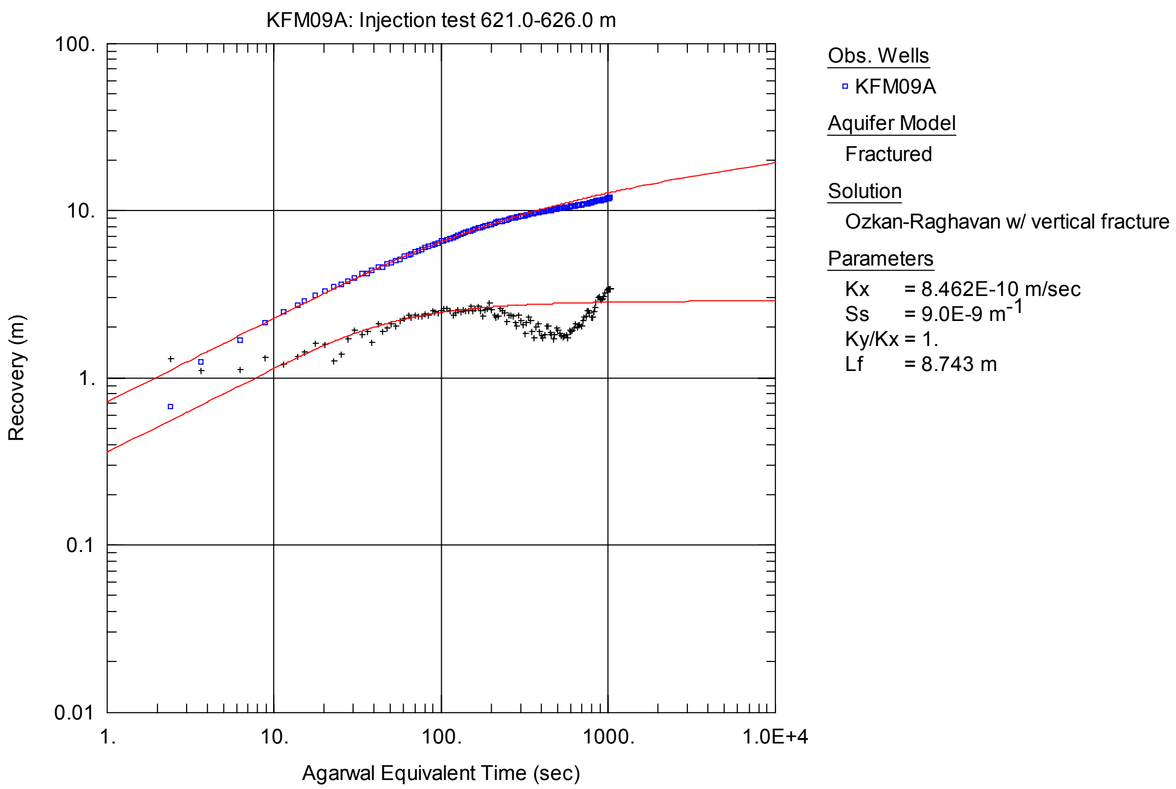


Figure A3-519. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 621.0-626.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

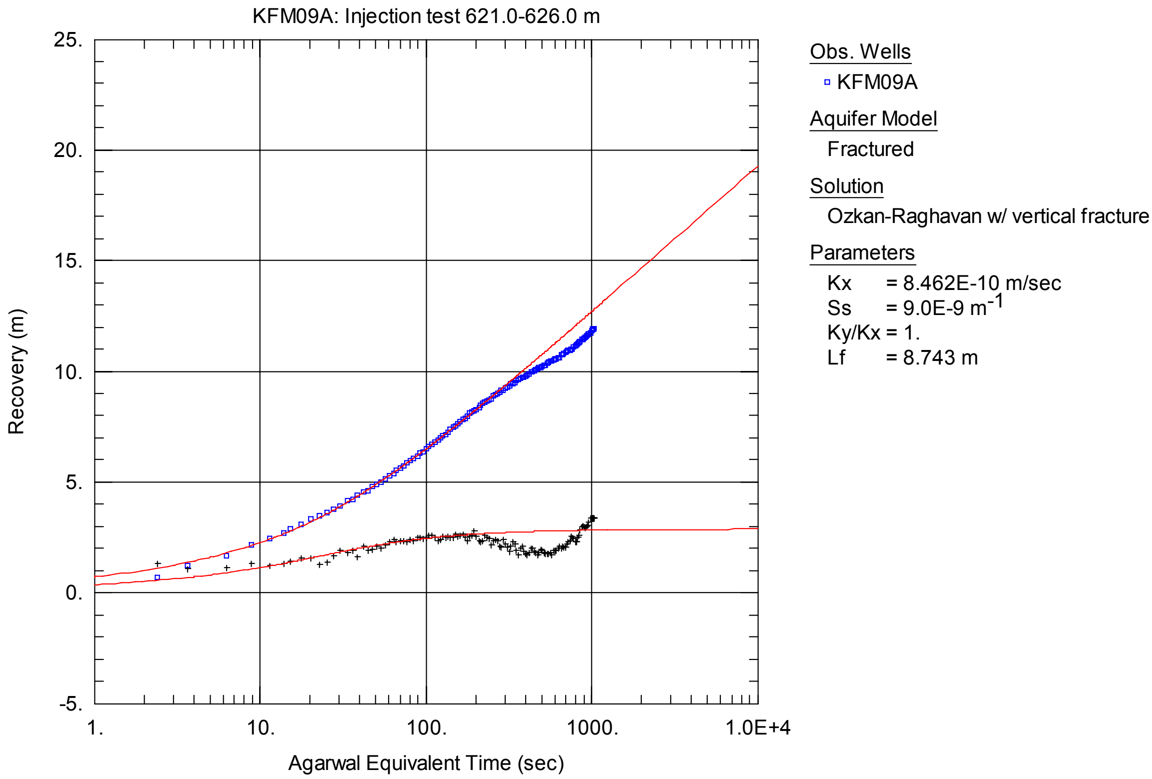


Figure A3-520. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 621.0-626.0 m in KFM09A.This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

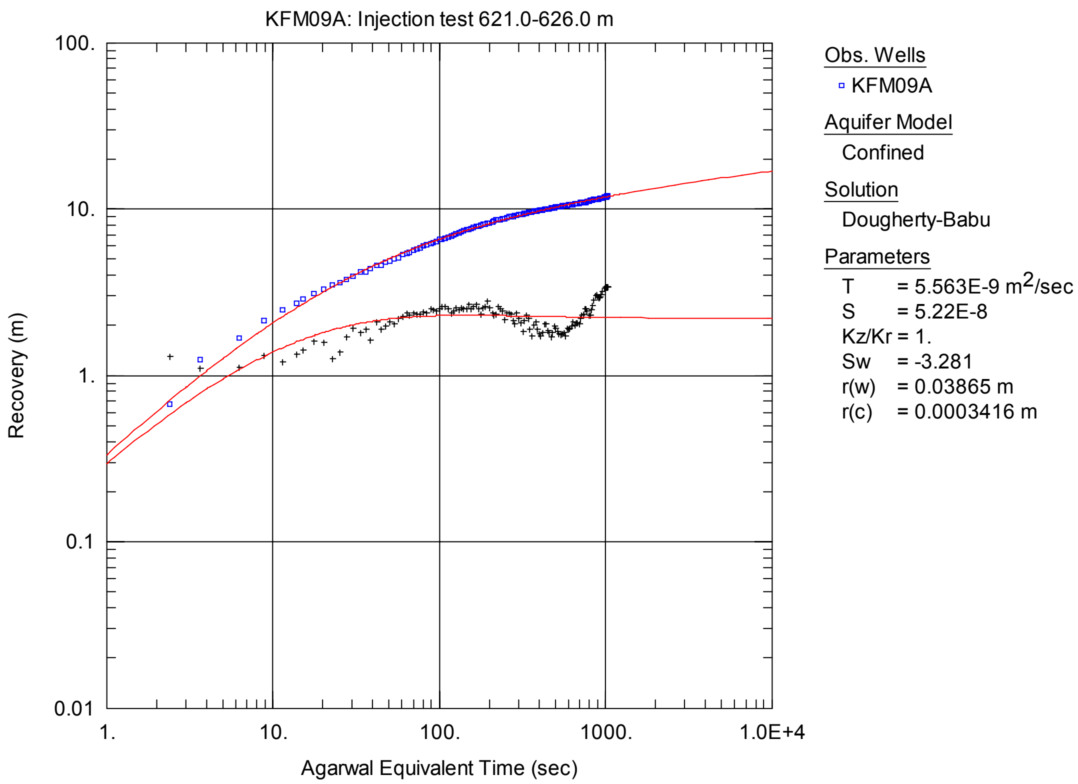


Figure A3-521. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 621.0-626.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

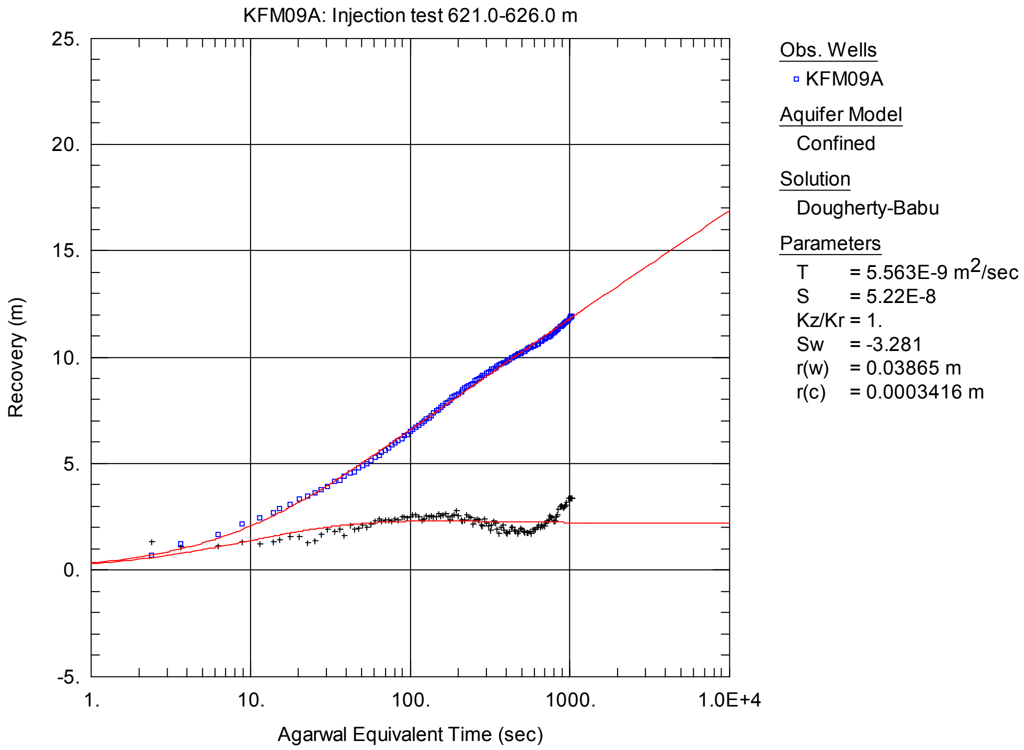


Figure A3-522. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 621.0-626.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

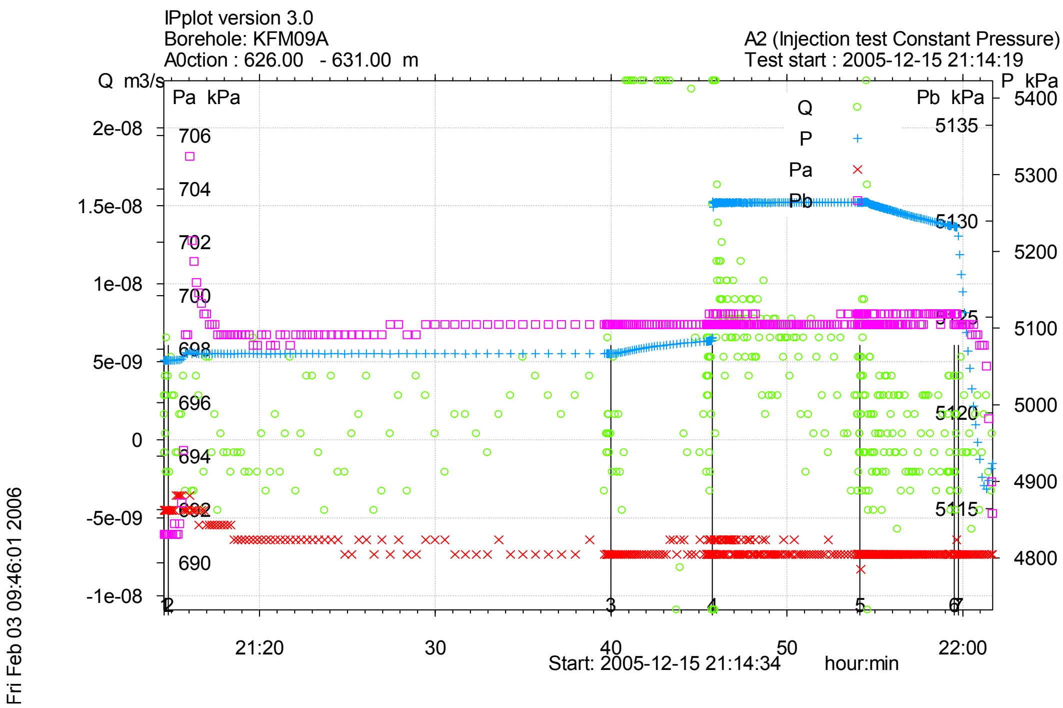


Figure A3-523. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 626.0-631.0 m in borehole KFM09A.*

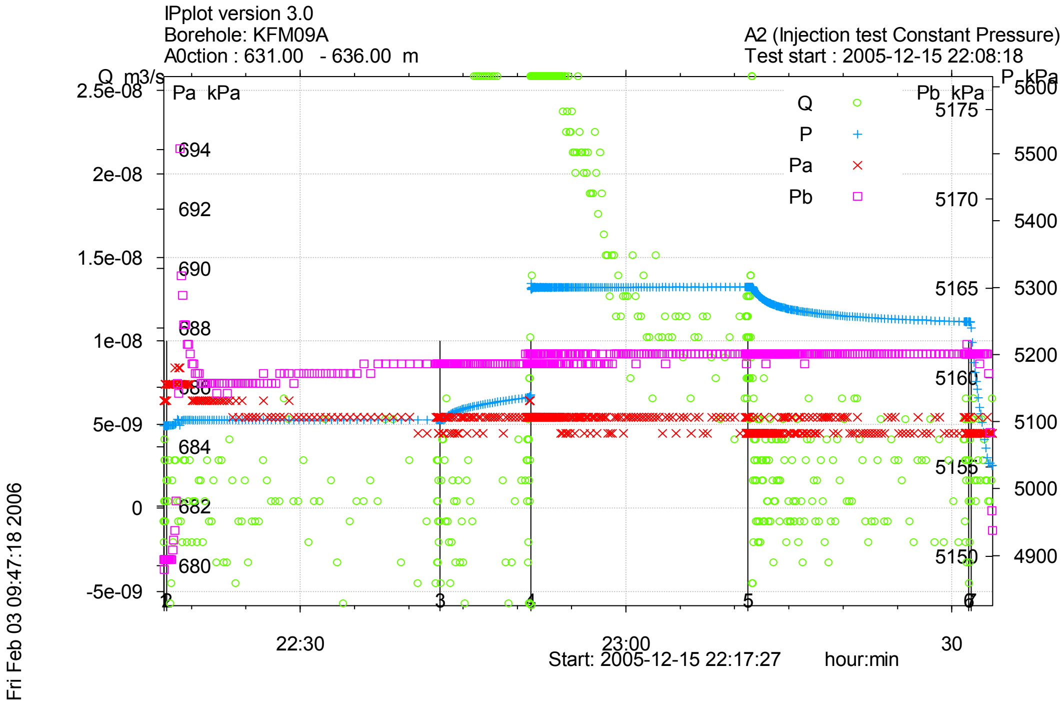


***Figure A3-524.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 631.0-636.0 m in borehole KFM09A.*

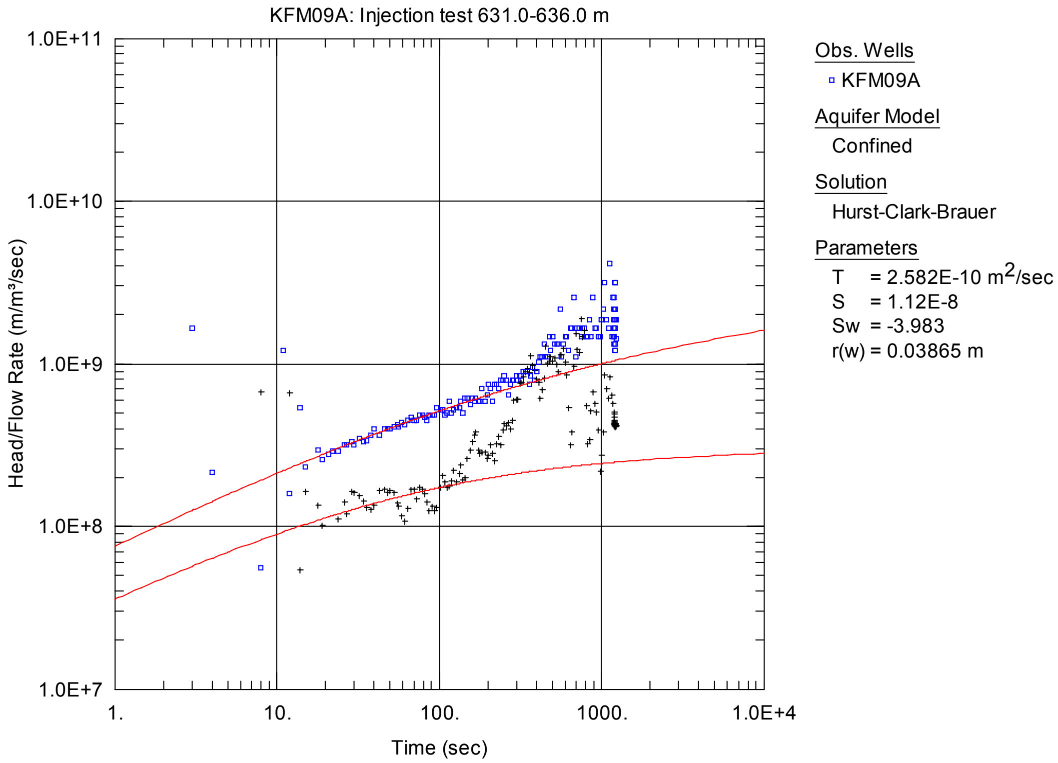


***Figure A3-525.** Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 631.0-636.0 m in KFM09A.*

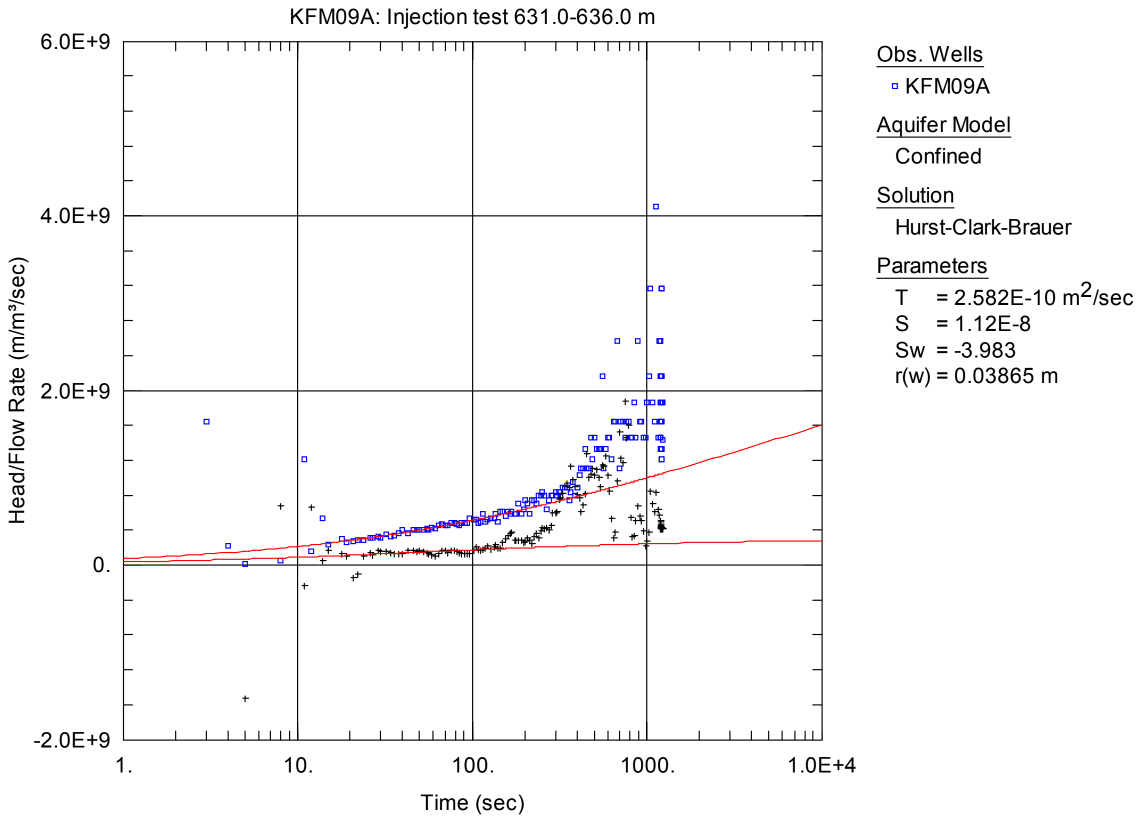


Figure A3-526. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 631.0-636.0 m in KFM09A.*

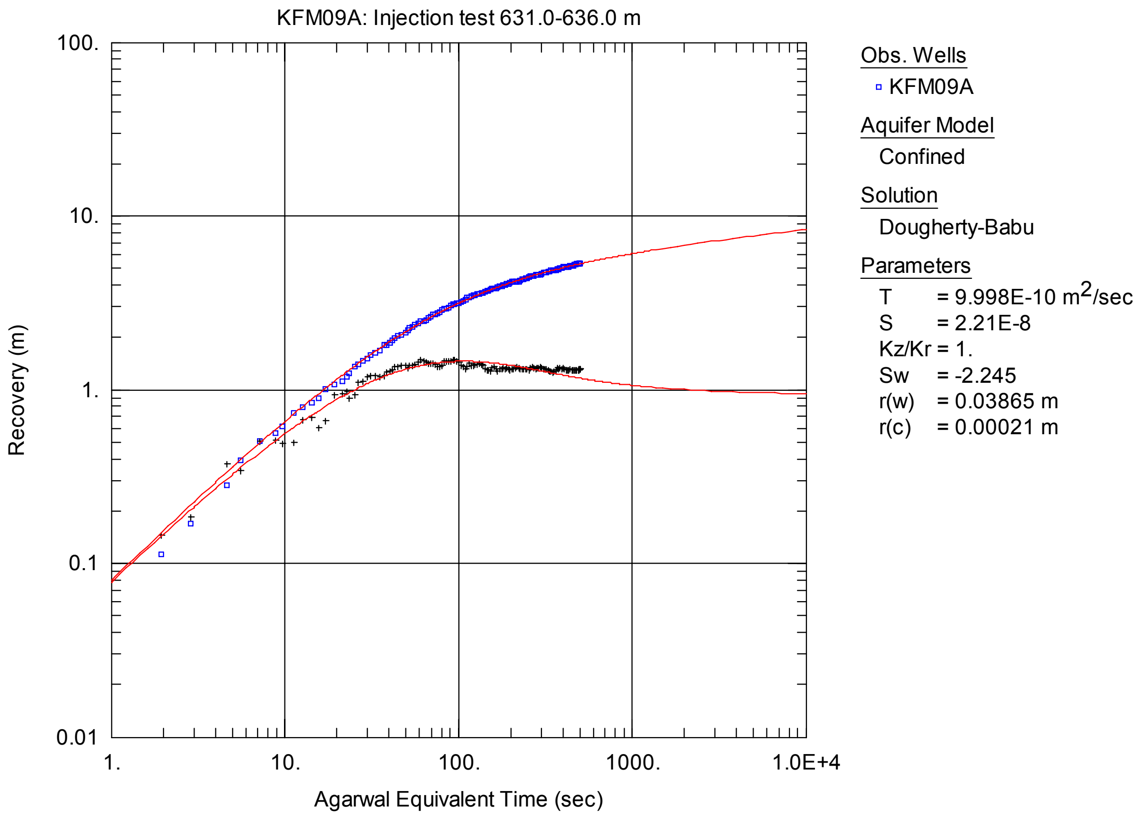


Figure A3-527. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 631.0-636.0 m in KFM09A.*

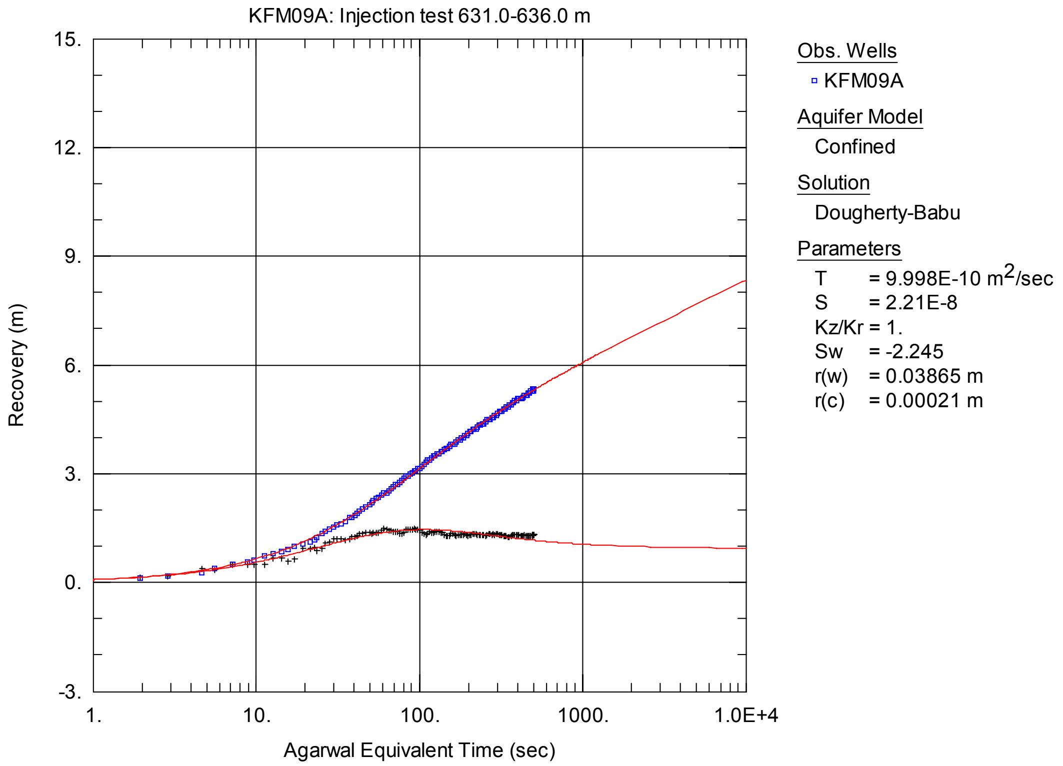


Figure A3-528. Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 631.0-636.0 m in KFM09A.

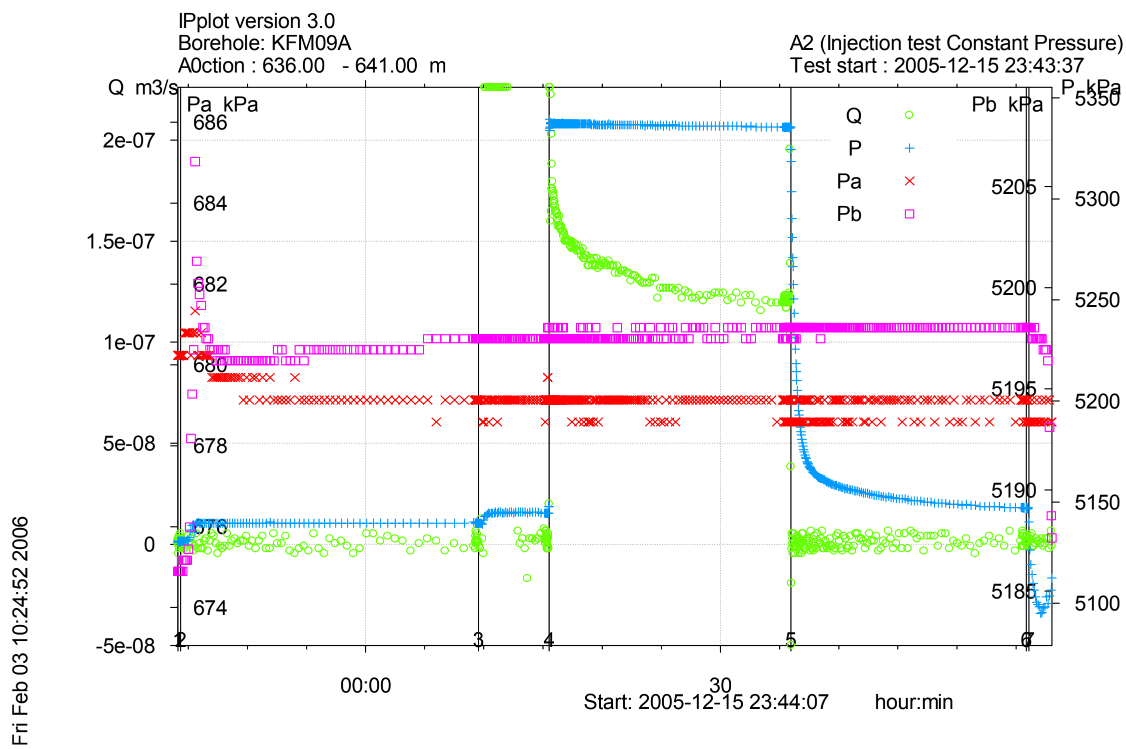


Figure A3-529. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 636.0-641.0 m in borehole KFM09A.

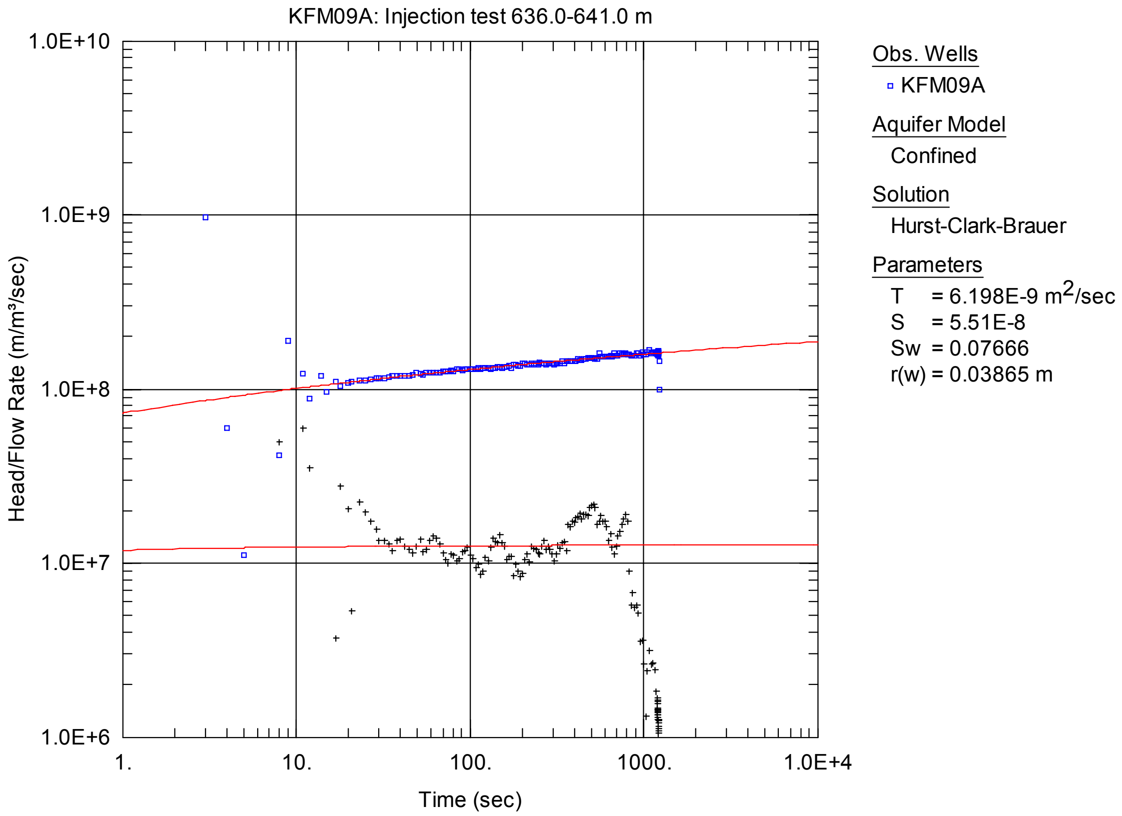


Figure A3-530. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 636.0-641.0 m in KFM09A.*

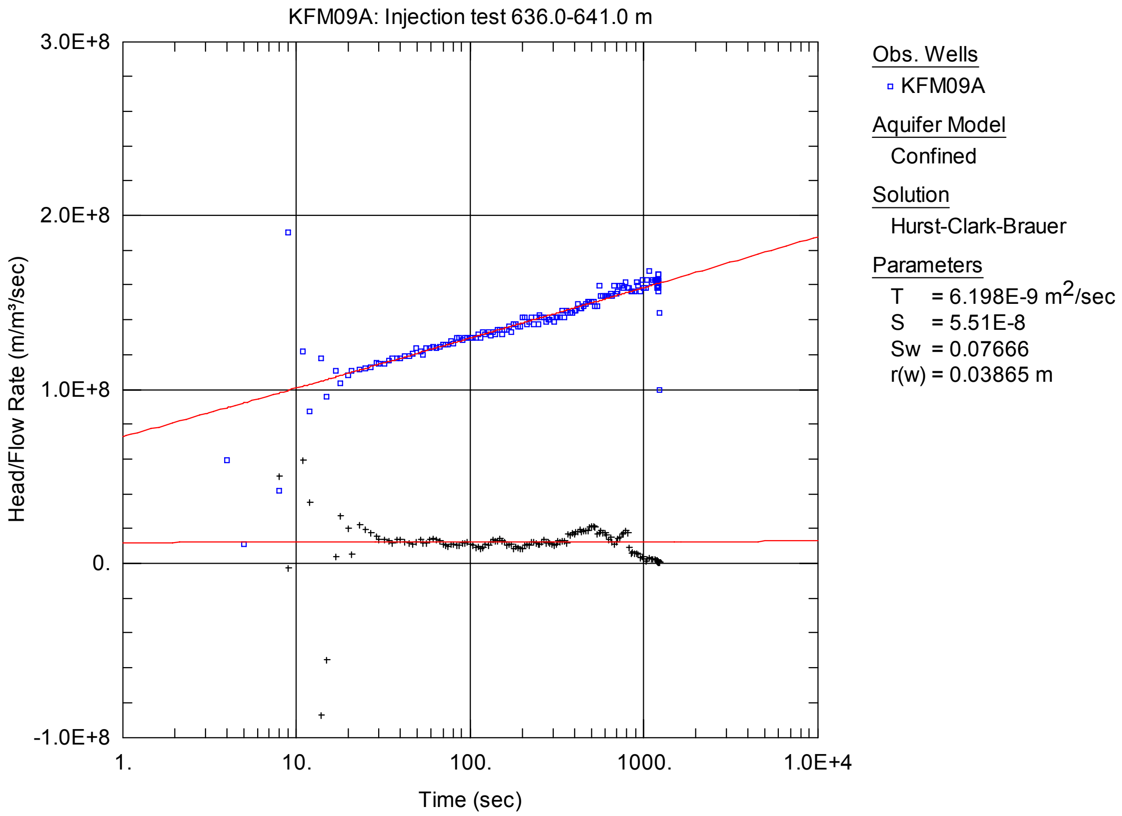


Figure A3-531. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 636.0-641.0 m in KFM09A.*

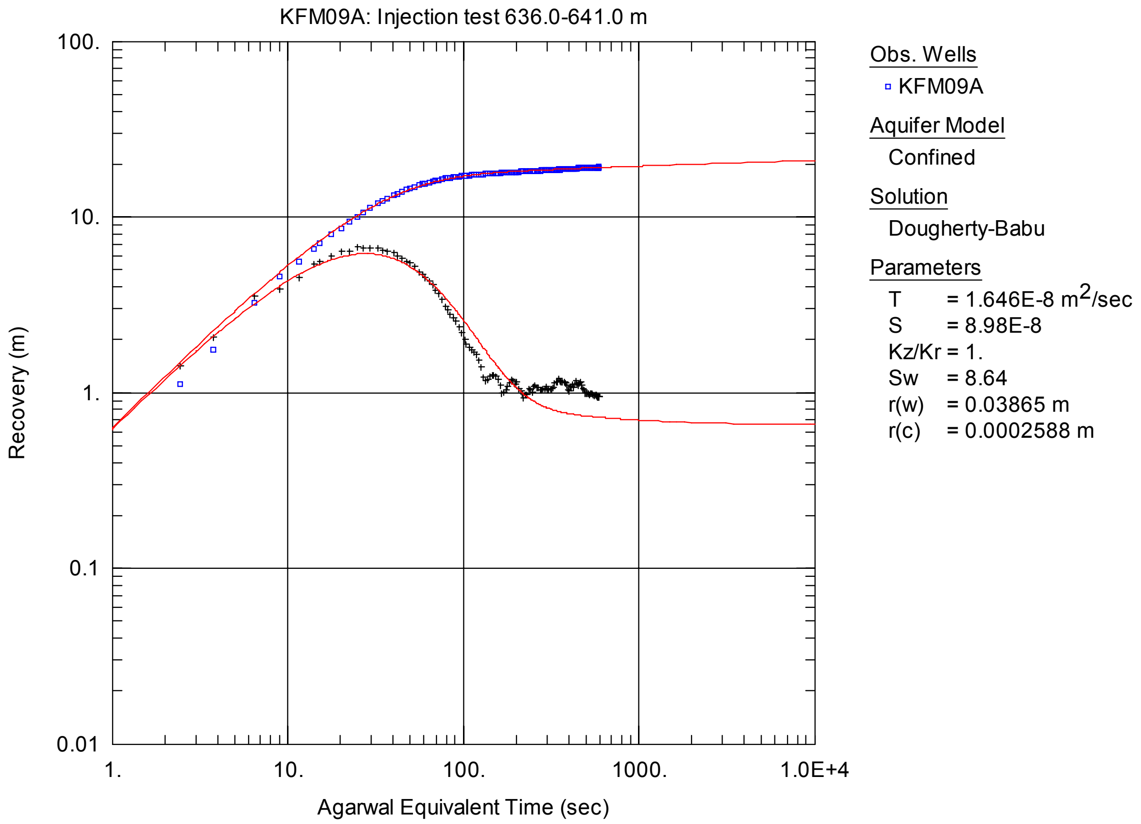


Figure A3-532. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 636.0-641.0 m in KFM09A.*

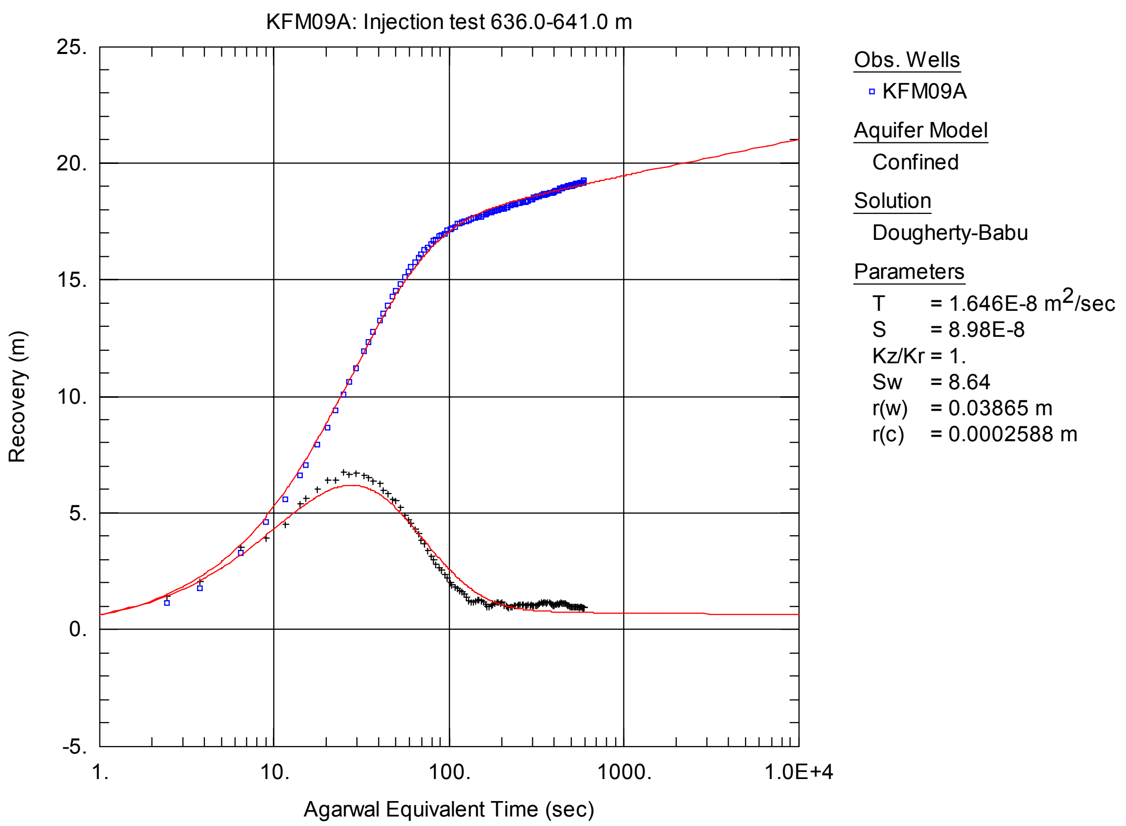


Figure A3-533. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 636.0-641.0 m in KFM09A.*

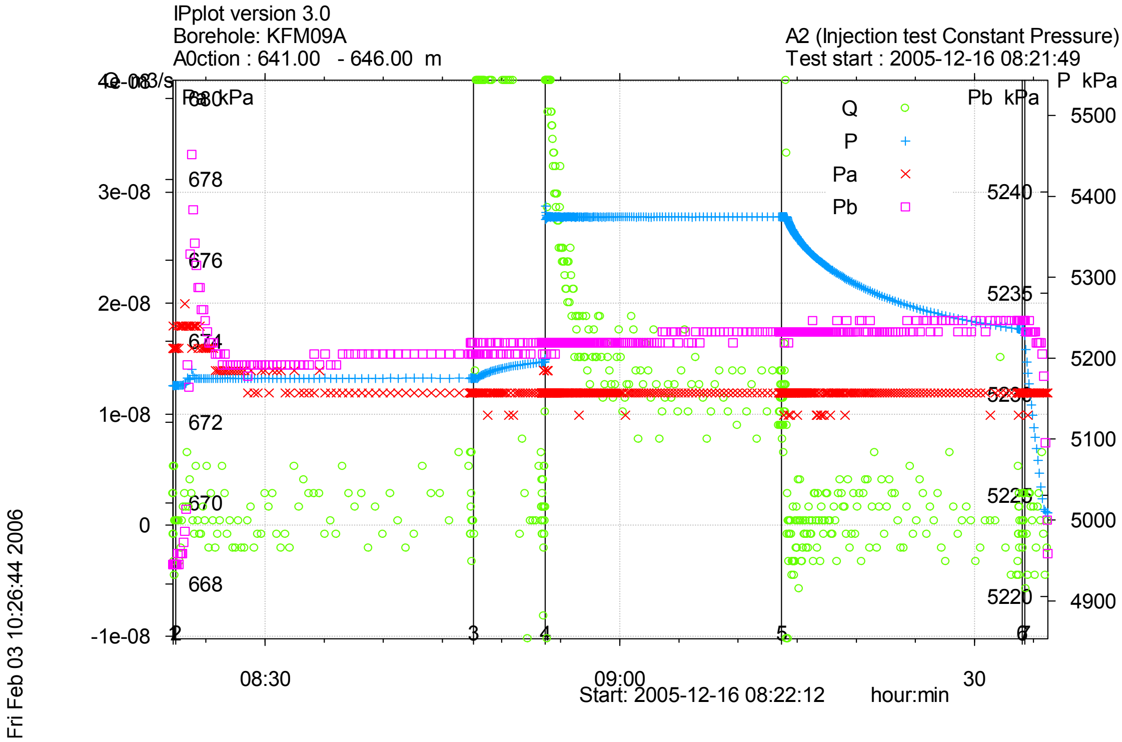


Figure A3-534. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 641.0-646.0 m in borehole KFM09A.

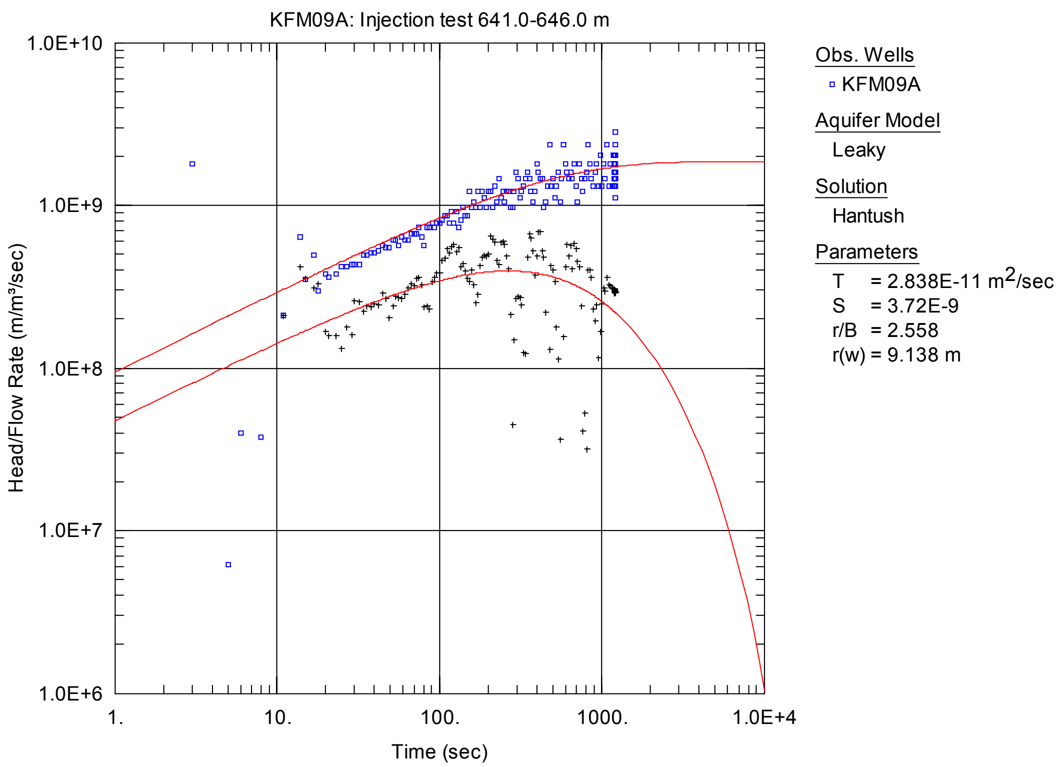


Figure A3-535. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 641.0-646.0 m in KFM09A.

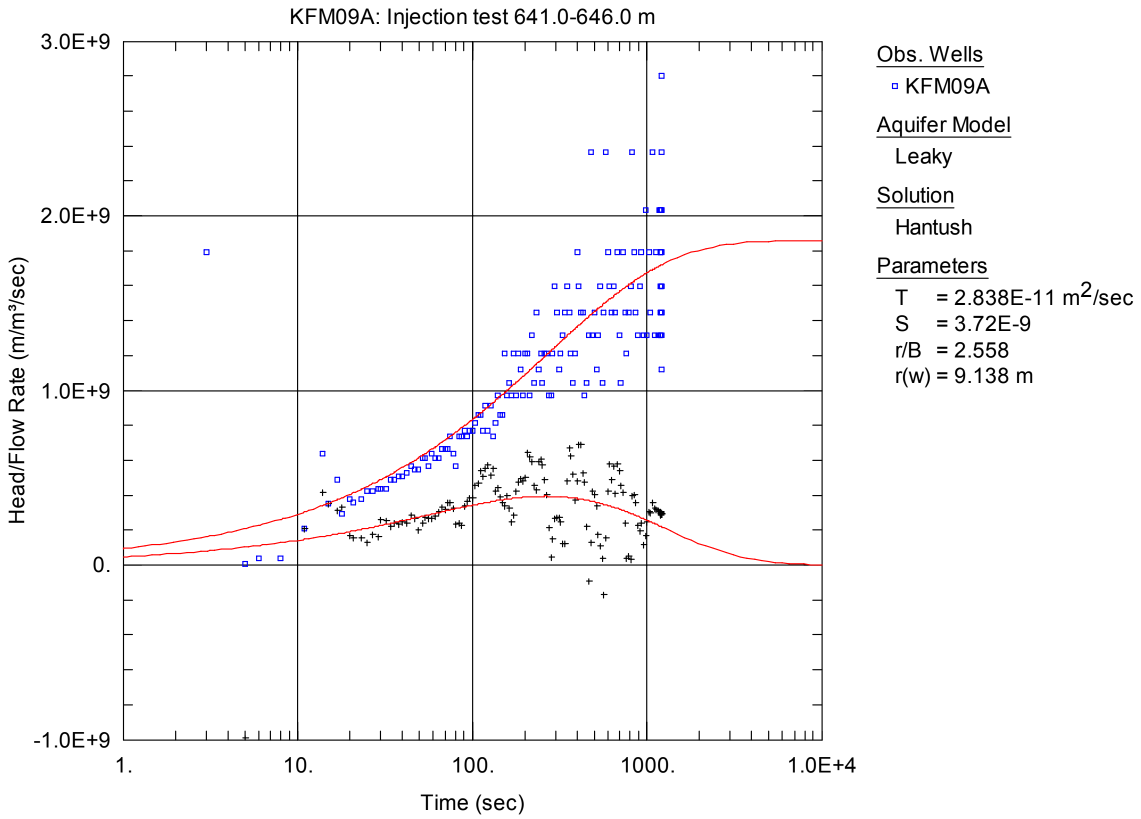


Figure A3-536. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 641.0-646.0 m in KFM09A.*

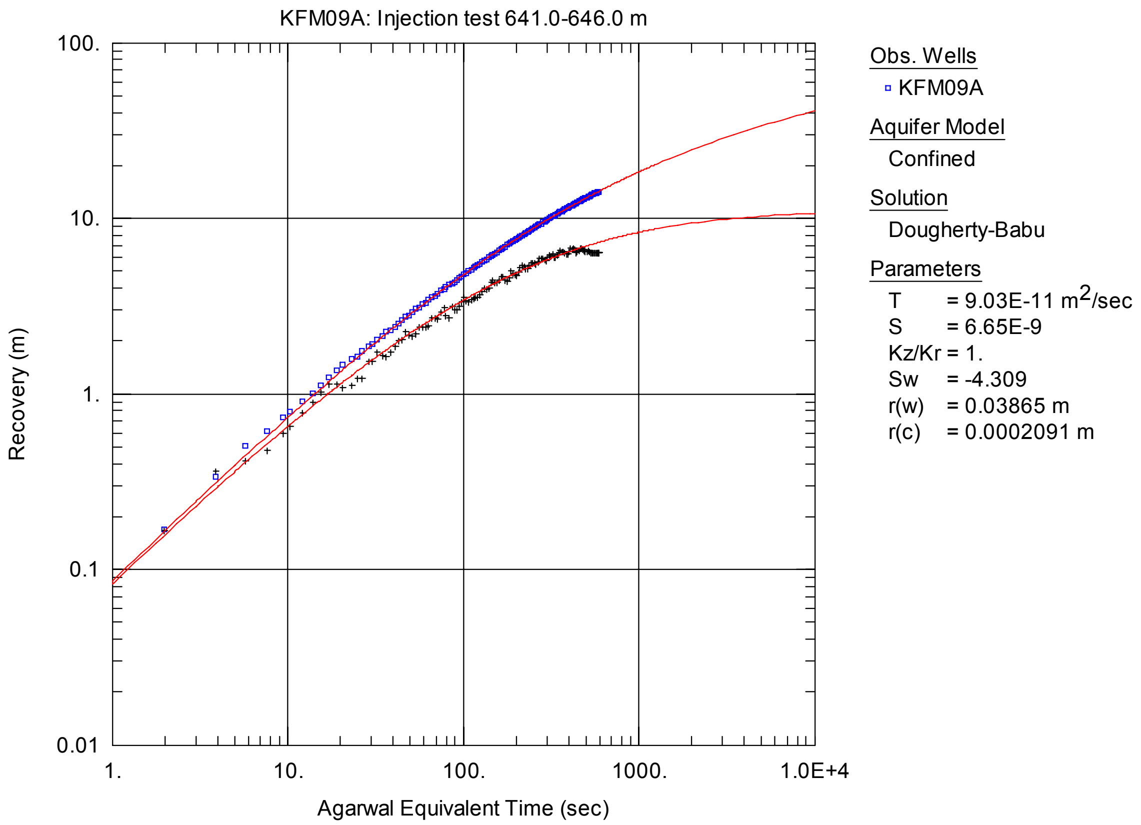


Figure A3-537. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 641.0-646.0 m in KFM09A.*

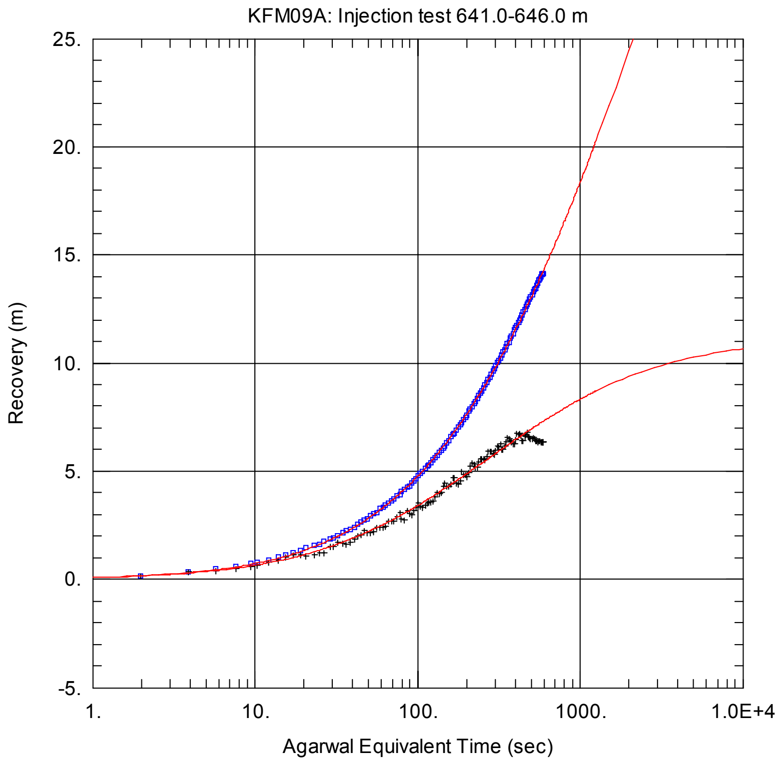


Figure A3-538. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 641.0-646.0 m in KFM09A.*

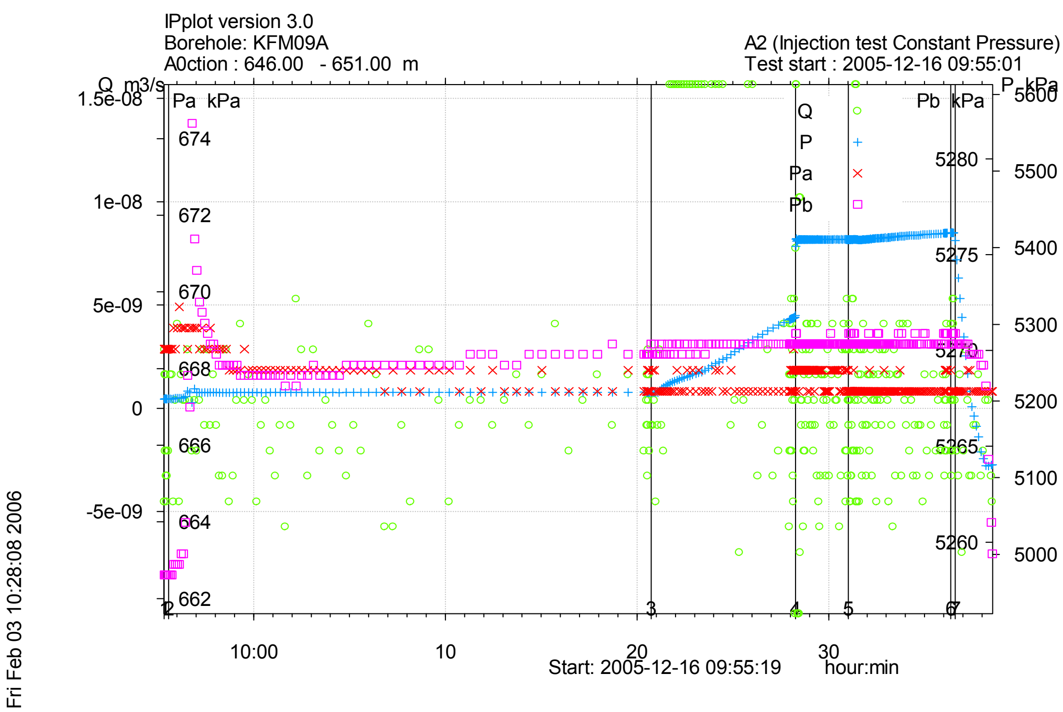


Figure A3-539. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 646.0-651.0 m in borehole KFM09A.*

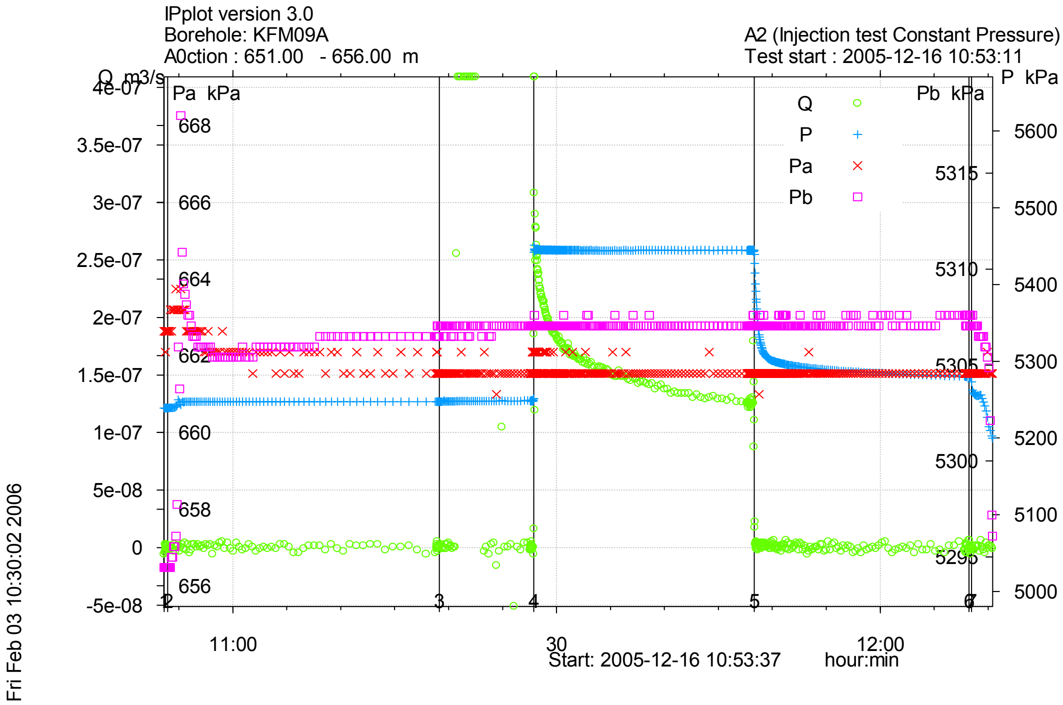


Figure A3-540. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 651.0-656.0 m in borehole KFM09A.*

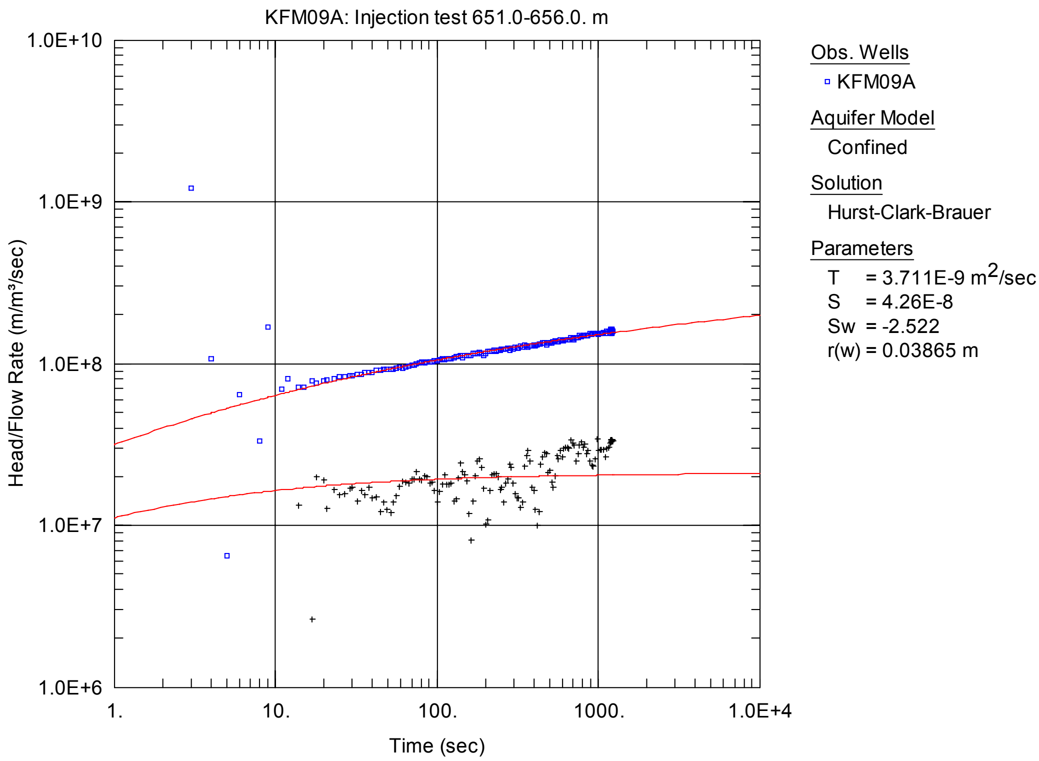


Figure A3-541. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 651.0-656.0 m in KFM09A.*

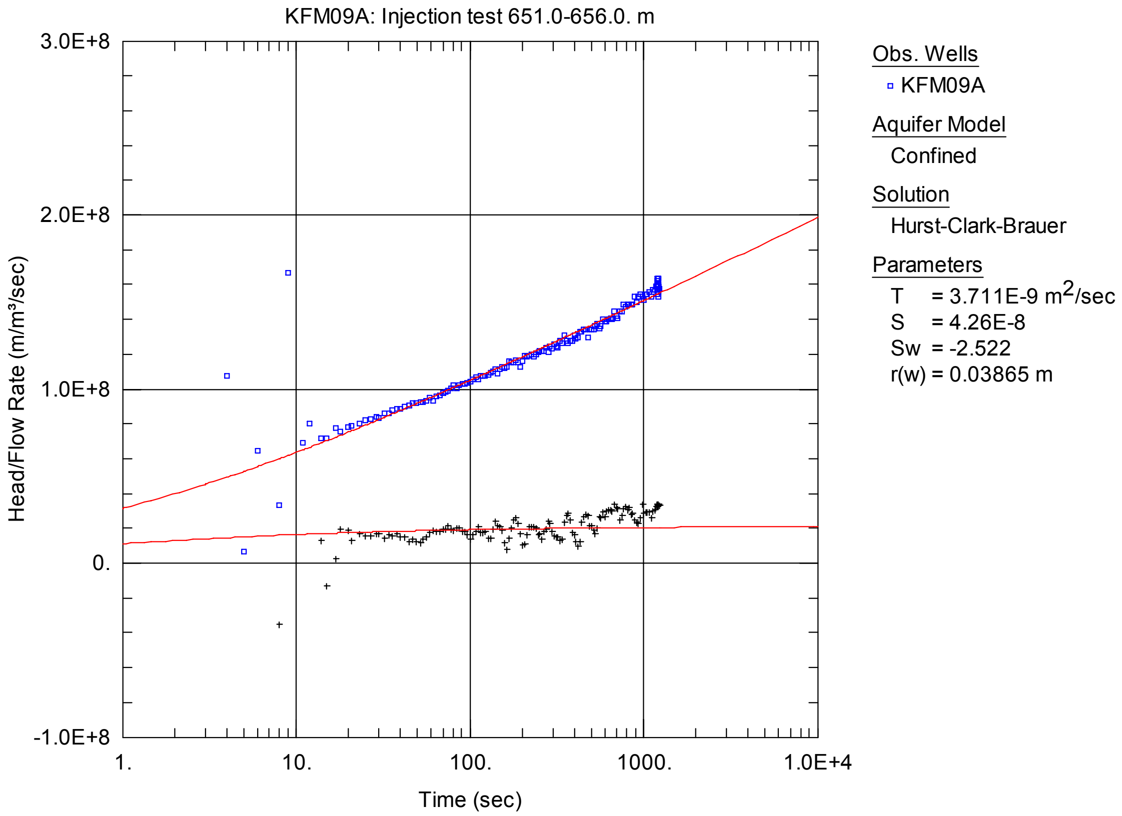


Figure A3-542. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 651.0-656.0 m in KFM09A.*

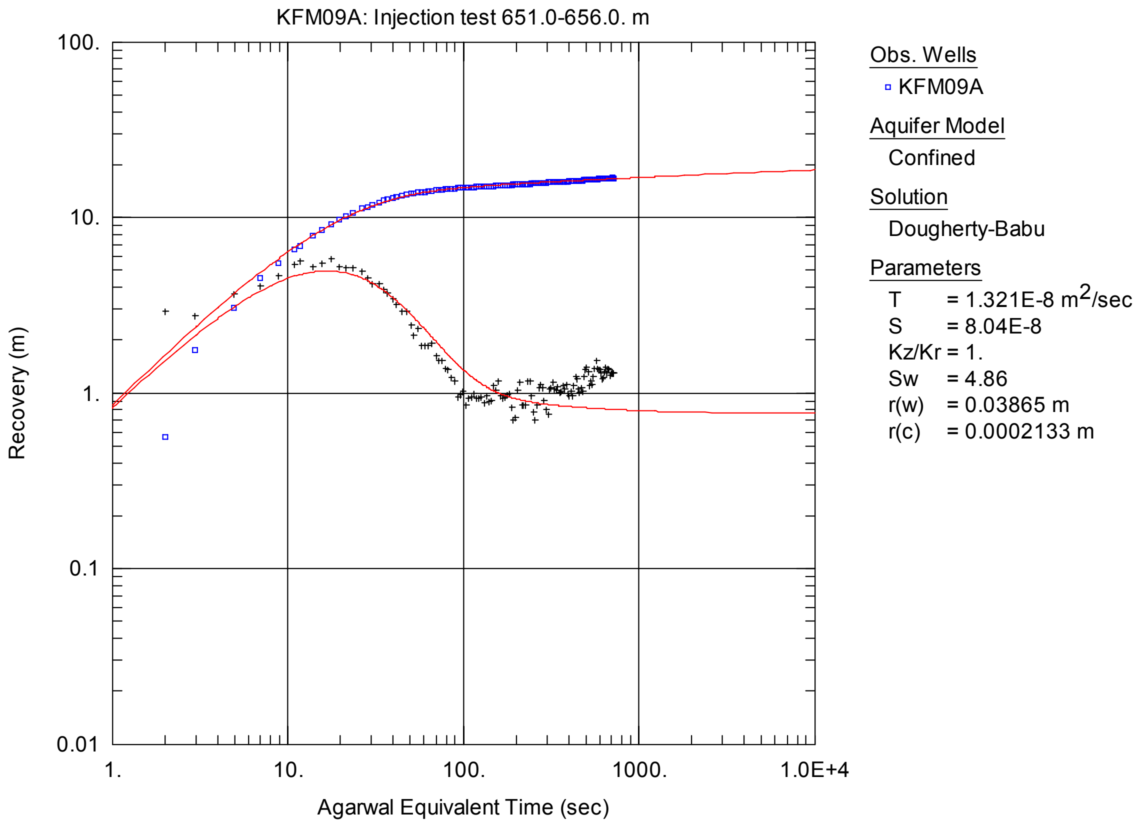


Figure A3-543. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 651.0-656.0 m in KFM09A.*

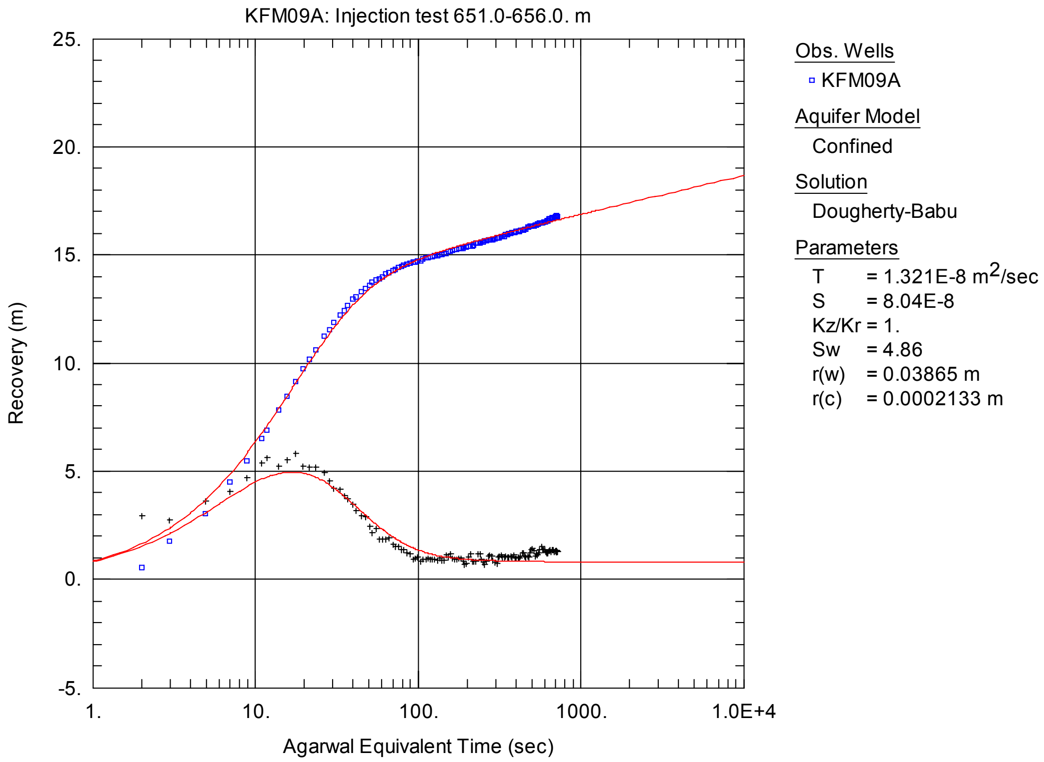


Figure A3-544. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 651.0-656.0 m in KFM09A.*

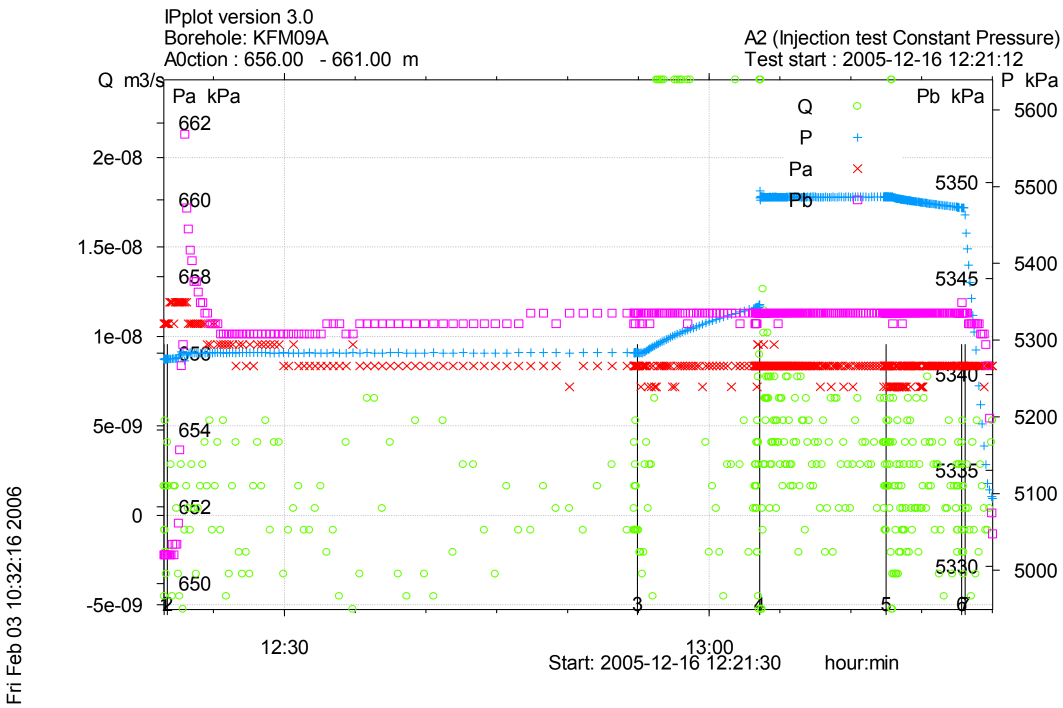


Figure A3-545. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 656.0-661.0 m in borehole KFM09A.*

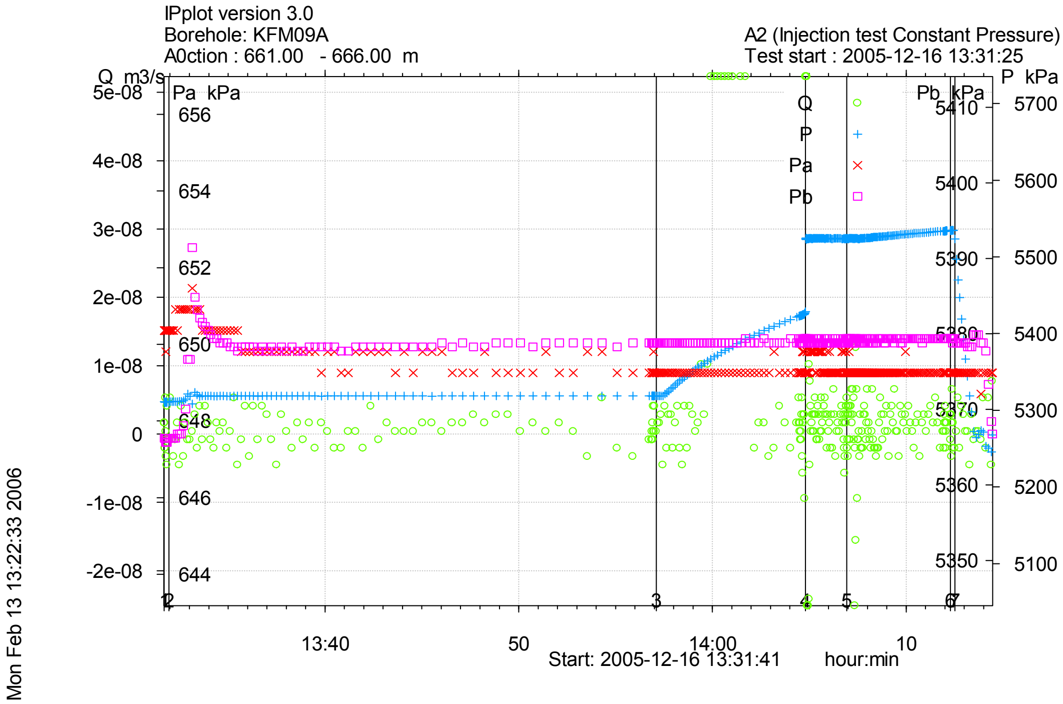


***Figure A3-546.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 661.0-666.0 m in borehole KFM09A.*

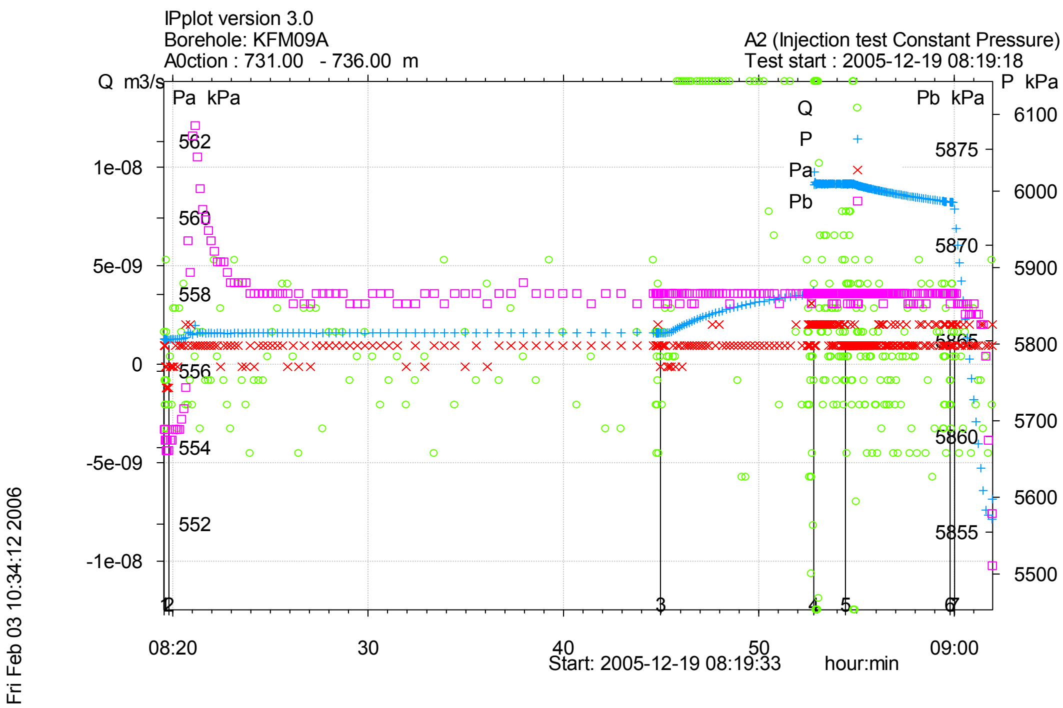


***Figure A3-547.** Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 731.0-736.0 m in borehole KFM09A.*

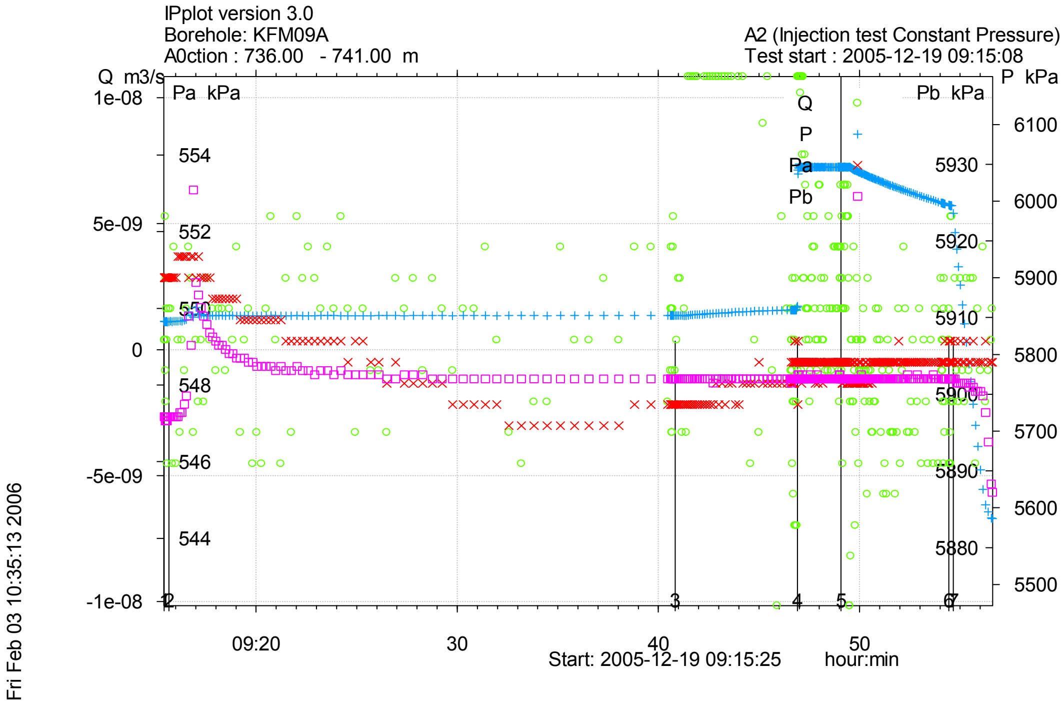


Figure A3-548. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 736.0-741.0 m in borehole KFM09A.*

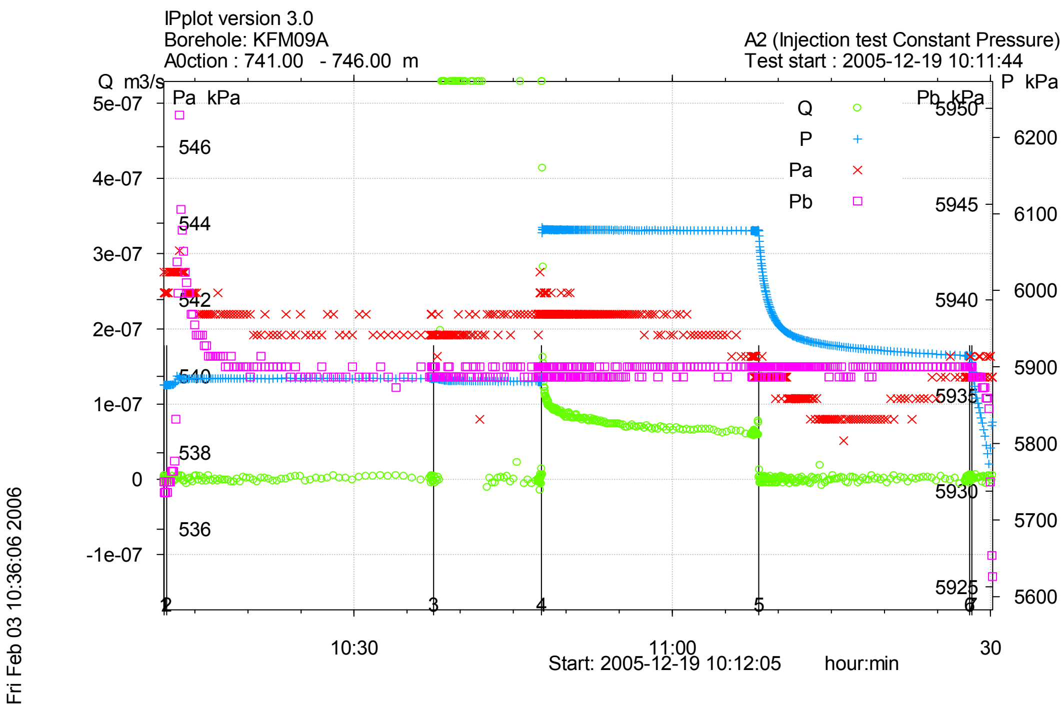


Figure A3-549. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 741.0-746.0 m in borehole KFM09A.*

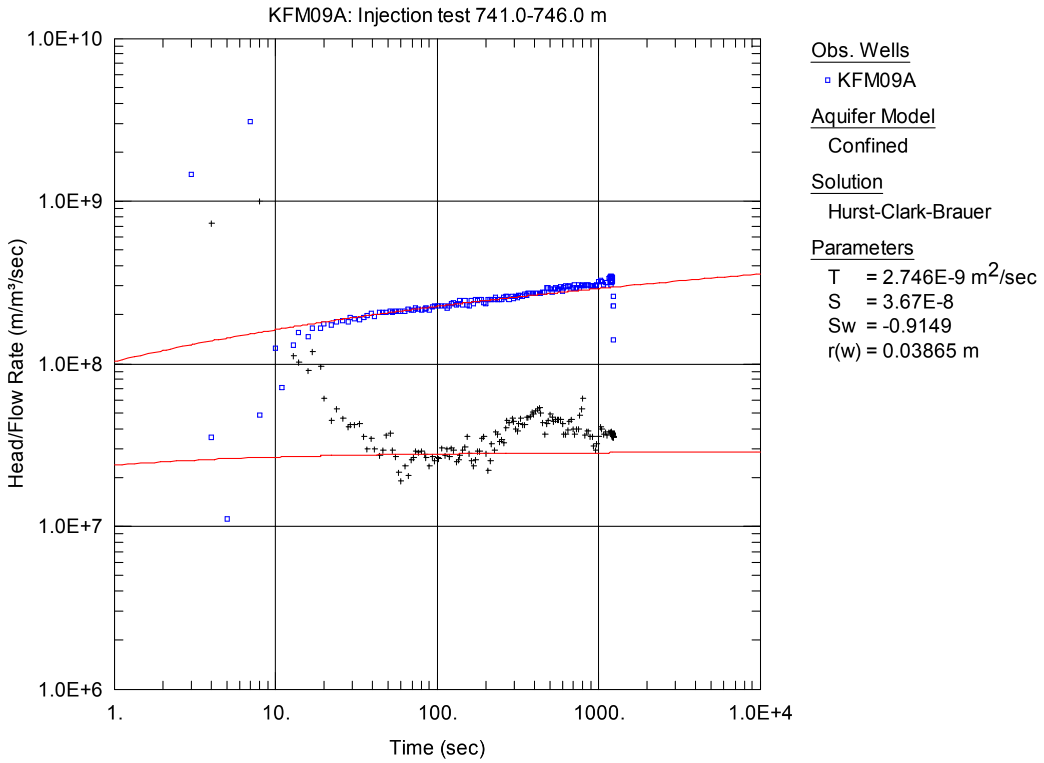


Figure A3-550. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 741.0-746.0 m in KFM09A. This plot shows a fit to the first of two different PRF:s during the injection period in this section.*

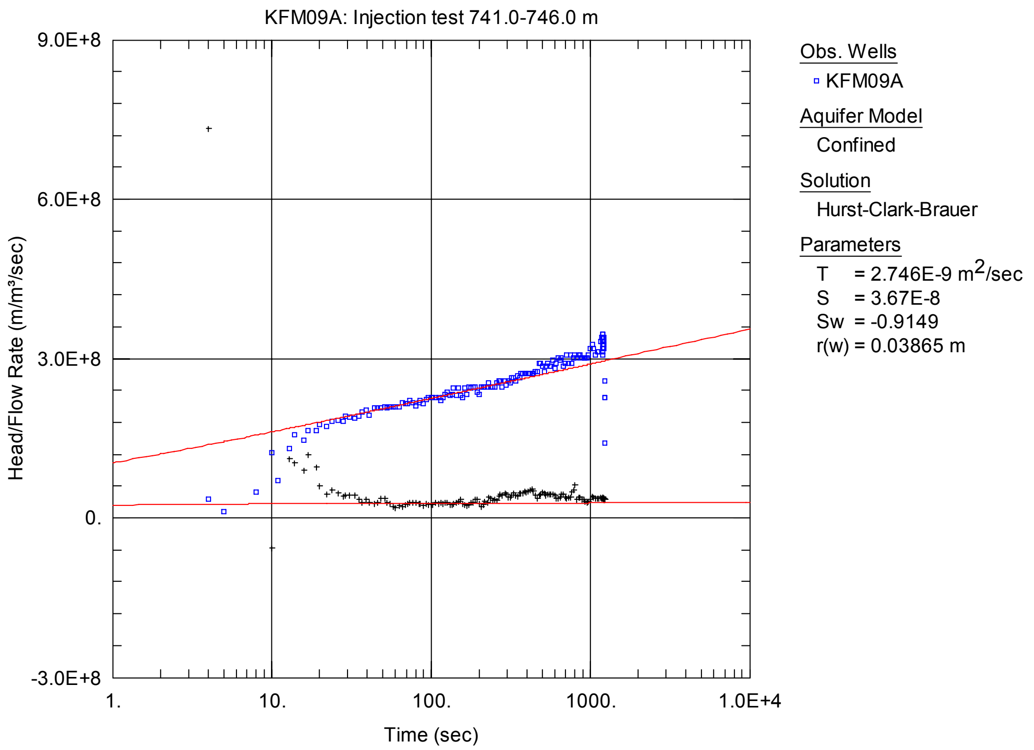


Figure A3-551. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 741.0-746.0 m in KFM09A. This plot shows a fit to the first of two different PRF:s during the injection period in this section.*

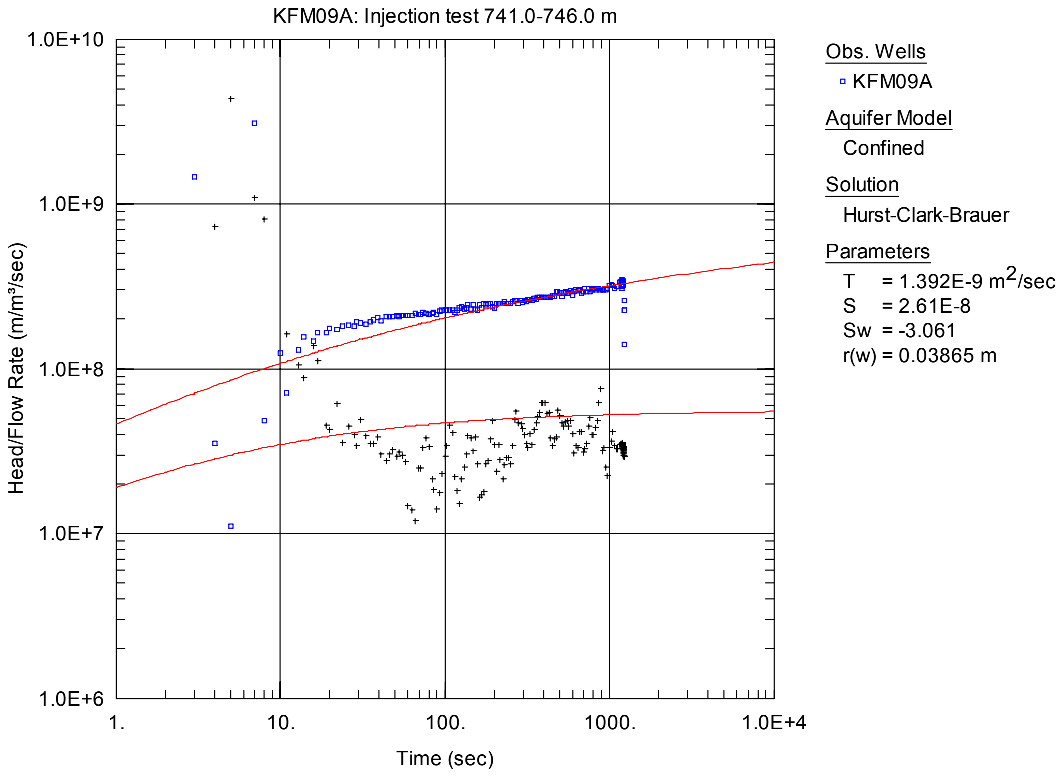


Figure A3-552. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 741.0-746.0 m in KFM09A. This plot shows a fit to the second of two different PRF:s during the injection period in this section.*

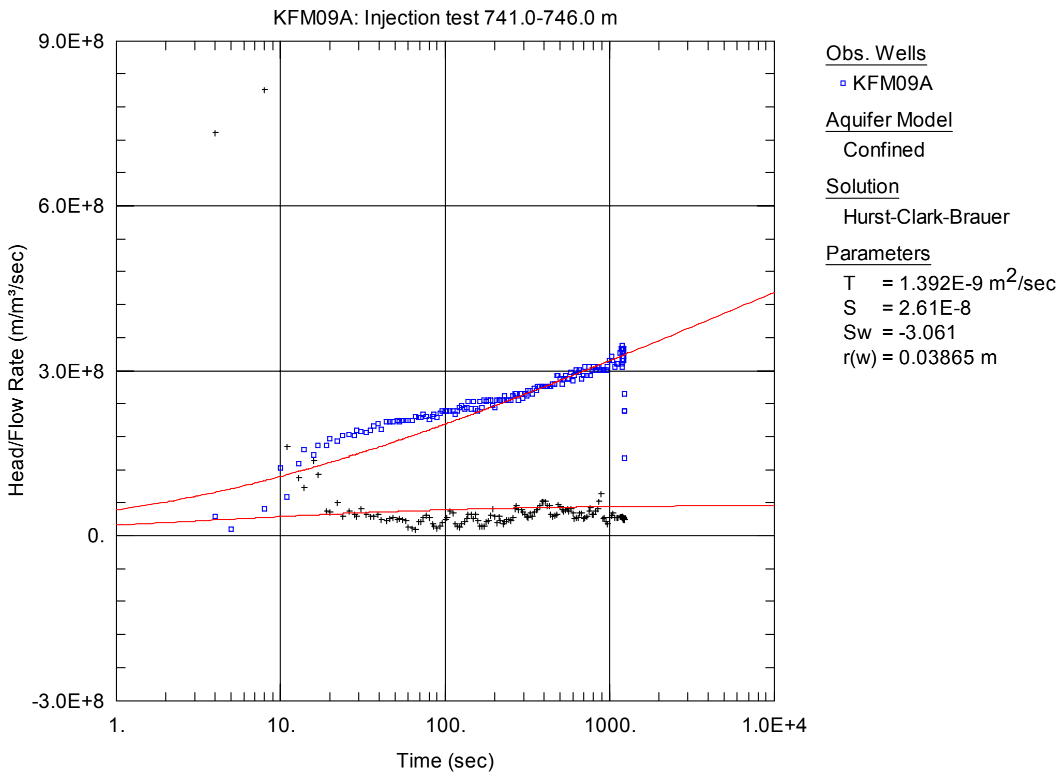


Figure A3-553. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 741.0-746.0 m in KFM09A. This plot shows a fit to the second of two different PRF:s during the injection period in this section.*

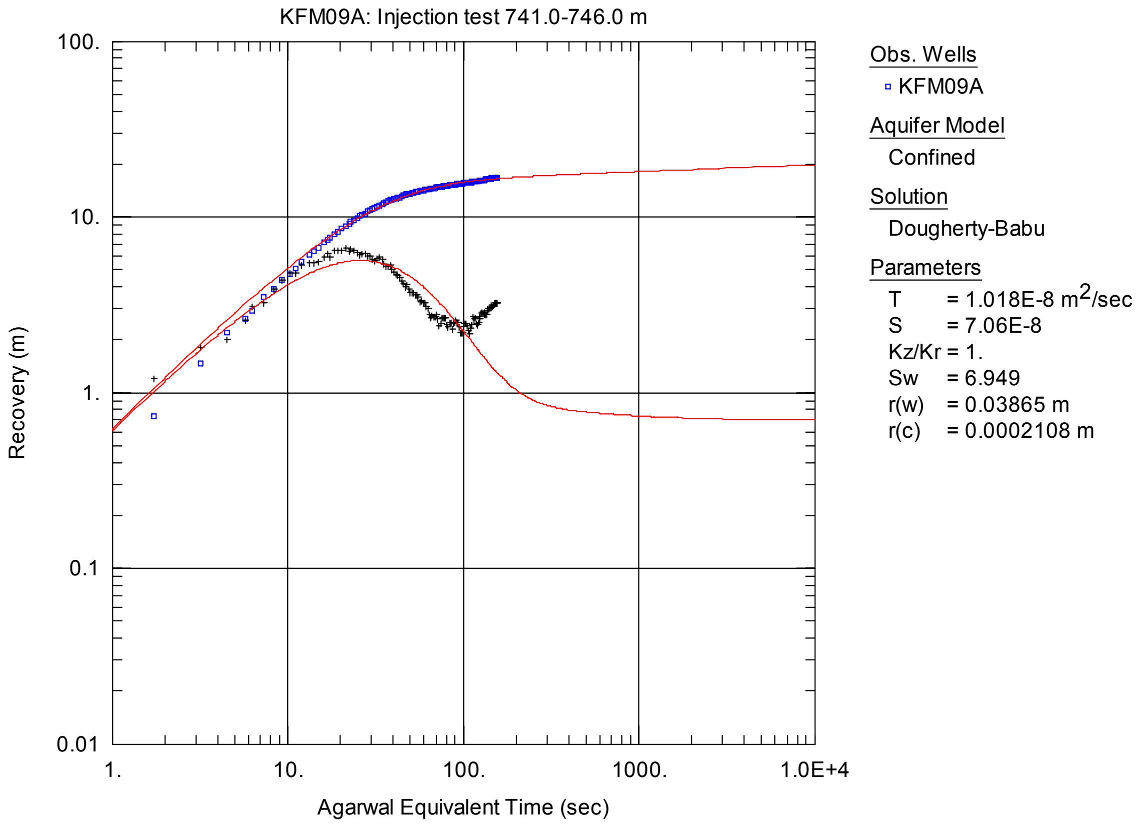


Figure A3-554. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 741.0-746.0 m in KFM09A.*

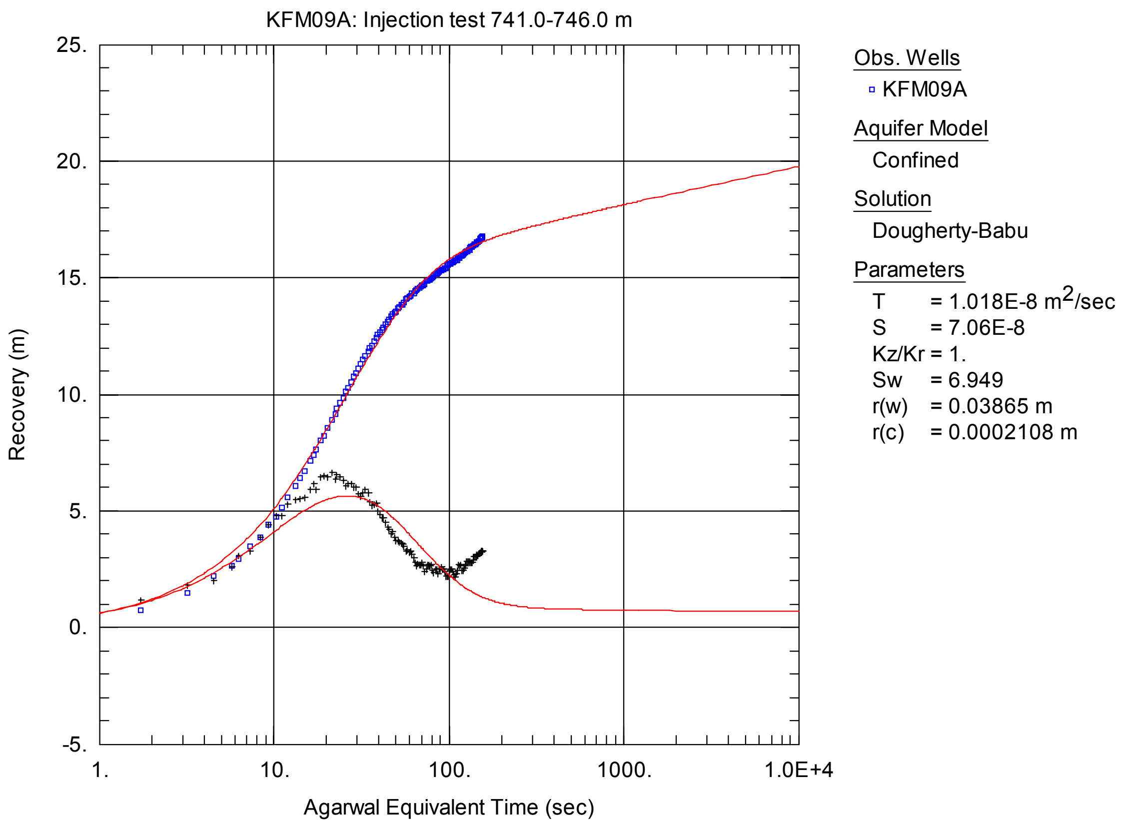


Figure A3-555. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 741.0-746.0 m in KFM09A.*

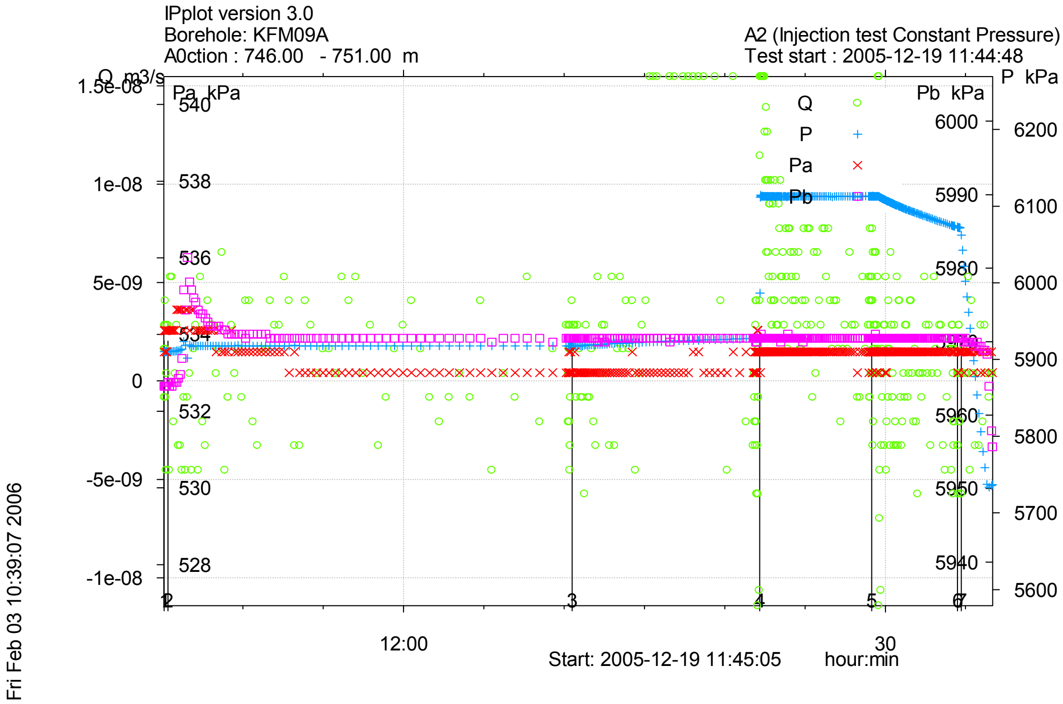


Figure A3-556. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 746.0-751.0 m in borehole KFM09A.

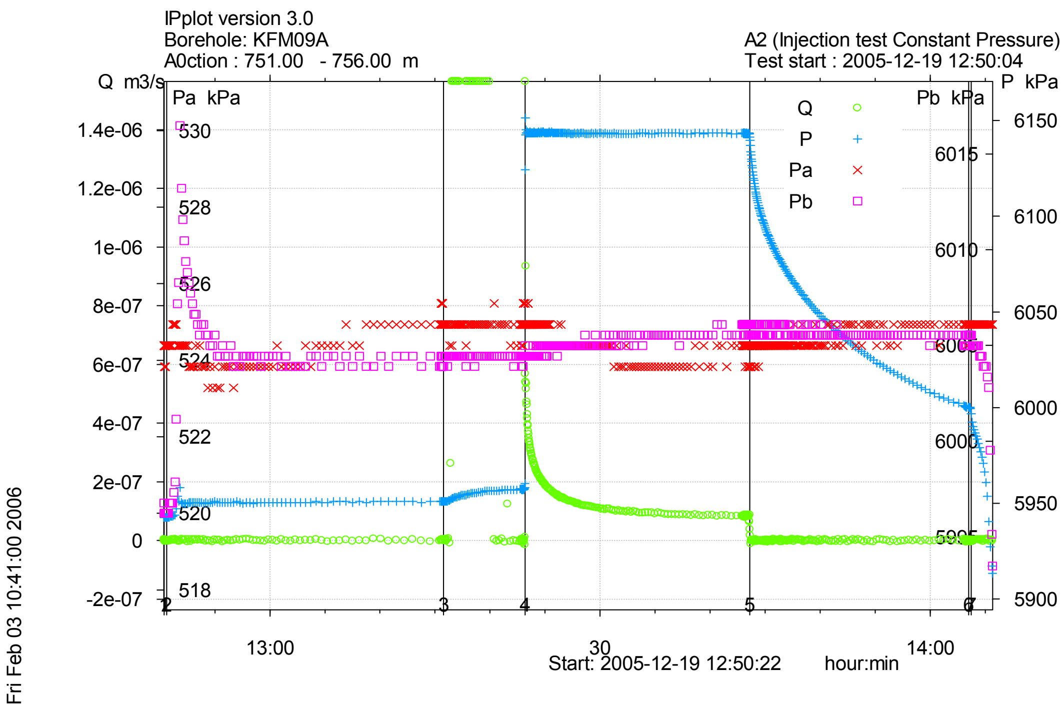


Figure A3-557. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 751.0-756.0 m in borehole KFM09A.

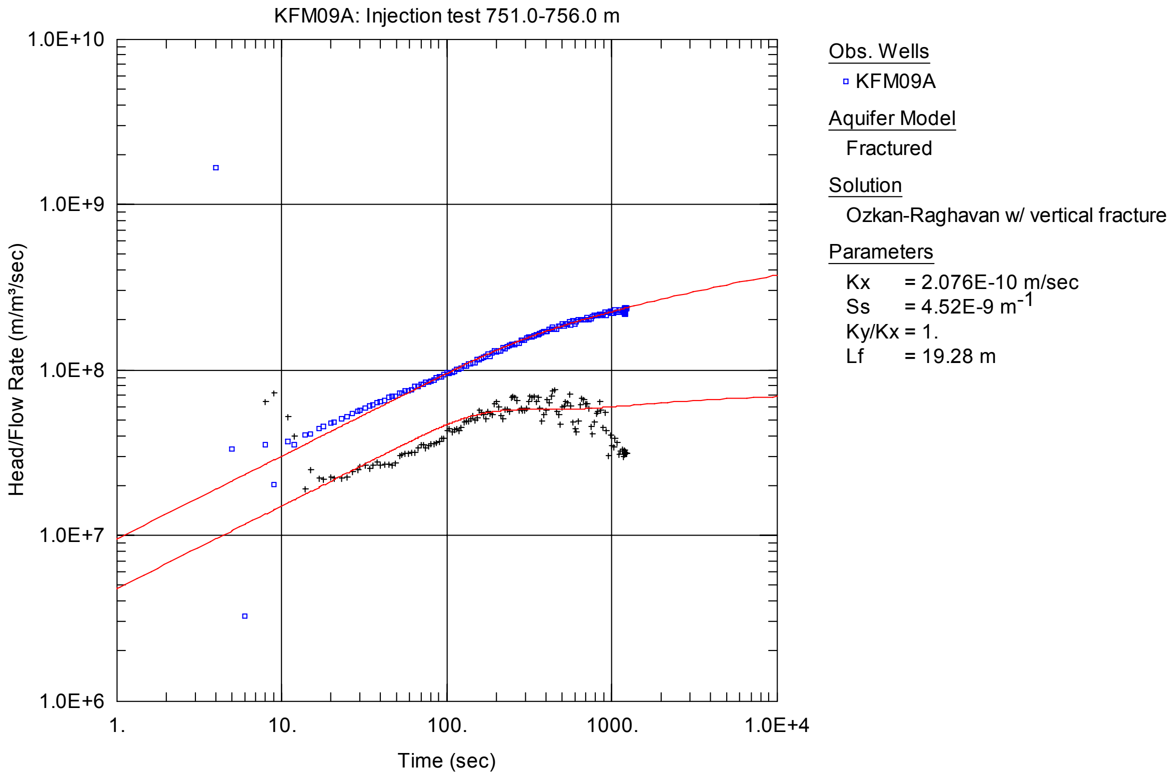


Figure A3-558. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 751.0-756.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

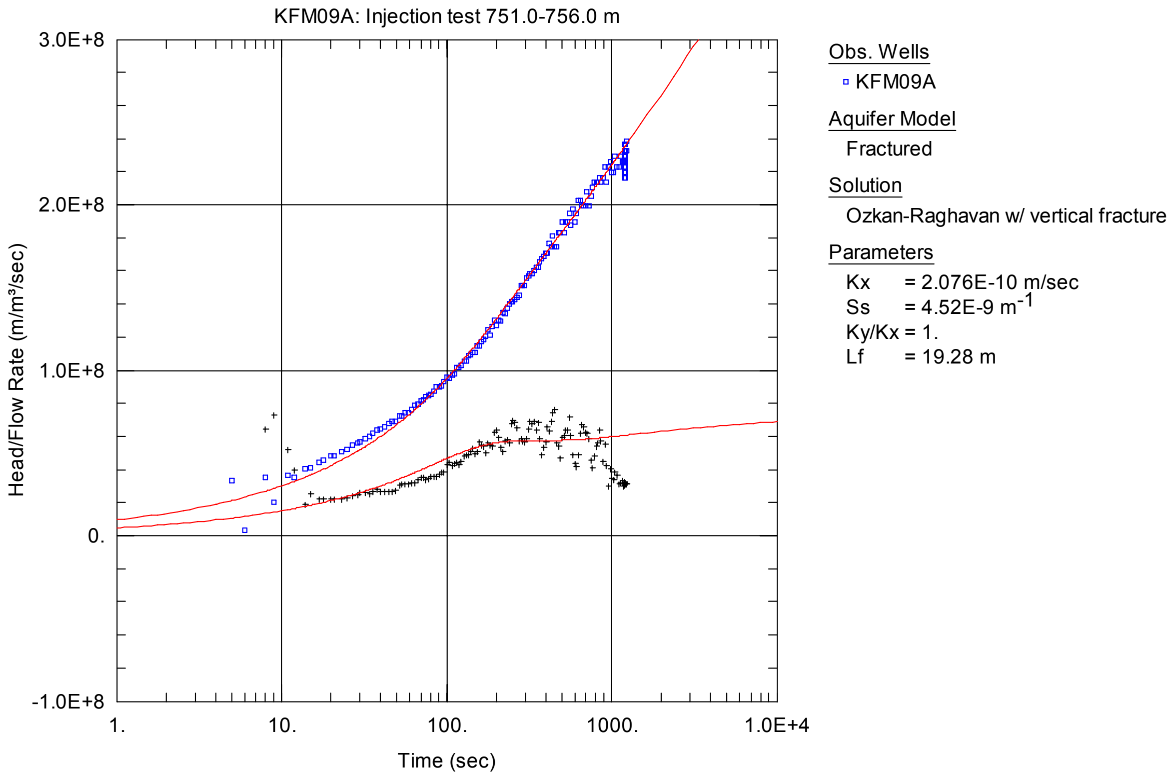


Figure A3-559. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 751.0-756.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

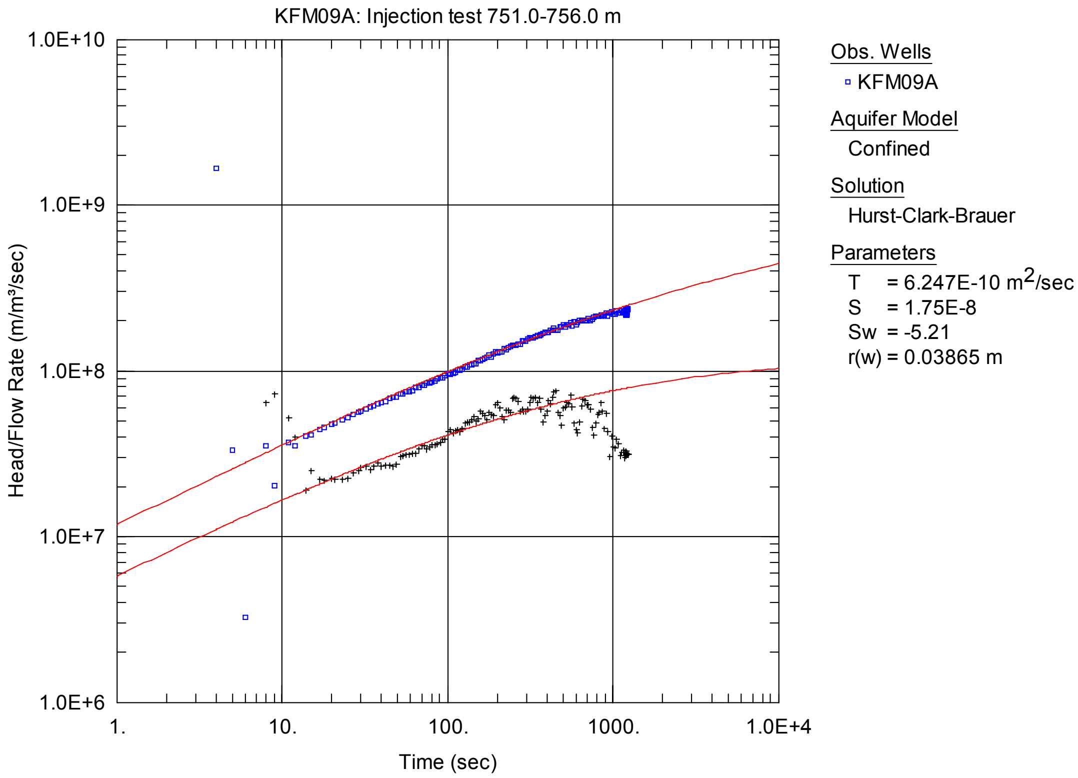


Figure A3-560. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 751.0-756.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for a pseudo-radial response.*

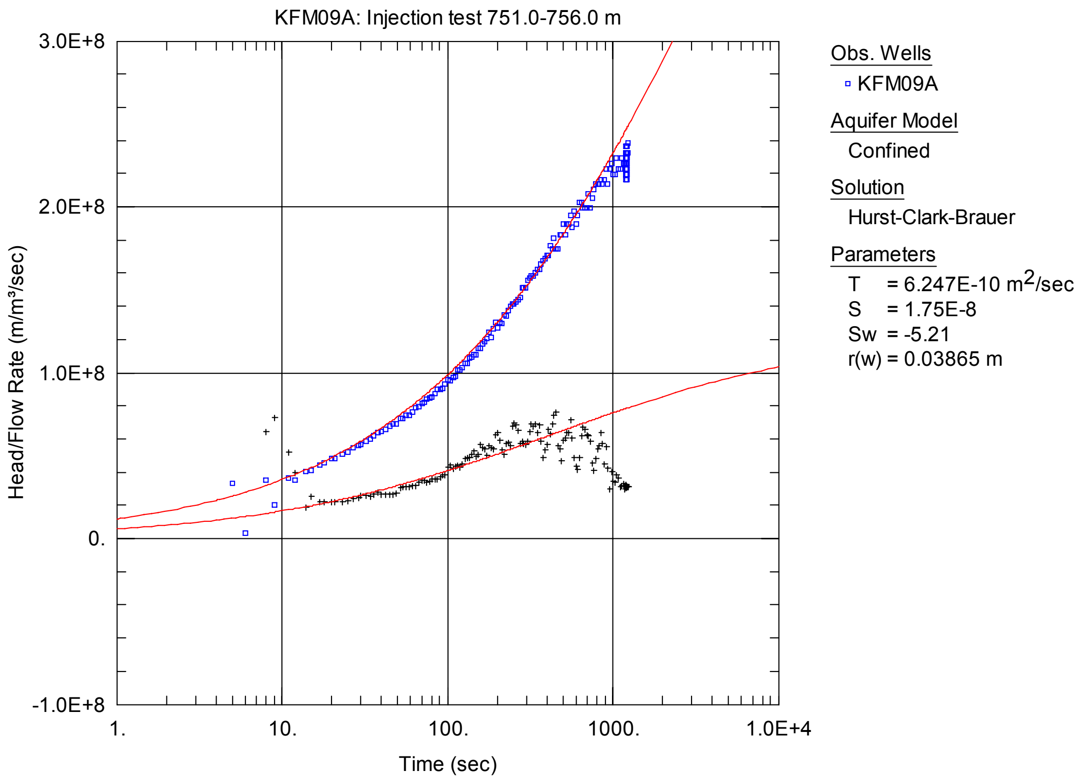


Figure A3-561. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 751.0-756.0 m in KFM09A. This evaluation is made with the Hurst-Clark-Brauer model for a pseudo-radial response.*

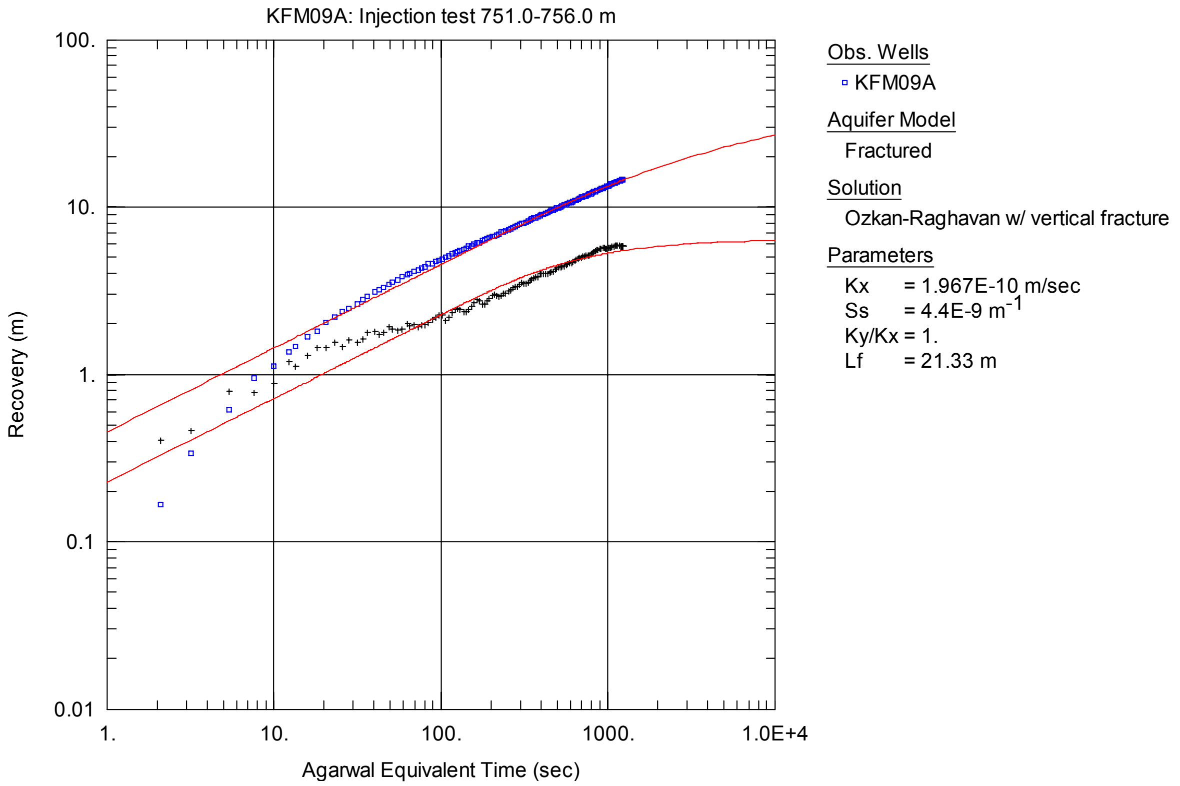


***Figure A3-562.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 751.0-756.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

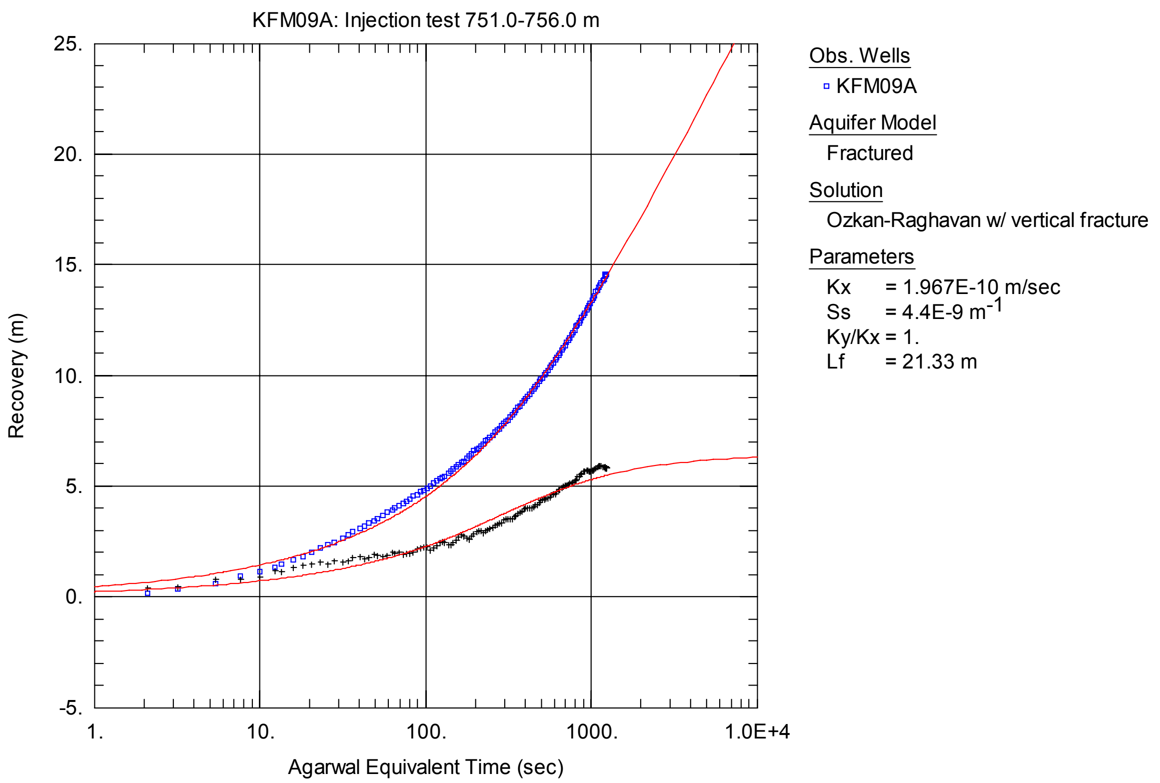


***Figure A3-563.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 751.0-756.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

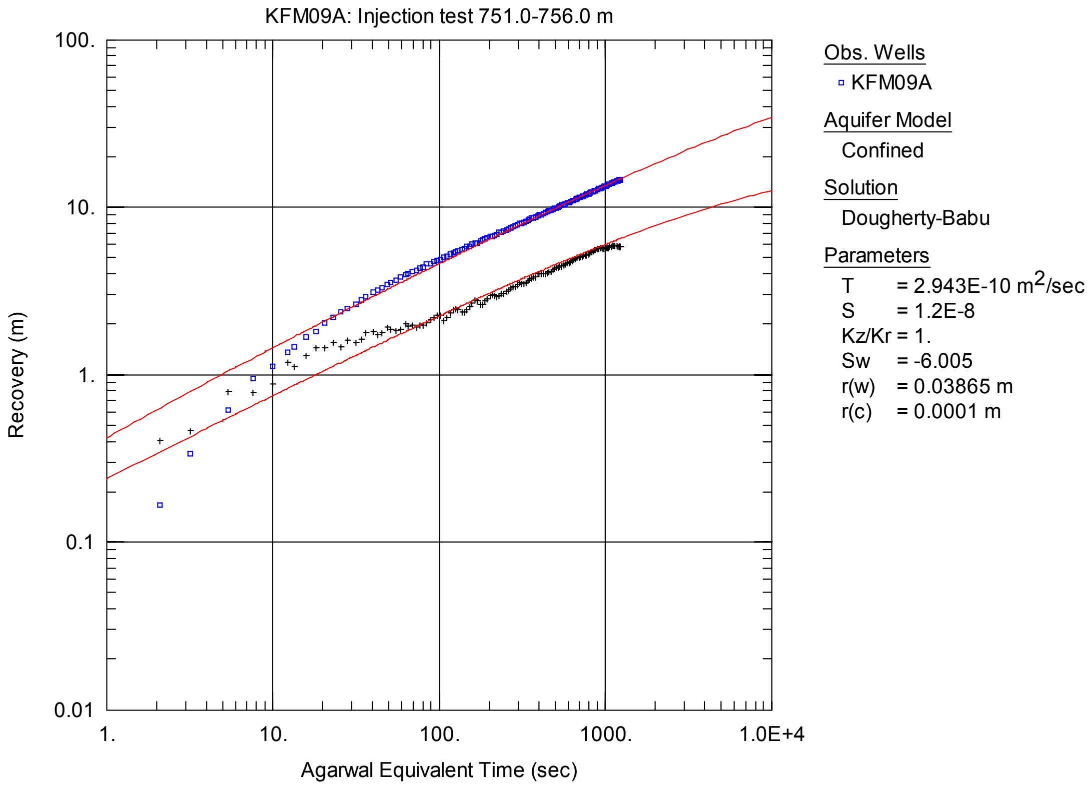


Figure A3-564. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 751.0-756.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

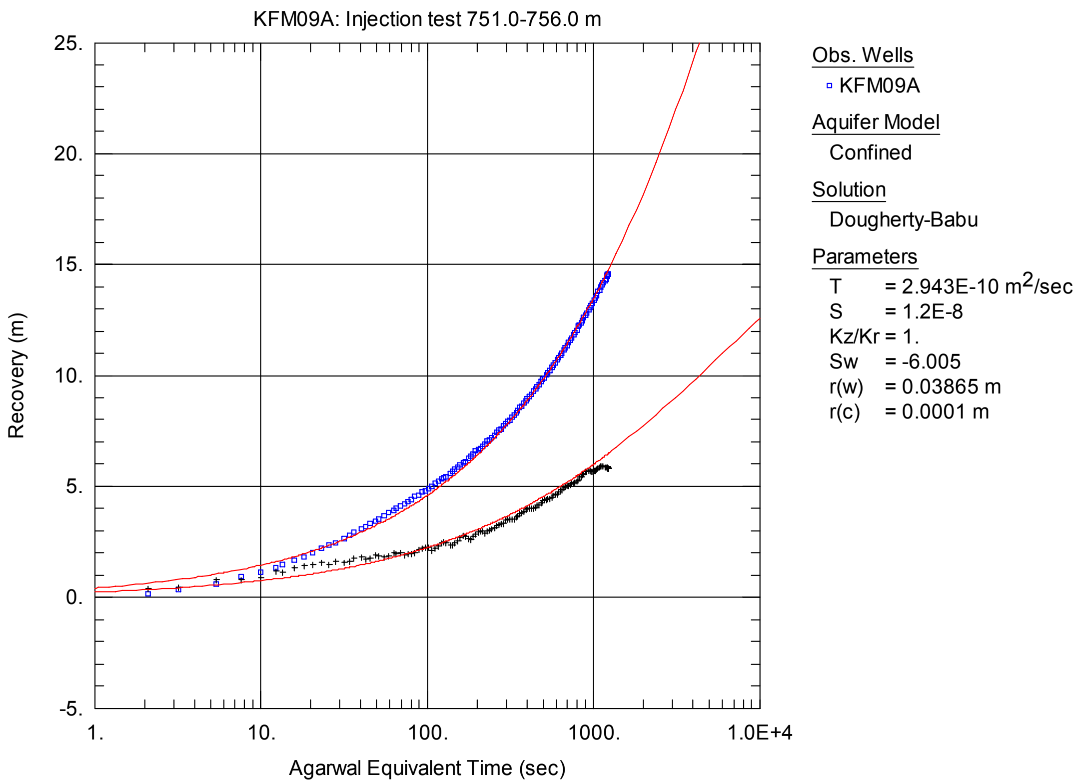


Figure A3-565. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 751.0-756.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

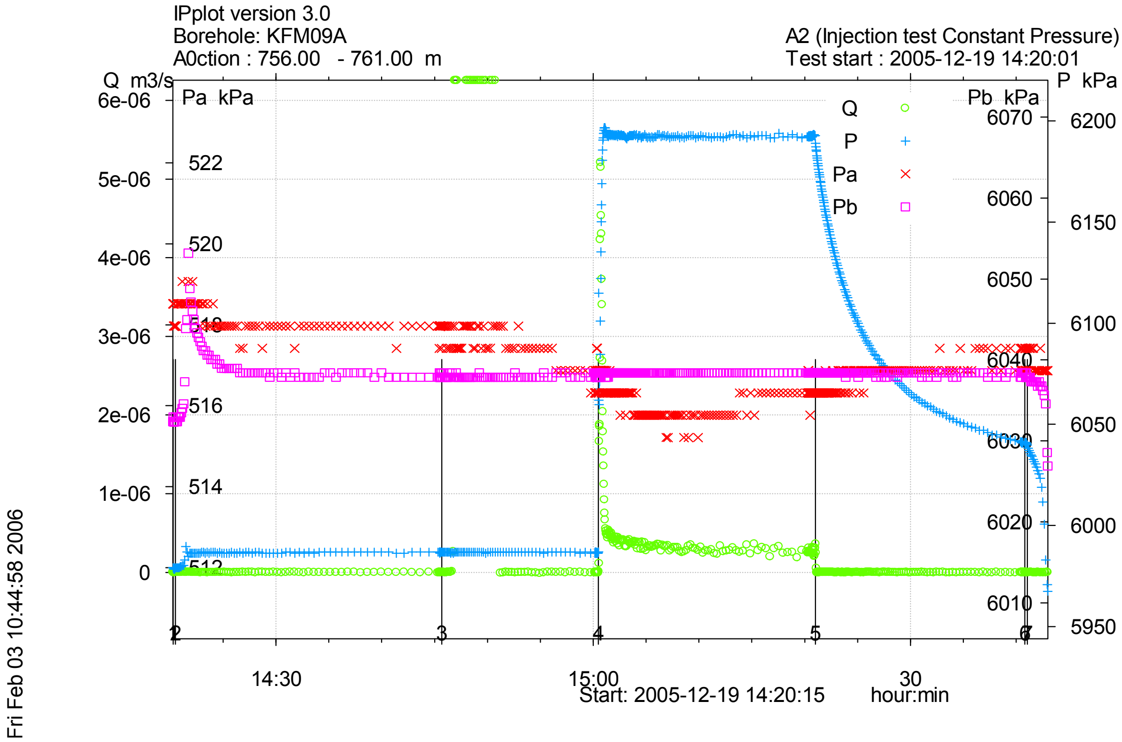


Figure A3-566. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 756.0-761.0 m in borehole KFM09A.*

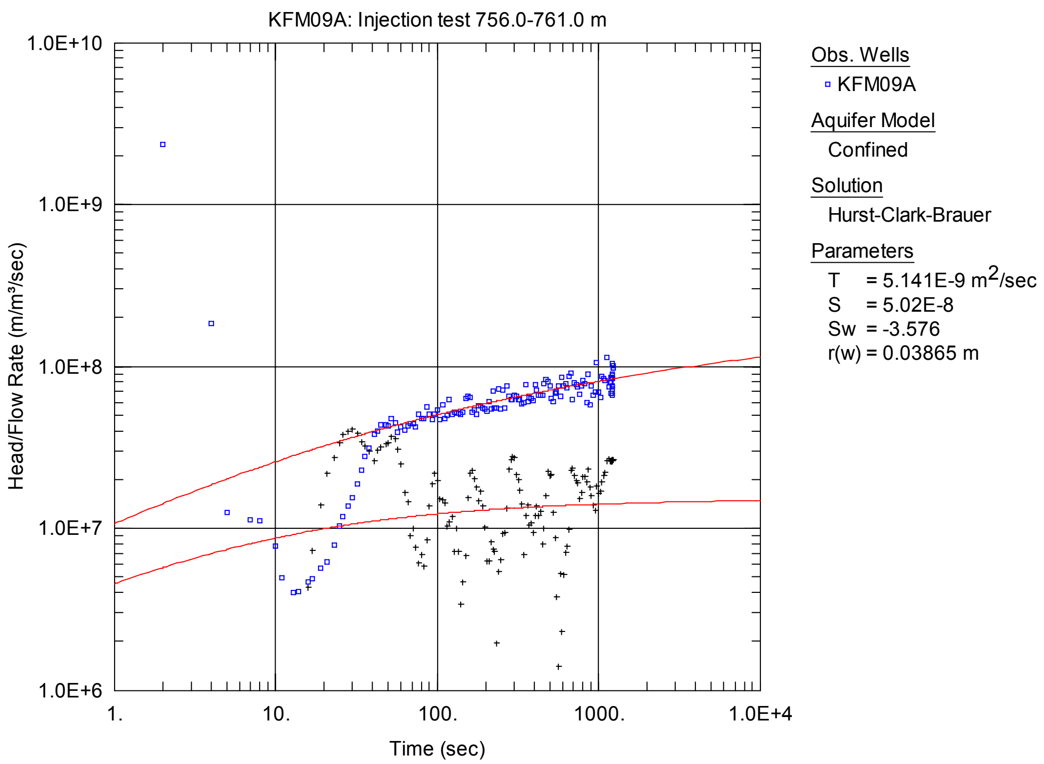


Figure A3-567. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 756.0-761.0 m in KFM09A.*

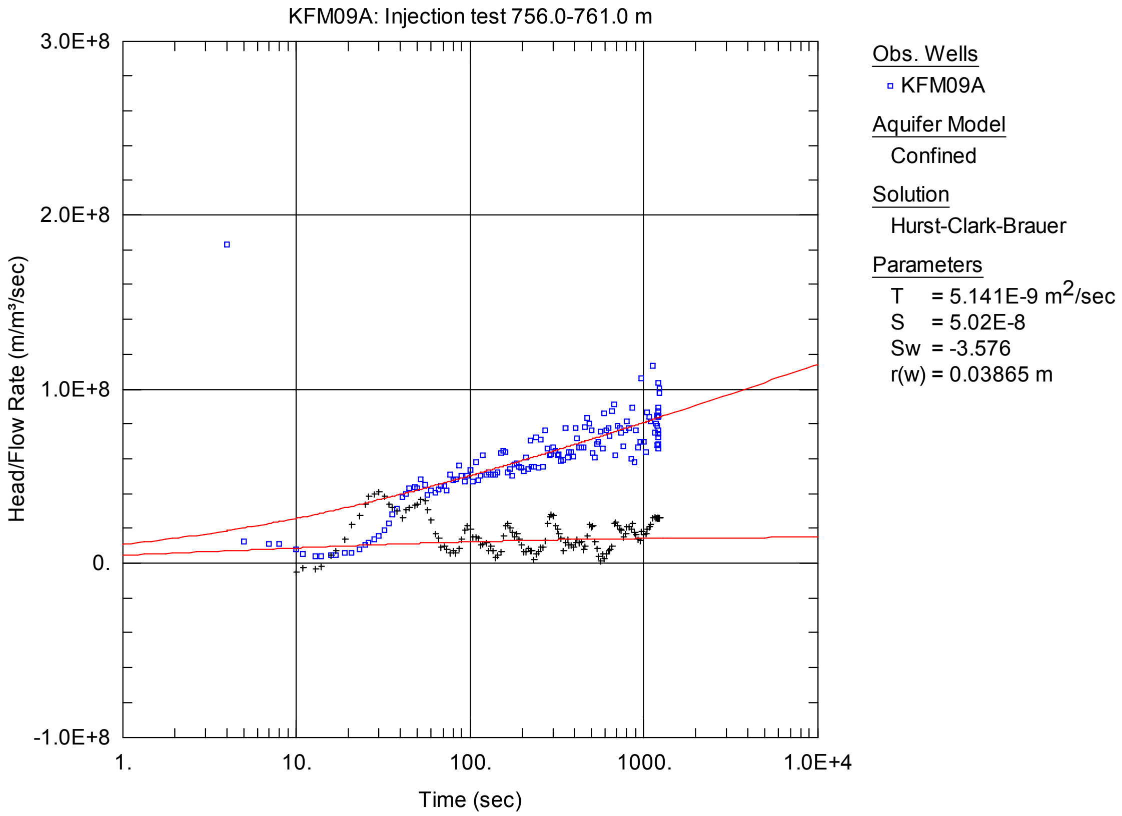


Figure A3-568. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 756.0-761.0 m in KFM09A.*

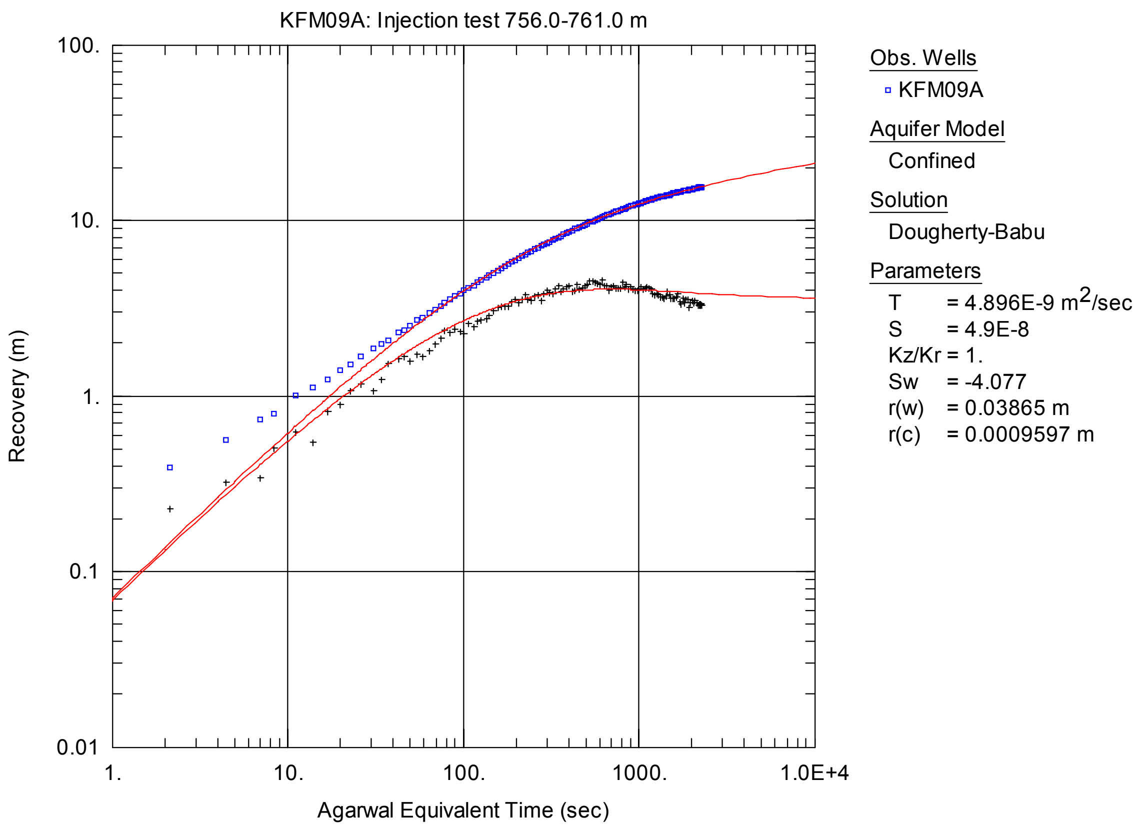


Figure A3-569. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 756.0-761.0 m in KFM09A.*

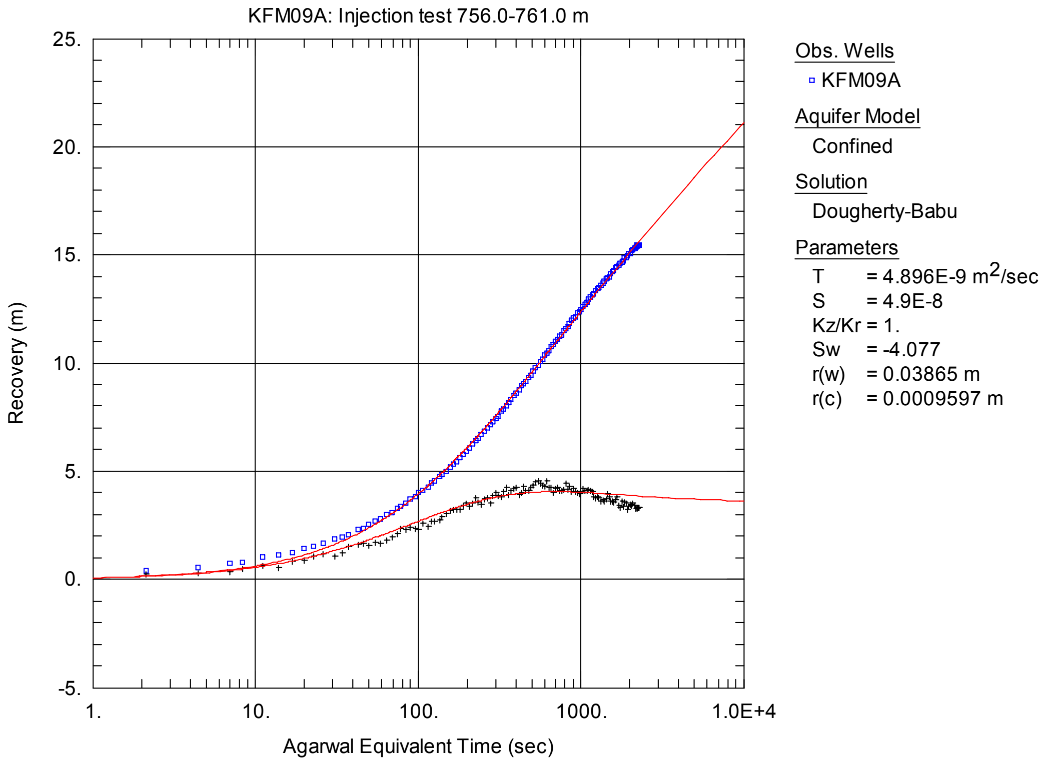


Figure A3-570. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 756.0-761.0 m in KFM09A.*

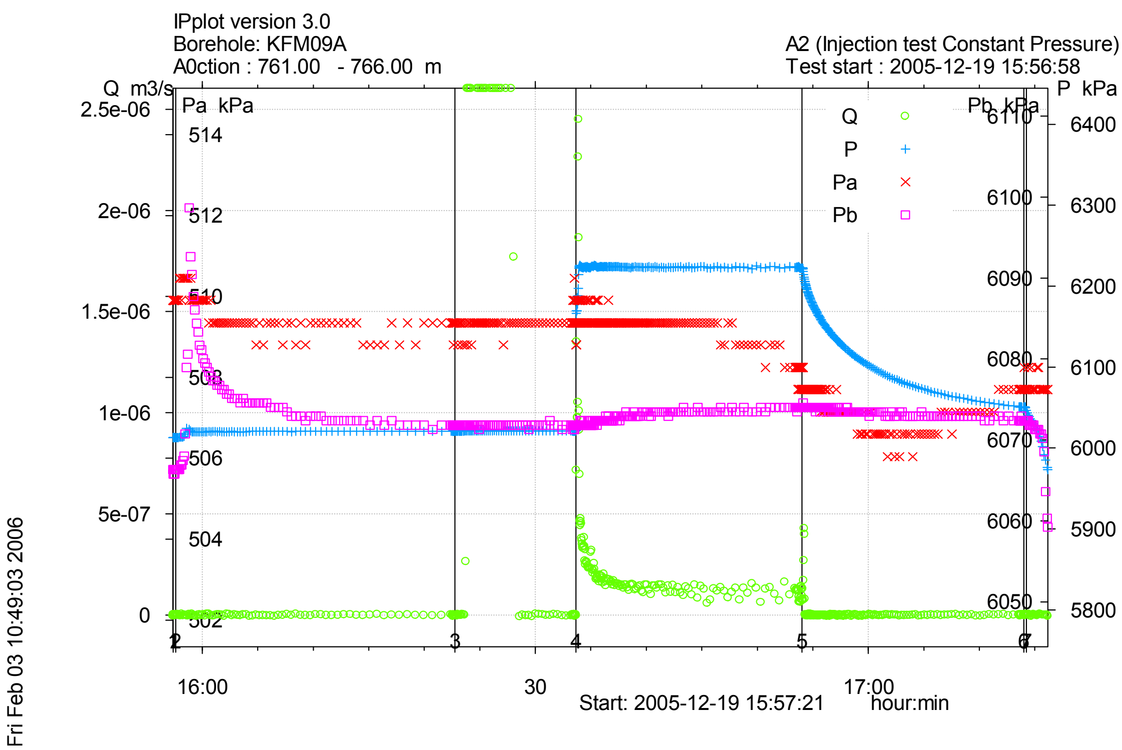


Figure A3-571. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 761.0-766.0 m in borehole KFM09A.*

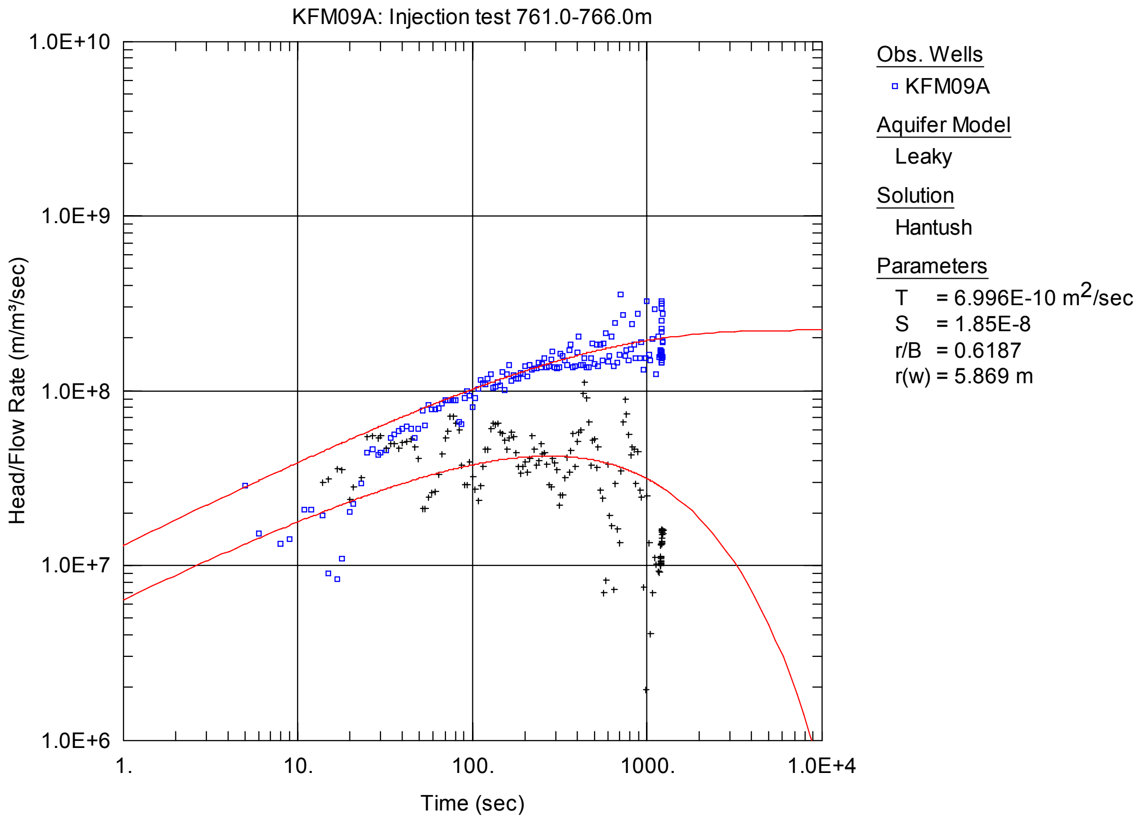


Figure A3-572. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 761.0-766.0 m in KFM09A.*

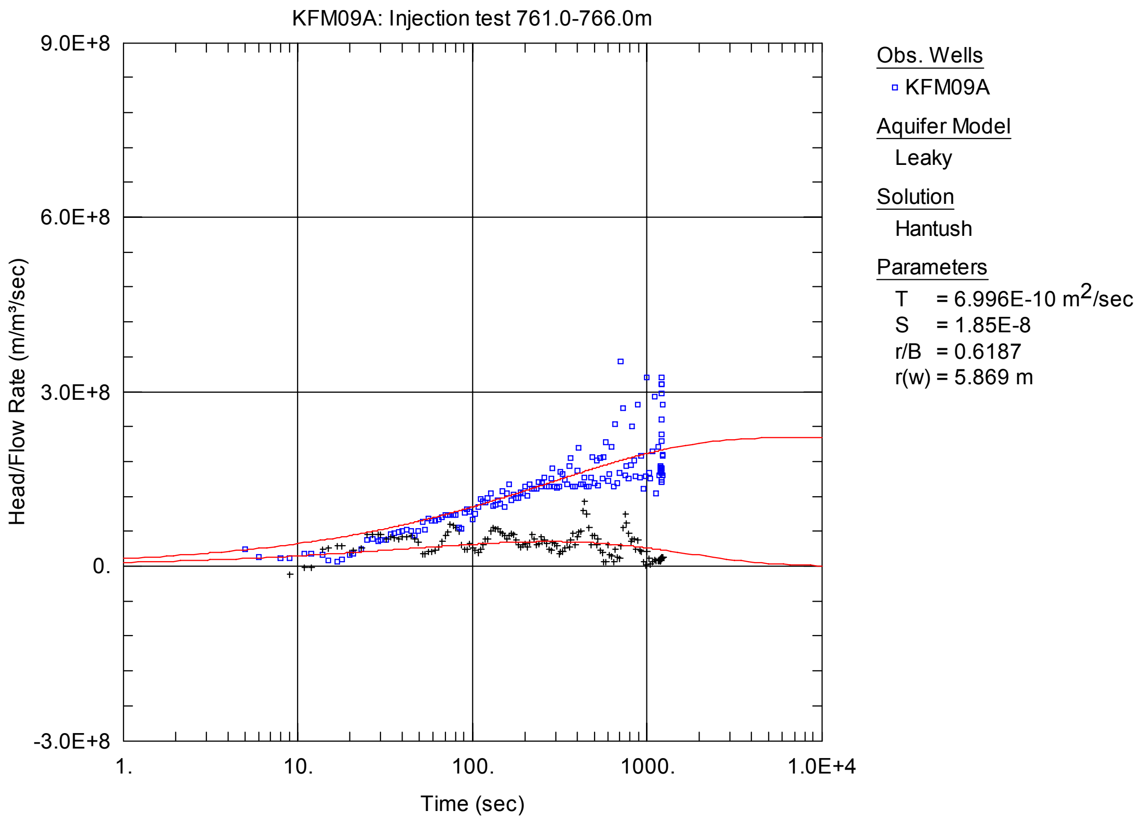


Figure A3-573. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 761.0-766.0 m in KFM09A.*

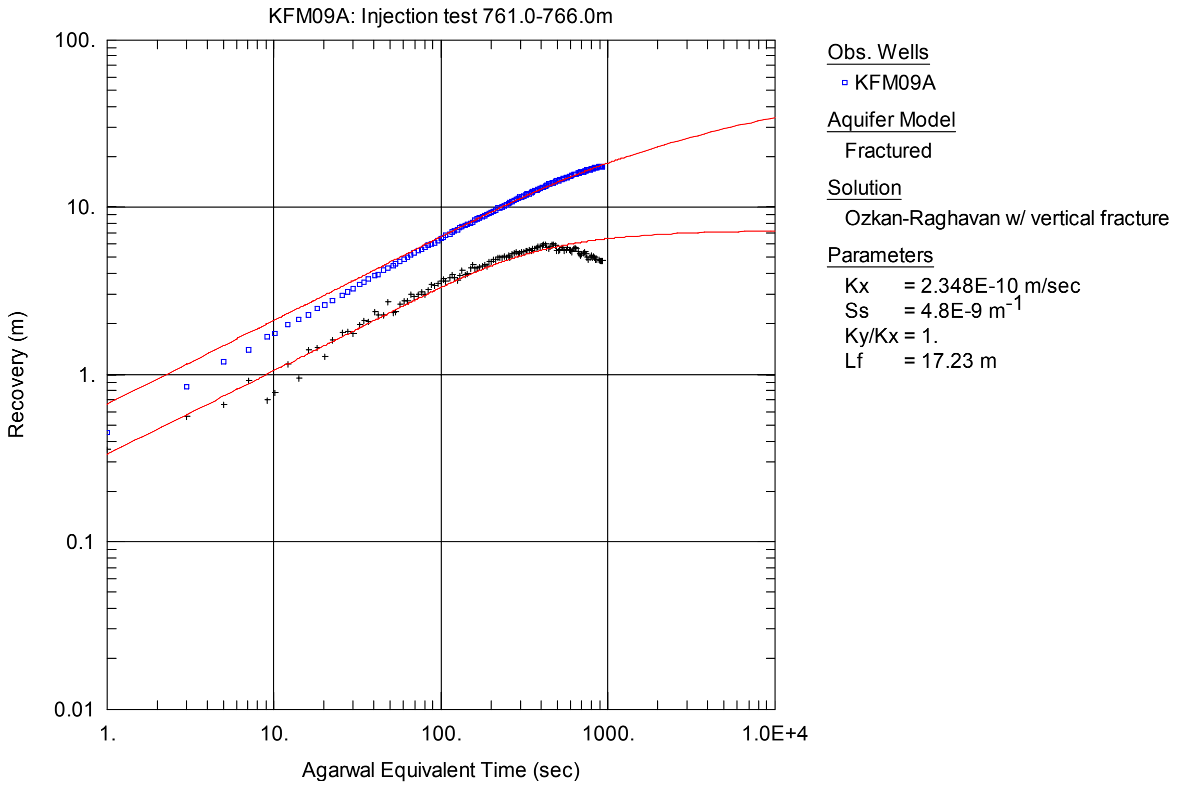


Figure A3-574. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 761.0-766.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

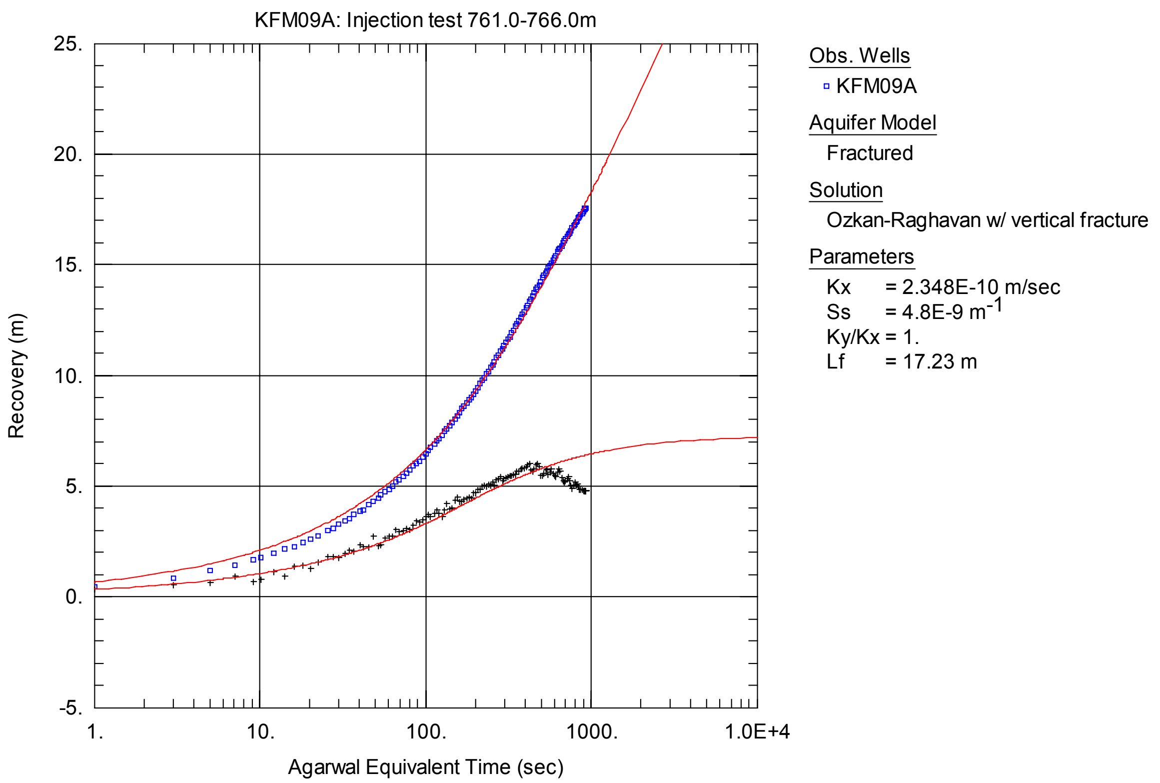


Figure A3-575. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 761.0-766.0 m in KFM09A. This evaluation is made with the Ozkan-Raghavan model for a vertical fracture response.*

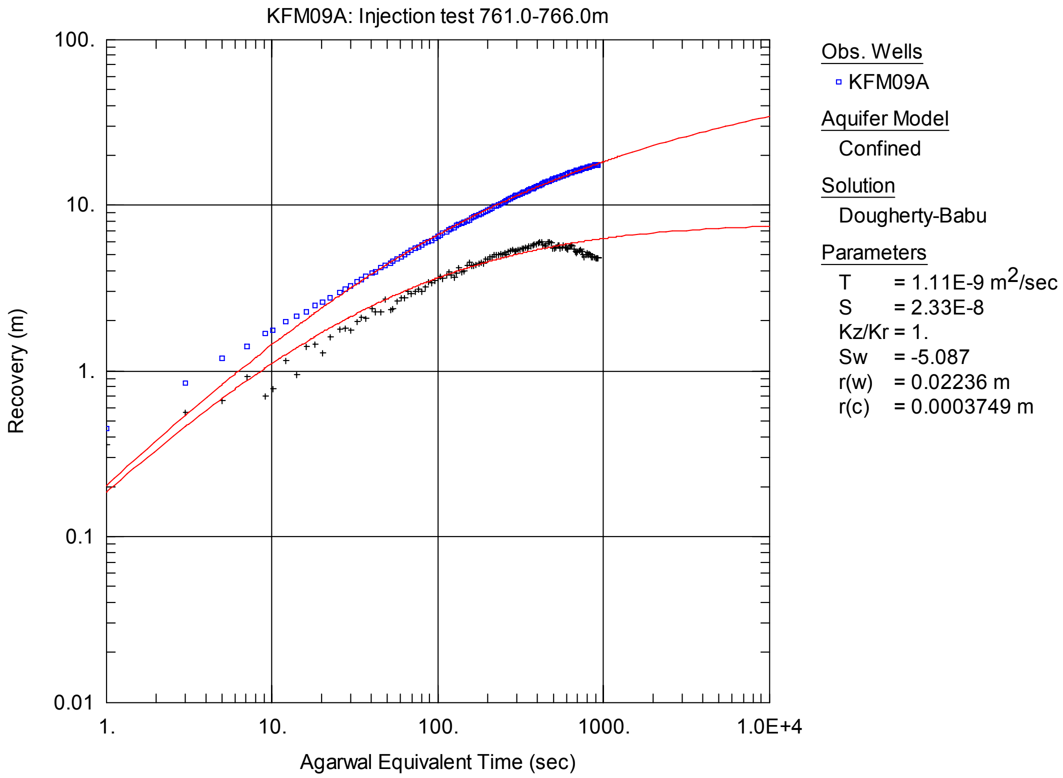


Figure A3-576. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 761.0-766.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

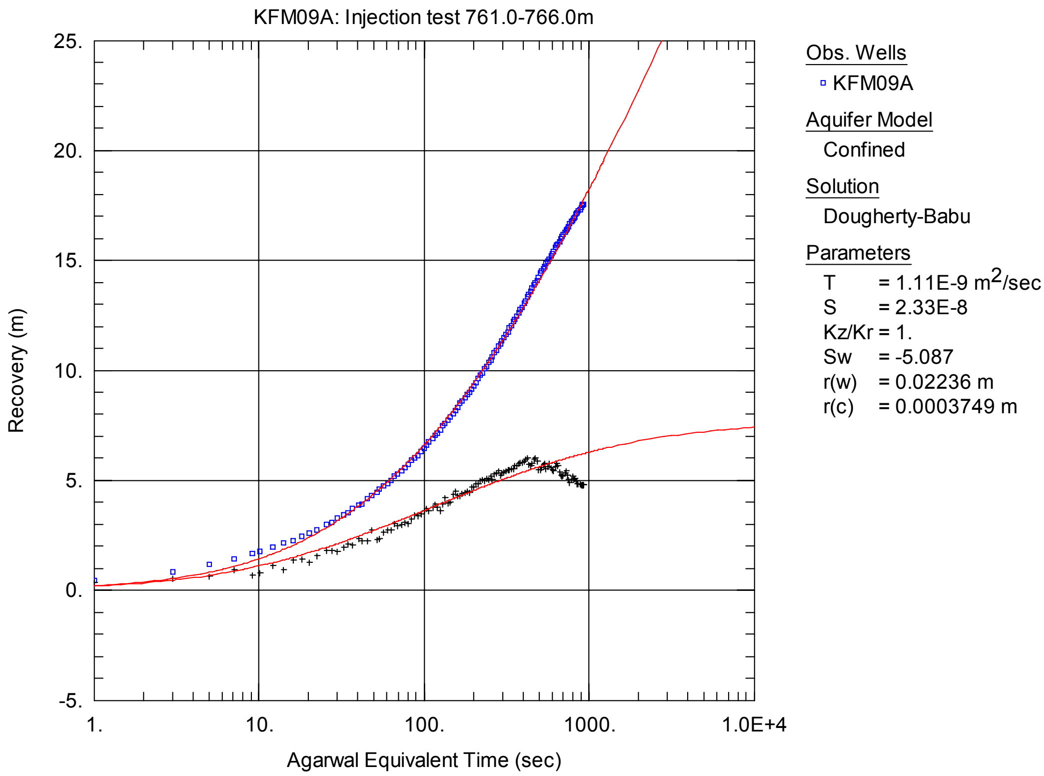


Figure A3-577. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 761.0-766.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

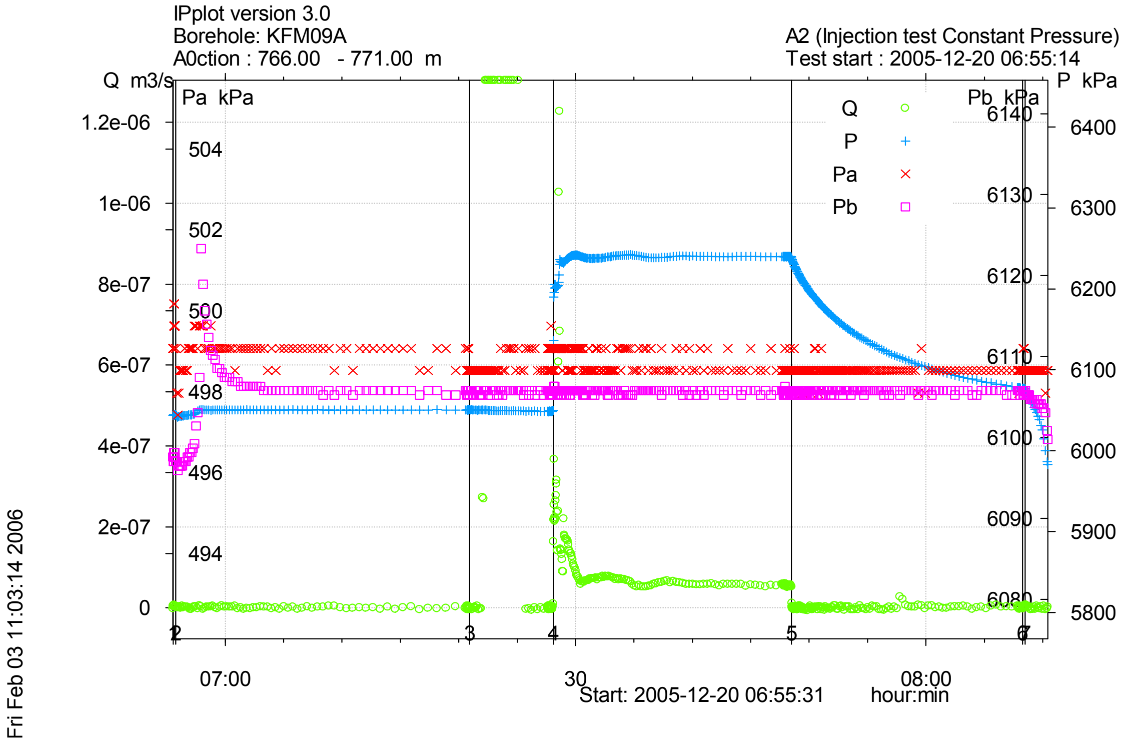


Figure A3-578. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 766.0-771.0 m in borehole KFM09A.*

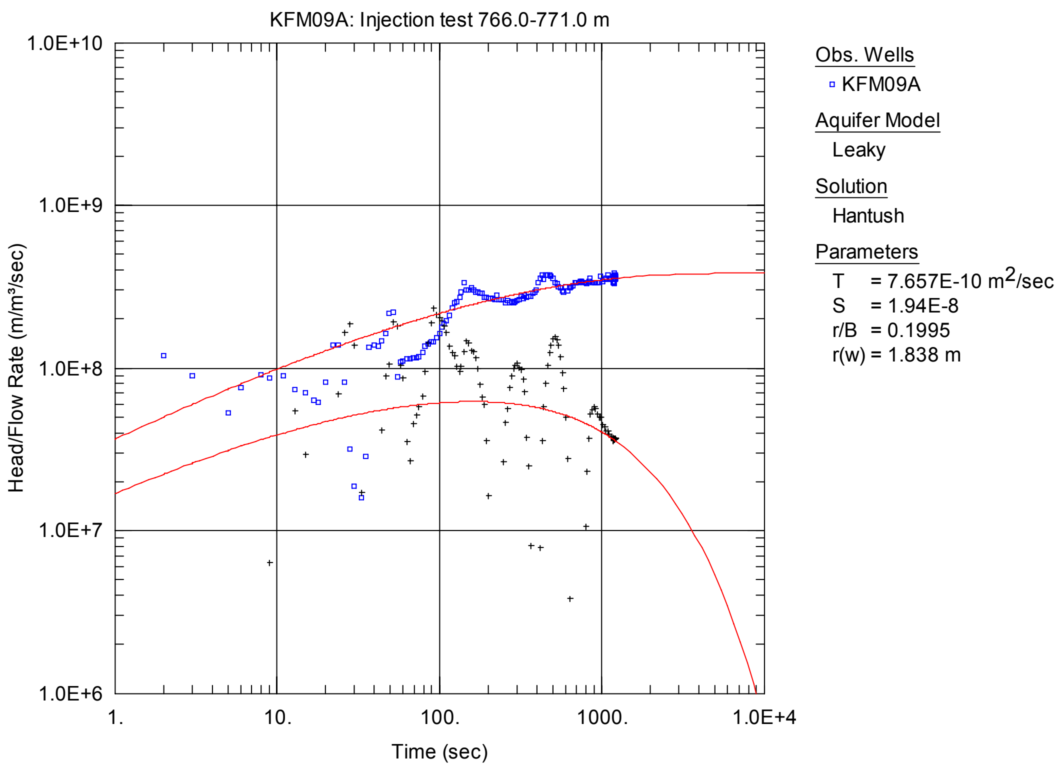


Figure A3-579. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 766.0-771.0 m in KFM09A.*

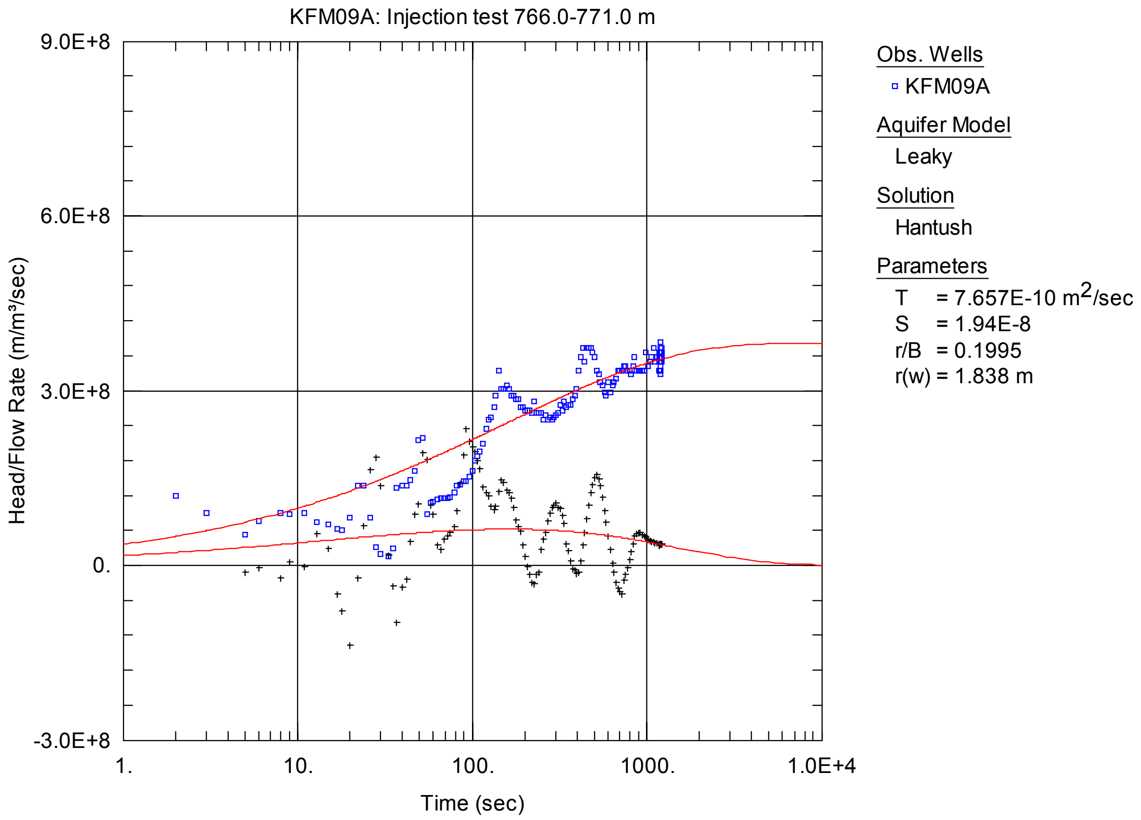


Figure A3-580. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 766.0-771.0 m in KFM09A.*

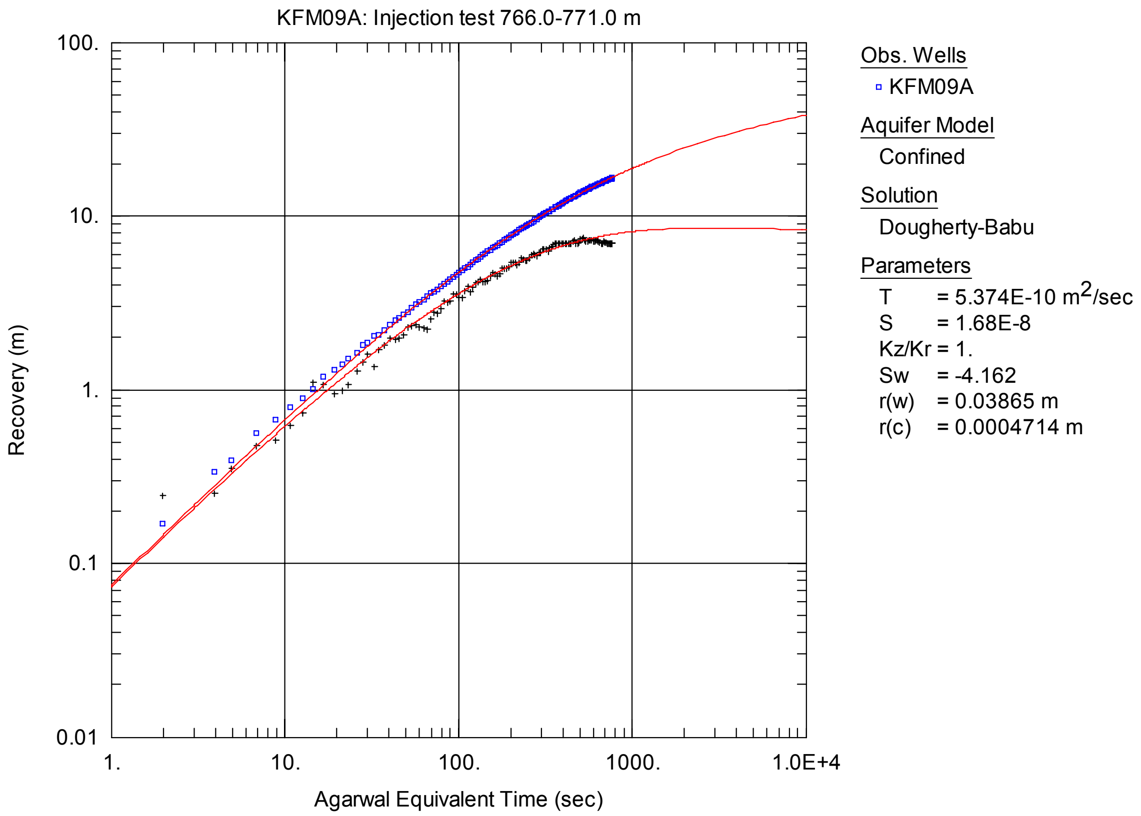


Figure A3-581. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 766.0-771.0 m in KFM09A.*

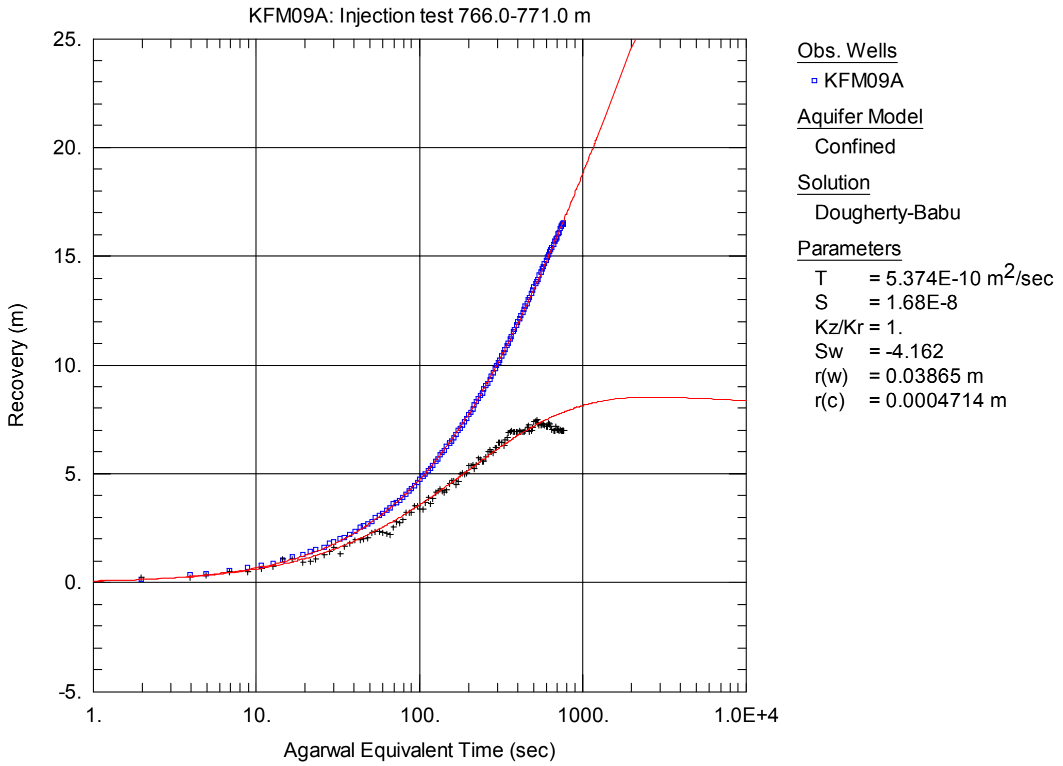


Figure A3-582. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 766.0-771.0 m in KFM09A.*

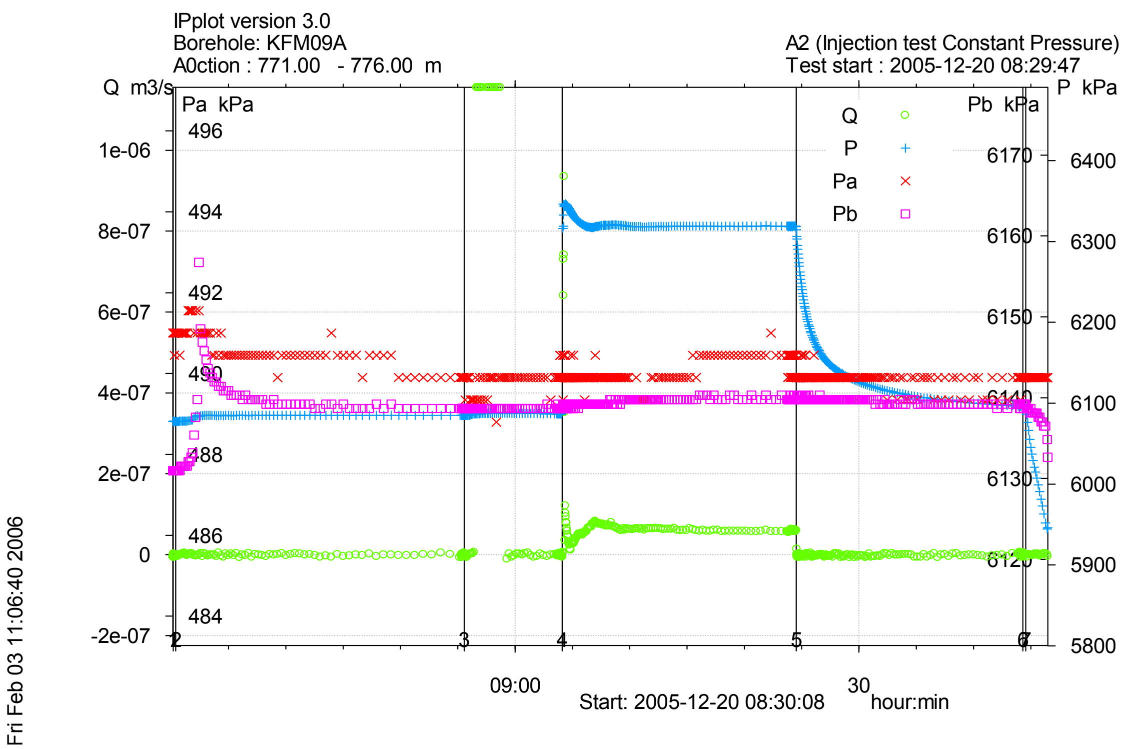


Figure A3-583. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 771.0-776.0 m in borehole KFM09A.*

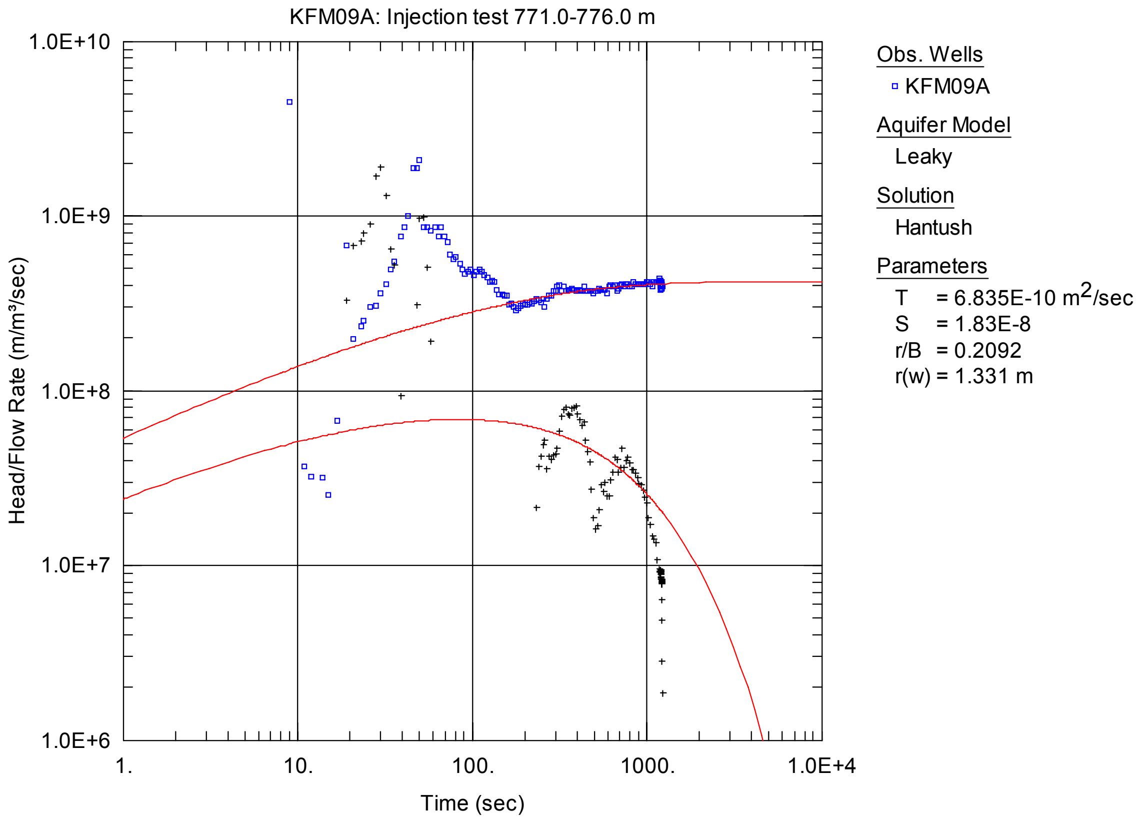


Figure A3-584. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 771.0-776.0 m in KFM09A.*

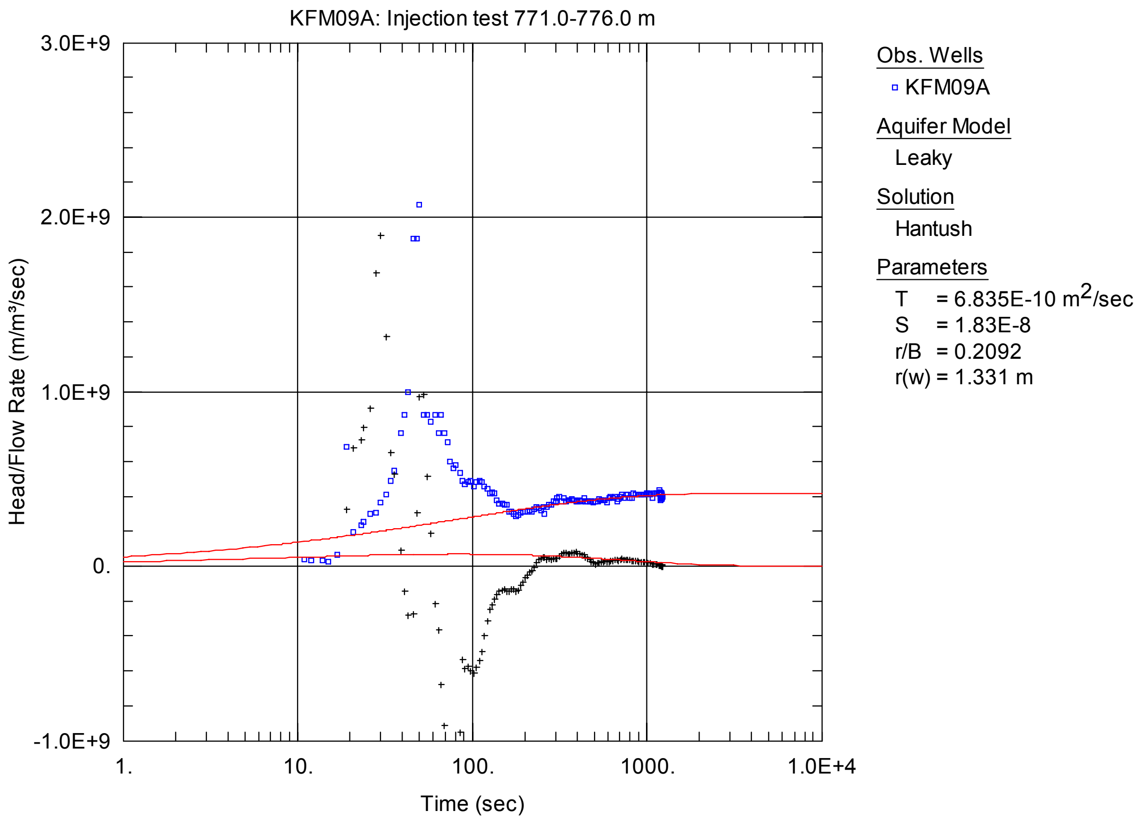


Figure A3-585. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 771.0-776.0 m in KFM09A.*

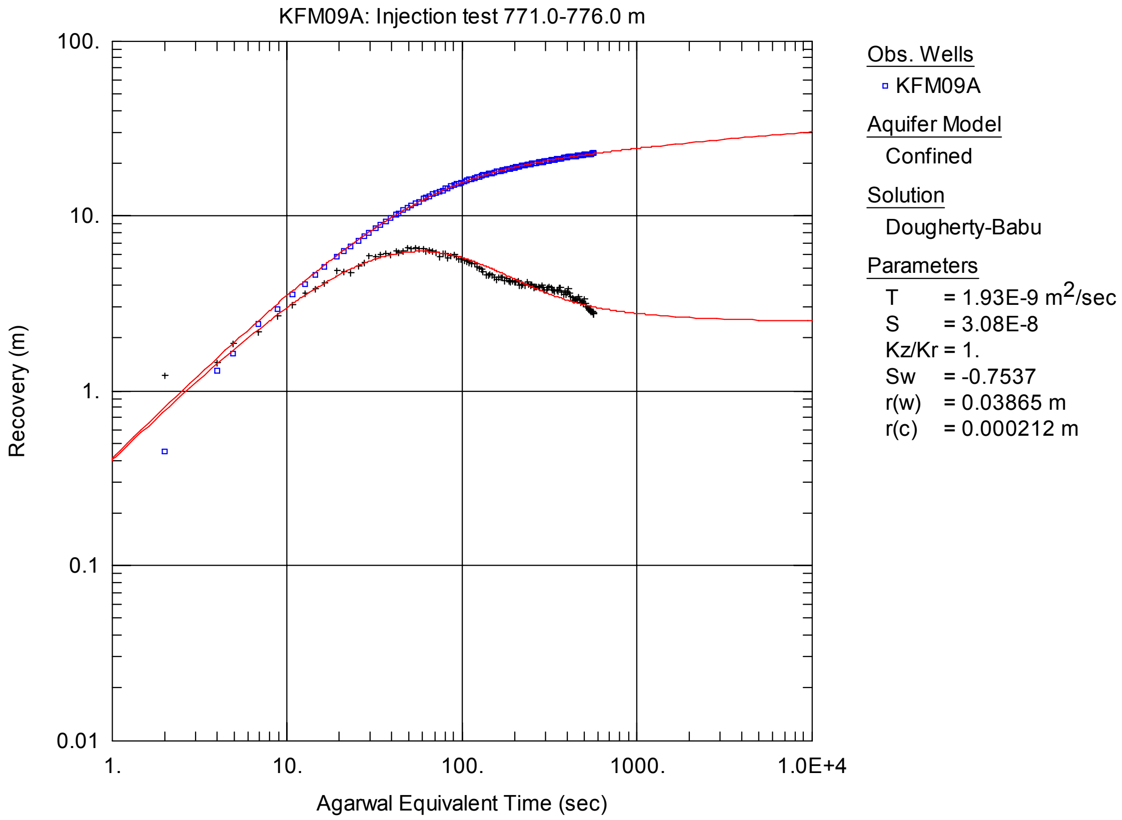


Figure A3-586. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 771.0-776.0 m in KFM09A.*

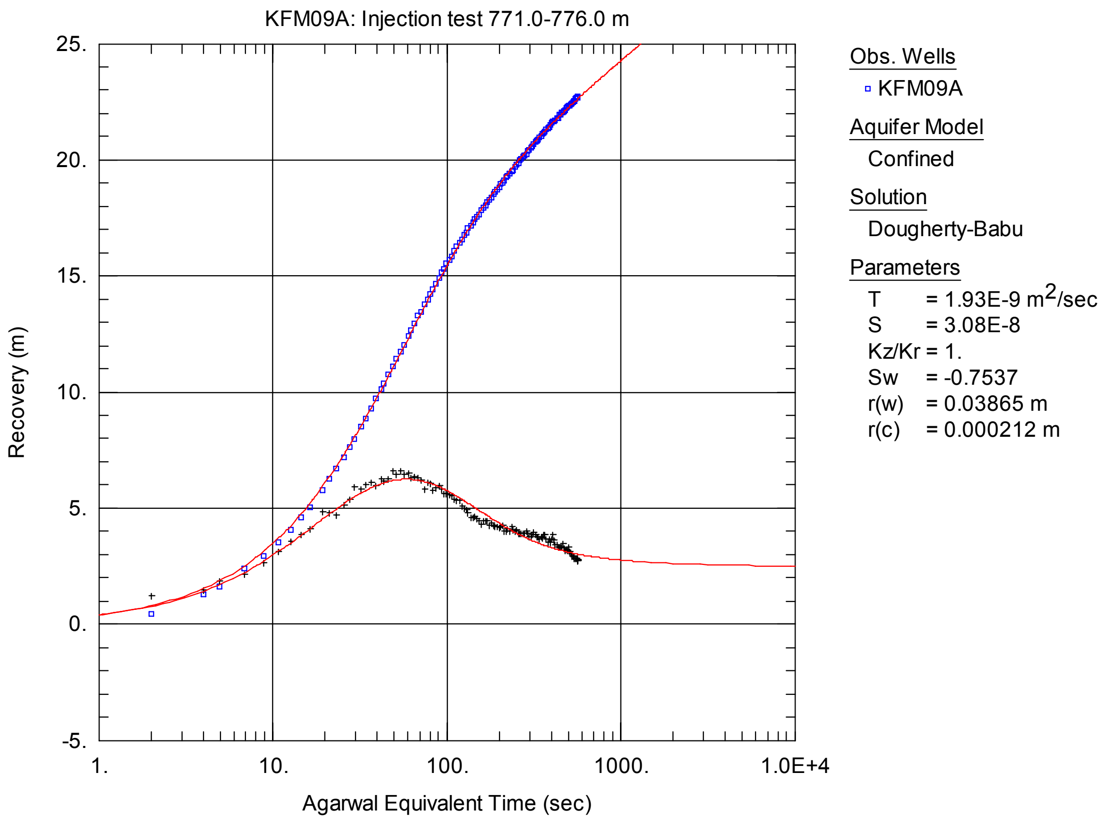


Figure A3-587. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 771.0-776.0 m in KFM09A.*

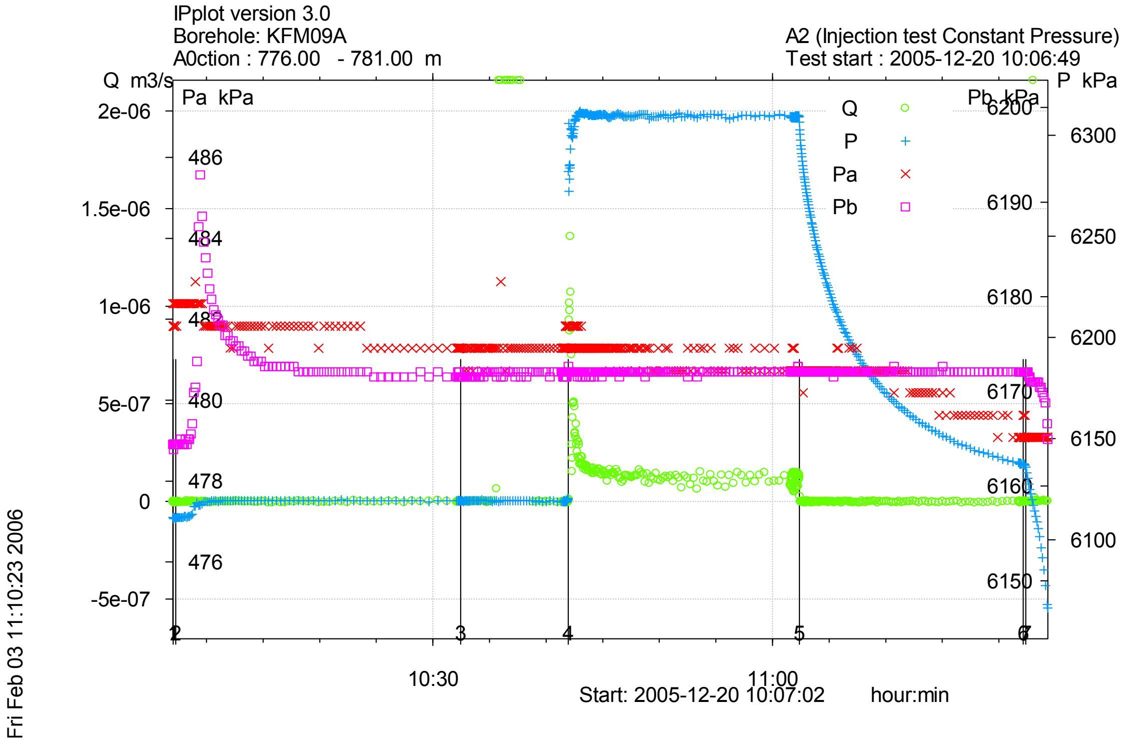


Figure A3-588. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 776.0-781.0 m in borehole KFM09A.

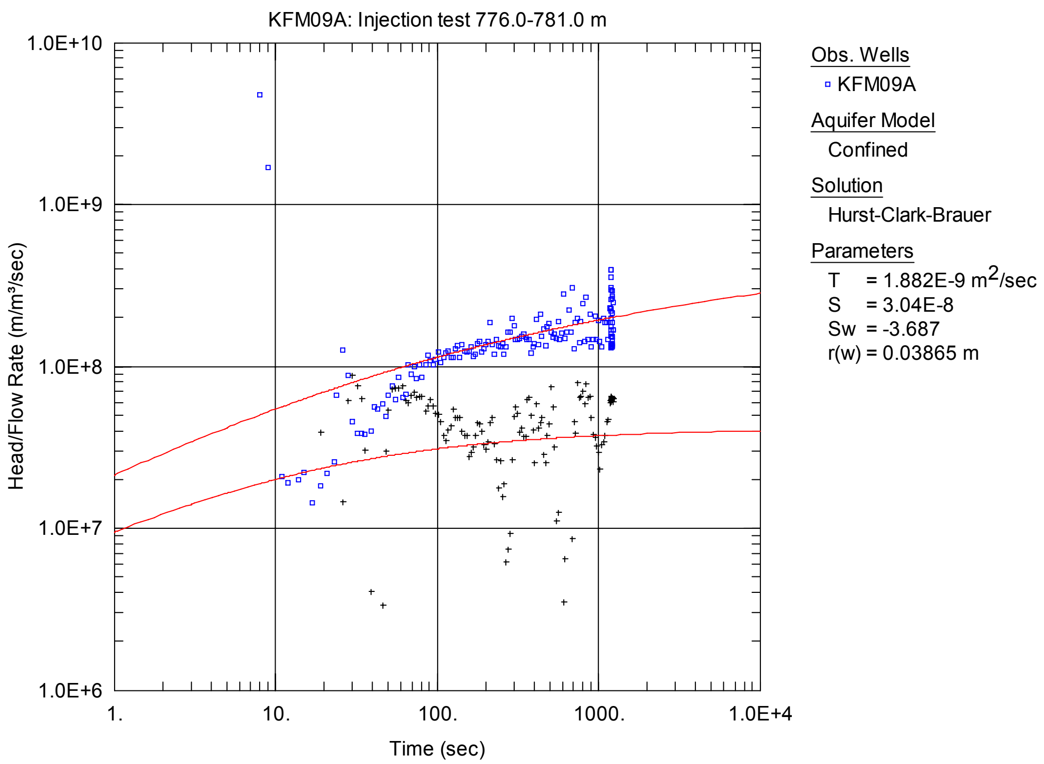


Figure A3-589. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 776.0-781.0 m in KFM09A.

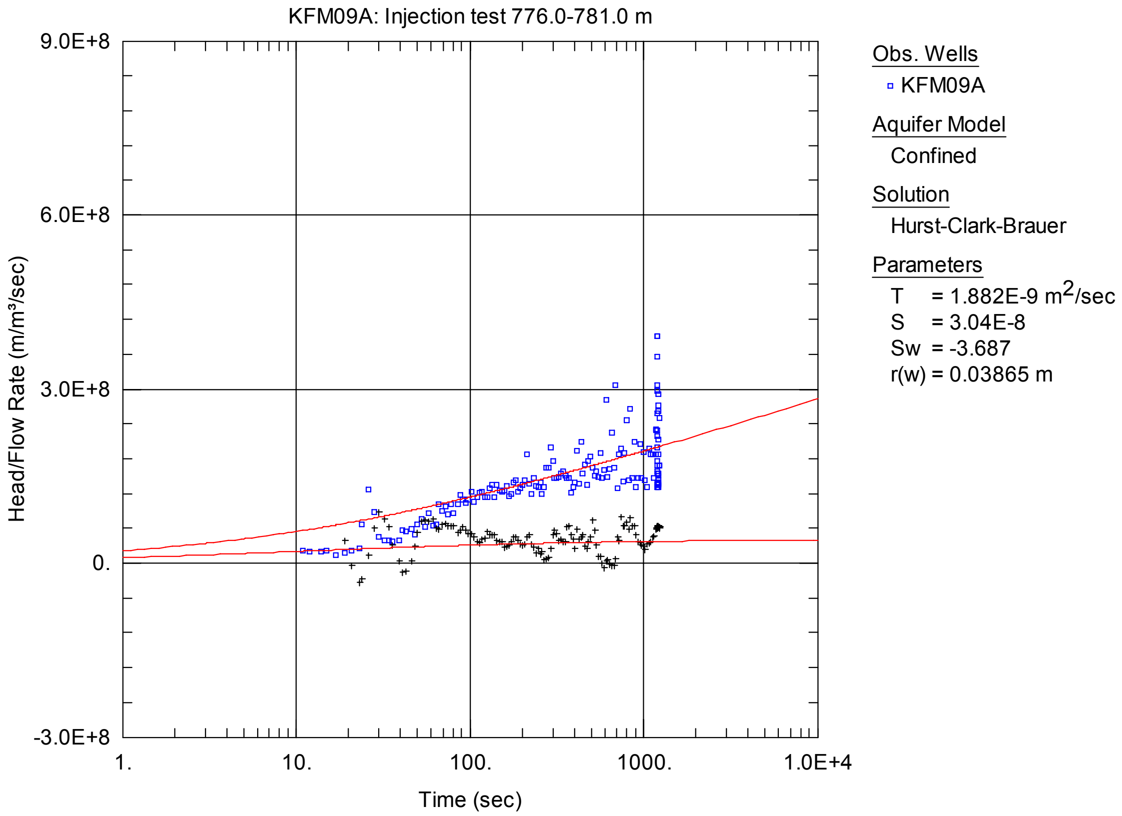


Figure A3-590. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 776.0-781.0 m in KFM09A.*

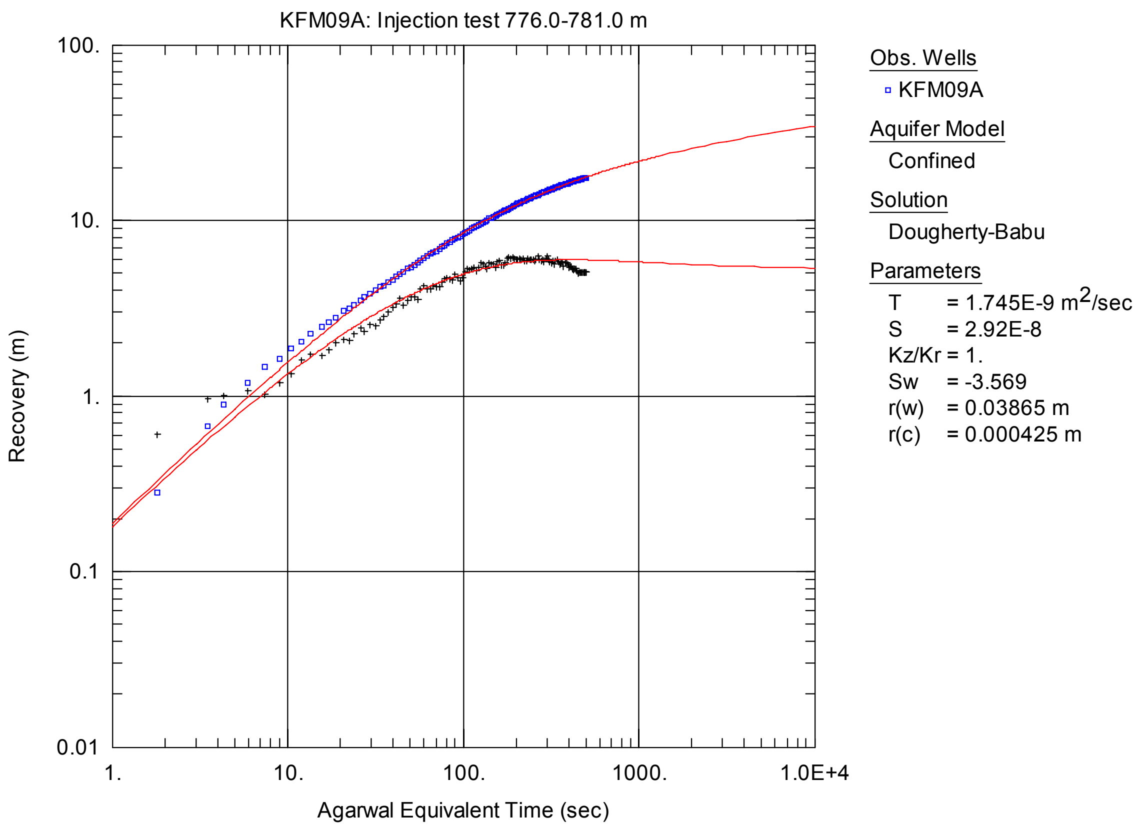


Figure A3-591. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 776.0-781.0 m in KFM09A.*

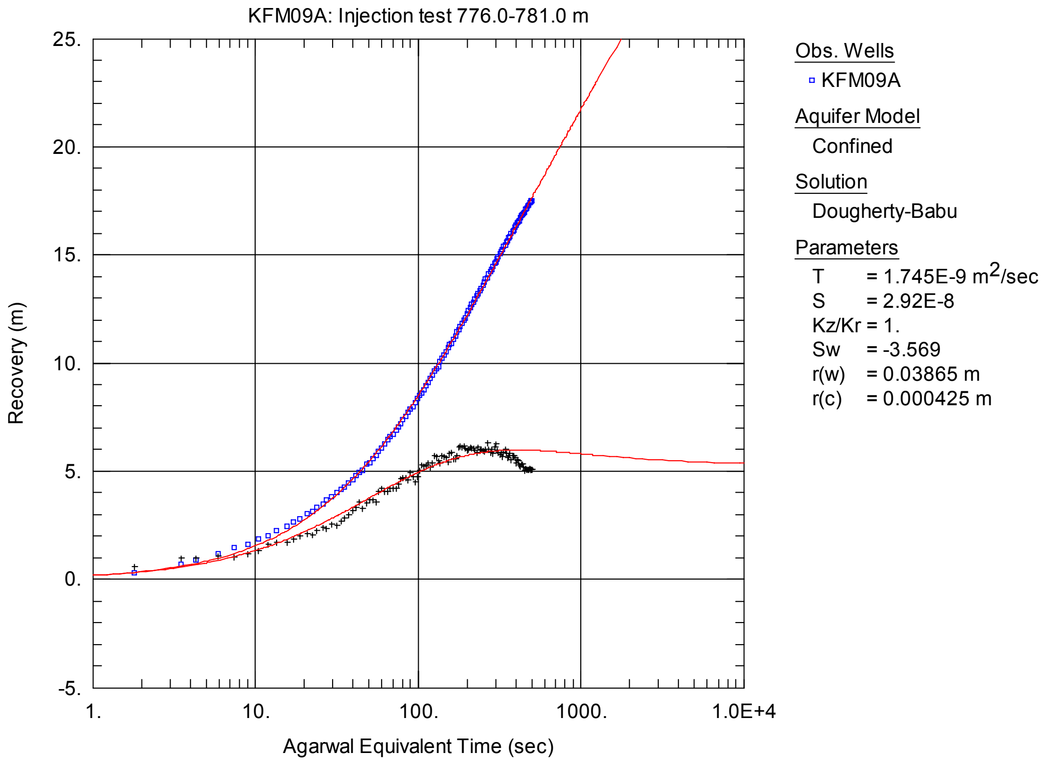


Figure A3-592. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 776.0-781.0 m in KFM09A.*

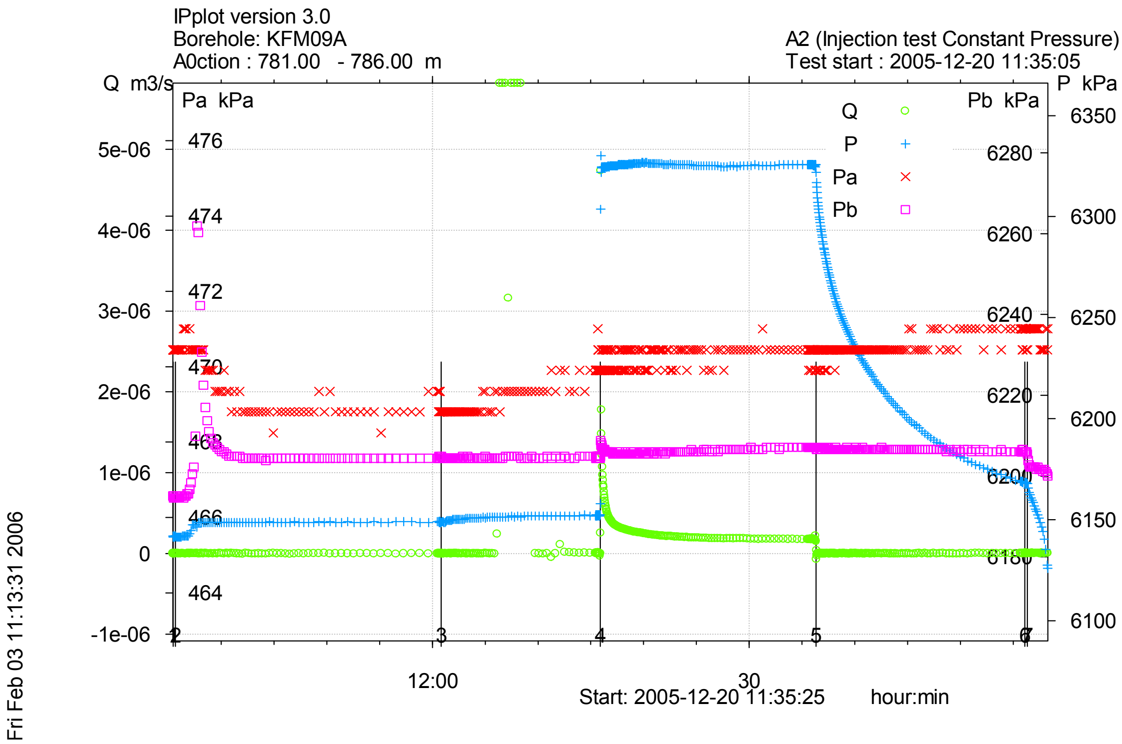


Figure A3-593. *Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 781.0-786.0 m in borehole KFM09A.*

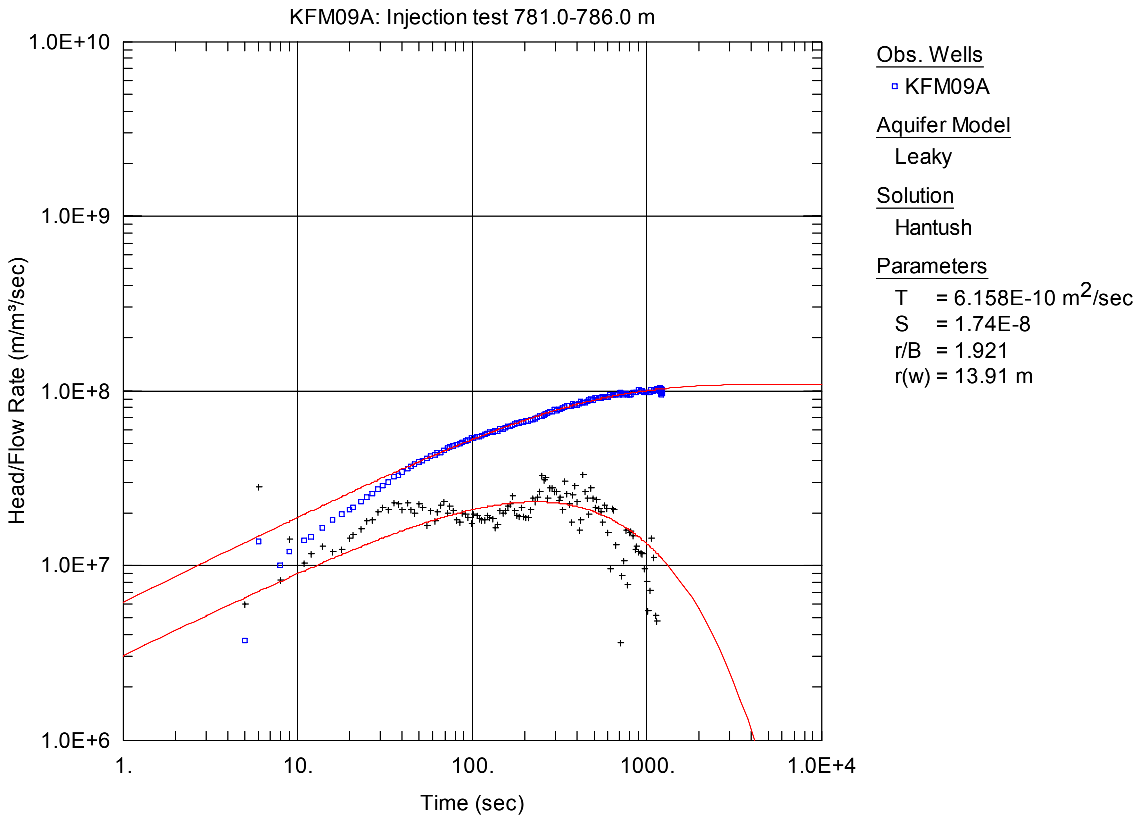


Figure A3-594. *Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 781.0-786.0 m in KFM09A.*

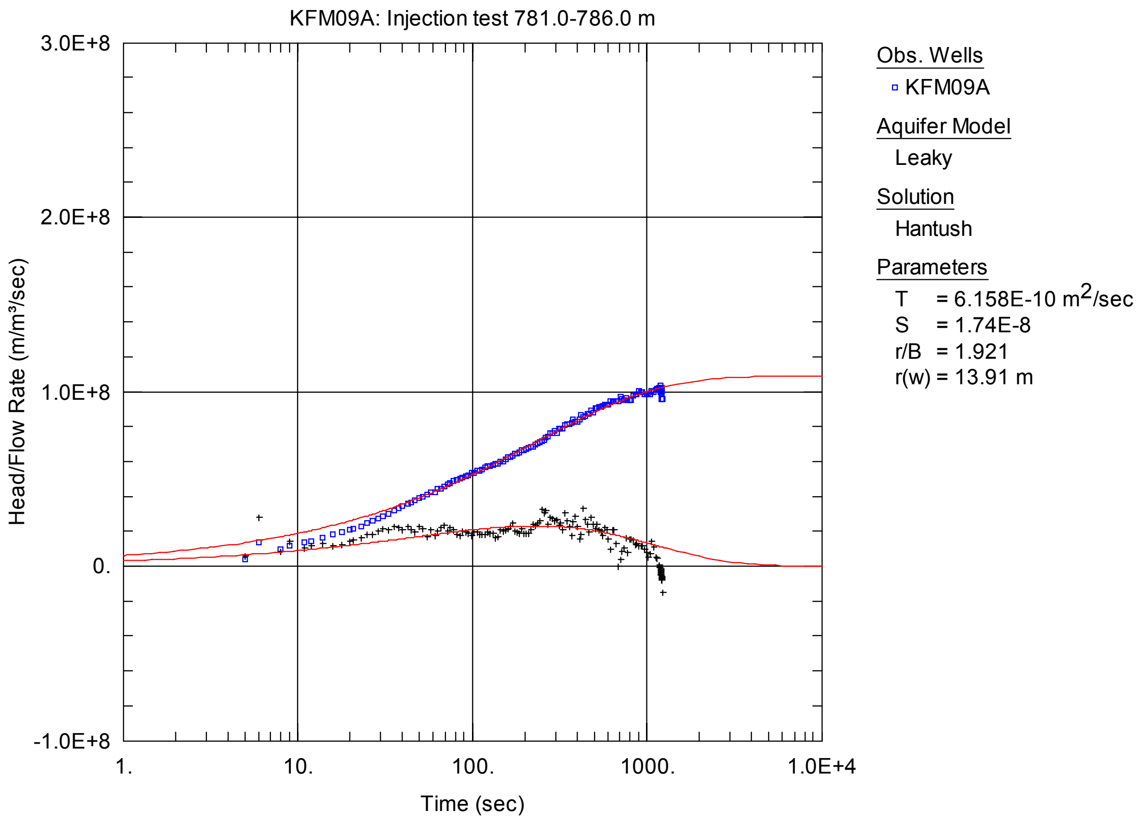


Figure A3-595. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 781.0-786.0 m in KFM09A.*

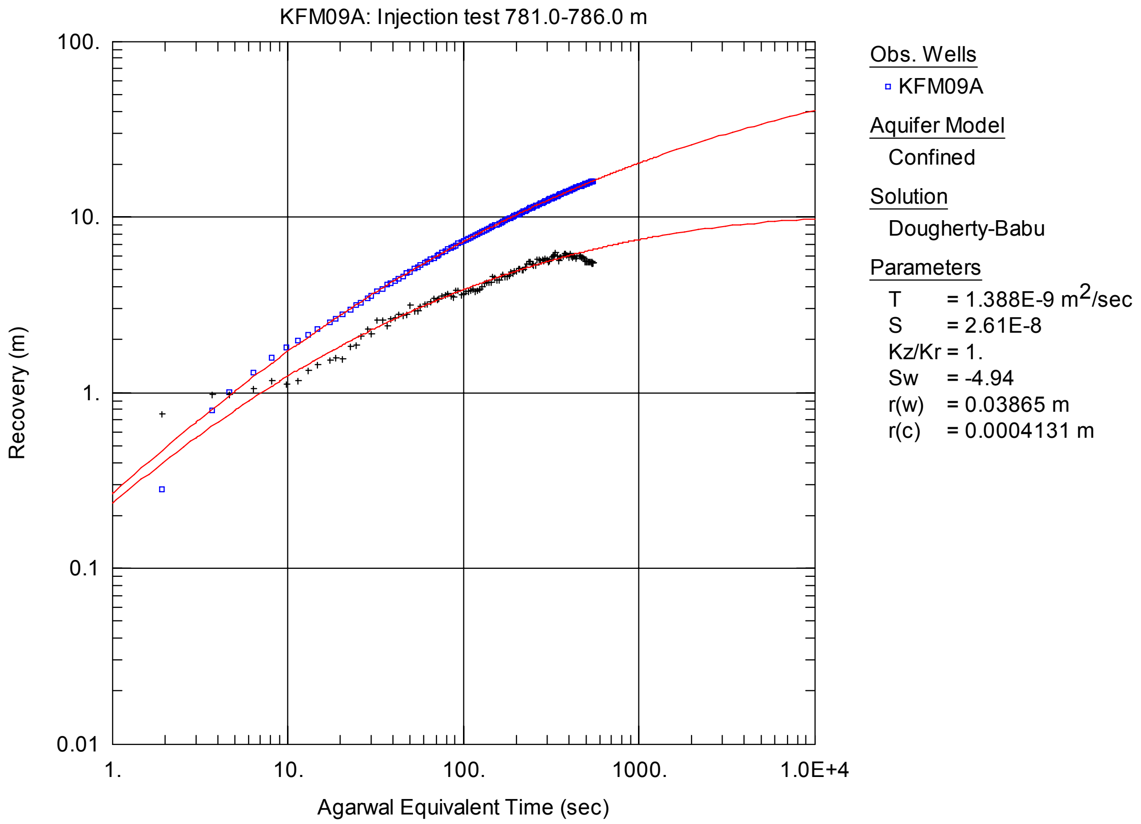


Figure A3-596. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 781.0-786.0 m in KFM09A.*

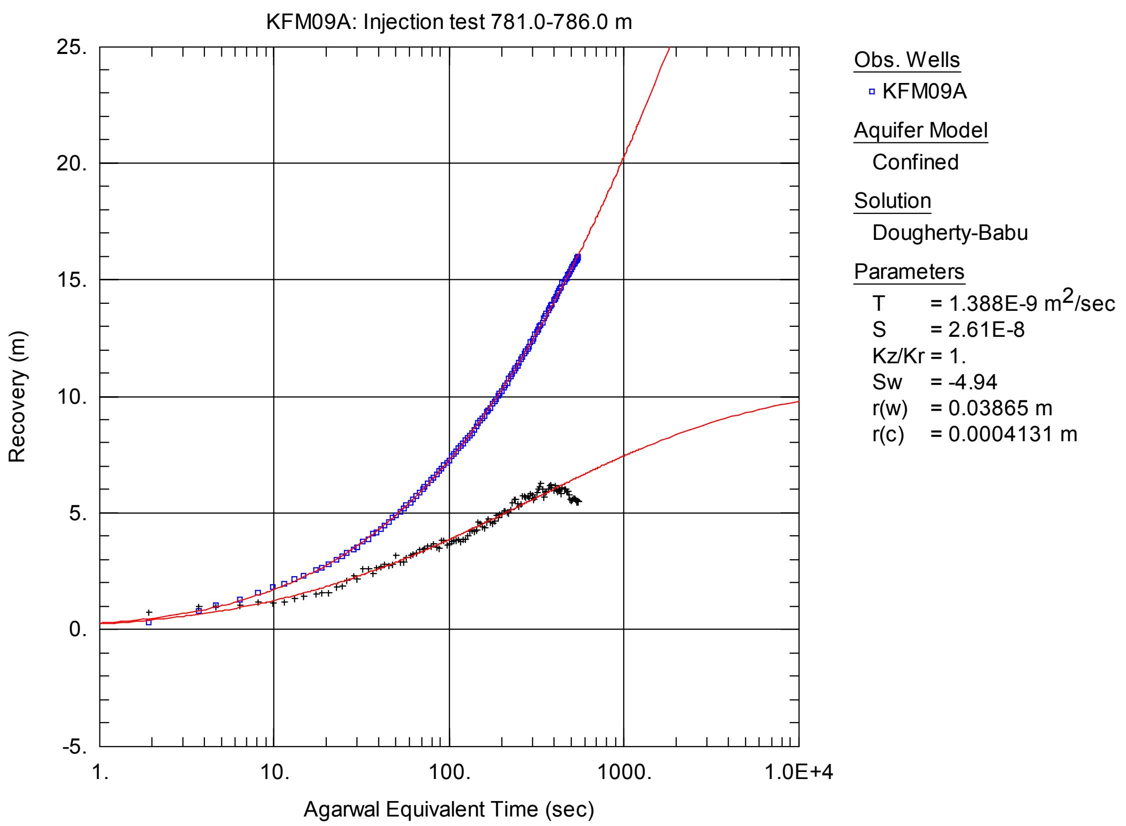


Figure A3-597. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 781.0-786.0 m in KFM09A.*

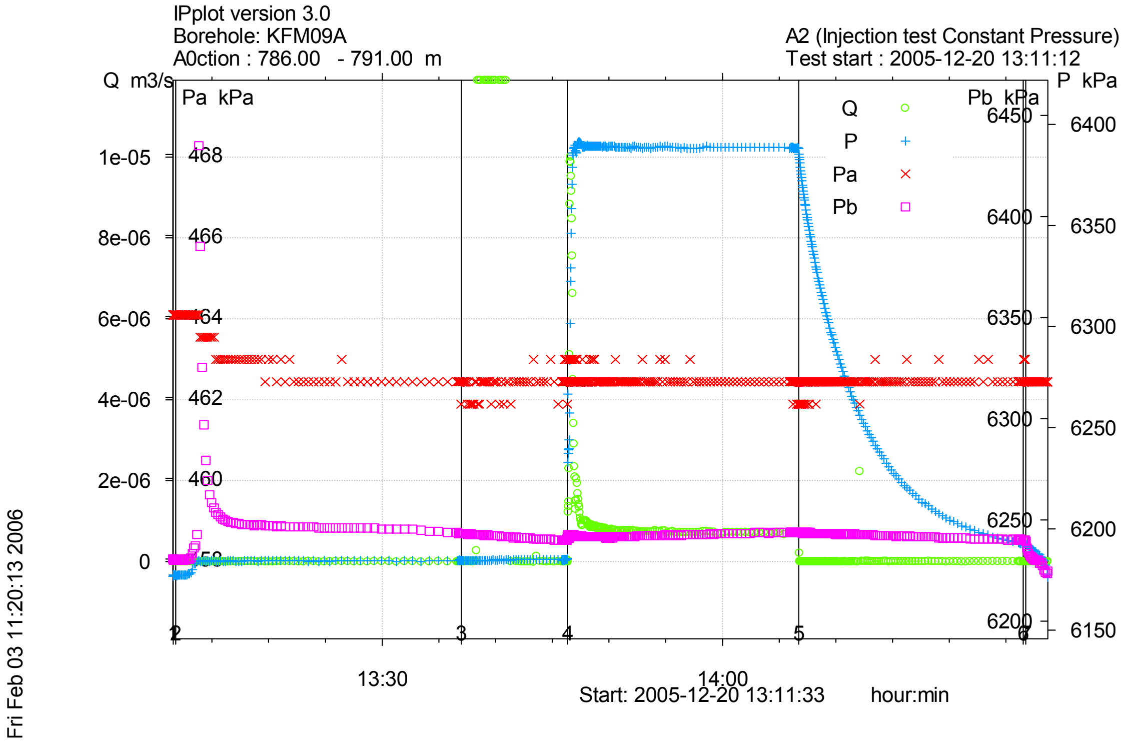


Figure A3-598. Linear plot of flow rate (Q), pressure (P), pressure above section (Pa) and pressure below section (Pb) versus time from the injection test in section 786.0-791.0 m in borehole KFM09A.

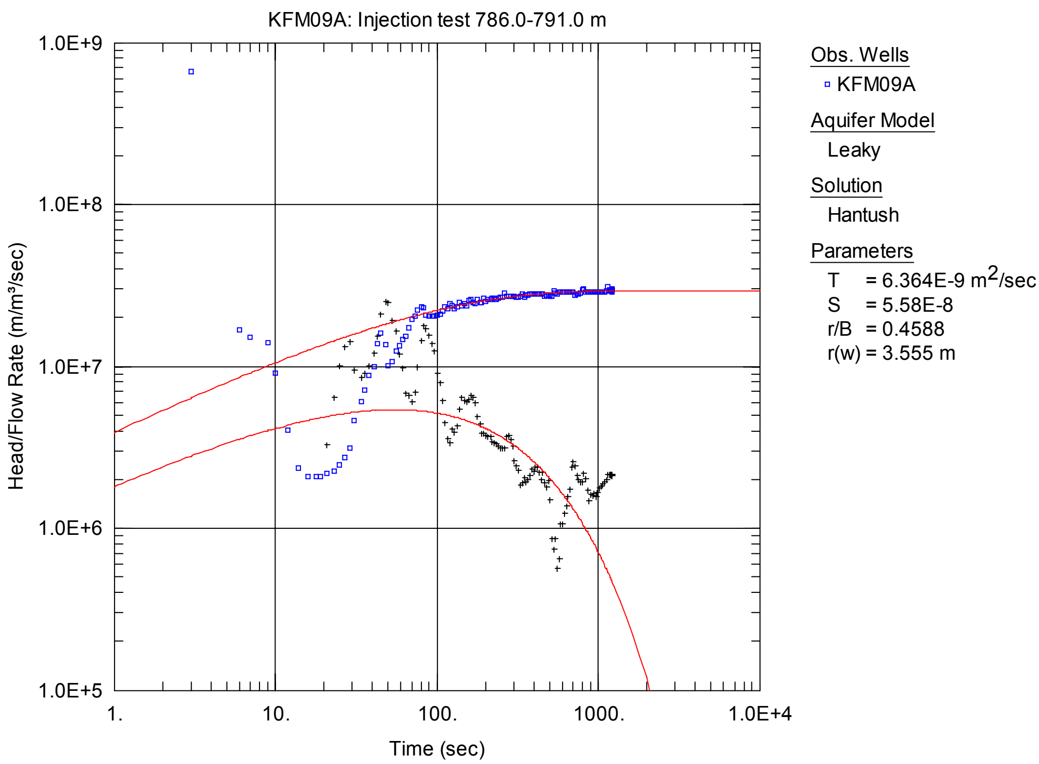


Figure A3-599. Log-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 786.0-791.0 m in KFM09A.

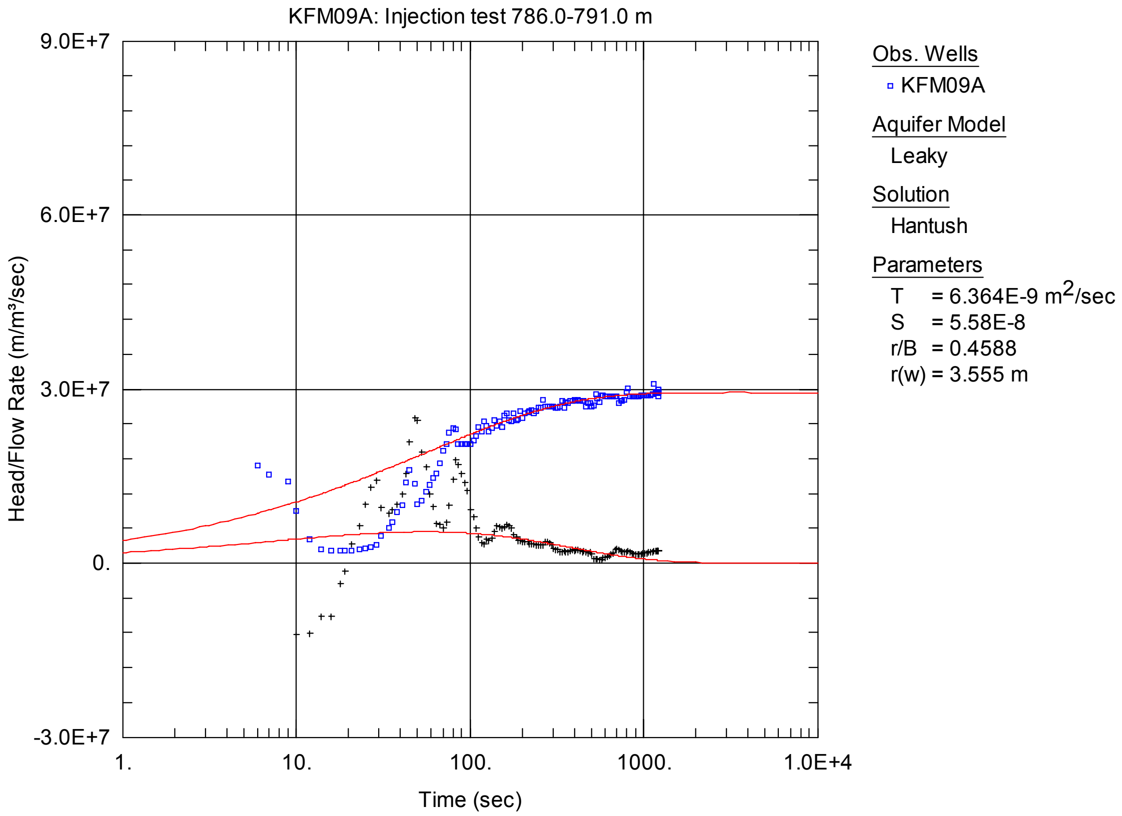


Figure A3-600. *Lin-log plot of head/flow rate (□) and derivative (+) versus time, from the injection test in section 786.0-791.0 m in KFM09A.*

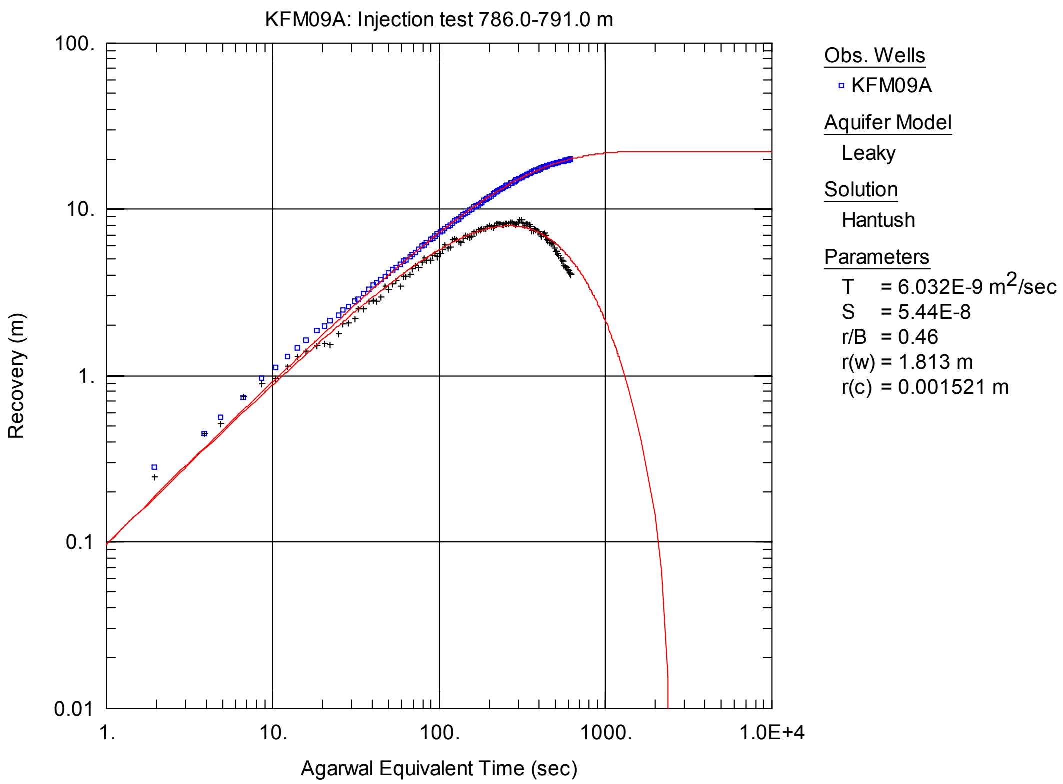


Figure A3-601. *Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 786.0-791.0 m in KFM09A. This evaluation is made with the Hantush model for a pseudo-spherical response.*

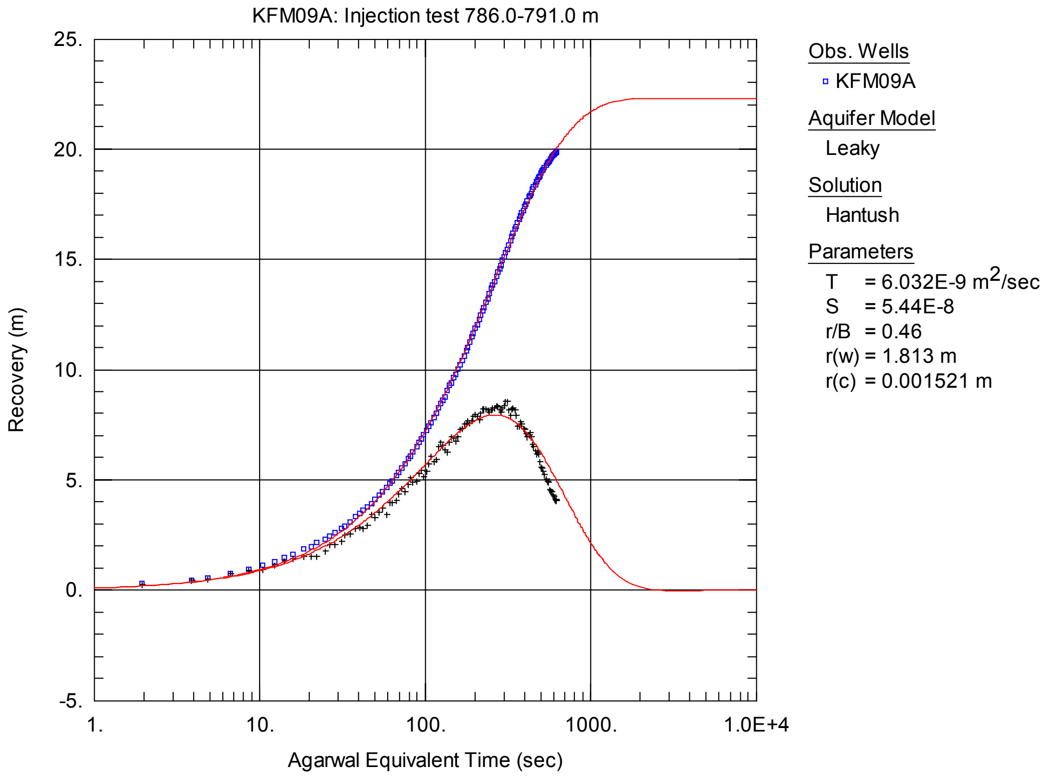


***Figure A3-602.** Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 786.0-791.0 m in KFM09A. This evaluation is made with the Hantush model for a pseudo-spherical response.*

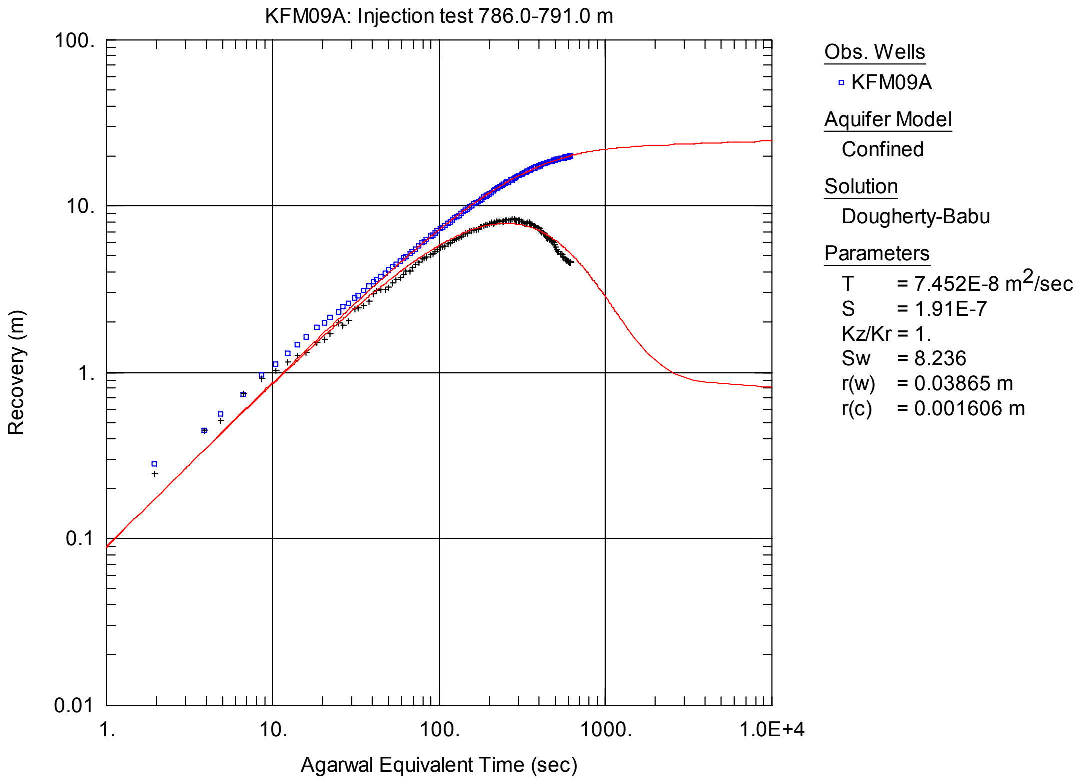


***Figure A3-603.** Log-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 786.0-791.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

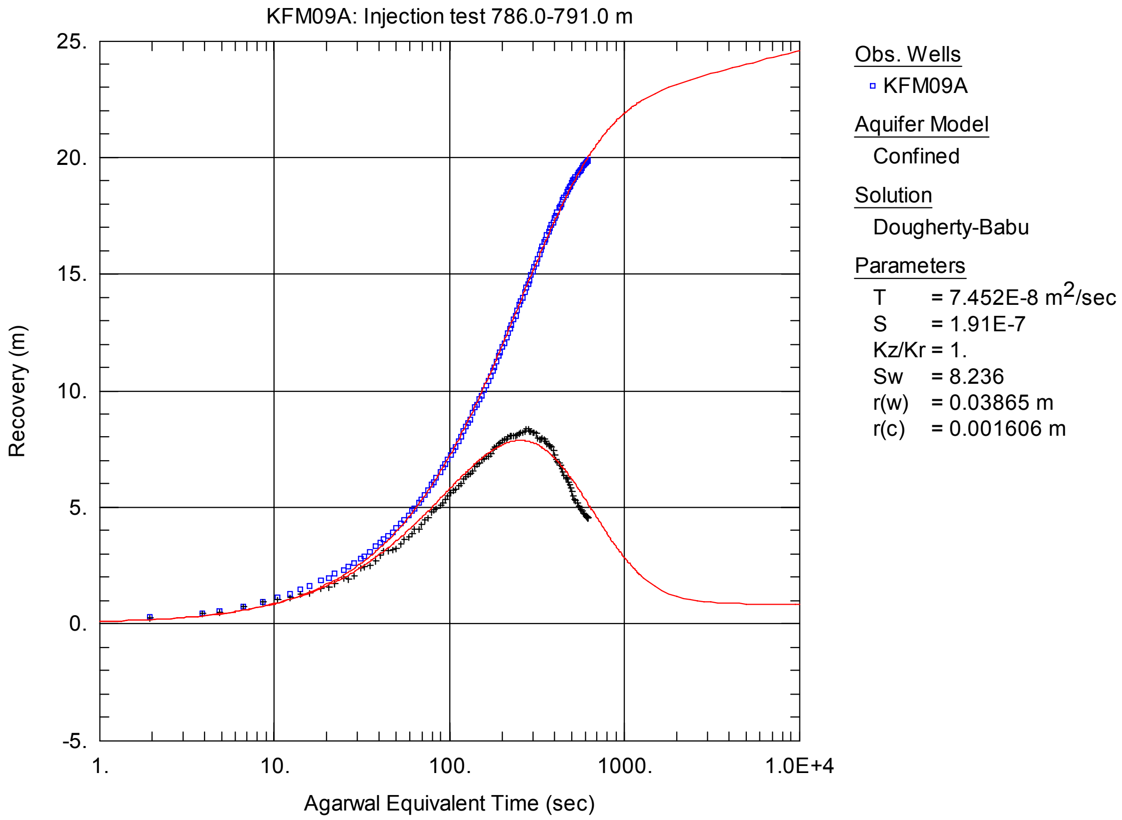
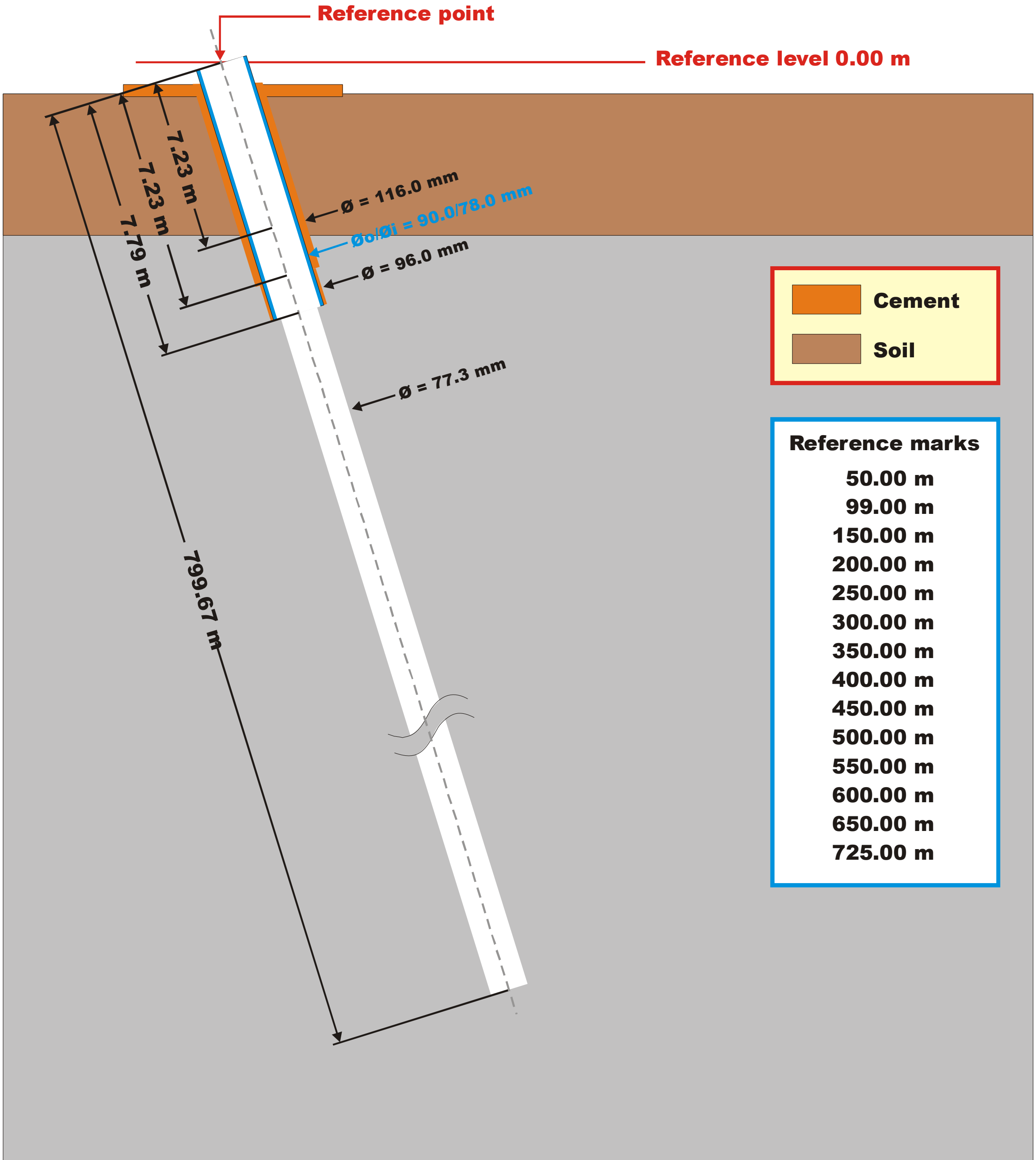


Figure A3-604. *Lin-log plot of recovery (□) and derivative (+) versus equivalent time, from the injection test in section 786.0-791.0 m in KFM09A. This evaluation is made with the Dougherty-Babu model for a pseudo-radial response.*

Appendix 4. Borehole technical data

Technical data

Borehole KFM09A



Drilling reference point

Northing: 6700115.04 (m), RT90 2,5 gon V 0:-15
Easting: 1630647.50 (m), RT90 2,5 gon V 0:-15
Elevation: 4.29 (m), RHB 70

Orientation

Bearing: 200.08°
Inclination: -59.46°

Drilling period

Drilling start date: 2005-09-05
Drilling stop date: 2005-10-27

2005-11-09 rev 2

Appendix 5. Sicada tables

Nomenclature plu_s_hole_test_d

Column	Datatype	Unit	Column Description	Alt. Symbol
site	CHAR		Investigation site name	
activity_type	CHAR		Activity type code	
start_date	DATE		Date (yymmdd hh:mm:ss)	
stop_date	DATE		Date (yymmdd hh:mm:ss)	
project	CHAR		project code	
idcode	CHAR		Object or borehole identification code	
secup	FLOAT	m	Upper section limit (m)	
seclow	FLOAT	m	Lower section limit (m)	
section_no	INTEGER	number	Section number	
test_type	CHAR		Test type code (1-7), see table description	
formation_type	CHAR		1: Rock, 2: Soil (superficial deposits)	
start_flow_period	DATE	yyyymmdd	Date & time of pumping/injection start (YYYY-MM-DD hh:mm:ss)	
stop_flow_period	DATE	yyyymmdd	Date & time of pumping/injection stop (YYYY-MM-DD hh:mm:ss)	
flow_rate_end_qp	FLOAT	m**3/s	Flow rate at the end of the flowing period	
value_type_qp	CHAR		0:true value,-1<lower meas.limit1:>upper meas.limit	
mean_flow_rate_qm	FLOAT	m**3/s	Arithmetic mean flow rate during flow period	
q_measl__l	FLOAT	m**3/s	Estimated lower measurement limit of flow rate	**Q-measl-L**
q_measl__u	FLOAT	m**3/s	Estimated upper measurement limit of flow rate	Q-measl-U
tot_volume_vp	FLOAT	m**3	Total volume of pumped or injected water	
dur_flow_phase_tp	FLOAT	s	Duration of the flowing period of the test	
dur_rec_phase_tf	FLOAT	s	Duration of the recovery period of the test	
initial_head_hi	FLOAT	m	Hydraulic head in test section at start of the flow period	
head_at_flow_end_hp	FLOAT	m	Hydraulic head in test section at stop of the flow period.	
final_head_hf	FLOAT	m	Hydraulic head in test section at stop of recovery period.	
initial_press_pi	FLOAT	kPa	Groundwater pressure in test section at start of flow period	
press_at_flow_end_pp	FLOAT	kPa	Groundwater pressure in test section at stop of flow period.	
final_press_pf	FLOAT	kPa	Ground water pressure at the end of the recovery period.	
fluid_temp_tew	FLOAT	oC	Measured section fluid temperature, see table description	
fluid_elcond_ecw	FLOAT	mS/m	Measured section fluid el. conductivity,see table descr.	
fluid_salinity_tdsw	FLOAT	mg/l	Total salinity of section fluid based on EC,see table descr.	
fluid_salinity_tdswm	FLOAT	mg/l	Tot. section fluid salinity based on water sampling,see...	
reference	CHAR		SKB report No for reports describing data and evaluation	
comments	VARCHAR		Short comment to data	
error_flag	CHAR		If error_flag = "*" then an error occured and an error	
in_use	CHAR		If in_use = "*" then the activity has been selected as	
sign	CHAR		Signature for QA data accknowledge (QA - OK)	
lp	FLOAT	m	Hydraulic point of application	

Nomenclature plu_s_hole_test_ed1

Column	Datatype	Unit	Column Description	Alt. Symbol
site	CHAR		Investigation site name	
activity_type	CHAR		Activity type code	
start_date	DATE		Date (yymmdd hh:mm:ss)	
stop_date	DATE		Date (yymmdd hh:mm:ss)	
project	CHAR		project code	
idcode	CHAR		Object or borehole identification code	
secup	FLOAT	m	Upper section limit (m)	

Column	Datatype	Unit	Column Description	Alt. Symbol
seclow	FLOAT	m	Lower section limit (m)	
section_no	INTEGER	number	Section number	
test_type	CHAR		Test type code (1-7), see table description!	
formation_type	CHAR		Formation type code. 1: Rock, 2: Soil (superficial deposits)	
lp	FLOAT	m	Hydraulic point of application for test section, see descr.	
seclen_class	FLOAT	m	Planned ordinary test interval during test campaign.	
spec_capacity_q_s	FLOAT	m**2/s	Specific capacity (Q/s) of test section, see table descript.	Q/s
value_type_q_s	CHAR		0:true value,-1:Q/s<lower meas.limit,1:Q/s>upper meas.limit	
transmissivity_tq	FLOAT	m**2/s	Tranmissivity based on Q/s, see table description	
value_type_tq	CHAR		0:true value,-1:TQ<lower meas.limit,1:TQ>upper meas.limit.	
bc_tq	CHAR		Best choice code. 1 means TQ is best choice of T, else 0	
transmissivity_moye	FLOAT	m**2/s	Transmissivity,TM, based on Moye (1967)	T_M
bc_tm	CHAR		Best choice code. 1 means Tmoye is best choice of T, else 0	
value_type_tm	CHAR		0:true value,-1:TM<lower meas.limit,1:TM>upper meas.limit.	
hydr_cond_moye	FLOAT	m/s	K_M: Hydraulic conductivity based on Moye (1967)	K_M
formation_width_b	FLOAT	m	b:Aquifer thickness repr. for T(generally b=Lw) ,see descr.	b
width_of_channel_b	FLOAT	m	B:Inferred width of formation for evaluated TB	
tb	FLOAT	m**3/s	TB:Flow capacity in 1D formation of T & width B, see descr.	
l_measl_tb	FLOAT	m**3/s	Estimated lower meas. limit for evaluated TB,see description	
u_measl_tb	FLOAT	m**3/s	Estimated upper meas. limit of evaluated TB,see description	
sb	FLOAT	m	SB:S=storativity,B=width of formation,1D model,see descript.	
assumed_sb	FLOAT	m	SB* : Assumed SB,S=storativity,B=width of formation,see...	
leakage_factor_lf	FLOAT	m	Lf:1D model for evaluation of Leakage factor	
transmissivity_tt	FLOAT	m**2/s	TT:Transmissivity of formation, 2D radial flow model,see...	T_T
value_type_tt	CHAR		0:true value,-1:TT<lower meas.limit,1:TT>upper meas.limit,	
bc_tt	CHAR		Best choice code. 1 means TT is best choice of T, else 0	
l_measl_q_s	FLOAT	m**2/s	Estimated lower meas. limit for evaluated TT,see table descr	Q/s-measl-L
u_measl_q_s	FLOAT	m**2/s	Estimated upper meas. limit for evaluated TT,see description	Q/s-measl-U
storativity_s	FLOAT		S:Storativity of formation based on 2D rad flow,see descr.	
assumed_s	FLOAT		Assumed Storativity,2D model evaluation,see table descr.	
bc_s	FLOAT		Best choice of S (Storativity) ,see descr.	
ri	FLOAT	m	Radius of influence	
ri_index	CHAR		ri index=index of radius of influence :-1,0 or 1, see descr.	
leakage_coeff	FLOAT	1/s	K'/b':2D rad flow model evaluation of leakage coeff,see desc	
hydr_cond_ksf	FLOAT	m/s	Ksf:3D model evaluation of hydraulic conductivity,see desc.	
value_type_ksf	CHAR		0:true value,-1:Ksf<lower meas.limit,1:Ksf>upper meas.limit,	
l_measl_ksf	FLOAT	m/s	Estimated lower meas.limit for evaluated Ksf,see table desc.	
u_measl_ksf	FLOAT	m/s	Estimated upper meas.limit for evaluated Ksf,see table descr	
spec_storage_ssf	FLOAT	1/m	Ssf:Specific storage,3D model evaluation,see table descr.	
assumed_ssf	FLOAT	1/m	Ssf*:Assumed Spec.storage,3D model evaluation,see table des.	
c	FLOAT	m**3/pa	C: Wellbore storage coefficient; flow or recovery period	C
cd	FLOAT		CD: Dimensionless wellbore storage coefficient	
skin	FLOAT		Skin factor;best estimate of flow/recovery period,see descr.	ξ
dt1	FLOAT	s	Estimated start time of evaluation, see table description	
dt2	FLOAT	s	Estimated stop time of evaluation. see table description	
t1	FLOAT	s	Start time for evaluated parameter from start flow period	t_1
t2	FLOAT	s	Stop time for evaluated parameter from start of flow period	t_2
dte1	FLOAT	s	Start time for evaluated parameter from start of recovery	dte_1
dte2	FLOAT	s	Stop time for evaluated parameter from start of recovery	dte_2
p_horner	FLOAT	kPa	p*:Horner extrapolated pressure, see table description	
transmissivity_t_nlr	FLOAT	m**2/s	T_NLR Transmissivity based on None Linear Regression...	
storativity_s_nlr	FLOAT		S_NLR=storativity based on None Linear Regression,see..	
value_type_t_nlr	CHAR		0:true value,-1:T_NLR<lower meas.limit,1:>upper meas.limit	

Column	Datatype	Unit	Column Description	Alt. Symbol
bc_t_nlr	CHAR		Best choice code. 1 means T_NLR is best choice of T, else 0	
c_nlr	FLOAT	m**3/pa	Wellbore storage coefficient, based on NLR, see descr.	
cd_nlr	FLOAT		Dimensionless wellbore storage constant, see table descrip.	
skin_nlr	FLOAT		Skin factor based on Non Linear Regression,see desc.	
transmissivity_t_grf	FLOAT	m**2/s	T_GRF:Transmissivity based on Genelized Radial Flow,see...	
value_type_t_grf	CHAR		0:true value,-1:T_GRF<lower meas.limit,1:>upper meas.limit	
bc_t_grf	CHAR		Best choice code. 1 means T_GRF is best choice of T, else 0	
storativity_s_grf	FLOAT		S_GRF:Storativity based on Generalized Radial Flow, see des.	
flow_dim_grf	FLOAT		Inferred flow dimesion based on Generalized Rad. Flow model	
comment	VARCHAR	no_unit	Short comment to the evaluated parameters	
error_flag	CHAR		If error_flag = "*" then an error occured and an error	
in_use	CHAR		If in_use = "*" then the activity has been selected as	
sign	CHAR		Signature for QA data accknowledge (QA - OK)	

Nomenclature plu_s_hole_test_obs

Column	Datatype	Unit	Column Description
site	CHAR		Investigation site name
activity_type	CHAR		Activity type code
idcode	CHAR		Object or borehole identification code
start_date	DATE		Date (yymmdd hh:mm:ss)
secup	FLOAT	m	Upper section limit (m)
seclow	FLOAT	m	Lower section limit (m)
obs_secup	FLOAT	m	Upper limit of observation section
obs_seclow	FLOAT	m	Lower limit of observation section
pi_above	FLOAT	kPa	Groundwater pressure above test section,start of flow period
pp_above	FLOAT	kPa	Groundwater pressure above test section,at stop flow period
pf_above	FLOAT	kPa	Groundwater pressure above test section at stop recovery per
pi_below	FLOAT	kPa	Groundwater pressure below test section at start flow period
pp_below	FLOAT	kPa	Groundwater pressure below test section at stop flow period
pf_below	FLOAT	kPa	Groundwater pressure below test section at stop recovery per
comments	VARCHAR		Comment text row (unformatted text)

KFM09A plu_s_hole_test_d. Left (This result table to SICADA includes more columns which are empty, these columns are not presented here.)

idcode	start_date	stop_date	secup	seclow	test_type	Formation_type	start_flow_period	stop_flow_period	flow_rate_end_qp	Value_type_qp	mean_flow_rate_qm
KFM09A	20051117 16:09	20051117 17:59	106.00	206.00	3	1	20051117 16:57:06	20051117 17:27:25	7.07E-05	0	9.33E-05
KFM09A	20051117 19:03	20051117 20:53	206.00	306.00	3	1	20051117 19:50:48	20051117 20:21:10	1.31E-06	0	1.62E-06
KFM09A	20051117 21:47	20051117 23:36	306.00	406.00	3	1	20051117 22:34:02	20051117 23:04:29	4.06E-06	0	7.19E-06
KFM09A	20051118 09:59	20051118 11:49	406.00	506.00	3	1	20051118 10:46:49	20051118 11:17:10	1.07E-05	0	3.77E-05
KFM09A	20051121 12:52	20051121 15:13	506.00	606.00	3	1	20051121 14:11:02	20051121 14:41:23	1.94E-06	0	8.12E-06
KFM09A	20051121 06:14	20051121 08:03	606.00	706.00	3	1	20051121 07:00:34	20051121 07:30:54	5.72E-07	0	8.03E-07
KFM09A	20051121 08:51	20051121 10:40	691.00	791.00	3	1	20051121 09:37:30	20051121 10:07:51	8.41E-07	0	1.23E-06
KFM09A	20051128 16:44	20051128 18:19	106.00	126.00	3	1	20051128 17:36:29	20051128 17:56:45	8.47E-06	0	9.98E-06
KFM09A	20051129 06:29	20051129 07:43	126.00	146.00	3	1	20051129 07:01:05	20051129 07:21:21	2.71E-05	0	4.44E-05
KFM09A	20051129 08:20	20051129 09:35	146.00	166.00	3	1	20051129 08:53:25	20051129 09:13:42	4.50E-06	0	1.26E-05
KFM09A	20051129 10:00	20051129 11:15	166.00	186.00	3	1	20051129 10:33:21	20051129 10:53:39	4.24E-05	0	4.98E-05
KFM09A	20051129 12:14	20051129 13:31	186.00	206.00	3	1	20051129 12:48:51	20051129 13:09:11	1.41E-07	0	1.63E-07
KFM09A	20051129 14:01	20051129 14:47	206.00	226.00	3	1	20051129 14:36:49	20051129 14:40:14		-1	
KFM09A	20051129 15:38	20051129 16:56	226.00	246.00	3	1	20051129 16:13:49	20051129 16:34:11	9.72E-07	0	1.18E-06
KFM09A	20051129 17:18	20051129 18:37	238.00	258.00	3	1	20051129 17:54:33	20051129 18:14:55	2.46E-07	0	3.84E-07
KFM09A	20051129 18:58	20051129 20:17	258.00	278.00	3	1	20051129 19:35:15	20051129 19:55:42	5.18E-08	0	9.90E-08
KFM09A	20051129 21:03	20051129 22:25	278.00	298.00	3	1	20051129 21:42:40	20051129 22:03:04	1.11E-07	0	1.57E-07
KFM09A	20051129 22:41	20051129 23:57	286.00	306.00	3	1	20051129 23:15:24	20051129 23:35:54	6.13E-08	0	9.62E-08
KFM09A	20051130 06:29	20051130 07:48	306.00	326.00	3	1	20051130 07:05:44	20051130 07:26:04	2.78E-07	0	6.73E-07
KFM09A	20051130 08:16	20051130 09:35	326.00	346.00	3	1	20051130 08:53:03	20051130 09:13:26	2.09E-08	0	4.56E-08
KFM09A	20051130 10:06	20051130 11:22	346.00	366.00	3	1	20051130 10:40:24	20051130 11:00:46	4.37E-08	0	5.89E-08
KFM09A	20051130 12:06	20051130 13:23	366.00	386.00	3	1	20051130 12:41:16	20051130 13:01:46	1.28E-06	0	1.60E-06
KFM09A	20051130 13:50	20051130 15:08	386.00	406.00	3	1	20051130 14:25:53	20051130 14:46:29	2.69E-06	0	5.50E-06
KFM09A	20051130 15:30	20051130 16:47	406.00	426.00	3	1	20051130 16:04:48	20051130 16:25:26	3.99E-07	0	4.89E-07
KFM09A	20051130 18:18	20051130 19:38	426.00	446.00	3	1	20051130 18:55:34	20051130 19:16:08	1.85E-05	0	4.93E-05
KFM09A	20051130 20:03	20051130 21:45	446.00	466.00	3	1	20051130 21:02:55	20051130 21:23:31	7.09E-08	0	9.94E-08
KFM09A	20051130 22:03	20051130 23:20	466.00	486.00	3	1	20051130 22:37:39	20051130 22:58:37	4.00E-08	0	7.55E-08
KFM09A	20051201 08:06	20051201 09:34	486.00	506.00	3	1	20051201 08:51:37	20051201 09:11:58	1.17E-07	0	2.67E-07

idcode	start_date	stop_date	secup	seclow	test_type	Formation_type	start_flow_period	stop_flow_period	flow_rate_end_qp	Value_type_qp	mean_flow_rate_qm
KFM09A	20051201 10:01	20051201 11:22	506.00	526.00	3	1	20051201 10:39:48	20051201 11:00:08	4.34E-08	0	7.76E-08
KFM09A	20051201 11:41	20051201 13:46	526.00	546.00	3	1	20051201 13:03:33	20051201 13:23:52	2.91E-06	0	9.83E-06
KFM09A	20051201 14:21	20051201 15:09	545.00	565.00	3	1	20051201 14:59:12	20051201 15:02:07		-1	
KFM09A	20051201 15:34	20051201 16:17	566.00	586.00	3	1	20051201 16:08:01	20051201 16:10:17		-1	
KFM09A	20051202 07:55	20051202 08:37	586.00	606.00	3	1	20051202 08:28:21	20051202 08:29:58		-1	
KFM09A	20051202 08:58	20051202 10:22	606.00	626.00	3	1	20051202 09:40:01	20051202 10:00:18	4.76E-07	0	7.39E-07
KFM09A	20051202 10:43	20051202 12:05	626.00	646.00	3	1	20051202 11:22:44	20051202 11:43:05	8.54E-08	0	1.15E-07
KFM09A	20051202 13:12	20051202 14:35	646.00	666.00	3	1	20051202 13:52:57	20051202 14:13:15	1.04E-07	0	1.27E-07
KFM09A	20051202 14:57	20051202 16:13	666.00	686.00	3	1	20051202 15:30:57	20051202 15:51:01	1.19E-08	0	3.11E-08
KFM09A	20051205 08:22	20051205 09:53	686.00	706.00	3	1	20051205 09:10:31	20051205 09:30:35	9.44E-09	0	2.33E-08
KFM09A	20051205 10:10	20051205 11:12	691.00	711.00	3	1	20051205 10:52:46	20051205 11:05:04		-1	
KFM09A	20051205 12:46	20051205 13:30	711.00	731.00	3	1	20051205 13:20:23	20051205 13:22:52		-1	
KFM09A	20051205 13:49	20051205 15:12	731.00	751.00	3	1	20051205 14:29:26	20051205 14:49:46	6.26E-08	0	8.05E-08
KFM09A	20051205 15:30	20051205 16:54	751.00	771.00	3	1	20051205 16:12:15	20051205 16:32:33	3.61E-07	0	1.07E-07
KFM09A	20051205 18:09	20051205 19:26	771.00	791.00	3	1	20051205 18:44:18	20051205 19:04:38	8.90E-07	0	4.69E-05
KFM09A	20051207 07:32	20051207 08:52	106.00	111.00	3	1	20051207 08:10:17	20051207 08:30:41	5.70E-07	0	6.88E-07
KFM09A	20051207 09:08	20051207 10:24	111.00	116.00	3	1	20051207 09:42:13	20051207 10:02:37	6.00E-08	0	7.52E-08
KFM09A	20051221 15:48	20051208 17:51	116.00	121.00	3	1	20051221 16:27:38	20051221 16:47:54	2.15E-06	0	1.42E-07
KFM09A	20051207 12:52	20051207 14:09	121.00	126.00	3	1	20051207 13:26:31	20051207 13:46:51	5.98E-06	0	6.93E-06
KFM09A	20051207 14:26	20051207 16:04	126.00	131.00	3	1	20051207 15:21:48	20051207 15:42:09	3.85E-08	0	1.12E-07
KFM09A	20051207 16:21	20051207 17:40	128.00	133.00	3	1	20051207 16:58:15	20051207 17:18:34	1.74E-05	0	2.61E-05
KFM09A	20051207 17:58	20051207 19:16	133.00	138.00	3	1	20051207 18:34:22	20051207 18:54:23	1.66E-05	0	2.67E-05
KFM09A	20051207 19:42	20051207 21:13	138.00	143.00	3	1	20051207 20:30:41	20051207 20:50:56	3.09E-07	0	3.51E-07
KFM09A	20051207 21:27	20051207 22:45	141.00	146.00	3	1	20051207 22:03:25	20051207 22:23:49	1.24E-06	0	2.35E-06
KFM09A	20051207 23:02	20051208 00:17	146.00	151.00	3	1	20051207 23:35:21	20051207 23:55:41	1.33E-06	0	5.33E-06
KFM09A	20051208 06:16	20051208 06:59	151.00	156.00	3	1	20051208 06:49:42	20051208 06:51:37		-1	
KFM09A	20051208 07:10	20051208 08:26	156.00	161.00	3	1	20051208 07:44:24	20051208 08:04:38	4.26E-06	0	1.07E-05
KFM09A	20051208 08:36	20051208 09:52	161.00	166.00	3	1	20051208 09:10:22	20051208 09:30:41	1.02E-07	0	1.07E-07
KFM09A	20051208 10:03	20051208 11:19	166.00	171.00	3	1	20051208 10:36:39	20051208 10:56:56	4.09E-05	0	4.69E-05
KFM09A	20051208 12:12	20051208 13:29	171.00	176.00	3	1	20051208 12:47:14	20051208 13:07:30	5.50E-08	0	8.37E-07
KFM09A	20051208 13:43	20051208 14:57	176.00	181.00	3	1	20051208 14:15:22	20051208 14:35:42	2.91E-07	0	3.41E-07

idcode	start_date	stop_date	secup	seclow	test_type	Formation_type	start_flow_period	stop_flow_period	flow_rate_end_qp	Value_type_qp	mean_flow_rate_qm
KFM09A	20051208 15:13	20051208 16:28	181.00	186.00	3	1	20051208 15:45:32	20051208 16:05:52	2.50E-07	0	1.90E-06
KFM09A	20051208 16:36	20051208 17:51	186.00	191.00	3	1	20051208 17:09:19	20051208 17:29:36	1.23E-07	0	1.42E-07
KFM09A	20051208 18:03	20051208 18:50	191.00	196.00	3	1	20051208 18:35:40	20051208 18:42:32		-1	
KFM09A	20051208 19:02	20051208 19:47	196.00	201.00	3	1	20051208 19:35:04	20051208 19:39:45		-1	
KFM09A	20051208 19:57	20051208 20:39	201.00	206.00	3	1	20051208 20:30:56	20051208 20:32:09		-1	
KFM09A	20051208 20:58	20051208 21:40	226.00	231.00	3	1	20051208 21:30:25	20051208 21:32:31		-1	
KFM09A	20051208 21:54	20051208 23:08	232.00	237.00	3	1	20051208 22:26:14	20051208 22:46:32	8.39E-07	0	8.63E-07
KFM09A	20051208 23:21	20051209 00:35	237.00	242.00	3	1	20051208 23:52:47	20051209 00:13:05	1.70E-06	0	1.86E-06
KFM09A	20051209 08:08	20051209 09:24	240.80	245.80	3	1	20051209 08:41:39	20051209 09:01:58	3.22E-07	0	4.57E-07
KFM09A	20051221 13:55	20051221 14:35	246.80	251.80	3	1	20051221 14:26:40	20051221 14:28:04		-1	
KFM09A	20051209 09:40	20051209 10:22	251.50	256.50	3	1	20051209 10:12:05	20051209 10:14:57		-1	
KFM09A	20051209 10:34	20051209 11:18	256.50	261.50	3	1	20051209 11:06:25	20051209 11:10:31		-1	
KFM09A	20051209 11:30	20051209 13:22	273.00	278.00	3	1	20051209 12:39:59	20051209 13:00:19	6.80E-08	0	1.00E-07
KFM09A	20051209 13:34	20051209 14:48	278.00	283.00	3	1	20051209 14:05:39	20051209 14:26:00	9.75E-08	0	1.44E-07
KFM09A	20051209 15:04	20051209 15:51	283.00	288.00	3	1	20051209 15:36:41	20051209 15:44:08		-1	
KFM09A	20051209 16:00	20051209 17:15	288.00	293.00	3	1	20051209 16:33:16	20051209 16:53:38	1.57E-08	0	2.83E-08
KFM09A	20051212 08:21	20051212 09:42	293.00	298.00	3	1	20051212 08:59:52	20051212 09:20:12	3.38E-08	0	4.10E-08
KFM09A	20051221 12:39	20051221 13:28	296.00	301.00	3	1	20051221 13:11:23	20051221 13:21:20		-1	
KFM09A	20051221 11:45	20051221 12:29	301.00	306.00	3	1	20051221 12:18:01	20051221 12:21:31		-1	
KFM09A	20051212 09:58	20051212 10:39	306.00	311.00	3	1	20051212 10:30:37	20051212 10:31:58		-1	
KFM09A	20051212 10:49	20051212 12:33	311.00	316.00	3	1	20051212 12:23:33	20051212 12:25:31		-1	
KFM09A	20051212 12:43	20051212 13:31	316.00	321.00	3	1	20051212 13:19:35	20051212 13:23:52		-1	
KFM09A	20051212 13:44	20051212 15:02	321.00	326.00	3	1	20051212 14:20:06	20051212 14:40:29	2.98E-07	0	6.68E-07
KFM09A	20051212 15:31	20051212 16:14	346.00	351.00	3	1	20051212 16:05:39	20051212 16:06:46		-1	
KFM09A	20051221 10:04	20051221 11:19	351.00	356.00	3	1	20051021 10:36:43	20051021 10:56:56	5.07E-08	0	6.90E-08
KFM09A	20051221 08:54	20051221 09:50	356.00	361.00	3	1	20051221 09:25:06	20051221 09:43:27		-1	
KFM09A	20051221 07:28	20051221 08:43	361.00	366.00	3	1	20051221 08:00:40	20051221 08:20:51	1.76E-08	0	9.48E-09
KFM09A	20051212 16:39	20051212 17:54	363.00	368.00	3	1	20051212 17:11:54	20051212 17:32:16	1.17E-08	0	1.62E-08
KFM09A	20051213 06:27	20051213 07:24	368.00	373.00	3	1	20051213 07:15:59	20051213 07:17:12		-1	
KFM09A	20051213 07:35	20051213 08:48	371.00	376.00	3	1	20051213 08:09:41	20051213 08:23:48	1.47E-06	0	2.13E-06
KFM09A	20051213 09:02	20051213 09:58	376.00	381.00	3	1	20051213 09:37:12	20051213 09:51:20		-1	
KFM09A	20051213 10:10	20051213 11:25	381.00	386.00	3	1	20051213 10:42:36	20051213 11:02:40		-1	

idcode	start_date	stop_date	secup	seclow	test_type	Formation_type	start_flow_period	stop_flow_period	flow_rate_end_qp	Value_type_qp	mean_flow_rate_qm
KFM09A	20051213 11:57	20051213 13:16	386.00	391.00	3	1	20051213 12:33:30	20051213 12:53:52	2.47E-06	0	5.33E-06
KFM09A	20051213 13:28	20051213 14:48	391.00	396.00	3	1	20051213 14:05:53	20051213 14:26:16	1.66E-07	0	1.87E-07
KFM09A	20051213 15:06	20051213 15:49	396.00	401.00	3	1	20051213 15:37:15	20051213 15:41:39		-1	
KFM09A	20051213 16:00	20051213 17:15	401.00	406.00	3	1	20051213 16:33:21	20051213 16:53:44	4.26E-07	0	4.98E-07
KFM09A	20051213 17:25	20051213 18:18	406.00	411.00	3	1	20051213 17:56:34	20051213 18:10:55		-1	
KFM09A	20051213 18:36	20051213 19:50	411.00	416.00	3	1	20051213 19:07:32	20051213 19:27:56	3.70E-07	0	5.52E-07
KFM09A	20051213 20:06	20051213 21:22	414.00	419.00	3	1	20051213 20:39:31	20051213 20:59:55	1.30E-08	0	1.05E-08
KFM09A	20051213 21:32	20051213 22:46	419.00	424.00	3	1	20051213 22:04:11	20051213 22:24:35	5.68E-08	0	6.90E-08
KFM09A	20051213 22:55	20051214 00:09	421.00	426.00	3	1	20051213 23:26:44	20051213 23:47:06	5.78E-08	0	7.13E-08
KFM09A	20051214 06:51	20051214 07:59	426.00	431.00	3	1	20051214 07:32:04	20051214 07:52:07		-1	
KFM09A	20051214 08:11	20051214 09:31	431.00	436.00	3	1	20051214 08:49:02	20051214 09:09:24	1.61E-05	0	5.02E-05
KFM09A	20051214 09:47	20051214 10:29	436.00	441.00	3	1	20051214 10:20:56	20051214 10:22:10		-1	
KFM09A	20051214 10:44	20051214 12:00	441.00	446.00	3	1	20051214 11:18:15	20051214 11:38:42	2.09E-07	0	1.94E-06
KFM09A	20051214 12:13	20051214 14:04	446.00	451.00	3	1	20051214 13:21:31	20051214 13:41:55	3.75E-08	0	1.55E-07
KFM09A	20051214 14:22	20051214 15:38	451.00	456.00	3	1	20051214 14:56:20	20051214 15:16:46	1.24E-08	0	1.48E-08
KFM09A	20051214 15:55	20051214 17:12	456.00	461.00	3	1	20051214 16:30:00	20051214 16:50:24	6.76E-08	0	5.90E-08
KFM09A	20051214 17:32	20051214 18:15	461.00	466.00	3	1	20051214 18:04:52	20051214 18:07:43		-1	
KFM09A	20051214 18:35	20051214 19:50	471.00	476.00	3	1	20051214 19:08:00	20051214 19:28:26	5.28E-08	0	7.96E-08
KFM09A	20051214 20:01	20051214 21:23	476.00	481.00	3	1	20051214 20:40:37	20051214 21:00:58	4.27E-08	0	5.18E-08
KFM09A	20051214 21:40	20051214 22:31	486.00	491.00	3	1	20051214 22:17:49	20051214 22:23:53		-1	
KFM09A	20051214 22:58	20051215 00:12	491.00	496.00	3	1	20051214 23:29:36	20051214 23:49:58	7.80E-08	0	1.03E-07
KFM09A	20051215 06:33	20051215 07:57	496.00	501.00	3	1	20051215 07:15:10	20051215 07:35:32	6.24E-08	0	1.75E-07
KFM09A	20051215 08:14	20051215 09:00	501.00	506.00	3	1	20051215 08:47:17	20051215 08:53:08		-1	
KFM09A	20051220 19:00	20051220 20:23	506.00	511.00	3	1	20051220 19:41:12	20051220 20:01:35	1.64E-08	0	1.77E-08
KFM09A	20051220 20:50	20051220 22:05	511.00	516.00	3	1	20051220 21:22:36	20051220 21:42:55	2.98E-08	0	2.82E-08
KFM09A	20051220 22:14	20051220 23:28	516.00	521.00	3	1	20051220 22:45:57	20051220 23:06:17	1.94E-08	0	2.24E-08
KFM09A	20051215 09:25	20051215 10:11	521.00	526.00	3	1	20051215 10:01:53	20051215 10:03:44		-1	
KFM09A	20051215 10:26	20051215 11:07	526.00	531.00	3	1	20051215 10:58:38	20051215 10:59:49		-1	
KFM09A	20051215 11:23	20051215 12:44	531.00	536.00	3	1	20051215 12:01:54	20051215 12:22:16	2.91E-06	0	1.06E-05
KFM09A	20051215 13:19	20051215 14:03	536.00	541.00	3	1	20051215 13:52:58	20051215 13:56:08		-1	
KFM09A	20051215 14:14	20051215 15:28	541.00	546.00	3	1	20051215 14:46:13	20051215 15:06:37	8.67E-09	0	5.55E-08
KFM09A	20051220 17:14	20051220 17:58	561.00	566.00	3	1	20051220 17:49:31	20051220 17:50:36		-1	

idcode	start_date	stop_date	secup	seclow	test_type	Formation_type	start_flow_period	stop_flow_period	flow_rate_end_qp	Value_type_qp	mean_flow_rate_qm
KFM09A	20051215 16:19	20051215 17:00	606.00	611.00	3	1	20051215 16:50:43	20051215 16:52:47		-1	
KFM09A	20051215 17:19	20051215 18:35	611.00	616.00	3	1	20051215 17:52:51	20051215 18:13:12	3.96E-07	0	6.14E-07
KFM09A	20051215 18:50	20051215 19:31	616.00	621.00	3	1	20051215 19:21:48	20051215 19:23:40		-1	
KFM09A	20051215 19:44	20051215 21:03	621.00	626.00	3	1	20051215 20:21:06	20051215 20:41:34	1.53E-07	0	2.22E-07
KFM09A	20051215 21:14	20051215 22:01	626.00	631.00	3	1	20051215 21:45:46	20051215 21:54:10		-1	
KFM09A	20051215 22:08	20051215 23:33	631.00	636.00	3	1	20051215 22:51:11	20051215 23:11:40	1.17E-08	0	2.06E-08
KFM09A	20051215 23:43	20051216 00:58	636.00	641.00	3	1	20051216 00:15:28	20051216 00:35:56	1.35E-07	0	1.34E-07
KFM09A	20051216 08:21	20051216 09:36	641.00	646.00	3	1	20051216 08:53:39	20051216 09:14:01	1.27E-08	0	9.09E-07
KFM09A	20051216 09:55	20051216 10:38	646.00	651.00	3	1	20051216 10:28:16	20051216 10:31:02		-1	
KFM09A	20051216 10:53	20051216 12:10	651.00	656.00	3	1	20051216 11:27:51	20051216 11:48:20	1.27E-07	0	2.02E-05
KFM09A	20051216 12:21	20051216 13:20	656.00	661.00	3	1	20051216 13:03:34	20051216 13:12:30		-1	
KFM09A	20051216 13:31	20051216 14:14	661.00	666.00	3	1	20051216 14:04:48	20051216 14:06:57		-1	
KFM09A	20051219 08:19	20051219 09:01	731.00	736.00	3	1	20051219 08:52:49	20051219 08:54:27		-1	
KFM09A	20051219 09:15	20051219 09:56	736.00	741.00	3	1	20051219 09:46:55	20051219 09:49:06		-1	
KFM09A	20051219 10:11	20051219 11:30	741.00	746.00	3	1	20051219 10:47:39	20051219 11:08:09	8.87E-08	0	7.57E-08
KFM09A	20051219 11:44	20051219 12:36	746.00	751.00	3	1	20051219 12:22:11	20051219 12:29:10		-1	
KFM09A	20051219 12:50	20051219 14:05	751.00	756.00	3	1	20051219 13:23:07	20051219 13:43:35	7.95E-08	0	1.26E-07
KFM09A	20051219 14:20	20051219 15:42	756.00	761.00	3	1	20051219 15:00:30	20051219 15:20:59	2.15E-07	0	3.66E-07
KFM09A	20051219 15:56	20051219 17:16	761.00	766.00	3	1	20051219 16:33:37	20051219 16:54:07	1.07E-07	0	1.57E-07
KFM09A	20051220 06:55	20051220 08:10	766.00	771.00	3	1	20051220 07:28:05	20051220 07:48:28	5.47E-08	0	7.57E-08
KFM09A	20051220 08:29	20051220 09:46	771.00	776.00	3	1	20051220 09:04:02	20051220 09:24:27	5.99E-08	0	6.39E-08
KFM09A	20051220 10:06	20051220 11:24	776.00	781.00	3	1	20051220 10:41:52	20051220 11:02:21	1.15E-07	0	1.40E-07
KFM09A	20051220 11:35	20051220 12:58	781.00	786.00	3	1	20051220 12:15:53	20051220 12:36:19	1.85E-07	0	2.36E-07
KFM09A	20051220 13:11	20051220 14:28	786.00	791.00	3	1	20051220 13:46:19	20051220 14:06:43	7.06E-07	0	9.09E-07
KFM09A	20051118 13:32	20051118 14:28	506.00 [1)]	606.00	3	1	20051118 14:18:02	20051118 14:26:00			
KFM09A	20051130 17:10	20051130 18:03	426.00[1)]	446.00	3	1	20051130 17:43:55	20051130 17:56:57			
KFM09A	20051207 10:38	20051207 12:39	116.00[1)]	121.00	3	1	20051207 12:36:48	20051207 12:38:34			

[1)] Incomplete test, interrupted and re-performed later.

KFM09A plu_s_hole_test_d. Right (This result table to SICADA includes more columns which are empty, these columns are not presented here.)

idcode	secup	seclow	q_measl__l	q_measl__u	tot_volume_vp	dur_flow_phase_tp	dur_rec_phase_tf	initial_press_pi	press_at_flow_end_pp	final_press_pf	fluid_temp_tew
KFM09A	106.00	206.00	1.7E-08	1.0E-03	1.70E-01	1819	1800	929.78	1114.19	948.54	7.92
KFM09A	206.00	306.00	1.7E-08	1.0E-03	2.95E-03	1822	1800	1746.27	1963.05	1759.94	8.08
KFM09A	306.00	406.00	1.7E-08	1.0E-03	1.31E-02	1827	1797	2542.61	2753.18	2631.48	8.87
KFM09A	406.00	506.00	1.7E-08	1.0E-03	6.87E-02	1821	1800	3314.26	3517.70	3472.12	9.51
KFM09A	506.00	606.00	1.7E-08	1.0E-03	1.48E-02	1821	1800	4075.97	4296.20	4263.63	10.58
KFM09A	606.00	706.00	1.7E-08	1.0E-03	1.46E-03	1820	1803	4781.92	4987.26	4843.19	11.54
KFM09A	691.00	791.00	1.7E-08	1.0E-03	2.24E-03	1821	1801	5371.98	5548.07	5405.64	12.22
KFM09A	106.00	126.00	1.7E-08	1.0E-03	1.22E-02	1216	1206	939.44	1152.92	946.07	7.29
KFM09A	126.00	146.00	1.7E-08	1.0E-03	5.40E-02	1216	1206	1108.50	1324.71	1158.02	7.35
KFM09A	146.00	166.00	1.7E-08	1.0E-03	1.54E-02	1217	1200	1277.24	1460.00	1389.29	7.52
KFM09A	166.00	186.00	1.7E-08	1.0E-03	6.07E-02	1218	1205	1439.66	1628.85	1451.67	7.50
KFM09A	186.00	206.00	1.7E-08	1.0E-03	1.99E-04	1220	1202	1609.00	1908.70	1627.19	7.82
KFM09A	206.00	226.00	5.1E-09	1.0E-03		205	321	1799.82	1971.07	1959.47	7.99
KFM09A	226.00	246.00	1.7E-08	1.0E-03	1.45E-03	1222	1200	1936.29	2142.18	1942.92	8.15
KFM09A	238.00	258.00	1.7E-08	1.0E-03	4.70E-04	1222	1197	2036.61	2246.50	2073.17	8.27
KFM09A	258.00	278.00	1.7E-08	1.0E-03	1.22E-04	1227	1194	2205.79	2409.18	2271.89	8.43
KFM09A	278.00	298.00	1.7E-08	1.0E-03	1.92E-04	1224	1194	2363.51	2574.60	2423.68	8.61
KFM09A	286.00	306.00	1.7E-08	1.0E-03	1.19E-04	1230	1191	2426.85	2640.10	2497.64	8.67
KFM09A	306.00	326.00	1.7E-08	1.0E-03	8.23E-04	1220	1203	2588.71	2788.52	2720.63	8.83
KFM09A	326.00	346.00	1.7E-08	1.0E-03	5.58E-05	1223	1202	2751.68	2952.80	2816.12	8.99
KFM09A	346.00	366.00	1.7E-08	1.0E-03	7.20E-05	1222	1200	2908.57	3113.84	2949.69	9.17
KFM09A	366.00	386.00	1.7E-08	1.0E-03	1.98E-03	1230	1189	3063.39	3264.59	3103.70	9.33
KFM09A	386.00	406.00	1.7E-08	1.0E-03	6.80E-03	1236	1185	3219.88	3419.73	3326.14	9.51
KFM09A	406.00	426.00	1.7E-08	1.0E-03	6.05E-04	1238	1184	3378.16	3578.01	3432.11	9.68
KFM09A	426.00	446.00	1.7E-08	1.0E-03	6.10E-02	1234	1185	3545.41	3765.49	3714.71	9.66
KFM09A	446.00	466.00	1.7E-08	1.0E-03	1.23E-04	1236	1184	3693.33	3922.81	3730.72	10.03
KFM09A	466.00	486.00	1.7E-08	1.0E-03	9.52E-05	1258	1162	3856.58	4029.33	3923.36	10.21
KFM09A	486.00	506.00	1.7E-08	1.0E-03	3.27E-04	1221	1200	4001.32	4206.10	4108.27	10.39

idcode	secup	seclow	q_measl__l	q_measl__u	tot_volume_vp	dur_flow_phase_tp	dur_rec_phase_tf	initial_press_pi	press_at_flow_end_pp	final_press_pf	fluid_temp_tew
KFM09A	506.00	526.00	1.7E-08	1.0E-03	9.50E-05	1220	1200	4171.74	4362.23	4210.38	10.56
KFM09A	526.00	546.00	1.7E-08	1.0E-03	1.20E-02	1219	1203	4303.10	4508.03	4472.57	10.73
KFM09A	545.00	565.00	5.1E-09	1.0E-03		175	321	4514.10	4661.19	4675.69	10.91
KFM09A	566.00	586.00	5.1E-09	1.0E-03		136	321	4631.11	4820.31	4823.61	11.09
KFM09A	586.00	606.00	5.1E-09	1.0E-03		97	322	4765.93	4982.58	4989.21	11.28
KFM09A	606.00	626.00	1.7E-08	1.0E-03	9.01E-04	1217	1205	4896.47	5096.82	4980.92	11.45
KFM09A	626.00	646.00	1.7E-08	1.0E-03	1.41E-04	1221	1200	5050.61	5258.42	5072.55	11.61
KFM09A	646.00	666.00	1.7E-08	1.0E-03	1.55E-04	1218	1205	5186.25	5389.93	5211.64	11.79
KFM09A	666.00	686.00	5.1E-09	1.0E-03	3.74E-05	1204	1221	5355.15	5533.99	5469.96	11.97
KFM09A	686.00	706.00	5.1E-09	1.0E-03	2.81E-05	1204	1221	5498.11	5687.43	5619.55	12.13
KFM09A	691.00	711.00	3.9E-09	1.0E-03		738	321	5561.73	5724.42	5713.38	12.17
KFM09A	711.00	731.00	3.9E-09	1.0E-03		149	321	5679.43	5864.34	5869.58	12.36
KFM09A	731.00	751.00	1.7E-08	1.0E-03	9.84E-05	1220	1203	5782.93	5995.56	5819.36	12.52
KFM09A	751.00	771.00	1.7E-08	1.0E-03	1.31E-04	1218	1203	5915.12	6118.38	1406.62	12.67
KFM09A	771.00	791.00	1.7E-08	1.0E+00	5.72E-02	1220	1184	6056.14	6271.55	1456.30	12.83
KFM09A	106.00	111.00	1.7E-08	1.0E-03	8.42E-04	1224	1195	948.90	1151.62	995.96	7.28
KFM09A	111.00	116.00	1.7E-08	1.0E-03	9.20E-05	1224	1197	993.19	1200.74	1037.91	7.30
KFM09A	116.00	121.00	1.7E-08	1.1E+01	1.73E-04	1216	1206	1025.62	1225.72	1627.41	7.26
KFM09A	121.00	126.00	1.7E-08	1.0E-03	8.47E-03	1220	1197	1074.34	1252.70	1076.55	7.31
KFM09A	126.00	131.00	1.7E-08	1.0E-03	1.37E-04	1221	1196	1121.53	1323.83	1249.86	7.42
KFM09A	128.00	133.00	1.7E-08	1.0E-03	3.18E-02	1219	1197	1131.88	1348.66	1163.76	7.30
KFM09A	133.00	138.00	1.7E-08	1.0E-03	3.21E-02	1201	1197	1174.24	1409.45	1217.29	7.36
KFM09A	138.00	143.00	1.7E-08	1.0E-03	4.28E-04	1215	1197	1215.08	1415.79	1219.50	7.51
KFM09A	141.00	146.00	1.7E-08	1.0E-03	2.88E-03	1224	1194	1240.89	1466.23	1321.06	7.53
KFM09A	146.00	151.00	1.7E-08	1.0E-03	6.51E-03	1220	1187	1284.09	1510.35	1450.22	7.53
KFM09A	151.00	156.00	5.1E-09	1.0E-03		115	321	1349.21	1565.72	1571.10	7.56
KFM09A	156.00	161.00	1.7E-08	1.0E-03	1.31E-02	1214	1197	1365.50	1573.10	1482.79	7.57
KFM09A	161.00	166.00	1.7E-08	1.0E-03	1.31E-04	1219	1199	1408.00	1586.50	1406.62	7.70
KFM09A	166.00	171.00	1.7E-08	1.0E-03	5.72E-02	1217	1200	1447.05	1626.80	1456.30	7.44
KFM09A	171.00	176.00	1.7E-08	1.0E-03	1.03E-03	1216	1184	1496.45	1703.03	1687.02	7.76
KFM09A	176.00	181.00	1.7E-08	1.0E-03	4.15E-04	1220	1199	1534.00	1734.49	1557.86	7.76

idcode	secup	seclow	q_measl__l	q_measl__u	tot_volume_vp	dur_flow_phase_tp	dur_rec_phase_tf	initial_press_pi	press_at_flow_end_pp	final_press_pf	fluid_temp_tew
KFM09A	181.00	186.00	1.7E-08	1.0E-03	2.35E-03	1220	1184	1575.38	1803.90	1780.30	7.77
KFM09A	186.00	191.00	1.7E-08	1.0E-03	1.73E-04	1217	1200	1616.92	1832.60	1627.41	7.81
KFM09A	191.00	196.00	5.3E-09	1.0E-03		412	322	1677.49	1875.23	1828.87	7.85
KFM09A	196.00	201.00	4.1E-09	1.0E-03		281	321	1710.62	1916.50	1891.79	7.88
KFM09A	201.00	206.00	5.3E-09	1.0E-03		73	322	1766.78	1957.48	1965.21	7.93
KFM09A	226.00	231.00	5.3E-09	1.0E-03		126	321	1961.89	2161.15	2158.94	8.13
KFM09A	232.00	237.00	1.7E-08	1.0E-03	1.05E-03	1218	1202	1992.95	2191.65	1995.02	8.20
KFM09A	237.00	242.00	1.7E-08	1.0E-03	2.27E-03	1218	1203	2032.55	2232.77	2040.28	8.25
KFM09A	240.80	245.80	1.7E-08	1.0E-03	5.58E-04	1219	1202	2060.01	2263.69	2071.18	8.29
KFM09A	246.80	251.80	4.1E-09	1.0E+01		84	322	2184.89	2323.99	2971.99	8.27
KFM09A	251.50	256.50	5.3E-09	1.0E-03		172	321	2217.45	2385.25	2408.43	8.35
KFM09A	256.50	261.50	6.5E-09	1.0E-03		246	321	2239.39	2427.20	2424.45	8.39
KFM09A	273.00	278.00	1.7E-08	1.0E-03	1.22E-04	1220	1200	2328.68	2560.78	2393.53	8.54
KFM09A	278.00	283.00	1.7E-08	1.0E-03	1.76E-04	1221	1202	2369.80	2576.30	2435.48	8.58
KFM09A	283.00	288.00	5.3E-09	1.0E-03		447	321	2409.26	2618.73	2574.58	8.62
KFM09A	288.00	293.00	1.0E-08	1.0E-03	3.40E-05	1222	1221	2459.90	2659.88	2540.35	8.67
KFM09A	293.00	298.00	1.7E-08	1.0E-03	5.00E-05	1220	1203	2493.43	2728.00	2549.74	8.71
KFM09A	296.00	301.00	4.1E-09	7.0E+00		597	322	2521.45	2730.23	3349.53	8.72
KFM09A	301.00	306.00	4.1E-09	8.0E+00		210	321	2567.81	2767.21	3301.51	8.73
KFM09A	306.00	311.00	6.5E-09	1.0E-03		81	321	2678.48	2831.80	2864.35	8.81
KFM09A	311.00	316.00	2.8E-09	1.0E-03		118	322	2652.96	2872.36	2868.77	8.85
KFM09A	316.00	321.00	4.1E-09	1.0E-03		257	321	2674.48	2942.73	2935.01	8.88
KFM09A	321.00	326.00	1.7E-08	1.0E-03	8.16E-04	1223	1202	2712.56	2913.42	2845.04	8.94
KFM09A	346.00	351.00	6.5E-09	1.0E-03		67	321	3017.39	3117.02	3125.44	9.14
KFM09A	351.00	356.00	1.7E-08	3.0E+00	8.44E-05	1213	1211	2958.18	3169.22	3512.92	9.19
KFM09A	356.00	361.00	4.1E-09	4.0E+00		1101	321	2991.17	3206.99	3532.23	9.25
KFM09A	361.00	366.00	4.1E-09	5.0E+00	1.14E-05	1211	1221	3026.22	3242.46	3698.38	9.25
KFM09A	363.00	368.00	5.0E-09	1.0E-03	1.95E-05	1222	1221	3062.65	3254.73	3095.07	9.29
KFM09A	368.00	373.00	5.3E-09	1.0E-03		73	321	3128.47	3316.41	3294.88	9.35
KFM09A	371.00	376.00	1.7E-08	1.0E-03	2.12E-03	847	1221	3108.19	3309.50	3140.33	9.38
KFM09A	376.00	381.00	5.0E-09	1.0E-03		848	321	3174.01	3361.53	3334.08	9.40
KFM09A	381.00	386.00	5.3E-09	1.0E-03		1204	1221	3234.58	3403.07	3284.95	9.45

idcode	secup	seclow	q_measl__l	q_measl__u	tot_volume_vp	dur_flow_phase_tp	dur_rec_phase_tf	initial_press_pi	press_at_flow_end_pp	final_press_pf	fluid_temp_tew
KFM09A	386.00	391.00	1.7E-08	1.0E-03	6.53E-03	1222	1200	3226.58	3437.98	3349.53	9.52
KFM09A	391.00	396.00	1.7E-08	1.0E-03	2.29E-04	1223	1202	3274.47	3481.73	3301.51	9.55
KFM09A	396.00	401.00	6.5E-09	1.0E-03		264	321	3321.10	3524.50	3485.87	9.57
KFM09A	401.00	406.00	1.7E-08	1.0E-03	6.09E-04	1223	1200	3346.08	3547.69	3369.95	9.61
KFM09A	406.00	411.00	5.3E-09	1.0E-03		861	321	3392.03	3584.11	3550.45	9.65
KFM09A	411.00	416.00	1.7E-08	1.0E-03	6.76E-04	1224	1200	3426.25	3621.31	3496.35	9.69
KFM09A	414.00	419.00	5.3E-09	1.0E-03	1.27E-05	1224	1221	3460.47	3654.12	3480.91	9.72
KFM09A	419.00	424.00	1.7E-08	1.0E-03	8.44E-05	1224	1200	3488.63	3692.58	3512.92	9.77
KFM09A	421.00	426.00	1.7E-08	1.0E-03	8.73E-05	1222	1200	3515.00	3708.32	3532.23	9.79
KFM09A	426.00	431.00	7.8E-09	1.0E-03		1203	322	3560.79	3773.30	3698.38	9.89
KFM09A	431.00	436.00	1.7E-08	1.0E-03	6.15E-02	1222	1200	3579.70	3802.83	3753.02	9.65
KFM09A	436.00	441.00	6.0E-09	1.0E-03		74	321	3649.79	3829.74	3837.47	10.00
KFM09A	441.00	446.00	1.7E-08	1.0E-03	2.41E-03	1227	1182	3661.40	3888.20	3871.14	10.03
KFM09A	446.00	451.00	1.7E-08	1.0E-03	1.90E-04	1224	1200	3702.24	3909.77	3866.72	10.02
KFM09A	451.00	456.00	5.3E-09	1.0E-03	1.78E-05	1226	1221	3761.02	3951.96	3840.22	10.05
KFM09A	456.00	461.00	1.7E-08	1.0E-03	7.22E-05	1224	1200	3787.78	3990.92	3815.94	10.09
KFM09A	461.00	466.00	2.8E-09	1.0E-03		171	322	3916.81	4031.76	4071.50	10.13
KFM09A	471.00	476.00	1.7E-08	1.0E-03	9.75E-05	1226	1199	3902.46	4111.10	3964.42	10.23
KFM09A	476.00	481.00	1.7E-08	1.0E-03	6.33E-05	1221	1203	3964.43	4153.74	4008.03	10.28
KFM09A	486.00	491.00	5.3E-09	1.0E-03		364	321	4047.08	4229.36	4217.76	10.36
KFM09A	491.00	496.00	1.7E-08	1.0E-03	1.26E-04	1222	1200	4063.22	4261.51	4095.23	10.41
KFM09A	496.00	501.00	1.7E-08	1.0E-03	2.15E-04	1222	1200	4090.13	4297.53	4222.18	10.46
KFM09A	501.00	506.00	5.0E-09	1.0E-03		351	321	4165.19	4330.23	4289.52	10.49
KFM09A	506.00	511.00	4.1E-09	1.0E-03	2.13E-05	1223	1221	4215.56	4366.80	4289.52	10.54
KFM09A	511.00	516.00	1.7E-08	1.0E-03	3.44E-05	1219	1206	4232.67	4403.23	4229.36	10.60
KFM09A	516.00	521.00	7.7E-09	1.0E-03	2.70E-05	1220	1221	4254.20	4440.03	4285.67	10.63
KFM09A	521.00	526.00	5.3E-09	1.0E-03		111	321	4405.30	4484.51	4539.01	10.67
KFM09A	526.00	531.00	5.3E-09	1.0E-03		71	321	4442.14	4520.81	4592.00	10.73
KFM09A	531.00	536.00	1.7E-08	1.0E-03	1.30E-02	1222	1199	4354.65	4571.03	4535.15	10.76
KFM09A	536.00	541.00	5.3E-09	1.0E-03		190	320	4479.13	4594.76	4560.54	10.86
KFM09A	541.00	546.00	5.3E-09	1.0E-03	6.67E-05	1224	1221	4437.45	4632.29	4613.53	10.88
KFM09A	561.00	566.00	5.3E-09	1.0E-03		65	321	4726.95	4774.42	4801.19	11.02

idcode	secup	seclow	q_measl__l	q_measl__u	tot_volume_vp	dur_flow_phase_tp	dur_rec_phase_tf	initial_press_pi	press_at_flow_end_pp	final_press_pf	fluid_temp_tew
KFM09A	606.00	611.00	4.1E-09	1.0E-03		124	322	5042.26	5120.24	5224.00	11.42
KFM09A	611.00	616.00	1.7E-08	1.0E-03	7.50E-04	1221	1200	4956.43	5148.26	5044.06	11.46
KFM09A	616.00	621.00	5.3E-09	1.0E-03		112	322	5077.59	5206.34	5272.02	11.51
KFM09A	621.00	626.00	1.7E-08	1.0E-03	2.73E-04	1228	1194	5032.46	5244.56	5127.97	11.55
KFM09A	626.00	631.00	4.1E-09	1.0E-03		504	322	5085.18	5263.75	5233.38	11.60
KFM09A	631.00	636.00	5.3E-09	1.0E-03	2.47E-05	1229	1220	5136.79	5301.28	5249.39	11.64
KFM09A	636.00	641.00	1.7E-08	1.0E-03	1.64E-04	1228	1194	5144.52	5335.36	5146.73	11.68
KFM09A	641.00	646.00	2.8E-09	1.0E-03	1.11E-03	1222	1221	5195.30	5374.69	5235.59	11.75
KFM09A	646.00	651.00	2.8E-09	1.0E-03		166	321	5309.69	5410.56	5419.40	11.78
KFM09A	651.00	656.00	1.7E-08	1.0E-03	9.65E-03	1229	1194	5248.56	5444.23	5280.30	11.82
KFM09A	656.00	661.00	6.5E-09	1.0E-03		536	321	5344.46	5486.74	5472.94	11.87
KFM09A	661.00	666.00	4.1E-09	1.0E-03		129	321				
KFM09A	731.00	736.00	5.3E-09	1.0E-03		98	321	5867.31	6009.44	5986.26	12.49
KFM09A	736.00	741.00	5.3E-09	1.0E-03		131	321	5860.27	6044.22	5996.20	12.57
KFM09A	741.00	746.00	1.7E-08	1.0E-03	9.31E-05	1230	1191	5881.11	6078.44	5914.50	12.59
KFM09A	746.00	751.00	5.3E-09	1.0E-03		419	321	5928.44	6112.66	6074.02	12.64
KFM09A	751.00	756.00	1.7E-08	1.0E-03	1.55E-04	1228	1194	5957.42	6143.29	6000.07	12.66
KFM09A	756.00	761.00	1.7E-08	1.0E-03	4.51E-04	1229	1189	5986.68	6192.63	6040.91	12.71
KFM09A	761.00	766.00	1.7E-08	1.0E-03	1.92E-04	1230	1199	6021.04	6221.97	6050.29	12.75
KFM09A	766.00	771.00	1.7E-08	1.0E-03	9.27E-05	1223	1187	6049.32	6239.82	6077.34	12.79
KFM09A	771.00	776.00	1.7E-08	1.0E-03	7.84E-05	1225	1187	6086.85	6319.41	6096.65	12.83
KFM09A	776.00	781.00	1.7E-08	1.0E-03	1.71E-04	1229	1187	6119.15	6309.34	6137.49	12.87
KFM09A	781.00	786.00	1.7E-08	1.0E-03	2.90E-04	1226	1187	6152.12	6325.44	6168.40	12.92
KFM09A	786.00	791.00	1.7E-08	1.0E-03	1.11E-03	1224	1187	6184.96	6388.23	6192.69	12.96
KFM09A	506.00 [1)]	606.00				478	24	4063.27	4265.15	4264.74	10.56
KFM09A	426.00[1)]	446.00				782	253	3535.19	3703.67	3675.53	9.70
KFM09A	116.00[1)]	121.00				106	13	1074.89	1242.69	1074.34	7.32

[1)] Incomplete test, interrupted and re-performed later.

KFM09A plu_s_hole_test_ed1. Left (This result table to SICADA includes more columns which are empty, these columns are not presented here.)

idcode	start_date	stop_date	secup	seclow	test_type	formation_type	spec_capacity_q_s	value_type_q_s	transmissivity_moye	bc_tm	value_type_tm	hydr_cond_moye	formation_width_b
KFM09A	20051117 16:09	20051117 17:59	106.00	206.00	3	1	3.76E-06	0	4.89E-06	0	0	4.89E-08	100.00
KFM09A	20051117 19:03	20051117 20:53	206.00	306.00	3	1	5.92E-08	0	7.69E-08	0	0	7.69E-10	100.00
KFM09A	20051117 21:47	20051117 23:36	306.00	406.00	3	1	1.89E-07	0	2.46E-07	0	0	2.46E-09	100.00
KFM09A	20051118 09:59	20051118 11:49	406.00	506.00	3	1	5.18E-07	0	6.74E-07	1	0	6.74E-09	100.00
KFM09A	20051121 12:52	20051121 15:13	506.00	606.00	3	1	8.66E-08	0	1.13E-07	1	0	1.13E-09	100.00
KFM09A	20051121 06:14	20051121 08:03	606.00	706.00	3	1	2.74E-08	0	3.56E-08	0	0	3.56E-10	100.00
KFM09A	20051121 08:51	20051121 10:40	691.00	791.00	3	1	4.69E-08	0	6.09E-08	0	0	6.09E-10	100.00
KFM09A	20051128 16:44	20051128 18:19	106.00	126.00	3	1	3.89E-07	0	4.06E-07	0	0	2.03E-08	20.00
KFM09A	20051129 06:29	20051129 07:43	126.00	146.00	3	1	1.23E-06	0	1.28E-06	0	0	6.42E-08	20.00
KFM09A	20051129 08:20	20051129 09:35	146.00	166.00	3	1	2.41E-07	0	2.52E-07	0	0	1.26E-08	20.00
KFM09A	20051129 10:00	20051129 11:15	166.00	186.00	3	1	2.20E-06	0	2.29E-06	0	0	1.15E-07	20.00
KFM09A	20051129 12:14	20051129 13:31	186.00	206.00	3	1	4.62E-09	0	4.82E-09	0	0	2.41E-10	20.00
KFM09A	20051129 14:01	20051129 14:47	206.00	226.00	3	1	2.55E-10	-1	2.66E-10	0	-1	1.33E-11	20.00
KFM09A	20051129 15:38	20051129 16:56	226.00	246.00	3	1	4.63E-08	0	4.83E-08	0	0	2.42E-09	20.00
KFM09A	20051129 17:18	20051129 18:37	238.00	258.00	3	1	1.15E-08	0	1.20E-08	0	0	6.00E-10	20.00
KFM09A	20051129 18:58	20051129 20:17	258.00	278.00	3	1	2.50E-09	0	2.61E-09	0	0	1.30E-10	20.00
KFM09A	20051129 21:03	20051129 22:25	278.00	298.00	3	1	5.15E-09	0	5.37E-09	0	0	2.69E-10	20.00
KFM09A	20051129 22:41	20051129 23:57	286.00	306.00	3	1	2.82E-09	0	2.95E-09	0	0	1.47E-10	20.00
KFM09A	20051130 06:29	20051130 07:48	306.00	326.00	3	1	1.37E-08	0	1.43E-08	0	0	7.13E-10	20.00
KFM09A	20051130 08:16	20051130 09:35	326.00	346.00	3	1	1.02E-09	0	1.06E-09	0	0	5.31E-11	20.00
KFM09A	20051130 10:06	20051130 11:22	346.00	366.00	3	1	2.09E-09	0	2.18E-09	0	0	1.09E-10	20.00
KFM09A	20051130 12:06	20051130 13:23	366.00	386.00	3	1	6.23E-08	0	6.50E-08	0	0	3.25E-09	20.00
KFM09A	20051130 13:50	20051130 15:08	386.00	406.00	3	1	1.32E-07	0	1.38E-07	1	0	6.89E-09	20.00
KFM09A	20051130 15:30	20051130 16:47	406.00	426.00	3	1	1.96E-08	0	2.04E-08	1	0	1.02E-09	20.00
KFM09A	20051130 18:18	20051130 19:38	426.00	446.00	3	1	8.24E-07	0	8.60E-07	1	0	4.30E-08	20.00
KFM09A	20051130 20:03	20051130 21:45	446.00	466.00	3	1	3.03E-09	0	3.16E-09	0	0	1.58E-10	20.00
KFM09A	20051130 22:03	20051130 23:20	466.00	486.00	3	1	2.27E-09	0	2.37E-09	0	0	1.19E-10	20.00
KFM09A	20051201 08:06	20051201 09:34	486.00	506.00	3	1	5.62E-09	0	5.86E-09	0	0	2.93E-10	20.00
KFM09A	20051201 10:01	20051201 11:22	506.00	526.00	3	1	2.24E-09	0	2.33E-09	0	0	1.17E-10	20.00
KFM09A	20051201 11:41	20051201 13:46	526.00	546.00	3	1	1.39E-07	0	1.45E-07	1	0	7.27E-09	20.00

idcode	start_date	stop_date	secup	seclow	test_type	formation_type	spec_capacity_q_s	value_type_q_s	transmissivity_moye	bc_tm	value_type_tm	hydr_cond_moye	formation_width_b
KFM09A	20051201 14:21	20051201 15:09	545.00	565.00	3	1	2.55E-10	-1	2.66E-10	0	-1	1.33E-11	20.00
KFM09A	20051201 15:34	20051201 16:17	566.00	586.00	3	1	2.55E-10	-1	2.66E-10	0	-1	1.33E-11	20.00
KFM09A	20051202 07:55	20051202 08:37	586.00	606.00	3	1	2.55E-10	-1	2.66E-10	0	-1	1.33E-11	20.00
KFM09A	20051202 08:58	20051202 10:22	606.00	626.00	3	1	2.33E-08	0	2.43E-08	0	0	1.22E-09	20.00
KFM09A	20051202 10:43	20051202 12:05	626.00	646.00	3	1	4.03E-09	0	4.21E-09	0	0	2.10E-10	20.00
KFM09A	20051202 13:12	20051202 14:35	646.00	666.00	3	1	5.01E-09	0	5.22E-09	0	0	2.61E-10	20.00
KFM09A	20051202 14:57	20051202 16:13	666.00	686.00	3	1	6.54E-10	0	6.82E-10	1	0	3.41E-11	20.00
KFM09A	20051205 08:22	20051205 09:53	686.00	706.00	3	1	4.89E-10	0	5.10E-10	0	0	2.55E-11	20.00
KFM09A	20051205 10:10	20051205 11:12	691.00	711.00	3	1	1.94E-10	-1	2.02E-10	0	-1	1.01E-11	20.00
KFM09A	20051205 12:46	20051205 13:30	711.00	731.00	3	1	1.94E-10	-1	2.02E-10	0	-1	1.01E-11	20.00
KFM09A	20051205 13:49	20051205 15:12	731.00	751.00	3	1	2.89E-09	0	3.01E-09	0	0	1.51E-10	20.00
KFM09A	20051205 15:30	20051205 16:54	751.00	771.00	3	1	1.74E-08	0	1.82E-08	0	0	9.10E-10	20.00
KFM09A	20051205 18:09	20051205 19:26	771.00	791.00	3	1	4.06E-08	0	4.23E-08	0	0	2.12E-09	20.00
KFM09A	20051207 07:32	20051207 08:52	106.00	111.00	3	1	2.76E-08	0	2.27E-08	0	0	4.54E-09	5.00
KFM09A	20051207 09:08	20051207 10:24	111.00	116.00	3	1	2.84E-09	0	2.33E-09	0	0	4.67E-10	5.00
KFM09A	20051221 15:48	20051208 17:51	116.00	121.00	3	1	1.06E-07	0	8.68E-08	0	0	1.74E-08	5.00
KFM09A	20051207 12:52	20051207 14:09	121.00	126.00	3	1	3.29E-07	0	2.71E-07	0	0	5.41E-08	5.00
KFM09A	20051207 14:26	20051207 16:04	126.00	131.00	3	1	1.87E-09	0	1.54E-09	0	0	3.07E-10	5.00
KFM09A	20051207 16:21	20051207 17:40	128.00	133.00	3	1	7.90E-07	0	6.50E-07	0	0	1.30E-07	5.00
KFM09A	20051207 17:58	20051207 19:16	133.00	138.00	3	1	6.94E-07	0	5.71E-07	0	0	1.14E-07	5.00
KFM09A	20051207 19:42	20051207 21:13	138.00	143.00	3	1	1.51E-08	0	1.24E-08	0	0	2.49E-09	5.00
KFM09A	20051207 21:27	20051207 22:45	141.00	146.00	3	1	5.38E-08	0	4.43E-08	0	0	8.86E-09	5.00
KFM09A	20051207 23:02	20051208 00:17	146.00	151.00	3	1	5.77E-08	0	4.75E-08	0	0	9.49E-09	5.00
KFM09A	20051208 06:16	20051208 06:59	151.00	156.00	3	1	2.55E-10	-1	2.10E-10	0	-1	4.20E-11	5.00
KFM09A	20051208 07:10	20051208 08:26	156.00	161.00	3	1	2.02E-07	0	1.66E-07	0	0	3.32E-08	5.00
KFM09A	20051208 08:36	20051208 09:52	161.00	166.00	3	1	5.60E-09	0	4.60E-09	1	0	9.21E-10	5.00
KFM09A	20051208 10:03	20051208 11:19	166.00	171.00	3	1	2.23E-06	0	1.84E-06	0	0	3.67E-07	5.00
KFM09A	20051208 12:12	20051208 13:29	171.00	176.00	3	1	2.61E-09	0	2.15E-09	1	0	4.30E-10	5.00
KFM09A	20051208 13:43	20051208 14:57	176.00	181.00	3	1	1.42E-08	0	1.17E-08	0	0	2.34E-09	5.00
KFM09A	20051208 15:13	20051208 16:28	181.00	186.00	3	1	1.07E-08	0	8.83E-09	1	0	1.77E-09	5.00
KFM09A	20051208 16:36	20051208 17:51	186.00	191.00	3	1	5.60E-09	0	4.60E-09	0	0	9.21E-10	5.00
KFM09A	20051208 18:03	20051208 18:50	191.00	196.00	3	1	2.64E-10	-1	2.17E-10	0	-1	4.35E-11	5.00
KFM09A	20051208 19:02	20051208 19:47	196.00	201.00	3	1	2.04E-10	-1	1.68E-10	0	-1	3.36E-11	5.00

idcode	start_date	stop_date	secup	seclow	test_type	formation_type	spec_capacity_q_s	value_type_q_s	transmissivity_moye	bc_tm	value_type_tm	hydr_cond_moye	formation_width_b
KFM09A	20051208 19:57	20051208 20:39	201.00	206.00	3	1	2.64E-10	-1	2.17E-10	0	-1	4.35E-11	5.00
KFM09A	20051208 20:58	20051208 21:40	226.00	231.00	3	1	2.64E-10	-1	2.17E-10	0	-1	4.35E-11	5.00
KFM09A	20051208 21:54	20051208 23:08	232.00	237.00	3	1	4.14E-08	0	3.41E-08	0	0	6.81E-09	5.00
KFM09A	20051208 23:21	20051209 00:35	237.00	242.00	3	1	8.31E-08	0	6.84E-08	0	0	1.37E-08	5.00
KFM09A	20051209 08:08	20051209 09:24	240.80	245.80	3	1	1.55E-08	0	1.27E-08	0	0	2.55E-09	5.00
KFM09A	20051221 13:55	20051221 14:35	246.80	251.80	3	1	2.04E-10	-1	1.68E-10	0	-1	3.36E-11	5.00
KFM09A	20051209 09:40	20051209 10:22	251.50	256.50	3	1	2.64E-10	-1	2.17E-10	0	-1	4.35E-11	5.00
KFM09A	20051209 10:34	20051209 11:18	256.50	261.50	3	1	3.27E-10	-1	2.69E-10	0	-1	5.37E-11	5.00
KFM09A	20051209 11:30	20051209 13:22	273.00	278.00	3	1	2.88E-09	0	2.37E-09	0	0	4.73E-10	5.00
KFM09A	20051209 13:34	20051209 14:48	278.00	283.00	3	1	4.63E-09	0	3.81E-09	0	0	7.62E-10	5.00
KFM09A	20051209 15:04	20051209 15:51	283.00	288.00	3	1	2.64E-10	-1	2.17E-10	0	-1	4.35E-11	5.00
KFM09A	20051209 16:00	20051209 17:15	288.00	293.00	3	1	7.71E-10	0	6.35E-10	1	0	1.27E-10	5.00
KFM09A	20051212 08:21	20051212 09:42	293.00	298.00	3	1	1.41E-09	0	1.16E-09	0	0	2.33E-10	5.00
KFM09A	20051221 12:39	20051221 13:28	296.00	301.00	3	1	2.04E-10	-1	1.68E-10	0	-1	3.36E-11	5.00
KFM09A	20051221 11:45	20051221 12:29	301.00	306.00	3	1	2.04E-10	-1	1.68E-10	0	-1	3.36E-11	5.00
KFM09A	20051212 09:58	20051212 10:39	306.00	311.00	3	1	3.25E-10	-1	2.67E-10	0	-1	5.35E-11	5.00
KFM09A	20051212 10:49	20051212 12:33	311.00	316.00	3	1	1.42E-10	-1	1.16E-10	0	-1	2.33E-11	5.00
KFM09A	20051212 12:43	20051212 13:31	316.00	321.00	3	1	2.04E-10	-1	1.67E-10	0	-1	3.35E-11	5.00
KFM09A	20051212 13:44	20051212 15:02	321.00	326.00	3	1	1.46E-08	0	1.20E-08	0	0	2.40E-09	5.00
KFM09A	20051212 15:31	20051212 16:14	346.00	351.00	3	1	3.27E-10	-1	2.69E-10	0	-1	5.37E-11	5.00
KFM09A	20051221 10:04	20051221 11:19	351.00	356.00	3	1	2.36E-09	0	1.94E-09	0	0	3.88E-10	5.00
KFM09A	20051221 08:54	20051221 09:50	356.00	361.00	3	1	2.04E-10	-1	1.67E-10	0	-1	3.35E-11	5.00
KFM09A	20051221 07:28	20051221 08:43	361.00	366.00	3	1	7.97E-10	0	6.56E-10	0	0	1.31E-10	5.00
KFM09A	20051212 16:39	20051212 17:54	363.00	368.00	3	1	5.99E-10	0	4.93E-10	0	0	9.86E-11	5.00
KFM09A	20051213 06:27	20051213 07:24	368.00	373.00	3	1	2.64E-10	-1	2.17E-10	0	-1	4.35E-11	5.00
KFM09A	20051213 07:35	20051213 08:48	371.00	376.00	3	1	7.16E-08	0	5.89E-08	0	0	1.18E-08	5.00
KFM09A	20051213 09:02	20051213 09:58	376.00	381.00	3	1	2.50E-10	-1	2.06E-10	0	-1	4.11E-11	5.00
KFM09A	20051213 10:10	20051213 11:25	381.00	386.00	3	1	2.64E-10	-1	2.17E-10	0	-1	4.34E-11	5.00
KFM09A	20051213 11:57	20051213 13:16	386.00	391.00	3	1	1.15E-07	0	9.43E-08	1	0	1.89E-08	5.00
KFM09A	20051213 13:28	20051213 14:48	391.00	396.00	3	1	7.87E-09	0	6.48E-09	0	0	1.30E-09	5.00
KFM09A	20051213 15:06	20051213 15:49	396.00	401.00	3	1	3.27E-10	-1	2.69E-10	0	-1	5.37E-11	5.00
KFM09A	20051213 16:00	20051213 17:15	401.00	406.00	3	1	2.07E-08	0	1.70E-08	0	0	3.41E-09	5.00
KFM09A	20051213 17:25	20051213 18:18	406.00	411.00	3	1	2.65E-10	-1	2.18E-10	0	-1	4.35E-11	5.00
KFM09A	20051213 18:36	20051213 19:50	411.00	416.00	3	1	1.86E-08	0	1.53E-08	0	0	3.06E-09	5.00

idcode	start_date	stop_date	secup	seclow	test_type	formation_type	spec_capacity_q_s	value_type_q_s	transmissivity_moye	bc_tm	value_type_tm	hydr_cond_moye	formation_width_b
KFM09A	20051213 20:06	20051213 21:22	414.00	419.00	3	1	6.59E-10	0	5.42E-10	0	0	1.08E-10	5.00
KFM09A	20051213 21:32	20051213 22:46	419.00	424.00	3	1	2.73E-09	0	2.25E-09	0	0	4.50E-10	5.00
KFM09A	20051213 22:55	20051214 00:09	421.00	426.00	3	1	2.93E-09	0	2.41E-09	0	0	4.82E-10	5.00
KFM09A	20051214 06:51	20051214 07:59	426.00	431.00	3	1	3.88E-10	-1	3.19E-10	0	-1	6.38E-11	5.00
KFM09A	20051214 08:11	20051214 09:31	431.00	436.00	3	1	7.09E-07	0	5.83E-07	1	0	1.17E-07	5.00
KFM09A	20051214 09:47	20051214 10:29	436.00	441.00	3	1	3.00E-10	-1	2.47E-10	0	-1	4.94E-11	5.00
KFM09A	20051214 10:44	20051214 12:00	441.00	446.00	3	1	9.04E-09	0	7.44E-09	1	0	1.49E-09	5.00
KFM09A	20051214 12:13	20051214 14:04	446.00	451.00	3	1	1.77E-09	0	1.46E-09	0	0	2.92E-10	5.00
KFM09A	20051214 14:22	20051214 15:38	451.00	456.00	3	1	6.35E-10	0	5.22E-10	1	0	1.04E-10	5.00
KFM09A	20051214 15:55	20051214 17:12	456.00	461.00	3	1	3.26E-09	0	2.69E-09	0	0	5.37E-10	5.00
KFM09A	20051214 17:32	20051214 18:15	461.00	466.00	3	1	1.42E-10	-1	1.16E-10	0	-1	2.33E-11	5.00
KFM09A	20051214 18:35	20051214 19:50	471.00	476.00	3	1	2.49E-09	0	2.04E-09	0	0	4.09E-10	5.00
KFM09A	20051214 20:01	20051214 21:23	476.00	481.00	3	1	2.21E-09	0	1.82E-09	0	0	3.64E-10	5.00
KFM09A	20051214 21:40	20051214 22:31	486.00	491.00	3	1	2.64E-10	-1	2.17E-10	0	-1	4.35E-11	5.00
KFM09A	20051214 22:58	20051215 00:12	491.00	496.00	3	1	3.86E-09	0	3.18E-09	0	0	6.35E-10	5.00
KFM09A	20051215 06:33	20051215 07:57	496.00	501.00	3	1	2.95E-09	0	2.43E-09	0	0	4.85E-10	5.00
KFM09A	20051215 08:14	20051215 09:00	501.00	506.00	3	1	2.50E-10	-1	2.06E-10	0	-1	4.11E-11	5.00
KFM09A	20051220 19:00	20051220 20:23	506.00	511.00	3	1	1.06E-09	0	8.76E-10	0	0	1.75E-10	5.00
KFM09A	20051220 20:50	20051220 22:05	511.00	516.00	3	1	1.44E-09	0	1.19E-09	0	0	2.37E-10	5.00
KFM09A	20051220 22:14	20051220 23:28	516.00	521.00	3	1	1.03E-09	0	8.43E-10	0	0	1.69E-10	5.00
KFM09A	20051215 09:25	20051215 10:11	521.00	526.00	3	1	2.64E-10	-1	2.17E-10	0	-1	4.35E-11	5.00
KFM09A	20051215 10:26	20051215 11:07	526.00	531.00	3	1	2.64E-10	-1	2.17E-10	0	-1	4.34E-11	5.00
KFM09A	20051215 11:23	20051215 12:44	531.00	536.00	3	1	1.32E-07	0	1.09E-07	1	0	2.17E-08	5.00
KFM09A	20051215 13:19	20051215 14:03	536.00	541.00	3	1	2.65E-10	-1	2.18E-10	0	-1	4.35E-11	5.00
KFM09A	20051215 14:14	20051215 15:28	541.00	546.00	3	1	4.36E-10	0	3.59E-10	0	0	7.18E-11	5.00
KFM09A	20051220 17:14	20051220 17:58	561.00	566.00	3	1	2.65E-10	-1	2.18E-10	0	-1	4.35E-11	5.00
KFM09A	20051215 16:19	20051215 17:00	606.00	611.00	3	1	2.04E-10	-1	1.68E-10	0	-1	3.36E-11	5.00
KFM09A	20051215 17:19	20051215 18:35	611.00	616.00	3	1	2.03E-08	0	1.67E-08	0	0	3.33E-09	5.00
KFM09A	20051215 18:50	20051215 19:31	616.00	621.00	3	1	2.65E-10	-1	2.18E-10	0	-1	4.35E-11	5.00
KFM09A	20051215 19:44	20051215 21:03	621.00	626.00	3	1	7.07E-09	0	5.82E-09	0	0	1.16E-09	5.00
KFM09A	20051215 21:14	20051215 22:01	626.00	631.00	3	1	2.04E-10	-1	1.67E-10	0	-1	3.35E-11	5.00
KFM09A	20051215 22:08	20051215 23:33	631.00	636.00	3	1	7.00E-10	0	5.76E-10	0	0	1.15E-10	5.00
KFM09A	20051215 23:43	20051216 00:58	636.00	641.00	3	1	6.96E-09	0	5.72E-09	0	0	1.14E-09	5.00
KFM09A	20051216 08:21	20051216 09:36	641.00	646.00	3	1	6.92E-10	0	5.70E-10	0	0	1.14E-10	5.00

idcode	start_date	stop_date	secup	seclow	test_type	formation_type	spec_capacity_q_s	value_type_q_s	transmissivity_moye	bc_tm	value_type_tm	hydr_cond_moye	formation_width_b
KFM09A	20051216 09:55	20051216 10:38	646.00	651.00	3	1	1.42E-10	-1	1.16E-10	0	-1	2.33E-11	5.00
KFM09A	20051216 10:53	20051216 12:10	651.00	656.00	3	1	6.35E-09	0	5.23E-09	0	0	1.05E-09	5.00
KFM09A	20051216 12:21	20051216 13:20	656.00	661.00	3	1	3.27E-10	-1	2.69E-10	0	-1	5.37E-11	5.00
KFM09A	20051216 13:31	20051216 14:14	661.00	666.00	3	1	2.04E-10	-1	1.68E-10	0	-1	3.36E-11	5.00
KFM09A	20051219 08:19	20051219 09:01	731.00	736.00	3	1	2.65E-10	-1	2.18E-10	0	-1	4.35E-11	5.00
KFM09A	20051219 09:15	20051219 09:56	736.00	741.00	3	1	2.65E-10	-1	2.18E-10	0	-1	4.35E-11	5.00
KFM09A	20051219 10:11	20051219 11:30	741.00	746.00	3	1	4.41E-09	0	3.63E-09	0	0	7.26E-10	5.00
KFM09A	20051219 11:44	20051219 12:36	746.00	751.00	3	1	2.65E-10	-1	2.18E-10	0	-1	4.35E-11	5.00
KFM09A	20051219 12:50	20051219 14:05	751.00	756.00	3	1	4.20E-09	0	3.45E-09	0	0	6.91E-10	5.00
KFM09A	20051219 14:20	20051219 15:42	756.00	761.00	3	1	1.03E-08	0	8.44E-09	0	0	1.69E-09	5.00
KFM09A	20051219 15:56	20051219 17:16	761.00	766.00	3	1	5.25E-09	0	4.32E-09	0	0	8.63E-10	5.00
KFM09A	20051220 06:55	20051220 08:10	766.00	771.00	3	1	2.82E-09	0	2.32E-09	0	0	4.64E-10	5.00
KFM09A	20051220 08:29	20051220 09:46	771.00	776.00	3	1	2.53E-09	0	2.08E-09	0	0	4.16E-10	5.00
KFM09A	20051220 10:06	20051220 11:24	776.00	781.00	3	1	5.95E-09	0	4.90E-09	0	0	9.80E-10	5.00
KFM09A	20051220 11:35	20051220 12:58	781.00	786.00	3	1	1.05E-08	0	8.62E-09	0	0	1.72E-09	5.00
KFM09A	20051220 13:11	20051220 14:28	786.00	791.00	3	1	3.41E-08	0	2.81E-08	0	0	5.61E-09	5.00
KFM09A	20051118 13:32	20051118 14:28	506.00 [1)]	606.00	3	1							100.00
KFM09A	20051130 17:10	20051130 18:03	426.00 [1)]	446.00	3	1							20.00
KFM09A	20051207 10:38	20051207 12:39	116.00 [1)]	121.00	3	1							5.00

[1)] Incomplete test, interrupted and re-performed later.

KFM09A plu_s_hole_test_ed1. Right (This result table to SICADA includes more columns which are empty, these columns are not presented here.)

idcode	secup	seclow	transmissivity_tt	value_type_tt	bc_tt	l_measl_q_s	u_measl_q_s	assumed_s	bc_s	ri	ri_index	c	skin	t1	t2	dte1	dte2
KFM09A	106.00	206.00	4.56E-07	0	1	8.9E-10	5.0E-04	4.73E-07	4.73E-07	62.84	-1		-6.79				
KFM09A	206.00	306.00	4.19E-08	0	1	7.5E-10	5.0E-04	1.43E-07	1.43E-07	34.41	0		-2.54	150	1800		
KFM09A	306.00	406.00	1.29E-07	0	1	7.8E-10	5.0E-04	2.51E-07	2.51E-07	45.55	1		-5.13				
KFM09A	406.00	506.00	1.14E-06	0	0	8.0E-10	5.0E-04	5.75E-07	5.75E-07	69.31	1		-5.76				
KFM09A	506.00	606.00	3.17E-07	0	0	7.4E-10	5.0E-04	2.35E-07	2.35E-07	44.31	1		-5.12				
KFM09A	606.00	706.00	1.64E-08	0	1	8.0E-10	5.0E-04	8.95E-08	8.95E-08	12.82	1	3.24E-10	-3.54	20	400		
KFM09A	691.00	791.00	6.92E-09	0	1	9.3E-10	5.0E-04	5.82E-08	5.82E-08	22.07	-1		-5.60				
KFM09A	106.00	126.00	2.51E-07	0	1	7.7E-10	5.0E-04	3.51E-07	3.51E-07	43.97	0		-3.14	100	1200		
KFM09A	126.00	146.00	5.35E-07	0	1	7.6E-10	5.0E-04	5.12E-07	5.12E-07	53.12	0		-4.71	550	1200		
KFM09A	146.00	166.00	4.22E-08	0	1	8.9E-10	5.0E-04	1.44E-07	1.44E-07	28.35	0						
KFM09A	166.00	186.00	6.19E-07	0	1	8.6E-10	5.0E-04	5.51E-07	5.51E-07	55.49	-1		-5.02				
KFM09A	186.00	206.00	3.28E-09	0	1	5.5E-10	5.0E-04	4.01E-08	4.01E-08	14.99	-1	5.75E-11	-1.13				
KFM09A	206.00	226.00		-1	0	2.6E-10	5.0E-04										
KFM09A	226.00	246.00	4.65E-08	0	1	7.9E-10	5.0E-04	1.51E-07	1.51E-07	28.85	0		-0.24	300	1200		
KFM09A	238.00	258.00	4.90E-09	0	1	7.8E-10	5.0E-04	4.90E-08	4.90E-08	16.43	0	5.01E-10	-3.44	200	1200		
KFM09A	258.00	278.00	1.46E-09	0	1	8.0E-10	5.0E-04	2.68E-08	2.68E-08	12.12	0	7.53E-11	-3.09				
KFM09A	278.00	298.00	2.59E-09	0	1	7.7E-10	5.0E-04	3.56E-08	3.56E-08	7.01	0		-3.42	10	300		
KFM09A	286.00	306.00	1.39E-09	0	1	7.7E-10	5.0E-04	2.61E-08	2.61E-08	11.95	-1		-3.56				
KFM09A	306.00	326.00	3.12E-08	0	1	8.2E-10	5.0E-04	1.24E-07	1.24E-07	7.53	1		-2.23	20	100		
KFM09A	326.00	346.00	4.17E-10	0	1	8.1E-10	5.0E-04	1.43E-08	1.43E-08	8.87	0		-3.21	30	1200		
KFM09A	346.00	366.00	7.25E-10	0	1	8.0E-10	5.0E-04	1.88E-08	1.88E-08	10.19	0	5.57E-11	-3.71	300	1200		
KFM09A	366.00	386.00	2.44E-08	0	1	8.1E-10	5.0E-04	1.09E-07	1.09E-07	24.54	0		-4.23	200	1200		
KFM09A	386.00	406.00	4.53E-08	0	0	8.2E-10	5.0E-04	2.60E-07	2.60E-07	38.40	1		-6.01				
KFM09A	406.00	426.00	2.31E-08	0	0	8.2E-10	5.0E-04	1.00E-07	1.00E-07	23.85	1		-1.36				
KFM09A	426.00	446.00	1.26E-06	0	0	7.4E-10	5.0E-04	6.49E-07	6.49E-07	60.65	1		-5.73				
KFM09A	446.00	466.00	1.97E-09	0	1	7.1E-10	5.0E-04	3.11E-08	3.11E-08	13.08	0		-1.90	200	1200		
KFM09A	466.00	486.00	1.86E-09	0	1	9.5E-10	5.0E-04	3.02E-08	3.02E-08	8.32	1		-2.90			100	500
KFM09A	486.00	506.00	1.00E-09	0	1	8.0E-10	5.0E-04	2.21E-08	2.21E-08	11.14	1						

idcode	secup	seclow	transmissivity_tt	value_type_tt	bc_tt	l_measl_q_s	u_measl_q_s	assumed_s	bc_s	ri	ri_index	c	skin	t1	t2	dte1	dte2
KFM09A	506.00	526.00	2.06E-10	0	1	8.6E-10	5.0E-04	1.00E-08	1.00E-08	7.44	0		-5.47				
KFM09A	526.00	546.00	4.12E-07	0	0	8.0E-10	5.0E-04	2.67E-07	2.67E-07	38.65	0		-4.72			100	1400
KFM09A	545.00	565.00		-1	0	2.6E-10	5.0E-04										
KFM09A	566.00	586.00		-1	0	2.6E-10	5.0E-04										
KFM09A	586.00	606.00		-1	0	2.6E-10	5.0E-04										
KFM09A	606.00	626.00	1.28E-08	0	1	8.2E-10	5.0E-04	7.92E-08	7.92E-08	10.44	1		-3.99	50	300		
KFM09A	626.00	646.00	2.70E-09	0	1	7.9E-10	5.0E-04	3.64E-08	3.64E-08	14.16	-1	7.25E-11	-1.83				
KFM09A	646.00	666.00	4.21E-09	0	1	8.0E-10	5.0E-04	4.54E-08	4.54E-08	15.82	0		-0.94	50	1200		
KFM09A	666.00	686.00	2.40E-11	0	0	2.8E-10	5.0E-04	1.83E-08	1.83E-08	10.05	1		-6.35				
KFM09A	686.00	706.00	9.24E-11	0	1	2.6E-10	5.0E-04	6.73E-09	6.73E-09	6.10	1						
KFM09A	691.00	711.00		-1	0	1.9E-10	5.0E-04										
KFM09A	711.00	731.00		-1	0	1.9E-10	5.0E-04										
KFM09A	731.00	751.00	3.41E-09	0	1	7.7E-10	5.0E-04	4.09E-08	4.09E-08	15.03	-1	6.28E-11	0.71				
KFM09A	751.00	771.00	3.50E-09	0	1	8.0E-10	5.0E-04	4.14E-08	4.14E-08	15.22	1		-5.20				
KFM09A	771.00	791.00	6.54E-09	0	1	7.6E-10	5.0E-04	5.66E-08	5.66E-08	17.81	-1	1.41E-09	-5.10				
KFM09A	106.00	111.00	1.32E-08	0	1	8.1E-10	5.0E-04	8.04E-08	8.04E-08	21.26	-1		-2.89				
KFM09A	111.00	116.00	1.04E-09	0	1	7.9E-10	5.0E-04	2.26E-08	2.26E-08	11.26	-1		-3.22				
KFM09A	116.00	121.00	4.25E-08	0	1	8.2E-10	5.0E-04	1.44E-07	1.44E-07	16.28	0		-4.44	50	400		
KFM09A	121.00	126.00	1.69E-07	0	1	9.2E-10	5.0E-04	2.88E-07	2.88E-07	21.51	0		-3.66	80	350		
KFM09A	126.00	131.00	6.83E-10	0	1	8.1E-10	5.0E-04	1.83E-08	1.83E-08	10.02	1						
KFM09A	128.00	133.00	2.69E-07	0	1	7.5E-10	5.0E-04	3.63E-07	3.63E-07	45.08	-1		-4.87				
KFM09A	133.00	138.00	2.10E-07	0	1	7.0E-10	5.0E-04	3.21E-07	3.21E-07	41.99	0		-4.48				
KFM09A	138.00	143.00	8.19E-09	0	1	8.1E-10	5.0E-04	6.33E-08	6.33E-08	18.68	0		-2.86	100	1200		
KFM09A	141.00	146.00	2.77E-08	0	1	7.3E-10	5.0E-04	1.16E-07	1.16E-07	25.58	0		-3.50				
KFM09A	146.00	151.00	7.80E-09	0	1	7.2E-10	5.0E-04	6.18E-08	6.18E-08	18.36	1						
KFM09A	151.00	156.00		-1	0	2.6E-10	5.0E-04										
KFM09A	156.00	161.00	3.44E-08	0	1	7.9E-10	5.0E-04	1.30E-07	1.30E-07	26.90	0						
KFM09A	161.00	166.00	4.85E-09	0	0	9.2E-10	5.0E-04	4.75E-08	4.75E-08	16.31	-1		0.00				
KFM09A	166.00	171.00	1.13E-06	0	1	9.1E-10	5.0E-04	7.44E-07	7.44E-07	64.48	-1		-3.98				
KFM09A	171.00	176.00		0	0	7.9E-10	5.0E-04	3.25E-08	3.25E-08	13.46							
KFM09A	176.00	181.00	4.78E-09	0	1	8.2E-10	5.0E-04	4.84E-08	4.84E-08	16.33	0	7.41E-11	-3.96	50	1200		

idcode	secup	seclow	transmissivity_tt	value_type_tt	bc_tt	l_measl_q_s	u_measl_q_s	assumed_s	bc_s	ri	ri_index	c	skin	t1	t2	dte1	dte2
KFM09A	181.00	186.00		0	0	7.2E-10	5.0E-04	6.58E-08	6.58E-08	19.20							
KFM09A	186.00	191.00	4.58E-09	0	1	7.6E-10	5.0E-04	4.74E-08	4.74E-08	16.16	0	2.51E-11	-0.92	40	1200		
KFM09A	191.00	196.00		-1	0	2.6E-10	5.0E-04										
KFM09A	196.00	201.00		-1	0	2.0E-10	5.0E-04										
KFM09A	201.00	206.00		-1	0	2.6E-10	5.0E-04										
KFM09A	226.00	231.00		-1	0	2.6E-10	5.0E-04										
KFM09A	232.00	237.00	6.48E-08	0	1	8.2E-10	5.0E-04	1.78E-07	1.78E-07	31.56	-1		3.62				
KFM09A	237.00	242.00	7.88E-08	0	1	8.2E-10	5.0E-04	1.96E-07	1.96E-07	32.90	0		-0.90	50	1200		
KFM09A	240.80	245.80	4.95E-09	0	1	8.0E-10	5.0E-04	4.92E-08	4.92E-08	16.60	-1		-3.88				
KFM09A	246.80	251.80		-1	0	2.0E-10	5.0E-04										
KFM09A	251.50	256.50		-1	0	2.6E-10	5.0E-04										
KFM09A	256.50	261.50		-1	0	3.3E-10	5.0E-04										
KFM09A	273.00	278.00	2.00E-09	0	1	7.0E-10	5.0E-04	3.13E-08	3.13E-08	5.36	0	3.85E-11	-2.81	30	200		
KFM09A	278.00	283.00	1.47E-09	0	1	7.9E-10	5.0E-04	2.68E-08	2.68E-08	7.84	1		-4.20	60	500		
KFM09A	283.00	288.00		-1	0	2.6E-10	5.0E-04										
KFM09A	288.00	293.00	6.90E-11	0	0	4.9E-10	5.0E-04	1.76E-08	1.76E-08	9.95	0	1.73E-11	-5.42				
KFM09A	293.00	298.00	6.79E-10	0	1	7.0E-10	5.0E-04	1.82E-08	1.82E-08	10.02	0	1.72E-11	-2.68	10	1200		
KFM09A	296.00	301.00		-1	0	2.0E-10	5.0E-04										
KFM09A	301.00	306.00		-1	0	2.0E-10	5.0E-04										
KFM09A	306.00	311.00		-1	0	3.3E-10	5.0E-04										
KFM09A	311.00	316.00		-1	0	1.4E-10	5.0E-04										
KFM09A	316.00	321.00		-1	0	2.0E-10	5.0E-04										
KFM09A	321.00	326.00	2.01E-08	0	1	8.1E-10	5.0E-04	9.92E-08	9.92E-08	9.54	1		-3.28	30	200		
KFM09A	346.00	351.00		-1	0	3.3E-10	5.0E-04										
KFM09A	351.00	356.00	1.42E-09	0	1	7.8E-10	5.0E-04	2.63E-08	2.63E-08	12.05	0	1.74E-11	-1.68	30	1200		
KFM09A	356.00	361.00		-1	0	2.0E-10	5.0E-04										
KFM09A	361.00	366.00	2.32E-10	0	1	1.9E-10	5.0E-04	1.07E-08	1.07E-08	7.67	0		-2.96	20	1200		
KFM09A	363.00	368.00	2.32E-10	0	1	2.5E-10	5.0E-04	1.07E-08	1.07E-08	7.66	0	1.84E-11	-2.93	30	1200		
KFM09A	368.00	373.00		-1	0	2.6E-10	5.0E-04										
KFM09A	371.00	376.00	3.05E-08	0	1	8.1E-10	5.0E-04	1.22E-07	1.22E-07	18.36	0		-5.05	100	600		
KFM09A	376.00	381.00		-1	0	2.5E-10	5.0E-04										
KFM09A	381.00	386.00		-1	0	2.6E-10	5.0E-04										

idcode	secup	seclow	transmissivity_tt	value_type_tt	bc_tt	l_measl_q_s	u_measl_q_s	assumed_s	bc_s	ri	ri_index	c	skin	t1	t2	dte1	dte2
KFM09A	386.00	391.00	8.27E-08	0	0	7.7E-10	5.0E-04	2.15E-07	2.15E-07	34.73	1						
KFM09A	391.00	396.00	1.42E-09	0	1	7.9E-10	5.0E-04	2.64E-08	2.64E-08	6.03	-1		-4.46	20	300		
KFM09A	396.00	401.00		-1	0	3.3E-10	5.0E-04										
KFM09A	401.00	406.00	2.04E-08	0	1	8.1E-10	5.0E-04	1.00E-07	1.00E-07	10.71	1	1.30E-10	-0.66	100	250		
KFM09A	406.00	411.00		-1	0	2.6E-10	5.0E-04										
KFM09A	411.00	416.00	2.37E-08	0	1	8.4E-10	5.0E-04	1.08E-07	1.08E-07	7.03	0		-1.98	20	100		
KFM09A	414.00	419.00	3.17E-10	0	1	2.7E-10	5.0E-04	1.25E-08	1.25E-08	8.29	0		-1.85	30	1200		
KFM09A	419.00	424.00	1.95E-09	0	1	8.0E-10	5.0E-04	3.09E-08	3.09E-08	9.23	0	1.61E-11	-1.79	30	600		
KFM09A	421.00	426.00	1.68E-09	0	1	8.5E-10	5.0E-04	2.87E-08	2.87E-08	12.57	0	1.90E-11	-2.50	20	1200		
KFM09A	426.00	431.00		-1	0	3.9E-10	5.0E-04										
KFM09A	431.00	436.00	1.51E-06	0	0	7.3E-10	5.0E-04	5.35E-07	5.35E-07	54.77	1		-5.47				
KFM09A	436.00	441.00		-1	0	3.0E-10	5.0E-04										
KFM09A	441.00	446.00	4.01E-08	0	0	7.2E-10	5.0E-04	6.04E-08	6.04E-08	18.44	1		-6.42				
KFM09A	446.00	451.00	8.19E-10	0	1	7.9E-10	5.0E-04	2.00E-08	2.00E-08	10.51	1		-6.02				
KFM09A	451.00	456.00	1.57E-10	0	0	2.7E-10	5.0E-04	1.60E-08	1.60E-08	9.49	0		-3.30				
KFM09A	456.00	461.00	2.00E-09	0	1	8.1E-10	5.0E-04	3.13E-08	3.13E-08	9.29	1		-1.04	20	600		
KFM09A	461.00	466.00		-1	0	1.4E-10	5.0E-04										
KFM09A	471.00	476.00	2.93E-10	0	1	7.8E-10	5.0E-04	1.20E-08	1.20E-08	8.22	-1		-5.33				
KFM09A	476.00	481.00	1.65E-09	0	1	8.6E-10	5.0E-04	2.84E-08	2.84E-08	3.61	1		-1.97	20	100		
KFM09A	486.00	491.00		-1	0	2.6E-10	5.0E-04										
KFM09A	491.00	496.00	1.58E-09	0	1	8.2E-10	5.0E-04	2.78E-08	2.78E-08	12.38	0	7.15E-11	-3.36	60	1200		
KFM09A	496.00	501.00	2.97E-10	0	1	7.9E-10	5.0E-04	1.21E-08	1.21E-08	8.15	1						
KFM09A	501.00	506.00		-1	0	2.5E-10	5.0E-04										
KFM09A	506.00	511.00	4.79E-10	0	1	2.6E-10	5.0E-04	1.53E-08	1.53E-08	9.28	-1		0.00				
KFM09A	511.00	516.00	4.65E-10	0	1	8.1E-10	5.0E-04	1.51E-08	1.51E-08	9.19	-1		-1.98				
KFM09A	516.00	521.00	2.41E-10	0	1	4.1E-10	5.0E-04	1.09E-08	1.09E-08	7.81	0	1.56E-11	-3.69				
KFM09A	521.00	526.00		-1	0	2.6E-10	5.0E-04										
KFM09A	526.00	531.00		-1	0	2.6E-10	5.0E-04										
KFM09A	531.00	536.00	4.23E-07	0	0	7.6E-10	5.0E-04	2.31E-07	2.31E-07	35.98	1		-4.75			100	5000
KFM09A	536.00	541.00		-1	0	2.6E-10	5.0E-04										
KFM09A	541.00	546.00	3.09E-09	0	1	2.7E-10	5.0E-04	3.89E-08	3.89E-08	2.99	1		-3.26	10	50		
KFM09A	561.00	566.00		-1	0	2.6E-10	5.0E-04										

idcode	secup	seclow	transmissivity_tt	value_type_tt	bc_tt	l_measl_q_s	u_measl_q_s	assumed_s	bc_s	ri	ri_index	c	skin	t1	t2	dte1	dte2
KFM09A	606.00	611.00		-1	0	2.0E-10	5.0E-04										
KFM09A	611.00	616.00	1.56E-08	0	1	8.5E-10	5.0E-04	8.75E-08	8.75E-08	8.96	1		-3.50	30	200		
KFM09A	616.00	621.00		-1	0	2.6E-10	5.0E-04										
KFM09A	621.00	626.00	2.38E-09	0	1	7.7E-10	5.0E-04	3.41E-08	3.41E-08	7.92	1		-4.28	40	400		
KFM09A	626.00	631.00		-1	0	2.0E-10	5.0E-04										
KFM09A	631.00	636.00	2.58E-10	0	1	3.2E-10	5.0E-04	1.12E-08	1.12E-08	2.27	1	1.71E-11	-3.98	30	100		
KFM09A	636.00	641.00	6.19E-09	0	1	8.6E-10	5.0E-04	5.51E-08	5.51E-08	17.42	0	2.64E-11	0.08	20	1200		
KFM09A	641.00	646.00	9.03E-11	0	1	1.5E-10	5.0E-04	6.65E-09	6.65E-09	6.11	0		-4.31				
KFM09A	646.00	651.00		-1	0	1.4E-10	5.0E-04										
KFM09A	651.00	656.00	3.71E-09	0	1	8.4E-10	5.0E-04	4.26E-08	4.26E-08	15.33	0		-2.52	40	1200		
KFM09A	656.00	661.00		-1	0	3.3E-10	5.0E-04										
KFM09A	661.00	666.00															
KFM09A	731.00	736.00		-1	0	2.6E-10	5.0E-04										
KFM09A	736.00	741.00		-1	0	2.6E-10	5.0E-04										
KFM09A	741.00	746.00	2.75E-09	0	1	8.3E-10	5.0E-04	3.67E-08	3.67E-08	7.11	0	1.92E-11	-0.91	40	300		
KFM09A	746.00	751.00		-1	0	2.6E-10	5.0E-04										
KFM09A	751.00	756.00	1.04E-09	0	1	8.8E-10	5.0E-04	2.26E-08	2.26E-08	8.51	-1			200	700		
KFM09A	756.00	761.00	5.14E-09	0	1	7.9E-10	5.0E-04	5.02E-08	5.02E-08	16.63	0		-3.58	70	1200		
KFM09A	761.00	766.00	7.00E-10	0	1	8.1E-10	5.0E-04	1.85E-08	1.85E-08	10.23	-1		-5.02				
KFM09A	766.00	771.00	7.66E-10	0	1	8.6E-10	5.0E-04	1.94E-08	1.94E-08	10.43	-1	7.66E-11	-3.86				
KFM09A	771.00	776.00	6.84E-10	0	1	7.0E-10	5.0E-04	1.83E-08	1.83E-08	10.15	-1		-3.54				
KFM09A	776.00	781.00	1.88E-09	0	1	8.6E-10	5.0E-04	3.04E-08	3.04E-08	12.93	0	7.00E-11	-3.69	100	1200		
KFM09A	781.00	786.00	6.16E-10	0	1	9.4E-10	5.0E-04	1.74E-08	1.74E-08	9.89	-1		-5.89				
KFM09A	786.00	791.00	6.36E-09	0	1	8.0E-10	5.0E-04	5.58E-08	5.58E-08	17.71	0	6.30E-10	-4.52				

KFM09A plu_s_hole_test_obs (This result table to SICADA includes more columns which are empty, these columns are not presented here.)

idcode	start_date	stop_date	secup	seclow	obs_secup	obs_seclow	pi_above	pp_above	pf_above	pi_below	pp_below	pf_below	comments
KFM09A	20051117 16:09	20051117 17:59	106.00	206.00	7.79	105.00	938.78	938.36	938.36				
KFM09A	20051117 16:09	20051117 17:59	106.00	206.00	207.00	799.67				1792.58	1793.95	1794.77	
KFM09A	20051117 19:03	20051117 20:53	206.00	306.00	7.79	205.00	944.46	943.92	943.92				
KFM09A	20051117 19:03	20051117 20:53	206.00	306.00	307.00	799.67				2608.72	2610.37	2611.60	
KFM09A	20051117 21:47	20051117 23:36	306.00	406.00	7.79	305.00	910.90	910.90	910.36				
KFM09A	20051117 21:47	20051117 23:36	306.00	406.00	407.00	799.67				3403.22	3405.41	3407.06	
KFM09A	20051118 09:59	20051118 11:49	406.00	506.00	7.79	405.00	858.19	857.91	858.05				
KFM09A	20051118 09:59	20051118 11:49	406.00	506.00	507.00	799.67				4184.43	4188.82	4191.57	
KFM09A	20051121 12:52	20051121 15:13	506.00	606.00	7.79	505.00	818.01	815.81	821.72				
KFM09A	20051121 12:52	20051121 15:13	506.00	606.00	607.00	799.67				4947.58	4948.68	4949.22	
KFM09A	20051121 06:14	20051121 08:03	606.00	706.00	7.79	605.00	693.26	692.84	692.84				
KFM09A	20051121 06:14	20051121 08:03	606.00	706.00	707.00	799.67				5659.22	5661.27	5662.50	
KFM09A	20051121 08:51	20051121 10:40	691.00	791.00	7.79	690.00	586.37	585.41	599.74				
KFM09A	20051121 08:51	20051121 10:40	691.00	791.00	792.00	799.67				6238.42	6243.76	6242.12	
KFM09A	20051128 16:44	20051128 18:19	106.00	126.00	7.79	105.00	943.46	943.32	943.32				
KFM09A	20051128 16:44	20051128 18:19	106.00	126.00	127.00	799.67				1128.14	1129.23	1129.23	
KFM09A	20051129 06:29	20051129 07:43	126.00	146.00	7.79	125.00	961.18	964.76	961.18				
KFM09A	20051129 06:29	20051129 07:43	126.00	146.00	147.00	799.67				1299.06	1299.61	1298.52	
KFM09A	20051129 08:20	20051129 09:35	146.00	166.00	7.79	145.00	958.79	962.51	960.86				
KFM09A	20051129 08:20	20051129 09:35	146.00	166.00	167.00	799.67				1463.96	1464.92	1463.96	
KFM09A	20051129 10:00	20051129 11:15	166.00	186.00	7.79	165.00	954.47	957.78	953.91				
KFM09A	20051129 10:00	20051129 11:15	166.00	186.00	187.00	799.67				1633.25	1633.79	1633.79	
KFM09A	20051129 12:14	20051129 13:31	186.00	206.00	7.79	185.00	948.78	953.60	951.95				
KFM09A	20051129 12:14	20051129 13:31	186.00	206.00	207.00	799.67				1798.01	1798.56	1799.24	
KFM09A	20051129 14:01	20051129 14:47	206.00	226.00	7.79	205.00	947.77	948.33	949.42				
KFM09A	20051129 14:01	20051129 14:47	206.00	226.00	227.00	799.67				1963.32	1963.59	1963.59	
KFM09A	20051129 15:38	20051129 16:56	226.00	246.00	7.79	225.00	938.22	943.45	940.29				

idcode	start_date	stop_date	secup	seclow	obs_secup	obs_seclow	pi_above	pp_above	pf_above	pi_below	pp_below	pf_below	comments
KFM09A	20051129 15:38	20051129 16:56	226.00	246.00	247.00	799.67				2128.49	2129.03	2129.59	
KFM09A	20051129 17:18	20051129 18:37	238.00	258.00	7.79	237.00	934.81	934.39	937.01				
KFM09A	20051129 17:18	20051129 18:37	238.00	258.00	259.00	799.67				2226.01	2226.82	2227.10	
KFM09A	20051129 18:58	20051129 20:17	258.00	278.00	7.79	257.00	933.38	929.52	930.62				
KFM09A	20051129 18:58	20051129 20:17	258.00	278.00	279.00	799.67				2389.81	2390.36	2390.91	
KFM09A	20051129 21:03	20051129 22:25	278.00	298.00	7.79	277.00	927.00	925.89	922.04				
KFM09A	20051129 21:03	20051129 22:25	278.00	298.00	299.00	799.67				2549.77	2550.87	2551.42	
KFM09A	20051129 22:41	20051129 23:57	286.00	306.00	7.79	285.00	921.14	919.49	921.14				
KFM09A	20051129 22:41	20051129 23:57	286.00	306.00	307.00	799.67				2611.00	2612.23	2613.33	
KFM09A	20051130 06:29	20051130 07:48	306.00	326.00	7.79	305.00	914.76	916.00	914.21				
KFM09A	20051130 06:29	20051130 07:48	306.00	326.00	327.00	799.67				2774.38	2774.38	2774.94	
KFM09A	20051130 08:16	20051130 09:35	326.00	346.00	7.79	325.00	903.28	903.97	905.07				
KFM09A	20051130 08:16	20051130 09:35	326.00	346.00	347.00	799.67				2932.72	2933.27	2933.81	
KFM09A	20051130 10:06	20051130 11:22	346.00	366.00	7.79	345.00	895.93	894.56	897.03				
KFM09A	20051130 10:06	20051130 11:22	346.00	366.00	367.00	799.67				3093.23	3093.78	3093.78	
KFM09A	20051130 12:06	20051130 13:23	366.00	386.00	7.79	365.00	883.49	886.79	888.44				
KFM09A	20051130 12:06	20051130 13:23	366.00	386.00	387.00	799.67				3250.46	3251.42	3252.11	
KFM09A	20051130 13:50	20051130 15:08	386.00	406.00	7.79	385.00	872.14	873.66	873.80				
KFM09A	20051130 13:50	20051130 15:08	386.00	406.00	407.00	799.67				3407.28	3408.78	3409.33	
KFM09A	20051130 15:30	20051130 16:47	406.00	426.00	7.79	405.00	865.21	864.11	865.21				
KFM09A	20051130 15:30	20051130 16:47	406.00	426.00	427.00	799.67				3564.37	3565.47	3566.56	
KFM09A	20051130 18:18	20051130 19:38	426.00	446.00	7.79	425.00	852.77	854.83	853.87				
KFM09A	20051130 18:18	20051130 19:38	426.00	446.00	447.00	799.67				3730.38	3732.01	3732.57	
KFM09A	20051130 20:03	20051130 21:45	446.00	466.00	7.79	445.00	840.32	842.80	836.47				
KFM09A	20051130 20:03	20051130 21:45	446.00	466.00	467.00	799.67				3887.60	3888.28	3888.69	
KFM09A	20051130 22:03	20051130 23:20	466.00	486.00	7.79	465.00	825.13	824.58	827.33				
KFM09A	20051130 22:03	20051130 23:20	466.00	486.00	487.00	799.67				4036.74	4038.80	4040.45	
KFM09A	20051201 08:06	20051201 09:34	486.00	506.00	7.79	485.00	813.24	813.93	811.59				
KFM09A	20051201 08:06	20051201 09:34	486.00	506.00	507.00	799.67				4187.67	4189.46	4190.55	
KFM09A	20051201 10:01	20051201 11:22	506.00	526.00	7.79	505.00	794.46	797.48	798.04				
KFM09A	20051201 10:01	20051201 11:22	506.00	526.00	527.00	799.67				4340.66	4342.17	4343.40	
KFM09A	20051201 11:41	20051201 13:46	526.00	546.00	7.79	525.00	776.23	775.68	775.68				

idcode	start_date	stop_date	secup	seclow	obs_secup	obs_seclow	pi_above	pp_above	pf_above	pi_below	pp_below	pf_below	comments
KFM09A	20051201 11:41	20051201 13:46	526.00	546.00	547.00	799.67				4497.61	4497.88	4498.44	
KFM09A	20051201 14:21	20051201 15:09	545.00	565.00	7.79	544.00	843.61	843.06	842.92				
KFM09A	20051201 14:21	20051201 15:09	545.00	565.00	566.00	799.67				4637.86	4638.13	4638.13	
KFM09A	20051201 15:34	20051201 16:17	566.00	586.00	7.79	565.00	823.27	823.14	823.14				
KFM09A	20051201 15:34	20051201 16:17	566.00	586.00	587.00	799.67				4793.72	4793.72	4794.27	
KFM09A	20051202 07:55	20051202 08:37	586.00	606.00	7.79	585.00	802.83	802.56	802.42				
KFM09A	20051202 07:55	20051202 08:37	586.00	606.00	607.00	799.67				4940.00	4940.00	4940.54	
KFM09A	20051202 08:58	20051202 10:22	606.00	626.00	7.79	605.00	782.13	781.72	782.27				
KFM09A	20051202 08:58	20051202 10:22	606.00	626.00	627.00	799.67				5089.54	5090.10	5090.64	
KFM09A	20051202 10:43	20051202 12:05	626.00	646.00	7.79	625.00	676.40	675.72	675.99				
KFM09A	20051202 10:43	20051202 12:05	626.00	646.00	647.00	799.67				5235.55	5236.37	5236.93	
KFM09A	20051202 13:12	20051202 14:35	646.00	666.00	7.79	645.00	738.51	737.54	738.10				
KFM09A	20051202 13:12	20051202 14:35	646.00	666.00	667.00	799.67				5379.90	5381.00	5381.55	
KFM09A	20051202 14:57	20051202 16:13	666.00	686.00	7.79	665.00	629.20	628.93	628.51				
KFM09A	20051202 14:57	20051202 16:13	666.00	686.00	687.00	799.67				5521.80	5522.48	5522.89	
KFM09A	20051205 08:22	20051205 09:53	686.00	706.00	7.79	685.00	690.62	692.27	693.92				
KFM09A	20051205 08:22	20051205 09:53	686.00	706.00	707.00	799.67				5660.53	5661.22	5661.49	
KFM09A	20051205 10:10	20051205 11:12	691.00	711.00	7.79	690.00	601.52	600.28	601.38				
KFM09A	20051205 10:10	20051205 11:12	691.00	711.00	712.00	799.67				5695.46	5696.01	5696.01	
KFM09A	20051205 12:46	20051205 13:30	711.00	731.00	7.79	710.00	573.37	572.97	571.87				
KFM09A	20051205 12:46	20051205 13:30	711.00	731.00	732.00	799.67				5832.14	5832.56	5832.42	
KFM09A	20051205 13:49	20051205 15:12	731.00	751.00	7.79	730.00	542.48	542.89	538.49				
KFM09A	20051205 13:49	20051205 15:12	731.00	751.00	752.00	799.67				5968.29	5968.56	5968.83	
KFM09A	20051205 15:30	20051205 16:54	751.00	771.00	7.79	750.00	507.99	507.85	508.41				
KFM09A	20051205 15:30	20051205 16:54	751.00	771.00	772.00	799.67				6104.56	6104.70	6105.24	
KFM09A	20051205 18:09	20051205 19:26	771.00	791.00	7.79	770.00	475.99	476.68	477.78				
KFM09A	20051205 18:09	20051205 19:26	771.00	791.00	792.00	799.67				6234.67	6240.97	6238.92	
KFM09A	20051207 07:32	20051207 08:52	106.00	111.00	7.79	105.00	971.33	973.12	970.79				
KFM09A	20051207 07:32	20051207 08:52	106.00	111.00	112.00	799.67				1005.56	1004.74	1004.87	
KFM09A	20051207 09:08	20051207 10:24	111.00	116.00	7.79	110.00	967.12	971.94	972.08				

idcode	start_date	stop_date	secup	seclow	obs_secup	obs_seclow	pi_above	pp_above	pf_above	pi_below	pp_below	pf_below	comments
KFM09A	20051207 09:08	20051207 10:24	111.00	116.00	117.00	799.67				1047.60	1046.51	1045.41	
KFM09A	20051221 15:48	20051208 17:51	116.00	121.00	7.79	115.00	964.65	964.65	964.65				
KFM09A	20051221 15:48	20051208 17:51	116.00	121.00	122.00	799.67				1078.83	1079.93	1080.48	
KFM09A	20051207 12:52	20051207 14:09	121.00	126.00	7.79	120.00	966.41	970.82	969.72				
KFM09A	20051207 12:52	20051207 14:09	121.00	126.00	127.00	799.67				1131.42	1131.42	1130.87	
KFM09A	20051207 14:26	20051207 16:04	126.00	131.00	7.79	125.00	968.12	965.50	967.15				
KFM09A	20051207 14:26	20051207 16:04	126.00	131.00	132.00	799.67				1172.51	1173.06	1172.51	
KFM09A	20051207 16:21	20051207 17:40	128.00	133.00	7.79	127.00	969.68	969.00	969.54				
KFM09A	20051207 16:21	20051207 17:40	128.00	133.00	134.00	799.67				1189.09	1194.43	1191.69	
KFM09A	20051207 17:58	20051207 19:16	133.00	138.00	7.79	132.00	965.88	969.75	966.44				
KFM09A	20051207 17:58	20051207 19:16	133.00	138.00	139.00	799.67				1231.68	1232.23	1231.68	
KFM09A	20051207 19:42	20051207 21:13	138.00	143.00	7.79	137.00	967.19	968.29	965.53				
KFM09A	20051207 19:42	20051207 21:13	138.00	143.00	144.00	799.67				1272.77	1272.49	1272.77	
KFM09A	20051207 21:27	20051207 22:45	141.00	146.00	7.79	140.00	962.51	962.64	963.33				
KFM09A	20051207 21:27	20051207 22:45	141.00	146.00	147.00	799.67				1297.69	1297.97	1297.42	
KFM09A	20051207 23:02	20051208 00:17	146.00	151.00	7.79	145.00	962.42	962.98	962.42				
KFM09A	20051207 23:02	20051208 00:17	146.00	151.00	152.00	799.67				1339.05	1339.19	1339.05	
KFM09A	20051208 06:16	20051208 06:59	151.00	156.00	7.79	150.00	965.79	965.51	965.37				
KFM09A	20051208 06:16	20051208 06:59	151.00	156.00	157.00	799.67				1381.24	1381.24	1381.24	
KFM09A	20051208 07:10	20051208 08:26	156.00	161.00	7.79	155.00	965.57	965.57	960.62				
KFM09A	20051208 07:10	20051208 08:26	156.00	161.00	162.00	799.67				1422.32	1423.42	1423.42	
KFM09A	20051208 08:36	20051208 09:52	161.00	166.00	7.79	160.00	964.66	962.46	964.66				
KFM09A	20051208 08:36	20051208 09:52	161.00	166.00	167.00	799.67				1464.10	1463.83	1463.42	
KFM09A	20051208 10:03	20051208 11:19	166.00	171.00	7.79	165.00	958.10	962.65	962.65				
KFM09A	20051208 10:03	20051208 11:19	166.00	171.00	172.00	799.67				1508.88	1509.43	1508.88	
KFM09A	20051208 12:12	20051208 13:29	171.00	176.00	7.79	170.00	958.45	958.45	958.45				
KFM09A	20051208 12:12	20051208 13:29	171.00	176.00	177.00	799.67				1549.84	1550.52	1550.52	
KFM09A	20051208 13:43	20051208 14:57	176.00	181.00	7.79	175.00	957.95	957.53	957.53				
KFM09A	20051208 13:43	20051208 14:57	176.00	181.00	182.00	799.67				1590.52	1591.06	1591.61	
KFM09A	20051208 15:13	20051208 16:28	181.00	186.00	7.79	180.00	956.63	956.08	956.08				
KFM09A	20051208 15:13	20051208 16:28	181.00	186.00	187.00	799.67				1631.59	1632.15	1632.69	
KFM09A	20051208 16:36	20051208 17:51	186.00	191.00	7.79	185.00	955.17	954.76	954.62				

idcode	start_date	stop_date	secup	seclow	obs_secup	obs_seclow	pi_above	pp_above	pf_above	pi_below	pp_below	pf_below	comments
KFM09A	20051208 16:36	20051208 17:51	186.00	191.00	192.00	799.67				1673.78	1674.32	1674.88	
KFM09A	20051208 18:03	20051208 18:50	191.00	196.00	7.79	190.00	953.71	953.71	953.71				
KFM09A	20051208 18:03	20051208 18:50	191.00	196.00	197.00	799.67				1714.60	1714.87	1714.87	
KFM09A	20051208 19:02	20051208 19:47	196.00	201.00	7.79	195.00	953.08	952.80	953.35				
KFM09A	20051208 19:02	20051208 19:47	196.00	201.00	202.00	799.67				1755.42	1755.96	1755.96	
KFM09A	20051208 19:57	20051208 20:39	201.00	206.00	7.79	200.00	951.76	951.62	951.35				
KFM09A	20051208 19:57	20051208 20:39	201.00	206.00	207.00	799.67				1796.91	1796.64	1797.05	
KFM09A	20051208 20:58	20051208 21:40	226.00	231.00	7.79	225.00	945.16	945.16	945.16				
KFM09A	20051208 20:58	20051208 21:40	226.00	231.00	232.00	799.67				2002.07	2002.07	2002.49	
KFM09A	20051208 21:54	20051208 23:08	232.00	237.00	7.79	231.00	943.24	942.83	942.96				
KFM09A	20051208 21:54	20051208 23:08	232.00	237.00	238.00	799.67				2050.15	2052.48	2052.90	
KFM09A	20051208 23:21	20051209 00:35	237.00	242.00	7.79	236.00	941.65	941.51	941.51				
KFM09A	20051208 23:21	20051209 00:35	237.00	242.00	243.00	799.67				2091.78	2092.88	2093.43	
KFM09A	20051209 08:08	20051209 09:24	240.80	245.80	7.79	239.80	940.36	940.36	939.81				
KFM09A	20051209 08:08	20051209 09:24	240.80	245.80	246.80	799.67				2119.73	2120.55	2121.37	
KFM09A	20051221 13:55	20051221 14:35	246.80	251.80	7.79	245.80	936.51	936.51	936.51				
KFM09A	20051221 13:55	20051221 14:35	246.80	251.80	252.80	799.67				2155.47	2155.61	2156.43	
KFM09A	20051209 09:40	20051209 10:22	251.50	256.50	7.79	250.50	936.76	936.62	936.49				
KFM09A	20051209 09:40	20051209 10:22	251.50	256.50	257.50	799.67				2208.47	2208.61	2209.02	
KFM09A	20051209 10:34	20051209 11:18	256.50	261.50	7.79	255.50	935.03	935.03	935.03				
KFM09A	20051209 10:34	20051209 11:18	256.50	261.50	262.50	799.67				2248.74	2249.01	2249.01	
KFM09A	20051209 11:30	20051209 13:22	273.00	278.00	7.79	272.00	929.01	929.01	929.01				
KFM09A	20051209 11:30	20051209 13:22	273.00	278.00	279.00	799.67				2384.88	2385.43	2385.98	
KFM09A	20051209 13:34	20051209 14:48	278.00	283.00	7.79	277.00	927.55	927.41	927.55				
KFM09A	20051209 13:34	20051209 14:48	278.00	283.00	284.00	799.67				2423.36	2424.73	2424.87	
KFM09A	20051209 15:04	20051209 15:51	283.00	288.00	7.79	282.00	925.96	925.82	925.54				
KFM09A	20051209 15:04	20051209 15:51	283.00	288.00	289.00	799.67				2463.21	2463.63	2463.77	
KFM09A	20051209 16:00	20051209 17:15	288.00	293.00	7.79	287.00	924.08	924.08	924.08				
KFM09A	20051209 16:00	20051209 17:15	288.00	293.00	294.00	799.67				2504.58	2505.40	2506.50	
KFM09A	20051212 08:21	20051212 09:42	293.00	298.00	7.79	292.00	923.18	923.73	924.83				
KFM09A	20051212 08:21	20051212 09:42	293.00	298.00	299.00	799.67				2542.66	2542.66	2542.66	
KFM09A	20051221 12:39	20051221 13:28	296.00	301.00	7.79	295.00	920.42	920.56	920.42				

idcode	start_date	stop_date	secup	seclow	obs_secup	obs_seclow	pi_above	pp_above	pf_above	pi_below	pp_below	pf_below	comments
KFM09A	20051221 12:39	20051221 13:28	296.00	301.00	302.00	799.67				2558.54	2559.09	2559.63	
KFM09A	20051221 11:45	20051221 12:29	301.00	306.00	7.79	300.00	917.86	917.86	918.42				
KFM09A	20051221 11:45	20051221 12:29	301.00	306.00	307.00	799.67				2595.26	2595.53	2596.35	
KFM09A	20051212 09:58	20051212 10:39	306.00	311.00	7.79	305.00	917.10	916.97	916.41				
KFM09A	20051212 09:58	20051212 10:39	306.00	311.00	312.00	799.67				2648.39	2648.39	2648.39	
KFM09A	20051212 10:49	20051212 12:33	311.00	316.00	7.79	310.00	917.15	917.02	917.15				
KFM09A	20051212 10:49	20051212 12:33	311.00	316.00	317.00	799.67				2687.83	2688.25	2687.83	
KFM09A	20051212 12:43	20051212 13:31	316.00	321.00	7.79	315.00	914.87	914.59	914.59				
KFM09A	20051212 12:43	20051212 13:31	316.00	321.00	322.00	799.67				2728.10	2728.37	2728.37	
KFM09A	20051212 13:44	20051212 15:02	321.00	326.00	7.79	320.00	912.73	910.38	912.04				
KFM09A	20051212 13:44	20051212 15:02	321.00	326.00	327.00	799.67				2767.81	2768.37	2768.91	
KFM09A	20051212 15:31	20051212 16:14	346.00	351.00	7.79	345.00	896.35	896.49	896.49				
KFM09A	20051212 15:31	20051212 16:14	346.00	351.00	352.00	799.67				2966.27	2966.68	2966.68	
KFM09A	20051221 10:04	20051221 11:19	351.00	356.00	7.79	350.00	895.85	895.99	896.13				
KFM09A	20051221 10:04	20051221 11:19	351.00	356.00	357.00	799.67				2999.56	3000.65	3001.75	
KFM09A	20051221 08:54	20051221 09:50	356.00	361.00	7.79	355.00	892.47	892.88	893.02				
KFM09A	20051221 08:54	20051221 09:50	356.00	361.00	362.00	799.67				3037.62	3038.86	3039.00	
KFM09A	20051221 07:28	20051221 08:43	361.00	366.00	7.79	360.00	888.39	889.35	889.35				
KFM09A	20051221 07:28	20051221 08:43	361.00	366.00	367.00	799.67				3071.87	3073.65	3075.70	
KFM09A	20051212 16:39	20051212 17:54	363.00	368.00	7.79	362.00	888.98	888.98	888.98				
KFM09A	20051212 16:39	20051212 17:54	363.00	368.00	369.00	799.67				3099.80	3100.49	3101.45	
KFM09A	20051213 06:27	20051213 07:24	368.00	373.00	7.79	367.00	890.70	890.83	890.83				
KFM09A	20051213 06:27	20051213 07:24	368.00	373.00	374.00	799.67				3141.44	3141.44	3141.44	
KFM09A	20051213 07:35	20051213 08:48	371.00	376.00	7.79	370.00	889.19	889.05	886.43				
KFM09A	20051213 07:35	20051213 08:48	371.00	376.00	377.00	799.67				3165.55	3166.10	3166.65	
KFM09A	20051213 09:02	20051213 09:58	376.00	381.00	7.79	375.00	886.50	883.61	884.98				
KFM09A	20051213 09:02	20051213 09:58	376.00	381.00	382.00	799.67				3205.40	3205.95	3205.54	
KFM09A	20051213 10:10	20051213 11:25	381.00	386.00	7.79	380.00	883.66	881.88	882.98				
KFM09A	20051213 10:10	20051213 11:25	381.00	386.00	387.00	799.67				3244.71	3245.53	3245.53	
KFM09A	20051213 11:57	20051213 13:16	386.00	391.00	7.79	385.00	880.55	880.42	878.75				
KFM09A	20051213 11:57	20051213 13:16	386.00	391.00	392.00	799.67				3283.88	3284.57	3285.52	
KFM09A	20051213 13:28	20051213 14:48	391.00	396.00	7.79	390.00	877.86	875.10	877.86				

idcode	start_date	stop_date	secup	seclow	obs_secup	obs_seclow	pi_above	pp_above	pf_above	pi_below	pp_below	pf_below	comments
KFM09A	20051213 13:28	20051213 14:48	391.00	396.00	397.00	799.67				3324.97	3325.51	3326.07	
KFM09A	20051213 15:06	20051213 15:49	396.00	401.00	7.79	395.00	874.60	873.36	873.09				
KFM09A	20051213 15:06	20051213 15:49	396.00	401.00	402.00	799.67				3363.18	3363.32	3363.32	
KFM09A	20051213 16:00	20051213 17:15	401.00	406.00	7.79	400.00	872.18	869.42	872.18				
KFM09A	20051213 16:00	20051213 17:15	401.00	406.00	407.00	799.67				3403.03	3403.86	3404.40	
KFM09A	20051213 17:25	20051213 18:18	406.00	411.00	7.79	405.00	866.86	868.79	868.52				
KFM09A	20051213 17:25	20051213 18:18	406.00	411.00	412.00	799.67				3442.61	3443.17	3442.75	
KFM09A	20051213 18:36	20051213 19:50	411.00	416.00	7.79	410.00	863.61	865.41	865.96				
KFM09A	20051213 18:36	20051213 19:50	411.00	416.00	417.00	799.67				3480.83	3481.65	3482.20	
KFM09A	20051213 20:06	20051213 21:22	414.00	419.00	7.79	413.00	864.32	864.04	861.56				
KFM09A	20051213 20:06	20051213 21:22	414.00	419.00	420.00	799.67				3504.39	3505.20	3505.76	
KFM09A	20051213 21:32	20051213 22:46	419.00	424.00	7.79	418.00	857.90	857.90	857.35				
KFM09A	20051213 21:32	20051213 22:46	419.00	424.00	425.00	799.67				3542.45	3543.55	3544.11	
KFM09A	20051213 22:55	20051214 00:09	421.00	426.00	7.79	420.00	857.53	856.99	858.09				
KFM09A	20051213 22:55	20051214 00:09	421.00	426.00	427.00	799.67				3558.34	3559.44	3559.99	
KFM09A	20051214 06:51	20051214 07:59	426.00	431.00	7.79	425.00	857.17	853.87	855.53				
KFM09A	20051214 06:51	20051214 07:59	426.00	431.00	432.00	799.67				3597.80	3598.34	3598.34	
KFM09A	20051214 08:11	20051214 09:31	431.00	436.00	7.79	430.00	854.76	854.76	854.07				
KFM09A	20051214 08:11	20051214 09:31	431.00	436.00	437.00	799.67				3641.20	3644.35	3644.35	
KFM09A	20051214 09:47	20051214 10:29	436.00	441.00	7.79	435.00	852.33	852.06	852.06				
KFM09A	20051214 09:47	20051214 10:29	436.00	441.00	442.00	799.67				3683.25	3683.25	3683.25	
KFM09A	20051214 10:44	20051214 12:00	441.00	446.00	7.79	440.00	848.67	848.39	846.74				
KFM09A	20051214 10:44	20051214 12:00	441.00	446.00	447.00	799.67				3719.96	3721.61	3721.61	
KFM09A	20051214 12:13	20051214 14:04	446.00	451.00	7.79	445.00	844.32	845.29	845.83				
KFM09A	20051214 12:13	20051214 14:04	446.00	451.00	452.00	799.67				3760.91	3761.59	3762.15	
KFM09A	20051214 14:22	20051214 15:38	451.00	456.00	7.79	450.00	842.17	842.46	840.53				
KFM09A	20051214 14:22	20051214 15:38	451.00	456.00	457.00	799.67				3797.62	3798.85	3799.95	
KFM09A	20051214 15:55	20051214 17:12	456.00	461.00	7.79	455.00	839.21	837.41	839.07				
KFM09A	20051214 15:55	20051214 17:12	456.00	461.00	462.00	799.67				3836.65	3837.88	3838.84	
KFM09A	20051214 17:32	20051214 18:15	461.00	466.00	7.79	460.00	836.37	836.09	836.51				
KFM09A	20051214 17:32	20051214 18:15	461.00	466.00	467.00	799.67				3875.54	3875.68	3876.10	
KFM09A	20051214 18:35	20051214 19:50	471.00	476.00	7.79	470.00	829.18	829.18	828.08				

idcode	start_date	stop_date	secup	seclow	obs_secup	obs_seclow	pi_above	pp_above	pf_above	pi_below	pp_below	pf_below	comments
KFM09A	20051214 18:35	20051214 19:50	471.00	476.00	477.00	799.67				3952.23	3953.89	3954.98	
KFM09A	20051214 20:01	20051214 21:23	476.00	481.00	7.79	475.00	826.34	826.20	826.07				
KFM09A	20051214 20:01	20051214 21:23	476.00	481.00	482.00	799.67				3992.38	3993.34	3994.43	
KFM09A	20051214 21:40	20051214 22:31	486.00	491.00	7.79	485.00	861.26	860.98	860.98				
KFM09A	20051214 21:40	20051214 22:31	486.00	491.00	492.00	799.67				4070.03	4070.03	4070.03	
KFM09A	20051214 22:58	20051215 00:12	491.00	496.00	7.79	490.00	858.42	856.77	857.32				
KFM09A	20051214 22:58	20051215 00:12	491.00	496.00	497.00	799.67				4108.38	4109.47	4110.02	
KFM09A	20051215 06:33	20051215 07:57	496.00	501.00	7.79	495.00	853.52	852.83	853.11				
KFM09A	20051215 06:33	20051215 07:57	496.00	501.00	502.00	799.67				4145.63	4146.73	4147.83	
KFM09A	20051215 08:14	20051215 09:00	501.00	506.00	7.79	500.00	807.49	807.21	807.76				
KFM09A	20051215 08:14	20051215 09:00	501.00	506.00	507.00	799.67				4184.11	4184.52	4184.52	
KFM09A	20051220 19:00	20051220 20:23	506.00	511.00	7.79	505.00	806.16	806.30	805.75				
KFM09A	20051220 19:00	20051220 20:23	506.00	511.00	512.00	799.67				4220.68	4222.87	4224.52	
KFM09A	20051220 20:50	20051220 22:05	511.00	516.00	7.79	510.00	797.41	794.65	794.38				
KFM09A	20051220 20:50	20051220 22:05	511.00	516.00	517.00	799.67				4262.59	4263.97	4265.06	
KFM09A	20051220 22:14	20051220 23:28	516.00	521.00	7.79	515.00	794.02	794.84	795.67				
KFM09A	20051220 22:14	20051220 23:28	516.00	521.00	522.00	799.67				4299.57	4301.36	4302.86	
KFM09A	20051215 09:25	20051215 10:11	521.00	526.00	7.79	520.00	792.29	792.15	792.57				
KFM09A	20051215 09:25	20051215 10:11	521.00	526.00	527.00	799.67				4337.92	4338.19	4338.47	
KFM09A	20051215 10:26	20051215 11:07	526.00	531.00	7.79	525.00	789.04	788.91	787.80				
KFM09A	20051215 10:26	20051215 11:07	526.00	531.00	532.00	799.67				4375.17	4375.17	4375.73	
KFM09A	20051215 11:23	20051215 12:44	531.00	536.00	7.79	530.00	785.10	782.62	784.14				
KFM09A	20051215 11:23	20051215 12:44	531.00	536.00	537.00	799.67				4416.27	4417.22	4417.36	
KFM09A	20051215 13:19	20051215 14:03	536.00	541.00	7.79	535.00	777.58	777.72	777.17				
KFM09A	20051215 13:19	20051215 14:03	536.00	541.00	542.00	799.67				4454.61	4454.61	4454.61	
KFM09A	20051215 14:14	20051215 15:28	541.00	546.00	7.79	540.00	773.92	773.51	773.51				
KFM09A	20051215 14:14	20051215 15:28	541.00	546.00	547.00	799.67				4492.55	4493.09	4493.50	
KFM09A	20051220 17:14	20051220 17:58	561.00	566.00	7.79	560.00	760.10	760.10	760.52				
KFM09A	20051220 17:14	20051220 17:58	561.00	566.00	567.00	799.67				4643.07	4643.07	4643.07	
KFM09A	20051215 16:19	20051215 17:00	606.00	611.00	7.79	605.00	712.54	712.12	711.58				
KFM09A	20051215 16:19	20051215 17:00	606.00	611.00	612.00	799.67				4977.25	4977.25	4977.25	
KFM09A	20051215 17:19	20051215 18:35	611.00	616.00	7.79	610.00	706.40	706.40	706.26				

idcode	start_date	stop_date	secup	seclow	obs_secup	obs_seclow	pi_above	pp_above	pf_above	pi_below	pp_below	pf_below	comments
KFM09A	20051215 17:19	20051215 18:35	611.00	616.00	617.00	799.67				5014.09	5014.77	5015.04	
KFM09A	20051215 18:50	20051215 19:31	616.00	621.00	7.79	615.00	701.91	701.50	701.50				
KFM09A	20051215 18:50	20051215 19:31	616.00	621.00	622.00	799.67				5051.48	5051.20	5051.76	
KFM09A	20051215 19:44	20051215 21:03	621.00	626.00	7.79	620.00	696.18	695.63	695.63				
KFM09A	20051215 19:44	20051215 21:03	621.00	626.00	627.00	799.67				5087.91	5088.18	5088.45	
KFM09A	20051215 21:14	20051215 22:01	626.00	631.00	7.79	625.00	690.32	690.32	690.32				
KFM09A	20051215 21:14	20051215 22:01	626.00	631.00	632.00	799.67				5124.61	5124.75	5125.17	
KFM09A	20051215 22:08	20051215 23:33	631.00	636.00	7.79	630.00	684.99	684.72	684.45				
KFM09A	20051215 22:08	20051215 23:33	631.00	636.00	637.00	799.67				5160.77	5161.32	5161.87	
KFM09A	20051215 23:43	20051216 00:58	636.00	641.00	7.79	635.00	679.13	678.86	679.13				
KFM09A	20051215 23:43	20051216 00:58	636.00	641.00	642.00	799.67				5197.61	5198.02	5198.02	
KFM09A	20051216 08:21	20051216 09:36	641.00	646.00	7.79	640.00	672.72	672.72	672.72				
KFM09A	20051216 08:21	20051216 09:36	641.00	646.00	647.00	799.67				5232.40	5233.08	5233.64	
KFM09A	20051216 09:55	20051216 10:38	646.00	651.00	7.79	645.00	667.82	667.68	667.95				
KFM09A	20051216 09:55	20051216 10:38	646.00	651.00	652.00	799.67				5270.33	5270.33	5270.89	
KFM09A	20051216 10:53	20051216 12:10	651.00	656.00	7.79	650.00	661.82	661.53	661.53				
KFM09A	20051216 10:53	20051216 12:10	651.00	656.00	657.00	799.67				5307.04	5307.32	5307.04	
KFM09A	20051216 12:21	20051216 13:20	656.00	661.00	7.79	655.00	655.67	655.67	655.67				
KFM09A	20051216 12:21	20051216 13:20	656.00	661.00	662.00	799.67				5343.20	5343.20	5343.20	
KFM09A	20051216 13:31	20051216 14:14	661.00	666.00	667.00	799.67	649.39	649.39	649.26				
KFM09A	20051216 13:31	20051216 14:14	661.00	666.00	667.00	667.00				5379.36	5379.22	5379.36	
KFM09A	20051219 08:19	20051219 09:01	731.00	736.00	7.79	730.00	557.22	556.94	556.66				
KFM09A	20051219 08:19	20051219 09:01	731.00	736.00	737.00	799.67				5867.48	5867.48	5867.48	
KFM09A	20051219 09:15	20051219 09:56	736.00	741.00	7.79	735.00	548.59	548.59	548.59				
KFM09A	20051219 09:15	20051219 09:56	736.00	741.00	742.00	799.67				5902.00	5902.13	5902.00	
KFM09A	20051219 10:11	20051219 11:30	741.00	746.00	7.79	740.00	541.76	539.98	539.98				
KFM09A	20051219 10:11	20051219 11:30	741.00	746.00	747.00	799.67				5936.37	5936.51	5936.51	
KFM09A	20051219 11:44	20051219 12:36	746.00	751.00	7.79	745.00	533.55	533.55	533.55				
KFM09A	20051219 11:44	20051219 12:36	746.00	751.00	752.00	799.67				5970.48	5970.48	5970.48	
KFM09A	20051219 12:50	20051219 14:05	751.00	756.00	7.79	750.00	524.93	524.11	524.93				
KFM09A	20051219 12:50	20051219 14:05	751.00	756.00	757.00	799.67				6004.58	6006.09	6005.00	
KFM09A	20051219 14:20	20051219 15:42	756.00	761.00	7.79	755.00	516.73	516.32	516.87				

idcode	start_date	stop_date	secup	seclow	obs_secup	obs_seclow	pi_above	pp_above	pf_above	pi_below	pp_below	pf_below	comments
KFM09A	20051219 14:20	20051219 15:42	756.00	761.00	762.00	799.67				6038.00	6038.40	6038.40	
KFM09A	20051219 15:56	20051219 17:16	761.00	766.00	7.79	760.00	509.21	508.11	507.70				
KFM09A	20051219 15:56	20051219 17:16	761.00	766.00	767.00	799.67				6071.83	6074.02	6072.38	
KFM09A	20051220 06:55	20051220 08:10	766.00	771.00	7.79	765.00	498.80	498.66	498.52				
KFM09A	20051220 06:55	20051220 08:10	766.00	771.00	772.00	799.67				6105.65	6105.52	6105.79	
KFM09A	20051220 08:29	20051220 09:46	771.00	776.00	7.79	770.00	489.90	490.04	489.90				
KFM09A	20051220 08:29	20051220 09:46	771.00	776.00	777.00	799.67				6138.67	6139.76	6139.21	
KFM09A	20051220 10:06	20051220 11:24	776.00	781.00	7.79	775.00	481.56	480.73	479.08				
KFM09A	20051220 10:06	20051220 11:24	776.00	781.00	782.00	799.67				6172.08	6172.35	6172.08	
KFM09A	20051220 11:35	20051220 12:58	781.00	786.00	7.79	780.00	469.90	470.18	471.01				
KFM09A	20051220 11:35	20051220 12:58	781.00	786.00	787.00	799.67				6204.54	6207.14	6206.04	
KFM09A	20051220 13:11	20051220 14:28	786.00	791.00	7.79	785.00	462.38	462.38	462.38				
KFM09A	20051220 13:11	20051220 14:28	786.00	791.00	792.00	799.67				6240.56	6243.85	6240.01	
KFM09A	20051118 13:32	20051118 14:28	506.00	606.00	7.79	505.00	789.23	789.09	789.23				Incomplete test, interrupted and re-performed later.
KFM09A	20051118 13:32	20051118 14:28	506.00	606.00	607.00	799.67				4942.10	4943.06	4942.65	Incomplete test, interrupted and re-performed later.
KFM09A	20051130 17:10	20051130 18:03	426.00	446.00	7.79	425.00	855.53	855.39	854.97				Incomplete test, interrupted and re-performed later.
KFM09A	20051130 17:10	20051130 18:03	426.00	446.00	447.00	799.67				3726.67	3728.72	3728.72	Incomplete test, interrupted and re-performed later.
KFM09A	20051207 10:38	20051207 12:39	116.00	121.00	7.79	115.00	970.07	969.51	970.07				Incomplete test, interrupted and re-performed later.
KFM09A	20051207 10:38	20051207 12:39	116.00	121.00	122.00	799.67				1088.56	1088.70	1088.70	Incomplete test, interrupted and re-performed later.